

1777



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1777

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to the inch, Center Line Red.
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BOOK. Left Hand Page as in this
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ENGINEERING and DRAFTING SUPPLIES

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CHICAGO

INDEXED

*completely
except page 26*

Xsec Alley Bk H Terabta Hrs	1
X-Sec. Lowell St. - Rosecrans to Harbor Dr.	6-21
u Macaulay, William to Plum	20
X-Sect. Alleys - 102-104-100 - Univ. Hts.	27-42
X-Sect. 41 st - Redwood to Thorn	43-52
u u Brunner and Josephina	} 53-59
u From Alley Bk "C" Silver	
u Terrace to Linda Vista Road	
Proposed Culvert Raymond & Torrence	60-65

see alley Blk H Terakta Hrs.

0 + 51 8.5 ft Sw Jan 21 Jan.

0 + 50 7.8 ft end last fence

0 + 41 E 2' Cor. walk

0 + 40 7.8 ft Beg. last fence

0 + 30 6.4 LT. Power Co. Guy Pole

0 + 15

New improvements noted in order.

Shots checked thus ✓ are O.K.

0 + 00 N.L. Monroe edge par.

0 - 12 N.C. Monroe

T.P. 2.84 384.30 1.94 381.46

S.E.P. 1.70 388.38 386.68
Monroe +
Sheraton

LT = West

6

R_T

2

380.48	381.6	381.6	381.3	381.3	381.53
380.07	381.0	381.6	380.8	380.4	380.9
380.01	380.8	381.6	380.8	380.4	381.2
379.43	380.2	381.6	380.8	380.4	381.2
379.25	379.80	381.6	380.8	380.4	381.2
379.05	379.53	381.6	380.8	380.4	381.2
379.45	379.78	381.6	380.8	380.4	381.2
378.54	379.26	381.6	380.8	380.4	381.2
379.26	379.26	381.6	380.8	380.4	381.2

1+75 C.8 Lt angle in picket fence
and 9' Rt end wire fence

1+72.5^{7.3 Lt} NE corner of Bd shed + Beg Picket
5.6 x 7.5

1+65 7.2 Lt SE Cor Bd shed + end Lark fence

1+50 C.7 Lt Beg Lark fence

1+37^{7.7 Rt} end Picket + Beg wire

1+15 8.8 Rt E 2.5 Cor, walk

T.P. 402 384.47 3.85 380.5

1+00 8 Rt end chick + Beg picket fence

0+24 8.8 Rt end Picket + Beg Bd. chick fence

0+71 8.7 Rt ~~NE Cor Bd shed~~ ~~6x6~~
Beg. Picket fence

0+19 2.2 Lt P.P. P.F. 4505

0+57 E Sugar dice fl ~~21.9 Lt~~

0+53 8 Rt. ± 12' Conc. apron to Sing. Gr. Conc. floor

384.30

out changed

Lt 389.7
20
389.6
75
389.4
5
389.3
25
389.0
50

389.9
389.9
389.9
389.4
389.5

380.105
380.105

380.1
380.1
380.1
380.1
380.13

381.1
381.1
381.1
380.9
380.9

384.30

edge apron

floor Grv.

Wood Movel

4380.39

470
18.8

2 + 17 8.4 ft end of wedge 2.5 Conc walk

2 + 54.7 ^{2.5 wide} Beg. Con. walk on Pr.

2 + 53.5 end Concrete apron on Pr.

2 + 42.5 ^{NE Cor. Bldg. apr.} N. entrance

2 + 27.5 Beg. Con. apron + 3 car garage

2 + 26.5 8.5 ft SE Cor Bldg. apr. North entrance

2 + 26 7.7 ft end picket fence

2 + 25 19 ft PP P.O. 4520

2 + 00 6.9 ft picket fence

1 + 77 - 9.1' Rt. - 4.5 Conc Walk

384.47

4.8
379.7
75

L
7
379.5
75

4.0
379.5
75

W
K
379.1
75

A
379.0
75

5.0
379.5
75

2.92
379.5
8.4

4.7
379.8
75

W
K
379.4
75

A
379.2
75

5.0
379.4
75

4.95
379.52
75

4.87
13.9
379.58

4.83
16.0
379.64

4.8
379.7
8.2
first floor

5.0
379.4
75

5.0
379.5
75

5.0
379.4
75

4.89
13.9
379.58
apron

4.87
16.0
379.60
90-ft.

4.6
379.9
75

4.8
379.7
75

5.0
379.4
75

4.4
379.4
75

4.0
379.5
75

4.0
378.5
75

4.0
378.3
75

384.47

4.4
379.4
75

4.0
379.5
75

4.0
378.5
75

4.0
378.3
75

Walker
Hendricks
Becker
Johnson
7-1-47
W.O. 22002

CROSS SECTION - LOWELL ST. from Rosecrans to Harbor Drive

Red notes put in 10-8-48
OHJ

INDEXED

2+17 57' RT - Tel Pole 34988T

2+06 Lt std

2+99 = 5" Polm 41' Lt
Tel Pole

2+91.7 4509 22' H 13' 4

2+74.5 5" Polm 41' Lt

2+51 19' RT Elec Pole #2911

2+29 Polm 41' Lt

2+06 18.5' H 4509 23' H

2+04.5 Polm 41' Lt

1+81 " "

1+59 " "

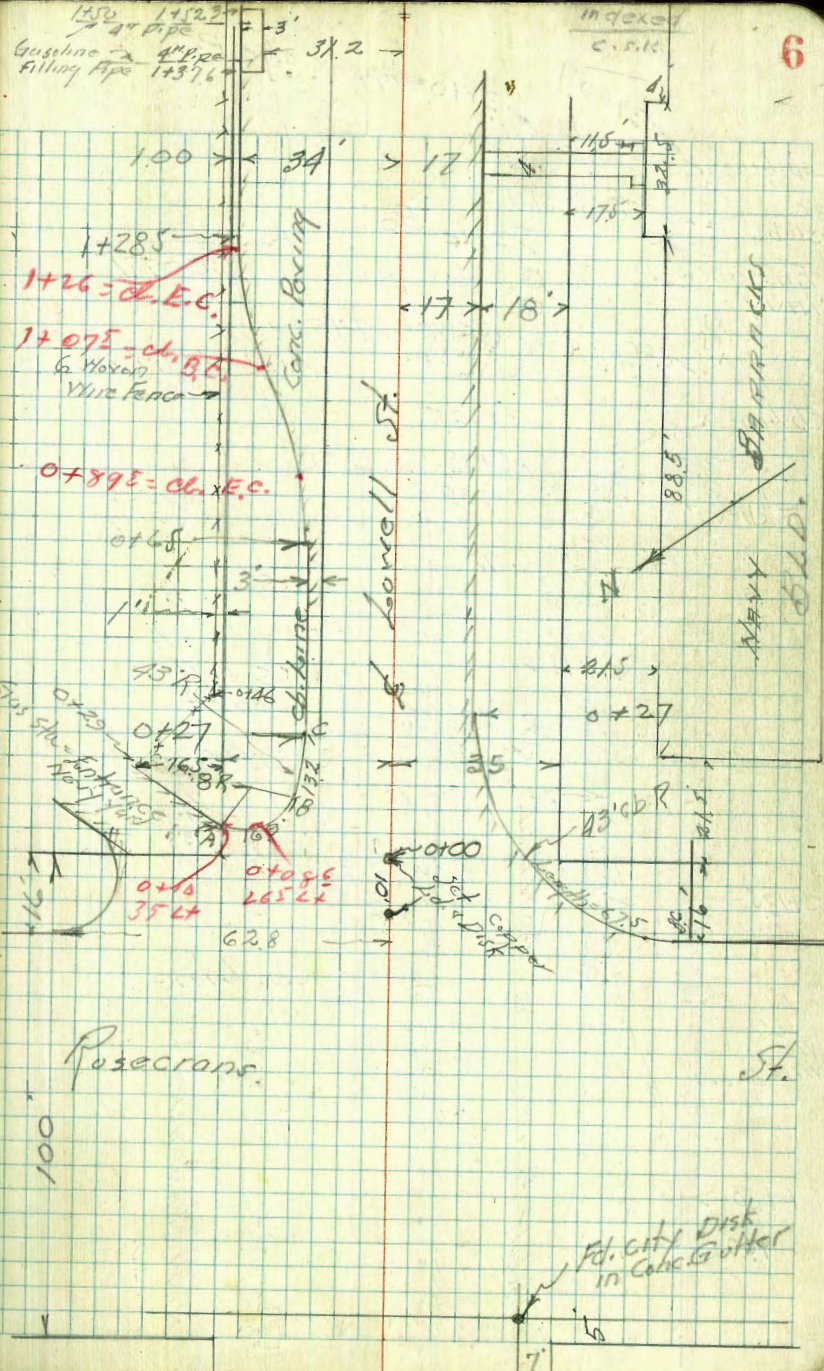
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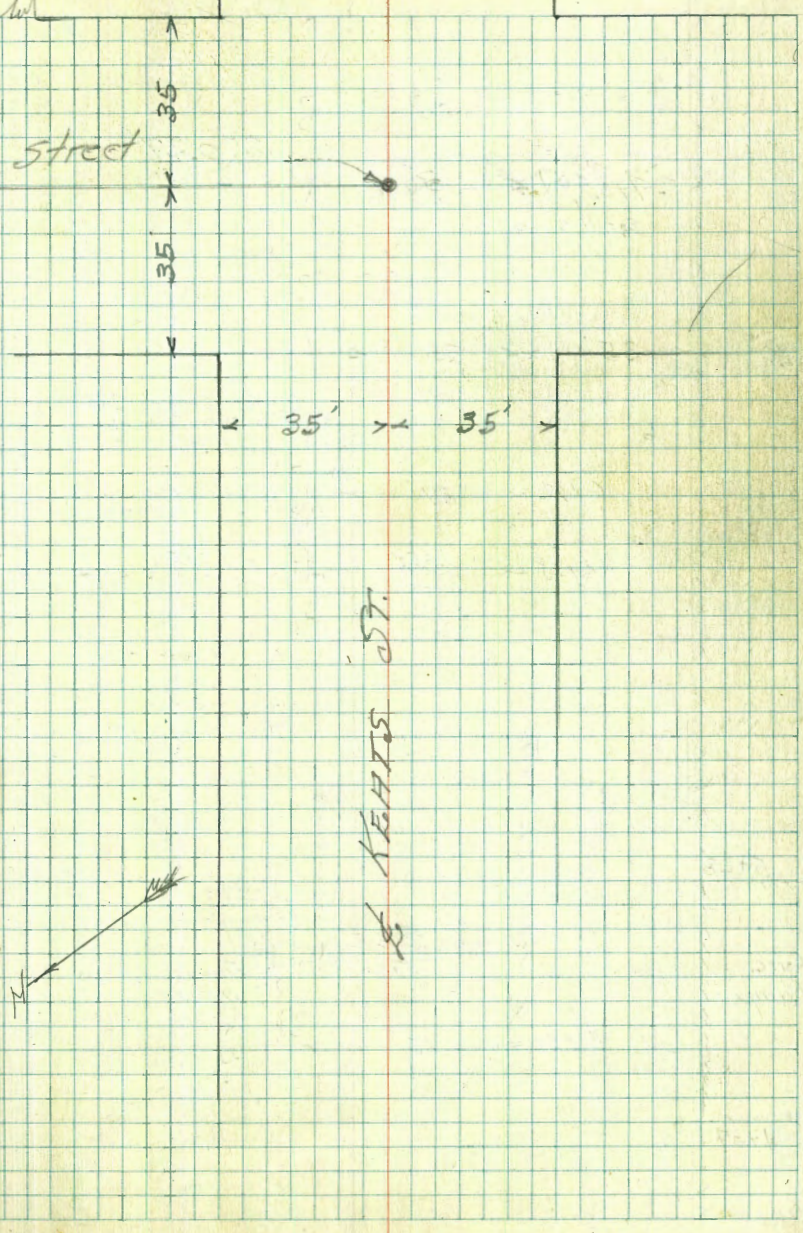
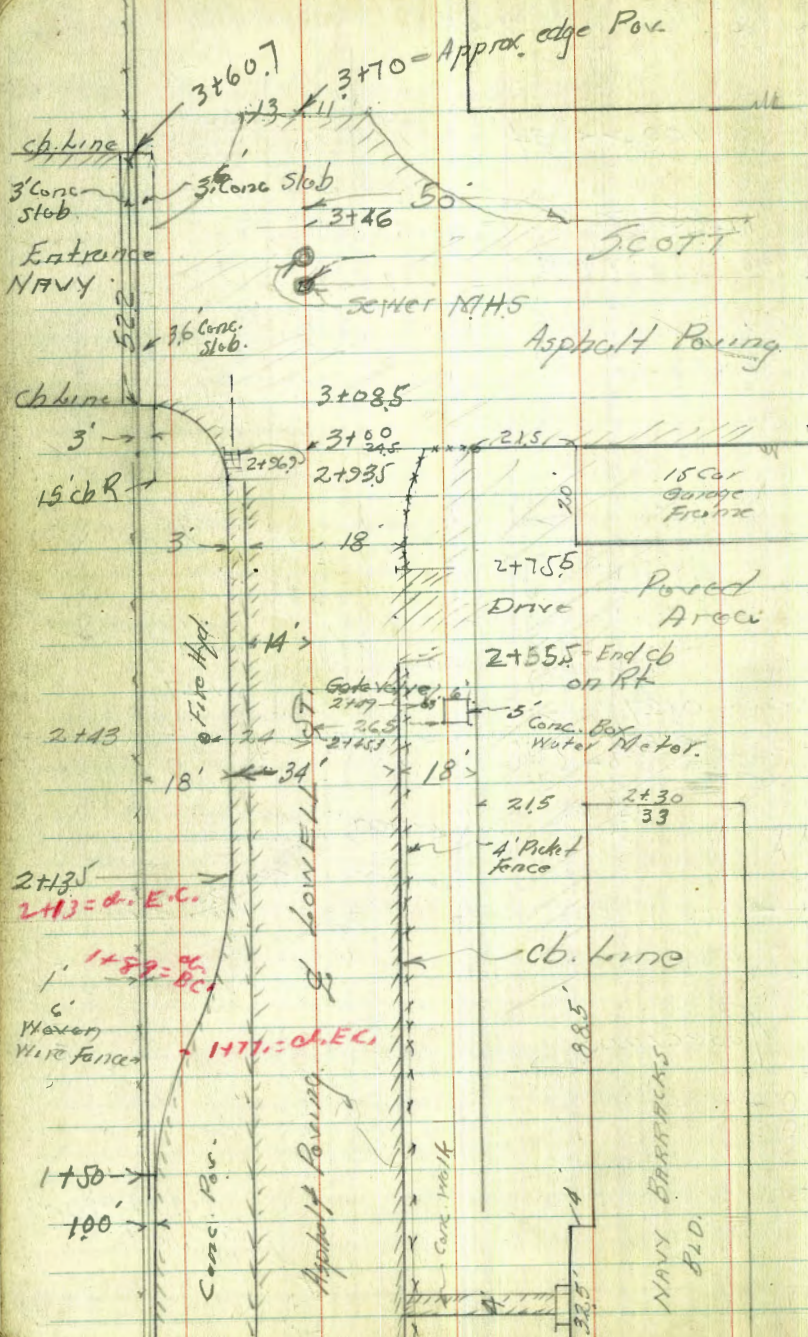
1+13 " "

0+88 " "

0+67 " "

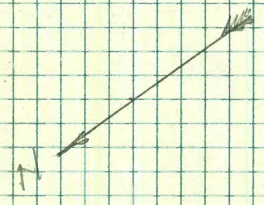
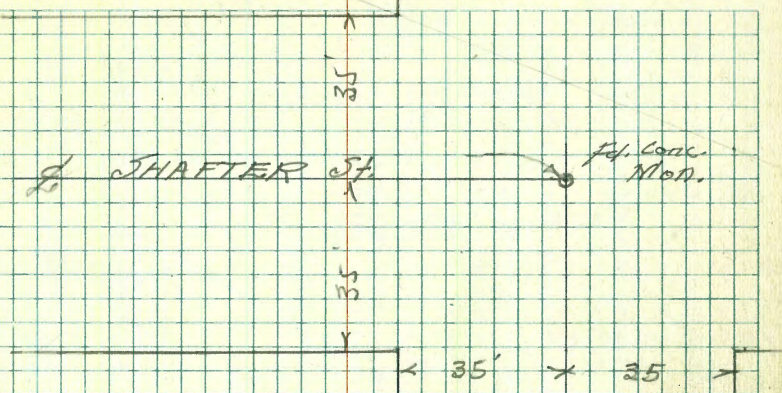
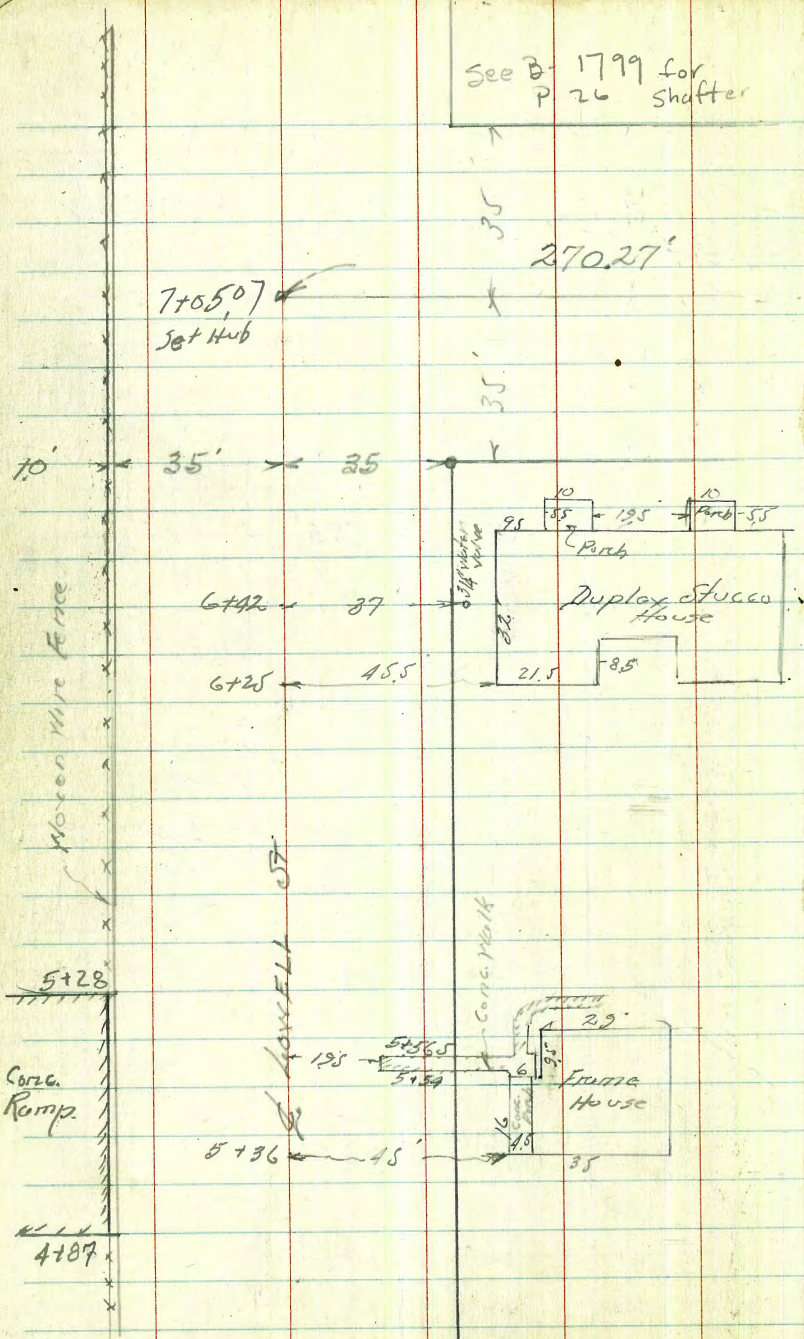
0+35 " "





Sections

See B-1799 for
P 26 Shafter



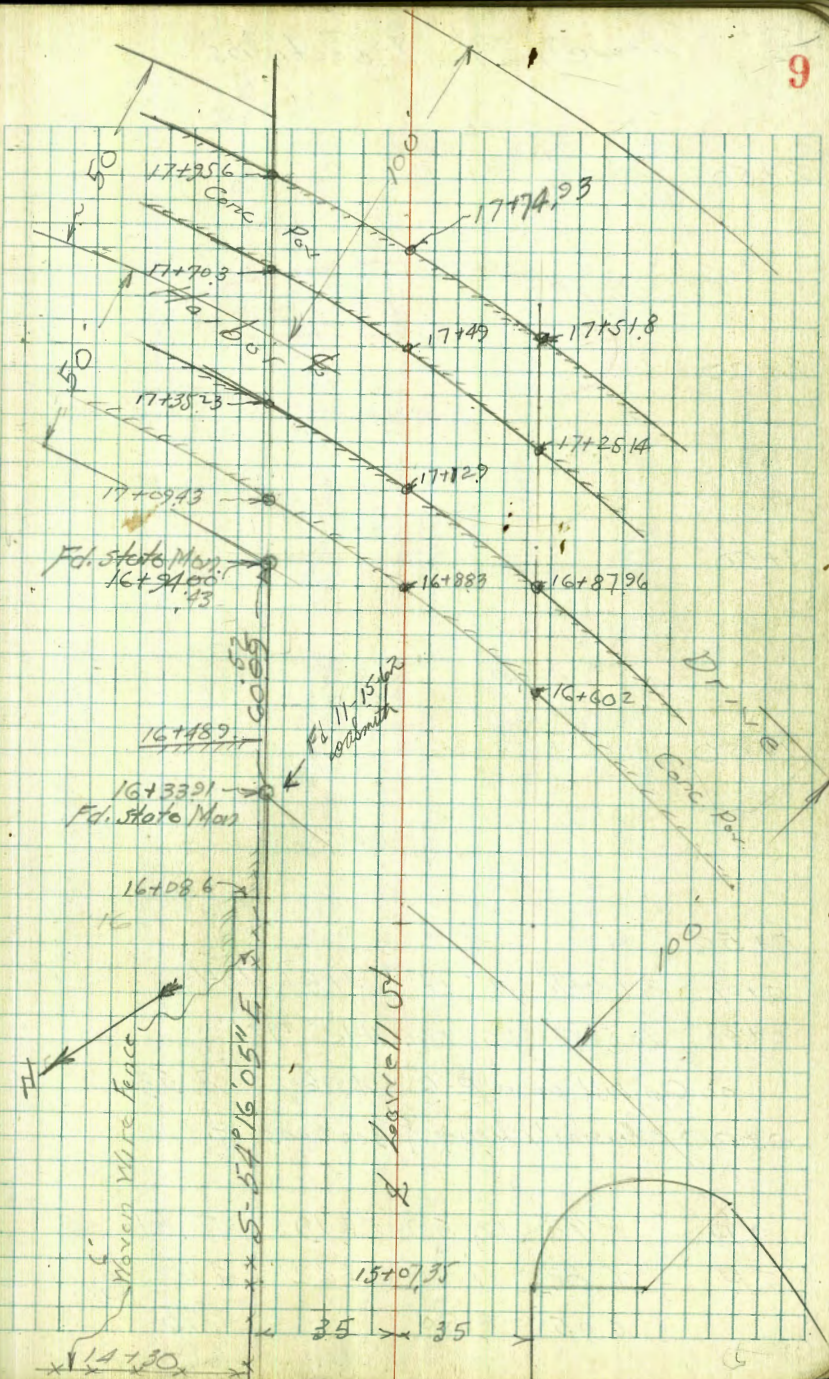
SHAFTER ST

HEARTS

Lowell St

X-Sections

9



Lowell St. X-Sections

	+	#1	-	K	DM
2+50					
	See <u>FB 1747</u> 53-59				
2+00					
1+50					
1+00					
0+50					
0+29	Tel Pole 18.5' Lt 412631-H				
0+28	18.5' Rt SDG & Elec Pole #2981				
	on Cap. Dist	0+00	P-6	4.06	8.53
0+00	Easterly Line Rosecrons St.				
TP	4.78	12.59	3.19	7.81	
TP	6.82	11.00	4.62	4.18	8M.
	6.05	8.80		2.76	

Reduced by W.K. Lear

2.82	2.18	2.39	2.06	2.57
9.77 17 cb.	10.41 17 cut	10.20 17 Rev.	10.53 17 cut	10.02 17 cb.
	3.45	3.55	3.30	3.84
	9.14 17 cut	9.04 17 Rev.	9.29 17 cut	8.75 17 cb.
	4.81	4.77	4.46	5.01
	7.78 17 cut	7.82 17 Rev.	8.13 17 cut	7.58 17 cb.
	6.09	6.03	5.74	6.22
	6.50 17 cut	6.57 17 Rev.	6.85 17 cut	6.37 17 cb.
	8.03	7.34	6.97	7.45
	4.56 17 cb.	5.27 17 cut	5.25 17 Rev.	5.61 17 cut
	8.51	8.53	8.28	
	4.08 17	4.06 17 Rev.	4.31 17 Rev.	
		12.59		

S.W. SP. Rosecrons - Garrison

SK

Scott & Lowell

Lowell St.

