

1768

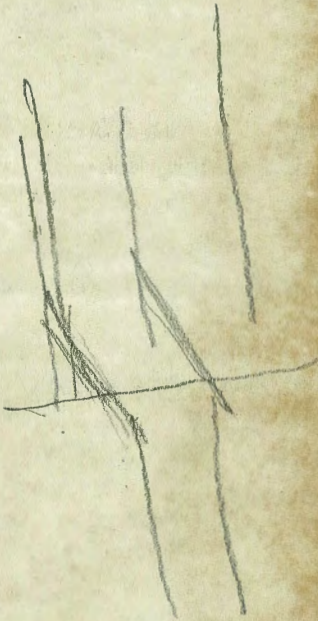


1768

MICROFILMED

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CITY ENGINEER'S OFFICE



MADE IN U. S. A.

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CHICAGO

Cross Section Grape St. 33rd to Fallon 2-5

Cross Section Meade Ave 35th to 40th St. 6-25

" " Wash. at 5th 26-27

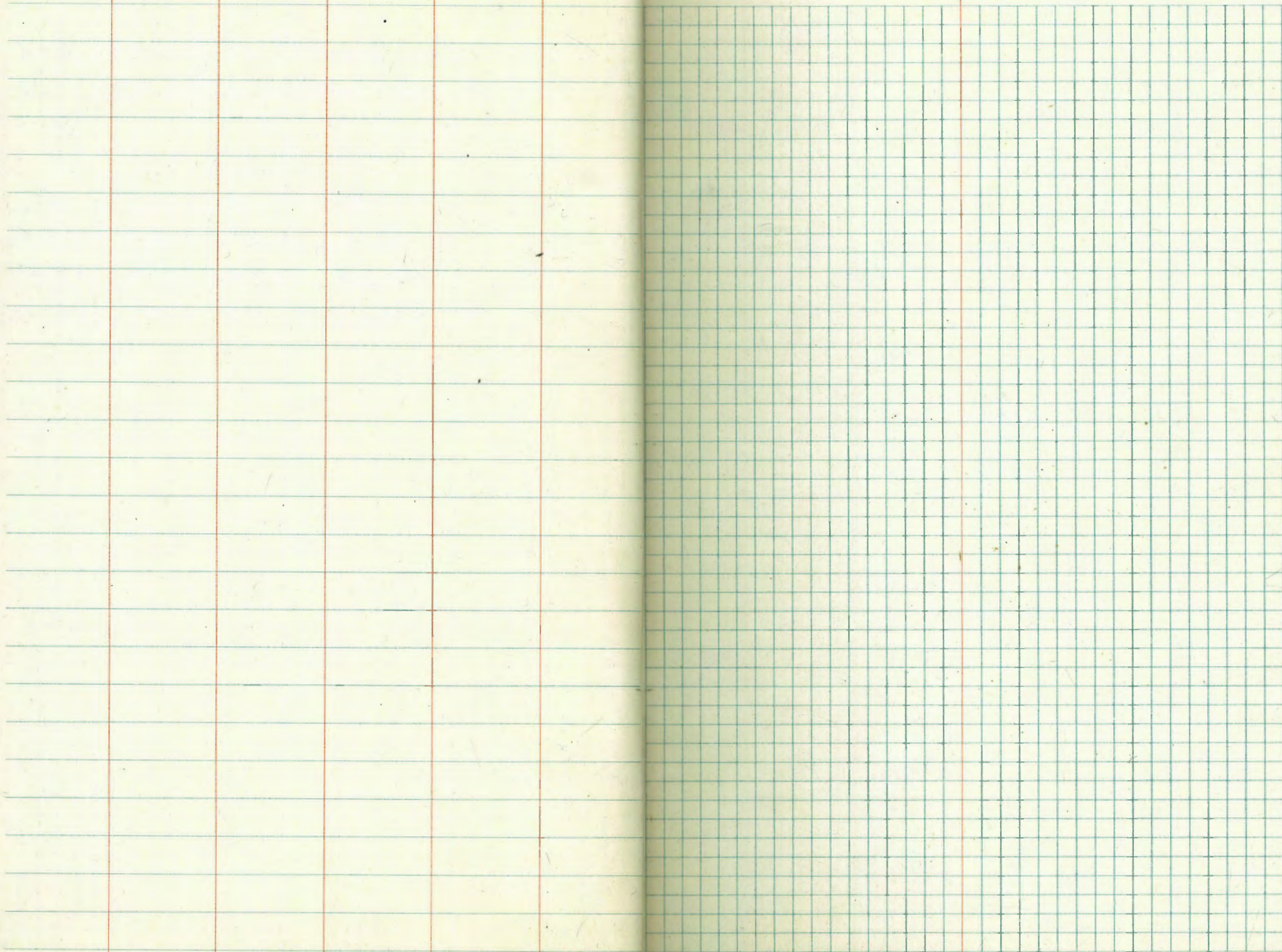
" " 63rd along Callwood Park 28-33

" " San Rafael Place Mission Blvd East 34-37

" " Pershing Dr at Florida 38-52

" " Hawk - Sutter South 58-63

" " Alley BIK. 58 O.B. 64-76

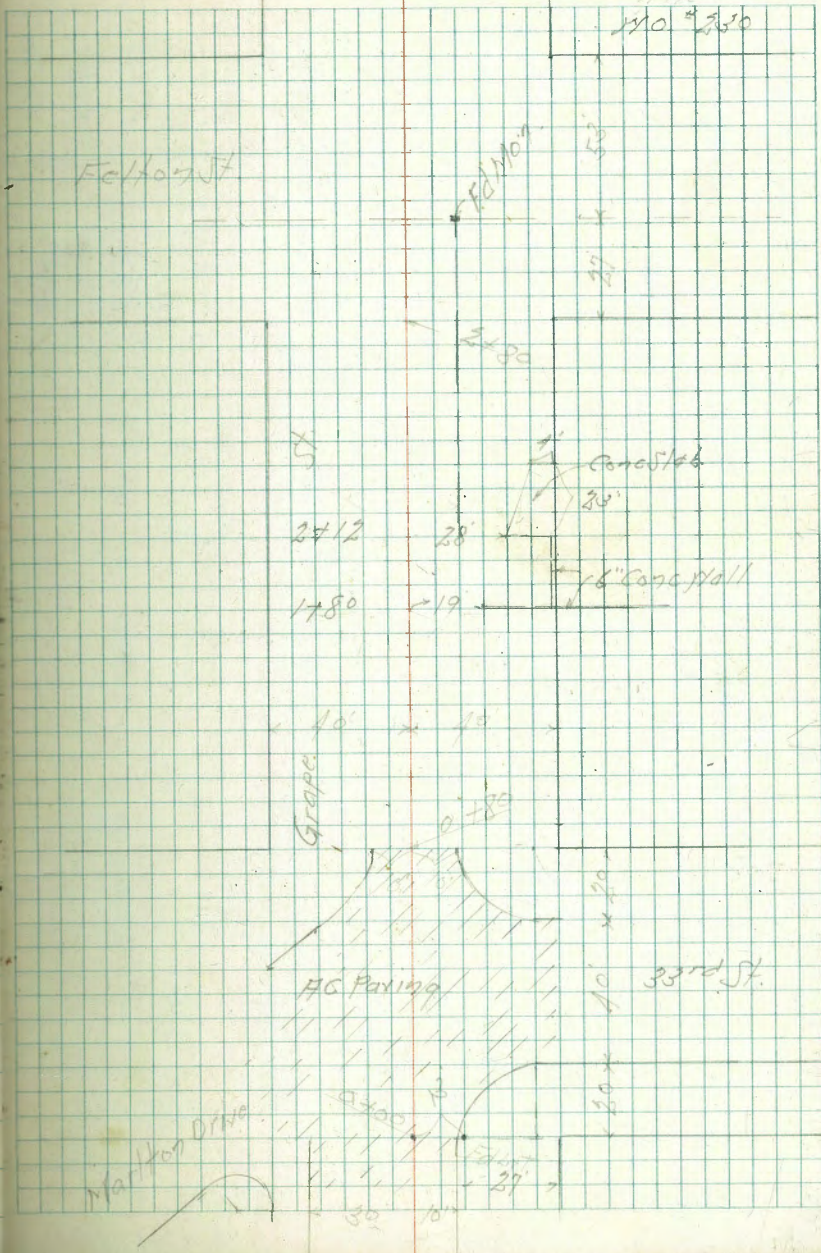


Cross Section Grape St.
33rd St to Felton St
Levels next page

Indexed
c.s.R.

March 19-47
Sisson
McCoy
Maddal
Filion
MO 2330

2



Cross Section, Grapes Pt.
3rd St to Fallon St.

Indexed
C.S.K.

LT-11

pt. 5

3

+80 = E.L. 3rd St to South = Fly Improvements

+60

+40

+20

0+0 = N.L. 3rd St

BM

TP

BM

4.85

266.02

LT-11
3rd St
270.87

270.87

893

870.45

270.87

279.38

276.96

S.M.B.P.
Grapes 3rd St

175 10	263.1	253.4	10.5	261.87
188 10	263.36	257.1	10.5	261.41
88 15	262.96	262.11	10.5	262.17
90 10	263.42	261.87	10.5	262.17
94 10	263.14	261.41	10.5	262.17
81 10	263.42	262.17	10.5	262.17
84 10	263.48	262.38	10.5	262.38
78 10	264.52	263.0	10.5	263.0
74 10	265.17	263.15	10.5	263.15
78 10	264.18	264.18	10.5	264.18
72 10	264.23	264.23	10.5	264.23
68 10	264.77	265.65	10.5	265.65
62 10	264.82	264.82	10.5	264.82
58 10	265.77	265.77	10.5	265.77
52 10	264.47	264.47	10.5	264.47
48 10	264.92	264.92	10.5	264.92
42 10	264.77	264.77	10.5	264.77
38 10	264.90	264.90	10.5	264.90
32 10	264.92	264.92	10.5	264.92
28 10	265.56	265.56	10.5	265.56
22 10	265.32	265.32	10.5	265.32
18 10	266.05	266.05	10.5	266.05
12 10	265.82	265.82	10.5	265.82
8 10	265.61	265.61	10.5	265.61
4 10	265.19	265.19	10.5	265.19
0 10	264.59	264.59	10.5	264.59

+80 = 1/2 Feltan St

TP 0.16 222.89 12.65 222.73

+30

0.71 225.38 12.43 224.67

0.76 247.10 12.93 246.34

2+12

+80

+53 1/2 of 1/2 Sly Power Pole

+50

TP 0.49 259.27 12.00 258.78

1+0

270.87

184.5
181.1
17.4
298
40
173.1

202.9
201.5
1.4
215.8
40
175.8

235.38

206.2
205.1
1.1
221.6
40
219.6
232.4
22.2
11.8

216.8
215.5
1.3
227.7
40
223.7
232.4
250.2
9.1
250.6
8.7
19.1

221.9
220.4
1.5
231.0
40
227.0
244.3
15.0
253.4
5.9
255.4
8.0
19.0

228.5
227.4
1.1
246.5
40
245.1
260.9
13.0
261.5
9.4
19.0

270.87

214.0
214.0
0
220.5
21.0
220.0
215.7

223.9
223.9
0
233.4
2.0
244.4
220.0
24.0
244.4
2.0
220.0
24.0
215.7

247.5
247.5
0
247.5
12.8
246.34
12.8
244.49
12.8
244.49

251.4
251.4
0
251.4
251.4
251.4
251.9
251.9
251.9
251.9
251.9

255.4
255.4
0
255.4
255.4
255.4
255.4
255.4
255.4
255.4
255.4

261.6
261.6
0
261.6
261.6
261.6
261.6
261.6
261.6
261.6
261.6

Grapa St.

Lt N

S

Rt S

5

BM

9.91

20594

13 May 24
Grapa St
Fetter

J+07

176.7
39.2
75

187.7
58.2
40

2031.4
12.5

216.7
70.8
40

224.9
78.0
65

TP

5.65

215.85

12.69

210.20

215.85

222.89

Cross Section Meade Tr. 40th St. West to 35th St.

1+40 = W.L. Alley

1+32.5 = E. Alley

1+25 = E.L. Alley

1+0

0+50

0+0 = W.L. 40th St. See #1746-35

BM 3.45 37333

369.88

#1746-35
Meade Tr.
40th St.
#1746-35

Notes Reduced and checked
4/17/47 by R.E. Coburn.

Indexed
C.S.K.

Lt=5

±

Rt=N

April 15 1947

6

J.S.S. 07
McCo
Haddel
Hiley
N.O. #60108

368.54

499
258

368.36

499
258

368.41

499
258

367.96

537
258

368.43

490
18

368.82

451

368.93

440
13

369.06

427
258

369.58

480
258

369.77

538
258

369.91

544
258

368.17

518
258

367.90

518
258

368.38

495
15

368.81

452

368.93

440
13

369.02

431
258

369.65

468
258

368.53

480
258

368.31

480
258

368.37

491
258

367.90

540
258

368.38

495
15

368.87

446

368.96

437
13

369.02

430
258

369.64

539
258

369.78

537
258

369.98

545
258

368.36

497
258

367.86

540
258

368.33

560
13

368.86

447

369.02

431
13

369.12

421
258

369.74

355
258

368.17

516
258

367.68

565
258

368.27

506
13

368.81

458

369.01

432
13

369.07

426
258

369.63

370
258

BM

358

369.75

✓
NORP
Mead
32754
36975

2195 = 2 of 39 1/2 ft.

2175 = F.C. of 39 1/2 ft.

2165 = F.L. 39 1/2 ft.

2150

210

1+50

37000 ✓

Lt.

+

pt.

369.09

369.13

369.28

369.34

369.43

369.54

369.69

421
130

430
139

405
135

599

590
13

579
137

578
138

368.98

368.36

368.48

368.62

368.81

368.86

368.97

369.07

369.57

435
135

427
137

485
139

421
13

452

447
13

438
137

426
138

376
138

368.91

368.83

368.82

369.07

369.02

368.86

369.47

447
137

500
139

461
13

428

431
13

447
137

536
137

368.92

368.33

368.63

368.99

369.07

368.88

369.40

441
137

500
139

470
13

434

431
13

445
138

593
138

368.13

368.51

368.83

368.96

368.87

369.40

520
138

483
13

450

457
137

445
138

593
138

368.40

367.97

368.44

368.88

368.96

368.99

369.55

473
137

526
139

489
13

475

457
137

451
138

578
138

37000 ✓

B

2

14325 = 2 H/10x

2

1425 = F.L. H/10x

TP 6.24 377.83 179 371.59 ✓

2

170

2

0750

2

0709
37257 = W.L. 39/15x

1

3715 = H.C. of 39/15x

373.33 ✓

370.68	370.45	370.82	371.11	371.17	371.14	371.45
7.5 10	7.33 25.9	7.01 13	6.22	6.65 13	6.69 25.7	6.38 10

370.72	370.96	370.41	370.78	371.12	371.19	371.09	371.65	371.59	371.83
6.9 10	5.97 25.9	7.43 23.9	7.05 13	6.71	6.64 13	6.24 23.7	6.18 26.7	6.11 25.1	6.00 20.23

370.55	370.00	370.40	370.82	370.83	370.63	371.18
7.28 13.9	5.63 26.9	7.23 13	2.57	2.50 13	2.70 23.7	2.15 25.7

369.83	369.36	369.63	370.02	370.08	369.86	370.38
3.30 25.9	3.27 25.9	3.70 13	3.31	3.25 13	3.13 23.7	2.95 26.7

369.08	368.69	369.01	369.20	369.12	369.00	369.57
4.25 26.9	4.61 26.9	4.33 13	4.13	4.21 13	4.33 23.7	3.26 26.7

368.16	368.59	368.69	368.78	368.90	368.93	368.95	369.12	369.71
4.17 26.9	4.14 26.9	4.69 26.9	4.65 13	4.45	4.40 13	4.38 25.7	4.21 26.9	3.62 26.23

373.33 ✓

2+75.15 = F.C. 6.0% 3873.54

2+65.15 = F.L. 3873.54

2+50

2+0

1+50

1+40 = 21/11/10

377.83

372.89	372.30	372.46	372.83	373.15	373.24	373.41	373.40	373.93
--------	--------	--------	--------	--------	--------	--------	--------	--------

491 75 48	5.53 70 804	5.39 26.9	5.00 13	4.68	4.39 13	4.28 25.9	4.13 70 54	3.90 10.66
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372.78	372.15	372.70	373.13	373.17	373.13	373.77
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5.03 23.9 16	5.70 25.9 54	5.15 13	4.70	4.66 13	4.70 25.9 54	4.06 26.9 86
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372.62	372.03	372.55	372.96	373.06	372.93	373.60
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5.27 23.9	5.80 23.9	5.38 13	4.87	4.77 13	4.90 23.9	4.23 23.9
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372.02	371.29	371.83	372.15	372.28	372.14	372.73
--------	--------	--------	--------	--------	--------	--------

5.8 23.9	6.64 23.9	6.00 13	5.68	5.58 13	5.69 23.9	5.10 23.9
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371.30	370.71	371.09	371.50	371.54	371.34	371.94
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5.53 23.9 2	7.12 23.9 54	6.71 13	6.33	6.39 13	6.49 23.9 54	5.89 23.9 23
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371.35	371.00	370.88	370.57	370.93	371.27	371.36	371.44	371.92	371.60	372.08
--------	--------	--------	--------	--------	--------	--------	--------	--------	--------	--------

6.48 10.66	6.88 10.66	6.95 23.9 54	7.26 23.9 54	6.90 13	6.56	6.47 13	6.69 23.9 54	6.91 23.9 54	6.20 10.66 54	5.85 10.66
---------------	---------------	--------------------	--------------------	------------	------	------------	--------------------	--------------------	---------------------	---------------

377.83

1+25 F.L. Alley

1+0

0+50

0+00
2+25.157 = M.L. 38¹/₂ St.

