

1784

ONE

\_\_\_\_\_

TWO

THREE

FOUR

\_\_\_\_\_

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.

MICRO For Single Track Embankment.

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.1  | 8.2  | 8.3  | 8.4  | 8.5  | 8.6  | 8.7  | 8.8  | 8.9  | 0  |
| 1  | 9.0  | 9.1  | 9.2  | 9.3  | 9.4  | 9.5  | 9.6  | 9.7  | 9.8  | 9.9  | 1  |
| 2  | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 2  |
| 3  | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 3  |
| 4  | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 4  |
| 5  | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 5  |
| 6  | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 6  |
| 7  | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 7  |
| 8  | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 8  |
| 9  | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 9  |
| 10 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 10 |
| 11 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 11 |
| 12 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 12 |
| 13 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 13 |
| 14 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 14 |
| 15 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 15 |
| 16 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 16 |
| 17 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 17 |
| 18 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 18 |
| 19 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 19 |
| 20 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 20 |
| 21 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 21 |
| 22 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 22 |
| 23 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 23 |
| 24 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 24 |
| 25 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 25 |
| 26 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 26 |
| 27 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 27 |
| 28 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 28 |
| 29 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 29 |
| 30 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 30 |
| 31 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 31 |
| 32 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 32 |
| 33 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 33 |
| 34 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 34 |
| 35 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 35 |
| 36 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 36 |
| 37 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 37 |
| 38 | 46.0 | 46.1 | 46.2 | 46.3 | 46.4 | 46.5 | 46.6 | 46.7 | 46.8 | 46.9 | 38 |
| 39 | 47.0 | 47.1 | 47.2 | 47.3 | 47.4 | 47.5 | 47.6 | 47.7 | 47.8 | 47.9 | 39 |
| 40 | 48.0 | 48.1 | 48.2 | 48.3 | 48.4 | 48.5 | 48.6 | 48.7 | 48.8 | 48.9 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.  
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1784

INDEXED

to page # 73  
except page # 25, 52

CITY ENGINEER'S OFFICE

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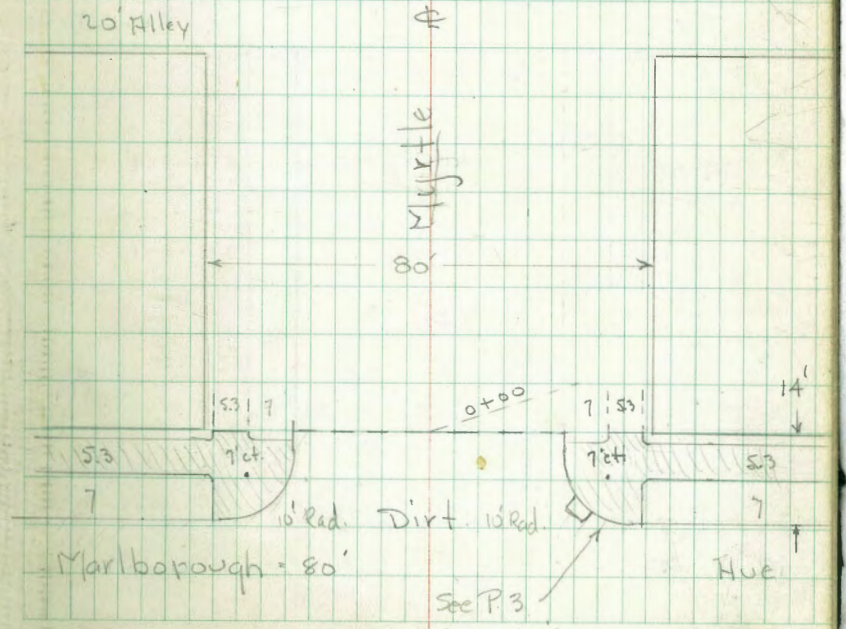
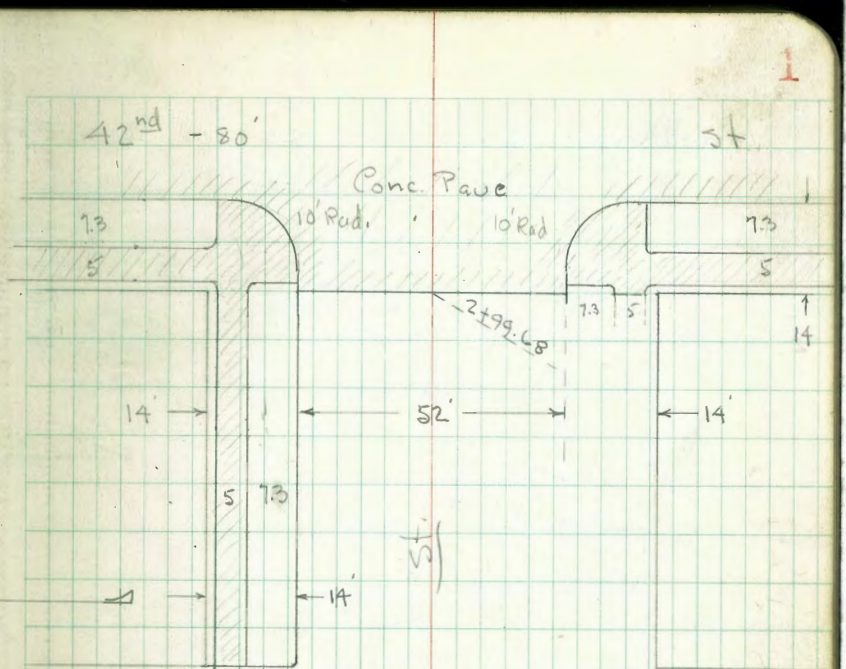
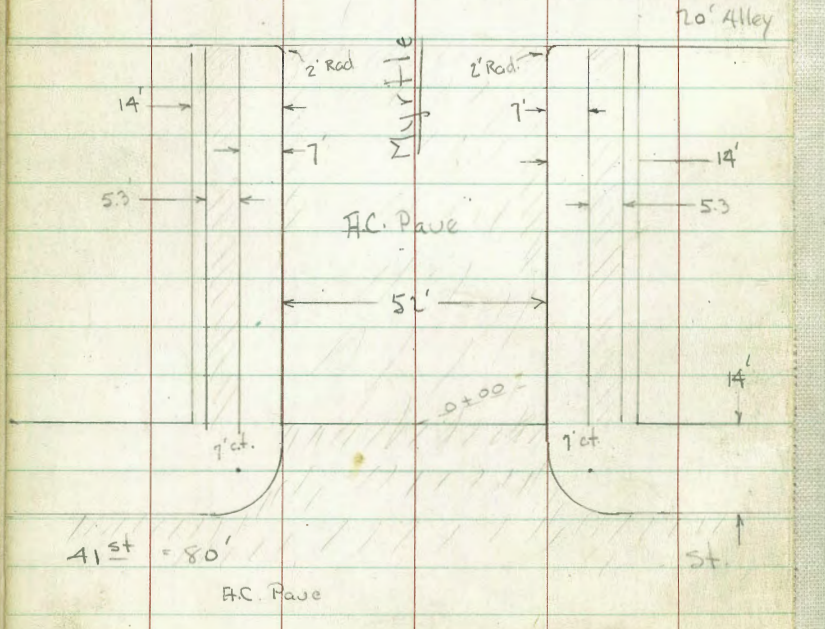
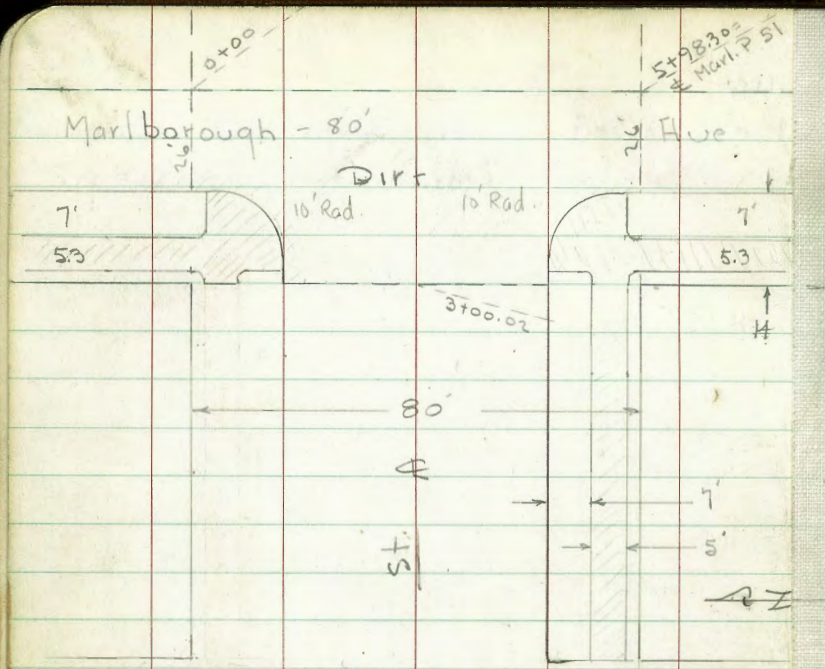
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Page

