

1771



THE  
MIA  
LIBRARY  
1837

1771

MICROFILMED

DEC 29 1964

CITY ENGINEER'S OFFICE

MADE IN U. S. A.

Our Leather Bound Engineers Note Books  
are carried in the following rulings:

- |                                 |  |
|---------------------------------|--|
| No. 380 LEVEL BOOK.             | Left and Right Hand Page<br>the same as Left Hand Page<br>of this Book.  |
| No. 382 FIELD BOOK.             | Left Hand Page as in this<br>Book, Right Hand Page 4x4<br>to the inch, Center Line Red.                                    |
| No. 384 MINING TRANSIT<br>BOOK. | Left Hand Page as in this<br>Book, Right Hand Page 8x8<br>to the inch, Center Line Red.                                    |
| No. 385 FIELD BOOK.             | Left Hand Page as in this<br>Book, Right Hand Page 8 ver-<br>tical and 4 horizontal lines to<br>the inch, Center Line Red. |

We also carry the Note Books listed above,  
bound in extra strong Fabri-Hide (otherwise  
the same quality of book,) which can be fur-  
nished at a somewhat lower price.

In ordering Fabri-Hide covered books, add  
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**THE FREDERICK POST CO.**

*ENGINEERING and DRAFTING SUPPLIES*

P. O. Box 803

CHICAGO

514  
21  
443

1993  
2353  
1810  
2055

Rancho Mission  
Beacon Hill

Proposed Trunk Sewer Sacramento, Mrs. etc, 1-

X-sec. Island - 25 to 26	21
" Nabaska, Maroulay to Capistrano	31
X-sec. Alley in Block 7, La Jolla Strand	46
Survey opening Ave. Comunal	54
X-sec. Alley Blk 13. Paulys Add.	} 59 to
" Myrtle - Mississippi to Alabama	

Check align. and levels of  
Sewer  
Proposed Trunk to serve  
"Rancho Mission", Meisch,  
"Beacon Hill" and Narragansett Hts.

Notes  
Begg Invert  
Green chain W.O. # 219  
Roberts "  
4-2-47

very windy

T.P. Back 9.81 282.57 0.95 272.70

2 + 92.54 1 2° 29' 30" 0.71 273.0

+ 50 1.1 272.1

2 2.5 271.2

+ 50 3.7 270.0

1 5.0 268.7

+ 50 5.5 268.2

0 + 00 6.2 267.5

T.P. 5.69 273.65 3.98 267.96

T.P. 10.91 271.94 0.55 261.03

T.P. 9.45 261.58 2.87 252.13

2" Pipe Sw. 1.56 255.00 253.44

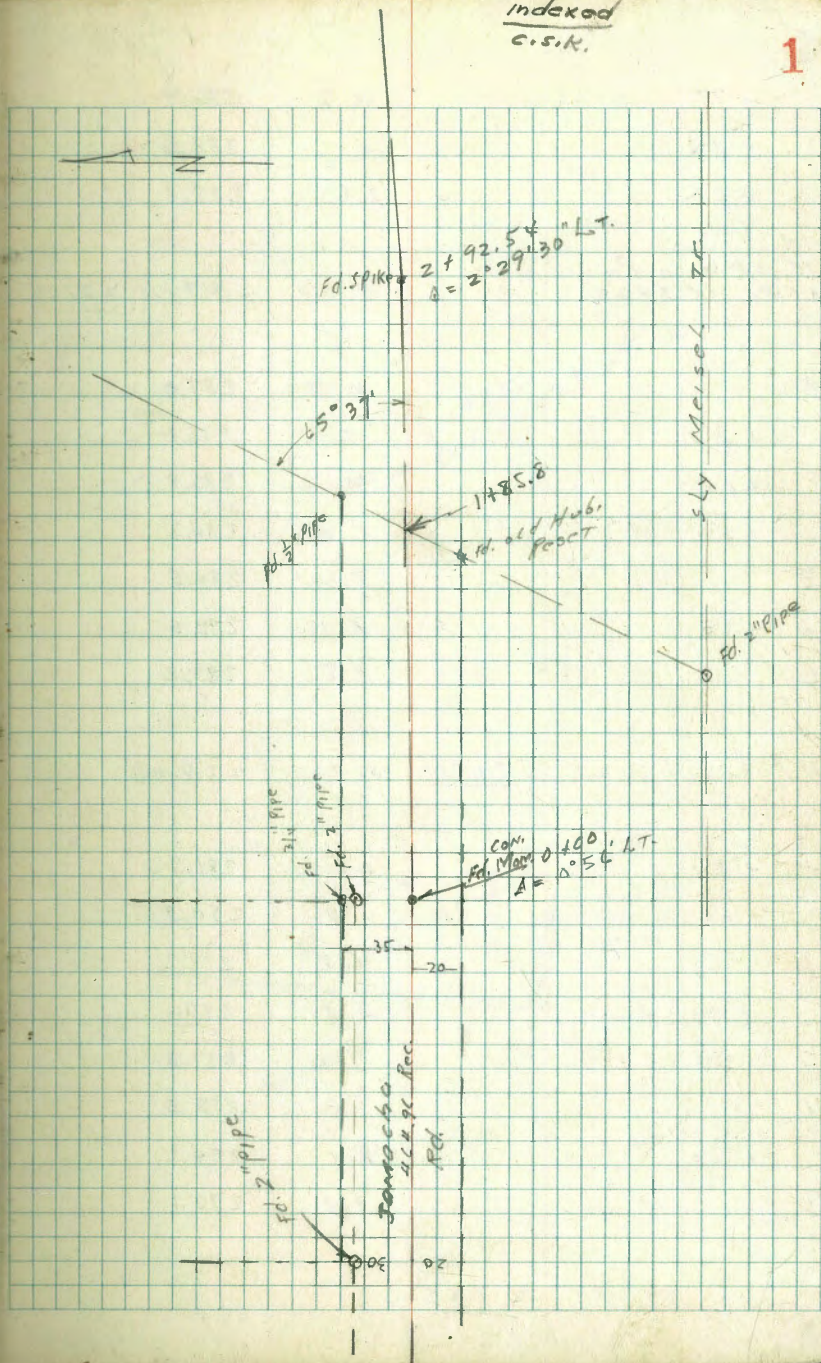
Box Culv.

Imperial

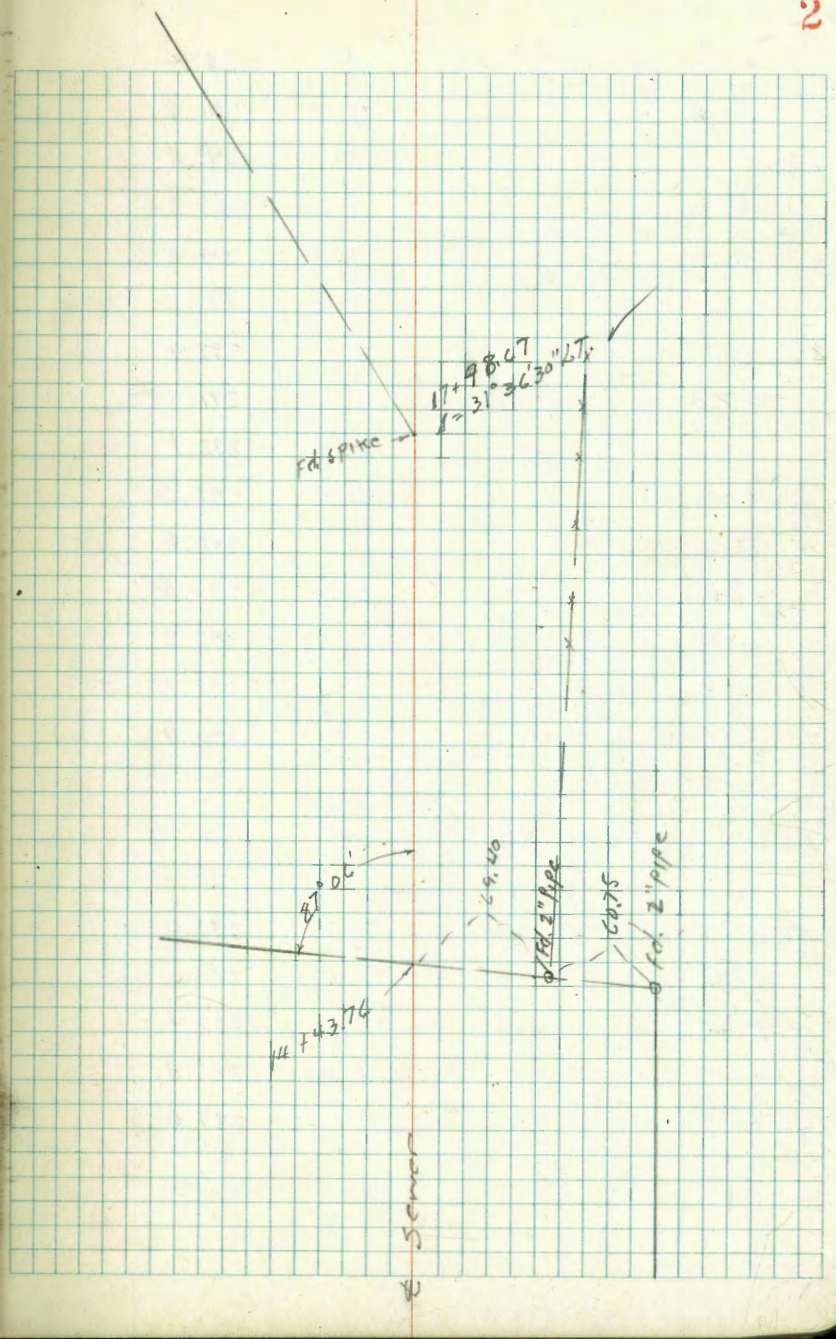
+ 69.74 F.B. 1558-37.

indexed  
C.S.K.

1



+77		4.8	286.9
+72		3.1	288.6
+50		2.6	288.1
FD			
BM, spike in Pole			
10' R of 8+35			
		4.07	287.61
			<u>287.58</u>
			0.03
8		4.7	287.0
+85		5.6	286.1
+65		4.9	286.8
+50		6.0	285.7
7		7.2	284.5
+50		8.1	283.6
6		8.5	283.2
T.P. Rock 1225 <u>291.71</u> 3.05 279.40			
+50		0.6	281.9
+04		1.7	280.8
5		2.8	279.7
+93		3.9	278.6
+50		5.2	277.3
4		7.0	275.5
+50		8.4	274.1
3		9.4	273.1
			<u>282.51</u>





T.P. 9.49 304.11 4.05 294.62

19 4.6 294.1

+50 5.5 293.2

18 6.7 292.0

17 + 98.67  $\Delta$  31°36'30" LT 6.7 292.0

+50 6.5 292.2

+04 6.4 292.3

+03 7.6 291.1

17 8.5 290.2

+96 cross wash 8.9 289.8

+94 + 9.8 288.9

+91 6.6 292.1

+50 7.2 291.5

16 7.6 291.1

+66 7.9 290.8

+50 8.4 290.3

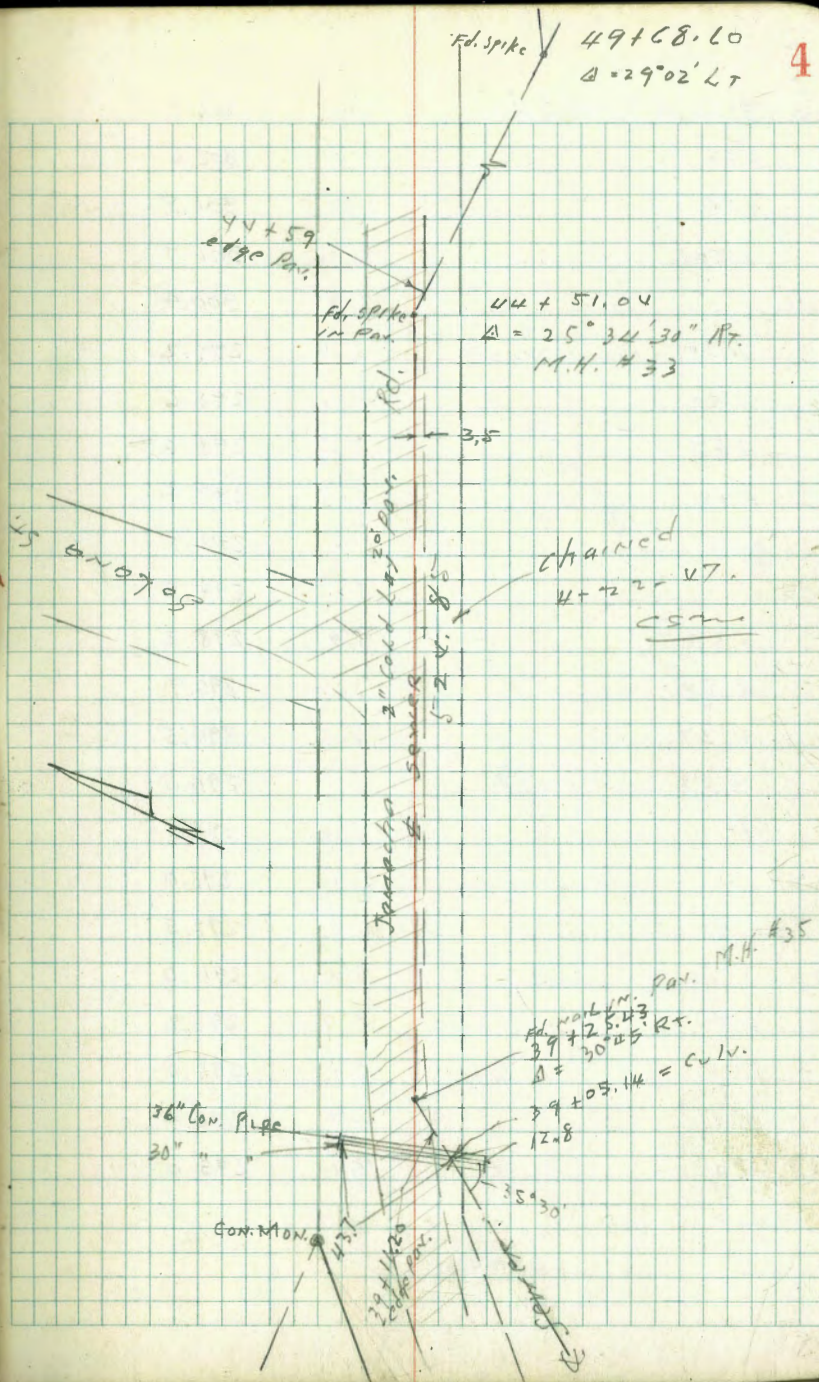
15 8.6 290.1

+50 8.6 290.1

T.P. 9.20 298.47 7.96 289.47

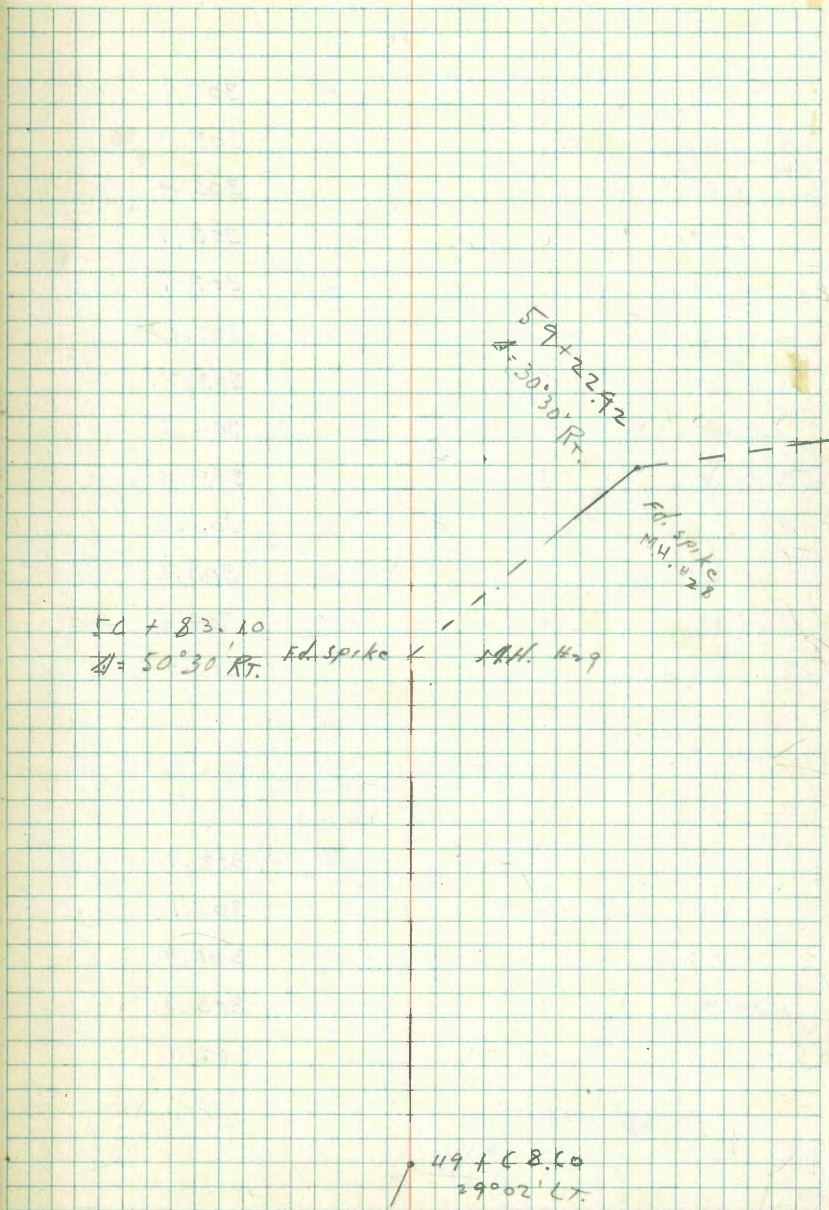
14 8.2 289.2

297.43



24	+93.50	A 19°18'27"	2.0	302.1
	+80		1.5	302.6
	+CC		2.3	301.8
	+50		2.2	301.9
24			3.7	300.4
	+55	Leave wash	4.9	299.2
	+50		5.5	298.6
	+37		5.5	298.6
	+24		6.7	297.4
	+17		6.2	297.9
23			5.6	298.5
	+55		5.9	298.2
	+50		7.2	296.9
	+37		9.6	294.5
	+29	in wash	8.1	296.0
	+14		5.6	298.5
22			6.1	298.0
	+50		6.6	297.5
21			7.1	296.0
	+72		6.9	297.2
	+50		6.1	298.0
20			7.7	296.4
	+19	+50	9.1	295.0

304.11





T.P. 12.75 319.03 4.22 306.28

+44.23	A (19 R)	3.4	307.1
28		4.8	305.7
+48	out wash	5.1	305.4
+47		6.8	303.7
+50		7.4	303.1
+38	in wash	7.4	303.1
+30		6.8	303.7
+25		6.0	304.5
+03		6.5	304.0
27		7.3	303.2
+64		7.3	303.2
+50		5.9	304.6
26		7.1	303.4

T.P. 7.63 310.50 12.4 302.87

+50	out wash	1.2	302.9
+46	in wash	3.0	301.1
+41		2.2	301.9
+34		0.8	303.3
25		2.0	302.1

304.11

M.H. 25  
K 8 124.68  
A = 21°47' R  
20°48' R

Fd spike

M.H. 26  
Fd spike

C 4 + 5413  
A = 20°11'30" L.T.  
18°10'30" L.T.