B.M.

353

374.30

NOV 89
Meade
38¹/₂ St.
374.88

2+12.15 = M.C. 38¹/₂ St.

2+95.15 = 38¹/₂ St.

377.85 ✓

374.99 28 299 15	374.91 30 301	374.63 28 28	374.21 30 301	374.54 30 301	374.94 29 29	374.95 28 28	374.88 28 28	375.34 28 28	375.26 28 28	375.58 28 28
374.39 34 34	373.86 37 37	374.30 35 35	374.77 36 36	374.82 30 30	374.63 30 30	375.18 36 36				
373.94 38 38	373.47 38 38	373.82 40 40	374.25 35 35	374.36 34 34	374.22 36 36	374.85 38 38				
373.28 45 45	372.81 50 50	373.25 45 45	373.68 45 45	373.79 40 40	373.71 45 45	374.32 45 45				
373.23 40 40	372.66 51 51	372.79 50 50	373.07 47 47	373.78 45 45	373.48 43 43	373.59 43 43	373.71 43 43	374.27 43 43		
372.91 47 47	372.93 49 49	373.11 47 47	373.46 43 43	373.85 48 48	373.66 47 47	373.85 48 48				
				377.85 ✓						

2+65 = EL McClintock

2+50

2+0

TP

7.00

382.98 ✓

1.85

375.98 ✓

1+50

1+40 = W.L. Hilley

1+36

16. R. Holtz - 7.2 x 2
S.D. Saur Co. Manhole

2.91

El. 374.92

Top of
Manhole

1+32.5

W.L. Hilley

377.83 ✓

376.34 375.76 376.04 376.27 376.20 376.02 376.59

6.54 7.22 6.91 6.71 6.78 6.98 6.59
26 26 15 15 15 25 26.5
541 541 541 541 541 541 541

376.25 375.58 375.81 376.25 376.18 375.91 376.52

6.73 7.10 7.11 6.73 6.80 7.07 6.51
26 26 15 15 15 26.5 26.5

375.58 375.04 375.30 375.66 375.54 375.38 376.08

7.10 7.91 7.68 7.32 7.47 7.60 6.98
26 26 15 15 15 26.5 26.5

375.01 374.47 374.81 375.24 375.08 375.06 375.68

2.83 3.52 3.02 2.59 2.75 2.79 2.15
26.5 26.5 15 15 15 26.5 26.5

375.28 375.01 374.91 374.33 374.72 375.14 375.13 374.97 375.61 375.38 375.74

2.58 2.82 2.99 3.50 3.11 2.69 2.70 2.86 2.42 2.48 2.00
26 26 26 26 15 15 15 26.5 26.5 26 26.5

374.75 374.31 374.59 374.96 374.94 374.88 375.17

3.08 3.52 3.24 2.89 2.80 2.95 2.66
26 26 15 15 15 26.5 26.5

377.83 ✓

170

0750

0405

37257 - WL McClintock

BM 814 38541 568

2713 - WCB McClintock

2795 - J McClintock

2777 - FCB McClintock

38298

378.67 377.80 378.38 378.89 379.09 378.89 379.52

689 764 706 655 635 635 597
279 279 14 14 14 276 376.28
WCB

377.81 377.83 377.70 378.12 378.14 378.02 378.54

763 821 774 732 700 728 690
279 279 14 14 14 276 276

377.00 376.47 376.83 377.13 377.09 376.89 377.35

841 897 841 831 835 853 809
279 279 14 14 14 276 276
WCB

376.86 376.34 376.44 376.70 376.84 376.83 376.79 376.69 377.21

613 664 654 628 614 615 610 629 577
276 276 279 14 14 14 276 276 276
WCB

376.60 376.54 376.52 376.64 376.60 376.64 376.95

638 641 641 634 638 624 603
276 276 276 14 14 276 276

376.33 375.84 375.99 376.18 376.43 376.35 376.17 376.09 376.53

665 714 699 680 655 663 681 646
276 276 276 14 14 14 276 276
WCB

38298

1771 = W.C. of 37th St to North

1753 = 37th to North

1740 = W.L. Alley to South

1735 = E.C. of 37th to North

1725 = Alley to South

1725 = E.L. Alley

38544 ✓

377.32	379.76	379.24	379.82	379.87	379.79	379.84	380.20
6.18 27.9 W.C.	6.68 27.9 W.C.	6.20 14	5.62	5.57 14	5.65 27.6	5.58 27.6 W.C.	5.72 27.6

377.69	379.64	379.14	380.17
5.75	5.80 14	5.70 27.6	5.87 27.6

379.46	379.09	379.04	378.51	378.98	379.43
5.88 27.6 W.C.	6.35 27.9 W.C.	6.40 27.9 W.C.	6.23 27.9 W.C.	6.16 14	6.01

379.34	379.51	379.50	379.45	379.99
6.10	5.93 14	5.91 27.6	5.90 27.6 W.C.	5.75 27.6

378.63	378.40	378.86	379.30
5.81 27.6	5.01 27.9	6.58 14	6.14

378.94	378.62	378.79	378.21	378.74	379.25	379.39	379.36	379.87
6.50 27.6	6.82 27.6 W.C.	6.65 27.9 W.C.	7.22 27.9 W.C.	6.70 14	6.19	6.83 14	6.68 27.6 W.C.	5.67 27.6 W.C.

38544 ✓

2+05.10 = 2 37¹/₂ ft to South

2+77.10 = FC 37¹/₂ to South

2+65.10 = FL 37¹/₂ to South

+52 10' 1/2 off = 2 2 1/2 5.07
50.905 19.11

2+50

2+0

1183 = 11 1/2 37¹/₂ to North

385 11 ✓

381.40	381.37	381.35	381.52	381.55	381.41
1.04	1.12	1.09	3.92	3.89	4.03
20	279	11		14	276

380.81	380.34	380.39	380.81	381.24	381.19	380.92	381.48
4.63	5.08	5.05	4.63	4.20	4.25	4.52	3.96
20.8	20.8	279	11		14	276	276

380.71	380.13	380.55	381.04	381.50	380.84	381.35
4.72	5.31	4.89	4.40	4.44	4.60	4.09
279	279	11		14	276	276

380.41	379.84	380.31	380.79	380.78	380.63	381.15
5.03	5.60	5.63	4.65	4.66	4.81	4.39
279	279	11		14	276	276

379.86	379.46	379.79	380.12	380.27	379.99	380.55
5.58	5.28	5.71	5.32	5.17	5.45	4.89
279	279	11		14	276	276

379.58	378.88	379.45	379.92	379.99	379.82	380.38
5.86	6.56	5.99	5.52	5.25	5.62	5.06
279	279	11		14	276	276

385 11 ✓

Top of
Manhole

1+02.50 = F.L. Cherokee to North

0+50

0+05
3745.10 = W.L. 37 1/2 South

IP 6.62 389.69 2.27 382.07

3+33.10 = W.C. 37 1/2 St to South

3+22.5 = W.L. Hilcy to North

3+20 10' R/O 17' 22' 2 3.71 El. 381.73 Top of Main Hole

37.15 = Hilcy to North

385.11

382.26 6.43 279 14	382.48 7.21 279 14 Sub	382.89 8.80 14	383.23 6.46	383.15 6.54 14	383.01 6.68 276 14 Sub	383.68 6.01 276 14			
	381.97 7.75 278 14 Sub	382.38 7.31 14	382.79 6.90	382.71 6.98 14	382.42 7.37 278 14	382.97 6.78 278			
	382.14 7.45 279	381.54 8.10 279	381.86 7.83 14	382.20 7.49	382.09 7.60 14	381.75 7.94 276	382.31 7.58 278		
	381.20 3.24 40:06	381.53 3.91 10:06 Sub	381.68 3.76 279	381.75 3.69 14	382.16 3.38	381.97 3.47 14	381.72 3.77 276 Sub	382.26 3.18 276 14	
	381.70 3.74 40	381.67 3.77 279	381.66 3.78 14	381.93 3.57	381.78 3.66 14	381.68 3.76 276 Sub	382.10 3.54 276 14 Sub	382.14 3.70 40:06 Sub	382.39 3.05 40:06
	381.60 3.84 40	381.58 3.86 279	381.52 3.92 14	381.75 3.69	381.68 3.76 14	381.56 3.88 278	381.74 3.90 40		

385.11

1+62.5 = W.L. Cherokee North

B.M.

544

384.25

✓ N.W.B.P.
Meade Hvc
Cherokee North
384.14

1+50 = W.C. Cherokee North

1+40 = W.L. Filley to South

384.02

567
40.05

1+32.5 = E Cherokee North

1+25 = E L. Filley to South

383.75

594
40.01

1+15 = E.C. Cherokee North

389.69 ✓

383.93 383.23 383.52 383.83 383.74 383.74 384.33

576 546 617 586 595 595 536
278 278 14 14 14 14 278
15 15 14 14 14 14 15

383.71

383.65

383.63

383.66

384.22

598

604

606

608

537

14

276

40

40
54

383.75

383.49

383.04

383.27

383.59

383.54

383.66

383.87

594

630

662

643

610

615

603

582

14

278

279

14

14

14

276

40

383.49

382.92

383.15

383.53

383.50

383.43

630

635

654

616

619

626

584

14

279

14

14

14

276

40

383.43

383.59

382.84

383.12

383.40

383.43

383.30

383.63

626

610

683

657

629

636

629

606

14

279

279

14

14

14

276

40

383.45

382.68

383.05

383.25

383.32

383.13

383.29

382.63

624

781

689

634

633

656

640

606

279

279

14

14

14

276

40

40
54

389.69 ✓

2 + 952 = Cherokee South

2 + 895 = F.L. Alley North

2 + 772 = F.C. Cherokee South

2 + 652 = F.L. Cherokee South

2 + 50

2 + 0

384.92	384.73	384.70	384.96	384.87	384.49	384.92
477 40	496 278	499 14	473	488 14	520 27.5	472 40
			384.93	384.81	384.37	384.87
			476	488 14	532 27.5	482 27.5
					541 34	497 40
						467 40
						385.02
			384.93	384.36	384.52	384.59
476 40	532 40	517 278	510 14	487	493 14	534 27.5
						481 27.5
						384.88
			384.93	384.47	384.45	384.74
			468 278	523 278	524 14	495
						513 14
						546 27.5
						480 27.5
						384.89
			384.96	384.28	384.25	384.54
473 278	541 278	544 14	515		384.49	384.11
					530 14	558 27.5
						488 27.5
						384.81
			383.61	383.85	384.19	384.19
			508 278	587 14	550	550 14
						583 27.5
						370 27.5
						384.59

589.69 ✓

589.69 ✓

1715 = EC6 36th N17025 = E.L. 36th St North

0750

040 J
372527 = W.L. Cherokee South

3132 = W.C. Cherokee South

37045 = W.L. Filly North

38969 ✓

Lt.

J

Pt.

18

				385.88	385.76	385.52	385.52	386.01
				381	4.23	4.17	4.17	3.68
					14	27.5	27.5	20.25
							201	
				385.90	385.24	385.57	385.87	385.75
				382	3.97	4.29	4.29	3.59
				23.8	27.8	14	27.5	27.5
								386.10
				385.51	384.99	385.23	385.48	385.36
				388	4.70	4.4	4.21	4.33
				22.8	27.8	14	14	27.5
								385.01
								385.57
				385.36	384.80	384.88	385.14	385.00
				4.33	4.87	4.81	4.55	4.69
				27.8	27.8	14	14	27.5
					5.01		5.07	4.50
							27.5	27.5
				385.32	384.69	384.76	384.86	385.28
				4.37	5.00	4.93	4.83	4.61
				27.8	40.5	27.8	14	14
					5.01			4.69
								5.15
								27.5
								27.5
								384.54
								385.13
				384.84	384.86	384.80	385.05	385.00
				4.85	4.83	4.89	4.64	4.69
				27.8	27.8	14	14	14
								5.08
								4.58
								27.5
								27.5
								4.62
								4.37
								4.00
								385.06
								385.42

38959 ✓

270

1+62.5 = W.L. 36th St North

TP 6.31 392.69 ✓ 3.31 586.38 ✓

1730 = W.C. 36th North

1740 = W.L. Alley South

1+32.5 = W.L. 36th North

1725 = F.L. Alley South

389.69 ✓

386.52 385.95 386.04 386.24 386.31 386.08 386.59

419 674 465 645 638 581 610
278 278 278 278 278 278 278
Sun Sun Sun Sun Sun Sun Sun

386.34 385.72 385.81 386.19 386.19 385.91 386.37

435 499 688 650 650 578 632
278 278 278 278 278 278 278
Sun Sun Sun Sun Sun Sun Sun

382.69 ✓

386.12 386.00 385.90 385.89 386.28

557 519 570 588 521
278 278 278 278 278
Sun Sun Sun Sun Sun

386.38 386.06 386.12 385.66 385.65 385.96 386.03 385.84 386.22

532 363 327 408 404 573 566 585 547
278 278 278 278 278 278 278 278
Sun Sun Sun Sun Sun Sun Sun Sun

386.05 385.67 385.64 385.94 385.97 385.81 386.27

364 302 495 575 572 588 540
278 278 278 278 278 278 278
Sun Sun Sun Sun Sun Sun Sun

386.47 386.13 386.28 385.59 385.66 385.91

356 341 410 405 378
278 278 278 278 278
Sun Sun Sun Sun Sun

389.69 ✓

37045 = W.L. Alley North

387.19 387.10 386.80 387.22 387.16 387.41
 550 550 539 539 551 539
 27.5 27.5 27.5 27.5 27.5 27.5

2795 = E.L. 36th to South

386.57 386.60 386.66 387.12 387.05 386.81 387.03
 548 609 683 537 539 588 566
 27 27.8 27.8 27 27.5 27.5 27

27895 = E.L. of Alley to North

387.02 386.93 386.76 387.18 387.19 387.51
 537 537 530 531 530 510
 27.3 27.3 27.5 27.5 27.5 27.5

2777 = E.C. 36th South

386.67 386.16 386.32 386.52 386.79 386.79 386.65 387.18
 503 653 639 619 590 590 604 636
 27.5 27 27.8 27 27.5 27.5 27.5 27.5