X-Sections

TR 4.34 5.73 4.20 1.39

Nail
1" Pole3+35 = ~~W~~ Scott St.

+ HE - E

3+18

3+08.5

3+00+ = W. Scott St.

2+96.9

2+93.5 = B.C. 15' cb Ret on Lt.

2+55.5 = End Exist cb. on Rt

TR 2.86 5.59 9.86 2.73

12.59

Lt.

L

Rt

11

3.71	2.78	2.74	2.35	1.29	1.41	1.09	0.94	0.82	0.59
188 50 Rev.	281 377 Rev.	285 38 Rev.	374 314 Rev.	436 17 Rev.	418 Kitt M.H.	456 17 Rev.	465 350 Rev.	477 50 Rev.	580 100 Rev.

4.02	2.96	2.97	2.50	1.48	1.51	1.21	0.91	0.89	.74
157 50 Rev.	263 377 Rev.	262 38 Rev.	303 319 Rev.	411 17 Rev.	408 Rev.	438 17 Rev.	468 35 Rev.	47 50 Rev.	485 100 Rev.

3.07	3.42	3.15	3.20	2.71	1.57	1.57
250 50 Rev.	211 35 Rev.	244 35 Rev.	239 316 Rev.	288 316 Rev.	402 17 Rev.	402 Rev.

1.56	1.61	1.15	1.23	1.89	2.29	2.25	3.04
403 17 Rev.	3.98 Rev.	444 17 Rev.	436 19 Rev.	3.7 23 Rev.	32 35 Rev.	284 50 Rev.	255 100 Rev.

-0.33	1.25
592 16 Floor	434 16 Garage
15" Conc. Culvert	

1.95	1.35
364 17 Rev.	434 17 Rev.

1.99	2.49
360 17 Rev.	310 17 Rev.

5.59
12.59

441
118
50
Rev.

Reduced by W.K. Lear

Lowell St
X-Sections

4+87 = West edge Conc. Ramp on Lt

4+63 = Tol Pole #450920-H 192 Lt

4+50

4+00

3+84 = Guy Anchor 24' Rt

3+70 = Eburne Scott St

3+61 = ~~FDK~~ Tol Pole Guy 450921-H 237 Rt

3+60.7

3+46 = East edge Pav on Rt

3+43.5 = ^{Sewer} ~~6~~ D.H.

5.73

Reduced by W.L. Lear

Lt

\$

Rt.

12

1.34	4.35									
49	36									
on Conc	on Conc Ramp									
2.0	0.2	0.02	0.23	0.73	0.4	0.1	1.6	1.9	2.1	
3.7	5.0	5.3	5.5	5.0	5.8	5.8	4.1	3.8	3.6	
35	17	17	9	15	17	21	24	35	45	
2.3	0.63	0.02	0.3	0.93	0.1	0.1				
3.4	5.1	5.3	5.7	4.8	5.6	5.6				
35	17	17	8	17	35	45				
2.1	0.69	0.32	0.65	0.05	0.43	0.4	0.2			
3.6	4.0	5.35	5.08	5.68	5.3	5.3	5.5			
35	17	13	17	11	17	35	45			
		Edge Pav	Edge Pav							
3.4	2.50	2.48	2.19							
2.9	3.3	3.25	3.54							
5.5	3.7	3.5	3.14							
Pav	Pav	Pav	Pav							
3.55	2.66	2.59	2.27	1.08	1.21	0.79	0.51	0.37	0.10	
2.18	3.07	3.14	3.46	4.65	4.52	4.24	5.22	5.36	5.63	
5.0	3.74	3.5	3.4	1.7	1.7	1.7	3.5	5.0	1.00	
Pav	Pav	Pav	Pav	Pav		Pav	Pav	Pav	Pav	
					1.42	1.41				
					Rim MH					
					5.73					

Lowell St,

X Sections

6+58 = Tel Pole 20.3' Lt No Number

6+50

6+21.2 = Bag Conc Ret Wall on Rt

6+00 Cont,

6+00

5+70 S.G. & E. No Number 24.6' Rt

5+50

5+28 = East end Conc. Ramp on Lt

5+18 S.G. & E. # 2841 12' Rt

5+00

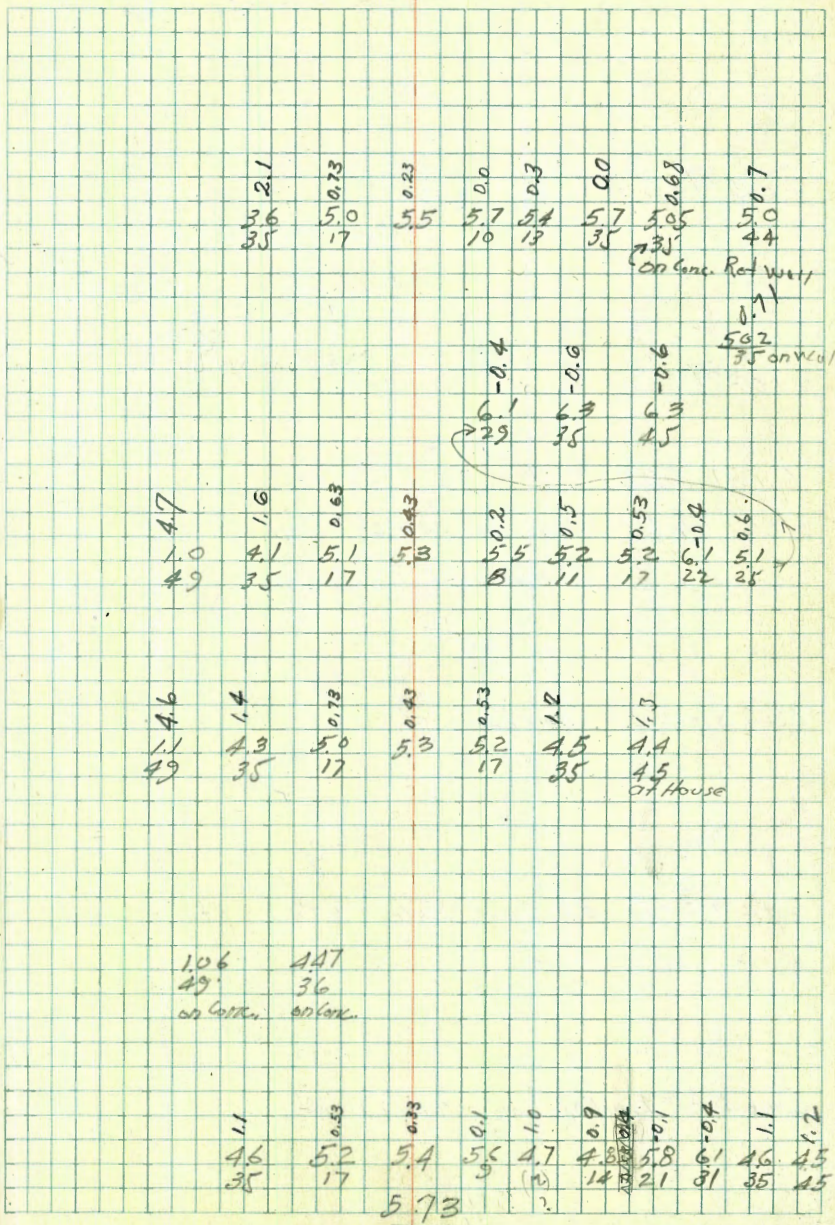
5.73

Lt

Rt

Rt

13



Lowell St.

X Sections

7+05.07 = Shaft on St.

See 1799 - P. 26

Shafter Sections

6+88.07

6+81 SDGE Pole #16.98 37' Rt

6+79 Tel Pole Anchor 19' Lt

on Pipe sur for Shafter = Lowell St

TR 9.77 10.54 4.96 0.77

6+70 = Wk. Shafter St.

6+67.3 = 52' Conc. Side Walk on Rt.

6+64.4 = End of 6' on Walk on Rt

5.73
8

66	2.8	9.13	0.69	10.5	0.0	0.0	-0.2
39	7.7	9.2	9.85	10.0	10.5	10.5	10.7
47	35	17	on Hub	17	35	50	17

60	2.6	6.9	0.7	10.3	10.1	10.1	0.2
45	7.9	9.6	9.8	10.3	10.6	10.4	10.3
47	35	17		17	35	50	11.6

56	2.4	10.10	10.54	0.0	0.0	0.6	0.7
61	3.3	4.8	1.4	5.7	5.2	5.7	5.0
46	35	17	53	15	17	29	35

0.74	0.72	1.31
4.99	5.01	4.45
35.2	47	11.65
on Walk	on Walk	End Walk
5.10		
5.03		
35		on Walk

5.73

Lowell St.

X Sections

8+57 = A Server MH

8+00

7+88 Tel Pole 35' H # 450932-H

7+80

7+70 = Elec. # 2781 21.6' R

7+64

7+40.07 = F. Line Shafter St.

7+22.07

10.54
10.54

Lt.

E

Pt.

15

496	50	52	73	50	514	55	61	54	80	70	56	57
42	35	21	16	12	Firm MH	13	17	24	31	35	39	50
conc. gutter												

5.5	5.1	4.1	2.1	3.9	3.6	3.4	3.0	2.5	3.9	3.6	3.6
5.0	5.4	6.4	8.4	6.6	6.9	7.1	6.2	8.0	6.6	6.9	6.9
40	35	20	17	15		17	37	36	42	38	38

5.8	4.8	3.6	1.6	2.6	2.9	2.5	2.2	1.9
4.7	5.7	6.2	8.9	7.0	7.6	8.0	8.2	8.0
45	35	19	16	18		17	35	25

4.4	3.4	2.4	2.2	1.5	1.2	2.2	1.8	1.7	1.6
6.1	7.1	8.1	8.3	9.0	9.3	8.3	8.7	8.8	8.9
35	17	14	50	40		7	17	35	45

7.0	3.7	2.1	1.5	1.1	1.4	1.3	1.3	1.4
25	6.8	8.4	9.0	9.4	9.1	9.1	9.2	9.2
47	35	17		17	35		50	117

6.5	3.2	1.8	1.1	0.7	0.8	0.5	0.7
4.0	7.8	8.7	9.4	9.8	9.7	10.0	9.8
47	35	17		17	35	50	117

10.54

Lowell St.
X-sections

10+88 = Tel Pole 450934-H 35' Lt

10+50

10+18.6 = Elec. Pole 185'R # 2761

10+00

10+07.6 = East end Ramp

9+66.4 = West end Asphalt Ramp on Lt

9+50

9+38 Tel Pole 450933-H 35' Lt

9+00

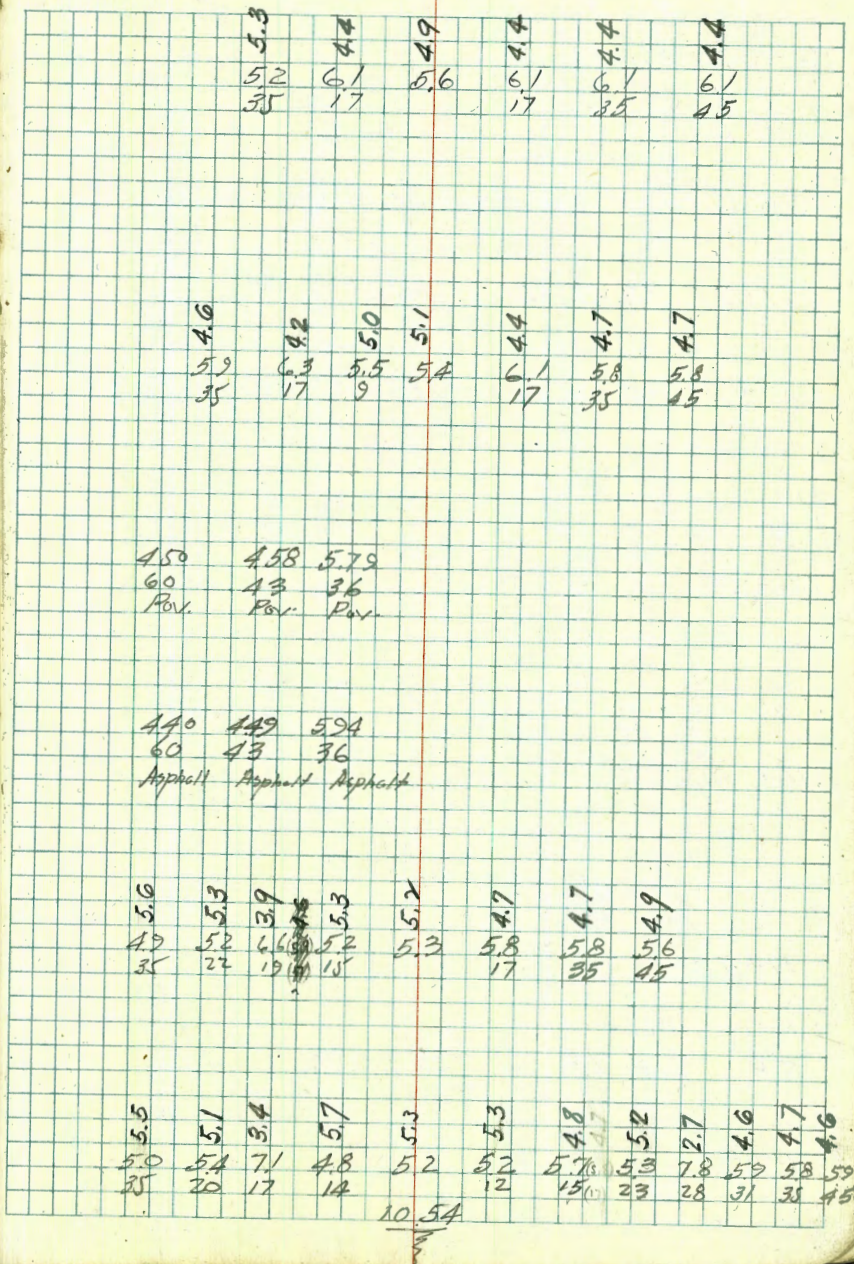
10.54
10.54

Lt.

Rt.

Rt.

16



Lowell St.

X-Sections

13+00

13+01 = East end Asphalt Ramp on Lt

12+627 12' RT = Elec. Pole # 2641

12+614 = West end Asphalt Ramp on Lt

12+50

12+00

11+50

TR 4.73 9.53 3.72 4.82

11+00

10.54

Lt.

Rt.

Rt.

17

4.7	4.2	4.7	4.9	4.6	4.6	4.4	4.2	4.1
4.8	5.3	4.8	4.6	4.9	5.1	5.3	5.1	5.1
35	17	10		12	17	35	35	45

6.44	6.36	5.68
4.10	4.18	4.86
5.0	4.3	3.6
Per	Per	Per

6.44	6.32	5.58
4.10	4.22	4.96
5.0	4.3	3.6
Per	Per	on Per

5.3	4.9	4.4	4.8	4.9	5.0	4.1	4.7	4.4	4.2
4.2	4.6	5.1	4.7	4.6	4.5	5.4	4.8	5.1	5.3
35	23	17	12		11	17	27	35	45

5.4	4.4	5.0	5.1	5.1	5.1	5.5	4.5	4.1
4.1	5.1	4.5	4.4	4.4	5.0	5.9	4.9	4.4
35	17	10		11	17	35	35	45

5.3	4.5	5.0	5.0	4.3	4.4	4.2
4.2	5.0	4.5	5.2	5.1	5.1	5.3
35	17		17	35	45	45

9.55

5.4	4.4	4.8	4.3	4.5	4.5
5.1	6.1	5.7	6.2	6.0	6.0
35	17		17	35	45

10.54

X-Sections

15+72

TR 4.81 9.13 5.23 4.32

15+50

+38 = Pole Anchor 20' Rt.

15+19.5 Elec Pole 25.81 20' Rt.

15+00

14+50

14+02 = S. Savick M.H.

13+50

2.55

16 10	45 35	47 35	46 26	32 16	48 12	42 19	45 16	40 18	34 20	45 20	40 35	48 35
49 40	46 35	46 35	43 22	34 17	44 14	42 53	43 12	37 17	43 20	44 27	44 35	40 50
45 30	45 35	43 22	37 17	43 13	44 51	40 17	40 35	37 25	36 45			
45 40	45 35	45 30	39 17	45 12	47 48	43 11	40 17	42 19	37 35	36 45		
48 40	47 35	45 33	40 17	45 12	48 474	47 11	41 17	42 35	38 45			
45 40	47 35	45 33	42 17	46 10	48 47	46 12	41 17	43 22	41 35	40 45		

9.13

9.55

Cont P-21

TP	11.58	12.97	4.15	1.39
TP	4.84	5.54	2.52	0.70
TP	5.12	10.22	4.03	5.10

17+24.93 Int. East edge Pav. Section on Pav.ing.

17+49 = Int. edge Conc. Pav. Section on Pav.ing.

17+24.7 4.1 Lt = Signal Std.

17+24

17+14 39.2 Rt = Signal Std.

17+12.9 Section on Edge Pav. See sketch P-9

16+88.3 Section on West edge Conc. Pav.

16+79 = Int. w/d shoulder to on rt'd shoulder Section Parallel to Pav.ing & Harbor

2.13

6.19	6.67	6.92	7.08	6.90	6.80	6.66	6.32	6.29
304	249	221	205	223	233	247	261	284
190.2	140.2	20.2	40.2		41.7	91.7	141.7	191.7
					Pav.	Pav.	Pav.	Pav.
5.94	5.99	5.93	5.62	5.60	5.51	5.3A	5.13	
315	314	320	351	353	362	379	382	
140.5	20.5	40.5		42.2	92.2	142.2	153.5	
					Pav.	Pav.		
5.0	4.8	4.7	4.6	4.5	4.18	3.96	3.90	4.2
41	43	44	45	46	435	517	523	49
131	31	40.8		42.6	516	92.6	129.6	143
					Pav. Edge	Pav.	Pav. Edge	
4.90	4.77	4.59	4.44	4.38	4.26	4.11		
423	441	454	469	475	487	502		
141.2	91.2	41.2		42.8	92.8	142.8		
					Pav.	Pav.		
3.96	3.65	3.51	3.34	3.22	3.10	2.9		
517	548	562	579	591	603	622		
141.7	21.7	41.7		43.6	93.6	143.6		
					Pav.	Pav.		
3.77	3.74	3.70	3.67	3.29	2.93	2.66	2.60	2.57
571	589	603	609	616	629	647	653	656
108	50	77	20		120	40	50	100
					Pav.			

9.13

Lowell St.