C 1 + 22.91  
A = 21°24' R  
20°20'30" R

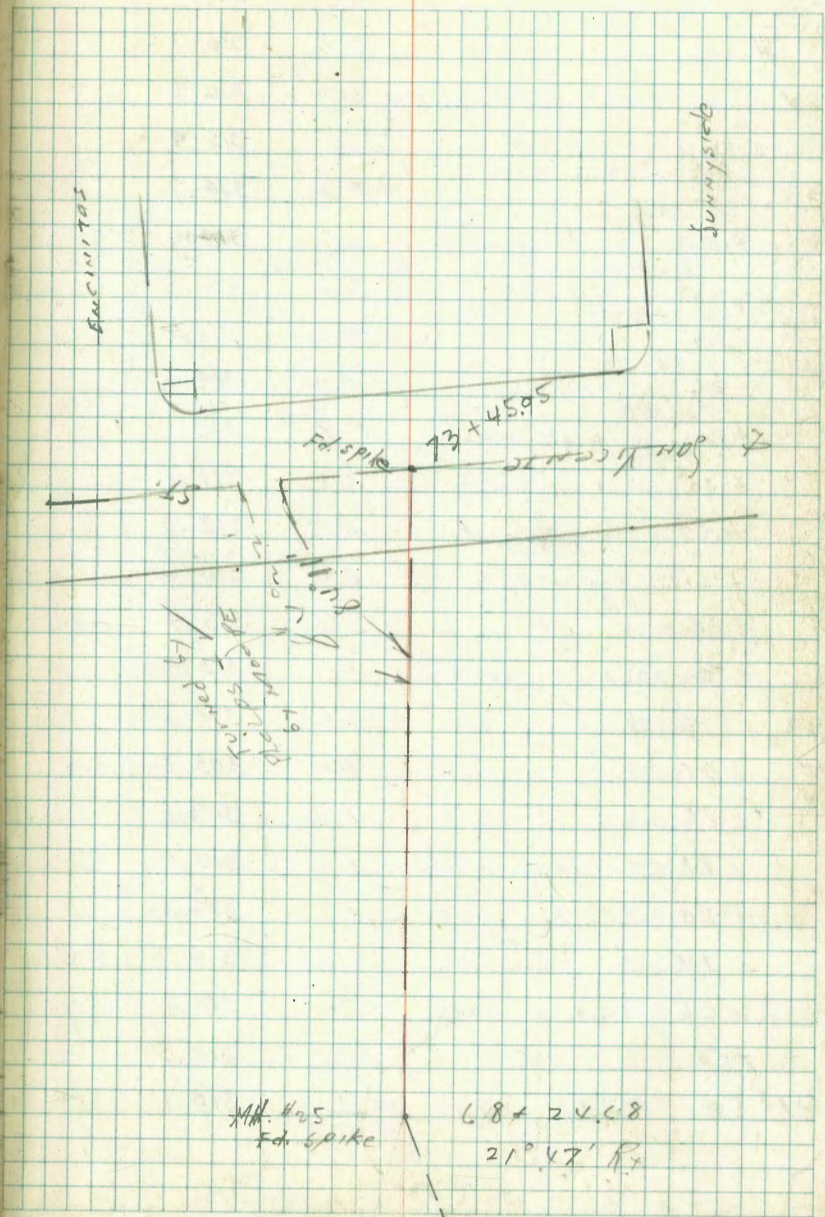
M.H. 27  
Fd spike

M.H. 28  
Fd spike

A 27 A 27.82  
A 30°30' R

+46		8.8	310.2
+40		9.4	309.6
+30		7.4	311.6
+31	in wash	8.0	311.0
+27		6.5	312.5
+20		8.5	310.5
+00		9.6	309.4
31		8.7	310.3
+81	out wash	10.5	308.5
+54		10.8	308.2
+50	in wash	11.5	307.5
+35		9.6	308.4
+19		9.7	308.3
+16		10.2	308.8
30		14.0	308.0
+77	out wash	11.8	307.2
+68	in wash	12.7	306.8
+50		11.6	307.4
+26	out wash	12.2	306.8
+20	in wash	13.0	306.0
+05		13.0	306.0
29+00		12.0	307.0
28+50		11.8	307.2

31903



35		1.6	317.4
+50		2.3	316.7
34		2.7	316.3
+50		3.0	315.4
33		4.3	314.7
+50	out wash	4.6	314.4
+44	side wash	6.8	312.2
31		4.6	314.4
+36		5.4	314.6
+37	out wash	6.9	312.1
+30	in wash	7.2	311.8
+27	out wash	5.5	313.5
+21	in wash	8.4	310.6
+18		5.6	313.4
30		5.1	313.9
+10	out wash	5.1	313.9
32		8.2	310.8
+94		9.1	308.9
+86		9.2	309.8
+81	in wash	8.0	310.0
+80		4.7	314.3
+74		4.3	314.7
29		5.0	313.0
+68	out wash	5.0	313.0
28		8.2	310.3
+60		8.2	310.3
31+50		8.9	310.1

319.03

40 +50		9.70	327.82	
T.P.	10.44	<u>336.30</u>	1.79	325.94
40		1.90	325.83	
+50		2.44	325.31	
39 +25.47	at 30° x 5 ft.	2.67	325.06	
+11.2	Reg. 2" Cold Exp. Pdy.	3.22	324.51	30° approx same
+05.14	43.7 ft.	6.54	321.19	30° in let
+05.44	42.8 ft.	6.95	320.78	out let 30"
+05.14		3.6	324.1	
Sat P.M. Con. Mon.		3.16	324.57	
5K. 10.11.01. 39.100				
39		3.2	324.5	
+85		5.3	322.4	
+50		6.1	321.6	
38		6.8	320.9	
+50		7.3	320.4	
37		7.4	320.3	
+50		8.0	319.7	
36		8.4	318.4	
35+50		9.4	318.3	
T.P.	9.74	<u>327.73</u>	1.06	317.97

319.03

49		2.8	343.7	
+50		4.3	342.4	
+15		4.8	341.9	
+08. wash		6.3	340.4	
+03		5.0	341.7	
48		4.8	341.9	
+50		6.2	340.5	
3 47		7.2	339.5	
+50		8.4	338.3	
46		9.0	337.7	
+50		10.2	336.5	
T.P.	11.33	346.7x	0.97	335.1x
30 45		1.2	335.2	
+59 end Cold Lay		1.3	335.1	
+51.0x Δ 25°34'30" R		4.3	335.1	
44		2.4	334.0	
+50		3.6	332.8	
43		4.6	331.8	
+50		5.5	330.9	
2 42		6.4	330.0	
28 +50		7.5	328.88	
41		8.5	328.72	

336.38

490		6.7	362.5	
+50		6.6	362.2	
55		8.8	360.0	
54+50		10.4	358.4	
54		10.3	358.5	
T.P.	11.61	<u>368.80</u>	0.82	357.19
+50		0.7	357.3	
53		3.3	354.7	
+50		5.4	352.6	
52		6.6	351.4	
+50		8.4	349.6	
51 1x wash		10.1	347.9	
50 + 50		9.4	348.6	
T.P.	11.97	<u>358.01</u>	0.70	347.0x
50		0.3	346.4	
49+48.6 Δ 29°02' L		1.5	345.2	
49+50		1.7	345.0	

346.7x

T.P.	12.06	<u>380.5C</u>	0.30	368.50
+50			3.1	365.7
+31			3.5	365.3
57			2.3	366.5
5C + 83/	Δ	50° 30' Pt	1.4	367.4
+55			5.1	365.7
+50			3.4	365.9
+30			6.1	362.7
56			8.6	360.2
55 + 97	Wash		7.3	359.5
55 + 96			8.8	360.0

369.80

+82			3.4	377.2
+50	Wash		4.6	376.0
+44			4.6	376.0
+41			3.3	377.3
+28			2.0	378.6
60			2.8	377.8
+52			6.9	373.7
+45	WASH		8.0	372.6
+40			7.3	373.3
+29	Δ	30° 30' Pt	7.7	372.9
59			8.4	372.2
+29			10.3	370.3
+44	WASH		12.0	368.6
+50			9.3	371.3
+38			8.7	371.9
58			10.8	369.6

380.5C

+73		3.2	388.7	
+50		5.4	386.5	
62		7.5	383.4	
+48		10.1	381.8	
+42		11.1	380.8	
+38		12.5	379.4	
+33	Wash	12.9	379.0	
+29		11.0	380.9	
41 + 22.91	△ 21° 24' P.	10.1	381.8	
T.P.	11.80	<u>391.89</u>	0.47	380.09
61		0.7	380.4	
+97		0.7	379.9	

380.56

64 + 54.13	△ 20° 11' 30" P.	7.5	396.4
+32		9.4	394.5
+30		10.7	393.2
+28		11.0	392.9
+25	Wash	11.9	392.0
+24		11.4	392.5
+23		8.8	395.1
+19		6.8	397.1
64		7.0	396.9
+87		7.3	396.6
+50		10.5	393.4

T.P. 12.77 403.86 0.80 391.09

A26		0.8	391.1
A12		3.5	388.4
63		3.1	388.8

391.89

+40		4.9	410.4	
+35		4.1	411.2	
+21		4.8	410.5	
66		2.2	408.1	
+75		9.0	406.3	
T.P.	12.00	<u>415.25</u>	0.01	403.25
+50		2.1	401.8	
+43	out	3.8	400.1	
+38	wash	5.9	398.0	
+18	wash	6.3	397.6	
+15		5.1	398.8	
65		4.7	399.2	
64 + 74		4.5	399.4	
				<u>403.80</u>

+97 wash 11.5 414.5 **12**

+96		10.4	415.6	
+81		9.5	416.5	
T.P.	11.37	<u>426.04</u>	0.58	414.07
+62		0.8	414.5	
+50		1.5	413.8	
+28		2.1	413.2	
+27		4.5	410.8	
+22		5.4	409.9	
+18		3.0	412.0	
67		1.5	413.8	
+92		2.3	413.0	
+74		5.5	409.7	
+54		7.5	407.8	
+50		9.6	405.7	
+49	wash	9.6	405.7	
66 + 43		6.0	409.3	
				<u>415.25</u>

+29	0.9	425.1
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70	2.1	423.4
----	-----	-------

+74	3.2	422.8
-----	-----	-------

+50	2.0	424.0
-----	-----	-------

69	2.1	418.9
----	-----	-------

+98	7.4	418.6
-----	-----	-------

+95 wash	9.0	417.0
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+80	7.5	418.5
-----	-----	-------

+67	5.4	420.6
-----	-----	-------

+50	6.6	419.4
-----	-----	-------

68 + 2468 Δ = 21° 47' RT	8.8	417.2
--------------------------	-----	-------

68	10.9	415.1
----	------	-------

426.04

+50	2.7	433.9
-----	-----	-------

+42	2.4	433.7
-----	-----	-------

+31	5.0	430.1
-----	-----	-------

72	6.9	429.2
----	-----	-------

+76	9.7	426.9
-----	-----	-------

+53 wash	9.5	426.6
----------	-----	-------

+48	7.8	428.3
-----	-----	-------

+40	7.4	428.7
-----	-----	-------

+18	9.0	427.1
-----	-----	-------

+12	10.1	426.0
-----	------	-------

+10	11.0	425.1
-----	------	-------

71 Wash	11.0	425.1
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+99	11.1	425.0
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+98	10.0	426.1
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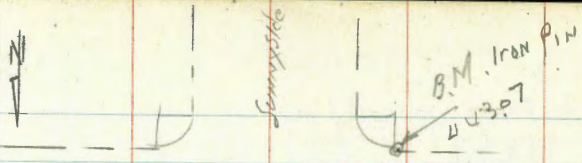
70 + 70	9.0	425.1
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T.P. 1170	436.12	11.2	424.42
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70 + 50	0.7	425.3
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426.04





San Vicente St.

Set B.M. Iron Pin Pt.  
SW Cor. San Vicente St  
& Sunnyside 2.97 443.07

73 + 4505 end Job 4.1 441.5 447.0  
on ground

+08 Shoulder fill 5.0 441.0

73 8.4 437.4

T.P. 11.6 446.0 1.7 434.38

+95 toe fill 1.4 434.7

+91 1.0 435.1

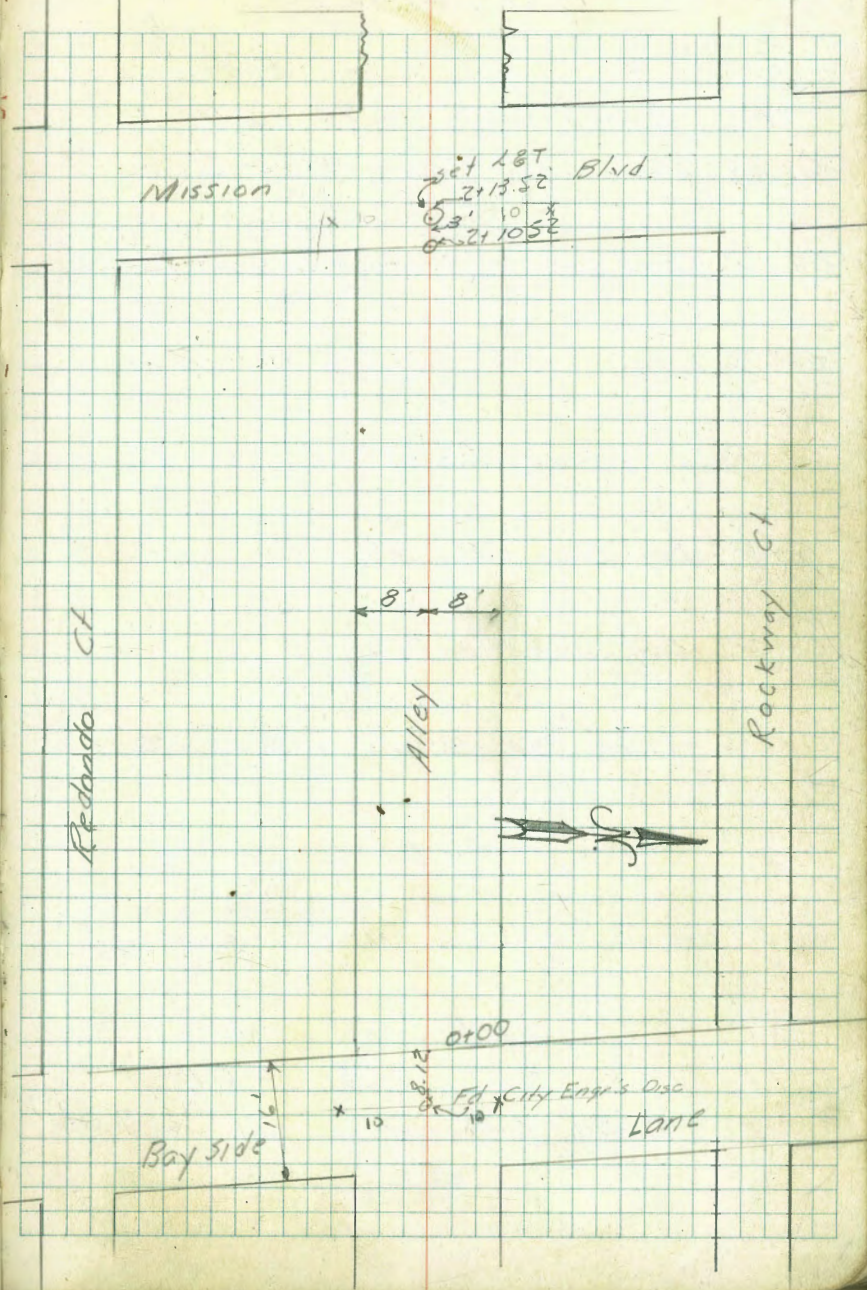
+84 2.2 433.9

72 + 58 3.7 432.9

436.12

July 14, 1947 X Sect's Alley Block 192  
 Hendricks  
 W Moore  
 Sherman  
 NO# 25001

Strand x 10 Way  
 Fd. City Engr's Disc 15





Levels Alley Block 192  
Mission Beach Cont'd

Sta. + H.L. - Elev B.M.

0+78 Beg Garage & Conc Ramp on Rt.

0+77 & 2' Conc Walk 7.8 Rt. E

0+76 End garage 14.0 Lt. Dirt Floor

0+75 End Shed 7.8 Rt. E

0+65

0+63 Beg Shed 7.6 Rt. E

0+60 End Conc Ramp & Conc. Floor Beg Dirt Fl. gar.

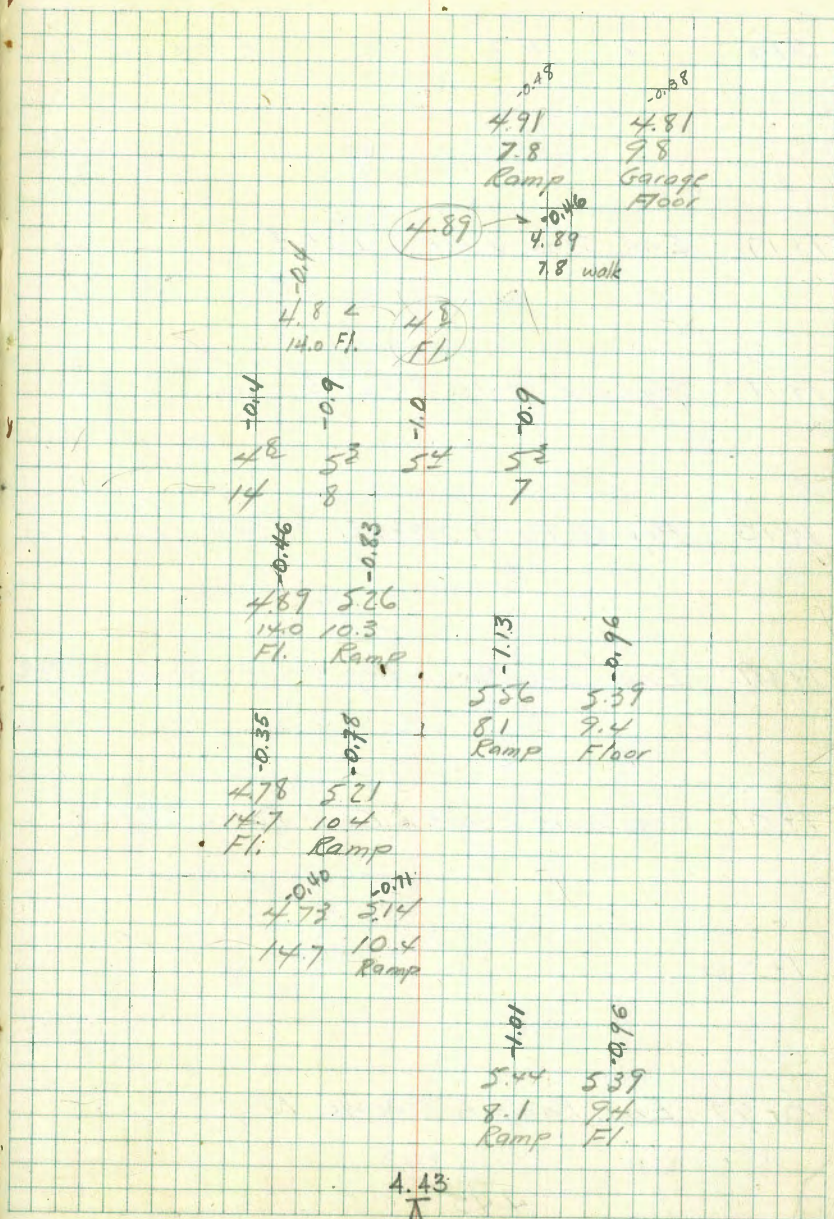
0+55 End garage & Ramp on Rt.

0+44 Beg Gar. 14.7 Lt. & Conc. Fl.

0+39 Beg Conc. Ramp 10.4 Lt. E

0+39 End Board Fence Beg. Gar 9.4 Rt. E  
Conc. Ramp & Fl.

4.43







Sta + H.I - Elev B.M

B.M 1.42 7.11 7.08  
T.P. 8.16 18.53 4.06 0.37

2+48.4 on East Edge of Parking Strip.  
Mission Blvd.

2+20.4 Ch Line Mission Blvd.

2+11.20 Beg Conc Paving.

2+10.52 PL

T.P. 5.25 4.43 5.25 -0.82

2+00

4.43

SWBP Sea Wall San Jose Pt.

4.49 4.60 4.53  
50 50

4.76 5.01 4.76 5.18 5.18 5.18 5.23 5.20 4.82 4.76 5.12  
50 50 10 10 808 772 102 102 50 50  
Cb G Cb G Cb G Cb G Cb G Cb

4.74 5.31 5.23 5.19 4.53  
808 808 772 772  
Cb G Cb

4.50 5.2 5.2 4.72  
808 8 77 7.72  
Cb Cb Cb

5.1 5.2 5.1  
80 80 80

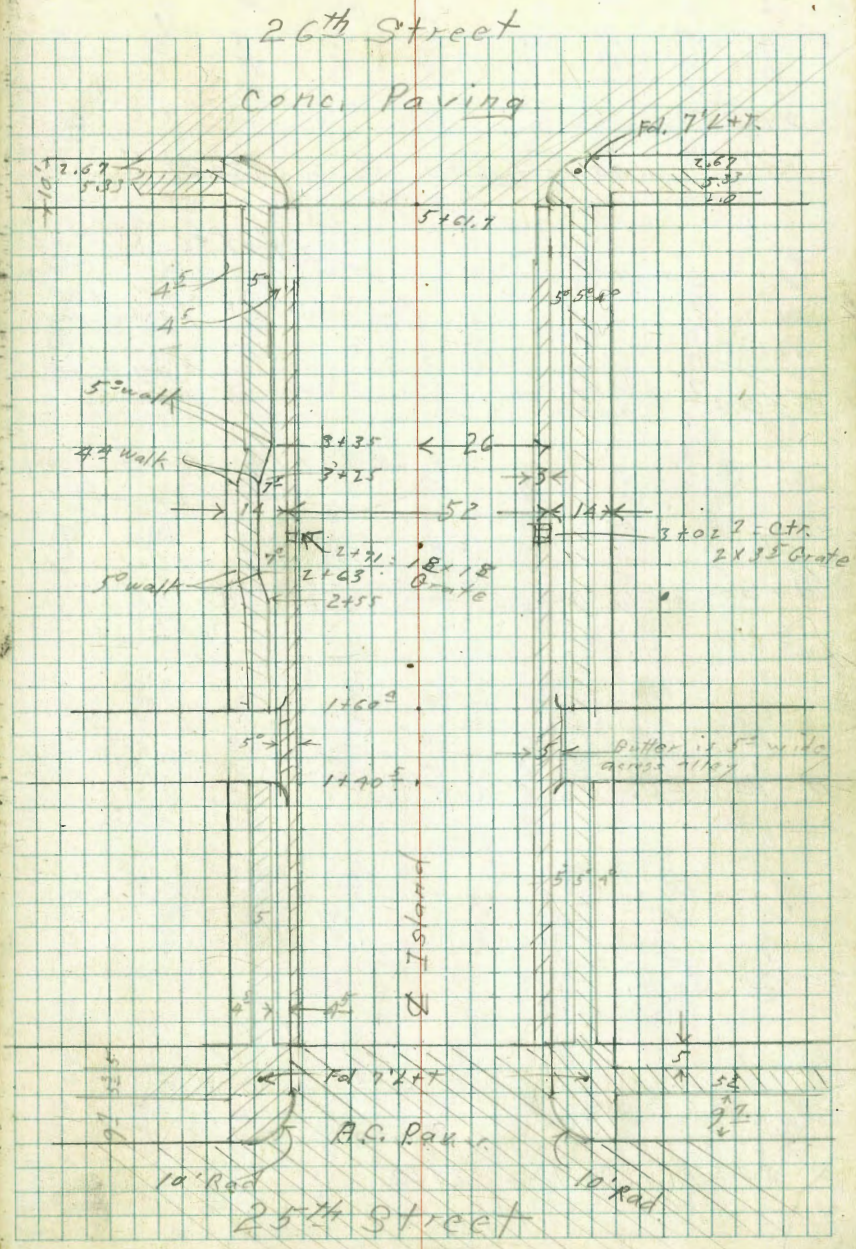
4.43

X-Section Island 25<sup>th</sup> to 26<sup>th</sup> 7-30-47  
 W.O. # 31183

Summer master  
 W Moore  
 Sherman  
 Lamore

NE B.P. 25<sup>th</sup>  
 to Island 8.96 137.63 — 130.67

Indexed  
 C.S.M.