2765 = E.L. 36th to South

386.87 386.25 386.46 386.76 386.74 386.55 387.04
 588 640 630 590 595 614 665
 27.8 27.8 27 27 27.5 27.5 27.5

2750

386.75 386.21 386.42 386.56 386.66 386.43 387.01
 594 618 627 613 603 626 568
 27.5 27.8 27 27 27.5 27.5 27.5

392.69 ✓

392.69 ✓

1725 = F.L. Hill/ South

1715 = F.C. Wilson

1702.50 = F.L. Wilson to North

0750

0700
37257 = W.L. 36 1/2 South

3713 = W.L. 36 1/2 South

39269 ✓

387.90 470 103 5	387.71 199 28	387.74 195 275 5	387.25 511 295 5	387.49 520 295 5	387.91 138
				387.87 482	387.93 477
					387.86 480 275
					387.85 476 275
					388.25 441 275
	387.56 519 275	386.95 524 275	387.32 529 275	387.85 484	387.79 490 275
					387.65 501 275
					388.09 460 275
	387.35 524 275	386.79 520 275	387.01 568 275	387.46 523	387.46 523 275
					387.16 553 275
					387.64 505 275
	387.20 529 275	386.65 502 275	386.89 521 275	387.34 538	387.17 552 275
					386.85 524 275
					387.35 524 275
	387.12 557 275	386.49 520 275	386.66 523 275	386.82 527 275	387.24 545
					387.16 553 275
					386.81 538 275
					387.24 545 275

39269 ✓

2+51 9.5 N of 2-2324 4.67 El. 387.55 top

2+50

2+0

1+62.5 = W.L.W. 1507

BM 3.75 392.22 4.22 388.47 ✓ NWBP Meade & Wilson 388.20

1+51 = W.C. Wilson North

1+40 = W.L. Hilley South

1+325 = W. Wilson North

392.69 ✓

387.87 387.36 387.53 387.72 387.80 387.59 388.12

4.35 4.86 4.69 4.50 4.43 4.63 4.10
27.5 27.5 14 14 27.5 27.5 13

387.77 387.27 387.30 387.76 387.79 387.65 388.22

4.15 4.95 4.95 4.46 4.43 4.57 4.00
27.5 27.5 14 27.5 27.5

387.67 387.14 387.47 387.65 387.87 387.90 388.44

4.53 4.98 4.75 4.57 4.35 4.52 4.28
27.5 27.5 14 27.5 27.5

392.22 ✓

387.80 387.95 388.09 388.19 388.43

4.89 4.74 4.60 4.60 4.56
14 27.5 40.5 40.5

387.88 387.89 387.79 387.21 387.43 387.91

4.80 4.90 5.48 5.26 4.78
27.5 27.5 14

387.73 387.22 387.38 387.90 388.04 388.21 388.65

4.95 5.37 5.31 4.79 4.65 4.48 4.84
27.5 27.5 14 27.5 27.5

392.69 ✓

L. Z P.

3+13 = N C6 Wilson South

387.56	387.16	387.30	387.44	387.88	387.85	387.47	388.16
4.67 27.25	5.06 28.54	4.92 27.8	4.78 27	4.34 27	4.37 27	4.78 27.5	4.06 27.8

3+02.5 = N L Hill to North

387.80	387.78	387.52	387.94	387.92	388.14
4.43 27	4.44 27	4.30 27.5	4.88 27.5	4.33 27	4.08 27.6

2+95.10 = E Wilson to South

387.72	387.60	387.52	387.80	387.72	387.52	387.88
4.50 27	4.52 27.5	4.70 27	4.45 27	4.50 27	4.70 27.5	4.84 27

2+87.5 = E L Hill to North

387.76	387.78	387.52	387.98	387.97	388.13
4.46 27	4.44 27	4.70 27.5	4.84 27.5	4.33 27	4.09 27.8

2+77 = E Curb of Wilson to South

387.93	387.53	387.66	387.56	387.78	387.86	387.53	388.02
4.79 27.5	4.69 27	4.57 27.5	4.66 27	4.44 27	4.38 27	4.80 27.5	4.30 27.5

2+65.10 = E Line Wilson to South

387.96	387.42	387.59	387.86	387.91	387.56	388.11
4.36 27.5	4.79 27.5	4.53 27	4.38 27	4.37 27	4.66 27.5	4.11 27.5

392.22 ✓

392.22 ✓

1+40 = W.L. Filley

1+325 = F. Filley to South

1+23 = F.L. Filley South

1+0

0+50

0+0.1
3+257 = W.L. Wilson South

392.22 ✓

387.31	387.10	387.15	386.81	386.88	387.33	387.41	387.17	387.49
513 48 25	507 28 27	511 28 26	504 28 541	504 17	489	481 14	505 272 541	423 272 541
387.11	386.82	386.89	387.27	387.39	387.23	387.61		
511 40	500 28	533 17	495	483	499 277	481 277		
387.35	387.19	387.14	386.83	386.96	387.25	387.35	387.25	387.62
503 40 25	508 28 24	539 28 541	515 17	497	487 17	497 277	460 277	
387.21	386.67	387.00	387.39	387.37	387.24	387.60		
531 28	535 27	523 17	483	485 17	498 277	452 277		
386.90	387.22	387.70	387.63	387.28	387.90			
533 28	550 17	452	459 17	492 277	453 277			
387.62	387.11	387.39	387.89	387.87	387.50	388.17		
464 28 26	511 28 541	485 17	434	435 17	492 277 541	405 277		

392.22 ✓

RM

507

387.15

HWP
35.75
386.81

2465 = FL 35.1551

2450

220

1750

39222 ✓

386.88	386.74	386.60	386.97	387.04	386.65	386.96
5.34 28.83	5.28 28 94	5.52 14	5.25	5.8	5.59 27.94	5.24 27.65

386.78	386.31	386.64	386.85	386.82	386.62	386.55
5.44 28	5.21 28	5.58 14	5.37	5.10	5.40 27.7	5.37 27.7

387.13	386.56	386.71	387.05	387.15	386.95	387.22
5.09 28	5.66 28	5.51 14	5.17	5.07 14	5.37 27.7	5.00 27.7

387.24	386.72	386.93	387.23	387.35	387.10	387.56
4.98 28 6	5.50 28 94	5.39 14	4.99	4.87 14	5.12 27.7 94	4.66 27.28

39225 ✓

index
C.S.K.

6-20-47

Cross section 5th + Washington

After cone laid between
tracks. Prior to topping.

Sommarmoyas
Melton
Sherman

0+90 = Φ 5th 31' Rt. = line of gutter

0+77 = W. 1/4 5th 26' Rt. = line of gutter

0+64 = W. cl. 5th

0+50 = W.L. 5th

0+25

0+00 = 50' West. West line 5th Ave

SW.R.R.
5th Φ
Washington

5122 289.24 - 284.02

L = South

Φ
Wash

R = North. 26

6.36
20

6.20
10

6.15

6.05
10

6.27
20

S. of line
Wash to W

6.17
31

Gutter

5.95
20

5.83
10

5.69

5.74
10

5.76
20

S. of line
Wash to Wash

6.08
26

Gutter

5.52
20

5.24
10

5.20

5.49
10

5.77
20

5.10
20

4.82
10

4.73

5.12
10

5.59
20

4.47
20

4.15
10

4.14

4.43
10

5.16
20

3.83
20

3.51
10

3.52

3.89
10

4.56
20

Gutter

Gr. Ho.

1/2

1/4

289.24

1+80

7.95	7.37	7.20	7.17	7.29	7.38	7.95
2.5	1.0		1.0	2.0	3.0	4.4
Gutter						Gutter

1+55 = 25' East. E. line 5th

8.00	7.84	7.34	7.15	7.10	7.20	7.33	7.87
2.4	2.0	1.0		1.0	2.0	3.0	4.5
Gutter							Gutter

1+38

8.15
2.2
at grade of C.B.

1+35 43 Rt. = E.C. Curb Rot.

2.77
2.31+30 = E.L. 5th 46' Rt. = gutter line

7.81	7.19	7.02	6.95	7.02	7.15	7.74
2.2	1.0		1.0	2.0	3.0	4.6
Gutter						

43' Rt. = line of gutter

1+16 = East. Cb. line 5th

7.27	6.93	6.85	6.80	6.76	6.84	7.07
2.4	1.0		1.0	2.0	3.0	4.7
Gutter					Sub. Wash to West	

20' Rt. = So. cb. line Wash to

North - gutter line as

shown each section.

1+03 = E. 1/2 5th S. gutter line = 38' Rt.

6.87	6.62	6.59	6.47	6.40	6.38	6.48
2.7	1.0		1.0	2.0	3.0	3.8
Gutter			1/2	0.1. to West	5/8 Wash to West	

289.2A

289.2A

E
Wash

Rt = South

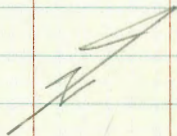
27

7-3-47 Cross Section 63rd St. (E to 18th East)
 Along Collwood park.

Work order 21001

Sommer mayer
 Melton
 Sherman

B.C. = 10+19.33



EC. = 5+07.73

$\Delta 19^{\circ}02'$
 $R = 737.37$
 $L = 171.57$

S Line Collwood Park

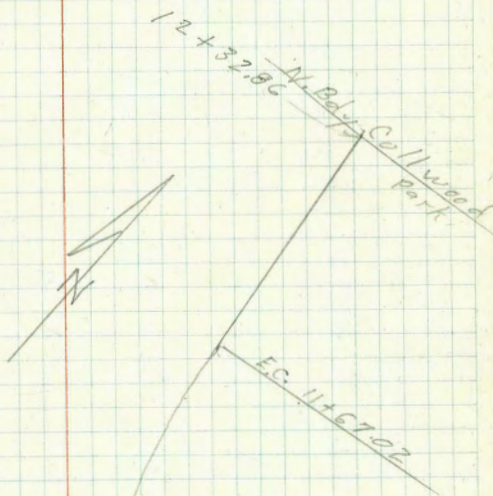
BC. = 2+62.78

- 2+55.87

Indexed
 e.s.k.

28

Stationing same as on
 L sheets 6787 + 6788



$\Delta 36^{\circ}47'30''$
 $R = 230$
 $L = 147.69$

B.C. 10+19.33

4+00

3+50

3+00

2+62.78 RC. Lt.

2+55.87 (Sketch P.28) Along S. line Callwood ^{Park}

T.P.	4.22	466.61	4.63	462.39
T.P.	3.83	467.02	5.67	463.19
N.W.B.P. El Cajon +63 rd	3.20	468.86	—	465.66

461.5	5.1	462.2	4.4	462.2	4.4	462.6	4.3	462.3
	$\frac{4.4}{2}$		$\frac{4.4}{8}$		$\frac{4.0}{13}$		$\frac{4.3}{18}$	
461.8	4.8	462.3	4.3	462.3	4.3	462.4	4.2	462.3
	$\frac{4.3}{2}$		$\frac{4.3}{12}$		$\frac{4.2}{18}$			
461.8	4.8	462.2	4.4	462.3	4.3	462.6	4.0	462.6
	$\frac{4.4}{2}$		$\frac{4.3}{12}$		$\frac{4.0}{18}$			
462.2	4.4	462.4	4.2	462.2	4.4	462.5	4.1	462.5
	$\frac{4.2}{2}$		$\frac{4.4}{12}$		$\frac{4.1}{18}$			
462.3	4.3	462.4	4.2	462.3	4.3	462.3	4.3	462.3
	$\frac{4.2}{2}$		$\frac{4.3}{12}$		$\frac{4.3}{20}$			
<u>466.61</u>								

7+00

6+50

6+00

5+50

T.P

3.44

461.92

5.13

461.48

5+07.73 E.C.

4+50

466.61

4

460.8

4.1

461.6

 $\frac{3.3}{2}$

461.6

 $\frac{3.3}{11}$

461.8

 $\frac{3.1}{14}$

462.0

 $\frac{2.9}{18}$

460.7

4.2

461.6

 $\frac{3.3}{2}$

461.6

 $\frac{3.3}{11}$

461.8

 $\frac{3.1}{13}$

462.0

 $\frac{2.9}{18}$

460.8

4.1

461.6

 $\frac{3.3}{3}$

461.7

 $\frac{3.2}{11}$

462.1

 $\frac{2.8}{13}$

462.3

 $\frac{2.6}{18}$

461.1

3.8

461.8

 $\frac{3.1}{1}$

462.0

 $\frac{2.9}{11}$

462.4

 $\frac{2.5}{14}$

462.2

 $\frac{2.7}{18}$ 464.92

461.1

5.5

461.8

 $\frac{4.8}{2}$

461.7

 $\frac{4.2}{13}$

462.4

 $\frac{4.2}{14}$

462.0

 $\frac{4.6}{18}$

461.3

5.3

461.9

 $\frac{4.7}{2}$

461.9

 $\frac{4.7}{9}$

462.3

 $\frac{4.3}{13}$

461.8

 $\frac{4.8}{18}$ 466.61

9+50

T.P. 5.31 465.57 4.66 460.26

9+00

8+50

8+00

7+50

7+30

464.92

460.3

5.3

460.3

 $\frac{5.3}{2}$

461.0

 $\frac{4.6}{6}$

461.0

 $\frac{4.6}{12}$

461.4

 $\frac{4.2}{18}$ 465.57

460.3

4.6

460.4

 $\frac{4.5}{2}$

460.8

 $\frac{4.1}{4}$

461.3

 $\frac{3.6}{18}$

460.2

4.7

460.2

 $\frac{4.7}{2}$

460.9

 $\frac{4.0}{4}$

461.2

 $\frac{3.7}{18}$

460.2

4.7

460.3

 $\frac{4.6}{2}$

461.1

 $\frac{3.8}{4}$

461.4

 $\frac{3.5}{18}$

460.6

4.3

460.7

 $\frac{4.2}{2}$

461.2

 $\frac{3.7}{4}$

461.6

 $\frac{3.3}{12}$

461.7

 $\frac{3.2}{18}$

460.6

4.3

460.7

 $\frac{4.2}{1}$

461.5

 $\frac{3.4}{3}$

461.8

 $\frac{3.1}{10}$

462.6

 $\frac{2.3}{12}$

463.0

 $\frac{1.9}{18}$ 464.92

11+67⁰² E.C.

11+48 15⁵ RT. = ϕ 3³ wide conc walk

11+00

10+50

10+19³³ B.C. RT.

10+00

465.57

ϕ RT

32

461.2	461.4	461.4	
4.4	4.2 71	4.2 18	
461.1	461.4	461.6	461.93
4.5	4.2 71	4.0 12	4.0 15.5 on walk
461.1	461.3	461.1	
4.5	4.3 3	4.5 18	
460.8	461.2	460.8	461.0
4.8	4.4 6	4.8 15	4.6 18
460.7	461.2	460.8	
4.9	4.4 7	4.8 18	
460.6	461.0	461.2	461.2
5.0	4.6 4	4.4 7	4.6 12 4.4 18

465.57

12+32.86 18' Lt. = End of curb. (Plat. ^{EL.} 461.45)

12+32.86 = Nly Line Callwood Park

12+23 12' Rt. = Ctr. 30" Tree. (Acacia)

12+00 12' Rt. = Ctr. 2" Tree (")

465.57

461.45
4.09

461.1	460.9	461.2	461.6	461.4
4.5	$\frac{4.7}{10}$	$\frac{4.4}{11}$	$\frac{4.0}{14}$	$\frac{4.2}{18}$

461.1	460.9	461.5	461.3
4.5	$\frac{4.7}{10}$	$\frac{4.1}{12}$	$\frac{4.3}{18}$

465.57

Cross Section San Rafael Place
Mission Blvd. to Bay Side Walk
Levels next page

indexed
c-s-k.