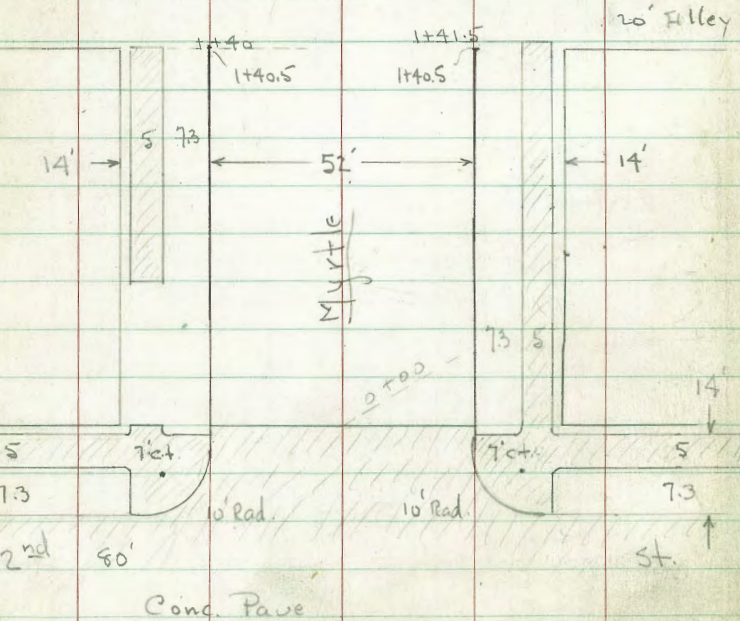
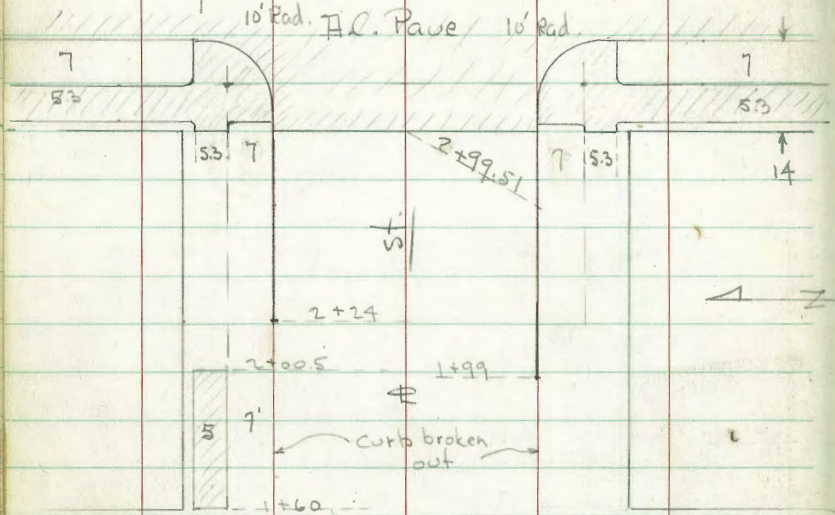
Index

1-C8 - X-Sect - Myrtle + Dwight - 41<sup>st</sup> to Fairmount  
Marlborough - Redwood to 175 N. of Dwight



Van Dyke - 80'