X-Sections

21

Rosecious (Garrison)				$\frac{0.01}{2.75}$	544.64
chk. starting 8M.		5.47		2.74	
T.R	4.63	8.21	6.87	3.58	
T.P	2.65	10.45	5.17	7.80	
	<u>12.97</u>				
	3	Cont. from p. 20			

X see Macaulay W.D. 21023
 Willow to Plum

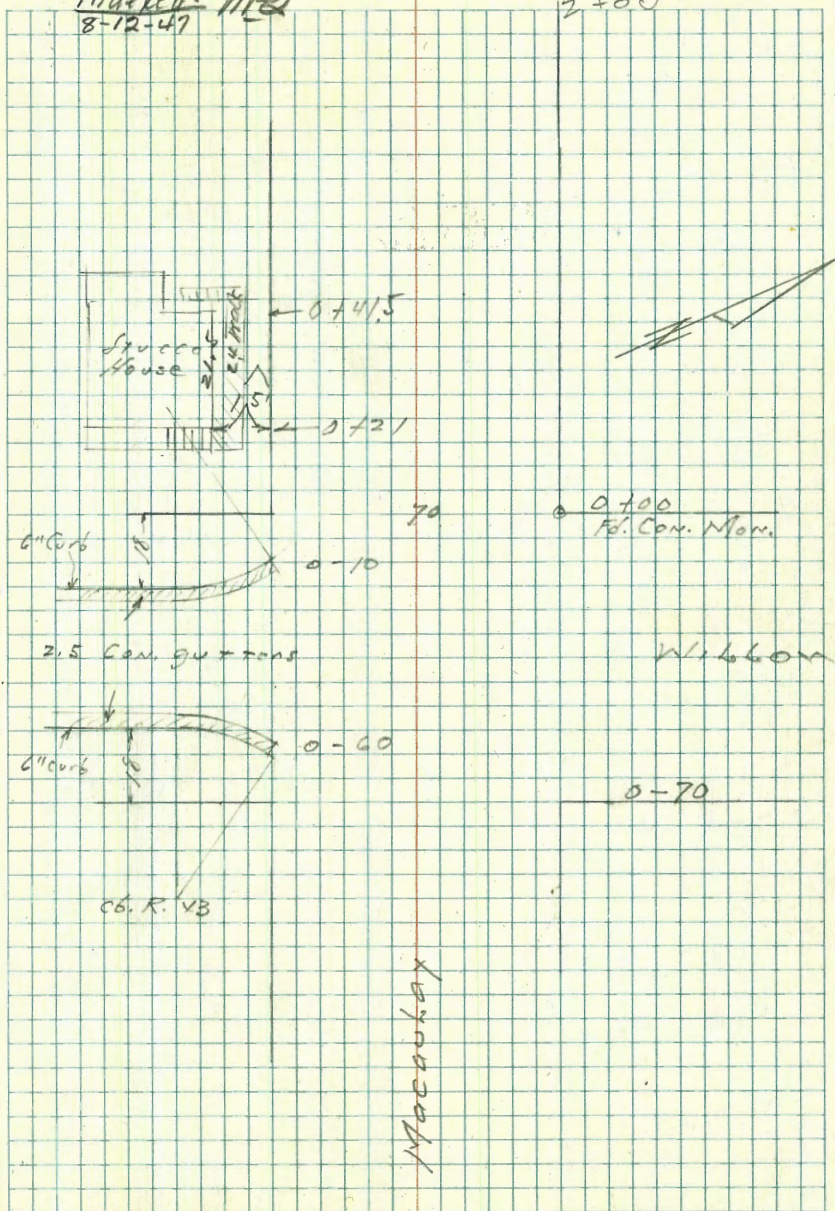
Moore
 Green
 Roberts

8-11-47

INDEXED

Indexed: M²
 8-12-47

2+00



Macaulay

0-10

60.3

9.8

60

0-18

0-35

T.P. 2.72 70.15 1.10 62.43

0-52

0-60

0-70 E.L. Willow

BM SWBP

Lowell

Willow

11.27

63.53

52.26

LT = 54
61.10 60.78 61.4 62.8 64.1 65.1 67.4 66.3 61.2 23

90.5 9.97 8.7 7.3 6.1 5.0 2.7 3.8 8.9
3.5 3.5 3.5 1.8 2.3 2.5 3.5 60
6 7 7.2

60.15 59.38 60.9 61.4 63.5 64.1 65.7 65.0 59.9
10.00 10.77 9.2 7.9 6.6 6.0 4.4 3.1 10.2
60 60 35 18 60 18 24 35 60

9.8 61.2 62.6 62.5 63.4 64.1 56.3
10.3 8.9 7.5 6.0 4.7 3.0 13.8
60 35 18 60 78 35 60

59.02 58.19 59.9 61.1 60.8 59.7 56.8 51.8
4.51 5.34 3.5 2.4 2.7 3.8 4.7 11.7
60 60 35 18 60 78 35 60
6 7

59.0 60.09 59.29 60.0 58.6 56.8 54.0 50.0
4.5 3.44 4.24 3.5 4.9 6.7 9.5 13.5
60 35 35 18 60 78 35 60
6 7.2

59.2 59.6 58.6 56.4 56.1 51.8 47.3
4.3 3.9 4.7 7.1 9.2 11.7 16.2
60 35 18 78 78 35 60

63.53

0767 Sing. gar. Con. Fl.

0755

0741.5

0731 27 Lt Po. Co. Gux Pole

0728 19 R T.C.P. 89759H

0721

T.P. 10.10 86.38 143 76.28

0714

T.P. 8.08 77.71 0.52 69.63

0702 28 Lt P.T. 1730

0700 W.L. Willow

70.15

5.80
64

80.0	80.5	80.9	80.4	79.4	77.0	76.6
6.4	5.9	5.5	6.0	7.0	8.8	9.8
45	35	18		18	35	45

18.6	19.0	19.3	19.2	18.0	16.0	15.9
7.9	7.0	7.1	7.2	8.4	10.4	12.5
47	35	18	7.2	18	35	45

Exwalk

79.4	76.3	76.4	77.0	76.1	75.6	73.0	71.4
7.0	10.1	10.0	9.4	10.3	10.8	12.8	15.2
50	17	35	18	10.3	18	35	45

Fl. Fl. Exwalk
N.E. Cor.
House

15.4	12.1	11.1	69.7	74.2	75.4	73.8	71.3	69.1
2.3	3.6	2.1	5.0	5.5	2.3	3.9	6.4	2.4
45	35	22	18	55	4	18	35	45

77.71

64.6	65.0	63.9	65.6	66.6	70.0	68.2	63.3
5.5	5.1	6.2	4.5	3.5	0.1	1.9	5.2
60	35	18	4.5	18	22	35	60

70.15

Check SWBP
 Plum + Lovell 5.93 87.23 87.22
 T.P. 837 93.16 11.98 84.79
 2100

1178

1150

1141 206 Pt 701 P. 89758 H

1125

T.P. 10.44 96.77 0.05 86.33

1100

1175 35' LT N end Rd. fence

86.38

R 25

87.8	87.9	90.2	91.9	92.4	92.5	92.5	93.7	94.3	95.8	96.1
10.0	8.9	6.6	5.4	4.4	4.3	4.3	3.1	2.5	1.0	0.7
45	35	18	7	2	1/2	1/2	1/2	1/8	3/5	1/5

85.9	87.2	88.8	90.0	91.0	90.9	91.0	92.2	92.9	94.6	94.4
10.9	9.6	8.5	6.8	5.8	5.9	5.8	4.6	3.9	2.7	2.4
45	35	18	8	5	5	1/2	1/4	1/8	3/5	1/5

85.1	86.0	87.1	88.6	89.5	89.4	89.2	90.4	90.9	91.8	91.4
11.7	10.8	9.1	8.2	7.3	7.4	7.5	6.4	5.9	5.0	5.4
45	35	18	8	5	7.4	11	13	18	35	45

84.0	84.7	86.0	87.0	87.9	87.1	87.5	88.6	89.1	88.6	88.0
12.8	12.1	10.8	9.8	8.9	9.1	9.3	8.2	7.1	6.2	5.8
45	35	18	8	5	9.1	10	13	18	35	45

82.9	83.4	84.8	85.4	86.0	86.77	85.2	86.2	85.7	85.2	84.4
3.5	3.0	1.6	1.0	0.4	0.8	1.0	0.7	0.7	1.0	2.0
45	35	18	9	6	0.8	9	12	18	35	45

81.4	81.9	82.2	82.0	82.2	82.0	82.9	82.1	81.1	80.2
5.0	4.5	4.0	3.4	3.6	4.0	3.7	3.0	2.3	1.4
45	35	18	7	3.6	7	9	18	35	45

86.38

L

e

R

26

A table with 10 columns and 20 rows, defined by blue horizontal lines and red vertical lines. The table is empty.

A large grid with 20 columns and 20 rows, defined by blue lines. The grid is empty.

X-Section 20' Alley in Block 102 - Univ. Hts.

1503

W.O. 31385 ± 25001

8-26-47

See T.P. Book - 21
P. 74

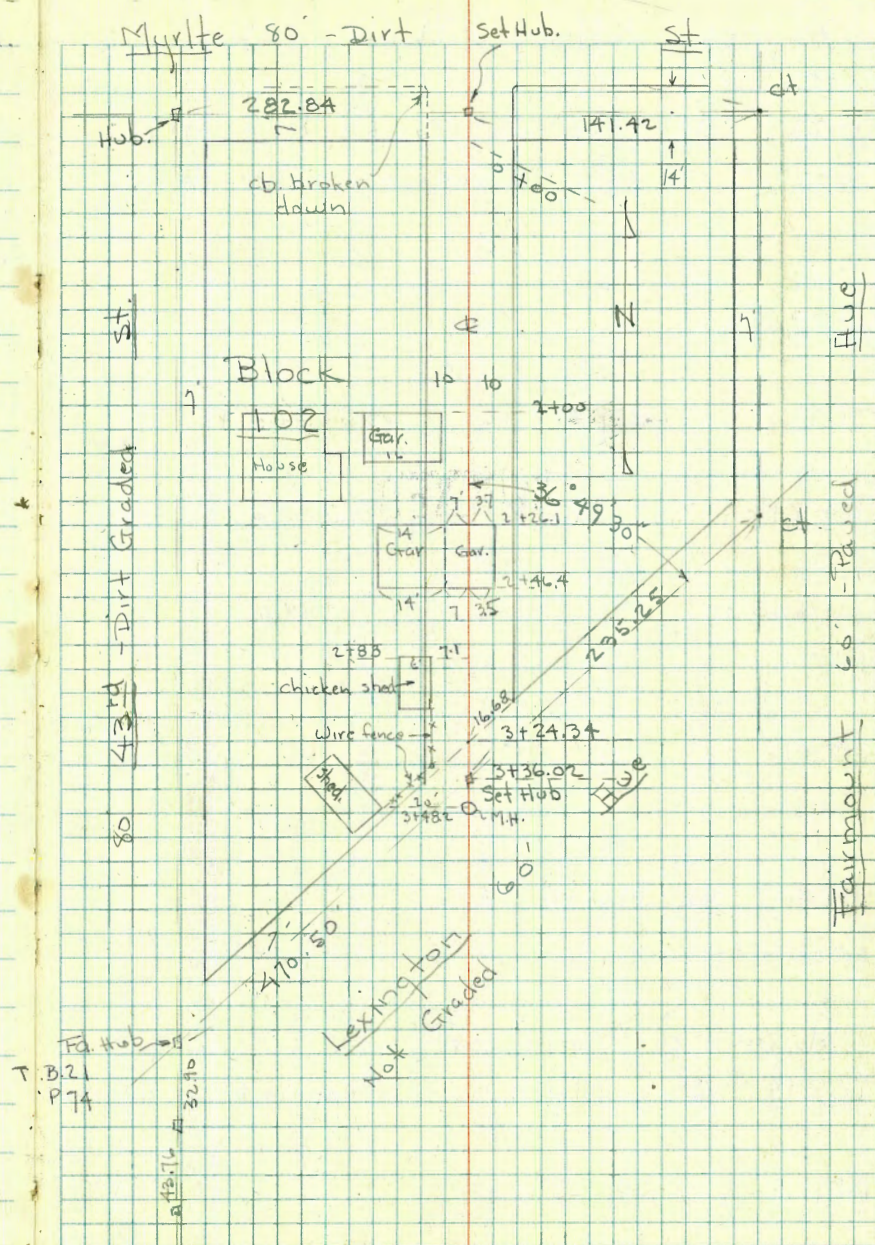
Osborne
Hardin
Worrell

Levels - Next Page

INDEXED

Indexed
C.S.K.

27



X-Sect. 20' Alley - Block 102

1+25

1+22 - 8.2 Rt. = Wly. P. pole #PA 3475

1+19 - 137 - Lt. = Φ Sing. Gar. - Conc. floor

1+00

T.P. 0.15 323.12 9.23 322.97

0+84 - 14.1 Lt. = Φ Sing. Gar. - Dirt floor

0+60

0+15

0+00 - S.L. Myrtle

down - see Myrtle - sections

0-14 - S. cb. Myrtle - curb Ret. on W. is broken

BM 0.20 332.20

332.00 New Myrtle
Fairmount

Lt. = E.

Φ = Rt = W.

28

	321.6 15 10	321.2 19	321.3 18 10	320.0 2.1 2.0	
0.70 13.7 floor					
	322.1 0.0 20	322.7 0.4 10	322.3 0.8	321.9 1.2 10	321.1 2.0 30
					320.1 4.4 60 15.0 10.0 bottom of wash
			323.12		
323.5 8.7 14.1 floor					
	324.3 7.9 20	324.3 7.9 10	323.8 8.4	323.5 8.7 10	323.7 9.0 20
	325.5 6.7 20	325.4 7.0 10	325.0 7.2	325.0 7.2 10	324.4 7.8 23 - Breaks down To wash on Rt.
	325.50 6.70 11.2 Top-end Ret.	325.4 6.8 11.2 9.4	324.6 7.4	324.76 7.44 9.1 Top + gut - end Ret.	
	325.30 6.82 11.2 Top 1 Rad. Ret	324.8 7.4 11.2 9.4	324.5 7.7	324.3 7.9 10 ground cb. buried see Sect.	
			332.20 ✓		

I.P. 141 313.81 10.72 312.40

2+46.4 = S. side Gar.

2+26.1 = N. side of Damp Gar. - Conc. floor
Gar on Rt. is lower.

2+25

2+20 - 31.9 Rt. = \oplus House

2+12 - 7.8 Rt. = SE Cor Gar. - steep Conc. slab Ramp

2+00 - 7.7 Rt. = NE Cor. Sing. gar. - Conc. floor

2+00 - 5.7 Lt. - 2" water main - exposed

1+80

1+50

1+38 - 7.3 Rt. = \oplus Guy - dead man

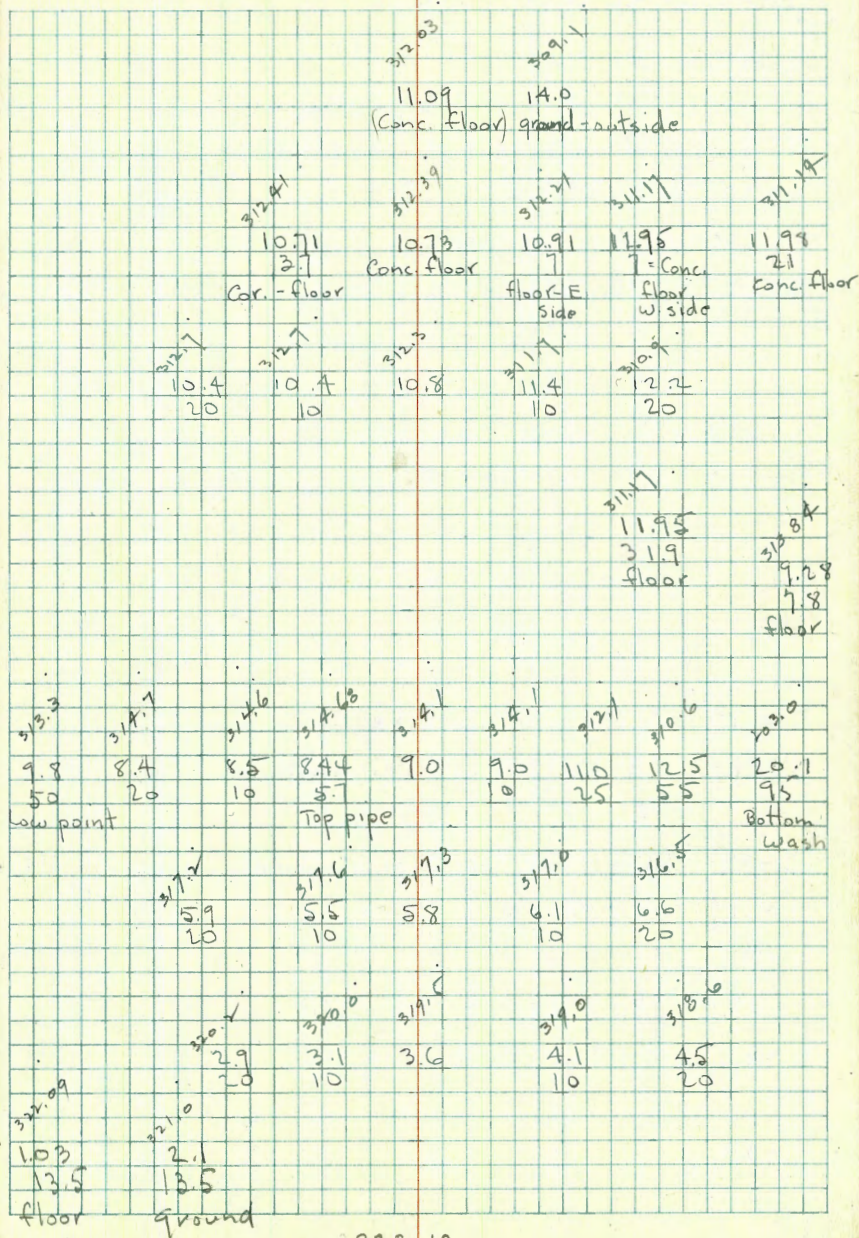
1+36 - 13.5 Lt. = \oplus frame House

Lt.

\oplus

Rt.

29



T.P. for check on Next Alley

8.10 305.71

3+48.2 = Φ Sewer M.H.

3+37.7 = W.L. Alley + N.L. Lexington

3+30 - 6.2 Rt. = Cor. = End-wire fence

slab over sewer

3+24.34 = Φ Alley + N.L. Lexington = end of Conc.

3+11.8 = E.L. Alley + N.L. Lexington

3+01 - 0.9 Lt. = Φ Beg. 18" Conc. Cover over Sewer

3+00

2+97 - 7.1 Rt. = Beg. wire fence

2+97 - 7.1 Rt. = S.E. Cor. chicken House - Conc. floor

2+83 - 7.1 Rt. = N.E. Cor. stucco chicken House - 6' wide

2+79 10.6 Rt. = Φ 6" Olive

2+75

2+68 - 10.9 Rt. = Φ 12" Olive

2+52 - 9.7 Rt. = Φ 4" Fig.

2+50

30

306.9 6.9 20	306.1 7.7 10	304.41 9.40 on Rim	301.9 11.9 5	301.9 11.9 10	301.6 12.2 20 = ground
					N.E. Cor. shed.
306.5 7.3 20	302.6 9.2 10	302.6 11.2 6	302.0 11.8 10	301.8 12.0 10	302.9 12.9 20
305.0 8.8 20	302.7 11.1 10	302.23 11.48 0.9 Φ slab.	302.3 11.5 10	302.0 11.8 10	301.9 11.9 20
303.5 10.3 20	302.8 11.0 10	302.67 11.14 0.9 Φ Conc. slab.	302.5 11.3 10	302.0 10.8 10	303.5 10.3 20
303.51 10.30 0.9 Top Conc.					
307.0 6.0 50	305.4 8.6 20	303.9 9.9 10	304.0 9.8 10	304.1 9.7 10	304.1 9.7 20
					302.8 13.0 70
					304.1 16.7 90 Bottom wash
					305.55 8.26 7.1 = Conc. floor
					305.83
307.8 6.0 20	307.5 6.3 10	307.1 6.7 10	307.1 6.7 10	307.1 7.2 20	7.98 = Conc. floor 306.6
308.2 3.5 6	308.1 3.7 10	309.3 4.5 10	308.7 5.1 10	308.4 5.4 20	

313.81

X-Section 20' Alley in Block 104 - City Hts.

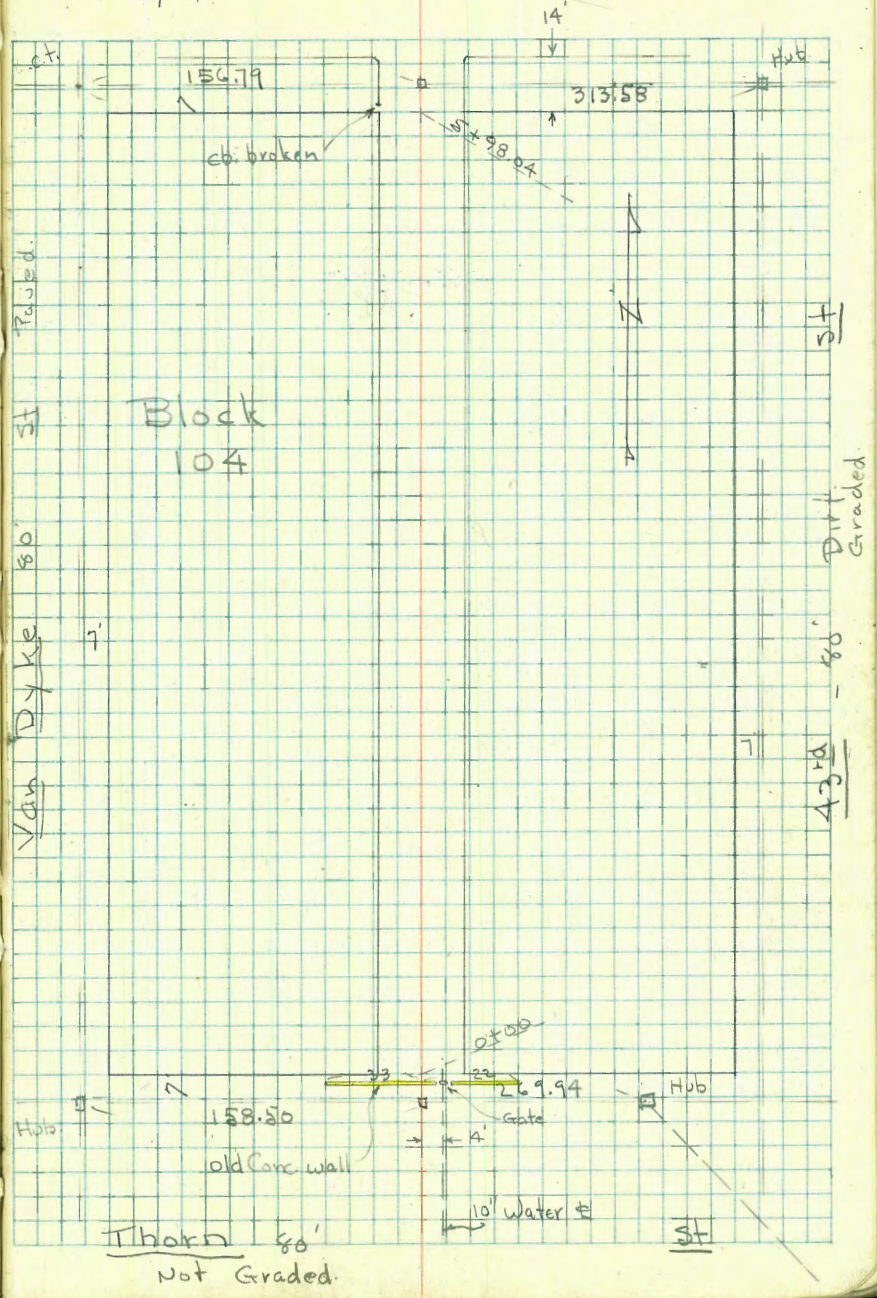
W.O. 31385 + 25001

8-27-47

See T.P. 21 - P. 74

Osborne
Hardin
Worrell

INDEXED



8-28-47
7.0.