0+25

T.P. 1.40 132.07 8.96 130.67

Note

13' Lt. + Rt. = Roadway  $\frac{1}{4}$   
 23' " " " = Edge of  
 3' Conc gutter  
 26' Lt + Rt. = Curb lines

0+00 - start Conc gutter

0+00 = Ely. line 25<sup>th</sup>

0-10 = E.C. Curb Ret.

0-20 Cont.

0-20 = Ely. Cb. line 25<sup>th</sup>

137.63

2.40 26 8.	3.18 26	3.14 23	2.7 15	2.9 17	3.8 13	4.88 23	5.07 26	9.50 26 ad.
129.67	128.89	128.93	129.37	129.17	128.27	127.19	127.00	127.57
130.64	129.90	129.88				128.42	128.38	128.61
8.99 26 cb.	9.93 26 Gut	9.25 23				11.21 23 Edge gut	11.25 26 Gut	11.07 26 cb.
130.66	129.93	129.94	129.74	129.64	128.93	128.51	128.45	128.62
8.97 26 cb.	9.70 26 Gut	9.69 23 on Pav	9.89 15 Pav	10.02	10.70 13 Pav	11.12 23 on Pav	11.18 26 Gut	11.01 26 cb.
130.63	129.88	129.79	129.71	128.92	128.34	128.63		
9.00 26 Top Cb.	9.75 26 Gut	9.87 13	10.22	10.71 13	11.29 26 Gut	11.00 26 Top Cb.		
130.62	138.69	130.65	129.99	127.75	128.59	119.91	119.91	128.57
0.26 1.40 Top Cb.	0.94 1.40 Gut	8.78 40 Top Cb.	9.61 40 Gut	11.88 40 Gut	11.09 40 Top Cb.	20.22 1.40 Gut	19.72 1.40 Gut	
130.62	129.80	129.76	129.54	129.15	128.77	128.29	127.88	128.57
9.01 36 Top Cb. S.C.	9.73 36 Gut	9.87 26	10.09 13	10.48	10.86 15	11.34 26	11.25 36 Gut	11.06 36 Top Cb. S.C.
			137.63					

T.P. Nail in  
Pole # 2517  
28' RT 1+38

1.74 120.80 13.01 119.06

1+00

0+74<sup>8</sup> End drive - start curb

0+64

0+59

0+57<sup>8</sup> End Curb Start drive

0+54

132.07

Lt.

±

Rt.

23

122.81	122.17	122.12	122.57	122.47	121.37	120.32	120.22	120.85
$\frac{9.26}{26}$ Curb	$\frac{9.90}{26}$	$\frac{9.95}{23}$	$\frac{9.5}{19}$	9.6	$\frac{10.7}{13}$	$\frac{11.75}{23}$	$\frac{11.85}{26}$	$\frac{11.22}{26}$ Curb
126.12	125.38	125.36						
$\frac{5.95}{26}$ Drive	$\frac{6.69}{26}$	$\frac{6.71}{23}$						
126.74	126.67	126.76	126.87	126.37	125.47	124.91	124.80	125.43
$\frac{5.33}{26}$ Drive	$\frac{5.40}{26}$	$\frac{5.81}{23}$	$\frac{5.2}{13}$	5.7	$\frac{6.6}{13}$	$\frac{7.16}{23}$	$\frac{7.27}{26}$	$\frac{6.64}{26}$ Curb
127.48	127.24	127.34	127.27	126.87	125.97	125.48	125.34	125.96
$\frac{4.64}{26}$ Drive	$\frac{4.83}{26}$	$\frac{4.83}{23}$	$\frac{4.8}{13}$	5.2	$\frac{6.1}{13}$	$\frac{6.57}{23}$	$\frac{6.23}{26}$	$\frac{6.11}{26}$ Curb
128.27	127.48	127.55	127.77	127.27	126.37	125.76	125.61	126.21
$\frac{3.99}{26}$ Curb	$\frac{4.75}{26}$ Curb	$\frac{4.66}{23}$						
$\frac{3.80}{26}$ Curb	$\frac{4.57}{26}$	$\frac{4.52}{23}$	$\frac{4.3}{13}$	4.8	$\frac{5.7}{13}$	$\frac{6.31}{23}$	$\frac{6.46}{26}$	$\frac{5.86}{26}$ Curb

132.07



2+00

1+90

T.R. 3.91 112.38 12.33 108.47

1+62<sup>A</sup> E.C. Alley Ret.

+60<sup>A</sup> Cont.

1.03  
62  
top wall

N+S.  
36.5 ft. - start Conc. Ret. Wall built  
1+60<sup>A</sup> Cont. on top of alley curb (6" wide)

1+60<sup>A</sup> Face Ely. Curb of N+S Alley

120.80

2.33 26 Ch.	3.97 26	2.97 23	2.7 13	2.7	3.7 13	4.74 23	4.94 26	4.30 26 Ch.
111.32	110.51	110.54	110.98	110.88	109.88	108.96	108.71	108.08
106 26 Ch.	187 26	184 23	14 13	1.5 114.38	2.5 13	3.42 23	3.67 26	3.03 26 Ch.
114.81	114.06	114.10	112.33	112.17	112.77	109.35		
5.97 26	6.74 26	6.70 23	8.47 23	8.63 26	8.03 26			
Curb E.C.								Curb LC
118.33	117.33	116.22	115.46					
2.47 42 top wall	3.47 40.1 top wall	4.58 40 top wall + 21"	5.34 40 top curb					
115.48	115.33	115.10	115.05	113.08	112.90	113.20		
3.32 36.3 top wall	5.47 36.3 Curb	5.7 29 Crd.	5.75 28 topok.	7.72 18 top Ok.	7.9 40 Crd.	7.60 26 end ok.		
114.41	114.24	114.36	114.60	114.60	113.60	112.56	112.42	112.65
6.39 28	6.56 26 Curb	6.44 23	6.2 13	6.2	7.2 13	8.24 23	8.38 26	8.15 28
				120.80			Enter	



3+60

3+40

3+20

3+08

+02<sup>1</sup> Cont.

3+02<sup>1</sup> =  $\phi$  Grate 25' Rts. { 24' N. + S. Culvert  
Thru Box.

120.80  
112.38

104.92	104.19	104.23	104.58	104.58	104.08	102.86	102.84	102.81	97.16
7.76 26 06	8.19 26	8.15 23	7.8 13	7.8	8.3 13	7.52 23	8.54 26 06	9.57 25	15.22 25
								Top Plate	F.L. Box
106.54	105.86	105.91	106.88	107.18	106.18	105.06	114.83	105.44	
5.81 26 06	6.52 26	6.47 23	5.5 13	5.2	6.2 13	7.32 23	7.55 26	6.94 26 06	
105.15	104.39	104.45	104.88	104.98	104.68	103.52	103.23	103.32	
6.65 26 06	7.46 26	7.46 23	6.6 13	6.5	7.2 13	8.20 23	8.37 26	7.70 26 06	
		Worked on point							
105.73	104.92		105.78	105.88	105.18	104.18	104.01	104.68	
103.46	103.24	103.86	103.46	103.24	103.46	103.24	103.86	103.24	
120.80	112.38	120.80	112.38						

T.P. 12.35 135.68 0.04 123.33

4+50

4+25

4+11

T.P. 12.78 123.37 1.79 110.59

4+00

3+90

3+80

112.38  
120.80

Lt

Rt

Rt

28

2.19 26 06.	3.05 26	2.97 23	3.2 13	3.6	4.2 13	4.61 23	4.74 26	4.84 26 cl.
121.08	120.31	120.40	120.17	119.77	119.17	118.71	118.43	117.33
7.13 26 cl.	7.85 26	7.91 23	7.8 13	7.9	7.0 13	7.86 23	9.99 26	7.29 26 cl.
116.24	115.52	115.41	115.57	115.47	114.37	113.51	113.38	114.08
7.82 26 cl.	10.52 26	10.48 23	10.2 13	10.4	11.6 13	12.66 23	12.79 26	12.17 26 cl.
113.55	112.85	112.89	113.17	112.97	111.77	110.71	110.58	111.20
111.64	110.85	110.83	111.58	111.28	109.08	109.04	108.86	109.53
0.74 26 cl.	1.53 26	1.55 23	0.8 13	1.1	2.3 13	3.34 23	3.55 26	2.85 26 cl.
110.23	109.43	109.51	109.98	109.78	108.78	107.73	107.55	108.21
2.15 26 06.	2.95 26	2.87 23	2.9 13	2.6	3.6 13	4.65 23	4.83 26	4.17 26 cl.
108.91	108.16	108.19	108.88	108.78	107.98	106.99	116.72	107.37
3.47 26 06.	4.22 26	4.19 23	3.5 13	3.6	4.4 13	5.37 23	5.66 26	5.91 26 cl.
108.23	107.43	107.51	107.98	107.78	106.78	105.73	105.55	106.21
112.38	120.80							

112.38  
120.80

5+612+ W. Line 26. <sup>to</sup> Start Conc. Paving.

5+50

5+40

5+25

T.P. 11.90 147.35 0.23 135.45

5+00

4+75

135.68

3.64 26.00	4.32 26	4.31 23	4.09 13	4.07	4.54 13	4.79 23	5.08 26	4.44 26.00
141.27	140.53	140.61	141.75	142.15	141.45	139.80	139.76	140.41
6.08 26.00	6.82 26	6.74 23	5.0 13	5.2	5.9 13	7.55 23	7.57 26	6.74 26.00
139.28	138.53	138.55	140.25	140.95	139.75	137.76	137.62	138.28
8.07 26.00	8.82 26	8.80 23	7.1 13	6.4	7.6 13	9.59 23	9.73 26	9.07 26.00
136.28	135.54	135.64	136.65	137.45	136.95	134.56	134.51	135.17
11.07 26.00	11.81 26	11.71 23	10.7 13	9.9	11.4 13	12.79 23	12.94 26	12.18 26.00
131.32	130.45	130.48	131.18	131.28	130.38	129.35	129.18	129.84
4.47 26.00	5.23 26	5.20 23	4.5 13	4.4	5.3 13	6.32 23	6.50 26	5.84 26.00
126.16	125.43	125.57	126.38	125.38	124.58	124.20	123.90	124.65
9.52 26	10.25 26	10.11 23	10.3 13	10.3	11.1 13	11.48 23	11.78 26	11.13 26.00
143.71	143.03	143.04	143.26	143.28	142.83	142.31	142.27	142.91

135.68



Orig B.M. (Page 21) 6.23 130.64 58.  
130.67

T.P. 0.51 136.87 10.79 136.36

T.P. 2.08 147.15 12.20 145.07

N.W.B.P. 25<sup>th</sup> + Market S, S, — 0.36 156.91 156.98

T.P. 11.85 157.27 ~~8.57~~ 145.42  
~~0.42~~ 153.99

Chisel & chr. }  
T.P. } 0.42 153.99 1.72 153.57  
S.W. Rot. }  
26 + Market }

T.P. 8.06 155.29 0.12 147.23

54912  
£ 26<sup>th</sup>

+712 Cont.

54712 Wly. Curb line 26<sup>th</sup>

147.35

145.61	145.44	145.22	145.14	144.95	144.83	144.69
1.74 40	1.91 26	2.06 13	2.21	2.40 13	2.52 26	2.66 40
147.07	146.53	143.92	143.95	142.43	142.95	141.14
0.28 140 06	0.82 140 part	3.43 40 06	3.70 40 part	1.92 40 06	4.40 40 06	6.21 100
143.90	143.38	143.24	143.08	142.94	142.68	142.53
3.45 36	3.97 36	4.11 26	4.27 13	4.41	4.67 13	4.82 26
E.C. Curb	Rot.					
147.35			147.35			
						Drive 140 06
						142.95 06
						142.41
						142.95 36
						Ch. Rot E.C.

x sec Wabaska Drive  
 Macaulay to Capistrano  
 For Opening

Moore  
 Bogg  
 Green  
 Roberts  
 9-8-47

N.O. 90051  
 Align Sketch and  
 Ref. for Property Lines  
FB 1387-6-8  
FB 1741-2

20' ± strip Cold Lay Pav.  
 Located off E on x sec.

1+50

1+25 23.5 Pt. end Eucals.

1+00

0+75 32 Pt. Beg. of Row of 10 Eucalyptus trees  
 16" to 24" di.

$\Delta = 40^{\circ}03'$   
 $\& P = 572.7$   $L = 699.00 \times 44 \times 572.7 = 401.02$

0+100 = B.C. Pt. at Eucalyptus FB 1387  
 Macaulay

BM. 3 nails  
 Strip Pole 6.70' 36.70 30.00  
 Macaulay  
 Eucalyptus  
 1387-19

11

8

R7

31

0.1	20.6
0.2	31.5
0.3	32.5
0.4	32.5
0.5	31.7
0.6	32.2
0.7	33.2
0.8	33.3
0.9	30.2
1.0	25.0
1.1	27.1
1.2	27.1
1.3	32.1
1.4	33.3

7.9	28.8
7.2	29.5
6.5	31.1
5.8	B12
5.1	30.7
4.4	32.0
3.7	24.0
3.0	25.7
2.3	26.6
1.6	29.6
0.9	31.5
0.2	32.7

30.70



+ 66

+ 40

6 + 00

5 + 50

T.P.

713

48.72

147

41.59

5 + 00

4 + 50

43.06

+ 7.7  
8  
55.9

+ 7.4  
28  
56.1

+ 3.5  
17  
45.2

+ 5.2  
15  
43.5

+ 7.7  
17  
44.0

+ 4.8  
15  
43.9

+ 4.4  
12  
44.3

+ 4.6  
27  
44.1

+ 13.5  
36  
35.2

+ 15.4  
40  
33.3

+ 11.5  
40  
37.2

+ 4.0  
50  
42.1

+ 5.4  
10  
54.1

+ 0.0  
31  
48.7

+ 3.3  
11  
45.4

+ 5.5  
15  
43.2

+ 6.3  
15  
43.5

+ 4.9  
7  
43.8

+ 4.9  
11  
43.8

+ 11.4  
27  
32.3

+ 14.4  
31  
34.3

+ 12.0  
39  
35.7

+ 9.0  
46  
34.7

+ 6.1  
50  
42.2

+ 9.7  
19  
57.9

+ 2.2  
28  
50.9

+ 4.8  
22  
43.9

+ 6.4  
11  
42.3

+ 5.1  
15  
42.6

+ 6.2  
15  
42.5

+ 5.7  
15  
43.0

+ 6.3  
14  
42.4

+ 16.8  
29  
31.9

+ 14.8  
22  
33.9

+ 14.5  
36  
34.2

+ 9.7  
42  
39.0

+ 7.8  
50  
40.9

+ 12.7  
19  
60.8

+ 2.8  
30  
51.5

+ 7.5  
17  
41.2

+ 1.1  
11  
41.6

+ 4.3  
14  
41.5

+ 5.2  
11  
42.1

+ 7.0  
10  
41.7

+ 17.0  
25  
31.3

+ 18.8  
11  
37.9

+ 9.2  
57  
39.5

+ 12.9  
15  
56.0

+ 6.7  
22  
49.8

+ 2.0  
19  
40.3

+ 2.5  
12  
40.6

+ 2.5  
15  
40.5

+ 2.1  
15  
41.0

+ 2.5  
12  
40.5

+ 18.1  
26  
33.0

+ 12.8  
30  
31.1

+ 10.5  
43  
32.6

+ 5.1  
50  
38.0

+ 14.1  
15  
57.2

+ 6.1  
28  
49.2

+ 3.8  
17  
39.3

+ 3.5  
12  
39.5

+ 3.9  
14  
39.7

+ 4.2  
21  
38.9

+ 8.6  
32  
34.5

+ 11.3  
35  
31.8

+ 11.9  
41  
31.2

+ 12.8  
44  
29.3

43.06

48.72

43.06

Bank















75.9	70.8	65.2	64.1	63.4	63.3	63.7	63.7	58.2	56.1	56.1	58.8	
+ 9.4	+ 7.3	+ 1.3	+ 2.4	+ 3.1	+ 2.2	+ 2.8	+ 2.8	+ 2.3	+ 10.8	+ 10.8	+ 7.7	
50	35	27	23	22	22	2	10	21	29	45	50	
73.2	68.5	62.8	61.9	62.0	62.6	62.6	57.0	55.4	52.3	53.4	55.5	57.2
+ 6.7	+ 2.0	+ 3.7	+ 4.6	+ 4.5	+ 3.9	+ 3.9	+ 9.5	+ 11.1	+ 14.2	+ 13.1	+ 11.0	+ 7.0
50	36	29	24	20	20	2	13	18	19	26	30	50
73.3	68.4	62.1	61.2	61.1	61.8	61.8	54.4	50.4	52.9	54.5	55.4	56.8
+ 6.8	+ 1.9	+ 5.1	+ 5.3	+ 5.2	+ 4.7	+ 5.7	+ 10.1	+ 16.1	+ 13.6	+ 12.0	+ 11.1	+ 7.7
50	37	28	24	20	20	2	16	18	19	24	39	50
71.5	67.0	62.0	60.6	60.7	61.2	50.5	50.4	52.2	54.9	56.3		
+ 5.0	+ 0.5	+ 4.5	+ 5.9	+ 5.8	+ 5.8	+ 16.0	+ 16.1	+ 14.3	+ 11.6	+ 10.2		
50	33	28	24	20	20	12	15	19	23	50		
70.4	65.7	60.8	59.5	59.6	59.9	59.9	57.6	51.7	49.7	51.2		
+ 8.4	+ 4.7	+ 0.3	+ 1.5	+ 1.4	+ 1.1	+ 1.1	+ 2.4	+ 9.3	+ 11.3	+ 9.8		
50	32	27	20	20	11	11	10	13	17	20		
61.03												

750

17 13 R7 P.P. #3554

175

16750

T.P. 6.06 66.54 0.55 60.48

16100

16400

61.03

61.03

52.7

53.7

54.6

+39 16 Ft. P.P. # P 3590

19

19

18+50

18+50

18+19 15 Ft. P.P. # 3562

J.P. 6.48 72.68 0.34 66.70

18+00

18+00

66.50

Lr

R

577

604

599

41

15.0  
5.0

12.3  
5.6

10.0  
6.6

+2.9  
5.0

75.6

+2.7  
2.7

70.0

+2.7  
2.0

67.0

+2.8  
2.8

66.9

+2.8  
2.8

66.9

+2.3  
2.3

67.4

+2.2  
2.2

67.5

+2.3  
2.3

62.4

+2.7  
2.7

57.5

+2.5  
2.5

56.8

15.0  
2.0

57.1

15.1  
2.0

57.3

13.8  
2.5

58.9

12.6  
2.3

60.1

11.8  
2.3

63.2

TOP WALL

+3.1  
5.0

75.8

+1.4  
2.0

71.3

+1.3  
2.0

66.4

+2.5  
2.5

66.2

+2.5  
2.5

66.2

+6.1  
3.0

66.6

+1.3  
2.0

66.4

+2.7  
2.0

63.0

+10.6  
2.9

62.1

+13.8  
2.0

58.9

72.68

1.1  
2.7

57.4

1.1  
2.7

59.4

1.0  
2.0

60.3

TOP WALL

+2.8  
2.0

75.3

+3.2  
2.5

69.7

+1.4  
2.0

65.1

+1.3  
2.0

65.2

+1.3  
2.0

65.2

+1.0  
2.5

65.5

+1.4  
2.5

61.1

+2.1  
2.0

58.1

+10.1  
2.0

56.4

+9.8  
2.0

56.7

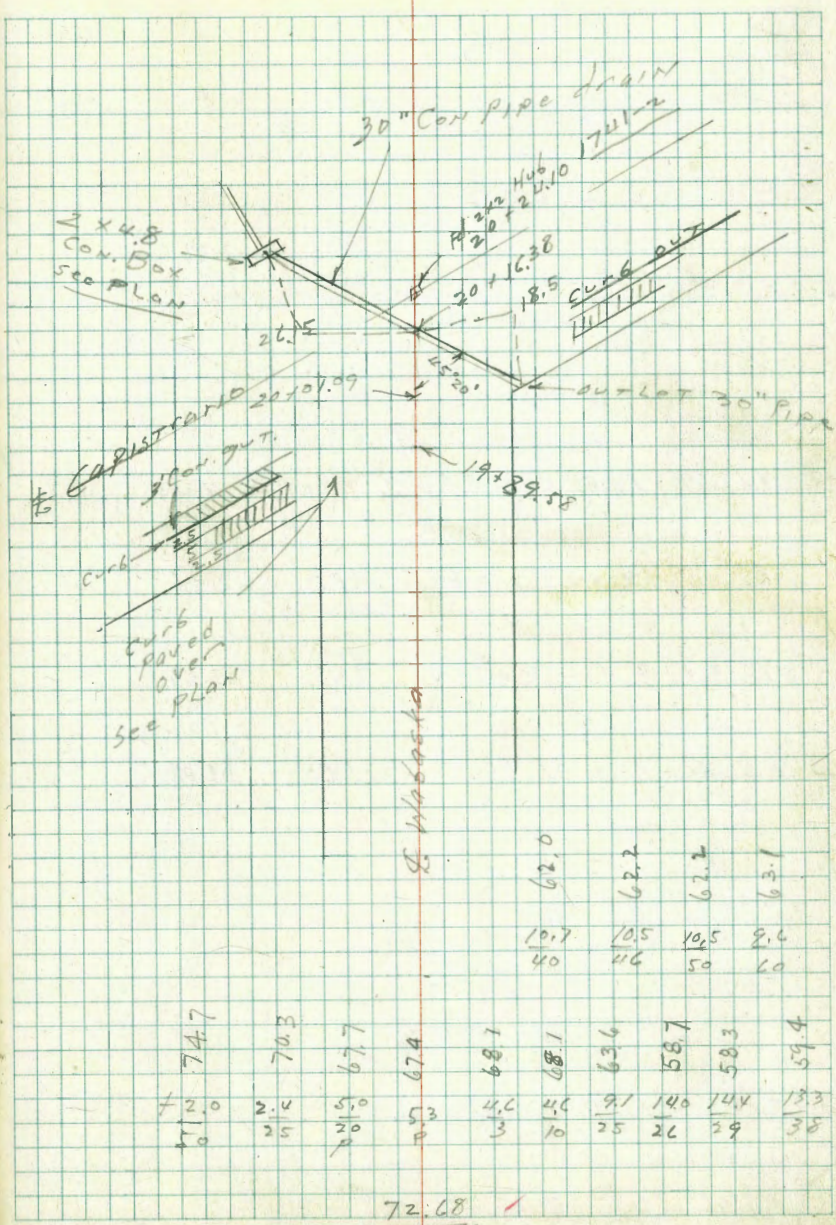
66.50

Levels cont'd. next page

19750

19750

72.68



72.68

Check to B.M. B.P. curb  
SE Pac & Chatsworth 2.36 78.18 78.21  
F.B. 1387-42 0.03  
Error

T.P. L.91 80.54 3.47 73.63

20+0109 Ely curb Capistrano  
END PAV.