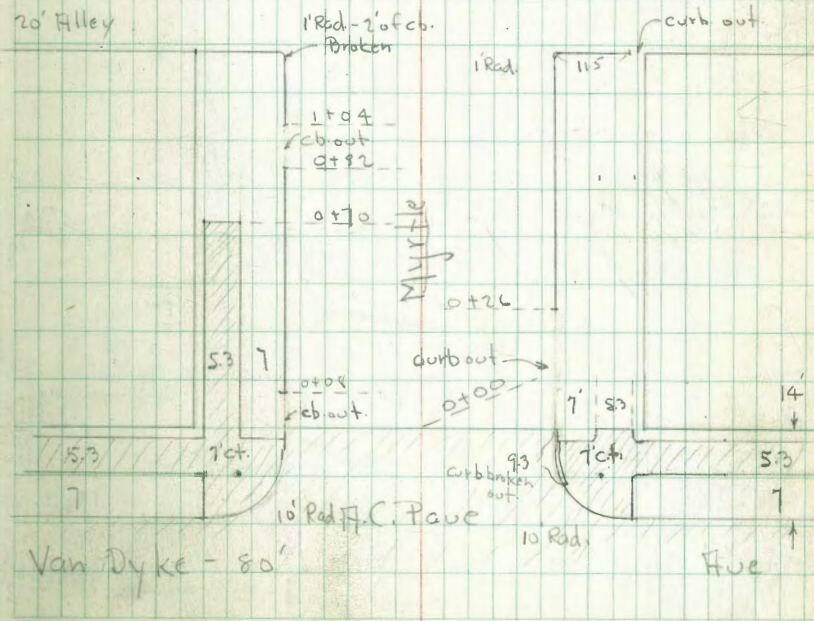
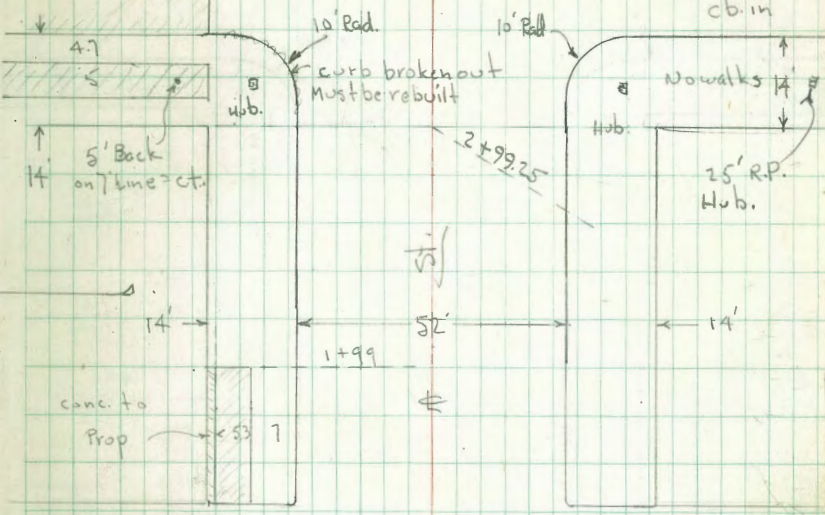
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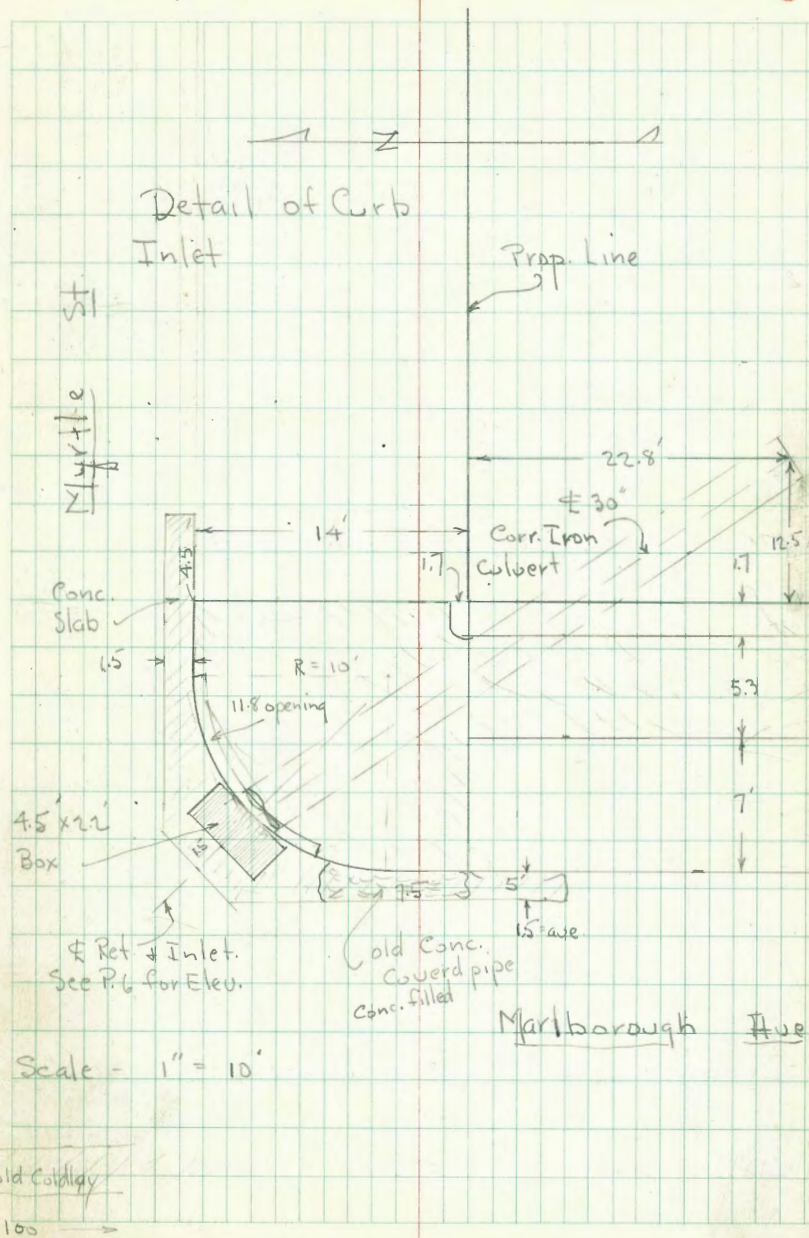
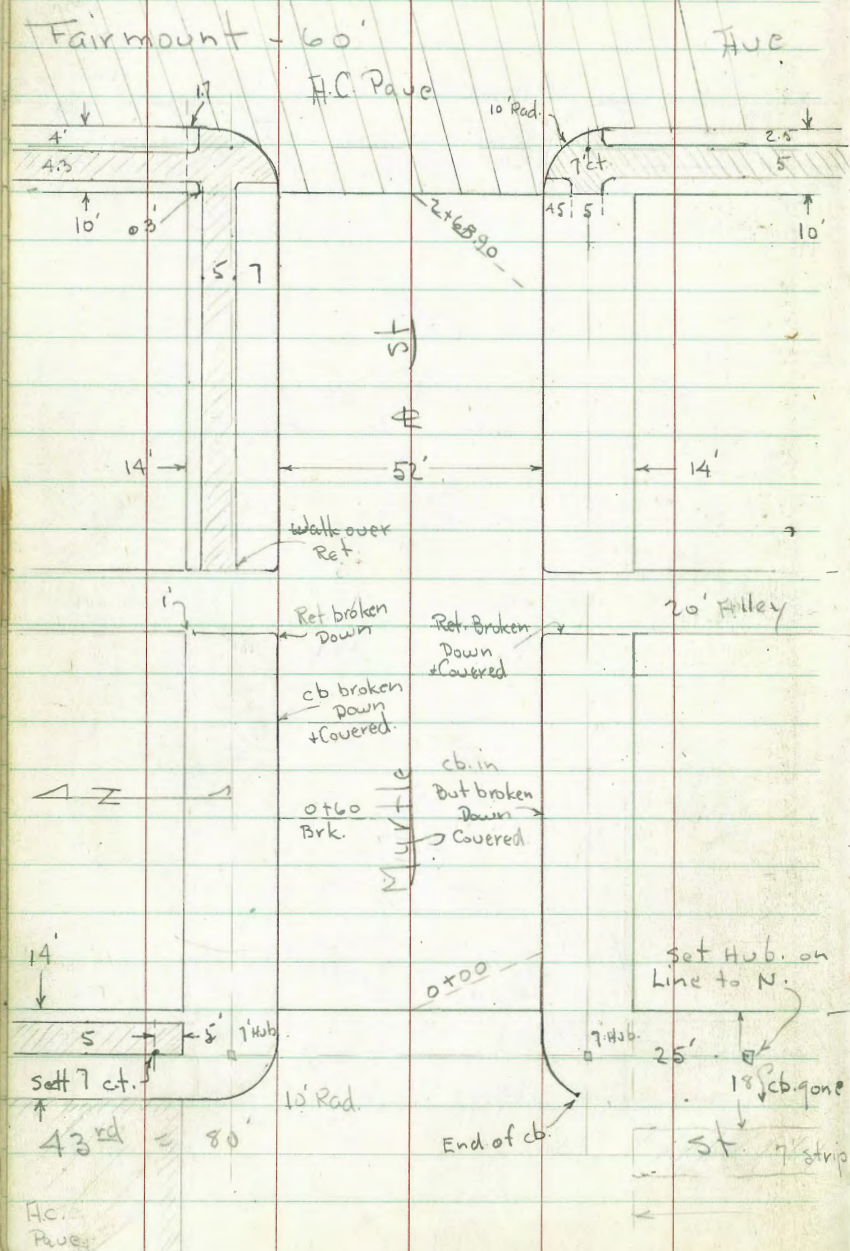