X-Sect. 20' Alley in Block 104

1+00

T.P. 13.04 313.04 0.10 300.00

0+65

0+52 - 6.5 Lt. = Wly. P. pole " A 3315

0+40

0+29 - 6.5 Lt. = E Guy - dead man

0+00 = N.L. Thorn

0-0.14 = N. side of 12' Ave. - old broken Conc.
Ret. wall - See sketch - Normal to Thorn

0-01.8 - 4' Rt. = E 10" Gate - Water

0-14 - N. cb. Thorn

T.P. 3.92 300.10 12.48 296.18 T.P. P.30
B.M. 2.95 308.66 305.71

Lt. = W.

E

Rt = E.

32

Station	16.7	22.1	23.9	20.5	29.3	30.1
16.3	10.8	9.1	5.5	3.7	4.3	
40	10		10	25	40	
313.04						
29.6	29.0	29.2	29.7	29.8	30.0	
1.5	5.1	3.3	2.4	0.3	+2.9	
40	20	10		10	25	
29.7	29.6	29.4	29.9	29.7	29.3	
5.4	9.5	7.7	6.2	2.9	0.8	
40	20	10		10	40	
29.0	28.1	28.7	28.1	28.8	29.3	29.5
2.1	11.9	12.4	11.0	11.2	7.8	4.8
50	20	10		4	10	40
Top water Pipe in ground.						
29.6	29.3	29.0	29.0	29.0	29.6	
6.4	7.2	9.0	8.1	8.1	7.4	
33	10	Top wall	10	10	22	
Top end						
28.7	28.1	28.9	28.5	28.7	29.0	29.5
14	12.0	13.2	12.5	13.0	8.1	8.6
50	10		4	10	25	50
Top water 10' Pipe - exposed						
300.10						

3+48- 9.2 Lt. = end fence
 3+37- 6.6 Lt. = Wly. P. pole # P.A. 3401
 2+00

2+82- 9.5 Lt. end wire + Beq. board fence
 2+70

2+48- 9.3 Lt. = Beq. wire fence
 2+35

2+22- 9.6 Lt. = end fence
 2+02- 8' Lt. = Wly. P. pole # P.A. 3375

2+00
 1+95- 9.7 Lt. = Beq. wire fence

1+82- 7.7 Lt. = Guy - dead man

1+75

I.P. 12.13 324.65 0.52 312.52

1+50

1+25

310.8	320.8	321.3	321.2	321.1
3.8 20	3.8 10	3.3	3.4 10	3.5 25
319.4	319.6	319.6	319.5	309.9
5.2 20	5.0 10	5.0	5.1 10	14.7 45
317.4	317.9	317.8	317.9	317.5
7.1 20	6.7 10	6.8	6.7 8	7.1 10
				14.8 20 Toe
315.7	315.9	316.2	316.5	309.16
8.9 20	8.7 10	8.4	8.1 10	15.0 27 = Toe slope
314.0	314.1	314.5	315.9	314.5
10.6 30	10.5 10	10.1	9.7 10	10.1 14
				15.6 20
		324.65		
305.8	311.8	312.3	313.0	313.0
7.2 30	1.2 10	0.7	0.0 10	0.0 18
				4.4 20
298.0	307.0	309.5	311.2	311.5
15.0 45	6.0 10	3.5	1.8 10	1.5 25
				4.6 25

4+87- 10.8 Lt. = N.E. Cor - This ^{1/2} is chicken House
 4+72 - 10' Rt. = Wly 4' Euc Tree
 old Doub. Gar. - Dirt floor
 4+52- 10.2 Lt. = end picket fence + S.E. Cor
 4+50

4+34- 14.8 Rt. = E House
 4+17- 10' Lt. = Beg. picket fence
 4+11- 10' Lt. = Ely. 4" Conc. Curb from Gar.

4+05- 21.5 Lt. = E Sing Gar. - Conc. floor

4+00

3+99- 9.8 Lt. = Ely. 4" curb from Gar.

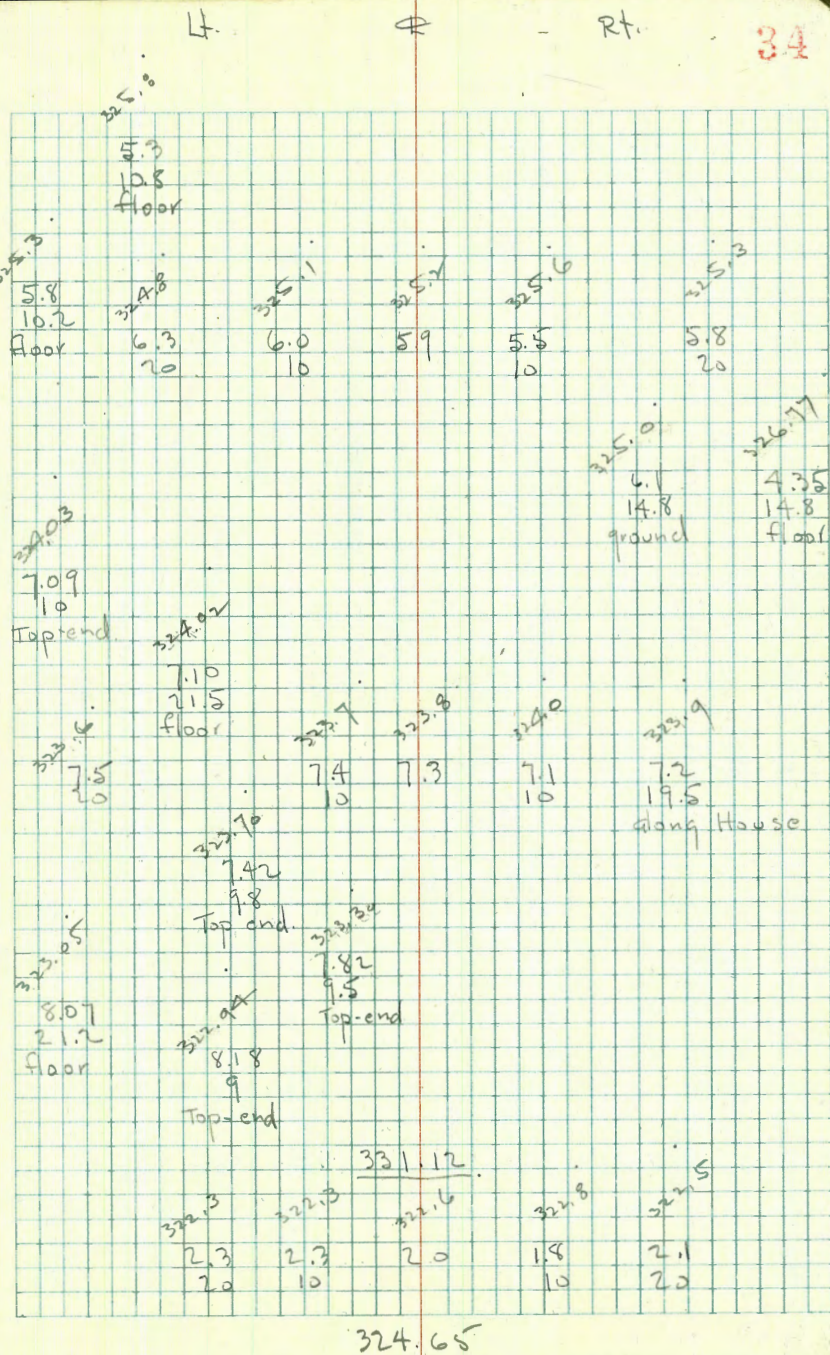
3+78- 9.5 Lt. = Ely. 4" curb from Gar.

3+72- 21.2 Lt. = E Sing. Gar. - Conc. floor

3+66- 9' Lt. = Ely. 4" Curb out from Gar.

T.P. 7.97 331.12 1.50 323.15

3+50



5+98.04 = S.L. Myrtle

5+93

5+75

5+72 - 15.1 Rt. = Φ House

5+55

5+53 - 10.6 Rt. = Φ Sing. Gar. - Dirt floor

5+40 - 11.2 Rt. = Φ old shed - Board floor

5+33 - 9.5 Rt. = U. Cor. Conc. Slab.

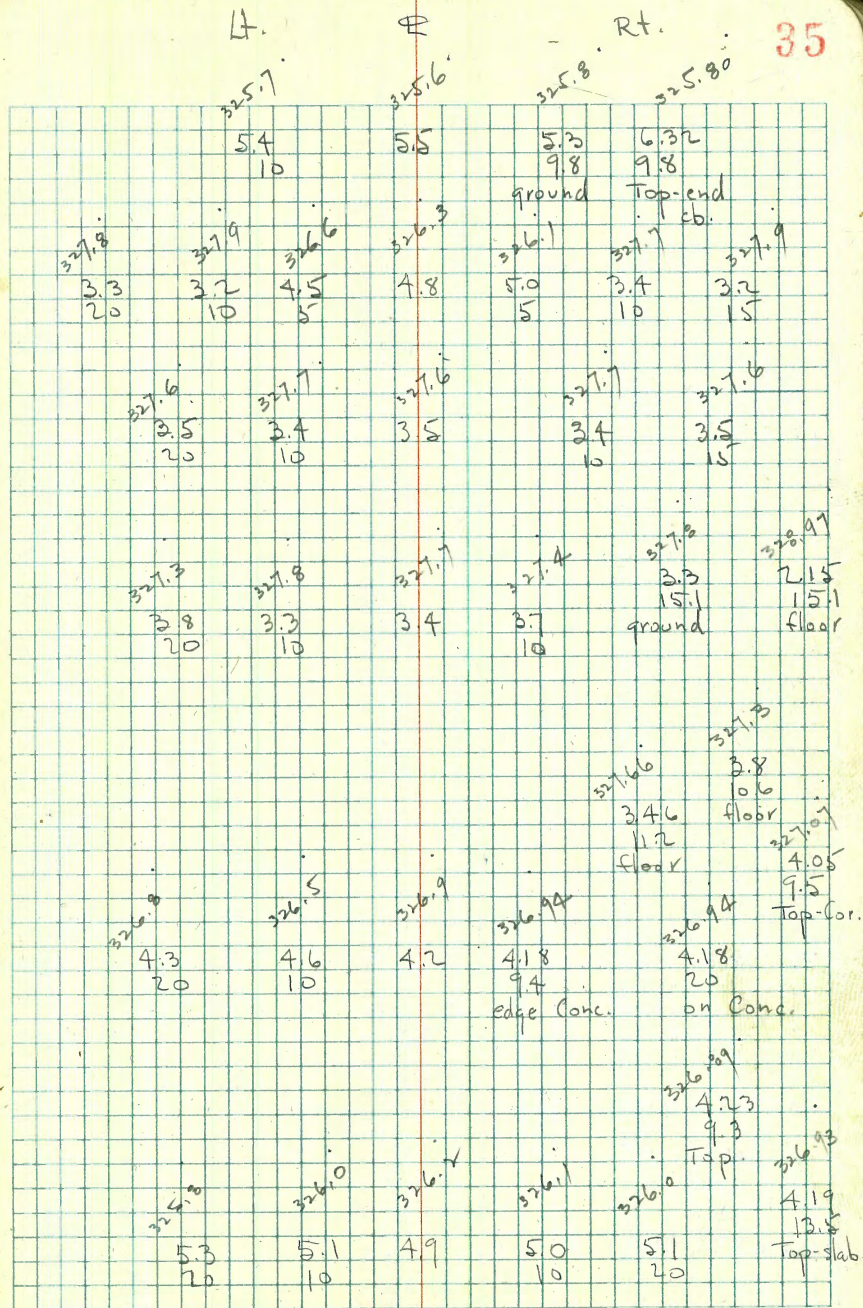
5+25

5+18 - 9.3 Rt. = Near Cor. - jog in slab.

5+11 - 8.1 Lt. = Wly. P. pole # PA. 3471

5+08 - 13.5 Rt. = Cor. Conc. slab.

5+00



331.12

check BM. nw. Myrtle + Van Dyke 4.24 326.08 326.11 = Book
 T.P. 5.38 330.32 6.18 324.94 326.09 = curs

6+12.04 = S. cb.

6+01- 9.2 Lt. = Beg. curb -

324.99	324.1	324.1	324.0	324.50
6.13	7.0	7.0	7.1	6.62
10	10		10	10
Top-1' Rad.	gut.		gut.	Top-1' Rad. Rad.
325.21				
5.91				
9.2				
Top-end cb.				
		331.12		

INDEXED
C.S.R. CITY

X-Sect. 20 Alley in Block 100 - Univ. Hts.

W.O. 31385 + 25001

8-28-47

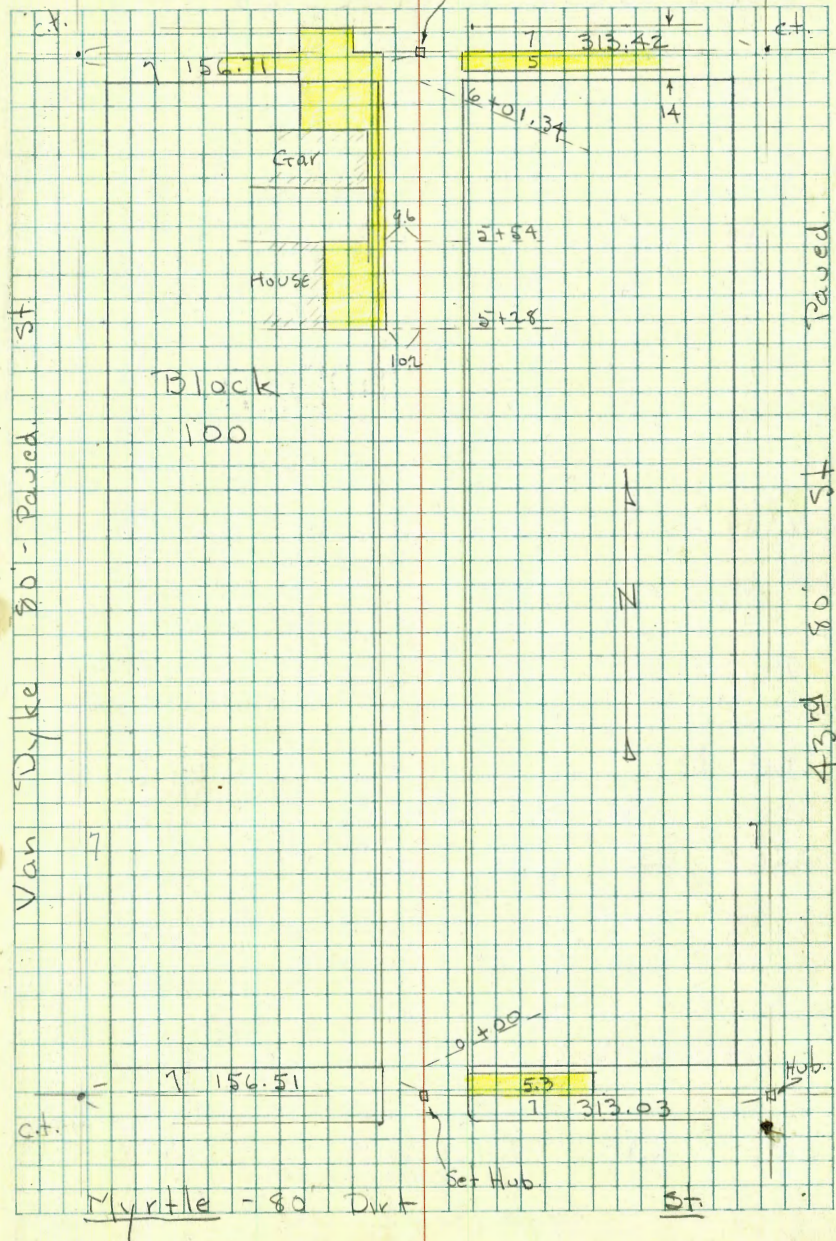
Osborne
Hardin
Worrell

9-15-47 - Notes Reduced Wherry

INDEXED

Dwight 80

Dirt St 37



X-Sect. 20 Alley in Block 100

0+50

0+38-15.9 Rt. = E House

0+30

I.P. 7.06 335.68 1.60 328.62

0+10 - 10.3 Rt. = end Conc. wall - fence Cont.

0+05

Behind 4th

0+00 - 10th Rt. = Beg Picket fence with 8" Conc. wall

0+00 = N.L. Myrtle

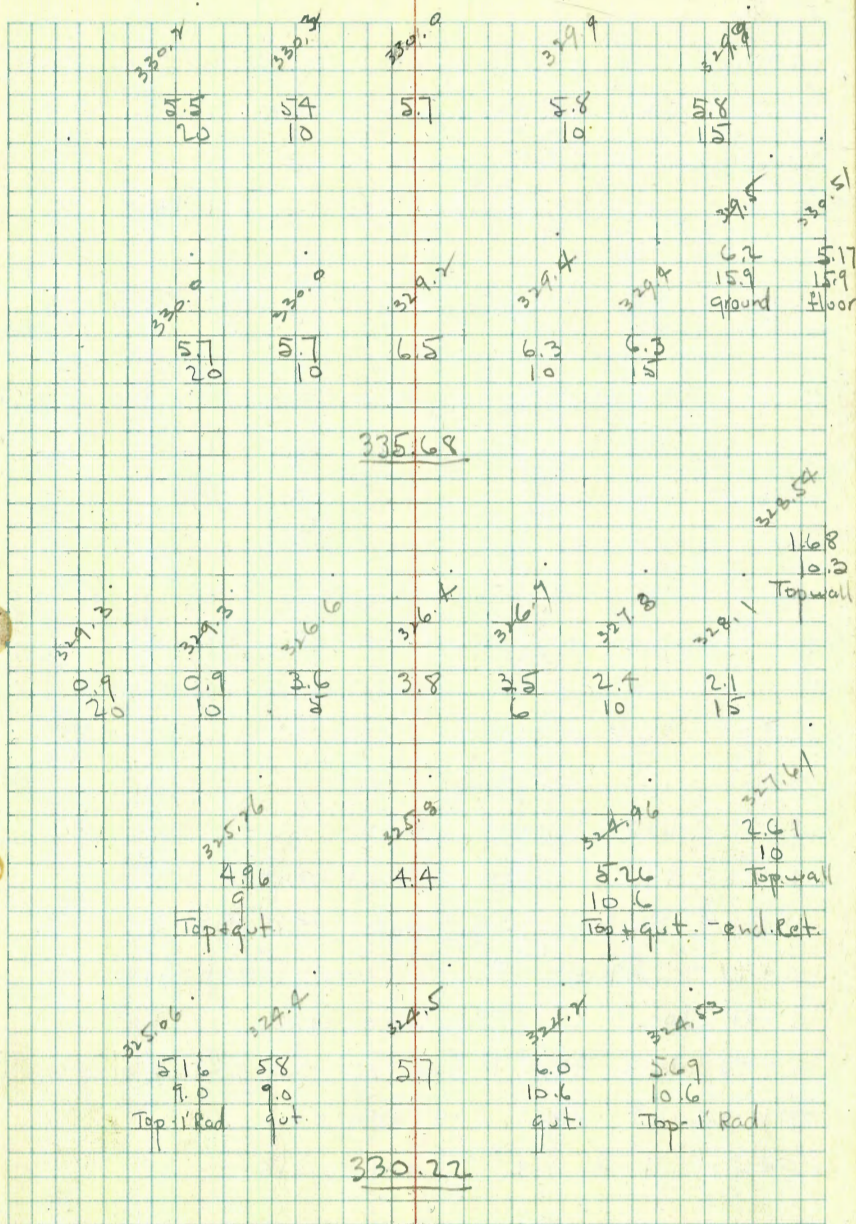
0-14 = N.cb. Myrtle

B.M. 4.13 330.22

326.09 NW Myrtle
+ Von Dyke

Lf. = W.

Rt. = E 38



parch

2+36 - 13.1 Lt. = Ely. of S. side Conc. Slab for

2+02 = 15.2 Lt. = ± 3' Conc. walk

2+12 - 10' Rt. = Beg. board fence

T.P. 6.12 337.26 4.54 331.14

2+00 - 9.9' Lt. = Wly. P. pole # PA 3533

1+90 - 14.3' Lt. = ± Sing. Gar. - Dirt floor

1+70

1+40

1+38 18.3' Lt. = ± Sing. Gar. - Conc. floor

1+32 - 9.9' Rt. = end fence

1+28 - 10.8' Lt. end fence

1+01 - 9.7' Lt. = Beg. board fence

1+00 - 9.2' Lt. = Wly. P. pole # PA 3519

0+92 - 15.4' Lt. = ± Sing. Gar. - Dirt floor

0+91 - 10' Rt. = Beg. Wire fence

0+85 16.2' Rt. = ± Sing. Gar. - Conc. floor + apron

0+77 - 9.9' Rt. = end fence

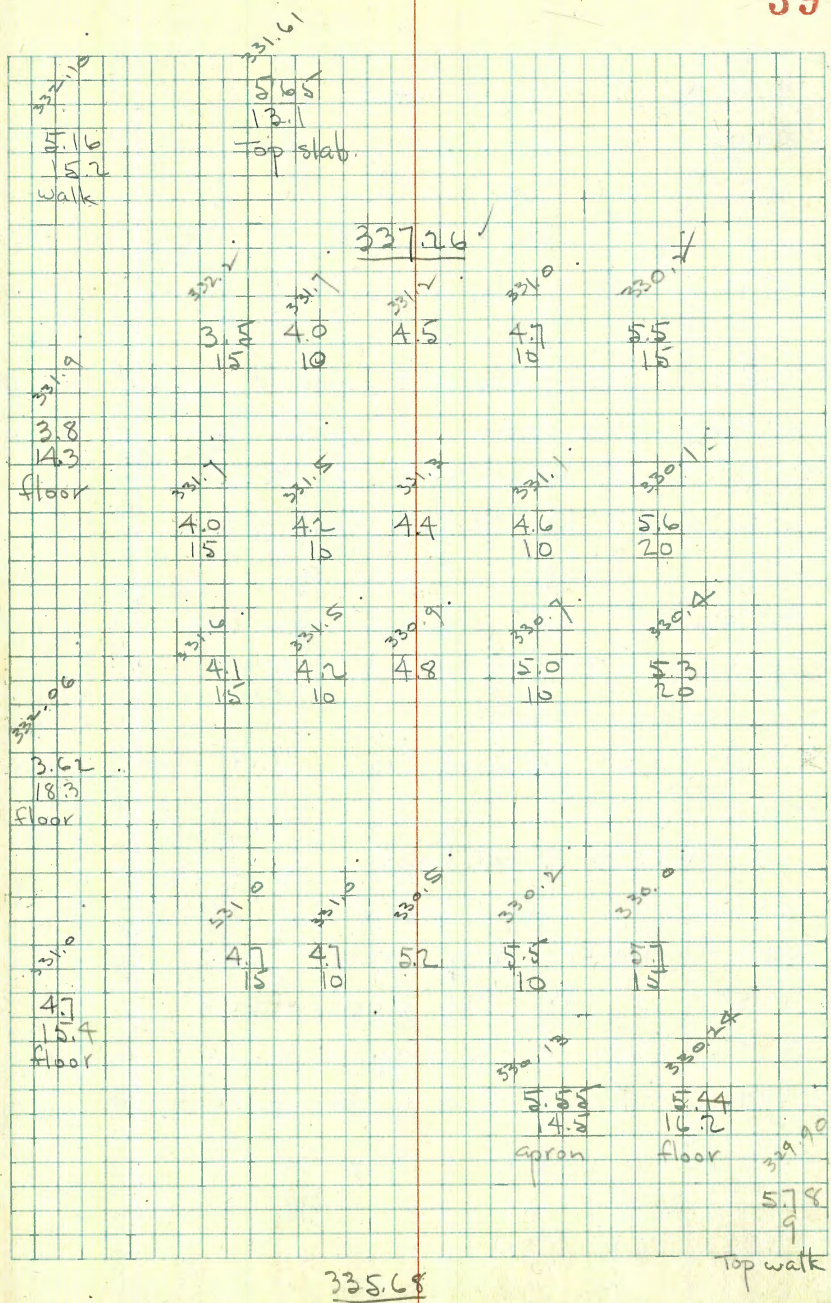
0+53 - 9' Rt. = ± 3' Conc. walk

Lt.