19+89.58 Sec. on Ely Capistrano

T.P. 9.44 77.30 4.82 67.86 77.30

F.L. 2x4.8 Con. Box 7.15 63.03

F.L. out Lot 30" Con. Pipe 11.60 61.08

19+75

19+75 Sec. parallel with Capistrano

72.68

For 20+24.10 See F.B. 1741-7  
Capistrano

76.08	77.10	70.65	71.64	68.30	47.6	67.8	67.9	68.7
1.20	0.20	4.65	5.66	21.900	9.7	9.5	9.9	8.6
90	90	50	50	25		50	20	100
97	26	91	96	107				

74.5	72.6	69.9	68.5	68.1	69.0	67.8	67.9
0.8	4.7	7.4	8.8	9.2	8.3	5.5	9.4
60	50	26	23		20	50	20

67.2	67.7	67.4
5.5	5.0	5.9
42	20	20

75.1	73.4	70.4	68.0	67.8	66.8	66.9	63.7	60.1	59.4	60.9
12.4	10.7	2.3	4.7	4.9	3.9	5.8	9.0	12.6	13.3	11.8
20	50	30	23	7	4	9	20	24	27	32

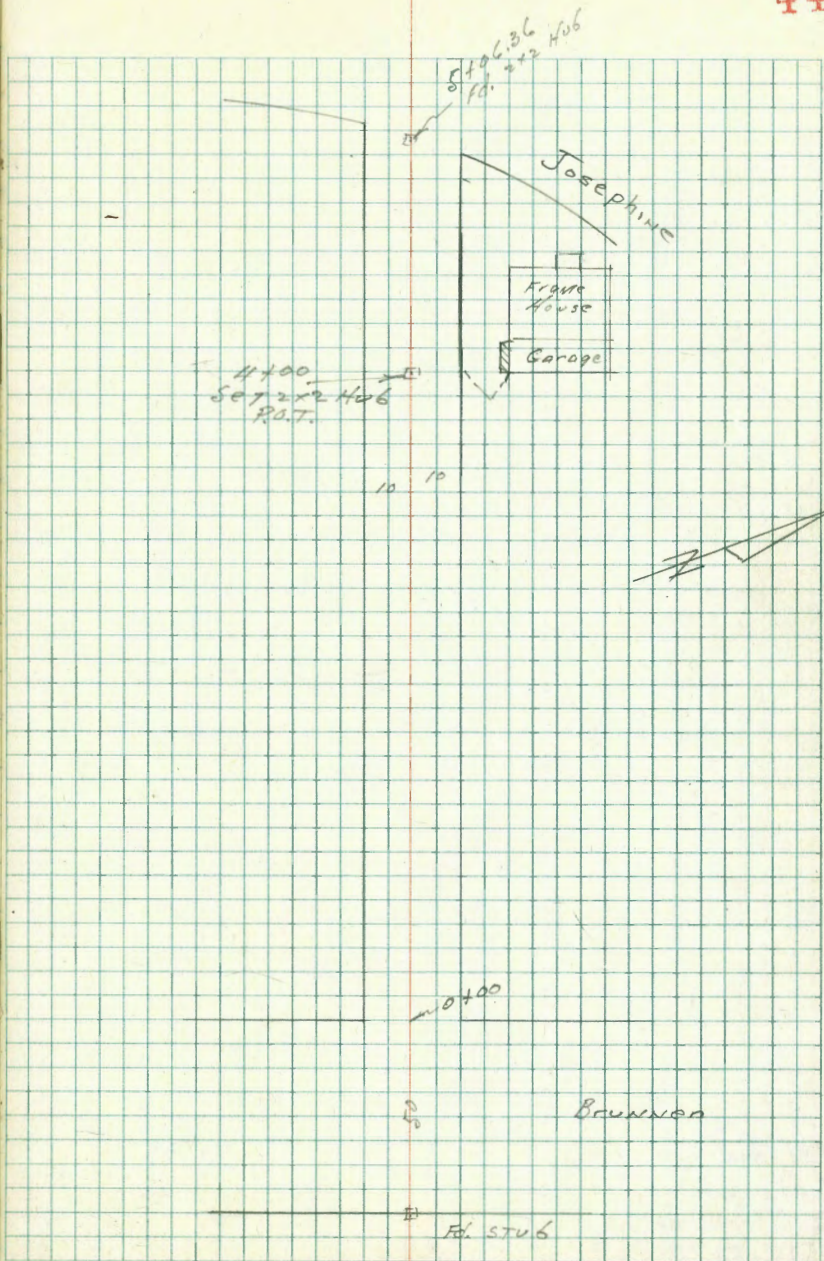
72.68

1.500 alley Blk. C

Silver Terrace

MOORE Sec Ref. F.B. 574-52  
 BC99  
 Parsons W.O. 31216  
 9-16-47

Cont'd. 1770



Lt = South  
Side

8

PT

45

~~CONF~~  
~~1772~~

B.M. Hub  
L alley +  
E.L. Josephine.  
574-52

130.32



Indexed  
C.S.K.

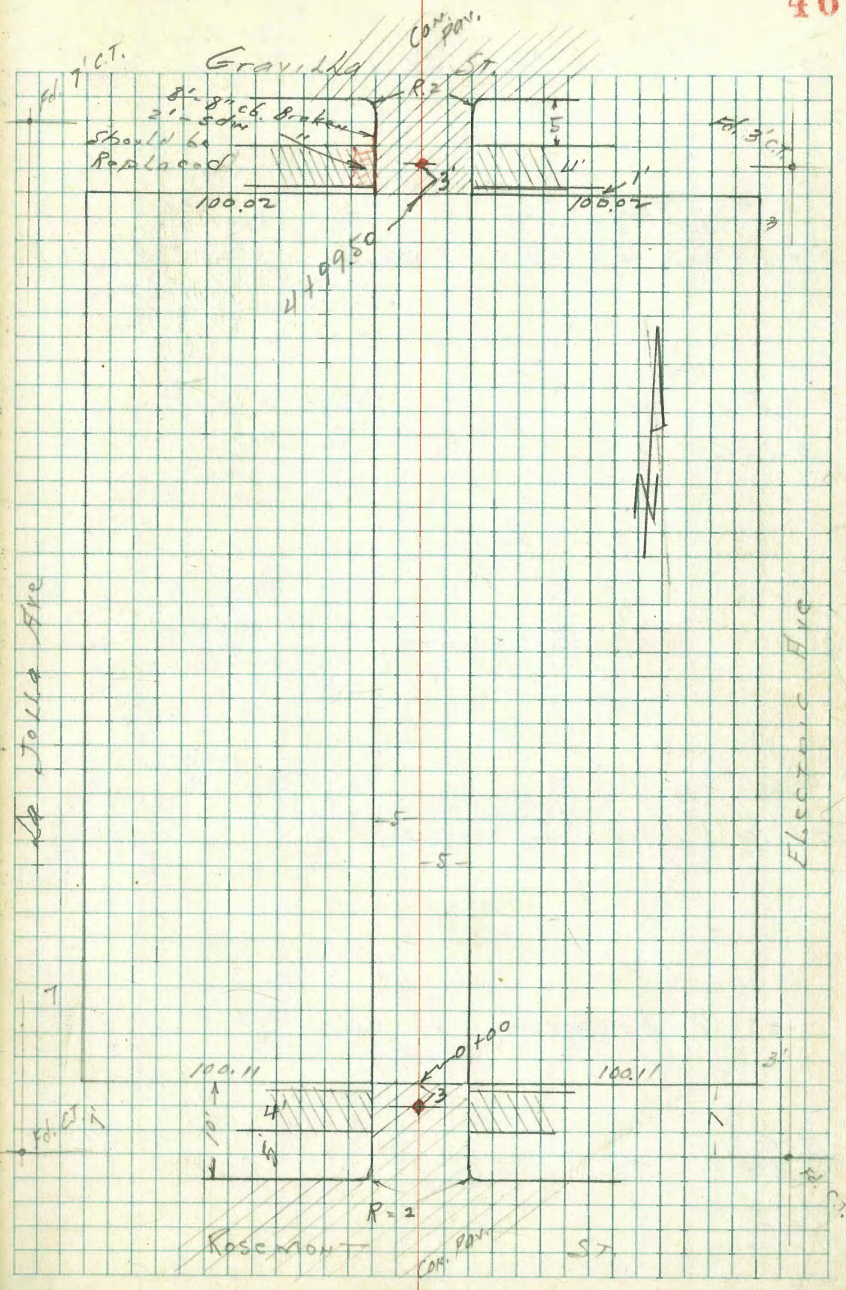
1 sec alley 10' wide  
Blk 7 La Jolla Strand (1216)

Moore notes  
Begg instr.  
Green chain  
Roberts chain  
10-6-47

W.O. 31261

• = set disk

John Lambert  
locate fences and poles



0120 4.6 1/2 E of 3' Con. walk <sup>garbage stand</sup>

0 + 18.3 4.7 1/2 end + east edge 1.5 Con. walk  
Parallel with alley

0 + 06

0 + 00 N.L. ROSEMONT 4.6 1/2 Beg. of E. h. of  
1.5 wide Con. walk  
parallel with alley

0 - 10 N c6. Line ROSEMONT

0 - 25 E ROSEMONT on Pav.

B.M.  
SEBP 7.05 90.85 83.80  
ROSEMONT  
ELECTRIC

LT = West  
84.58  
C. 27  
4.6

R 47

84.61	84.54	84.5	84.6	84.7	85.5	85.6
4.24	4.31	4.5	4.3	5.1	5.3	5.3
2	4.7	4.7		5	9	15
walk	walk	ground				

83.47	83.45	83.4	83.0	83.4	84.8	85.3
7.38	7.40	7.7	7.8	7.4	8.0	8.5
3	4.8	4.8		5	8	15
walk	walk	ground				

81.18	81.94	81.94	81.65	81.80	82.01
8.75	8.91	8.94	9.20	9.05	8.84
5	5	4.6	7.4	7.9	5.6
c6 and walk	Pav.	1/2 Pav. walk	Pav.		

81.74	80.65	81.87	81.27	81.33	81.44	81.81	82.04	82.53
9.64	10.20	9.08	9.58	9.54	9.41	9.04	8.81	8.32
45	45	7.6	7	7	7	7	5.0	5.0
26	97	26	77		97	26	77	26

81.14	81.91	82.70
9.74	8.94	8.15
5.0	Pav. M.H.	5.0

90.85

LT 29.5 7.3 RT <sup>strucen</sup> SW Cor. do. gar. Can floor, <sup>SLy</sup> entrance

1+13 C' LT, Beg. Bd. fence

0+98.3 E do gar. Can floor <sup>Level</sup> 14.7 wide

0+82 5.3 LT end Bd. fence

0+77 5.5 LT P.P. #419

0+60

0+45.2 5.2 LT, Beg. Bd. fence

0+41

0+27 5.6 LT, nudge of Can. <sup>Garbage</sup> <sup>stand</sup> <sup>Marfoara</sup>

0+25.5 5.2 LT, end Lattice fence

0+23 4.7 LT, Shaft

0+21.5 5.1 LT, Beg. Lattice fence

90.85

LT 82.4 82.4 82.6 83.3 84.10  
8.4 8.4 8.2 7.5 6.75  
6.2 5 5 5 7.2  
Fence Floor chg.

83.48 83.5 83.5 83.6 83.9  
7.37 7.3 7.3 7.2 6.9  
12.1 8.5 7.3 5 1.5  
Cap. floor

83.9 84.7 84.6 84.7  
6.9 6.6 6.5 6.4  
5 5 5 5

84.54 84.3 84.6 84.7 85.0  
6.3 6.4 6.2 6.1 5.8  
6.2 5 5 5 5  
door sill to Dwelling

84.54  
6.3  
5.2  
Can. <sup>garbage</sup> <sup>stand</sup>

90.85

2 + 94 E Sin 900 + Con, apron 8.2 wide

2 + 89 S, 6 Lt end Bd fence

2 + 52 Same N.H.

2 + 50 5.4 { Beg. Bd fence  
end wire fence  
46 Lt. P.P. Accu

2 + 00

1 + 64 6.9 Lt { Beg. wire fence  
NE Cor. Bd garage West  
entrance

1 + 50

1 + 48 7.2 Rt NW Cor Sinco 900, South  
entrance

1 + 40 6.4 Lt { S.E. Cor. of do. Bd. garage West  
end Bd fence entrance

T.P. #1 4.58 87.32 8.11 82.74  
90.85

Lt

6

R

49

80.37	80.30
6.95	7.02
6.0	5.7
99.0	apron

81.7  
6.1  
Apr

80.3	81.1	81.1	81.7	81.5
7.0	6.2	6.2	6.1	5.8
15	5	6.2	5	15

81.3	81.6	81.4	81.8	81.9	81.9	82.7	82.8
6.0	5.8	5.9	5.5	5.4	5.4	4.6	4.5
20	22 fence	5	5.5	5	7	10	15

82.3	82.3	82.6	82.9	83.2
6.0	5.0	4.8	4.4	4.1
6.5	5	4.8	5	15

against  
garage

87.32

3476

3450,7 U.S. R. Beg. 3.5 wide Con Walk Parallel

3450 S. 2 Lt. against Lark fence  
S. Lt. P.P. P.H. CCC9

3445

3420 N. edge do. Con gar. + Con apron  
Flood

3404 S. edge do. gar. con flood + apron

3400 S. 5 Lt. Beg. Lark fence

8732
$$\begin{array}{r} 80.3 \\ 7.0 \\ \hline 15 \end{array}$$
$$\begin{array}{r} 78.4 \\ 8.9 \\ \hline 5 \end{array}$$
$$\begin{array}{r} 78.6 \\ 8.7 \\ \hline \end{array}$$
$$\begin{array}{r} 78.9 \\ 8.4 \\ \hline 5 \end{array}$$
$$\begin{array}{r} 78.6 \\ 7.7 \\ \hline 11 \end{array}$$
$$\begin{array}{r} 79.84 \\ 7.48 \\ \hline 11.8 \end{array}$$
W. edge 3.5  
Con Walk
$$\begin{array}{r} 72.68 \\ 7.64 \\ \hline 11.6 \\ \text{W. edge Walk} \end{array}$$
$$\begin{array}{r} 79.4 \\ 8.3 \\ \hline 15 \end{array}$$
$$\begin{array}{r} 79.3 \\ 8.0 \\ \hline 5 \end{array}$$
$$\begin{array}{r} 79.1 \\ 8.2 \\ \hline \end{array}$$
$$\begin{array}{r} 79.3 \\ 8.0 \\ \hline 5 \end{array}$$
$$\begin{array}{r} 79.6 \\ 7.7 \\ \hline 15 \end{array}$$
$$\begin{array}{r} 80.74 \\ 6.60 \\ \hline 12 \\ \text{apron} \end{array}$$
$$\begin{array}{r} 80.91 \\ 6.41 \\ \hline 14.9 \end{array}$$
$$\begin{array}{r} 80.70 \\ 6.62 \\ \hline 12 \\ \text{apron} \end{array}$$
$$\begin{array}{r} 80.97 \\ 6.40 \\ \hline 14.9 \\ \text{gar.} \end{array}$$
$$\begin{array}{r} 80.11 \\ 7.2 \\ \hline 5 \end{array}$$
$$\begin{array}{r} 80.4 \\ 7.1 \\ \hline \end{array}$$
$$\begin{array}{r} 80.4 \\ 6.9 \\ \hline 5 \end{array}$$
$$\begin{array}{r} 80.6 \\ 4.7 \\ \hline 15 \end{array}$$
8732

4450 5.6 Lt P.P. P.A. 1187  
 4449.5 6.8 Rt end Bd fence  
 4448 5.9 Lt end Lark fence  
 4437 6.9 Rt Beg. Bd fence

4414 E Sim. gar Con. floor wide

4400 5' Rt Ed 1" pipe Con.  
 3499 6.2 Lt Beg. Lark fence  
 3497 11.7 Rt. N edge Con Landing to stairs

3492.5 E Sim. gar 6.2 Lt. W. entrance  
 12.5 wide  
 3480.1 S edge Con Landing at foot of stairs  
 Con.

3480 N. end Con apron for walk  
 90.7

3486.5 6.2 Lt end Lark fence

3485 E Sim gar. Con apron is continuation  
 of 3.5 walk

87.32

27  
 $\frac{76.6}{10.7}$   
 5  
 76.3  
 140  
 76.5  
 $\frac{10.8}{5}$   
 17  
 81

77.4  
 $\frac{10.1}{1.5}$   
 77.5  
 $\frac{9.8}{5}$   
 77.5  
 98  
 77.7  
 $\frac{9.6}{5}$   
 78.1  
 $\frac{9.2}{12}$   
 78.57  
 $\frac{8.80}{15.2}$   
 Con. gar. Floor

78.1  
 $\frac{9.2}{5}$   
 78.1  
 9.2  
 78.3  
 $\frac{9.0}{5}$   
 78.4  
 8.9  
 11.6  
 78.76  
 $\frac{7.56}{12.7}$   
 Con. Landing

79.94  
 $\frac{7.38}{11.7}$   
 79.94  
 $\frac{80.08}{7.22}$   
 $\frac{14.2}{15.2}$   
 Con. Landing at Landing at Bot. step

79.57  
 $\frac{7.80}{11.7}$   
 79.57  
 79.90  
 $\frac{7.42}{15.2}$   
 apron

79.63  
 $\frac{7.69}{11.7}$   
 apron  
 79.97  
 $\frac{7.35}{15.2}$   
 gar. Floor

87.32

S. cb line Gravilla

4+99.5 S. L. Gravilla

4+98

4+79.5 S. 8 LT N edge Con apron  
N. entrance

4+74.5 S. 8 LT NE Con Bldg apron N. entrance

4+54.7 S. 7 LT S.E. Con. Bldg apron North entrance

4+52 5' LT to Ctr. of 24" dia. Eucaly tree

T.P.#1 3.42 80.11 10.63 7669  
8732

72.71	72.10	73.70	73.04	73.16	73.79	73.91	74.13	74.84
7.40	8.01	6.35	7.07	6.23	6.82	6.20	5.98	5.27
50	50	50	50	50	50	50	50	50
66	66	66	66	66	66	66	66	66

73.87	73.63	73.43	73.65	74.04
6.2*	6.48	6.18	6.00	6.07
5	5	5	5	5
66	66	66	66	66

74.1	73.9	73.9	74.4	75.1
6.0	6.2	6.2	6.2	6.0
5	5	5	5	5
66	66	66	66	66

75.50	75.55
4.55	4.56
5	5
66	66
N edge apron	edge apron

76.44	76.47	76.17	76.16	75.6	75.7	74.9	74.1
3.66	3.69	2.14	4.7	4.6	4.4	4.1	4.0
5	5	5	5	5	5	5	5
66	66	66	66	66	66	66	66
N Garage	990						

80.11

check T.P. 5

STARTING B.M.	5.52	89.32		83.80	
T.P. #1	2.59	85.33	6.58	82.74	82.74 ✓
T.P. #2	3.45	80.12	8.11	76.67	<u>76.69</u> 0.02

M.H. Rim Talley + Gravilla	6.56			73.56	
T.P. #3	9.27	85.99	3.50	76.62	<u>76.64</u> 0.02
check to starting B.M.	2.18			83.81	<u>83.80</u> 0.01

check to starting B.M.	2.72			83.84	<u>83.80</u> 0.04 error
------------------------	------	--	--	-------	-------------------------------

T.P. #3	9.92	86.56	3.47	76.64	
---------	------	-------	------	-------	--

check to SEBP La Jolla Blvd, GRAVILLA	8.67			71.44	<u>71.29</u> 0.35
---------------------------------------	------	--	--	-------	----------------------