A.C. Pave  
43<sup>rd</sup>

80'

st.  
cb in





indexed  
c.s.kr

X-Section Myrtle - from E.L. 41<sup>st</sup> to  
Fairmount 80' st. 14' curbs.

# 1193

W.O. 31385

7-9-47

Osborne  
Smith  
Worrell

1+40 = W.L. 20' Alley + end H.C. Pavc

should be

1+00

0+50

0+00 = E.L. 41<sup>st</sup> = on H.C. Pavc

B.M. 3.40 324.92

321.52

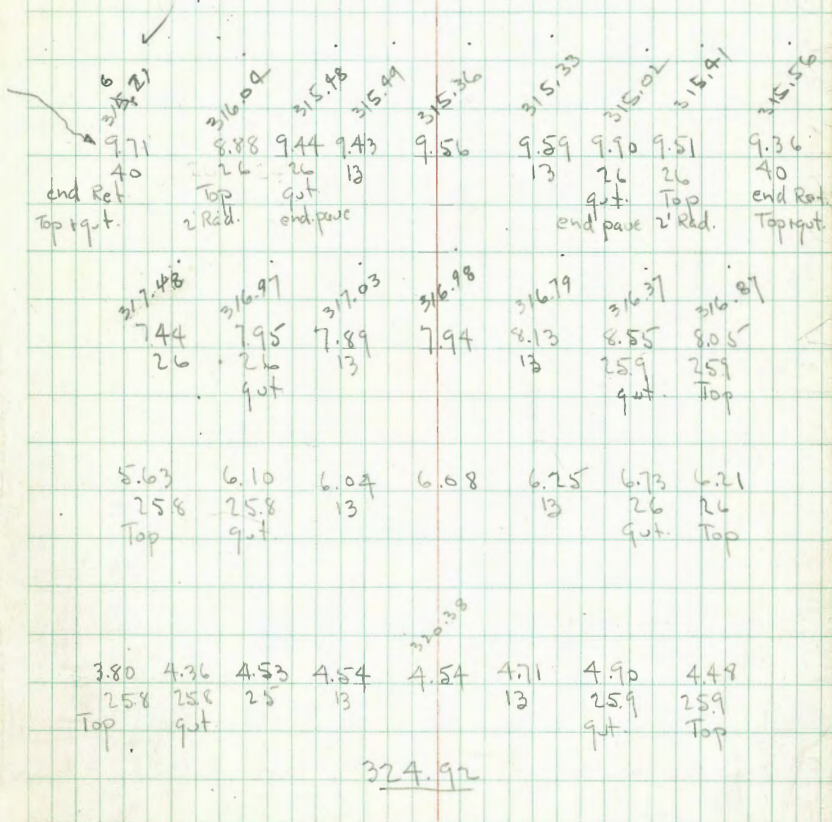
Myrtle + 41<sup>st</sup>  
NW.P.P.

Lt. = N

⊕

Rt. = S.