±

Rt

39



4+01 - 10.3 Rt. = end fence

4+00

3+75

3+57 - 10' Rt. = Beg. wire fence

3+50

3+32 - 9.5 Lt. = Wly. P. pole # PA. 3553

3+21 - 10.2 Rt. = \pm 2.5' Conc. walk

3+10

3+01 - 10.6 Rt. = end board fence

2+97 - 10' Lt. = \pm Sing. Gar. - Dirt floor

2+90 - 10' Lt. = end fence

2+75

2+53 - 9.6 Lt. = Beg. Picket fence

2+53 - 10' Rt. = Beg. board fence

2+48 - 36.2 Lt. = \pm Sing. Gar. - Dirt floor

2+42 - 20.8 Rt. = \pm Sing. Gar. - Conc. floor

2+40

2+32 - 10' Rt. = end fence

Lt.

Rt.

40

332.9	332.0	332.1	332.6	332.0	
3.4	3.3	3.2	2.9	2.3	
15	10		10	10	
332.8	332.6	332.2	332.7	332.2	
3.9	3.7	4.0	3.0	3.1	
15	10		10	15	
332.7	332.7	332.2	332.8	332.2	
4.2	4.6	5.1	4.9	4.1	
15	10		6	10	
332.5	332.8	331.7	331.7	331.9	332.9
4.8	5.5	5.6	5.6	5.4	4.9
20	10		10	15	10.2
					walk
331.6					
5.7					
10					
floor					
331.5	331.2	331.8	331.4	331.1	
5.8	6.1	5.9	6.2	6.2	
15	10		10	20	
332.8					
4.9					
36.2					
floor					
331.7	331.2	330.8	330.7	330.6	330.6
5.5	6.1	6.5	6.6	6.7	6.6
15	10		10	20	20.8
					floor
on Conc.					
		337.26			

5+62 - 93 Lt. = end fence
 5+60
 2.5' Conc. walk to along Gar.
 5+54 = 9.6 Lt. = N.E. Cor. slab + beg Ely. of
 5+54 - 10.1 Rt. = end fence
 5+28 - 10.2 Lt. = S.E. Cor. Conc. slab - behind fence
 5+26 - 94 Rt. = Beg. board fence
 5+25
 5+02 - 97 Lt. = Beg. Picket fence
 5+01 - 99 Lt. = Ely 4" Conc. wall - 5' High

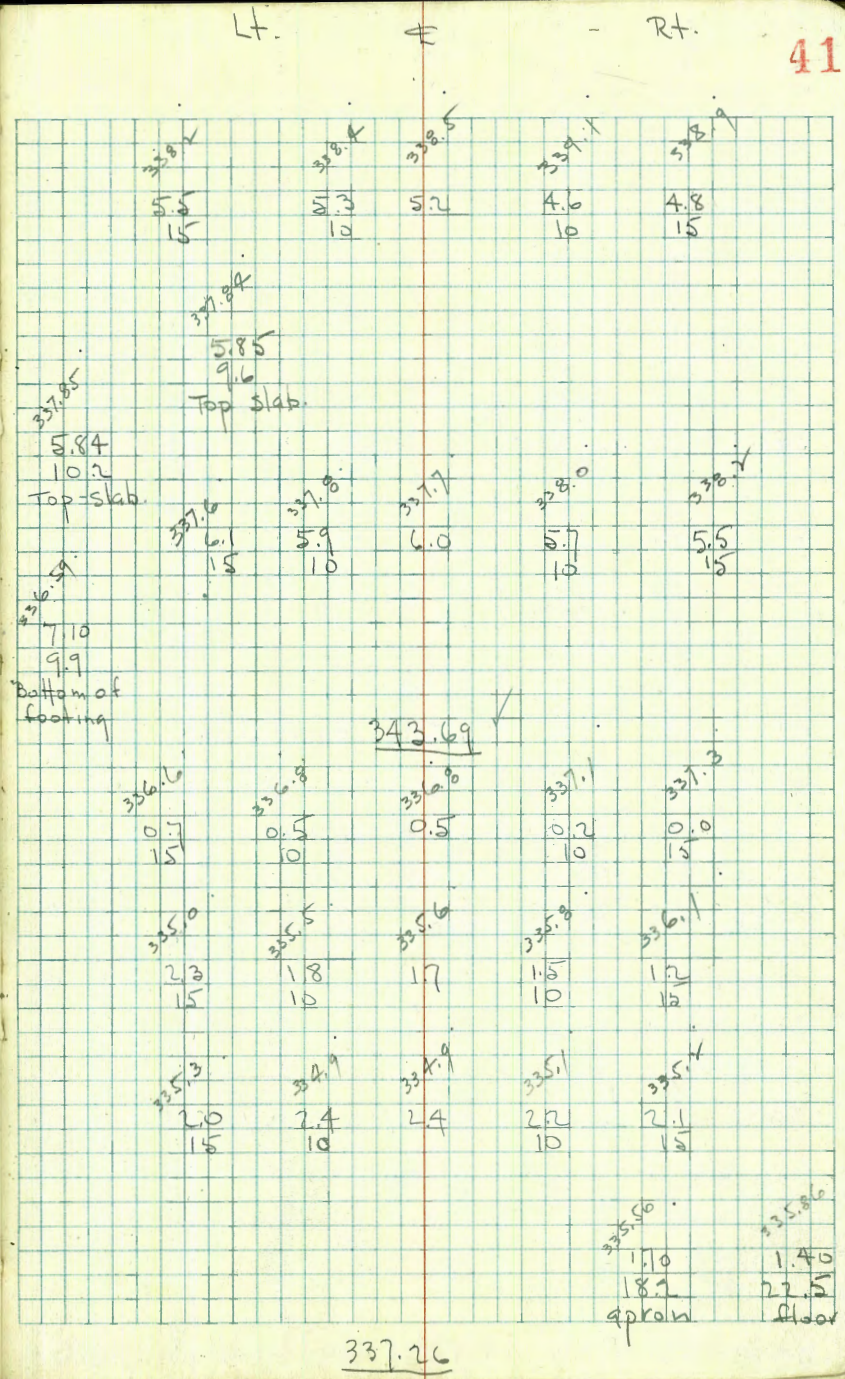
T.P. 7.03 343.69 0.60 336.66

5+00
 4+77 - 93 Lt. = wly. P. pole # P.A. 3575

4+60

4+25

4+11 = ← Sing Gar. on Rt. - Conc. floor apron



check B.M. NW 43rd
+ Dwight.

3.94 339.75 339.77

6+15.34

6+08.34 - 9.6' Rt. = Nly. End walk

6+08.34 - 8.9' Lt. = Cor. Conc. apron

6+02.34 - 9.6' Rt. = Sly. End walk

6+01.34 - S.L. Dwight - No Returns - See
Dwight Sections

+ apron

5+93- 11.6 Lt. = N.E. Cor. Gar. - Opens N. - Conc. floor

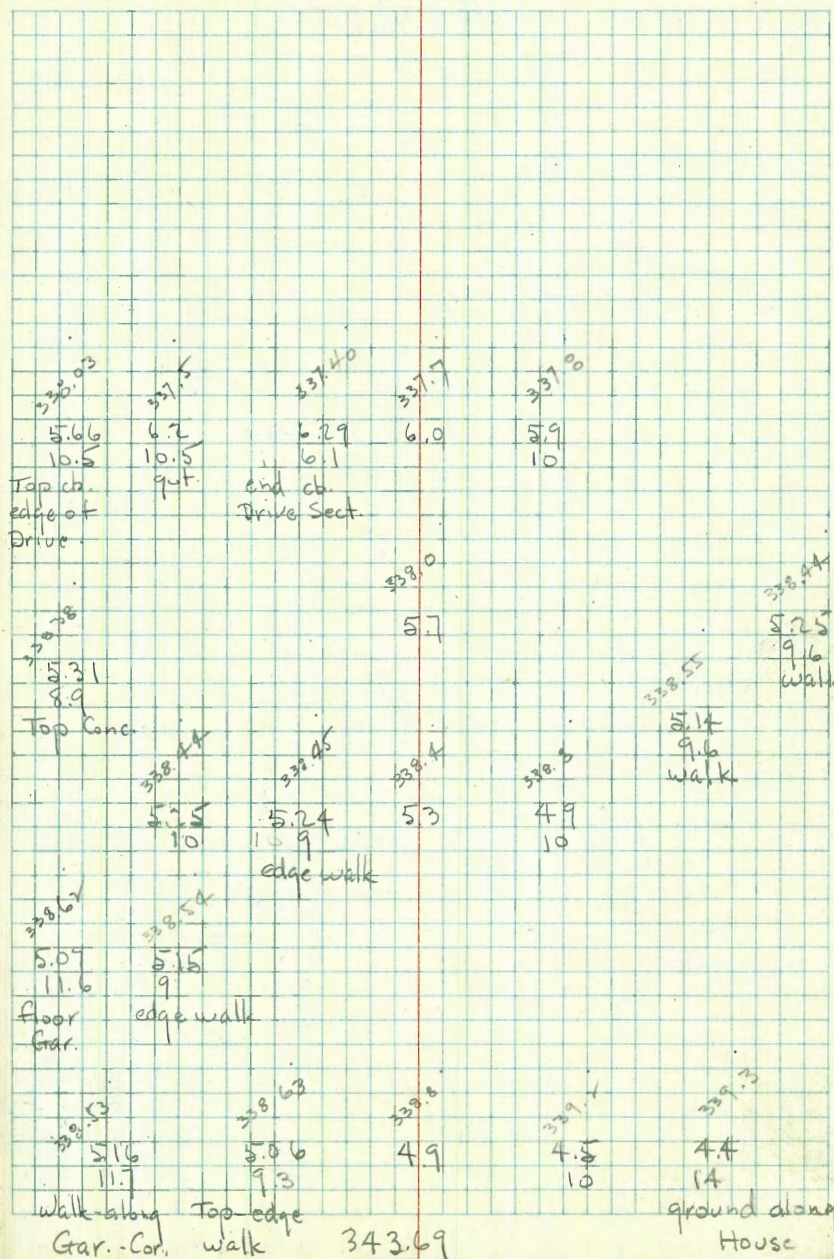
5+75

Lt.

F

Rt.

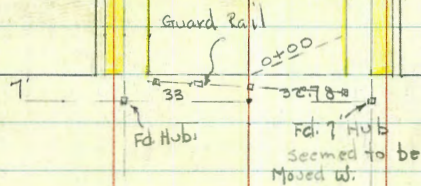
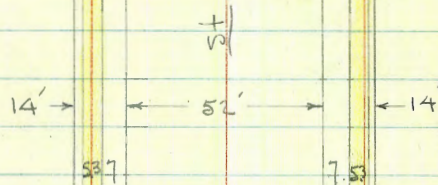
42



X-Sect. 41st
from S.L. Redwood
to N. of Thorn

INDEXED

Indexed
vs B



Redwood

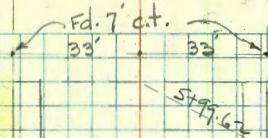
st

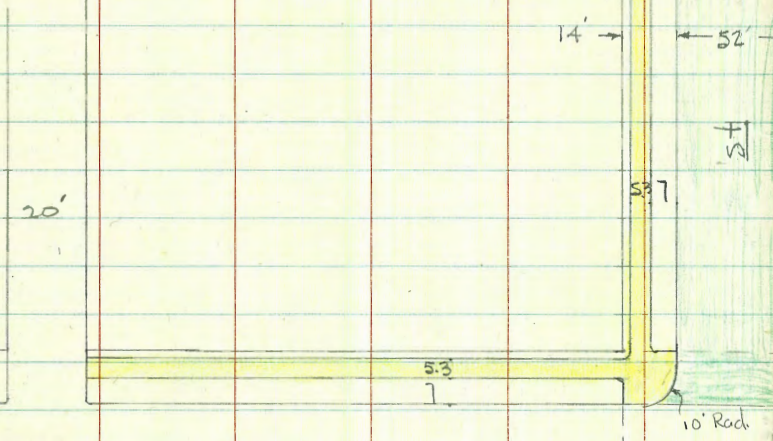
80

Int. - P. 44

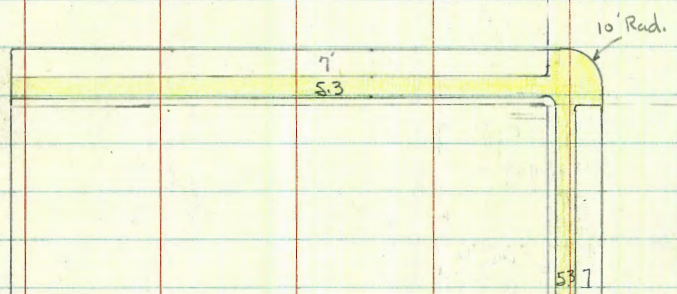
43

Thorn
7

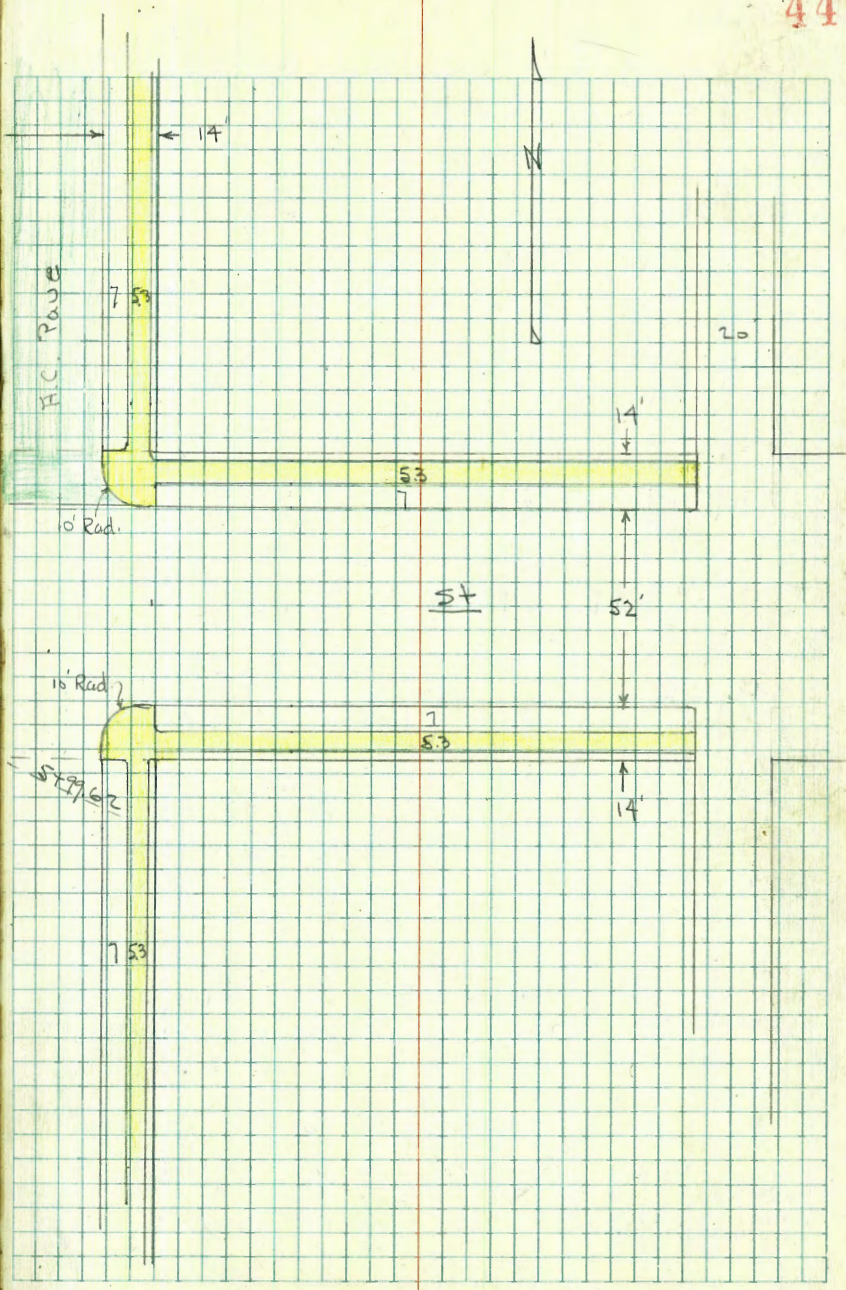




Thorn



41 ±



F.C. PAUSE

ST

587/52

X- Sect. 41st from S.L. Redwood to
N. of Thorn - 80st - 14' cb. s.

1867

11-3-47

W.O. 31470

Osborne
Hardin
Smith
Worrell

0-14 = N. cb.

0-27

T.P. 8.47 293.48 0.53 285.01

0-40 = E

0-66 = S. cb

0-80 = S.L. Redwood - in canyon - not Graded.

0.53 285.54 13.26 285.01

0.11 298.27 13.25 298.16

sw 7th of
T.P. Thorn #125

0.90 311.41 0.78 310.51

B.M. 9.47 311.29

301.82
out of Thorn
at Marlborough

285.7	285.8	286.2	286.0	287.1	287.6	287.7	287.8	288.1	289.9	291.0
148	7.7	7.3	7.5	4.4	5.9	5.8	5.7	5.4	2.6	1.5
60	40	25	26	13		13	26	34	40	50
291.0	296.8	299.2	284.3	286.8	287.6	287.0	288.1	289.0		
22.5	16.7	14.1	7.2	6.7	5.9	4.5	5.4	4.5		
60	40	26	13	67	13	26	40	30		
					293.48 ✓					
284.8	281.8	285.7	281.5	283.7	285.6	286.5	286.8	286.4		
20.7	17.7	9.8	4.0	1.8	0.1	1.0	0.3	1.0		
60	40	26	13		13	26	40	50		
288.1	286.9	283.6	284.2	284.0	286.8	286.4	289.1	286.4		
27.4	26.1	21.9	14.3	11.5	9.1	9.3	6.4	5.3		
60	40	26	13		13	26	40	50		
286.8	286.2	280.9	284.8	287.9	284.7	283.2	286.1	287.0		
29.1	29.3	26.6	20.7	17.6	15.8	12.3	9.4	8.2		
60	40	26	13		13	26	40	50		
					285.54 ✓					

2+00

Ramps

1+77 = \oplus Dr. on lt. cb. not broken - using wood

1+50

1+42 = \oplus 8' Dirt Dr. on lt. - cb broken out.

T.P. 12.89 305.21 116 292.32

1+00

0+50

0+25

0+00 = N.L. Redwood = Beg. cb's + walks

	298.99	298.5	298.8	299.1	298.7	298.3	298.99	46
	6.22	6.7	6.4	6.1	6.5	6.9	6.27	
	26	26	13		13	26	26	
	Top	gut				gut	Top	
	297.76		297.60					
	7.45		7.61					
	33		26					
	walk		Top					
	295.95	295.5	295.8	296.0	295.7	295.4	296.02	
	9.26	9.7	9.4	9.2	9.5	9.8	9.19	
	26	26	13		13	26	26	
	Top	gut				gut	Top	
	296.6	295.1						
	9.59	10.1						
	33	26						
	walk	gut						
				305.21				
	292.95	292.4	292.7	293.1	292.8	292.4	292.75	
	0.55	1.1	0.8	0.4	0.7	1.1	0.53	
	26	26	13		13	26.1	26.1	
	Top	gut				gut	Top	
	290.24	291.97	291.4	291.7	290.0	289.9	290.26	
	3.44	3.51	4.1	3.9	3.5	3.6	3.42	
	33	25.9	25.9	13		13	33	
	walk	Top	gut			gut	Top	walk
	288.6	288.8	288.57	288.4	288.9	288.2	288.01	288.57
	4.84	4.90	5.01	5.1	4.6	4.7	4.6	5.3
	38.3	33	25.9	25.9	13		13	26.1
	walk	Top	gut				gut	Top
	287.1	287.0	286.97	286.8	286.9	286.6	286.93	287.15
	6.4	6.5	6.64	6.49	6.0	6.55	5.6	5.5
	50	46	38.3	33	33	25.9	13	13
	walk	end	walk	Dirt	gut	walk	Dirt	Top
					293.48			cb

3+97.5 - 26 Rt. end cb. at S. side of Dr.

3+50

3+25

T.P. 9.10 213.91 0.40 304.81

New Gar. using wood ramp

3+08 - ± 9' Dirt Dr. on Rt. - cb. not broken

3+06 - ± 9' Conc. Dr. on Lt.

3+00

2+75

but Dr. in to back of cb. - will probably need a Dr.