July 28-47

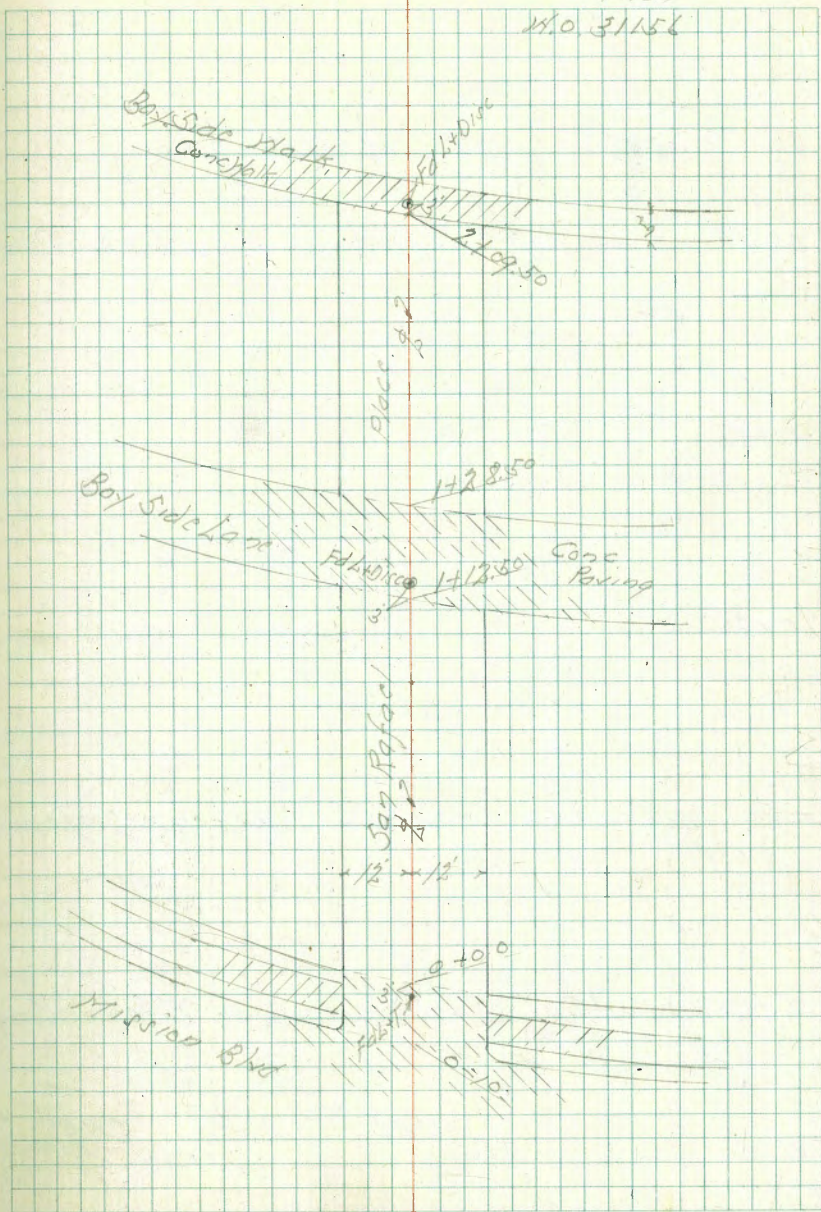
Sisson

McCol

Allen

No. 31156

34



1720.5 = $\frac{1}{2}$ Pav 29

Takes on Diag

~~5.18~~
5.191

~~5.24~~
5.197

~~5.25~~
5.198

1712.5 = $\frac{1}{4}$ Paving on Bay side Lane Takes Diag

~~4.94~~
1.67

~~5.15~~
-1.88

~~5.02~~
-1.75

170

~~4.85~~
-1.2

~~4.9~~
-1.6

~~4.7~~
-1.4

0781

119' Rt of $\frac{1}{2}$ Fly Picket Fence 6 - 12" x 12" Pickets ^{Brick}

~~4.4~~
-1.1

~~4.5~~
-1.2

~~4.25~~
-0.98

~~4.36~~
-0.99

0764

109' Fly Picket Fence
Cove Walk

120' Fly Picket Fence
Cove Walk

0760

~~4.1~~
-1.34

110' Fly Picket Fence
Cove Walk

0749

~~4.28~~
-1.01

117' Fly Picket Fence
Cove Walk

3.27

3.27

BM 2.39 7.13 SWBP
 TP 9.92 9.52 3.67 -0.40 San Rafael
 500 360 11
 12' Rt of $\frac{1}{2}$ = Fly Board Fence
 2 + 0950 = Wly 5' Concrete Walk Boyside Walk

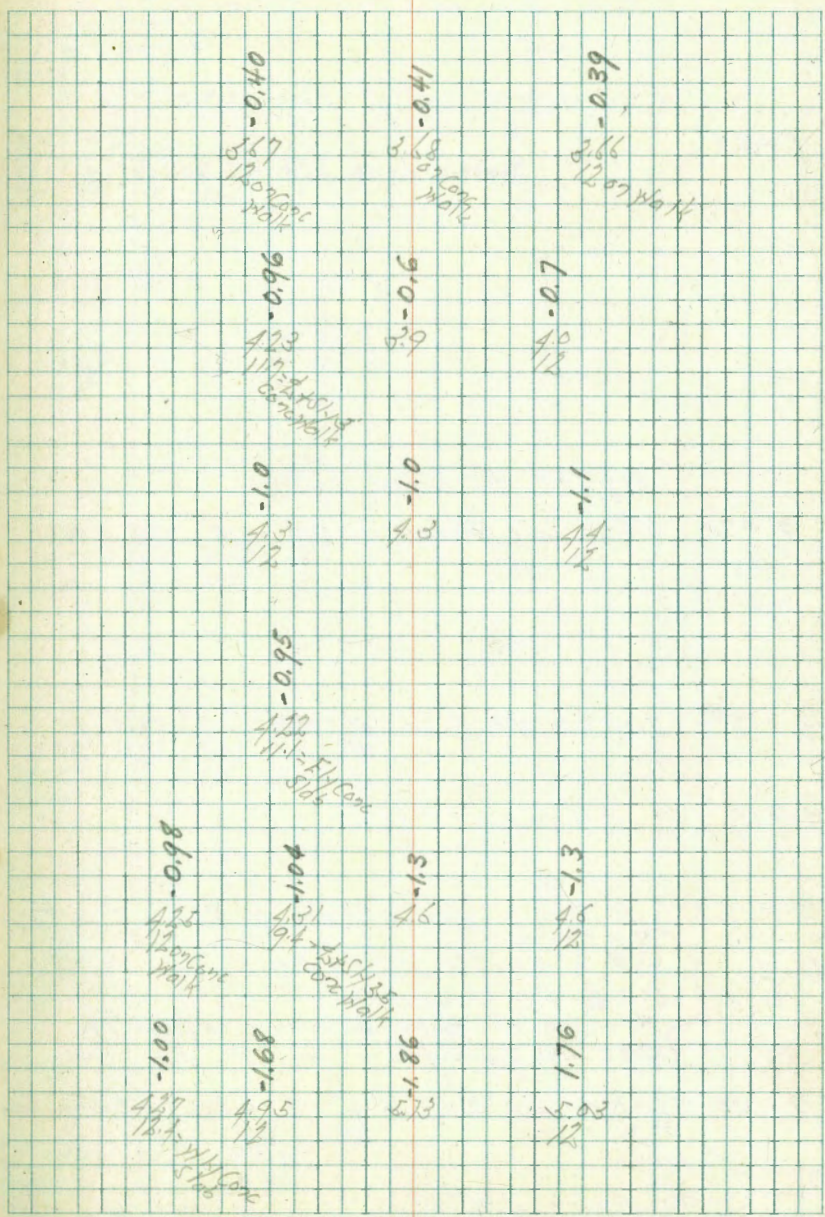
1+98

1+75

1+55 111' Lt of $\frac{1}{2}$ = Fly Picket Fence

1+41

1+285 12' Rt of $\frac{1}{2}$ = Wly Board Fence
 Fly Paving Boyside Lane
 12' Lt of $\frac{1}{2}$ = Wly
 Picket Fence



699.

Pershing Dr. at Florida
Cross Section
Sommermer
V Moore
Sherman
Lamore

W.O. 60135

see hard copy for sketch

1+25

↑
Traffic dept file No. 26-3

1+00

at 90° to base line.

0+70 Sections from here and taken

0+79⁸⁰ taken at A of 81°-42'-30" Lt. to B.L.

70+15 37°-Rt. = P. pole * C 1565

0+19.37 = Arch. of bridge Δ 72°-28' Lt.

Note {
S = stripe
D.S. = double stripe
P = Edge paving
H = Header board wherever it
can be spotted

0+00 Taken at Δ of 84°-01' Lt. to Base line

B.P. in Car
Pillar Ponder 424 94.12 — 89.88
Horse Canyon
Creek Bridge + Pershing Dr.

Pershing Dr. "A" Line
B.L.

38

7073
6013

INDEXED m²
8-10-47

86.23	86.26	86.25	86.54	86.42	86.40
-------	-------	-------	-------	-------	-------

7.37	7.76	7.87	7.58	7.70	7.72
53.8	49	36.9	26.4	14.9	6
P	H	S	D.S.	S	P

86.26	86.20	86.39	86.52	86.51	86.22
-------	-------	-------	-------	-------	-------

7.86	7.92	7.73	7.60	7.80	7.90
52.5	48.2	37	24.7	14.9	6
P	H	S	D.S.	S	P

86.18	86.39	86.44	86.24	86.09
-------	-------	-------	-------	-------

7.74	7.73	7.68	7.86	8.03
47.6	36.6	25.5	14.4	5.1
P	S	D.S.	S	P

86.24

86.33

86.30

54.4	7.88	7.75	7.79	7.75	8.26
ctr. pillar	49.3	36.7	26.1	14.1	11
	P	S	D.S.	S	ctr. pillar

85.05	85.29	85.39	85.52	85.30
-------	-------	-------	-------	-------

52	8.17	8.29	8.53	8.60	8.82
ctr. pillar	48.8	35.6	24.8	13.3	3.0
	P	S	D.S.	S	4.8
					ctr. pillar

94.12

2+75

87.25
6.87
92
P

2+46³

2+25 3³ Lt. = Pav. B.C. into 26th st. road

2+14² = 1/2 P.O.T. = 0+00 on "B" Line

2+00 26' Lt. = End double stripe

86.24
7.88
65.8
P

1+84 6³ Rt. = Directional sign (to Florida St.)

1+75

86.26
7.86
57.4
P

1+50

86.16
7.76
56.0
P

1+30 27⁵ Rt. = P. pole # C1585

94.12

87.67	87.67	88.07	89.06	89.66	89.52
6.45	6.48	6.05	5.06	4.46	4.60
78	51	38	17.8	1	5.6
07.00	H	S	S	H	P
86.87	87.31	87.60	88.52	88.92	89.73
7.25	6.81	6.48	5.60	5.30	5.37
79.6	48	36.8	16.1	2.5	P
P	H	S	S	H	
86.53	87.04	87.32	88.09	88.24	
7.59	7.08	6.80	6.03	5.88	
71.7	46.2	36.7	15.3	3.3	
P	H	S	S	P	
86.87	87.02	87.31	87.63	88.26	6.27
					Hub
7.25	7.10	6.81	6.57	6.47	
46.3	36.8	26	15	4.6	
H	S	0.5	S	P	
86.73	86.79	86.93	86.98	87.04	
7.59	7.33	7.19	7.14	7.08	
46.7	37	26.1	15.1	5.7	
H	S	0.5	S	P	
86.68	86.69	86.67	87.62		
86.48	7.64	7.43	7.47	7.50	
46.9	36.9	26.2	15	6.1	
H	S	0.5	S	P	

94.12

1.10 92.92 Hub. B.M.

3+59²⁷ = 2x2 L = 0+00" C + "D" Lines3+54⁶ = End pav. on B.L.

3+53 7.7 Lt. = Δ in pav.

1st Lt. = traffic button3+34⁵ Intersect & stripe on 26th St. roadR = Reflector buttons

3+25 33.7 Lt. = start reflector Buttons

3+00

94.12

92.92
1.20
Hub

92.81

1.31
P

93.00

1.12
7.7
H7th
Button

99.36 99.82 90.25 90.62 91.36

1.76	4.30	3.87	3.50	2.76
59.9	45.9	33.7	22.4	3.3
H	S	R	S	H

98.30 99.74 99.32 90.39

5.82	5.38	4.40	3.73
54.5	41.	19.3	1.1
H	S	S	H

99.57

4.25
1.68
P

94.12
1.20

"B" (Florida St)
LINE Road

1+70 40' Rt. = P. pole #C 1627 (overhead street light)

1+65

1+50

Pershing & Florida roads

1+40 38' Rt. = division of paving into

1+19 6' L Rt. = Traffic Button
start double stripe

1+01 35' Lt. = stop sign

0+90 50' Lt. = P. pole # 1610

0+05^L = start paving P = Edge paving

L = 45' - 38' Lt. off "A" Line

0+00 2+14^L of Line - Page 39 2/2 Hub

B.P. in Bridge

A.38 41.4 94.12 - 89.88

Lt.

BL

Rt.

41

89.34	89.53	89.90	89.13
5.78		5.22	4.94
5.51	5.59	4.79	4.88
3.8		11.6	26.2
P		D.S.	P
88.02	88.40	88.71	87.16
6.10	5.72	5.41	4.76
5.78	5.51	5.22	4.94
7.		10.5	29.5
P		D.S.	P
87.81	87.49	88.40	89.54
6.31	5.93	6.52	4.60
10		9.2	3.8
P		D.S.	P
89.44	84.23	88.28	
6.68	5.89	5.84	
16.3		6.2	
P.		D.S.	
	88.05		
	6.09		
	P		

94.12

'B' line

3+48⁶ ± 2 x 2 Hub. 3.00

3+00

2+50

2+41² Int. 24" Conc. Culvert Δ 80°-05' RT

2+27 42° RT. = No Pumping sign

2+25 15° RT. = End double stripe

2+00

1+83⁸

94.12 ~~94.12~~

Lt.

B.L.

Rt.

42

91.38	91.69	91.23
2.74	2.43	2.89
3.00	4.8	16.6
Hub	P	S
		P

90.62	90.90	90.48
3.42	3.22	3.64
4.3	16.2	29.7
P	S	P

89.92	90.13	89.86
4.20	3.99	4.26
4.	15.7	27.5
P	S	P

85.86 = EL.
72
Invert

EL = $\frac{86.26}{43.8}$
Invert

89.41	89.69	89.60
4.71	4.43	4.52
3.4	15.5	26.4
P	D.S.	P

88.91	89.30	89.41
5.21	4.82	4.71
2.4	14.6	27
P	D.S.	P

88.60	89.15	89.24
5.52	4.97	4.88
5.27	4.52	4.74
P	13.7	26.6
	D.S.	P

94.12

"C" Line (Persting Dr.)
Cont.

see Hard copy
upper road to 26th St.

0+83^E 27.5 Rt. = Junction Persting Dr. and

0+71^S

0+50

0+32

R = reflector button.

0+19 intersect paving edge

10° Lt. = L: in paving

0+00 = 3+59.27 on "A" line. L = 43° 54' Lt. off "A" line

2x
3+59.27 A. line 9.78 102.70 — 92.92
Page 40

Lt.

E

Rt.

43

95.38	96.44	97.13	97.92	99.00	98.99
7.32	6.26	5.57	4.78	3.70	3.71
53.8	19.5	7.4	3.6	23.4	27.5
P	S	R	S	HP	P 22 th St. Rd.

97.04 98.39

5.66
S
4.31
21.2
P

92.04	93.38	94.53	95.37	95.89	96.67
10.66	7.32	8.37	7.33	6.81	6.03
50	33.6	20.5	7.9		13.4
P	S	R	S		P

90.70	91.16	92.89	93.99	94.99	95.34
12.00	11.04	9.81	8.81	7.71	7.36
58.8	42.4	27	15.9		6.1
H	S	R.	S		P

94.38

8.32
P

93.02

92.92

~~7.68~~
~~7.2~~
~~H~~
9.78
44.6

102.70

1+90 16² Lt. Caution sign

1+62⁵ Intersect stripe

1+50 Cont.