4



27 E.

14 E. = w. cb.

T.P. 7.37 317.42 437 310.05 310.07

3+00.02 = W.L. Marlborough

Mid Pt. on Ret. = FL = 309.10

2+50

2+31 = 25.8 Rt. = ± 17' Doub. Conc. Dr.

T.P. 2.35 314.42 12.85 312.07

2+00

1+60 = E.L. Alley - No cb. on Lt.

| Lt.     |        |        |       | Rt.   |       |       |         |
|---------|--------|--------|-------|-------|-------|-------|---------|
| 310.0   | 309.8  | 309.7  | 309.6 | 309.4 | 309.3 | 309.0 |         |
| 7.4     | 7.6    | 7.7    | 7.8   | 8.0   | 8.1   | 8.4   |         |
| 40      | 26     | 13     |       | 13    | 26    | 40    |         |
| 310.0   | 310.03 | 309.6  | 309.6 | 309.6 | 309.1 | 308.6 | 308.3   |
| 7.4     | 7.39   | 7.8    | 7.8   | 7.9   | 8.3   | 8.8   | 8.49    |
| 40      | 40     | 26     | 13    |       | 13    | 26    | 40      |
| got     | Top    |        |       |       |       | Top   | got     |
| 317.42  |        |        |       |       |       |       |         |
| 310.3   | 310.16 | 309.88 | 309.7 | 309.8 | 309.3 | 308.5 | 308.24  |
| 4.1     | 4.26   | 4.54   | 4.7   | 4.6   | 4.5   | 5.1   | 5.9     |
| 40      | 383    | 25.9   | 25.9  | 13    |       | 13    | 25.9    |
| Cor.    | Top    | got    |       |       |       | got   | Top     |
| back of |        |        |       |       |       |       |         |
| walk    |        |        |       |       |       |       | walk    |
| 311.4   | 311.4  | 310.4  | 310.4 | 310.9 | 311.1 | 310.7 | 310.3   |
| 3.0     | 3.0    | 4.0    | 4.0   | 3.5   | 3.3   | 3.7   | 4.1     |
| 40      | 27     | 25     | 20    | 10    |       | 13    | 25.8    |
|         |        |        |       |       |       |       | got     |
|         |        |        |       |       |       |       | Top     |
|         |        |        |       |       |       |       | walk    |
|         |        |        |       |       |       |       | 311.2   |
|         |        |        |       |       |       |       | 310.99  |
|         |        |        |       |       |       |       | 3.30    |
|         |        |        |       |       |       |       | 25.8    |
|         |        |        |       |       |       |       | Dr.     |
|         |        |        |       |       |       |       | 25.8    |
|         |        |        |       |       |       |       | walk    |
| 314.42  |        |        |       |       |       |       |         |
| 314.0   | 314.7  | 312.7  | 312.5 | 312.8 | 312.8 | 312.5 | 312.3   |
| 10.9    | 10.2   | 12.7   | 12.4  | 12.1  | 12.1  | 12.4  | 12.6    |
| 40      | 28     | 26     | 20    | 10    |       | 13    | 25.8    |
|         |        |        |       |       |       |       | got     |
|         |        |        |       |       |       |       | Top     |
|         |        |        |       |       |       |       | 312.00  |
|         |        |        |       |       |       |       | 11.92   |
|         |        |        |       |       |       |       | 25.8    |
|         |        |        |       |       |       |       | got     |
|         |        |        |       |       |       |       | Top     |
|         |        |        |       |       |       |       | 314.62  |
|         |        |        |       |       |       |       | 314.88  |
|         |        |        |       |       |       |       | 19.04   |
|         |        |        |       |       |       |       | 40      |
|         |        |        |       |       |       |       | end Ret |
|         |        |        |       |       |       |       | Top+got |
| 324.92  |        |        |       |       |       |       |         |



0+25

0+04.5 = End of Conc. gutter slab for Inlet

80' E. = E.L. Marlborough = 0+00 ahead.

Elevations on  $\pm$  of Inlet. - See P. 3 for sketch

66' E. = E.cb.

53' E.

40' E. =  $\pm$

| Lt.                      |                    |             |       |       | Rt.              |             |                              |                                       |                                       |
|--------------------------|--------------------|-------------|-------|-------|------------------|-------------|------------------------------|---------------------------------------|---------------------------------------|
| 311.1                    | 310.9              | 309.7       | 310.2 | 310.4 | 310.1            | 309.7       | 310.2                        | 310.5                                 | 311.3                                 |
| 6.3                      | 6.5                | 7.7         | 7.2   | 7.0   | 7.2              | 7.7         | 7.2                          | 6.9                                   | 6.1                                   |
| 40                       | 26                 | 24          | 13    |       | 13               | 13          | 26                           | 40                                    | 50                                    |
|                          |                    |             |       |       |                  |             | 24.5' edge<br>Slab           |                                       | 26<br>edge slab                       |
|                          |                    |             |       |       |                  |             | 8.83                         |                                       | 8.85                                  |
|                          |                    |             |       |       |                  |             | 24.5' edge<br>Slab           |                                       | 26<br>edge slab                       |
| 310.24                   | 309.97             | 309.4       | 309.3 | 309.2 | 309.0            | 308.69      | 308.68                       | 309.50                                | 309.16                                |
| 7.16                     | 7.45               | 8.0         | 8.1   | 8.2   | 8.4              | 8.73        | 8.74                         | 7.92                                  | 7.6                                   |
| 38.3                     | 25.9               | 25.9        | 13    |       | 13               | 24.5        | 25.9                         | 25.9                                  | 38.3                                  |
| Cor. Ret.                | Top<br>end.cb.     | Top<br>cut. |       |       |                  | edge Conc.  | Top<br>cut.                  | Top<br>Cor.                           | Ret.                                  |
| 309.54                   | 309.68             | 309.59      |       |       | 308.36           | 305.29      | 308.31                       | 308.29                                |                                       |
| 14.88                    | 7.74               | 7.83        |       |       | 9.06             | 12.03       | 9.05                         | 9.03                                  |                                       |
| F.L. outlet.<br>30" Pipe | 10 Rod.<br>on Ret. | Top cb.     |       |       | Gut. on<br>Grate | F.L.<br>Box | 21" out.<br>edge of<br>Grate | 21" out.<br>edge of<br>Conc.<br>Slab. | 21" out.<br>edge of<br>Conc.<br>Slab. |
| 309.5                    | 310.05             | 309.1       | 309.1 | 309.0 | 308.8            | 308.5       | 308.39                       | 309.97                                | 308.47                                |
| 7.9                      | 7.37               | 8.3         | 8.3   | 8.4   | 8.6              | 8.9         | 9.03                         | 7.95                                  | 8.95                                  |
| 40                       | 40                 | 26          | 13    |       | 13               | 26          | 27.1                         | 40                                    | 40                                    |
| cut.                     | Top                |             |       |       |                  |             | edge Conc.<br>for inlet      | Top<br>cut.                           | cut.                                  |
| 310.0                    | 309.7              | 309.5       | 309.3 | 309.2 | 309.2            | 309.2       | 309.0                        | 309.0                                 | 309.2                                 |
| 7.4                      | 7.7                | 7.9         | 8.1   | 8.2   | 8.2              | 8.2         | 8.4                          | 8.4                                   | 8.2                                   |
| 40                       | 26                 | 13          |       | 13    | 26               | 26          | 40                           | 40                                    | 40                                    |
|                          |                    |             |       |       |                  |             |                              |                                       | on<br>Conc.                           |
| 309.2                    | 309.9              | 309.6       | 309.5 | 309.5 | 309.5            | 309.2       | 309.2                        | 309.2                                 |                                       |
| 7.2                      | 7.5                | 7.8         | 7.9   | 7.9   | 7.9              | 8.0         | 8.2                          | 8.2                                   |                                       |
| 40                       | 26                 | 13          |       | 13    | 26               | 26          | 40                           | 40                                    |                                       |