2+59 = ± 9' Conc. Dr. on Lt. - cb. not broken out

2+54 - ± 6' Conc. Dr. on Rt. (not used.)

2+50

Lt.

Rt. 306.49 47

305.90	305.11	305.5	305.9	305.7	306.0	304.3	305.21
8.01	8.8	8.4	8.0	8.2	9.0	8.19	
25.9	25.9	13		13	26	26	
Top	gut.				gut.	Top	
304.83	304.6	304.9	305.1		305.0	304.3	305.21
8.58	9.3	9.0	8.8		8.9	9.6	8.70
25.9	25.9	13			13	26	26
Top	gut.					gut.	Top
			213.91 ✓				
304.80	304.06				304.74	304.83	
0.41	1.15				0.47	0.38	
33	25.9				26	32	
walk	Dr.				Top	walk	
304.45	304.8	304.1	304.2	304.0	304.6	304.40	
0.76	1.4	1.1	1.0	1.2	1.4	0.75	
25.9	25.9	13		13	26	26	
Top	gut.				gut.	Top	
302.91	302.7	302.9	302.2	302.9	302.5	302.37	
1.89	2.5	2.3	2.0	2.3	2.7	1.89	
25.9	25.9	13		13	26	26	
Top	gut.				gut.	Top	
301.93	301.8	301.7	301.8	301.6	301.4	301.71	301.42
3.28	3.7	3.8	3.4	2.71	2.95	3.3	
26	26	13	34	25.9	26.4	26.4	
Top	gut.			Top	Top	walk	
				at back of cb.	at back of cb.	walk	
				13	13	26	
						Dr.	
					301.2	301.91	
					4.0	3.22	
					26	26	
					gut.	Top	

305.21

4+99.62 = S.L. Thorn - on Rt = Remains of
old abandoned 1' x 5' cb. outlet + 12" C.I. Pipe
see no other Inlets.

5+50

5+08 = \$ 9' Dirt Dr. on Rt - cb. broken out

5+00

4+74 = \$ 8.5 Conc. Dr. on Rt.

4+60 = end poor walk on Lt.

4+54 = \$ 7' Dirt Dr. on Lt. = cb. broken out

4+50

4+39 = \$ 9' Conc. Dr. on Rt.

4+00 = Beg. walk on Lt. Humped up by trees
check

48

Lt.				Rt.			
310.33	309.6	310.0	310.1	309.8	309.4	309.81	
3.58	4.3	3.9	3.8	4.1	4.5	4.10	
25.9	25.9	13		13	26	26	
Top	gut				gut	Top	
309.46	308.8	309.1	309.3	308.9	308.2	309.04	
4.45	5.1	4.8	4.6	5.0	5.6	4.87	
25.9	25.9	3		13	26	26	
Top	gut				gut	Top	
					307.8	306.4	
					6.1	5.40	
					26	33	
					Dr. gut.	walk	
309.51	308.0	308.2	308.4	308.1	307.6	308.24	
5.34	5.9	5.7	5.5	5.8	6.3	5.62	
25.9	25.9	13		13	26	26	
Top	gut				gut	Top	
					307.3	306.94	
					6.60	5.97	
					26	33	
					Dr.	walk	
307.97	307.4	307.2	307.4	307.4	306.8	307.40	
5.94	6.7	6.7	6.5	6.7	7.1	6.5	
33	25.8		13	13	26	26	
walk	Dr.				gut	Top	
307.65	307.33	307.48	307.6	307.4	306.8	307.40	
6.06	6.08	6.23	6.7	6.5	6.7	6.5	
38.3	33	25.8	25.8	13	13	26	
walk	Top		gut			gut	
					306.60	306.15	
					7.15	6.56	
					26	33	
					Dr.	walk	
306.44	306.81	306.72	306.0	306.5	306.0	306.61	
7.7	7.04	7.9	7.9	7.4	7.9	7.24	
34.3	33	25.9	25.9	13	13	33	
walk	Top		gut			walk	
					306.0	306.0	
					gut in	walk	
					Dr.		

31391

0+25

80' N. = N.L. Thorn = 0+00 ahead

66' N. = N. cb. = Beg. edge of Al Paul

53' N.

40' N. = Φ

27' N.

14' N. = S. cb.

Rods on Φ of Returns - 10' Radi

	LT			RT
	311.33	310.75	310.79	310.08
	2.58 26 Top	3.16 26 gut.	3.12	3.83 26 gut
	310.97	310.51	310.44	310.07
	2.94 26 Top	3.39 26 gut	3.49 13	3.84 13
	310.84	310.27	310.23	309.94
	3.07 40 Top	3.9 40 gut.	3.64 26	3.71 13
	310.0	310.2	310.1	310.0
	3.07 40 Top	3.9 26	3.7 13	3.8 13
	310.0	310.1	310.1	309.9
	3.9 40	3.8 26	3.7 13	3.8 13
	310.36	310.1	310.0	309.7
	3.55 40 Top	4.2 40 gut	4.1 26	3.7 13
	309.9	310.36	309.6	309.1
	4.0 40 gut	3.55 Top SW Ret.	4.2 26	4.8 40 gut
				309.19
				309.5
				309.17
				4.12 Top SE Ret
				4.4 gut

Rods around Returns - N.W. + N.E. Cor.

Thorn + 41st

N.W. Ret. 24' around - 4 parts - 6' each

Req. - W. end - W.L. 41 st	3.07	310.84	T = Top
	3.9		g = gut.
6' E = Req. Pauc in Gutter	3.09		T
	3.81		g
" = Φ	3.07	310.84	T
	3.56		g
"	3.01		T
	3.45		g
6' = end = N.L. Thorn	2.94	310.97	T
	3.39	310.52	g

T.P.

3.40

310.51

3 w. 1' ct.
P. 45

1 + 25 = end.

0 + 75

N.E. Ret. = 24' around - 4 - 6' each

Req. - N. end = N.L. Thorn	3.70	310.21	T
	4.20	310.71	g
4 5'	3.66		T
	4.20		g
6 = Φ	3.67	310.24	T
	4.24		g
Φ + 4' = end pauc in gut.	3.70		T
	4.52		g
6 = 3/4	3.70		T
	4.5		g
6' = end = E.L. 41 st	2.68	310.23	T
	4.6		g

312.06

0.95

26

312.04

1.86

26

Top

312.08

1.43

26

312.50

2.36

26

gut.

312.55

1.36

312.55

2.26

26

312.03

1.88

26

gut.

312.04

2.97

26

gut.

312.55

1.26

26

Top

312.43

2.49

26

Top

X-Section Thorn - from E.L. of 20' Alley
W. of 41st - to W.L. of 20' Alley E.

0+40

INDEXED

0+00 = E.L. 41st

Int. - see P. 49.

1+40 = W.L. 41st

1+00

0+50

0+00 = 140' W. of W.L. 41st = E.L. 20' Alley

3.93 214.44

3 Tot.
210.51 41st

Indexed
J.B.

Lt = N.

#

Rt. - S.

51

309.12 5.32 26 Top	309.12 6.1 26 gut.	309.12 5.8 13	309.12 5.7	309.12 6.1 13	309.12 6.4 26 gut.	309.12 5.14 26 Top					
310.73 4.21 26 Top	309.93 5.1 26 gut.	309.5 4.9 13	309.7 4.7	309.4 5.0 13	309.1 5.3 gut.	309.13 4.66 Top					
310.33 3.61 26 Top	310 4.4 26 gut.	309.9 4.5 13	309.9 4.5	309.8 4.6 13	309.6 4.8 26 gut.	310.36 4.08 26 Top					
310.19 4.25 25.9 Top	309.4 5.0 25.9 gut.	309.4 5.0 13	309.2 5.2	309.2 5.2 13	309.8 5.6 26 gut.	309.6 4.9 26 Top					
309.36 5.18 26 Top	308.5 5.9 26 gut.	308.6 5.8 13	308.8 5.6	308.6 5.9 13	308.1 6.3 25.9 gut.	308.10 5.65 25.9 Top					
308.67 5.77 40 Top	308.46 5.98 26 Top	307.1 6.5 26 gut.	308.2 6.2 13	308.2 6.2	307.9 6.5 13	307.4 7.0 26 Top	307.34 4.58 26 Top	308.07 6.37 40 Top			
Tot. gut and Ret.		2 Rad.		gut.		2 Rad. Ret.		Top cb gut.			
3			3			3			3		
210.51			214.44			214.44			214.44		

check starting B.M.

12.61 201.83 -201.82

1+40 = W.L. 20 Alley = end of cb. + walks.

0+90

0+70 = Brk. in cb. on Lt.

14.

#

Rt.

52

188	8.12	9.1	8.8	8.5	8.8	9.1	8.64	8.29
40	26	26	13		13	26	26	40
Top-end end Ret.	Top 2 Rad.	gut.				gut.	Top 2 Rad. Ret.	Top-end Ret/gut
168	7.6	7.3	7.0	7.4	8.0	7.7	7.23	
26	26	13		13	26	26		
Top	gut.				gut	Top		
18								
26								
Top cb.								

214.44

Cross Sec. for Brunner + Josephine Sts.

From Alley in Blk C. Silver Terrace to Linda Vista Rd.

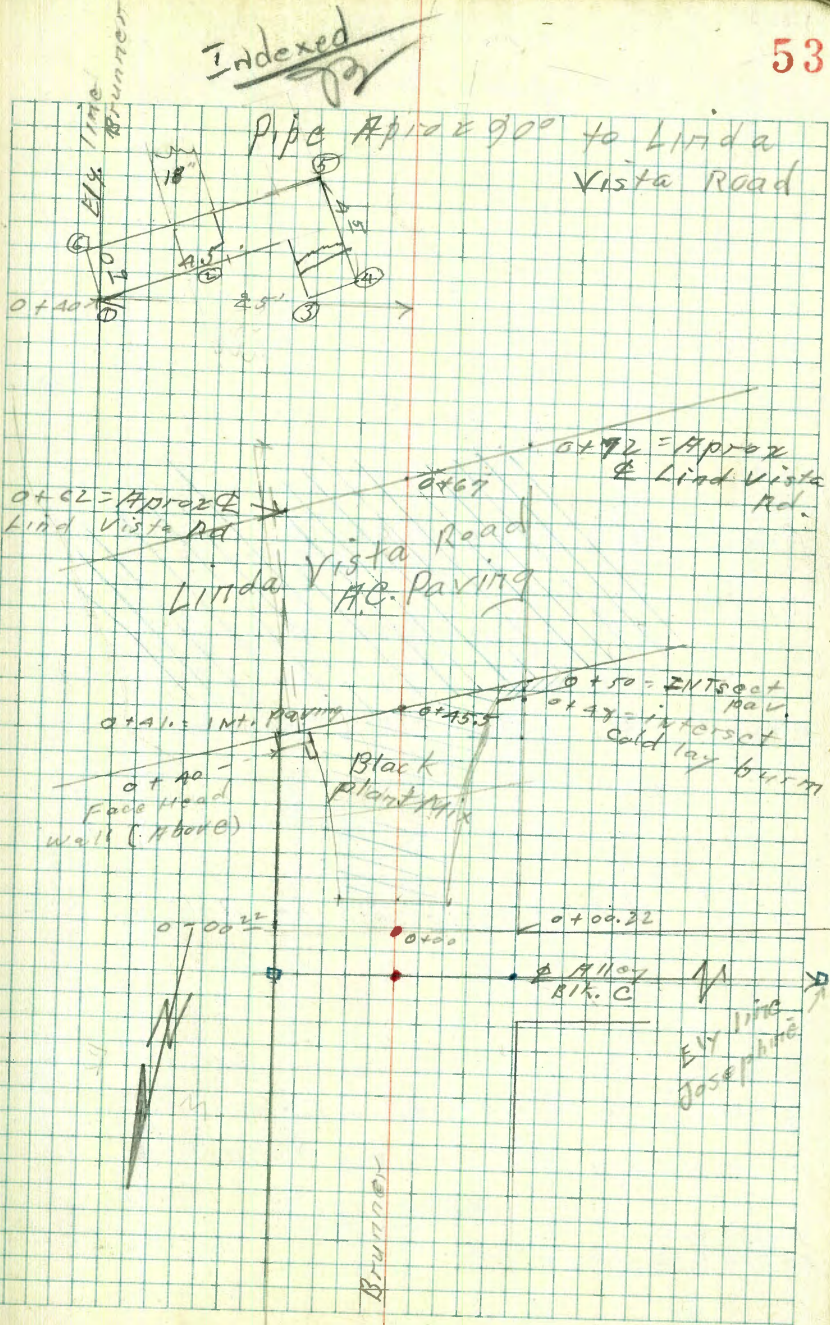
12-15-47
W.O. 25001

Sommermeier
vs. Moore
E. Sherman

INDEXED

Reference = T.P. #1
F.B. 574
FB 1630

Indexed



Brunner St.
N. of Linda Vista Road

0+18

0+09

0+03 ^{6 ft. 2} Edge of pav.
→ Approx start cold lay paving

0+00²² = 90° to Corr on Rt.

0+00 = Φ Brunner & S. Line Alley Bk.c.

0-00²² = 90° to line on Lt.

Sections at 90° to Base line:

T.P.	12.35	147.30	7.53	134.95	
Φ 4465 P. 52					
FB 574 P. 52	12.16	142.48	—	130.32	B.M.

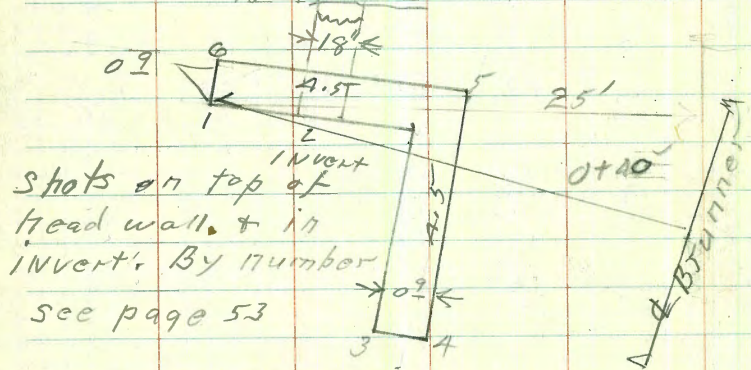
140.7	140.3	140.6	140.6	140.6	140.6	140.6	140.6	140.6	140.6
2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6	2.6
141.1	141.5	141.2	141.1	141.1	141.1	141.1	141.1	141.1	141.1
5.6	5.1	5.3	5.3	5.3	5.3	5.3	5.3	5.3	5.3
141.7	142.2	142.0	142.0	142.0	142.0	142.0	142.0	142.0	142.0
3.6	3.1	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3
144.5	144.6	142.6	142.3	142.3	142.3	142.3	142.3	142.3	142.3
3.0	2.7	4.7	5.1	5.1	5.1	5.1	5.1	5.1	5.1
144.4	144.7	142.9	142.3	142.3	142.3	142.3	142.3	142.3	142.3
2.0	2.6	4.6	5.0	5.0	5.0	5.0	5.0	5.0	5.0
144.4	144.7	142.9	142.3	142.3	142.3	142.3	142.3	142.3	142.3
2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9	2.9
147.30	147.30	147.30	147.30	147.30	147.30	147.30	147.30	147.30	147.30

0+45 Int. Linda Vista Pav.

0+41 25' Lt. Int. Linda Vista Pav.

N.E. Cor.
Hd. wall
T.P.

5175 144.06 8.99 138.31



0+32 20' Lt. start oiled burn

0+26

147.30

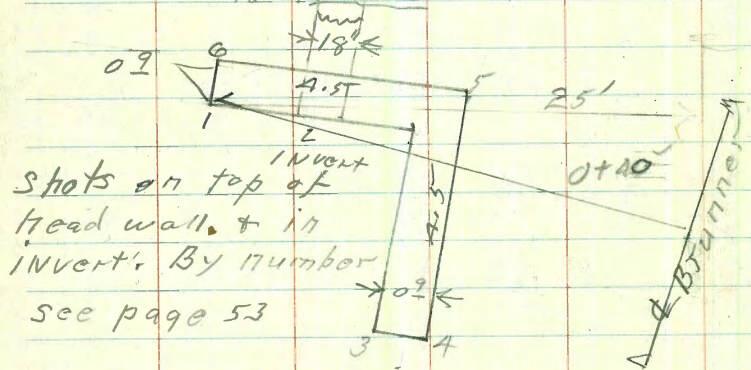
138.31	138.31	138.31	138.31	138.31	138.31	138.31
8.99	12.60	9.39	9.30	9.25	9.99	
1	2	3	4	5	6	
140.3	138.9	137.5	138.0	137.7	138.1	137.5
7.0	8.4	8.8	9.3	9.6	9.2	9.8
25	20	18	18	18	11	25
	Top Burn	Par		Par	Burn	
140.5	138.9	138.3	138.3	138.6	137.9	137.2
6.8	8.9	9.0	9.0	8.7	9.4	10.1
25	16	16	16	16	11	25
	Edge		Edge	Par	Par	
			147.30			

0+45 Int. Linda Vista Pav.

0+41 25' Lt. Int. Linda Vista Pav.

N.E. Cor.
Hd. wall
T.P.

5175 144.06 8.99 138.31



0+32 20' Lt. start oiled burn

0+26

147.30

138.31	138.31	138.31	138.31	138.31	138.31	138.31
8.99	12.60	9.39	9.30	9.25	9.99	
1	2	3	4	5	6	
140.3	138.9	137.5	138.0	137.7	138.1	137.5
7.0	8.4	8.8	9.3	9.6	9.2	9.8
25	20	18	18	18	11	25
	Top Burn	Par		Par	Burn	
140.5	138.9	138.3	138.3	138.6	137.9	137.2
6.8	8.9	9.0	9.0	8.7	9.4	10.1
25	16	16	16	16	11	25
	Edge		Edge	Par	Par	
			147.30			

T.P. 11.82 108.87 Temp. B.M.

T.P. 1.66 120.59 13.08 119.03

T.P. 1.08 132.11 13.03 ^{131.03}
~~133.03~~

0+45.

Vista road, taken on Δ off.
paving to show grade of Linda
This section along edge of state

142.8	139.7	137.1	136.1	140.8
$\frac{1.3}{100}$	$\frac{1.4}{50}$	7.0	$\frac{10.1}{50}$	$\frac{13.3}{100}$

0+50 = 25' Rt. = Int. Linda Vista Pav.

138.6	137.1	135.6
$\frac{5.5}{25}$	7.0	$\frac{8.6}{25}$

0+48 = 25' Rt. = Int. Bruner.

136.6	137.1	135.9
$\frac{3.6}{25}$	7.0	$\frac{8.2}{25}$
		Pav
		Bruner

144.06

144.06

JOSEPHINE St.

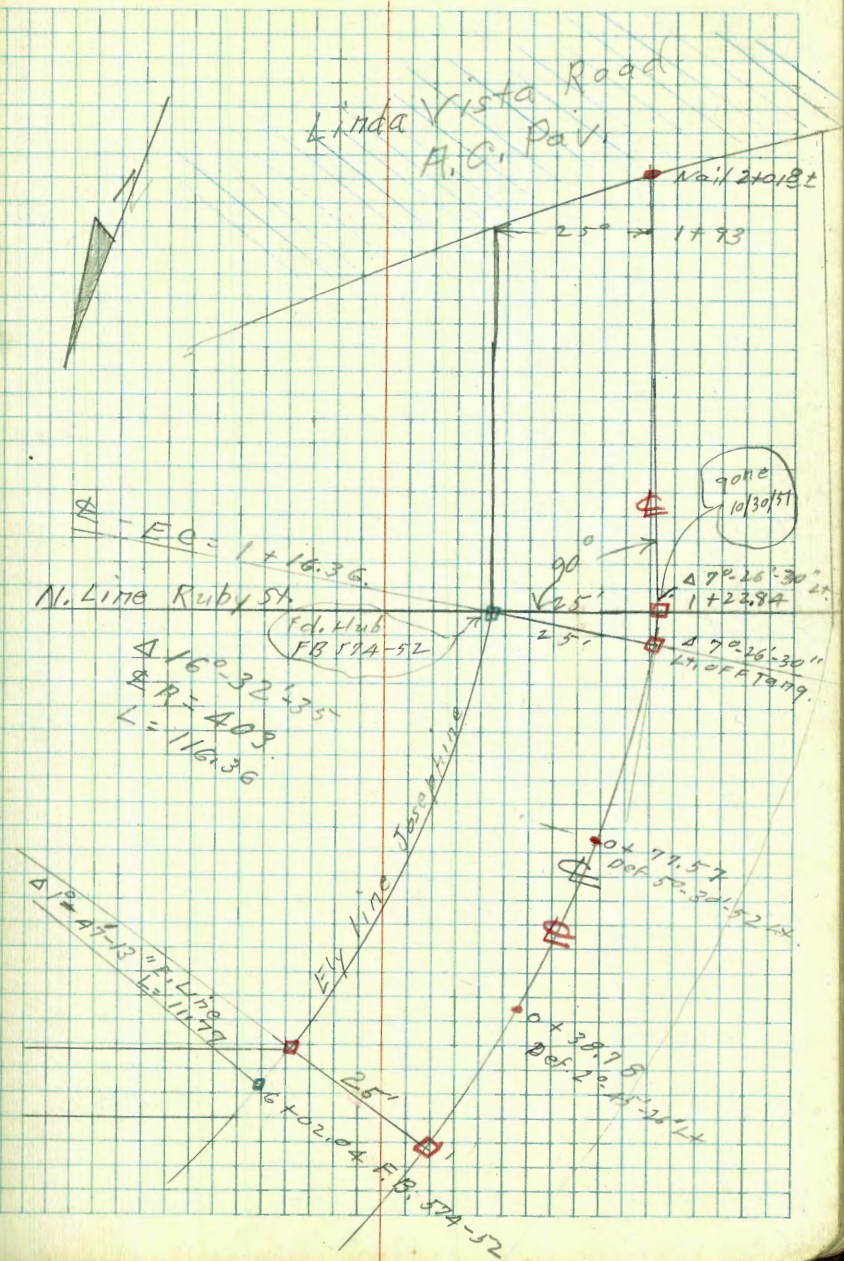
From Alley-Bk. "c" Silver Terrace
Linda Vista road

12-15-47

V.H.O. 25001

Sommarmeyer
W. Moore
E. Sherman

Base line run on
403' Rad. (25' off E. line) on
curve. W. line Josephine is
not tied in.