Gravilla

80.11

L

E

R

53

P. 49  
error P. 52

P. 53

This was derived from U.S.C. 16. See <sup>F.B.</sup> 1823-9

77.51  
7.40  
50

25.5  
6.55  
M.H. Rim

14.71  
5.40  
50

80.11

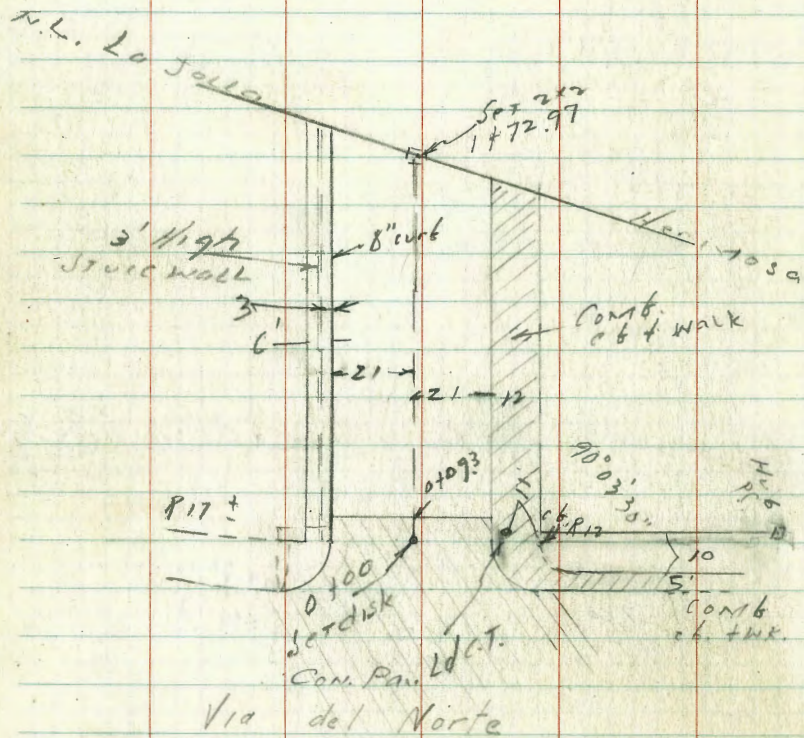


Survey for proposed  
opening of Ave. Central  
Nly to Dowling Drive

Maple  
B 99  
Green  
Rebars  
1-20-48

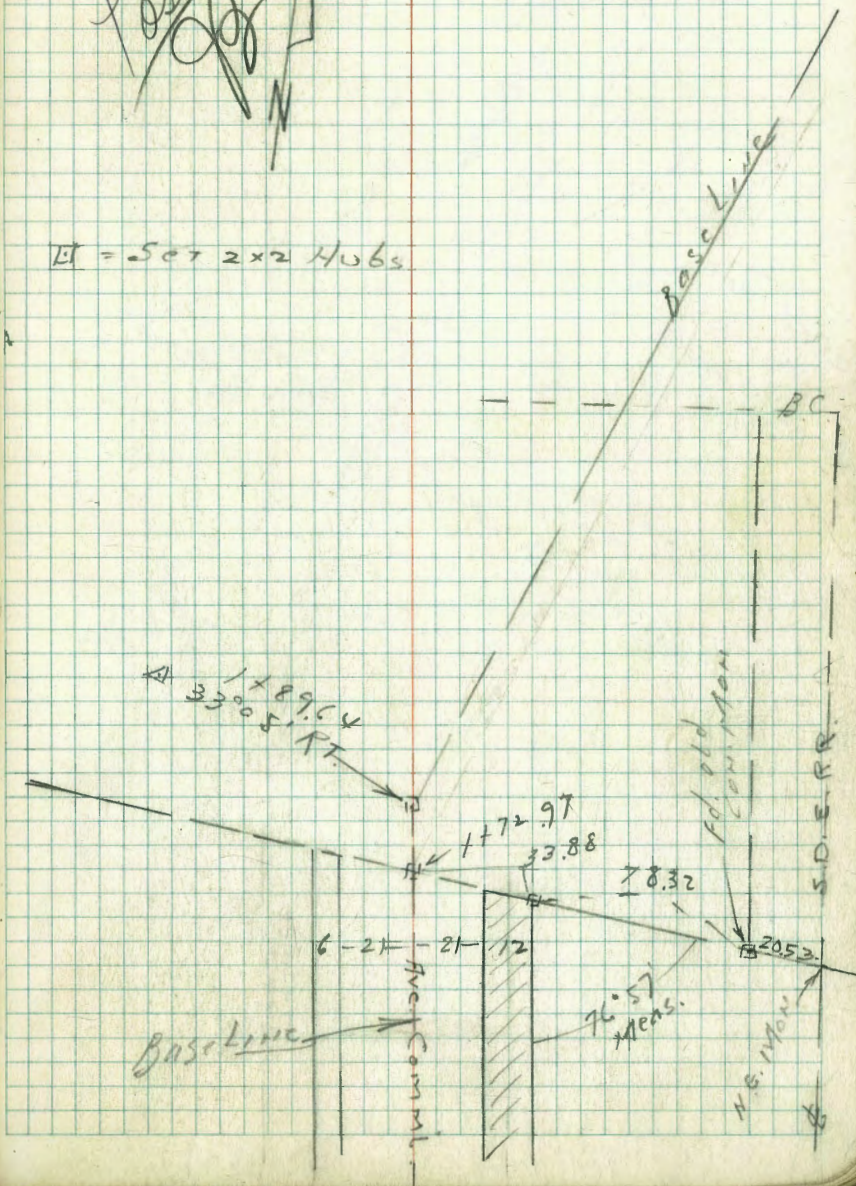
No. 27156

Ref. Ga BK 123-11

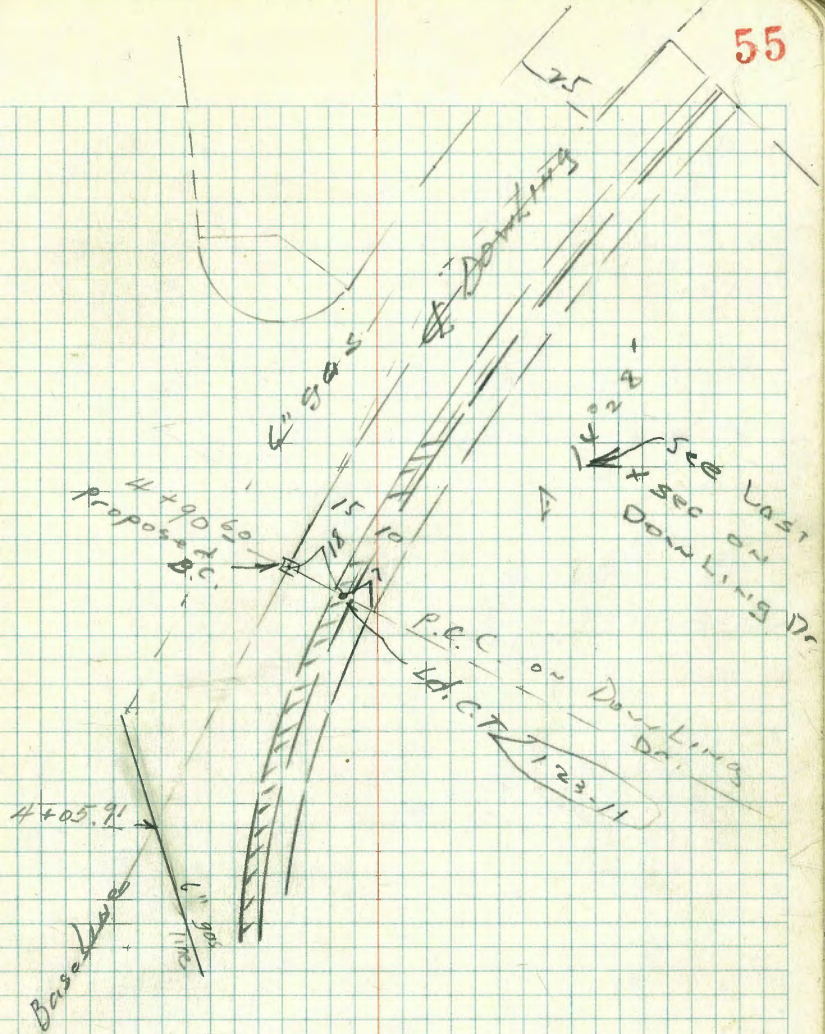


~~Posted~~

ET = Set 2x2 Hubs



Ave - Coram 6 -



X Sections Ave. Commercial ^ to

0 ± 50

0 ± 09.3 N. edge Com. Pav.

0 ± 00 N. by Via del Norte

-15 curb line on Rt gutter line on Rt

-30 d Via Del Norte

B.M. BP 1.81 93.70  
on curb

91.89 ←

L+

Baseline

Rt 56

Dowling

85.0 8.7 27	84.50 8.80 21 06	84.3 9.4 21	85.1 8.6	85.2 8.5 21	85.75 7.95 21 06	85.89 7.81 23 wack			
84.7 9.0 27	84.70 9.00 21 06	84.26 9.44 21	85.08 8.62	85.17 8.53 21	85.58 8.11 21 06	85.14 7.96 33 edge wk.			
		84.75 9.25 21 06	84.30 9.40 21 07	84.97 8.78	85.17 8.53 21 07	85.58 8.12 21 06	85.70 8.00 33 edge wk		
	84.35 9.35 30 06	84.24 9.51 24	84.30 9.40 21	84.86 8.84	85.13 8.57 21	85.32 8.32 33	85.62 8.08 33 06	85.84 7.84 50	86.36 7.30 50 06
	83.90 9.80 35	84.16 9.54 24	84.19 9.51 21	84.75 8.95	85.15 8.55 21	85.47 8.23 33	86.19 7.81 50		
									93.70

BM Dowling & Electric Ave B.P. E curb Dowling  
check this on Dowling x sec

2 + 60

2 + 20

1 + 89.64 Sec. on split of A

1 + 72.97 Sec. on Pueblo Line

1 + 50

1 + 00

93.70

L

R

P

57

B52	B60	B70	B70	B78	B87	B90
8.5	7.7	7.7	7.7	7.5	7.0	7.7
20	30	2	2	23	24	40

B82	B87	B87	B87	B87	B87	B92
9.5	7.7	7.0	7.3	7.0	7.5	7.5
60	30	7	7	27	24	60

B87	B87	B87	B87	B87	B87
10.0	5.7	7.8	7.0	6.8	5.0
60	30	7	25	27	60

B56	B54A	B53	B58	B58	B62A	B630
0.4	8.26	8.4	7.9	7.9	7.48	7.40
277	21.50	21.5	21.5	21.5	21.50	33.88
	6				6	11K

B53	B52A	B50	B57	B54	B61A	B61B	B67
8.4	8.4	8.7	8.0	8.3	7.55	7.52	7.0
27	21	21	21	21	21	33	50
	6				6	Walk	

B51	B50B	B57	B53	B52	B59A	B610
8.1	8.65	9.0	8.4	8.5	7.70	7.00
27	21	21	21	21	21	33
	6				6	Walk

93.70

check to orig. B.M. 1.81 91.89

4 + 90.60 P.C.C.

+50

4 + 00

+50

3 + 00

93.70

Lt.

B.L.

R- 58

See X-sec on Downing Dr.

88.1	90.1	91.2	91.4	92.11	92.16
5.7	5.7	4.5	5.3	1.59	1.54
60	30		17.6	17.6	22.7
				28	28
					note
					work

87.5	89.0	89.8	90.2	91.7	92.10	92.12
5.4	5.7	4.4	3.5	2.0	1.00	1.58
70	30	18		28	28	28.3
					28	28
						note
						work

86.8	88.1	88.8	88.9	90.9	91.9	92.18
4.9	5.0	4.9	4.8	5.8	1.8	1.52
60	30	11		30	22	58.4
						28
						note
						work

86.0	87.2	87.9	87.9	88.8	89.5	91.2
7.7	6.5	5.8	5.8	5.5	4.4	2.5
60	30	8		22	25	40
						note
						work

93.70

Paulys Addition Map #65

Cross section

Alley Bk. 13 - Levels on Page 61  
 Myrtle - Mississippi to Alabama.

4-20-48

V.L.O. 25001

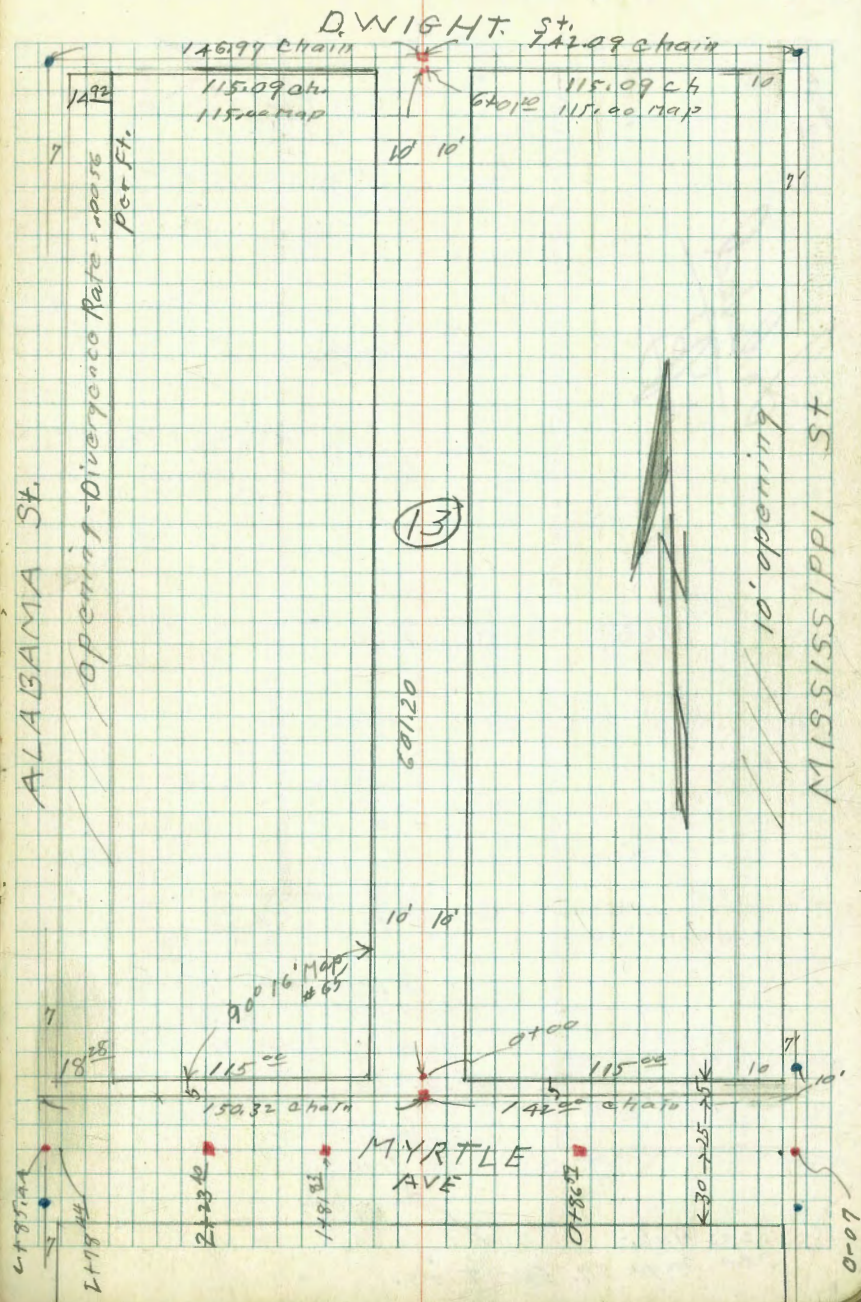
• = Ed. LIT. or L+Disk.

■ = Set 2x2 4x6 + disk

• = " Nail in pavement.

All distances chained except where noted otherwise.

Sammermeyer  
 McCoy X  
 W. Moore  
 Sherman





Levels  
 Alley BIK 13 Paulys Add.

T.P. 7.66 269.19 10.87 261.53

0+28 9<sup>5</sup> Lt. = start slat fence.

0+26.7 11<sup>3</sup> Lt. = End Garage. Conc. Floor.

start conc. block Gar. - south entrance.  
 conc.

0+17 11<sup>0</sup> Rt. = End 8" wide brick wall also =

0+12 11<sup>3</sup> Lt. = start Gar. Conc. floor

0+07 9<sup>2</sup> Lt. Back Edge Pole # 505508H

0+03<sup>2</sup> Cont.

0+03<sup>2</sup> 11<sup>e</sup> Rt. = start 8" wide <sup>conc</sup> brick wall.

0+00 Nly line Myrtle.

0+05 = 2x2 + disk

11.08 261.92

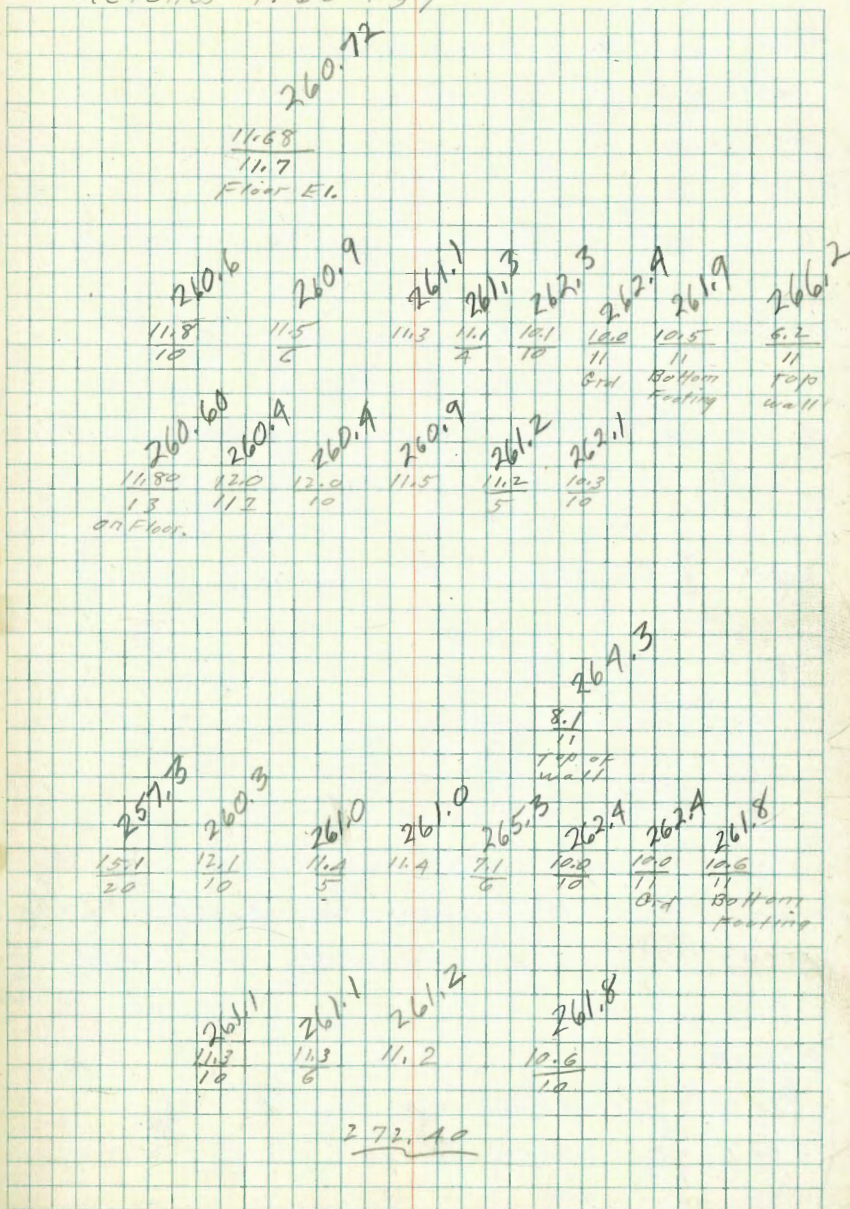
Set. B.M.  
 #1

Myrtle  
 Mississippi 1.42 272.40

— 270.98

N.W.  
 B.P.

sketches P. 60 + 59





T.P. 458 271.29 2.48 266.71 Fence  
 9<sup>5</sup> Lt.: End lath fence & start picket  
 Picket Fence  
 1701 10<sup>0</sup> Rt.: End stucco wall also start.

1+00 9<sup>2</sup> Lt.: back of pole #. J.P.C. 3519

0+79 8<sup>2</sup> Lt.: Ctr. dead man  
 on top of ground.