317.42

2+98 - 27.7 Rt. = ± P. pole # 4199

2+50

2+30 - 15.8 Lt. = ± 20' Conc. Dr.

2+00

TP. 8.58 325.46 0.54 316.88

1+62 = 28' Rt. = ± F.H.

1+60 = E.L. Alley - Beg. cb. and walk on Lt.

1+40 = W.L. 20' Alley

1+39 - 28.3 Rt. = ± P. pole # P 4175

1+00

0+50

Lt.

Rt.

7

|        |       |       |       |       |       |       |       |       |       |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 319.41 | 319.1 | 319.1 | 319.0 | 318.5 | 317.9 | 318.5 | 318.9 | 320.7 | 321.5 |
| 5.45   | 6.4   | 6.4   | 6.5   | 7.0   | 7.6   | 7.0   | 6.6   | 4.8   | 4.0   |
| 25.8   | 25.8  | 13    |       | 13    | 25    | 26    | 35    | 40    | 43    |
| Top    | gut.  |       |       |       |       |       |       |       |       |

|        |       |       |       |       |       |       |       |       |       |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 6.32   | 7.16  |       |       |       |       |       |       |       |       |
| 33.2   | 25.8  |       |       |       |       |       |       |       |       |
| Walk   | Dr.   |       |       |       |       |       |       |       |       |
| 317.76 | 317.0 | 317.4 | 317.1 | 316.7 | 316.0 | 316.7 | 316.9 | 318.4 | 320.2 |
| 7.70   | 8.5   | 8.3   | 8.4   | 8.8   | 9.5   | 8.8   | 8.6   | 7.1   | 5.3   |
| 25.9   | 25.9  | 13    |       | 13    | 25    | 26    | 35    | 40    | 43    |
| Top    | gut.  |       |       |       |       |       |       |       |       |

325.46

Topbank

|          |       |       |       |       |       |       |       |       |       |
|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 316.30   | 315.9 | 314.9 | 315.6 | 315.7 | 315.8 | 315.3 | 314.8 | 315.4 | 315.8 |
| 122      | 1.5   | 1.2   | 1.8   | 1.7   | 1.6   | 2.1   | 2.6   | 2.2   | 1.6   |
| 40       | 40    | 26    | 26    | 13    |       | 13    | 24    | 26    | 40    |
| Top      | gut.  | Top   | gut.  |       |       |       |       |       |       |
| end Ret. |       | Red.  |       |       |       |       |       |       |       |
| 315.0    | 314.8 | 314.9 | 314.9 | 315.0 | 314.6 | 314.1 | 314.8 | 315.4 | 315.4 |
| 2.4      | 2.6   | 2.5   | 2.4   | 2.9   | 3.3   | 2.6   | 2.2   | 2.2   | 2.2   |
| 40       | 26    | 13    |       | 13    | 24    | 26    | 40    |       |       |

|       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|
| 313.9 | 313.3 | 312.8 | 313.2 | 313.4 | 312.9 | 312.4 | 312.9 |
| 3.5   | 4.1   | 4.6   | 4.2   | 4.0   | 4.5   | 5.0   | 4.5   |
| 40    | 26    | 23    | 13    | 40    | 13    | 26    | 40    |

|       |       |       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 311.7 | 311.6 | 310.6 | 311.4 | 311.6 | 311.2 | 310.7 | 311.4 | 311.7 | 311.5 |
| 5.7   | 5.8   | 6.8   | 6.0   | 5.8   | 6.2   | 6.7   | 6.2   | 5.7   | 4.9   |
| 40    | 26    | 23    | 13    |       | 13    | 23    | 26    | 40    | 50    |

317.42

Cont. on P. 11

T.P. NW. 4<sup>th</sup>  
 Check B.M. 3.85 325.46 3.85 321.61 321.62

80' E. = E.L. 4<sup>th</sup> = 0+00 ahead - edge of Conc.  
 Pavc = 0.4 E. - Rods on Edge

66' E. = E. cb.

53' E.

40' E. = E

27' E.

14' E. = W cb.