1+50

Sec. 90° to Fwd Tang.

$$1+22.84 = \Delta 7^{\circ} 26' - 30'' \text{ Lt.}$$

$$1+16.36 = \text{E.C. } 2 \times 2 \text{ also } = \Delta 7^{\circ} 26' - 30'' \text{ Lt.}$$

T.P. 0.07 117.78 13.08 117.710+77⁵⁶0+38⁷⁸ 62' Rt. Bottom Canyon.0+00 45' Rt. - Bottom Canyon
Radial sectionsB.M. Page
54

0.A1 - 130.79 — 130.32

101.0	109.5	107.5	98.6	96.8
$\frac{6.8}{25}$	$\frac{6.0}{25}$	10.3	$\frac{13.2}{25}$	$\frac{13.0}{25}$
114.3	109.2	107.8	104.2	102.1
$\frac{3.5}{25}$	8.6	$\frac{10.0}{6}$	$\frac{13.6}{11}$	$\frac{15.7}{25}$
117.78	110.35	108.5	104.3	102.7
$\frac{3.5}{25}$	7.43	9.3	$\frac{13.5}{7.4}$	$\frac{15.1}{25}$
122.6	113.8	108.1	101.7	99.7
$\frac{8.2}{40}$	10.7	17.0	$\frac{22.1}{25}$	51.1
156.2	123.1	118.0	112.9	108.4
$\frac{6.6}{4}$	$\frac{6.7}{25}$	$\frac{6.9}{20}$	12.8	$\frac{17.9}{20}$
130.9	128.7	125.56	116.8	115.5
$\frac{10.1}{40}$	$\frac{2.1}{25}$	7.23	$\frac{14.0}{25}$	$\frac{15.3}{20}$
130.79	130.79	130.79	130.79	130.79

130.79

Temp. B.M. Page 56 (108.87) 0.51 108.86

Vista road paving.

2+01⁸ taken along edge of Linda

Slope for Linda Vista Road Fill.
88' At. - Bottom Canyon Also top of Pav.

2+01⁸ = Int. Edge of Linda Vista Road.

1+93

1+91

1+83

T.P. 0.51 109.37 8.92 108.86 Temp. B.M. P. 56
check temp. B.M. 117.78

105.0										
102.1										
99.1										
96.3										
	105.0									
	102.1									
	99.1									
	96.3									
	100.6									
	100.0									
	102.8									
	102.6									
	96.8									
	93.4									
	76.9									
	73.7									
	8.8									
	9.4									
	6.6									
	100.8									
	100.3									
	100.7									
	103.6									
	102.6									
	97.4									
	94.6									
	87									
	8.6									
	9.1									
	8.7									
	5.8									
	6.8									
	12.0									
	14.8									
	103.1									
	106.9									
	103.7									
	98.0									
	99.7									
	6.3									
	8.6									
	2.5									
	2.5									
	5.8									
	11.4									
	14.5									
	109.37									

Edge. L.V. Road. Pav

Edge Linda Vista Rd. Pav.

Top of Canyon

Bottom Canyon

Top of Canyon

Walker
Becker
Williams
3-11-48

Location - Proposed Culvert East
Blk 457 - West of Raymond Way
and North of Torrance St

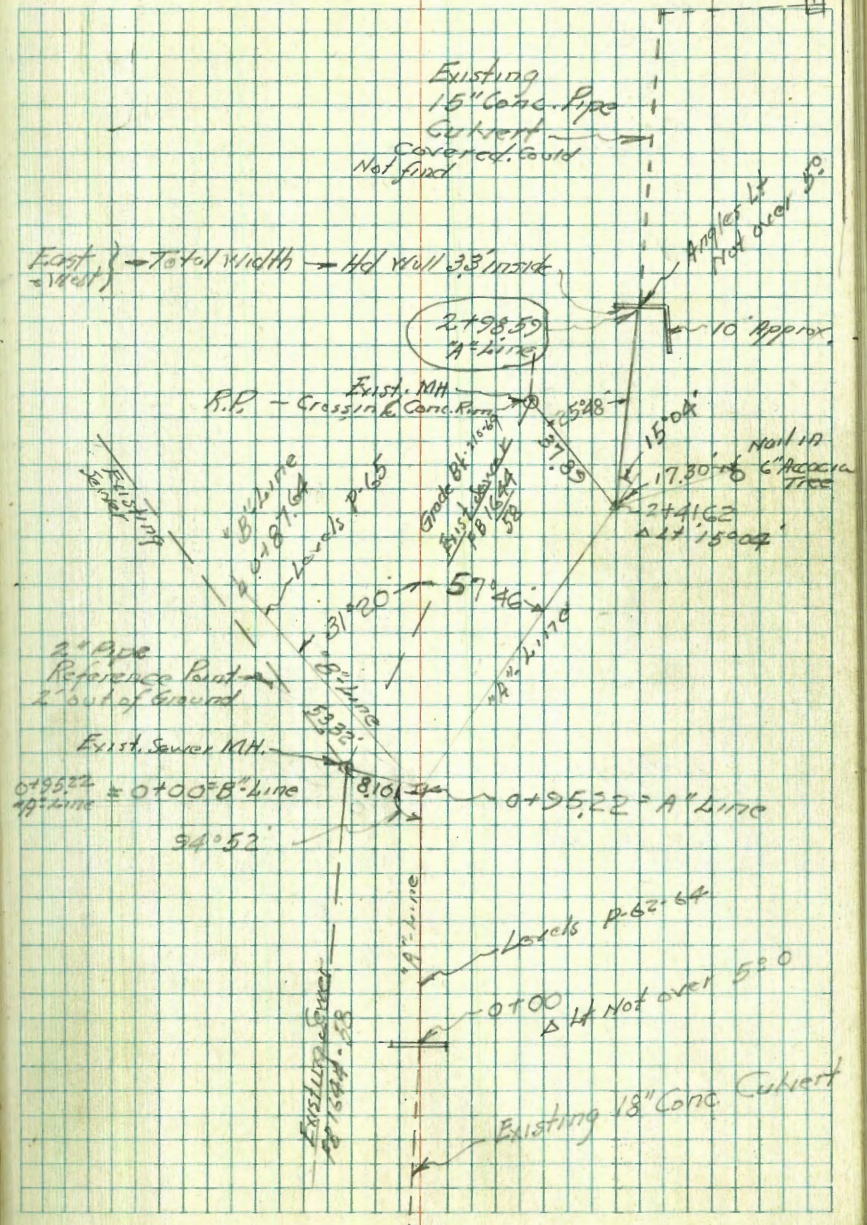
Levels - P. 63-65

~~Indexed~~
PB

INDEXED

0+95.22 = Δ R# 57°46'

0+00 = NLY Edge Hd. Wall - North end Pipe



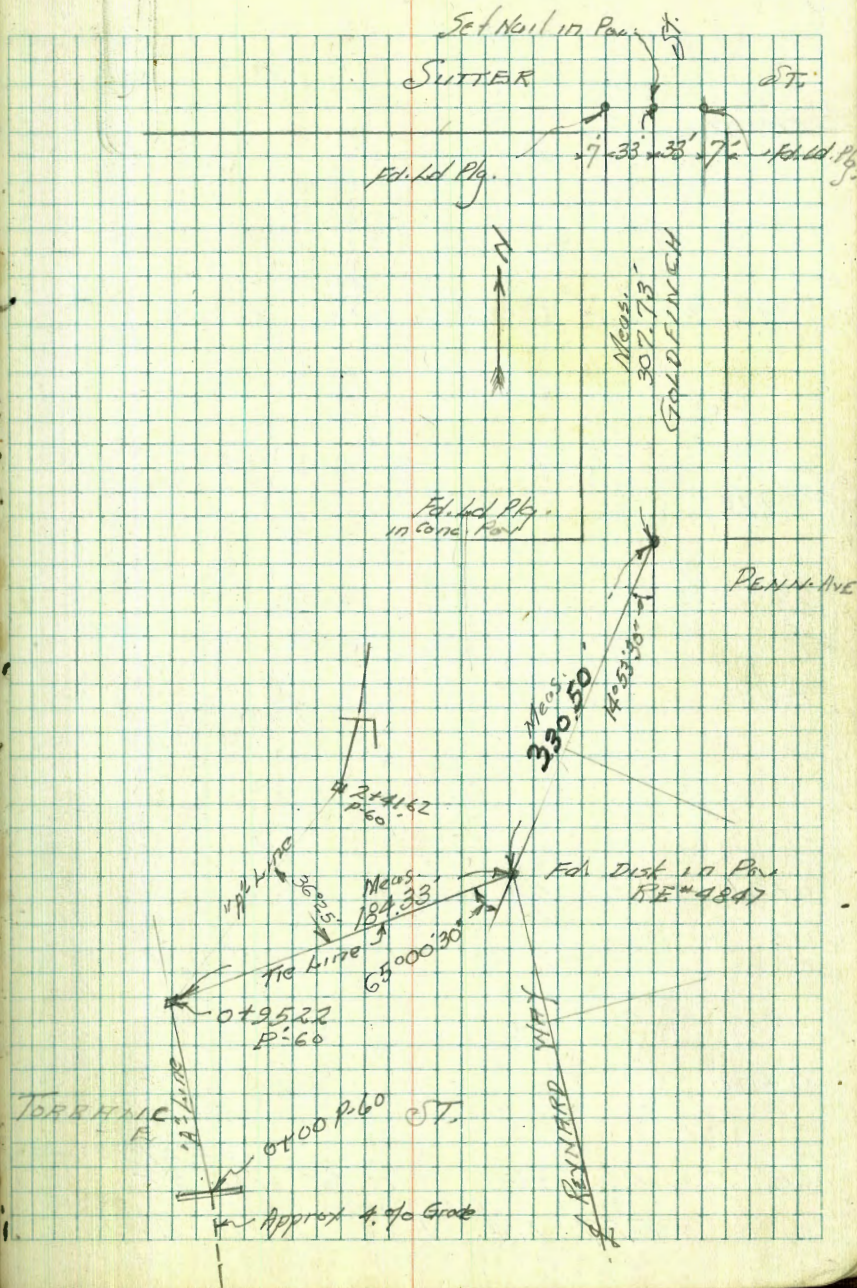
Walker
Decker
Williams
5-11-48

Location Proposed Culvert Ext.
Blk 457 - West Raymond Way
and North of Torrance St
Ties

Cont. from P. 60

180
63
115

(Note from 0+00 to 0+36
Culvert Ext. Grades in Grd Book 233
5)
4-9-48



Levels Proposed Culvert Est.
 "A" Line
 Location P-60

Station

0+95.22 - 2 ft 57°46' See on Biscator

0+75

0+50

0+21 This section on Natural Ground

0+00

chk. Flow Line MH

5.87 174.91

10.66

164.27 to 1644
 164.251
 59

169.04

Lt

R

Rt

62

172.3	171.1	167.8	167.7	168.7	170.5	171.7
5.6	5.3	6.0	6.2	9.4	9.7	2.7
38	14	on MH 6	8	15	24	

172.3	171.1	167.8	167.7	168.7	170.5	171.7
1.6	3.8	7.1	7.2	9.7	9.2	
31	25	10		8	15	

172.4	168.9	166.9	167	168.6	169.6	171.5
2.5	6.0	8.0	8.2	6.3	5.3	3.4
30	23	16	8		7	15

170.8	168.2	168.0	168.2	170.1
4.1	9.7	9.9	8.7	4.3
30	14	10		15

178.9	178.9	162.4	162.09	164.54	169.6	174.8	175.8
4.0	4.0	11.5	12.82	14.89	5.3	7.09	7.02
30	31	5	Flowline	5	8	17	2.5
on MH	Top Fill	Top		on MH	on MH	Top Fill	on MH

174.91

B.M. Run MH 0+00 FB 1644 P. 59

Station

2+57

2+55

2+50

TP 7.83 190.50 0.89 182.67

2+41.62 Δ 150.07 Lt Sec. Bisector

2+00

1+50

TP 11.71 183.56 3.06 171.85

1+25

174.91

180.4

101
17.0 Feb

9.0 181.5

184.3 182.4 181.5 178.8 181.5 183.9
52 81 90 117 20 66
15 10 3 11 15
D.H.B.

190.50 ↓

181.9 180.2 177.5 174.5 174.5 184.6
17 5.8 6.8 5.1 4.3 7.0
5 5 0 8 15
D.H.B.

179.7 177.2 176.5 175.6 175.2 178.0 180.9
8.9 6.8 8.1 8.0 7.9 5.6 2.7
17 5 4 5 5 7 15

172.0 174.7 173.8 171.8 171.6 173.0 174.7 177.7
6.6 8.9 10.1 11.8 12.0 10.6 8.9 5.9
25 5 6 3 4 4 10 20

183.56 ↓

174.5 172.3 171.4 170.1 170.0 171.9 174.3
0.4 2.6 3.6 4.8 4.9 3.3 0.6
25 14 2 5 5 7 18
174.91 *

chk. Starting 8 AM / 15.00 ⁰⁰¹ 169.04 / 169.05 /
 TP. 1.38 184.05 7.83 182.67

2+98.59 = Flow 15" Culvert

2+91

2+88.6

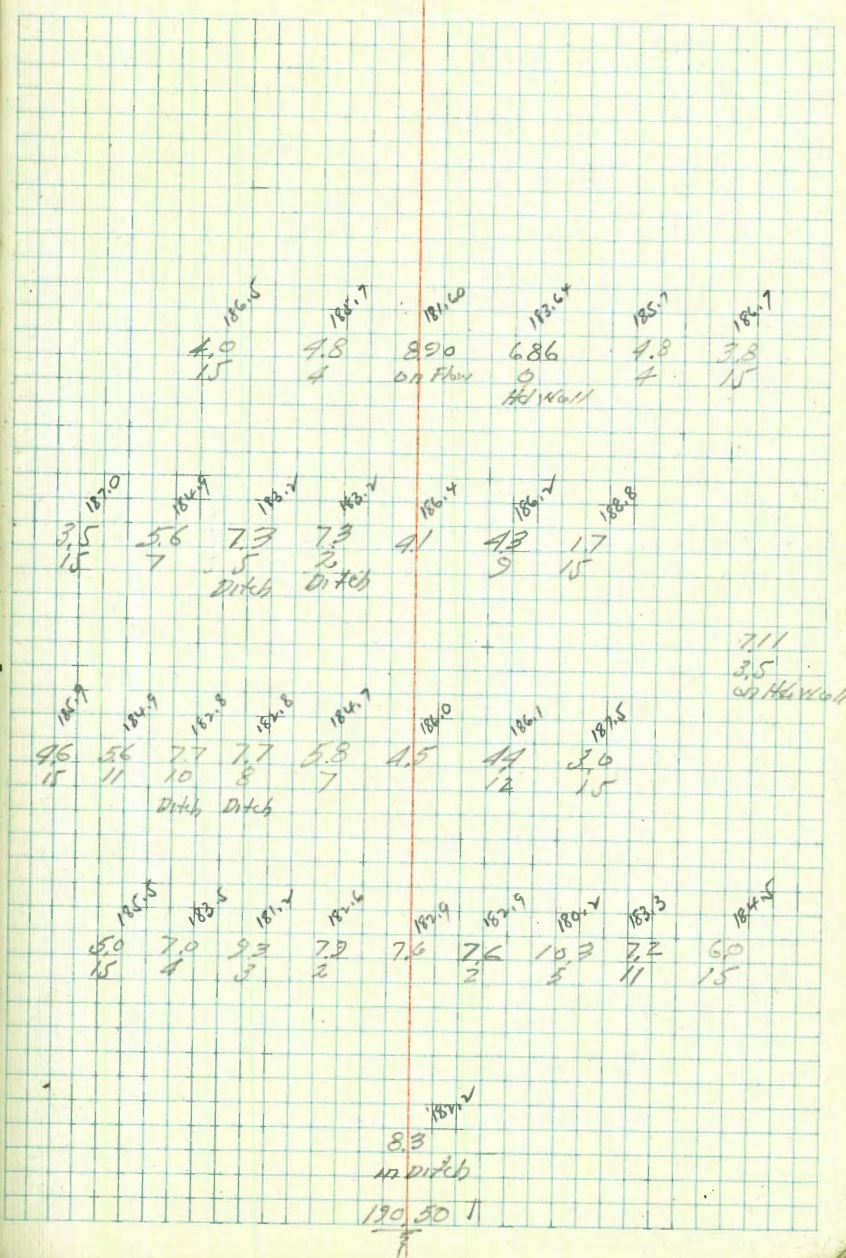
2+86 = 16" Accacia 3' Ht

2+73 = 14" Accacia leaning 45° on line
no good

2+66

2+61

190.50



Levels - "B" Line
 Proposed Culvert
 Location P-60

24

2

57.

65

0+87 - End

177.3	176.0	174.2	174.2	175.0	176.7
1.8	2.9	4.7	4.9	3.9	2.2
15	8	6	Ditch	10	15

0+50

174.5	173.2	170.6	169.7	171.1	172.9
4.4	5.7	8.3	9.2	7.8	5.0
13	9	5	Ditch	1	15

0+25

172.5	170.3	170.0	168.4	169.3	171.8
6.4	8.6	8.9	10.3	9.6	7.1
15	6	2	Ditch	3	15

0+00 = 0+95.22 on "A" Line

169.5	168.8	169.0
9.4	10.1	9.9
15		15

9.84

178.88

162.04

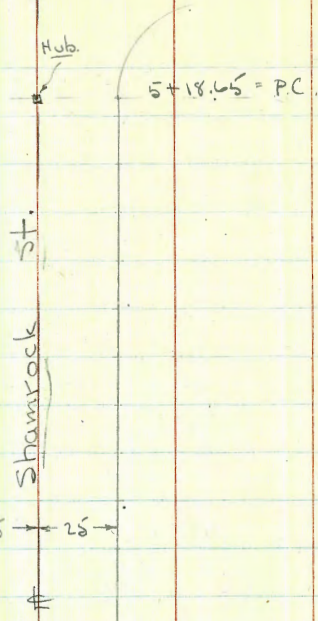
B.M. Rim MH P-62

178.88

PC 5+49.26

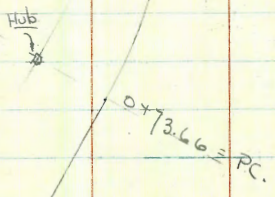
Sycamore Dr

INDEXED

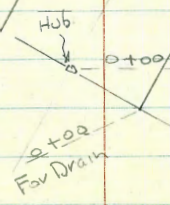


$\Delta = 20^{\circ} 33'$
 $R = 125$
 $L = 64.47$

1+38.13 = E.C.



Stand Par.
 S.outh



Prop. Drain along Sub. line

X-Section Shamrock - from Sub. line
 to Sycamore Dr. - 50 ft - 10' cbs.
 Rough Graded - for ties - B 1748 - P. 45
 Also Sycamore Sections - 1748 - 56

2171
 W.O. 25001

5-25-48
 Osborn
 Hardin
 Worrell
 Rorer

INDEXED
 MAY 26 1948

X-Sect. Shamrock - 50' st. 10' cbs.
 Rough Graded - for Grade est.

0+98 - 39.8' Rt. - \pm Sing. Gar. in House - under Const.

0+73.66 = P.C. - 42.9 Lt. - slp. of New House Conc. found.

0+50

0+45 - \pm Sing. Gar. on Lt. - Conc. floor \pm apron r.s. wide

0+25

0+04 - 16.6 Lt. - \pm P. pole # 4105

0+00 = 2L. Lexington Park.

0-17.2 - 30.4 Rt. - \pm F.H.

0-20

B.M. 0.56 264.31 7.66 263.75
 2.27 271.41 269.14

spt. in Pole
 sycamore &
 shamrock.
 744-57

Lt. - W.

\pm

Rt. - E.

67

5.4
 39.8
 ground

414
 39.8 = Top
 conc. found

5.78 42.9 floor house	8.0 42.9	6.7 25	6.2 15	6.0	6.2 15	5.9 25	4.0 35
--------------------------------	-------------	-----------	-----------	-----	-----------	-----------	-----------

7.8 35	8.2 25	7.8 15	7.0	7.1 15	6.7 25	6.8 35
-----------	-----------	-----------	-----	-----------	-----------	-----------

7.49 40.6 floor	7.56 25.6 = apron
-----------------------	----------------------

9.4 35	8.8 25	8.3 15	7.8	7.9 15	7.6 25	8.7 35
-----------	-----------	-----------	-----	-----------	-----------	-----------

11.2 25	10.3 25	9.8 15	9.6	9.4 15	9.1 25	9.3 35
------------	------------	-----------	-----	-----------	-----------	-----------

12.9 50	10.6 25	10.1 15	10.2	10.3 15	10.1 25	13.9 50
------------	------------	------------	------	------------	------------	------------

264.31

Lt.

+

Rt

4+00

5.4	5.5	5.7	5.5	4.9	4.9	4.7
3.5	2.5	1.5		1.5	2.5	3.5

3+72.5 - 22' Lt. - 2 P. pole # 2502

- 3+50

6.3	6.3	6.3	6.1	5.9	6.1	6.0
3.5	2.5	1.5		1.5	2.5	3.5

3+38.8 - 04' Lt. - Sewer MH 6.06 on Rim

3+00

8.0	7.9	7.7	7.4	7.3	7.3	7.4
3.5	2.5	1.5		1.5	2.5	3.5

2+50

9.0	8.9	8.5	8.3	8.8	8.3	8.6	9.0
3.5	2.5	1.5		1.0	1.5	2.5	3.5

2+00

10.7	10.3	9.9	10.0	10.3	9.6	9.7	10.2
3.5	2.5	1.5		1.0	1.5	2.5	3.5

I.P. 10.18 270.09 4.40 259.91

270.09

1+70

5.6	5.3	4.8	4.6	5.0	4.6	4.7	4.8
3.5	2.5	1.5		1.0	1.5	2.5	3.5

1+38.13 = F.C.

6.3	5.5	5.3	5.1	4.6	4.7	4.5
3.5	2.5	1.5		1.5	2.5	3.5

1+00

7.2	6.5	6.1	5.3	4.9	4.9	5.0
4.8	2.5	1.5		1.5	2.5	3.5

Sect. taken Radially

along
House

264.31

check starting B.M. 237 269.14 269.14
 T.P. 4.59 271.51 3.17 266.92
 See 1748-56-59 for Int.

5+49.36 = P.C. Prop. Curve on Lt. = end.

5+33-24.7 Lt. = 3.6 Conc Walk

5+18.65 = P.C. Prop. curve on Rt.
 5+08-17 Lt. = 4 Pole # J.P. 2548

5+00

4+68-11.2 Rt. = end Picket fence + 4" Conc wall
 4+53.5-24.9 Lt. = 3' Conc walk

4+50

4+43-11.6 Rt. = Beg. Picket fence

4+36-10.4 Rt. = 8' Conc Dr. - 4' E. then 2-2'

4+28.3-12' Rt. = Sly of w. end 4" Conc wall
 Picket fence on top.