0+59 9<sup>5</sup> Lt.: End Rocks in gravel. laying

0+50 9<sup>2</sup> Rt.: Start stucco wall (=

0+49<sup>3</sup> 11<sup>2</sup> Rt.: End conc. block wall, 5" wide  
 start lath fence.

setting on top of ground. also =

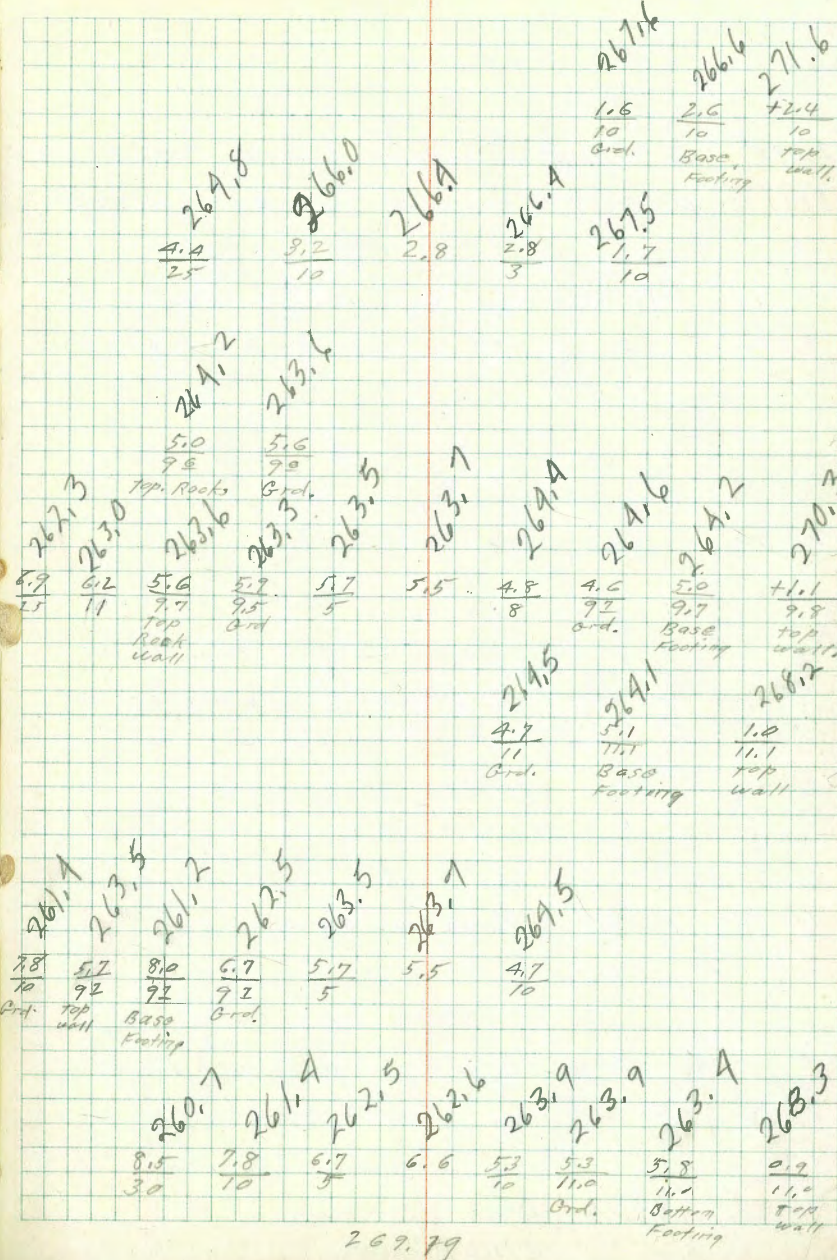
Also start row of rocks in gravel. 1' wide

0+49 9<sup>2</sup> Lt.: 4" wide E+W, conc. wall

conc. block wall

0+37 11<sup>0</sup> Rt.: End garage & start 8' wide

269.79



2+01<sup>3</sup> = 12<sup>±</sup>Rt. = Start Gar. doors. (Rough Conc. Floor)  
 2+01 = 10<sup>±</sup>Rt. = S.W. Cor. Dwelling + Gar. (2 story Bldg.)

9<sup>±</sup>Rt. = Face 4" diam Radio Mast.  
 10<sup>±</sup>Rt. = End 8" Conc. wall + lath Fence  
 2+00 9<sup>±</sup>Lt. = Back of pole # J.P.C. 3539

2+80

with lath Fence.  
 1+51 10<sup>±</sup>Rt. = start 9" wide Conc. wall. Topped  
 9<sup>±</sup>Lt. = Fence line

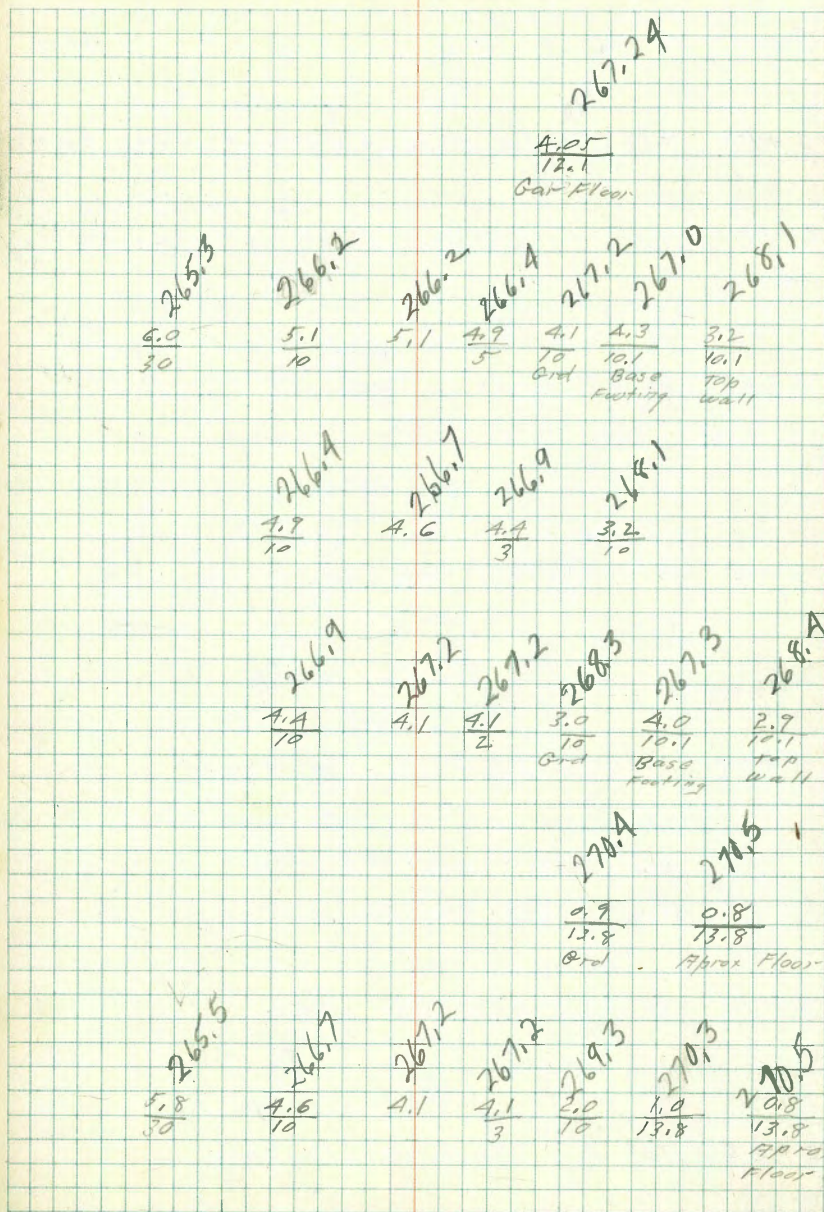
1+48 13<sup>±</sup>Rt. = N.W. Cor. Gar.

south entrance

13<sup>±</sup>Rt. = S.W. Cor. Gar. Conc. Floor  
 1+30 10<sup>±</sup>Rt. = End picket Fence

1+22 8<sup>±</sup>Lt. = Ctr. deadman

271.29

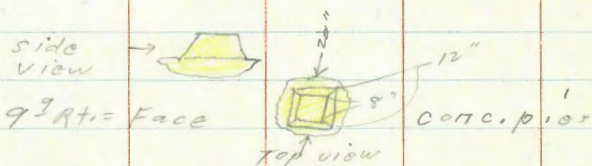


271.29

2+51 Foundation. Also = start picket fence.  
10' Rt. = N.W. Cor. Dwelling or shop cone.

2+50 9' Lt. = End picket + start wire fence

2+31 10' Rt. = S.W. Cor. dwelling (or work shop)  
Conc. Foundation



2+27 9' Rt. = Face

2+21 9' Lt. = start picket fence.

2+20 10' Lt. = End double Car.

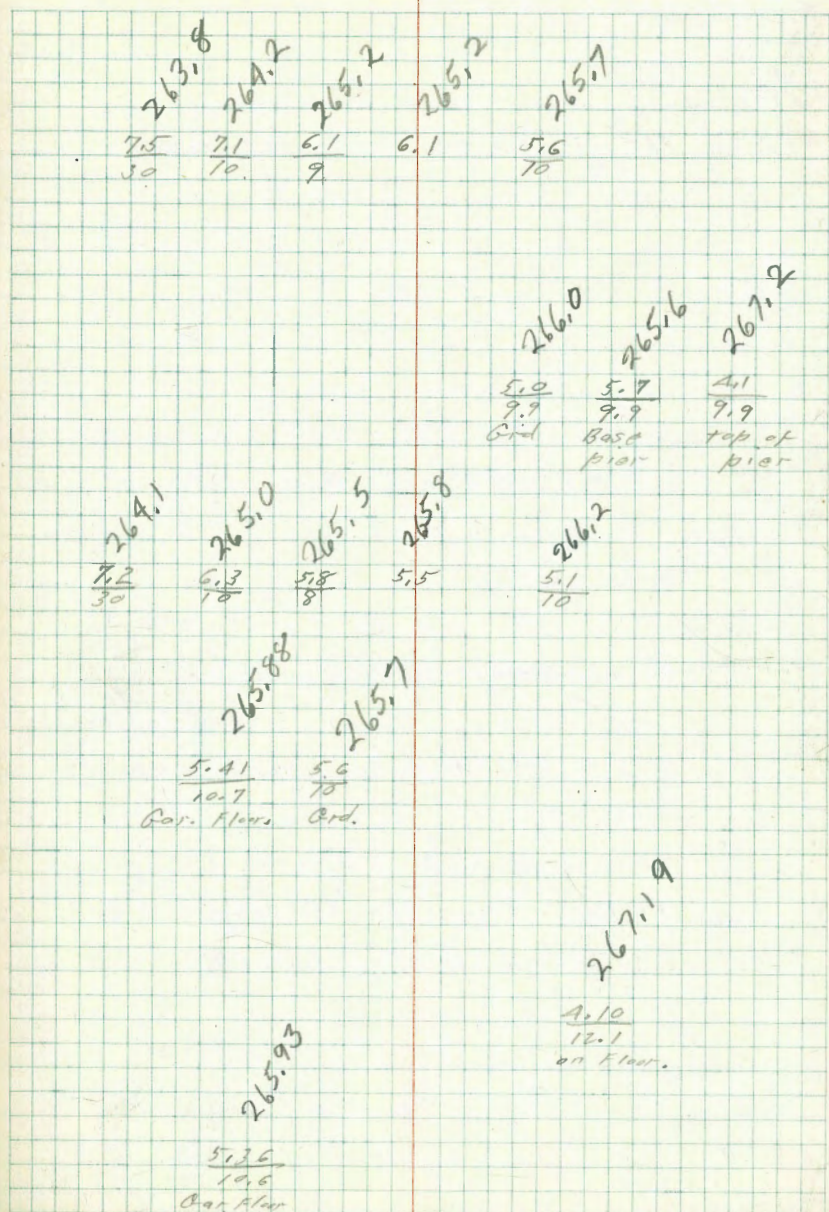
Also = start picket fence.

2+16<sup>E</sup> 10' Rt. = N.W. Cor. House foundation

2+16 12' Rt. = End Car doors.

2+06 10' Lt. = start double Car.

271.29



271.29



A+07 10<sup>2</sup> Lt. = E Sing. Gar. dirt floor.

A+03 = End 5" wide Conc. wall

+ E 5" E+W. wall.

A+01<sup>↓</sup> 10<sup>5</sup> Rt. = start 5" wide Conc. wall.

A+01 Cont.

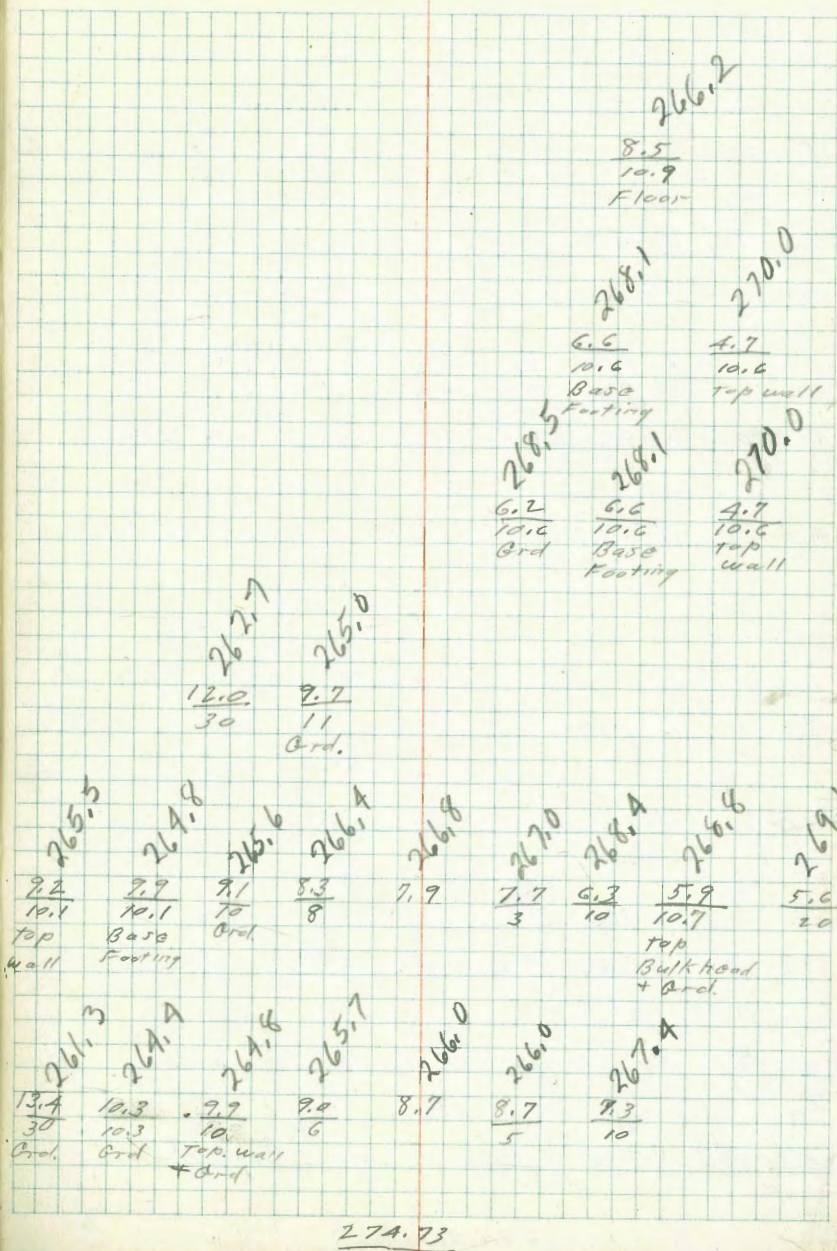
bulk head also = End wire fence.

10<sup>3</sup> Rt. = End 12" High 2" wide plank  
wide Conc. wall

A+01 } 9<sup>2</sup> Lt. = Pole # 8.P.C. 3579 10<sup>1</sup> Lt. = End A"

3+80

T.P. 8.65 274.73 5121 266.08  
271.29



T.P. 283 274.83 2.73 272.00

5+00

4+90 10<sup>±</sup> Lt. = start wire fence

4+85 8<sup>±</sup> Lt. = Ctr. dead man.

4+71 9<sup>±</sup> Lt. = End wire fence.

9<sup>±</sup> Lt. = End Batt. Fence. + start wire fence

10<sup>±</sup> Rt. = start board fence = N.W. cor. conc. slab.

4+50 10<sup>±</sup> Rt. End 4" wide Conc. wall + also

4+27 9<sup>±</sup> Lt. = Ctr. 6" diam apricot tree

wall under gate in fence.

4+20 10<sup>±</sup> Lt. = Ctr. 3" long 6" wide Conc.

4+19 10<sup>±</sup> Rt. = start wire fence on top of wall

+ also = S.W. Cor Conc. slab.

4+14<sup>±</sup> 10<sup>±</sup> Rt. = start 4" wide conc. wall.

4+12 10' Lt. = start Batt. fence.

4+08<sup>±</sup> 15<sup>±</sup> Rt. = E Sing. Cor. Conc. floor.

274.73

268.9  
5.8  
30

270.8  
3.7  
10

271.2  
3.5

271.7  
3.9  
10

266.7  
8.0  
30

268.0  
4.7  
10

268.4  
6.3  
9.5

269.0  
5.7

269.0  
5.7  
3

270.8  
3.9  
10

269.9  
4.8  
10.5  
Base top of wall

270.8  
3.9  
10.5  
top of slab.

271.0  
2.7  
12

266.9  
7.8  
10.1  
Ord.

267.6  
7.1  
10.1  
top of wall

266.8  
7.9  
10.1  
Base of wall

267.4  
7.3  
10  
Ord.

265.9  
8.8  
25

266.3  
8.4  
11

267.1  
7.6  
10

267.2  
7.5  
3

267.5  
7.2

269.2  
5.5  
10

268.9  
6.3  
10.5  
Base Footing

270.2  
4.5  
10.5  
top of wall

270.3  
4.4  
14  
07  
slab

266.4  
8.3  
10

266.8  
7.9  
3

267.3  
7.4

267.7  
7.0  
3

269.1  
5.6  
10

269.9  
4.8  
15

270.06  
4.67  
15.1  
Cor Floor

274.73

5+70 13<sup>2</sup> Lt. = start picket fence.  
 5+68 13<sup>2</sup> Lt. = End double Gar. Conc. Floor

5+60<sup>2</sup> 10<sup>2</sup> Rt. = <sup>start wall</sup> face 10" wide <sup>wall.</sup> rock + grout

5+60 10<sup>2</sup> Rt. = <sup>Gar. conc. floor.</sup> End Conc. apron to Sill

5+53 13<sup>2</sup> Lt. = start double Gar. Conc. Floor

5+51<sup>2</sup> 10<sup>2</sup> Rt. = <sup>Sill. Gar. Conc. floor.</sup> start Conc. Apron to

5+51 10<sup>2</sup> Lt. = End Bath. fence.

5+50

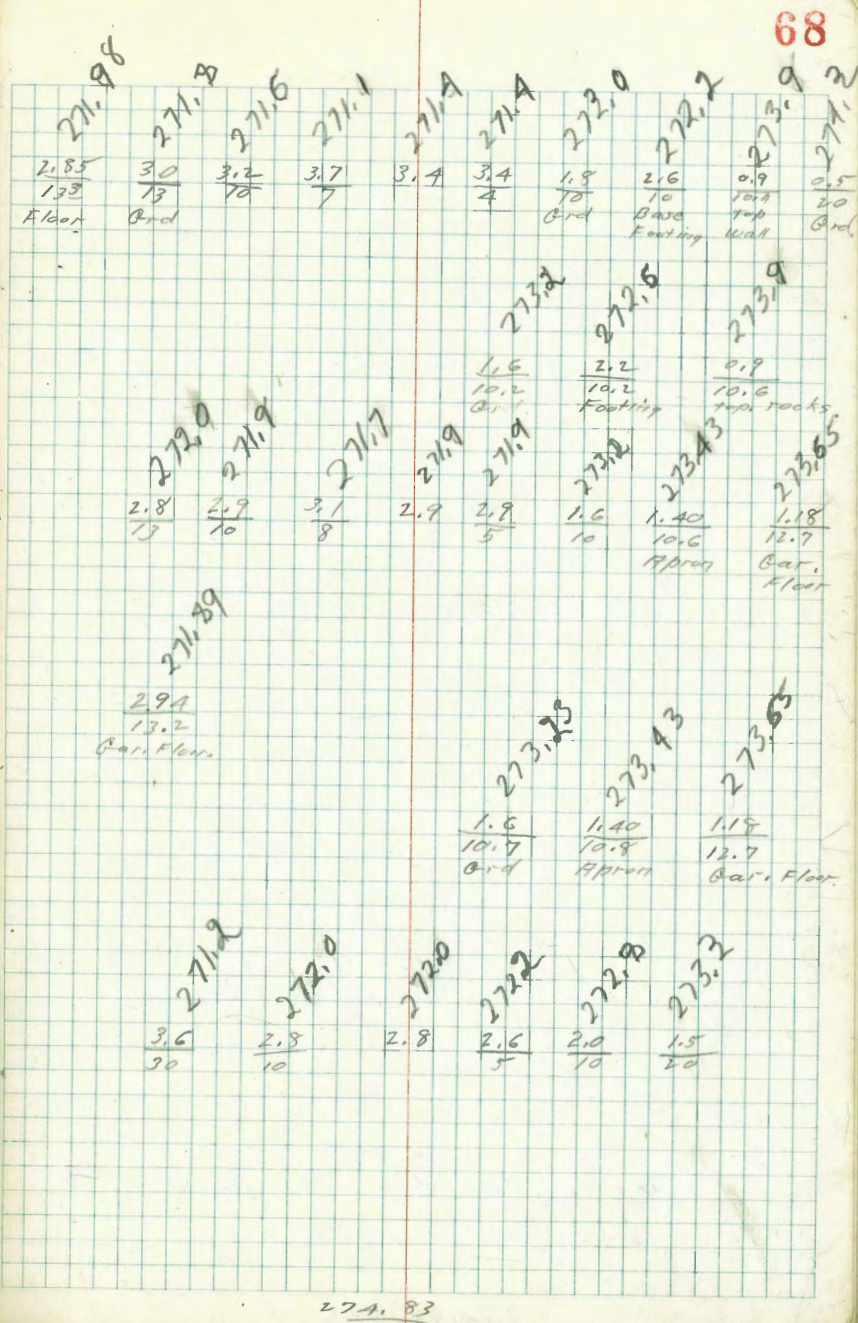
12<sup>5</sup> Rt. = start lath fence.

10' Rt. = End board fence

9<sup>2</sup> Lt. = start Bath. fence.

5+01 9<sup>2</sup> Lt. = Back of pole # S.P.C. 3589

274.83



274.83

on curb over hold.  
Plug gone.

W.E.B.P.  
Dwight +  
Alabama.

7.82 255.90 255.96

T.P. 1.62 263.72 12.73 262.10

6+16 Gutter as graded (unpaved street) Dwight.

6+01.2

9<sup>2</sup> Rt. = End 7" wide Conc. wall.