1+50

10.73 113.26 0.17 102.53

start double stripe.

1+46 7.5 Rt. = End of reflector buttons to
0.17

See hard copy for detail
W = Base cobble wall
G = Edge paving + cobble gutter

1+08 Intersect button line

102.70

102.86
10.40
S

102.56 102.03
10.70 11.23
45.5 50.4
G W

101.48 101.91 102.44 102.82 103.13 102.92
11.78 11.35 10.82 10.44 10.13 10.34
13.6 2.9 3.3 19.1 31.0 35.5
P S D.S. S H S

113.26

102.15
0.55
7.5
B

97.33 98.32 99.16 100.04 101.09 101.14 100.79 100.22
5.37 4.38 3.54 2.64 1.57 1.56 1.92 2.48
26.7 12.2 R 11. 28.3 40.1 52.5 58.4
P S S H S B W

102.70

"C" Line
Pershing

2+65 1.4 Rt. = Pav. E.C.
38' Lt. = Exit From bank - 41' Lt. = End Pipe
 $\Delta 138^\circ 35'$ Lt. to outlet.
Inlet Not located must be dead.
2+64 Int. probable line 12" corr. iron culvert

2+50 Cont

2+50

2+27 Intersect edge paving

2+00 Cont

2+00

113.26
~~102.70~~

Lt.

E

Rt.

45

	109.74			
	<u>3.52</u>			
	1.4			
	P			
101.92				
EL. Invert				
41				
	109.06	108.96	108.39	
	<u>4.22</u>	<u>4.30</u>	<u>4.87</u>	
	31.4	17.2	51.2	
	H	G	W	
	108.73	108.82	108.77	108.99
	<u>4.53</u>	<u>4.44</u>	<u>4.47</u>	<u>4.27</u>
	0.7	11.3	21.9	31
	P	S	DS	S
	107.19			
	<u>6.07</u>			
	P			
	105.89	105.73	105.73	105.73
	<u>7.37</u>	<u>7.53</u>	<u>8.13</u>	
	31.6	45.9	50.	
	H	G	VV	
	105.45	105.57	105.74	105.87
	<u>7.87</u>	<u>7.67</u>	<u>7.52</u>	<u>7.37</u>
	3.3	6.8	17.3	27.4
	P	S	DS	S
	113.26			
	102.70			

"C" line
Persting

Lt.

±

Rt.

46

3+54' Sort

50.4
G

54.
W

3+54'± 2x2 Hub.

1.3
P

71.6
S

21.6
D.S.

31.3
S and
H

B.M. (2x2) Page 43

7.61 92.92 OK

T.P. 0.14 100.53 12.37 100.39

3+00 Sort.

112.12
1.14

111.91
1.35

111.99
1.77

31.4
H

49
G

52.7
W

3+00

113.26

102.70

112.02
1.24

112.00
1.18

1.13
1.14

11
12

21.8
D.S.

31.3
S

113.46

102.70

D. Line

26th St. Road

1 + 25

1 + 00 Junction of pavings

0 + 75 Junction of ...

0 + 50

0 + 25

L = 61°-23' Rt. off "H" Line

0 + 00 = 3 + 59.22 on "H" line

2 x 1.37592
H.L. line (Page 10)

7.61 100.53 — 92.92

Lt.

B.L.

Rt.

47

91.125	91.08	91.47	92.19	91.10
9.10	8.45	8.06	8.34	8.63
22.0	16.8	2.9	15.1	28.4
W	G	S	S	P

92.25	92.77	92.98	93.71	92.87	92.45	92.72	91.45
8.28	7.76	7.55	7.62	7.66	7.88	8.41	9.08
22.7	2.7	14.6	0.5	PAV. +	4.8	16	27.9
W	G	S	P	DIRT	P	S	P

93.15	94.10	94.20	93.90	92.60	91.85	91.14
6.78	6.47	6.33	6.63	7.73	8.68	9.39
54.6	48.2	21.4	15.8	6.7	16.8	27.7
W	G	S	P	DIRT	P	S

96.02	96.23	95.99	95.24	92.67	91.81	90.59	
4.57	4.30	4.54	5.07	DIRT	7.86	8.72	9.74
82	74	54	35	DIRT	6.5	18	34
W	G	S	P	P	P	S	P

97.59	96.67	92.63	91.93	90.24
2.74	3.84	7.90	8.60	10.29
86	61	7.3	19	40
S	P	P	S	P

7.61
Hub

100.53

"D"
26th St. Road

2+06 End cobbler gutter

2+00

1+70

1+54 Joq. in paving

1+50

100.53

L7.

B.L.

Rt.

48

8838 8867
12.15 11.86
19.5 9.8
W Edge Gutter

8888 9069 9072 9113
11.65 9.84 9.84 9.40
14 2.3 13.2 28.3
W A 3 A

9055 9127 9099 9081
8.98 7.26 9.54 9.72
9.8 5 7.4 29.1
W G 5 P

9172
8.81
27.2
P44
J99

9089 9149 9193 9193 9173
9.64 9.04 8.60 8.60 8.80
13.5 9.1 7 14.6 28.6
W G 5 5 P P

100.53

"D" line
26th St. Road

Cont. on p. 50

T.P. 8.24 98.40 10.37 90.16

T.P. on
Head wall
Culvert

2+32.71 Nail C. = 0+00 { F Line
F Line

2+27

100.53

91.79
8.74
0.7
P

91.43 91.93
9.10 8.60
25 12.1
P S

100.53

"E" line
26th St Road Cont.

Lt.

B.L.

Rt.

50

1+25

94.56	95.69	96.42
3.84	2.92	1.98
<u>11.2</u>	<u>23.6</u>	<u>37.6</u>
P	S	P

1+00

93.91	95.13	95.99
4.49	3.27	2.41
<u>17</u>	<u>29.2</u>	<u>39.5</u>
P	S	P

0+75

93.98	94.55	94.32
5.02	3.85	3.08
<u>19.5</u>	<u>30.8</u>	<u>41</u>
P	S	P

0+50

92.85	93.76	94.35
5.55	4.64	4.05
<u>17</u>	<u>28.6</u>	<u>38</u>
P	S	P

0+20 Jct. in "Burma road" Pav.

92.39	92.93	93.49	93.84
6.01	5.47	4.91	4.56
<u>9.6</u>	<u>20.2</u>	<u>30.4</u>	<u>42</u>
P	S	L.H. Pav.	P

L = 33° off "D" Line.

0+00 = 1+32^{1/2} Nail on "D" Line

98.40 From P. 49

98.40

E" Line
26th St. Road Cont.

Lt.

B.L.

Rt.

51

2+20

97.66	97.93	98.33
0.74	0.47	0.97
49.1	37.5	21.8
P	S	P

1+94

96.72	97.27	98.03
1.68	1.13	0.37
27.5	14.5	P
P	S	

1+72⁸

96.27	96.74	97.58
2.13	1.66	0.82
74	\$	74
P		P

1+51

95.47	96.29	97.10
2.93	2.11	1.30
P	13	24.9
	S	P

98.40

98.40

"F" Line
"Burma Road"

Orig
B.M. 4.30 89.88 (99.88)

T.P. 3.13 94.18 7.35 91.05

1+50

1+00

0+85

0+51

0+35

0+24³

Cold lay paving

L = 107° Rt. off "D" Line.

0+00 = 2+32² on "D" Line

98.40 From Page 51

Lt.

B.L.

Rt.

52

90.8	90.2	89.8	89.1	88.4
<u>7.6</u>	8.2	8.6	9.3	10.0
22	8	25	4.3	
P			P	

91.4	90.9	90.3	89.5
<u>7.0</u>	7.5	8.1	8.9
16	10	2.7	
P		P	

91.7	92.2	90.0
<u>6.7</u>	7.2	8.4
16		2.1
P		P

92.3	92.4	92.1	91.6
<u>6.1</u>	6.0	6.3	6.8
22	15	9	
P		P	

92.90	92.60	92.3	91.8
<u>5.56</u>	<u>5.8</u>	6.1	5.6
30.3	10	12.3	
P		P	

92.15

6.25

92.5	92.5
P	P

98.40

Additional Notes "D" Line

1+39 ^{37 RT.} = End Grout ~~Apron~~

$\frac{11.4}{37}$ 11.8
East, End Apron

1+37 35 RT = End 2nd 24" Culvert

$\frac{11.76}{35}$
Invert

1+34 35 RT = End 24" Culvert

$\frac{11.76}{35}$
Invert

1+30 43 RT = Φ grout apron

$\frac{12.14}{43}$

1+28 Δ in Hd wall 34 RT start Grt. Apron

$\frac{4.5}{34}$ 11.3
Hd wall Grout
Apron

1+25 43 RT = ^{s.w. Cor} grout apron

$\frac{11.5}{43}$

1+21 start Head wall

$\frac{4.5}{29}$ 4.6 9.8
top wall Hd wall End

1+04 29 RT = start Cobble wall

$\frac{5.4}{29}$ 4.9
Bed Top wall

2x2146
3+59.27
At Line.
(Page 40)
4.30 97.22 — 92.92

97.22

also 36 RT = start grout slab

1+60 Break in spillway

$\frac{7.9}{30}$	$\frac{8.2}{36}$	$\frac{8.7}{36}$
Cobble	Cobble	Grout

1+54 Cont.

$\frac{6.7}{43}$

start Cobble + grout spillway

1+54 = 27² RT = ~~Brk.~~ Wall. 29² RT =

$\frac{5.7}{27}$	$\frac{4.9}{27.3}$	$\frac{4.9}{29.4}$	$\frac{6.4}{29.4}$
Par	top wall	Par	Spillway

Cobble + grout spillway

1+50 27³ RT = Brk. in wall + start

$\frac{5.4}{27}$	$\frac{4.5}{27.3}$	$\frac{4.5}{31}$
Base wall	top wall	

1+42 16.5 Lt. = Φ golf course drive

$\frac{3.65}{16.5}$
Conc

Back end
298 Lt. = Φ driveway to golf course

1+41 = End Head wall 39' RT

$\frac{5.99}{29.8}$
Conc

$\frac{4.7}{39}$

97.22

2+02⁶ 29 ft. on start cobble wall

5.7
2.9
07 wall

2+02⁵ End cobble spillway start cobble wall

5.99 6.4
2.84 3.3
Spillway St. cor. Cobble
 Spillway

1+97 35 ft = End grout

6.26 8.0 9.3
Edge 28.5 37
Avg. Cobble Grout +
29.4 Cobble

1+84 44 ft = Δ in grout

12.9
4.1

1+77 55 ft. = Δ in grout

9.3 11.6 13.3 13.3
3.6 3.6 4.2 5.5
Cobble Grout

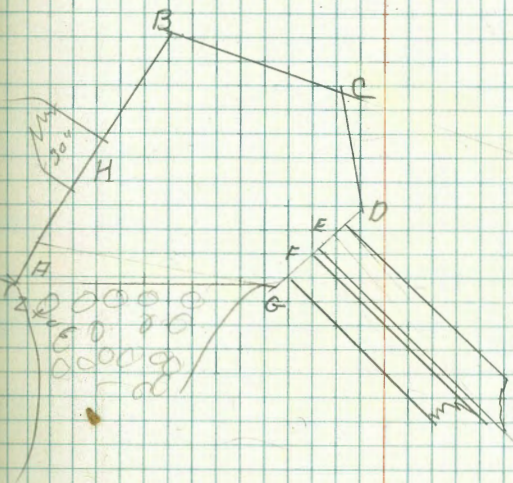
1+62 Δ in grout 46 ft.

9.7 10.0 12.0
3.6 3.6 4.6
Cobble Grout Δ in
 Grout

Rods by letter as per sketch
 see hard copy for detail.

10.7	10.7	7.0	10.6	10.60
E	F	G	G	H
Invert	Invert	top	Bottom	Invert

10.4	7.0	10.5	7.1	10.6	7.3	10.6
H	B	B	C	C	D	D
Bottom	top	Bottom	Top	Bottom	top	Bottom



Sta. 2+06 Cont.

head wall
 2+06 End Cobble gutter + start Conc.

7.0	8.6	8.4	7.2
19.5	19.5	7.8	7.7
o.s. wall	Gutter	Gutter	top

2+12 28 Rt. = End cobble wall

5.2
28
top wall

Cross Sec. Hawk. St. 11-3-47
 Sutter - south W.O. #25001

Sammermeyer
 W Moore
 E. Sherman

- = fd. L+T. in cl.
- = fd. 7' L+T.
- = set. Nail
- = set. Hub + Disk
- = points set 33' so. of mean of curbs on Sutter. Mean of these points used as so. 7' line Sutter.

0+00 = South line Sutter.

Lines run to fit improvements where no points were in.

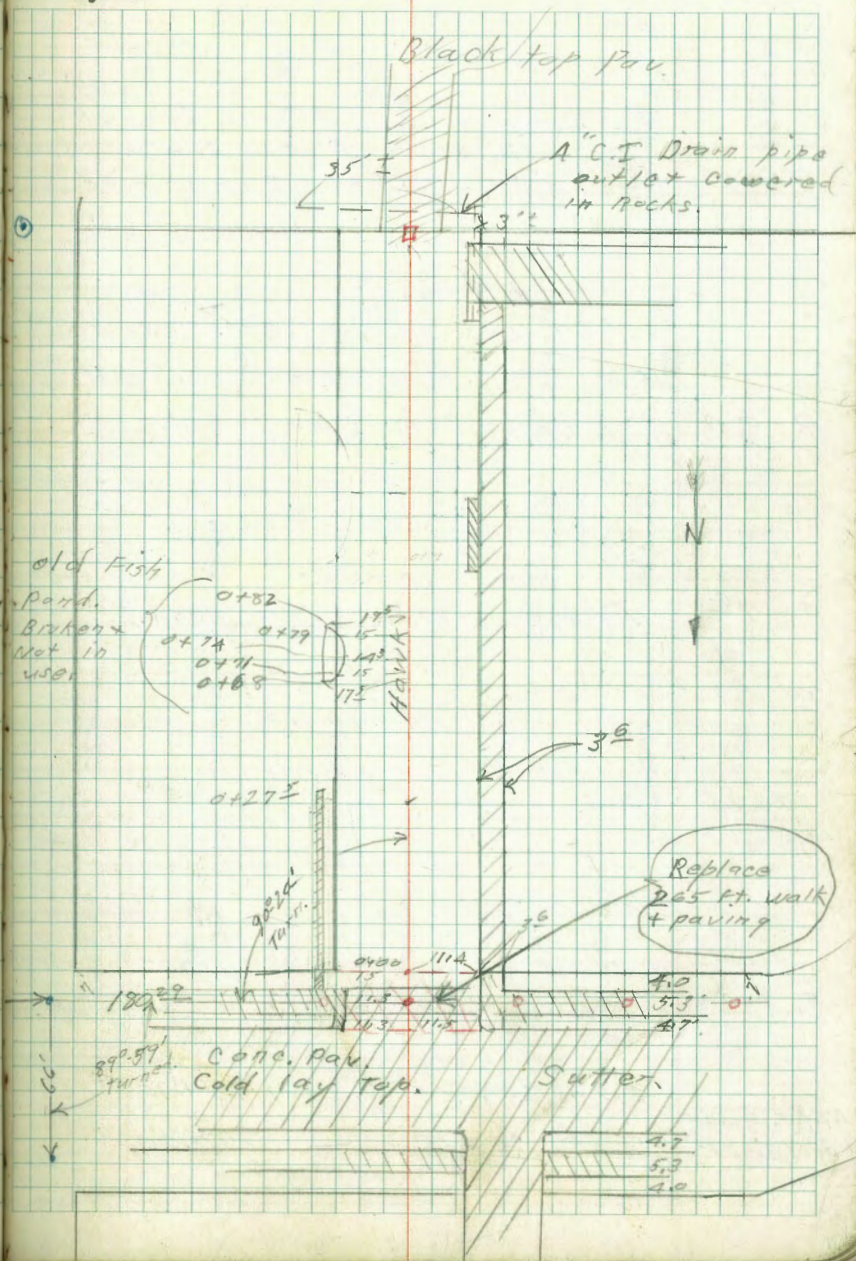
Reynard Way

Goldrich

INDEXED

JPB

58



tile set in cement 4" conc. border
 conc. walk. start 3" wide tile walk.
 0+00 = S.L. Sutter. 11 1/2 RT. = End 3" wide

16' Lt. = 2' Hedge.
 17' Lt. = W. Edge N. + S. 2" conc. walk
 15' Lt. = start. 5" wide N. + S. Conc. wall

0-04 S. Edge walk (Poor Cond.)