Lt. # Rt.

69

3.5	3.4	3.1	3.2	3.3	3.1	3.0
3.5	2.5	1.5		1.5	2.5	3.5

2.91
 4.0
 at Porch

2.91
 24.7 = walk

3.8	3.3	3.2	3.5	3.1	3.0	3.1
3.5	2.5	1.5		1.5	2.5	3.5

4.0	3.9	3.7	3.8	3.8	3.3	3.4	3.3
3.5	2.5	1.5		1.0	1.5	2.5	3.5

4.13	4.28	3.9	3.58
3.7	24.9 = walk	11.2	11.2
at Porch		ground	Top wall
			Top wall

4.2	4.4	4.9	4.6	4.2	4.0	4.1
3.5	2.5	1.5		1.5	2.5	3.5

4.44	4.44	4.35	4.22
10.4	14.4	2.5	4.0
Dr.	Dr.	Dr.	Dr.
	Beg. Strips		

4.7	3.92	3.94
1.2	1.2	2.5
ground	Top wall	

270.09

Walker Extension of Cross Sections
 Johnson
 Frank Gregory
 801161
 7-12-48 to Harbor Drive

1+26 = 2' 4" Conc. Walk on Rt. H0 2200%

1+15 30' Rt = 2" Tree

1+00

0+79 30' Rt = 2" Tree

0+50

0+46 " " " "

0+13.5 = M.H. Water Dept. 16.5' 4.

0+12 30' Rt 2" Tree

0+00

N.E. Ret.

S.E. Ret. 6 Rts

0-16 = East Ch. Rosecrans.

4.35 12.88

8.53

BM. 0400
 CP 0134
 P-10

Lt.

R.

Rt.

5.67

6.20

7.21

6.47

18.11
 on walk

46.5
 on walk

6.1	4.6	6.7	6.8
4.5	5.3	6.2	6.1
5.5	5.5	6.5	5.5

4.9	8.9	1.7	1.2
4.0	4.5	5.2	5.7
5.5	3.5	3.7	5.5

8.7	8.75	8.90	8.8
4.1	4.3	3.28	4.1
5.5	3.5	5.5	5.5
Por.	Por.	on edge walk	

8.87	8.63	8.8A	8.21	8.57	1.82
4.1	4.5	4.04	4.67	4.31	5.06
CB	Ent.	CB	Ent.	CB	Ent.
A	A	B	B	C	C

4.00	1.63	8.29	1.81	8.53	8.18	8.80	8.33	8.9A	4.43	9.01
4.8	5.25	4.6	5.01	4.35	4.20	4.98	4.55	3.94	4.45	3.87
CB	Ent.	CB	Ent.	CB	Ent.	CB	Ent.	CB	Ent.	CB
5.57	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6
Ent.	Ent.	Ent.	Ent.	Ent.	Ent.	Ent.	Ent.	Ent.	Ent.	Ent.

9.16	9.1A	8.96	8.90	8.73	8.33	9.88
3.12	3.74	3.92	3.98	4.15	4.35	3.90
6.28	6.28	17	17	17	6.0	6.0
CB	Ent.	Por.	Por.	Por.	Ent.	CB
					15.48	
					Rad.	

12.88

Sorrell St. Cont. from P 70

2+20

4+07 10.5 ft 5" Palm

4+00

3+70

3+69 10" Palm 40.5 ft.

T.P. 5.88 7.22 11.54 1.34

3+00

2+50

2+45.3 - WLY edge Conc. Box Water Meter
(see F.B. 1747, P 57)

2+23 30" H. - 2" Tree

2+00

1+945 " " "

1+765 " " "

1+575 " " "

1+50

12.88

Lt

R

17

71

4+635

Navy Barracks
1916.

3+907

7.0
5.9
5.5

1.8
2.1
5.5

4.0
4.9
5.5

6.8

5.4
5.5

2.1

4.8
3.5

0.7

6.5
1.7

0.9

6.8
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0.3

6.9
1.7

0.6

5.6
2.5

-0.3

7.5
5.5

6.6
0.6
5.5

5.1
1.8
3.5

7.8
2.1
5.5

7.0
5.9
5.5

1.8
2.1
5.5

4.0
4.9
5.5

76.8

7.22

3.8
2.1
5.5

1.7

8.2
8.5

5.1

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-0.3

7.5
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5.5

1.7

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8.5

5.1

2.5
2.5

5.1

6.6
6.6

-0.3

7.5
5.5

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5.5

5.1
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3.8
2.1
5.5

1.7

8.2
8.5

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5.1

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3.8
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1.7

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8.5

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-0.3

7.5
5.5

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3.8
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5.5

1.7

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6.6

-0.3

7.5
5.5

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5.1
1.8
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3.8
2.1
5.5

1.7

8.2
8.5

5.1

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2.5

5.1

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5.5

1.7

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8.5

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-0.3

7.5
5.5

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5.5

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8.2
8.5

5.1

2.5
2.5

5.1

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6.6

-0.3

7.5
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5.5

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8.5

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-0.3

7.5
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5.5

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3.5

3.8
2.1
5.5

1.7

8.2
8.5

5.1

2.5
2.5

5.1

6.6
6.6

0.6

5.6
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0.6
5.5

5.1
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3.8
2.1
5.5

1.7

8.2
8.5

5.1

2.5
2.5

5.1

6.6
6.6

-0.3

7.5
5.5

0.6
0.6
5.5

5.1
1.8
3.5

3.8
2.1
5.5

1.7

8.2
8.5

5.1

2.5
2.5

5.1

6.6
6.6

0.6

5.6
2.5

0.6
0.6
5.5

5.1
1.8
3.5

3.8
2.1
5.5

1.7

8.2
8.5

5.1

2.5
2.5

5.1

6.6
6.6

-0.3

7.5
5.5

0.6
0.6
5.5

5.1
1.8

6+88.07

T.P. 9.25 9.25 6.52 0.76 ^{off H&B} 7+05.07

6+50

6+40 = West end Transformer Wire Cage on Lt.

6+06 = Lt. std.

6+00

5+50

5+43 Lt. Pole 111 Navy Yard.

5+76 E. end Bld 82.3 Lt.

5+15 = W. end Bld. "

5+00

4+68 = S. Tower MH 67 Lt.

4+78.5 Palm 40.5 Lt.

4+58 = Lt. std.

4+50

4+42 40.5 Lt. - Palm ^{6"}

4+2.6

7.22

6.7

3.3
5.5

9.95

6.0

1.2
5.5

6.7

4.0
5.5

6.9

0.3
5.5

7.11
0.11
8.23
Canc. 7.0.4
59.4
Rim MH

7.62
2.33
6.23
Canc. 6.7

6.89
0.95
5.5
6.7 Ramp.

6.71

7.2

0.0
5.5

6.9 2.2 0.5 0.5 0.1 0.5 0.3 2.6 2.2 2.1
2.3 5.0 6.7 6.7 6.8 6.7 5.9 4.6 5.0 5.1
5.5 2.7 2.2 1.7 1.7 2.5 2.7 2.7 2.7 5.5

7.22

8+57

8+00

7+80

7+64

7+56 Light Standard 39' Lt.

7+44 Fire Hydrant 42' Lt.

7+40.07

7+22.07

7+15

7+05.07 E. Shafter St.

Lt.

£

Rt.

73

6.5

3.9
5.5

6.6

3.9
5.5

6.5

3.9
5.5

6.6

3.9
5.5

6.7

3.9
5.5

6.6

3.9
5.5

6.6

3.9
5.5

5.1

4.9
5.5

9.8

6.2
5.5

2.9

7.1
5.5

1.9

8.1
5.5

925

11+50

5.8
12
554.3
57
55

11+00

6.0
10
554.3
57
55

10+56 = light Standard 39' Lt.

10+50

6.0
10
554.5
55
55

10+00

6.2
3.8
555.2
48
55

9+50

6.3
3.7
554.9
51
55

9+37 Lt. Pole 60' Lt.

9+05.5 Light Standard 39' Lt.

9+00

6.1
3.6
554.7
53
55

9.95

Stations

15+50 53' Ft. = Light Standard
 15+45.5 End Transformer Cage
 15+29.5 beg. Transformer Cage
 15+06 Lt. Std. 39' Lt.
 15+00

14+02

13+87' 60' Lt. = Elec Pole
 (13+00)
 13+55 = Light Stand. 39' Lt.
 13+50

T.P. 3.41 8.41 4.95 5.00

13+00 69' Lt. = Sewer M.H.
 12+92.5 81' Lt. = Sewer Std.
 12+64.5 81' "
 12+52 = Fire Pk. 41' Lt.
 12+50

12+28 Elec. Pole
 12+06 = Light Standard 39' Lt.
 12+00

9.95

4.6

3.8
 5.5

4.6

3.8
 5.5

5.2

3.2
 5.5

5.1

5.0
 5.5

4.9

4.6
 5.5

5.9

4.6
 5.5

5.1

4.3
 5.5

3.9

4.5
 5.5

3.6

4.8
 5.5

3.8

4.6
 5.5

3.9

4.5
 5.5

4.1

5.2
 5.5

4.2

3.8
 5.5

4.3

5.7
 5.5

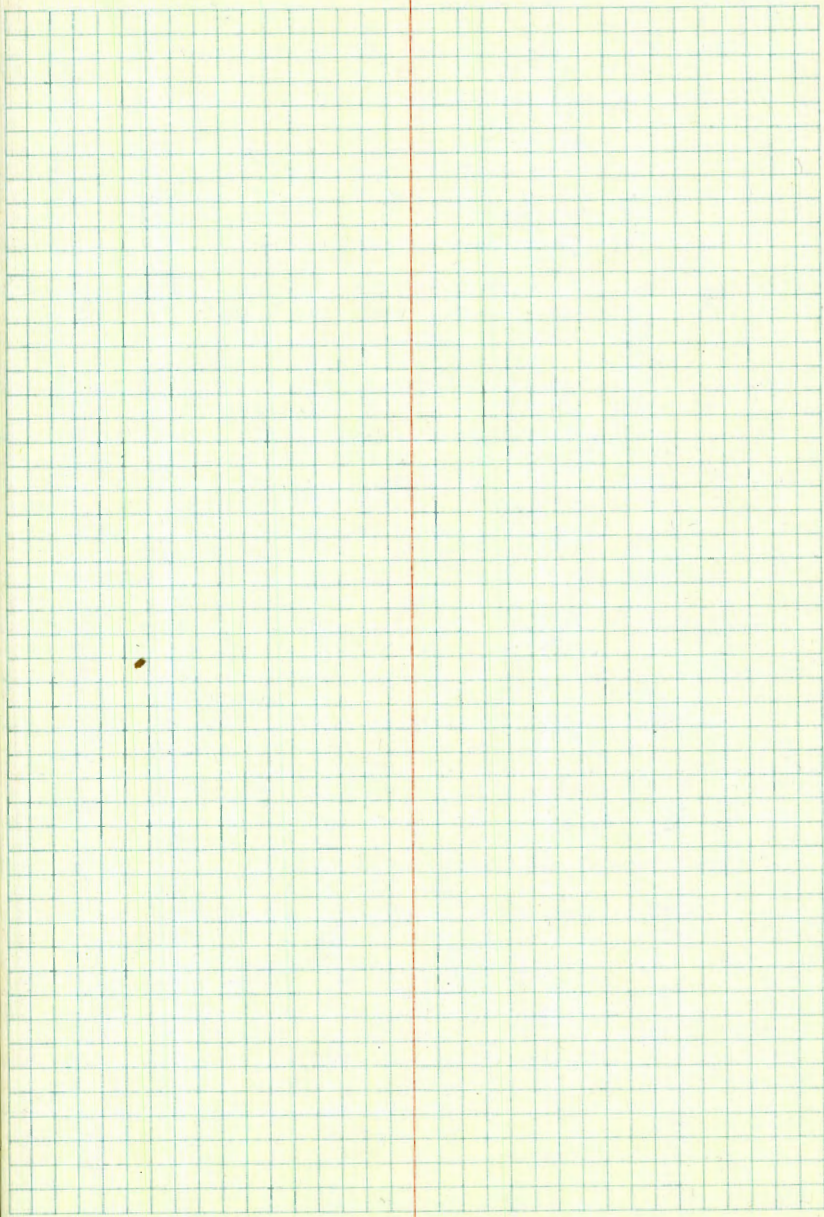
5.56

2.53
 5.5
 60.00 M.H.

8.41

9.95

Station



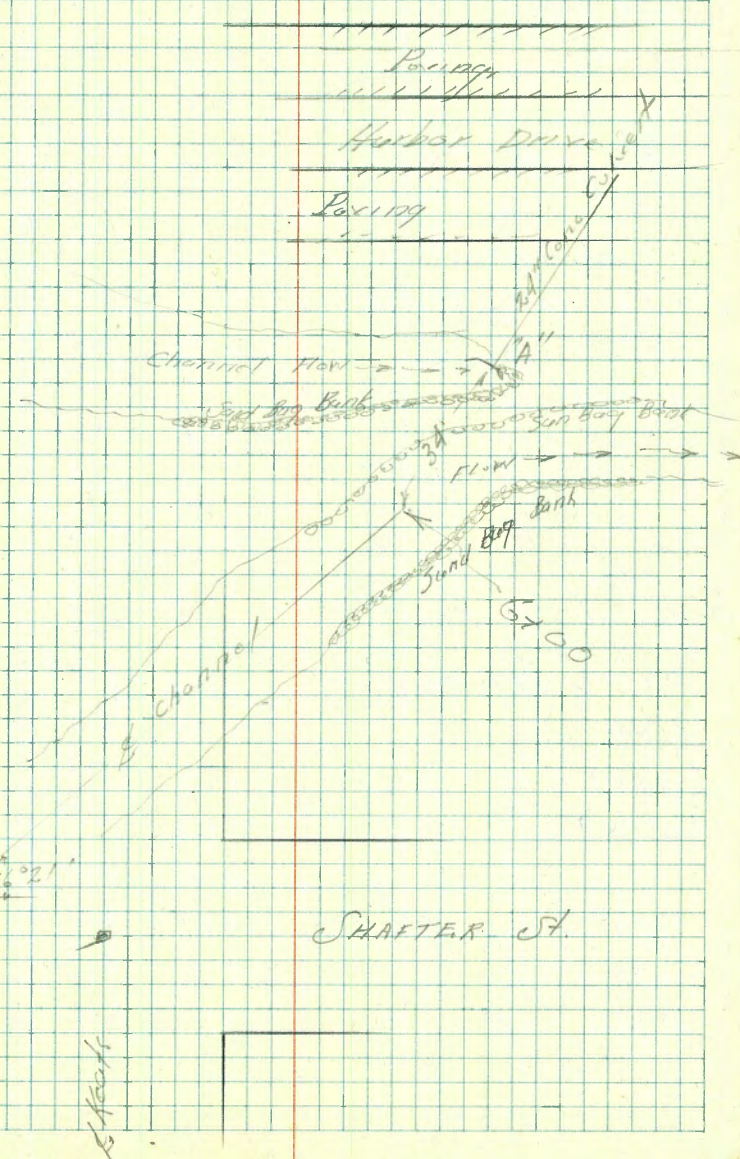
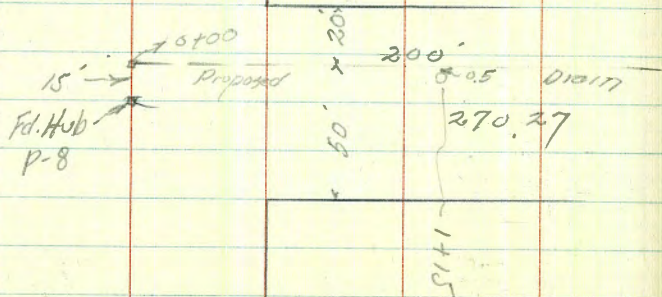
1673391 P-19		<u>0.01</u>
Check BM Conc. Mon	4.99	3.43
		3.42

Note. from 16700 to 16794 Elev. at 55'4" Same as 40'4"

8.41

LOWELL ST

35' x 25'



Levels - Proposed Drains

Lorvell & Strafter - Sketch P. 77

Station

Cont P. 79

8+00	76	-2.0
7+00	77	-2.1
"A" Flow 20" Pipe	6.65	-1.07
6+00	86	-3.0
5+65 Ground	82	-2.6
5+65 on Top 6" C.T. Sewer	61	-0.5
5+00	84	-2.8
4+00	77	-2.1
3+00 in ch.	78	-2.2
2+62 in channel	71	-1.5
(2+40) 8' RT	69	-1.3
2+40	53	0.3
(3+00) 2' RT-ditch	67	-1.1
2+00 "A" RT 16' 21"	6.12	-1.34
1+50	50	0.6
(1+00) 5' RT	58	-0.2
1+00	49	0.7
0+50	50	0.6
0+27	46	1.0
0+16	53	0.3
0+00 on Hub	447	1.11

4.88 5.58

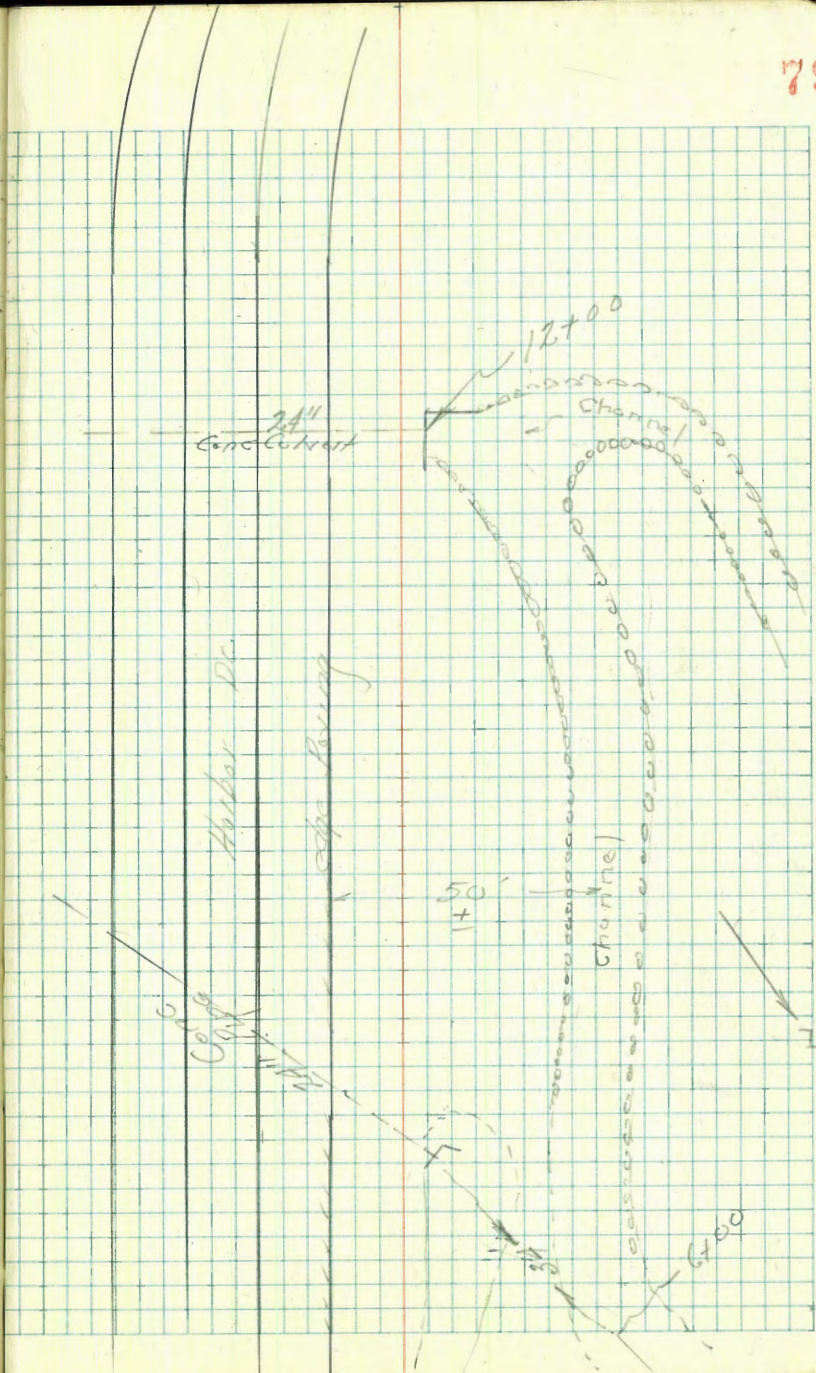
0.70

B.M.
HubSta 740507
P. 77

Lowell o Stroffer Drain

Cont. from p. 78

79



12+00	Flow Line 24" Pipe	9.0	-3.4
11+00		8.7	-2.5
10+00		7.7	-2.1
9+00		7.6	-2.0

5.58

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{13}{16}$
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{7}{8}$
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{15}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360°	= 21600'	= 1296000"
Radius	= arc of 57.2957790°	
Arc of 1° (radius = 1)	= .017453292	
Arc of 1' (radius = 1)	= .000290888	
Arc of 1" (radius = 1)	= .000004848	

$$\pi = 3.141592654$$

$$\frac{\pi}{4} = 0.785398163$$

$$\frac{\pi}{6} = 0.523598776$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167$$

$$\frac{\pi}{6} = 0.523598776$$

$$\frac{4\pi}{3} = 4.188790205$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$\sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\pi^2 = 9.869604401$$

$$\frac{1}{\pi^2} = 0.101321184$$

$$\sqrt{\pi} = 1.772453851$$

$$\frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11 $\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R $\frac{1}{2}$ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

10.1
3/
20.5
2.1

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C o /	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

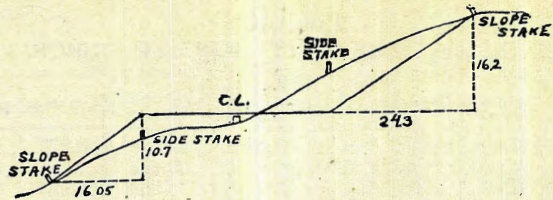
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.023	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 30"	.50833	40' 30"	.67500	50' 30"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 00	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

70507
17
6188.

SE Valtuero
- Warrington?

64 47
32 23
73 66
1+05.99
1+28.13 - E.C.

29.
35

106 447
49 76

17+24.7 4.1' ct. Light Signal

264.31
4.40
259.91
10.18
270.09

X
1054

923
131

573
131
442

115.032
47.46

10.9
10