2+99.68 = W.L. 4<sup>th</sup> St. = edge of Conc. pave

|  | Lt.     |        |        |        | Rt.    |        |        |        |        |
|--|---------|--------|--------|--------|--------|--------|--------|--------|--------|
|  | 321.95  | 321.80 | 321.64 | 321.10 | 321.05 | 320.98 | 320.55 | 320.10 | 320.65 |
|  | 351.366 | 382    | 436    | 441    | 4.58   | 4.91   | 5.36   | 4.81   |        |
|  | 382     | 332    | 259    | 259    | 13     | 13     | 259    | 259    |        |
|  | endwalk | Top    | gut.   |        |        |        | gut.   | Top    |        |
|  | 321.68  | 321.10 | 320.86 | 320.67 | 320.48 | 320.35 | 320.11 | 319.91 | 320.55 |
|  | 3.78    | 4.36   | 4.60   | 4.79   | 4.98   | 5.21   | 5.35   | 5.55   | 4.91   |
|  | 40      | 40     | 26     | 13     |        | 13     | 26     | 40     | 40     |
|  | Top     | gut.   |        |        |        |        | gut.   | Top    |        |
|  | 3.88    | 4.13   | 4.37   | 4.54   | 4.74   | 4.93   | 5.19   |        |        |
|  | 40      | 26     | 13     |        | 13     | 26     | 40     |        |        |
|  | 3.82    | 4.03   | 4.26   | 4.45   | 4.60   | 4.80   | 5.04   |        |        |
|  | 40      | 26     | 13     |        | 13     | 26     | 40     |        |        |
|  | 3.93    | 4.16   | 4.36   | 4.54   | 4.75   | 4.94   | 5.18   |        |        |
|  | 40      | 26     | 13     |        | 13     | 26     | 40     |        |        |
|  | 3.88    | 4.40   | 4.66   | 4.86   | 4.99   | 5.17   | 5.33   | 5.60   | 5.00   |
|  | 40      | 40     | 26     | 13     |        | 13     | 26     | 40     | 40     |
|  | Top     | gut.   |        |        |        |        | Top    | Top    |        |
|  | 3.84    | 4.46   | 4.43   | 4.60   | 4.97   | 5.50   | 4.83   | 4.71   | 4.64   |
|  | 259     | 259    | 13     |        | 13     | 259    | 259    | 33.1   | 33.1   |
|  |         |        |        |        |        | gut.   | Top    | walk   | 40     |

325.46

Indexed  
C.S.K.

Levels on 42<sup>nd</sup> - 100' Each way from  
Prop. Lines of Myrtle + Rods around  
Returns - 80' st. - 14' cbs - Paved Conc.

1+00 = 100' N. = end.

0+50

0+25

0+00 = N.L. Myrtle

See P. 8 for Int.

1+00 = S.L. Myrtle

0+50

0+00 = 100' S. of S.L. Myrtle on E 42<sup>nd</sup>

7.0.  
7-17-47

Lt. = W.

±

Rt. = E

9

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 1.84<br>26<br>Top | 2.43<br>26<br>gut. | 1.96<br>13 | 1.84 | 1.90<br>13 | 2.33<br>26<br>gut. | 1.77<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 2.87<br>26<br>Top | 3.45<br>26<br>gut. | 2.98<br>13 | 2.86 | 2.95<br>13 | 3.36<br>26<br>gut. | 2.78<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 3.34<br>26<br>Top | 3.98<br>26<br>gut. | 3.50<br>13 | 3.35 | 3.44<br>13 | 3.85<br>26<br>gut. | 3.31<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |  |            |                    |                   |
|-------------------|--------------------|------------|------|--|------------|--------------------|-------------------|
| 3.88<br>26<br>Top | 4.40<br>26<br>gut. | 3.93<br>13 | 3.82 |  | 3.88<br>13 | 4.36<br>26<br>gut. | 3.78<br>26<br>Top |
|-------------------|--------------------|------------|------|--|------------|--------------------|-------------------|

|             |              |            |      |            |            |            |
|-------------|--------------|------------|------|------------|------------|------------|
| 5.00<br>Top | 5.60<br>gut. | 5.18<br>13 | 5.04 | 5.19<br>13 | 5.55<br>26 | 4.91<br>26 |
|-------------|--------------|------------|------|------------|------------|------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 6.75<br>26<br>Top | 7.37<br>26<br>gut. | 7.00<br>13 | 6.84 | 6.96<br>13 | 7.39<br>26<br>gut. | 6.81<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 8.41<br>26<br>Top | 9.08<br>26<br>gut. | 8.72<br>13 | 8.59 | 8.65<br>13 | 9.04<br>26<br>gut. | 8.33<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

325.46 - P 8.

325.46

10

Rods around Returns — 42<sup>nd</sup> + Myrtle

N.W. Ret - 23.2 around - 4 parts - 5.8 each

325.46 = P.10

|                                 |      |        |
|---------------------------------|------|--------|
| Beq. WL 42 <sup>nd</sup> + N.cb | 3.83 | Top    |
| Myrtle                          | 4.46 | gut.   |
| 5.8 E.                          | 3.89 | Top    |
| "                               | 4.59 | gut.   |
| "                               | 3.90 | Top    |
| "                               | 4.61 | gut.   |
| "                               | 3.90 | Top    |
| "                               | 4.58 | gut.   |
| 5.8 = end = N.L. Myrtle         | 3.88 | T-Top  |
| + W.cb. 42 <sup>nd</sup>        | 4.40 | G-gut. |

Note: Ret. in Poor Cond.

N.E. Ret 23.7 around - 4 parts - 5.9 each

Prop. to Prop - Ret in Poor Cond.

|                             |      |    |
|-----------------------------|------|----|
| Beq. N.L. Myrtle            | 3.78 | T  |
| "                           | 4.36 | g. |
| 5.9 S.                      | 3.78 | T  |
| "                           | 4.50 | g. |
| "                           | 3.79 | T  |
| "                           | 4.52 | g. |
| "                           | 3.79 | T  |
| "                           | 4.45 | g. |
| 5.9 = E.L. 42 <sup>nd</sup> | 3.82 | T  |
| "                           | 4.36 | g. |

S.E. Ret. - Prop. to Prop: 24.4 - 4 parts - 6.1

|                              |      |    |
|------------------------------|------|----|
| Beq. - E.L. 42 <sup>nd</sup> | 4.81 | T  |
| "                            | 5.36 | g. |
| G.I.W.                       | 4.89 | T  |
| "                            | 5.35 | g. |
| "                            | 4.81 | T  |
| "                            | 5.36 | g. |
| "                            | 4.90 | T  |
| "                            | 5.42 | g. |
| G.I. = S.L. Myrtle           | 4.91 | T  |
| "                            | 5.55 | g. |

Ret. in Poor Cond.