0-9 1/2 = N. Edge walk. (Poor cond.)

0-14 Cont.

0-14 = S. Cb. line Sutter

N.E.B.R. Bush
 + Gold Pinch

4.74	257.64	7.25	254.90
2.15	262.15	—	260.00

	254.41	254.46	254.6	254.93	254.99
	5.12	5.10	5.10	4.71	4.65
	15		11.4	11.4	15
				walk	walk
	254.52	254.55	254.55	254.89	254.96
	5.12	5.09	5.09	4.75	4.68
	17.1	15	11.3	11.3	15
	walk	walk			
		+ top wall.			
	254.45	254.45	254.51	254.88	254.99
	5.19	5.19	5.13	4.76	4.65
	15	11.3		11.3	15
	254.36	253.94	254.24	255.19	255.36
	5.28	5.10	5.40	4.85	4.28
	100	100	49	50	100
	rad.	cut	top of.	rad.	cut
	253.39	254.34	254.02	254.23	254.69
	5.25	5.30	5.62	5.41	4.95
	49	106	113	11.8	100
	Top + Rad	0.5 Rad	cut	cut	1 Rad
	Grade	curb			cut
		rot.	259.64		
	254.71				

0+74

0+71

0+68 See Page 58

0+67 14⁵ Lt. = End wire fence.

0+60

old and are to come out.

These roses are about 30 years

0+52 15 Lt. = 12" diam Rose bush burl.

0+33 15 Lt. = 15" Rose bush burl.

T.P. 5.64 259.36 5.92 253.7216' Lt. = E. + End 2' wide N. + S. Hedge.
+ start wire fence.

0+27.5 15' Lt. = End 5" wide Cone wall

259.64

253.5

 $\begin{array}{r} 5.9 \\ 14.3 \end{array}$

253.5

 $\begin{array}{r} 5.9 \\ 15 \end{array}$

253.6

 $\begin{array}{r} 5.8 \\ 15 \end{array}$

253.6

 $\begin{array}{r} 5.6 \\ 11.4 \end{array}$

11.4

cb.

252.1

 $\begin{array}{r} 7.3 \\ 14.5 \end{array}$

252.1

 $\begin{array}{r} 7.3 \\ 15.2 \end{array}$

253.6

 $\begin{array}{r} 5.8 \\ 17.5 \end{array}$

top.

254.22

 $\begin{array}{r} 5.74 \\ 11.4 \end{array}$

11.4

cb.

254.59

 $\begin{array}{r} 3.05 \\ 11.4 \end{array}$

11.4

walk

252.1

 $\begin{array}{r} 7.3 \\ 17 \end{array}$

252.1

 $\begin{array}{r} 7.3 \\ 17 \end{array}$

252.4

 $\begin{array}{r} 7.0 \\ 17.5 \end{array}$

Bottom

254.29

 $\begin{array}{r} 5.07 \\ 15 \end{array}$

15

walk

254.0

 $\begin{array}{r} 5.4 \\ 15 \end{array}$

15

254.1

5.3

5.3

259.36

254.62

 $\begin{array}{r} 5.02 \\ 15 \end{array}$

15

15

wall.

253.7

5.9

14.9

Bottom

Footing

254.3

5.2

12.9

Brd

Brd

254.3

5.3

5.3

5.3

5.3

254.1

5.5

11.4

11.4

11.4

254.59

3.05

11.4

11.4

walk

254.61

5.03

15

15

15

259.64

1+01 10³ Rt. End same0+93 10³ Rt. = start Conc. Ramp to top of curb.0+89 14² Lt. = start Conc. Apron to double @ ar.

0+86 15' Lt. = 3' wide Conc. Walk

0+82 End old fish pond

0+79

259.36

$$\begin{array}{r} 5.0 \\ 15' \\ \hline 253.9 \end{array}$$

$$\begin{array}{r} 6.0 \\ 10' \\ \hline 253.4 \end{array}$$

$$\begin{array}{r} 5.8 \\ 10' \\ \hline 253.6 \end{array}$$

$$\begin{array}{r} 5.00 \\ 10' \\ \hline \text{Grd} \\ 253.6 \end{array}$$

$$\begin{array}{r} 5.65 \\ 10.3 \\ \hline \text{Edge} \\ \text{Ramp} \\ 253.71 \end{array}$$

$$\begin{array}{r} 5.50 \\ 11.4 \\ \hline \text{Cl.} \\ 253.86 \end{array}$$

254.20

$$\begin{array}{r} 5.16 \\ 22.6 \\ \hline \text{Bar. Apr.} \end{array}$$

253.95

$$\begin{array}{r} 8.41 \\ 14.8 \\ \hline \text{Apron} \end{array}$$

253.6

$$\begin{array}{r} 6.0 \\ 14.9 \\ \hline \text{Gr. Apr.} \end{array}$$

253.67

$$\begin{array}{r} 5.69 \\ 15' \\ \hline \text{Walk} \end{array}$$

253.5

$$\begin{array}{r} 3.9 \\ 15' \\ \hline \text{Grd} \end{array}$$

253.7

$$\begin{array}{r} 5.7 \\ 11.4 \\ \hline \end{array}$$

253.7

$$\begin{array}{r} 5.7 \\ 11.4 \\ \hline \end{array}$$

253.96

$$\begin{array}{r} 5.40 \\ 11.4 \\ \hline \text{Cl.} \end{array}$$

254.03

$$\begin{array}{r} 5.33 \\ 11' \\ \hline \text{Walk} \end{array}$$

253.5

$$\begin{array}{r} 5.9 \\ 15' \\ \hline \end{array}$$

253.5

$$\begin{array}{r} 5.9 \\ 17' \\ \hline \text{Top} \\ \text{Bar. Apr.} \end{array}$$

252.4

$$\begin{array}{r} 7.0 \\ 17' \\ \hline \text{Bar. Apr.} \end{array}$$

253.6

$$\begin{array}{r} 5.8 \\ 15' \\ \hline \end{array}$$

252.2

$$\begin{array}{r} 7.8 \\ 15.2 \\ \hline \end{array}$$

252.4

$$\begin{array}{r} 7.0 \\ 17' \\ \hline \end{array}$$
259.36

Drive into nursery yard.
 Also start Black stuff
 1+49⁸⁵ End of street.

11.2 Rt. = 4" Drain
 1+48 9² Rt. = End Conc. Dr.

98 Rt. = start Conc Dr. +
 1+41 11⁵ Rt. = End tile walk.

curb, 4" drain lengthwise thru ramp
 1+37 10' Rt. = start Conc. Ramp to top of

Conc. wall 18" ± High.
 1+05¹ 14.9 Lt. = Start Broken up 5" wide

T. P. 1+49⁸⁵ ± 4/2
 A.65 257.81 6.20 253.16

1+05 14.8 Lt. = End Conc. Apron to
 double Bar.

259.36

252.7	253.2	253.3	253.5		
5.1 15	A.6	1.5 6	1.3 15		
		252.36	252.99	252.51	253.59
		4.45 9.8 Drive Grd.	4.82 11.2 Top 2" Dr.	4.30 11.5	4.23 13
		253.39	253.51	253.51	253.51
		1.12 9.8 Grd. + Drive	4.30 11.3 Gr. in Dr.	4.26 15	10 Drive
253.0	253.3	253.4	253.41	253.43	253.53
4.8 14.9 Grd	1.5	4.1 10 Grd	4.40 10 Ramp	4.88 11.3 FL. 4" Dr. + Grd.	4.25 11.5 Cl.
254.16	253.91	253.7			
5.20 22.6 floor	5.45 14.8 Apron	5.7 14 Grd			
			<u>259.81</u>		
			<u>259.36</u>		

Orig B.M. 260.00 2.18 259.99

N.E. B.P.
Sutter +
Gold point SS. 5.16 257.01

T.P. 7.58 262.17 3.22 259.59

2+00

1+50

257.81

5.3
252.3
Edge par

4.8
253.0
Edge
par

5.4
252.4

4.6
253.2

257.81

5.2
252.6
Edge par.

4.5
253.3
Edge
par

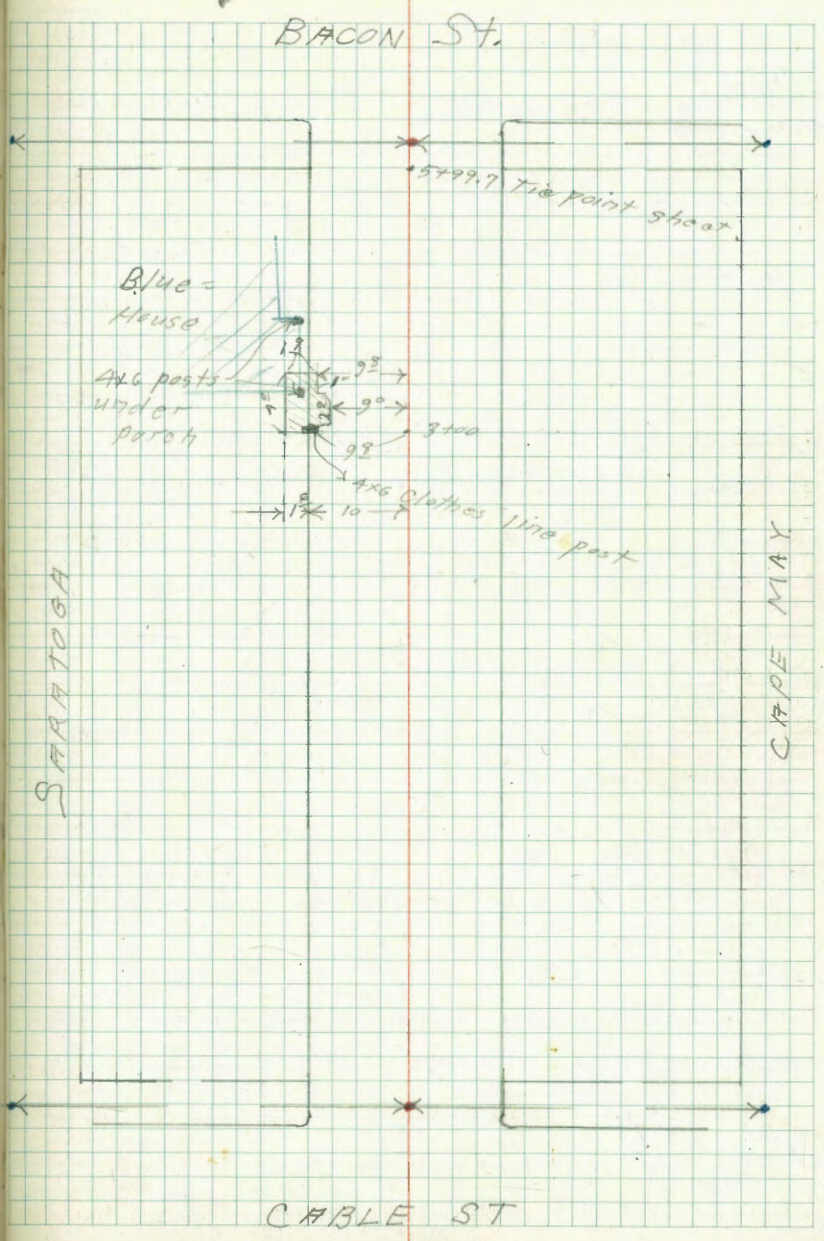
Cross Section
Alley BIK. 58 O.B.

V.O. # 31398

Sommermeier
W Moore
E Sherman

12-5-47

Indexed
B



T.R. inside
 End of sec. 3.67 18.00 5.21 14.33
 Alley curb

0+02 Cont.

11¹/₂ Lt. = start conc. Apron.
 0+02 13¹/₂ Lt. = start 4 Car Garage.

0+00 = End H.C. Paving

0-12 Cont.

0-12 = Wly. Ch. line Cable

S.W.B.P.
 Cable +
 Capc May.

6.49 19.54 — 13.05

14.88	14.5	14.5	13.7	13.5	13.6	14.3
4.71	5.0	5.0	5.8		5.9	5.2
11.5	11.5	10	5	6.0	5	10
E-90 H. 1109	0.74					
15.20	14.95	13.50	13.95	13.50	13.95	14.17
5.25	5.59	6.04	5.58	5.58	5.37	
10.07	10	1	9.6	9.6	9.65	
Top Cr.	part 0.74		part 0.74	part 0.74	part 0.74	Top Cr. end
19.65	14.05	13.32	13.66	12.80	13.82	
4.89	5.49	5.22	5.88	6.74	6.22	
100	100	50	50	100	100	
0.1	part 0.1	0.1	part 0.1	part 0.1	part 0.1	part 0.1
13.76	14.10	13.44	13.40	13.41	13.95	13.09
5.78	5.44	6.10	6.14	6.09	5.59	6.45
50	Top Cr.	10		10	Top Cr.	50
part	0.1	part		part	0.1, part	part
	Return					

19.54

0+54^E 12.9 Lt. = Φ Ctr. Car. door.

15.04	14.89	14.9	14.8	14.5	14.2	14.5	14.8
2.96	3.11	3.1	3.2	3.7	3.8	3.5	3.1
12.9	11.4	11	10	7		6	10
Bar	Apron						
Floor							

0+42 12.9 Lt. = start opening to 3 Car. Bar

15.13	14.88	14.8	14.7	14.5	14.5	14.5	15.00
2.87	3.12	3.2	3.3	3.7	3.7	3.5	3.0
12.9	11.4	11	10	6		7	10
Bar	Apron						
Floor							

0+38^E 4 car Bar
11th Lt. = Start come Apron to

15.25	14.7	14.6	14.2	14.2	14.4	14.9
3.15	3.3	3.4	3.8	3.8	3.6	3.6
11.4	11	10	7		6	10
Apron						

0+33^Z 12.9 Lt. = End 4 car Bar.
11.4 Lt. = End Come Apron

15.05	14.88	14.4	14.6	14.4	14.2	14.3	14.8
2.95	3.12	3.4	3.4	3.6	3.8	3.7	3.2
12.9	11.4	11	10	7		6	10
Bar	Apron						
Floor							

0+22^A 13th Lt. = 3rd door to 4 Car. Bar

15.07	14.86	14.2	14.2	14.0	14.1	14.4
2.93	3.14	3.7	3.8	4.0	3.9	3.6
13.1	11.5	10	7		7	10
Bar	Apron	3 rd				
Floor						

0+14 13th Lt.
 Φ 2nd door to 4 Car. Bar.