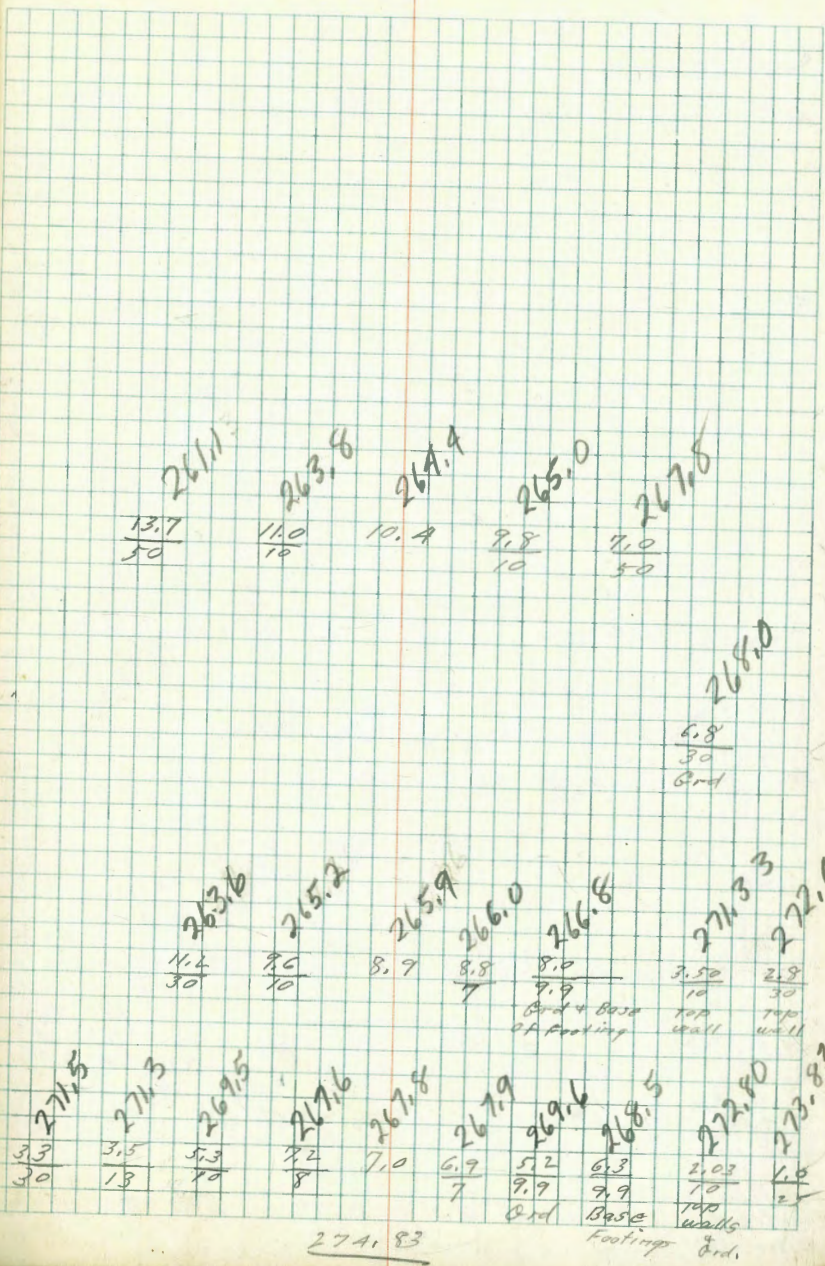
6+01<sup>20</sup> = S. Line Dwight.

also = start 7" wide Conc. wall.

9.9 Rt. = End Rock + gravel wall

3+90 13.6 Lt. = End picket fence.

274.83





Myrtle.

Sketch P. 59 + P. 71

also E. N. + S. wall.  
 0+38 27<sup>2</sup> Lt. = face 6" wide Conc wall

0+28 27<sup>5</sup> Lt. = start 6" wide Conc. wall,

0+12

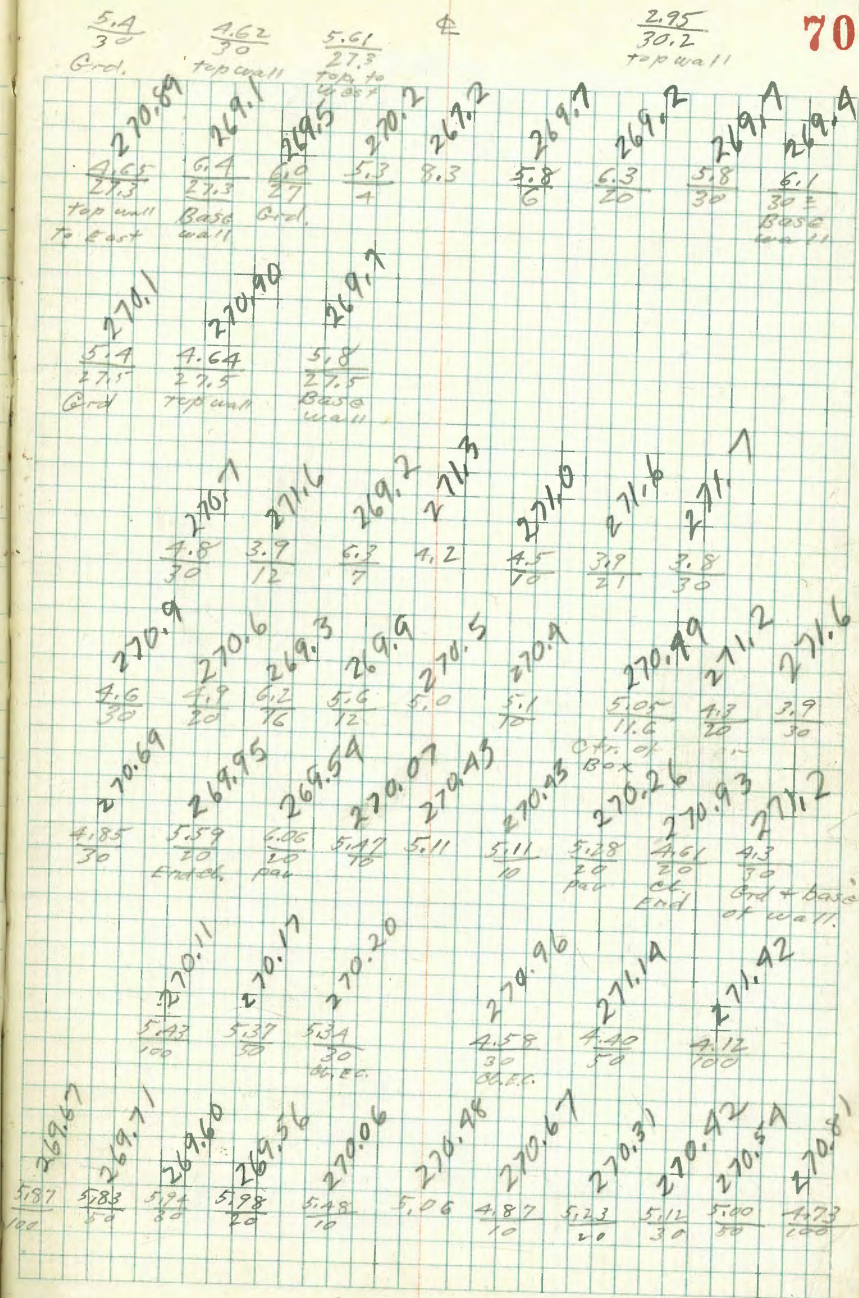
0+02 11<sup>E</sup> Rt. = Ctr 3<sup>8</sup> x 3<sup>8</sup> gas valve box

w. L. Miss.  
 0+00 30<sup>2</sup> Rt. = start 6" <sup>30</sup> Conc. block wall.  
 End Existing pavement.

0-10 = W. Curb line Mississippi

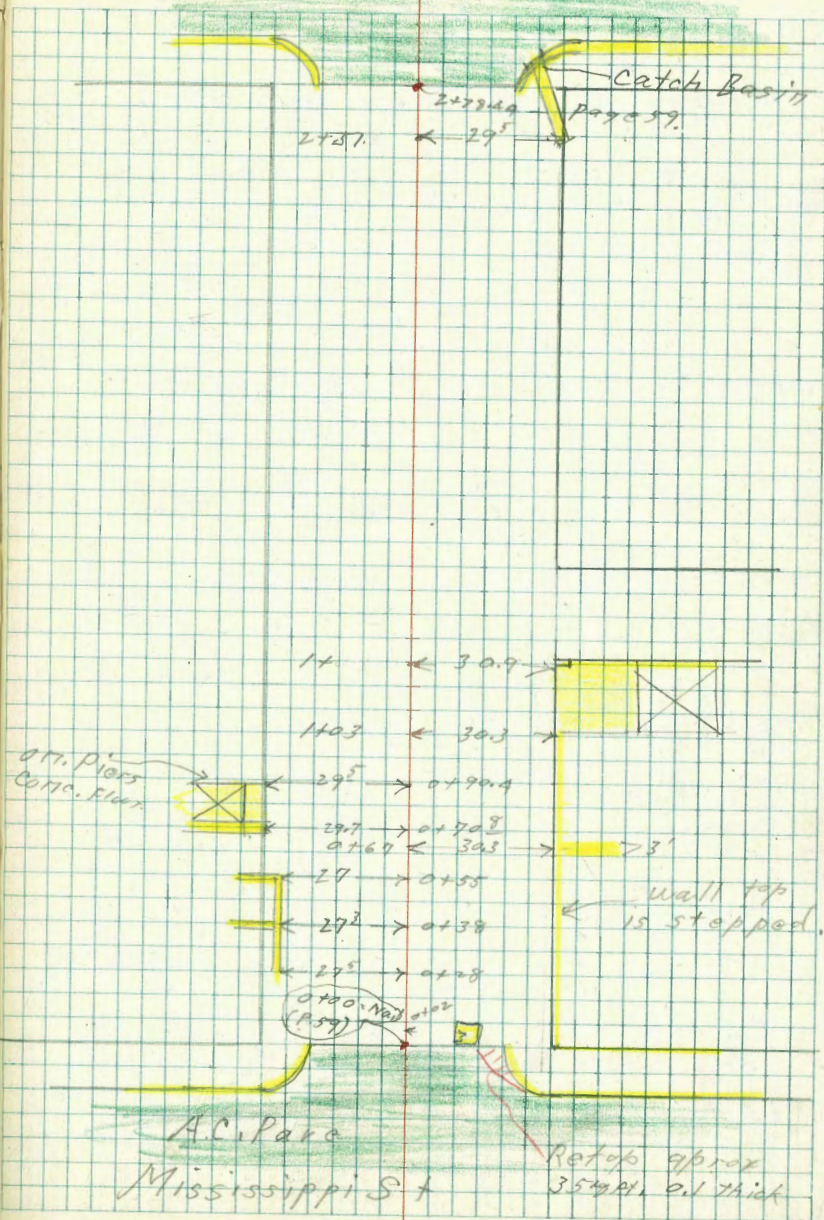
0-10' = W. Outer line Mississippi

N.W.B.P.  
 Myrtle + Mississippi 4.56 275.54 — 270.98



275.54

ALABAMA ST



0+90<sup>4</sup> 29<sup>5</sup> Lt. = End Conc. Apron + Gar.

0+75

double garage.

0+71<sup>2</sup> 29<sup>3</sup> Lt. = start Conc. Apron to

0+70<sup>2</sup> 29<sup>2</sup> Lt. =  $\phi$  2<sup>3</sup> wide Conc. walk

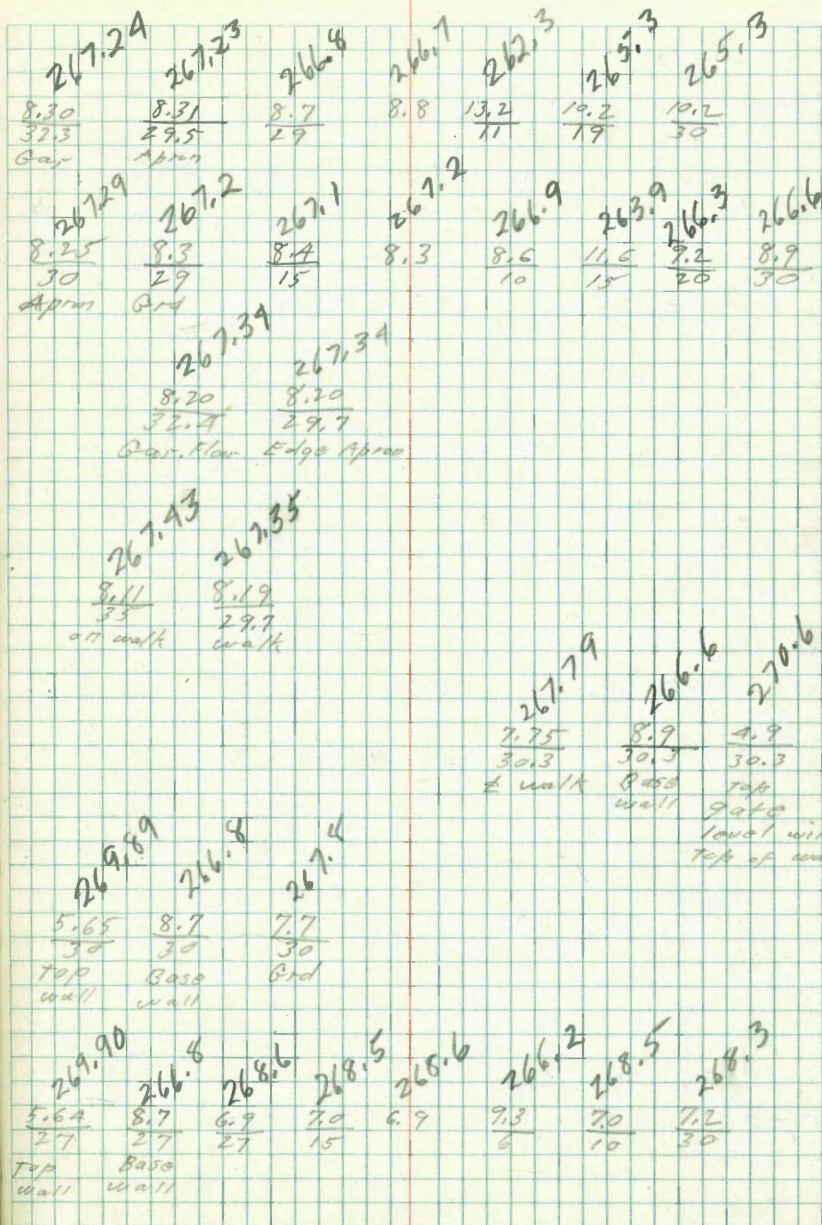
0+67 30<sup>3</sup> Rt. =  $\phi$  3' walk.

0+55 Cont.

also:  $\phi$  N.+S. 6" Conc. wall.

0+55 27<sup>2</sup> Lt. = End 6" Conc. wall.

275.54



275.54

T.P. 0.62 252.20 12.44 251.58

1+45

1+35

T.P. 1.41 264.02 12.93 262.61

1+23<sup>1/2</sup> 33<sup>1/2</sup> Rt. = ± 8" wide N+S, Concr. block wall.

1+23- 30<sup>2</sup> Rt. = End Apron.

1+05

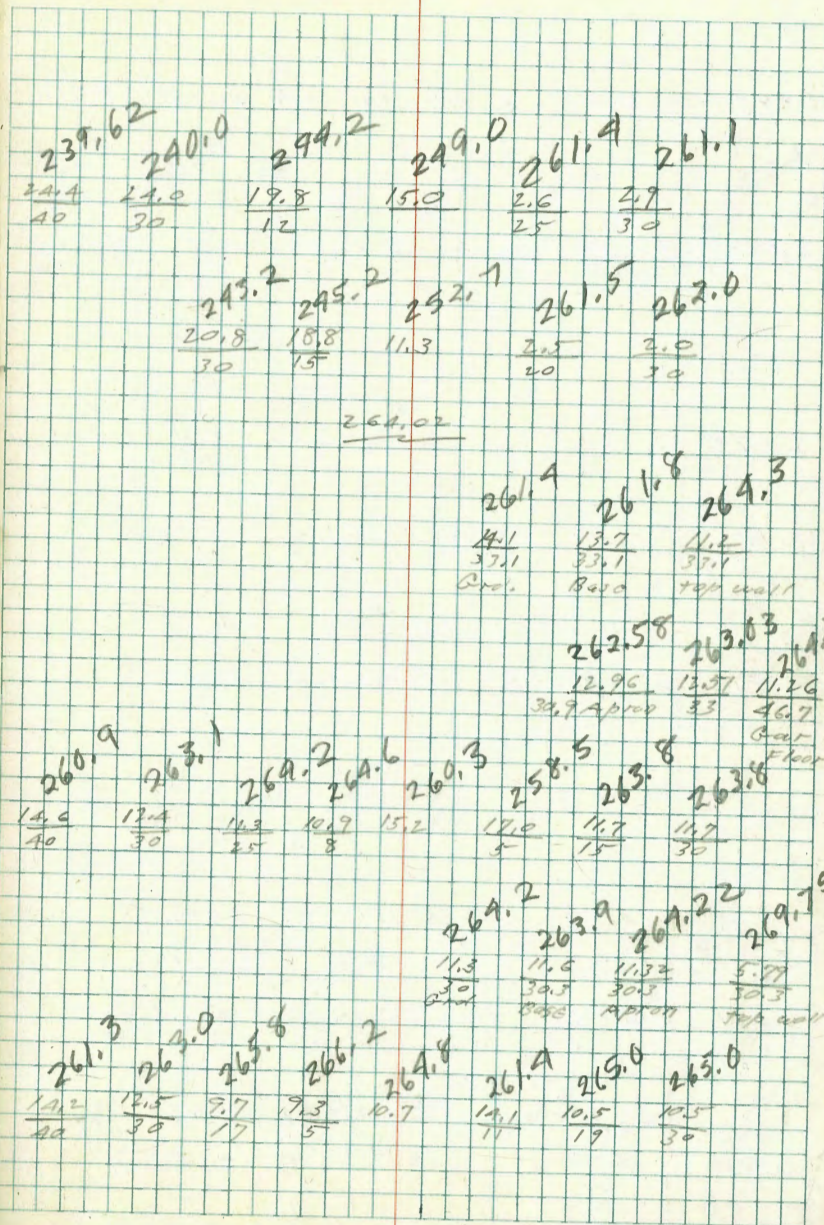
1+00

concr. drive to Gar.

1+03 30<sup>2</sup> Rt. = End 6" Concr wall. + start

0+95

275.54



275.57

2+85<sup>4</sup> 23<sup>4</sup> Rt. =  $\frac{1}{2}$  grate at curb (P. 71).

2+78<sup>49</sup> E.L. Alabama. Edge Exist Pavc.

2+72

T.P. 12.10 253.81 0.22 241.71

= start culvert

2+51 29<sup>5</sup> Rt. =  $\frac{1}{2}$  30" Conc. Culvert.