15.08	14.90	14.7	14.1	13.8	14.0	14.3
2.92	3.10	3.3	3.7	4.2	4.0	3.7
13.1	11.5	10	7	10	7	10
Bar	Apron					
Floor	3 rd					

18.00

18.00

1+74^E 9^L Rt. = 2' wide corner walk

5.1
10
5.3
7
5.6
5.2
9
12.8
5.02
9.1
walk
13.04
4.94
10
13.08
4.92
15

1+66 14^S Lt. = End 4 car Gar. dirt floor

13.2
4.8
14.8
13.3
4.7
10
12.9
5.1
7
12.5
5.5
6
12.8
5.2
6
13.3
4.7
10

1+50 9.8 Rt. = End board fence + start wire fence

1+31 15^L Lt. = start 4 car Gar. dirt floor

13.4
4.6
40
13.3
4.7
15
13.2
4.8
10
13.1
4.7
7
13.0
5.0
5
13.2
4.8
5
13.2
4.8
10
13.2
4.8
40

1+25 9^L Rt. = Line of board fence

1+00 9^L Rt. = start board fence
10^L Lt. = pole # P.H. 4920

0+99 9^L Rt. = 2 18" Conc. Walk

14.1
3.9
10
13.7
4.5
7
13.4
4.6
13.7
4.3
9.7
13.73
4.27
9.9
walk
13.74
4.26
10
walk

0+87 12^E Rt. = garage dirt floor no foundation
old prairie double

14.1
3.9
10
13.7
4.3
6
13.7
4.3
13.8
4.2
10
13.8
4.2
12.05

0+66 12.9 = End opening 3 car Gar.
11.4 Lt. = End Conc. Apron

15.08
2.92
12.9
Gar
Floor
14.89
3.11
11.9
Apron
14.8
3.2
11
14.7
3.3
10
13.1
3.9
7
14.1
3.9
6
14.3
3.7
6
14.5
3.5
10

18.00

18.00

2+43 14 Lt = End double bar. Conc. floor

11.9	B 11	11.7	11.8	11.5	11.7	11.7
6.01	6.2	6.3	6.2	6.7	6.3	6.3
14	14	10	7		0	10
Conc. Floor						

2+39 13⁵ Rt = 2 bar. drift floor No Foundation

12.01	11.8	11.8	11.8	11.9	11.7	11.8	11.9
6.01	6.2	6.2	6.2	6.6	6.3	6.2	6.1
14	14	10	7		0	10	13.5
Conc. Floor							

2+24^E 14 Lt = start double bars Conc. floor

12.10	11.9	12.1	12.2	11.6	11.8	12.0
6.00	6.1	5.9	5.8	6.4	6.2	6.0
14	14	10	8		5	10
Conc. Floor						

2+23 10² Rt = End lath fence

2+21 10¹ Lt = Pole # P.M. 4940

2+20 10.2 Rt = start lath fence
10.6 Rt = End shed

2+10 13³ Lt = End sing garage.
also 10² Rt = End wire fence and start shed.

12.45	12.2	12.3	12.0	12.0	12.1
5.55	5.6	5.4	6.0	6.0	5.9
13.8	13.7	10		4	10
Conc. Floor					

2+02 13³ Lt = start sing bar Conc. floor

12.45	12.4	12.4	12.1	12.2	12.5
5.55	5.6	5.6	5.9	5.8	5.7
13.8	13.7	10		4	10
Conc. Floor					

2+00 10¹ Rt = Line of wire fence

1+81 15² Lt = 2 sing bar drift floor

12.6	12.8	12.6	12.4	12.7	12.8
5.4	5.2	5.4	5.6	5.3	5.2
15.9	10	7		6	10

18.00

18.00

Alley BIK. 580.B.

3+07 9³ Lt. = Sing. Gar. dirt floor.

3+02 9³ Lt. = End board fence

2+82 10' Lt. = start board fence.

2+81⁵ 13⁸ Lt. = End double garage

2+71 16² Rt. = End double Gar.

2+65 13⁸ Lt. = start double Gar. Conc. floor no apron

2+56 16² Rt. = Start double garage conc. floor - no apron

Nail in
T.P. Pole PA 1940 2.27 15.48 4.79 13.21

2+44⁵ 14 Lt. = 3' wide Conc. walk

18.00

	11.0	11.0	10.8	10.8	
	4.5	4.5	4.7	4.6	
	9.9	7		7.0	
	11.42	11.4	11.4	11.6	10.9
	4.06	4.1	4.1	4.0	4.7
Floor	13.8	13.7	7.0	7	7.0
		11.4	11.3	11.0	11.1
		4.1	4.2	4.5	4.9
		7.0	7	7.0	7.0
					11.5
					11.63
					3.85
					16.4
					Floor
	11.53	11.5	11.6	11.4	11.0
	3.95	4.0	3.9	4.1	4.5
Floor	13.8	13.7	7.0	7	7.0
		11.8	11.7	11.1	11.4
		3.7	3.8	4.4	4.1
		7.0	7	7.0	7.0
					11.6
					3.88
					16.2
					Floor
	11.30	11.6	11.7	11.8	11.6
	6.59	6.5	6.3	6.6	6.4
walk	7.4	7.0	7	6	6
					12.1
					5.9
					7.0

~~Garage 2~~

18.00

Note $\left\{ \begin{array}{l} 5.4 \pm \\ \text{Floor - looks level so E.L. = end of} \\ \text{Garage full of furniture + junk.} \end{array} \right.$

3+73 \uparrow 17³ Rt. = End double Gar. Conc. Floor

3+62 14⁵ Lt. = Sing. Gar. dirt floor

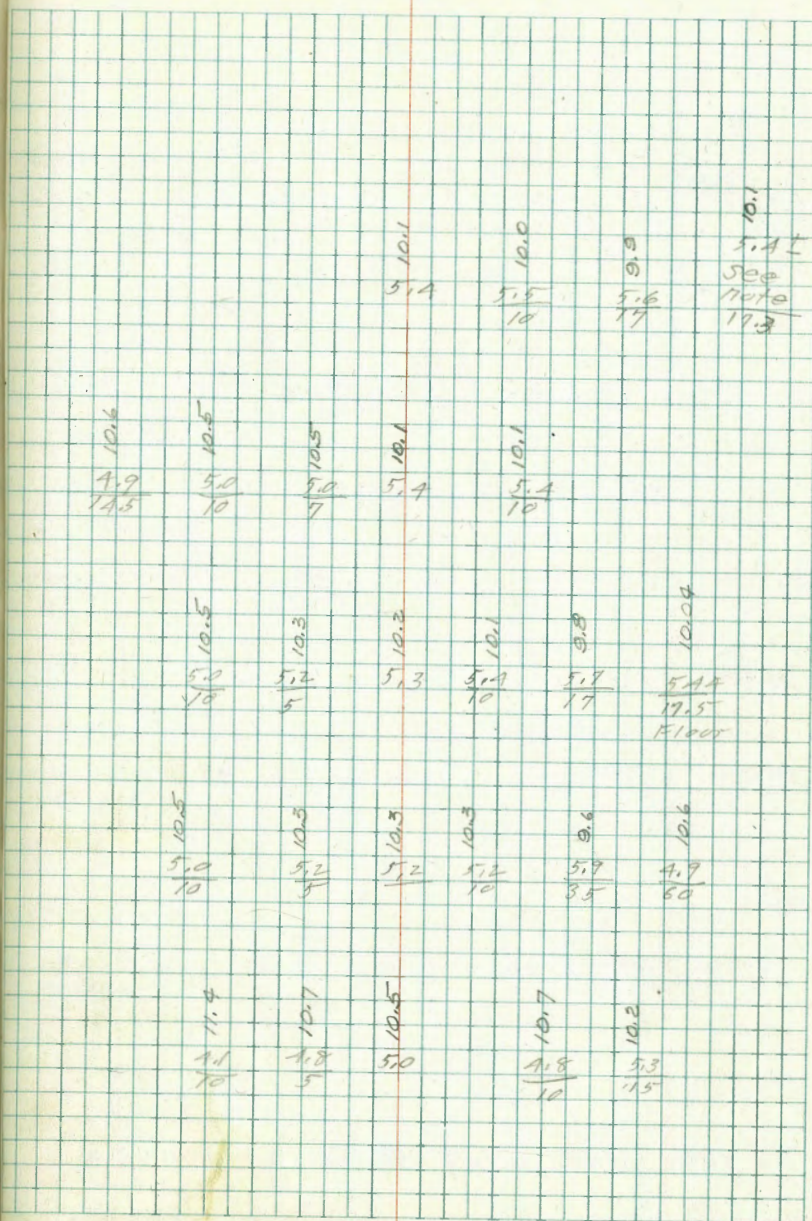
3+56 17⁵ Rt. = start double Gar. Conc. floor

3+50 9² Lt. = End board fence.
9⁵ Rt. = End lath fence

3+26 9⁴ Lt. = Pole ² R.H. 4954

3+21⁵ 9³ Rt. = Start lath fence

3+14⁵ 10⁴ Lt. = Start board fence



Alloy Bk. 58 Q. B.

4+26 10² Lt. = start pickat fence

4+25 9⁵ Lt. = ctr. 18" dead tree.

10² Lt. = start slat fence

10² Lt. = End Comb walk & @ar. Apron

4+22⁵ 9² Lt. = Pole # P. # 4970

4+17 13⁶ Lt. = # Sitg @ar. Conc. Floor

(Also = End of porch
to Sitg @ar. Conc.)

4+08 10² Lt. = start Comb walk + Apron

4+03 10² Lt. = start porch.

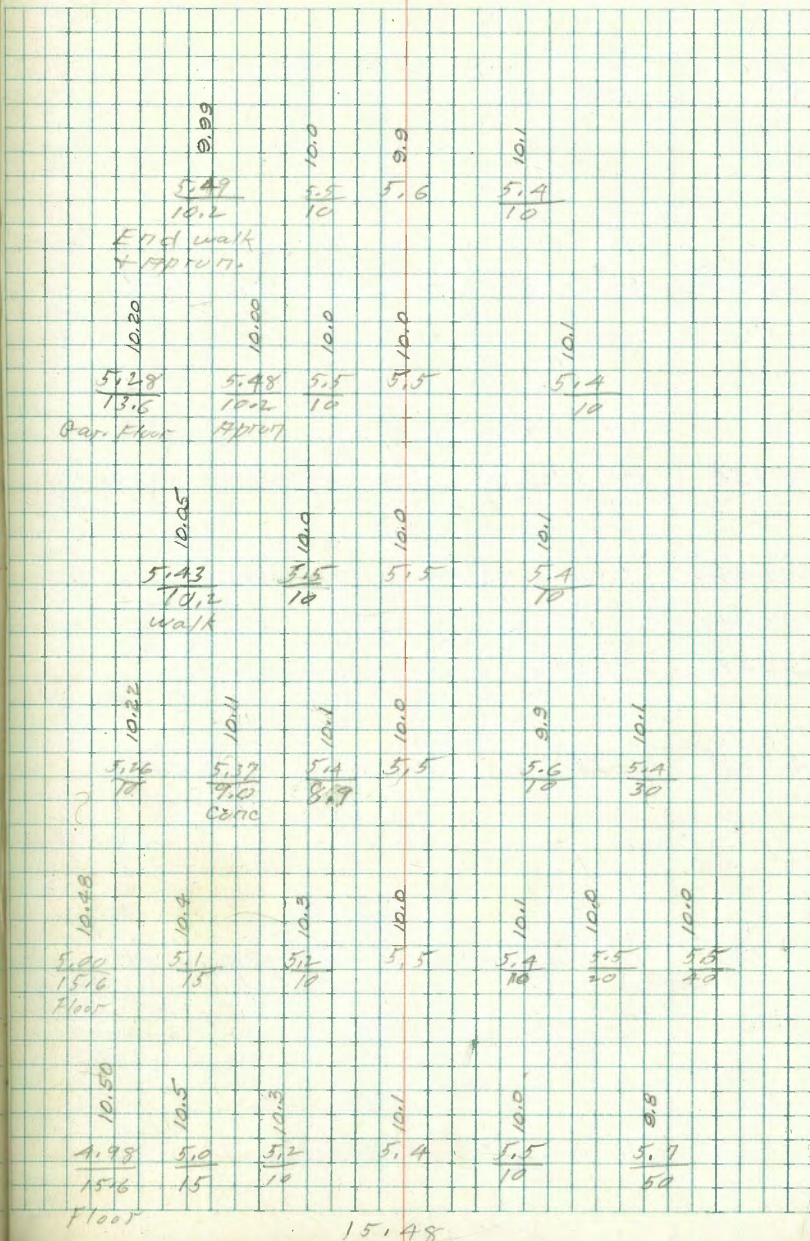
used as pier for porch corner.

4+02 9⁰ Lt. = # Conc. slab (see p. 6A)
Nuts 1/2 B

3+92 15⁶ Lt. = End double @ar. Conc. Floor

3+77 15⁶ Lt. = start double @ar. Conc. Floor.

15.48



15.48

A+65 19.3 Lt. = Φ double Garage.
 15.8 Rt. = Φ Double Garage

Conc floor

A+57^E 15⁸ Rt. = start double Gar.

Conc. floor

A+56 18³ Lt. = start double Gar.

9² Rt. = End Picket Fence.

A+49^E 9² Lt. = N. Face 10" diam post.

A+49 = 10² Lt. = End same

A+45 10² Lt. = start small shed

A+44^E 10⁶ Lt. = Φ 2' wide N+S walk

A+43^E 11² Lt. = End 2' wide Conc. walk

Conc walk

A+28 11² Lt. = start 2' wide E+W.

15.48

9.94	9.88	9.9	9.7	9.8	10.3	10.5	10.97
5.54	5.60	5.6	5.8	5.7	5.2	5.0	5.01
18.13	18	10		5	10	15	15.8
Floor							Floor

10.0	10.0	10.0	10.0	10.3	10.5	10.48
5.5	5.8	5.7	5.8	5.2	5.0	5.00
10		2	10	15		15.8
Floor						Floor

9.94	9.9	10.0	9.7	9.8	10.5	
5.54	5.6	5.5	5.8	5.7	5.2	
18.13	18	10		6	10	
Floor						

9.94	9.9	9.8	9.9	9.9
5.50	5.7	5.6	5.6	5.6
10.0	10	10	10	10
walk				

9.95	9.8	9.8	9.8	9.8
5.50	5.7	5.7	5.7	5.6
11.9	11.5	10	10	10
End walk				

10.01	10.0	10.0	9.9	10.2
5.47	5.5	5.5	5.6	5.3
11.9	11.8			10
walk				

15.48

5+25 9⁵ Rt. = End lath fence

5+19⁵ 13.7 Lt. = End of car Garage
10 = Lt. = End Conc. Apron

5+02 13² Lt. = Garage

4+84 10 Lt. = start Conc Apron to
1.6 car garage @ 13² Lt. = Bar.

4+75 9⁵ Rt. = start lath fence

T.P. 4.38 14.20 5.66 9.82

4+73 18.4 Lt. = }
15.8 Rt. = } End doors to double Bar
 } Conc. Floor

15.48

10.11	9.7	4.5	4.7	4.5	4.0	3.8
		10		5	10	20
10.11	9.65	4.52	4.6	4.6	4.4	
4.09	10	10	10	5	10	
13.9	End					
Bar Floor	Apron					
10.11	9.65	4.51	4.8	4.6	4.5	
4.09	10	10	10	5	10	
13.9	Apron					
Floor						
10.13	9.73	4.57	4.7	4.6	4.5	
4.07	10	10	10	5	10	
13.9	End					
Bar	Apron					
Floor						
			14.20			
9.94	9.0	5.6	5.9	5.7	5.0	4.98
		10	10	5	10	15
5.54	18					13.8
18.4						Floor
Floor						

15.48

1710y BIK, 58 O.B.

See sketch Page 75

5+65 16^E Rt. = start St 2100 Bldg.

12⁷ Lt. = start 2 story stucco Bldg.

5+61 12⁸ Lt. = End Apron to double Gar

5+52 15⁸ Lt. = 4 Gar.

start Conc Apron to double Gar.

5+42^E 12⁸ Lt. = End E+W, walk. Also

5+29^E 12⁸ Lt. = start 3' wide E+W, walk

5+26 10¹ Lt. = Pole # PA 4980

9^S Rt. = start plank + post retaining wall.