2+40

T.P. 0.87 241.93 11.14 241.06

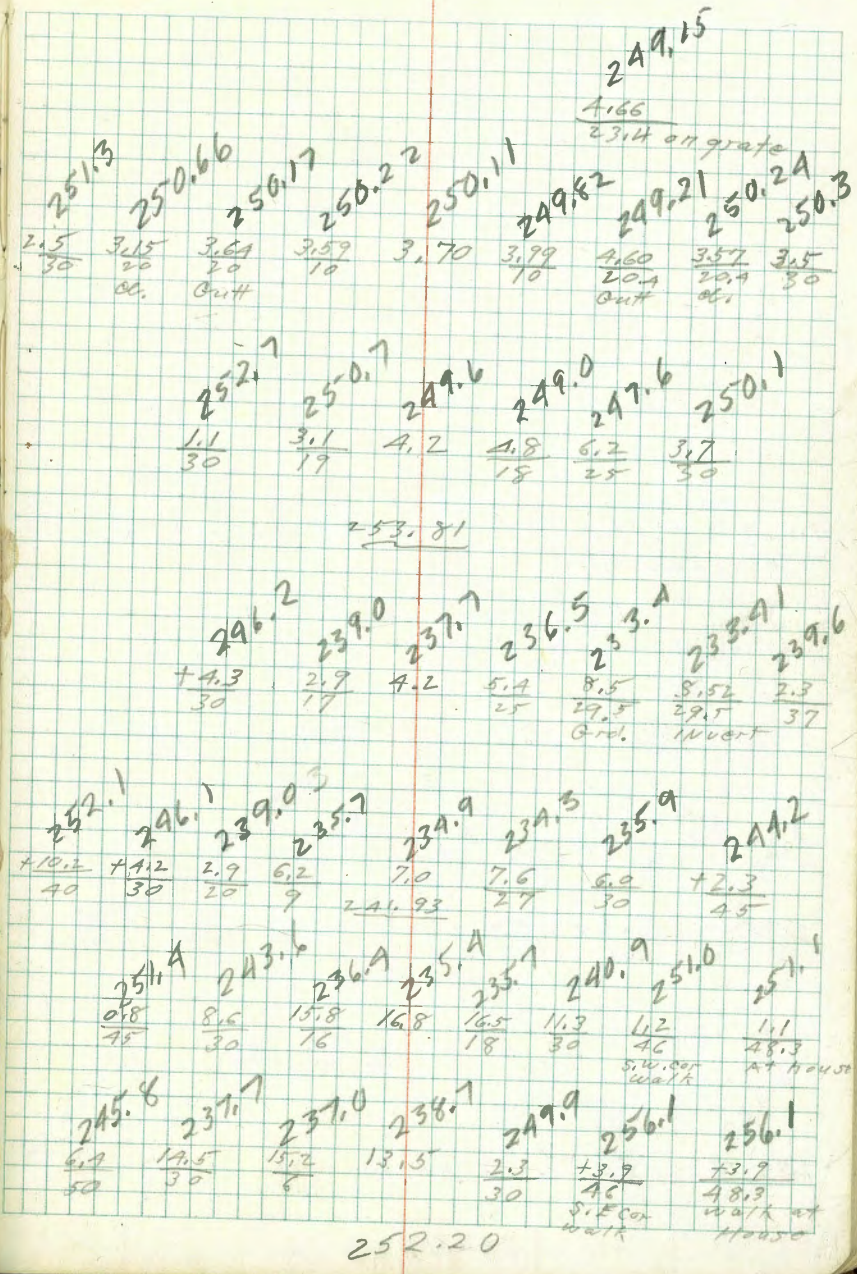
walk

2+11 46' Rt. = End. 2<sup>3</sup> wide Conc. F. + W.

conc. walk. along house

1+81 46' Rt. = start 2<sup>3</sup> wide F + W

252.20



N.W.B.R. Myrtle  
Alabama

2.35

251.46

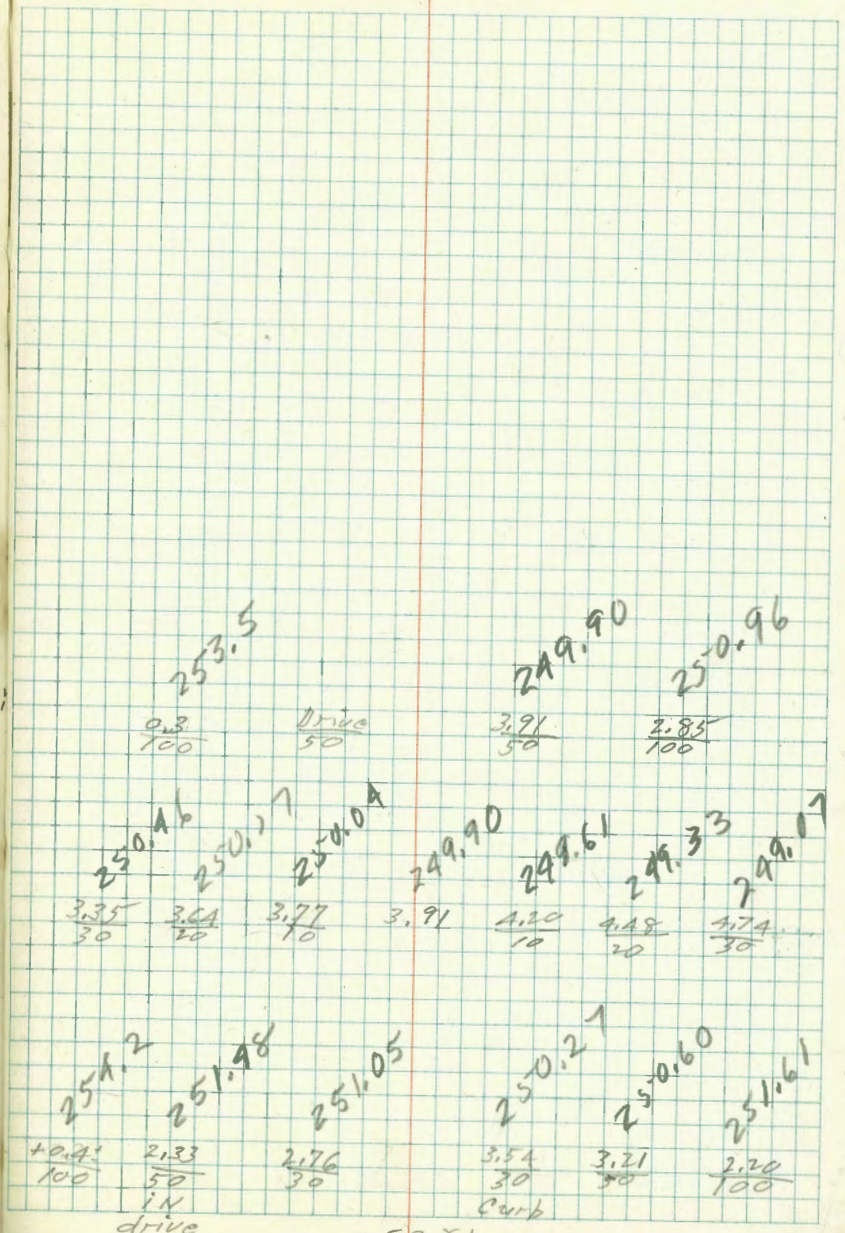
251.50

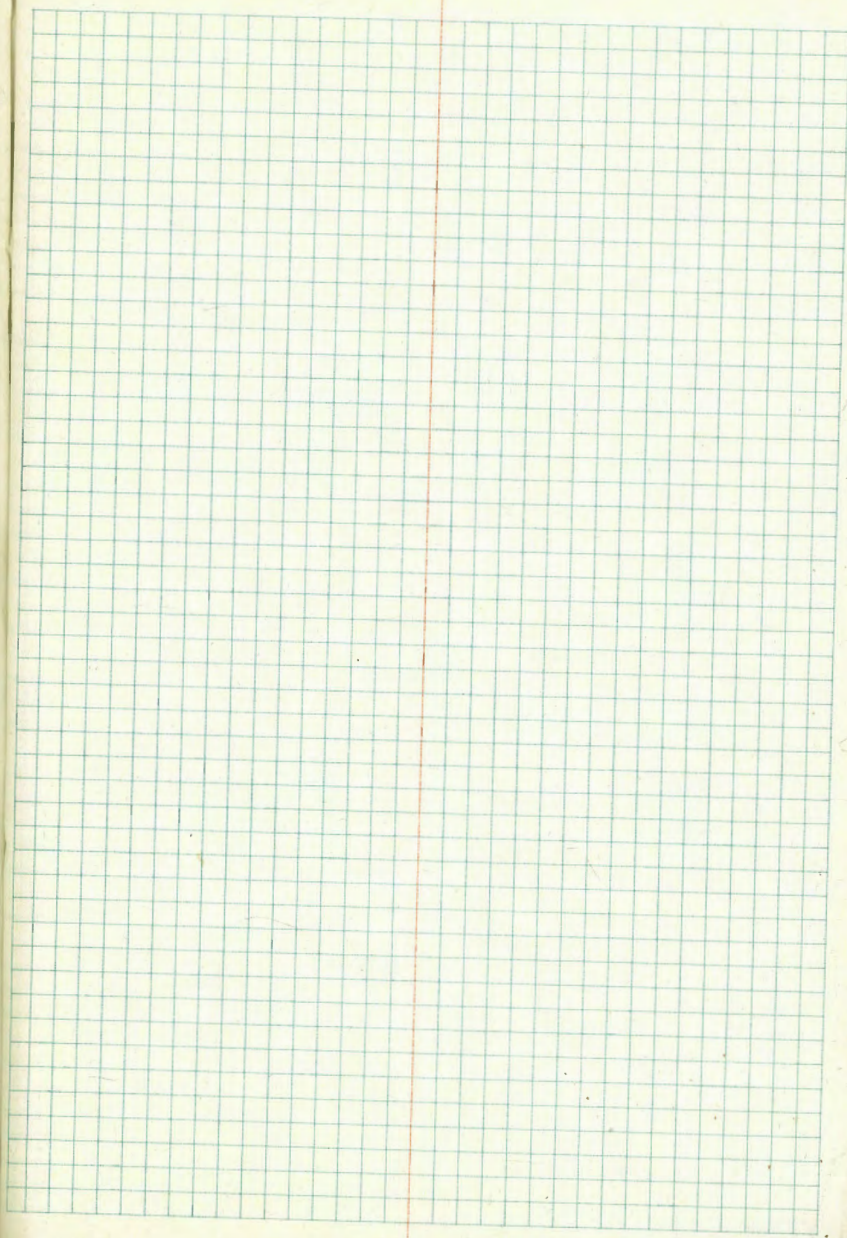
2485<sup>E</sup> Post.

2485<sup>E</sup> E. gutter.

2485<sup>44</sup> E. Ch. Alaba.

253.81

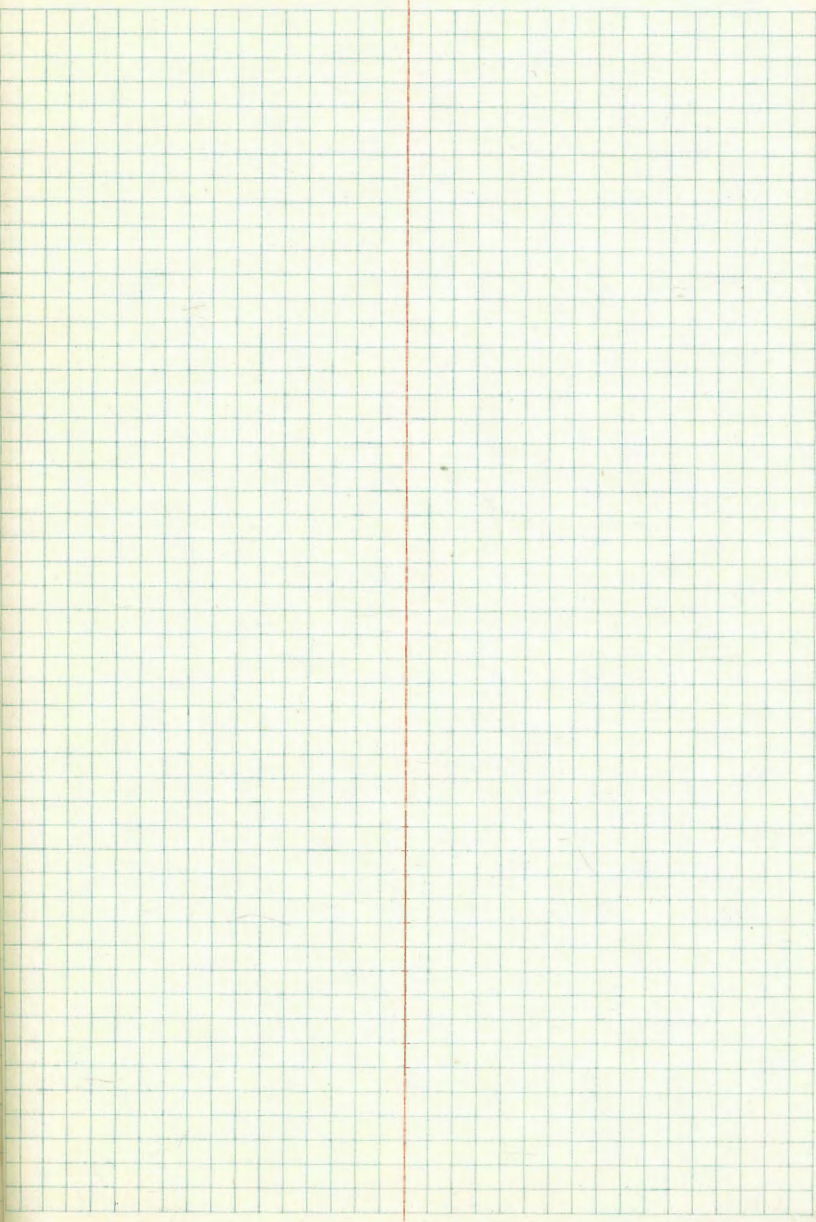
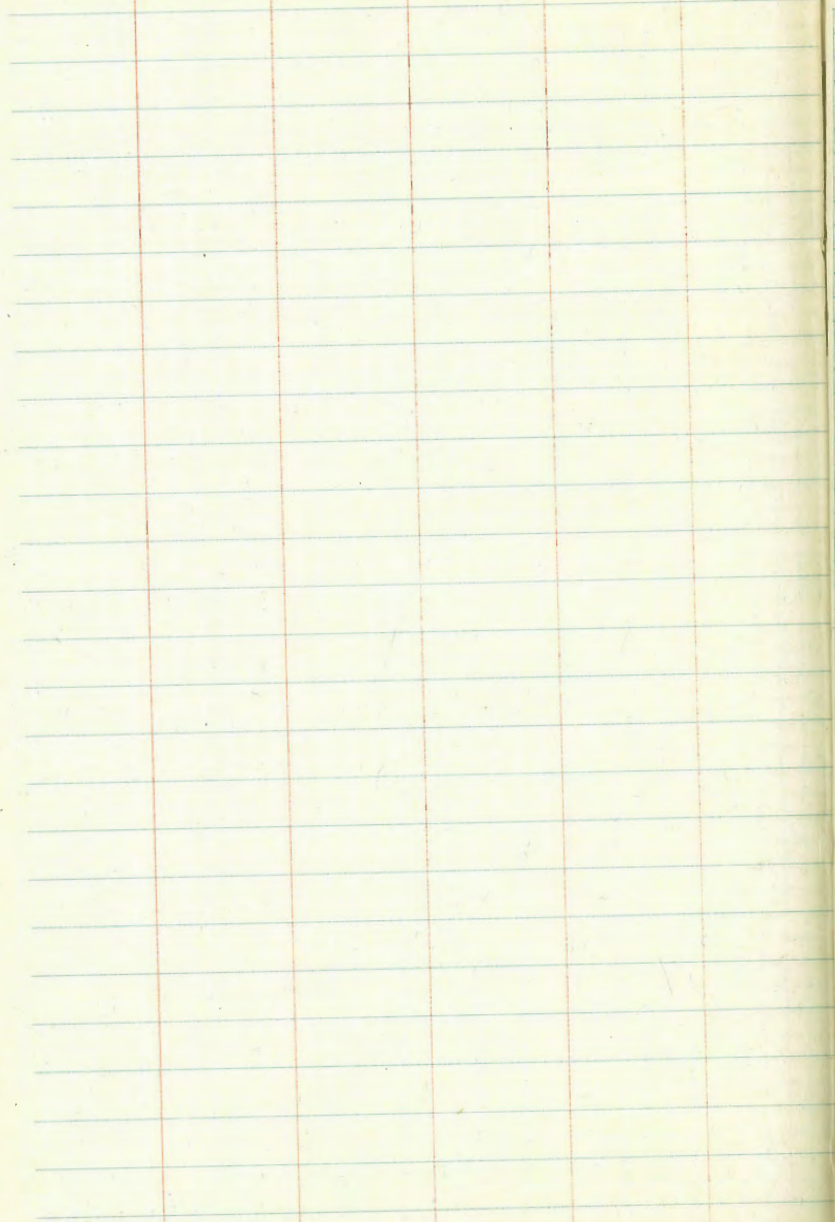


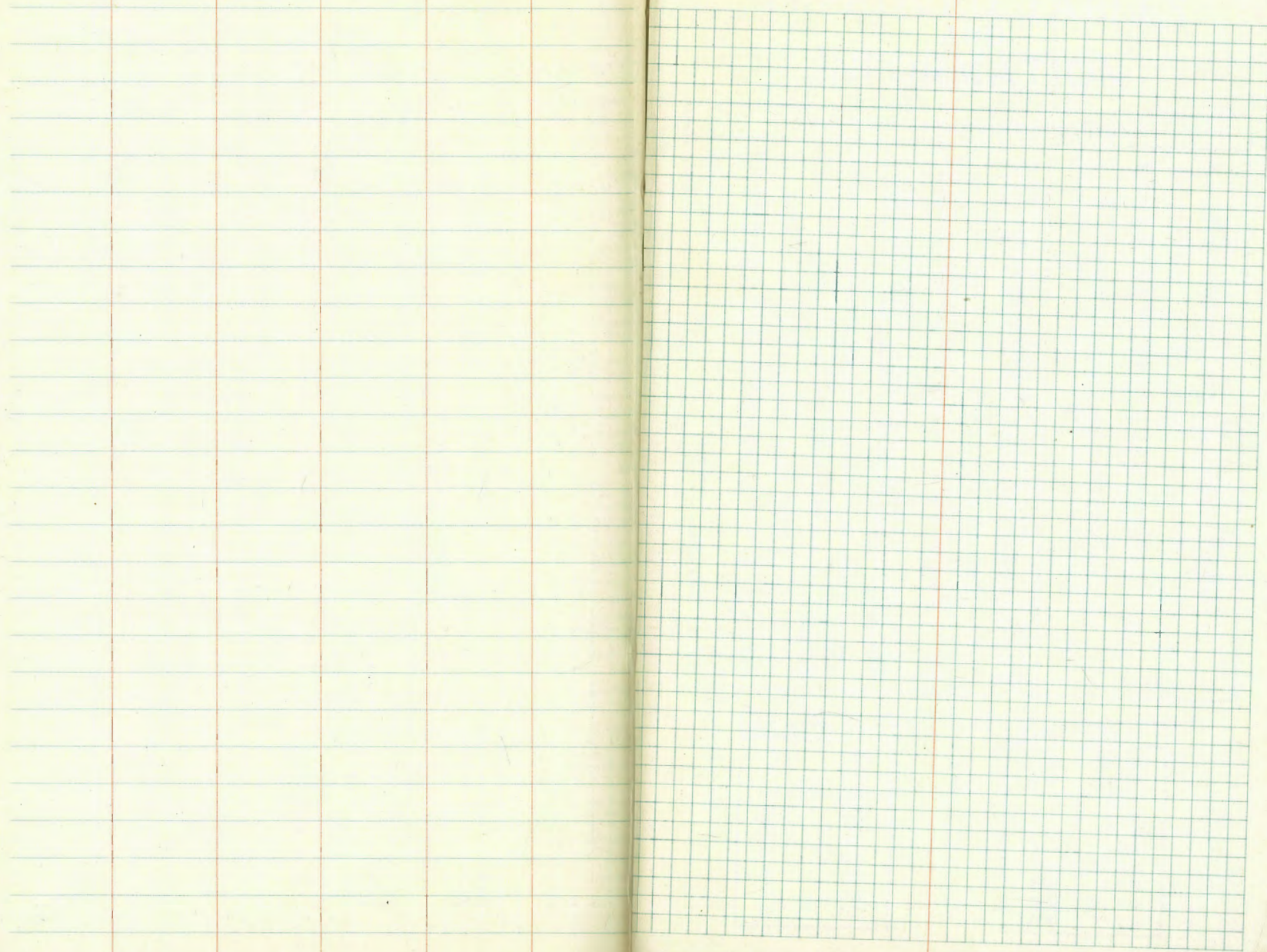


A ledger page with a grid of blue horizontal lines and four vertical red lines, creating five columns. The page is blank.

A graph page with a grid of blue horizontal and vertical lines, forming a square grid. The page is blank.







# IMPROVED TABLES AND INFORMATION

## HORIZONTAL STADIA CORRECTIONS

2°—00' — 0.1	21°—00' — 12.8	33°—00' — 29.7
3°—00' — 0.3	21°—30' — 13.4	33°—15' — 30.1
4°—00' — 0.5	22°—00' — 14.0	33°—30' — 30.5
5°—00' — 0.8	22°—30' — 14.7	33°—45' — 30.9
6°—00' — 1.1	23°—00' — 15.3	34°—00' — 31.3
7°—00' — 1.5	23°—30' — 15.9	34°—15' — 31.7
8°—00' — 1.9	24°—00' — 16.5	34°—30' — 32.1
9°—00' — 2.5	24°—30' — 17.2	34°—45' — 32.5
10°—00' — 3.0	25°—00' — 17.9	35°—00' — 32.9
10°—30' — 3.3	25°—30' — 18.6	35°—15' — 33.3
11°—00' — 3.6	26°—00' — 19.2	35°—30' — 33.7
11°—30' — 4.0	26°—30' — 19.9	35°—45' — 34.1
12°—00' — 4.3	27°—00' — 20.6	36°—00' — 34.6
12°—30' — 4.7	27°—30' — 21.3	36°—15' — 35.0
13°—00' — 5.1	28°—00' — 22.0	36°—30' — 35.4
13°—30' — 5.5	28°—30' — 22.8	36°—45' — 35.8
14°—00' — 5.9	29°—00' — 23.5	37°—00' — 36.2
14°—30' — 6.3	29°—30' — 24.3	37°—15' — 36.6
15°—00' — 6.7	30°—00' — 25.0	37°—30' — 37.1
15°—30' — 7.2	30°—15' — 25.4	37°—45' — 37.5
16°—00' — 7.6	30°—30' — 25.8	38°—00' — 37.9
16°—30' — 8.1	30°—45' — 26.2	38°—15' — 38.3
17°—00' — 8.5	31°—00' — 26.5	38°—30' — 38.7
17°—30' — 9.0	31°—15' — 26.9	38°—45' — 39.1
18°—00' — 9.5	31°—30' — 27.3	39°—00' — 39.6
18°—30' — 10.1	31°—45' — 27.7	39°—15' — 40.0
19°—00' — 10.6	32°—00' — 28.1	39°—30' — 40.5
19°—30' — 11.2	32°—15' — 28.5	
20°—00' — 11.7	32°—30' — 28.9	
20°—30' — 12.3	32°—45' — 29.3	

### Chains to Feet

1 .....	66
2 .....	132
3 .....	198
4 .....	264
5 .....	330
6 .....	396
7 .....	462
8 .....	528
9 .....	594
10 .....	660

### Feet to Chains

100 ....	1.515
200 ....	3.030
300 ....	4.545
400 ....	6.060
500 ....	7.575
600 ....	9.090
700 ....	10.606
800 ....	12.121
900 ....	13.636
1,000 ....	15.151

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

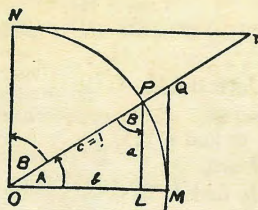
TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

75.54  
 14.93  
 262.67  
 1.41  
 264.02  
 12.04  
 251.58  
 62  
 251.71  
 12.10  
 264.02  
 1.41  
 262.67  
 87



75.5  
 69.3  
 73.7  
 1.2  
 72.40  
 10.6  
 61.8 Feet.  
 64.3 top.  
 61.4 - 0.4

TABLE II  
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

156.98

538

8.00

381

235

146