5+25^L 9^S Rt. = 4 N+S Retaining wall (Plank + post)

1A, 20

A.E.B.
"stuya"
OK

EB
How many times do you have to be told about stations on Bank of ...
Get location of Wood Retaining Wall and elevation along top put stations on garage as instructed 1984

9.87	9.65	9.6	9.4	9.4	9.1	9.5	11.8	11.0
4.33	4.55	4.6	4.8	5.3	5.1	4.3	2.1	2.3
15.8	12.8	12.7	10		7	9.4	9.5	20
floor	Apron							

9.85	9.65	9.6	9.5	9.1	9.5	11.7	11.0
4.35	4.57	4.6	4.7	5.1	4.9	2.5	2.3
15.8	12.8	12.7	10		9.3	9.4	20
Gar	Apron						
floor							

9.85	9.42	9.4	9.5	9.3	9.6	12.1	12.1
4.35	4.58	4.6	4.7	4.9	4.6	2.1	2.1
15.8	12.8	12.7	10		9.5	9.6	20
walk	walk						
+ Gar	Apron						
floor							

9.80	9.49	9.4	9.6	9.4	9.5	9.0	12.2	12.2
4.40	4.57	4.6	4.6	4.8	4.7	4.3	2.0	2.0
15.8	12.8	12.7	10		3	7.6	9.7	10
walk	walk							

9.7	9.5	10.1	12.3	12.3	13.05
4.5	4.7	4.1	4.9	1.9	1.8
10		7.6	7.7	10	20
			top		
			wall		

1A, 20

T.P. 4.53 12.11 6.62 7.58

5+99² E. Line Bacon = start A.C. Pav

5+97¹ ^{7.7 RT.} = start 3' wide N. & S. Conc. walk

5+97 also = E. N. & S. Plank Ret. wall
 9⁵ RT. = End plank retaining wall

5+94^E 12⁸ Lt. = End 2 story stucco.

5+86 10⁴ Lt. = E 3⁵ wide step.

5+70

14.20

7.77	7.41	7.07	7.10	7.54	7.78
6.43	6.79	7.13	7.10	6.66	6.48
7.92	7.8		4.5	9.6	9.68
Topd.	Pav			Pav.	Top curb
End					End

8.1	7.9	7.3	7.9	7.97	7.97
6.1	6.8	6.9	6.3	6.23	6.23
10	6		9.7	7.7	12
				Edge	
				walk	

8.50	8.1	7.4	7.3	8.5	10.8	10.8
7.7	6.1	6.8	6.9	5.4	7.1	3.4
15	10	6		7.5	10	15

9.22	9.21	8.7	8.1	7.9	8.2	9.6	10.9	10.9
4.98	4.99	5.5	6.1	6.3	6.1	4.6	3.3	3.3
12.8	12.4	10	7		7	9.5	9.6	14
at Bldg	at step							

8.6	9.4	8.9	8.6	8.6	8.7	11.4	11.4
4.6	4.8	5.3	5.6	5.6	4.5	2.8	2.8
12.8	10	8		7	9.5	9.6	14
at Bldg							

14.20

.01 or .02 higher
 curb. plug would be
 top of curb at hole in
 Plug out. - checked to

N/E Cape may
 + Bacon.

5.39. 6.72 6.76

Cont.

6+11 2 Ely Curb. line Bacon

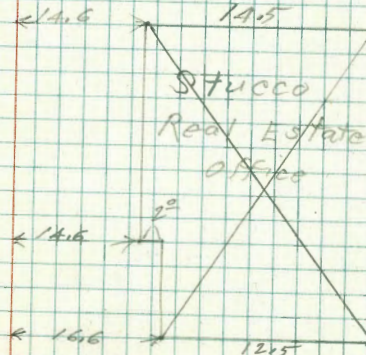
7.15	6.46	7.27	7.56	7.00	7.70
4.96	5.65	4.84	4.55	5.11	4.41
100	140	50	50	190	90
86	104	86	86	100	86

6.62	7.92	6.74	6.72	6.77	7.57	6.87
5.49	4.69	5.87	5.39	5.39	4.54	5.24
50	700	10	10	10	100	50
100	Rad. Rot.	10	12.11	10	Rad. Rot	100

5+94.5

5+74.5

5+65



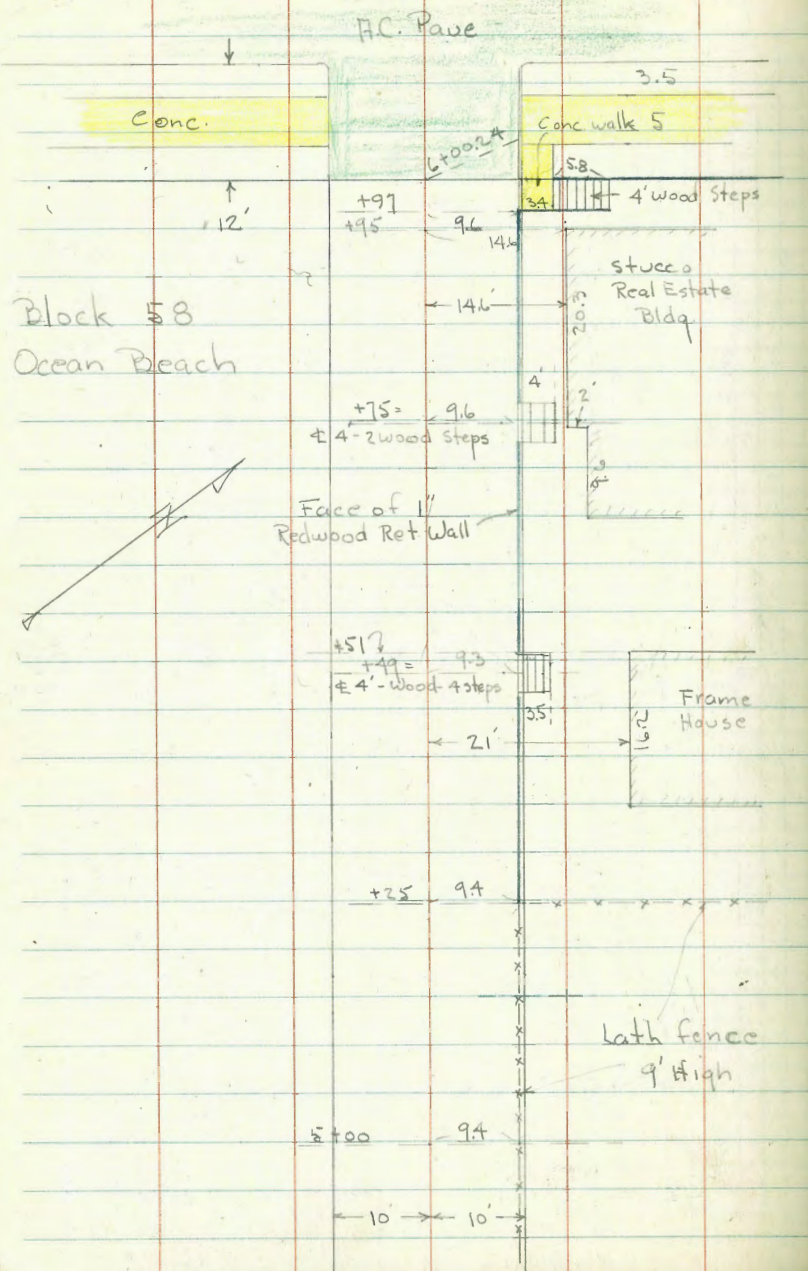
12.11

Bacon

st

90^{ca} lb.

77



Block 58
Ocean Beach

Detail of Alley in Block 58-OB
for Prop Retaining Wall. on NEly.
Side - Orig. Notes - P. 64

1-9-47

W.O. 25001

7.0.

Additional Notes on NEly. side
of Alley - Blk. 58 -

S+65 = opp. Ely. of Bldg.

S+51 = Opp. Wly. House

S+49 = \$ 4 Wood Steps - 4 steps

S+34.8 = opp. Ely. House

S+26[↓] = extend.

S+25 = o.k.

S+19.5 = Extend Sect.

S+00

T.P. Shawn 638 13.96
on P. 75

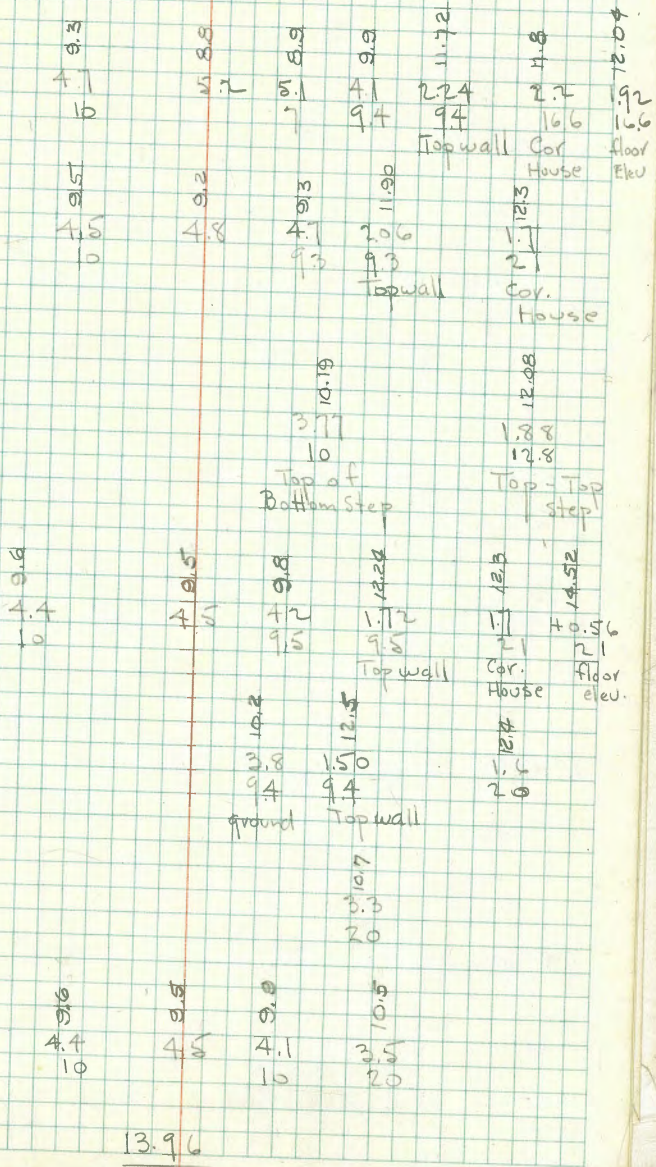
7.58

Lt.

ft

Rt.

78



6+03.74 = Back of 5' walks on Bacon

6+00.24 - Cont.

Cont on Rt.

6+00.24 - NEly. Line of Bacon - 5+99.7-P75

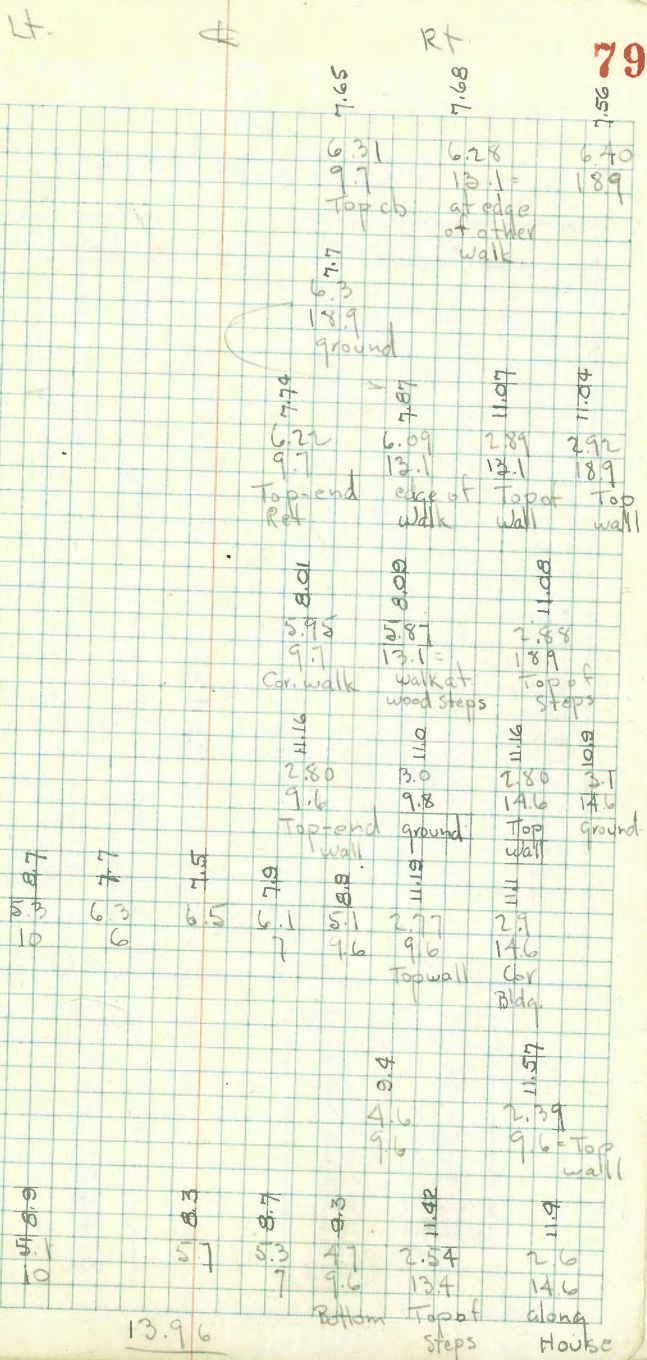
5+97 = 9.7 Rt. = Cor. Conc walk - low Sect.

5+97 - 9.6 - Rt. = End Ret wall - Cont. old Sect.

5+95 = opp. wly. of Bldg.

5+77 - 9.6 Rt = Ret wall at edge of Steps

5+75 = 4 wood steps on Rt - 2' steps



IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°-00' — 0.1	21°-00' — 12.8	33°-00' — 29.7
3°-00' — 0.3	21°-30' — 13.4	33°-15' — 30.1
4°-00' — 0.5	22°-00' — 14.0	33°-30' — 30.5
5°-00' — 0.8	22°-30' — 14.7	33°-45' — 30.9
6°-00' — 1.1	23°-00' — 15.3	34°-00' — 31.3
7°-00' — 1.5	23°-30' — 15.9	34°-15' — 31.7
8°-00' — 1.9	24°-00' — 16.5	34°-30' — 32.1
9°-00' — 2.5	24°-30' — 17.2	34°-45' — 32.5
10°-00' — 3.0	25°-00' — 17.9	35°-00' — 32.9
10°-30' — 3.3	25°-30' — 18.6	35°-15' — 33.3
11°-00' — 3.6	26°-00' — 19.2	35°-30' — 33.7
11°-30' — 4.0	26°-30' — 19.9	35°-45' — 34.1
12°-00' — 4.3	27°-00' — 20.6	36°-00' — 34.6
12°-30' — 4.7	27°-30' — 21.3	36°-15' — 35.0
13°-00' — 5.1	28°-00' — 22.0	36°-30' — 35.4
13°-30' — 5.5	28°-30' — 22.8	36°-45' — 35.8
14°-00' — 5.9	29°-00' — 23.5	37°-00' — 36.2
14°-30' — 6.3	29°-30' — 24.3	37°-15' — 36.6
15°-00' — 6.7	30°-00' — 25.0	37°-30' — 37.1
15°-30' — 7.2	30°-15' — 25.4	37°-45' — 37.5
16°-00' — 7.6	30°-30' — 25.8	38°-00' — 37.9
16°-30' — 8.1	30°-45' — 26.2	38°-15' — 38.3
17°-00' — 8.5	31°-00' — 26.5	38°-30' — 38.7
17°-30' — 9.0	31°-15' — 26.9	38°-45' — 39.1
18°-00' — 9.5	31°-30' — 27.3	39°-00' — 39.6
18°-30' — 10.1	31°-45' — 27.7	39°-15' — 40.0
19°-00' — 10.6	32°-00' — 28.1	39°-30' — 40.5
19°-30' — 11.2	32°-15' — 28.5	
20°-00' — 11.7	32°-30' — 28.9	
20°-30' — 12.3	32°-45' — 29.3	

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

107.19

116

108.35

623

101.72

99.92

400

94.52

826

86.26