S.W. Ret. - 24' around - 4 - 6'

|                               |      |        |    |
|-------------------------------|------|--------|----|
| Beq. S.L. Myrtle              | 5.00 | 320.46 | T  |
| "                             | 5.60 | 319.86 | g. |
| G.N.                          | 4.85 | 320.61 | T  |
| "                             | 5.45 | 320.91 | g. |
| "                             | 4.79 | 320.67 | T  |
| "                             | 5.39 | 320.14 | g. |
| "                             | 4.78 | 320.66 | T. |
| "                             | 5.32 | 320.14 | g. |
| G = end: WL. 42 <sup>nd</sup> | 4.84 | 320.67 | T  |
| "                             | 5.57 | 319.95 | g. |

Ret. in Fair Cond.

Cont from P 8

broken out + needs replacing from Here - East  
 originally a Driveway for Both Alleys But cb. is  
 1+40.5 - end of cb. on Both sides - There was  
 1+40.5 - 27.5' Rt. = ± P. pole # P4225  
 1+40 = w.l. 20' Alley = End of walk on Lt.

1+10 - 25.7' Rt. = ± 11' Conc. Dr.

1+00

0+86 - 25.8' Rt. = ± 8' Broken cb.

0+75

0+70 - 25.8' Lt. = ± 6' Broken cb.

0+63 - 25.8' Lt. = ± 8' Conc. Dr.

0+57 - 25.8' Rt. = ± 10' Conc. Dr.

0+59.1 - Beg. walk on Lt.

0+53 - 28.4' Lt. = ± 6" Acacia

0+50

0+25

No walk on Lt.

X-Sect Myrtle 11

Lt.

Rt.

|                    |                                   |                               |                                    |                    |                    |                            |                                 |                                       |                                       |
|--------------------|-----------------------------------|-------------------------------|------------------------------------|--------------------|--------------------|----------------------------|---------------------------------|---------------------------------------|---------------------------------------|
| 321.0<br>1.5<br>40 | 321.04<br>1.73<br>25.9-Top end cb | 321.97<br>1.74<br>25.9<br>Top | 322.12<br>2.2<br>25.9<br>gut       | 322.3<br>2.3<br>13 | 322.2<br>2.3<br>13 | 323.2<br>2.7<br>13         | 322.8<br>3.1<br>25.8<br>94. Top | 322.88<br>2.58<br>25.8<br>Top end cb. | 322.86<br>2.58<br>25.8<br>Top end cb. |
|                    |                                   |                               |                                    |                    |                    |                            | 321.94<br>3.52<br>25.7<br>Dr.   | 322.65<br>2.81<br>33.1<br>walk        |                                       |
|                    | 321.14<br>2.32<br>2.6<br>Top      | 322.3<br>3.2<br>2.6<br>gut    | 322.4<br>3.1<br>13                 | 322.9<br>3.1<br>13 | 321.9<br>3.1<br>13 | 321.1<br>3.4<br>13         | 321.7<br>3.8<br>25.8<br>94      | 322.7<br>3.19<br>25.8<br>Top          |                                       |
|                    | 322.63<br>2.83<br>2.6<br>Top      | 321.9<br>3.6<br>2.6<br>gut    | 322.0<br>3.5<br>13                 | 321.9<br>3.6<br>13 | 321.7<br>3.8<br>13 | 321.2<br>4.3<br>25.8<br>94 | 321.75<br>3.71<br>25.8<br>Top   |                                       |                                       |
|                    | 322.63<br>2.83<br>33.1<br>walk    | 321.95<br>3.53<br>25.8<br>Dr. | 322.54<br>2.92<br>33.1<br>car walk | 321.9<br>3.1<br>13 | 321.6<br>3.9<br>13 | 321.5<br>4.0<br>13         | 320.93<br>4.53<br>25.8<br>Dr.   | 321.60<br>3.86<br>33.1<br>walk        |                                       |
| 322.7<br>2.8<br>40 | 322.2<br>3.24<br>25.9<br>Top      | 321.6<br>3.9<br>25.9<br>94    | 321.7<br>3.8<br>13                 | 321.6<br>3.9<br>13 | 321.5<br>4.0<br>13 | 320.8<br>4.7<br>25.8<br>94 | 321.36<br>4.10<br>25.8<br>Top   |                                       |                                       |
| 322.3<br>3.2<br>40 | 321.82<br>3.63<br>25.9<br>top     | 321.2<br>4.3<br>25.9<br>94    | 321.3<br>4.2<br>13                 | 321.2<br>4.3<br>13 | 321.0<br>4.5<br>13 | 320.5<br>5.0<br>25.9<br>94 | 320.94<br>4.52<br>25.9<br>Top   |                                       |                                       |

325.46

2+96 - 27.4' Rt. =  $\pm$  P. oak # 4249  
1+95

2+60 = Brk. in cb. on Lt.

2+53 - 29.7' Rt. =  $\pm$  4" Acacia

T.P. 5.37 330.12 0.71 324.75

2+24 = End. of Broken cb. on Lt.

2+00.5 = end of walk on Lt.

2+00

1+99 - 25.8' Rt. = end broken cb. on Rt.

1+62 - 27.1' Rt. =  $\pm$  F.H.

1+60 = E.L. Alley + Beg. walk on Lt.

1+41.5 = End of Walk on Rt.

|         |            |        |        |        |       |         |        |        |       |
|---------|------------|--------|--------|--------|-------|---------|--------|--------|-------|
| 326.1   | 325.74     | 325.0  | 325.3  | 325.5  | 325.1 | 324.6   | 325.27 | 325.3  | 325.9 |
| 4.0     | 4.38       | 5.1    | 4.8    | 4.6    | 5.0   | 5.5     | 4.85   | 4.8    | 4.2   |
| 40      | 25.9       | 25.9   | 13     | 13     | 25.9  | 25.9    | 25.9   | 35     | 40    |
|         | Top        | got.   |        |        | got.  | got.    | Top    |        |       |
| 325.7   | 325.6      | 324.5  | 325.0  | 325.2  | 324.7 | 324.2   | 324.6  | 324.9  | 325.7 |
| 4.4     | 1.60       | 5.6    | 5.1    | 4.9    | 5.4   | 5.9     | 5.26   | 5.2    | 4.4   |
| 40      | 26         | 26     | 13     | 13     | 28.8  | 25.8    | 25.8   | 35     | 40    |
|         | Top        | got.   |        |        | got.  | Top     |        |        |       |
|         |            |        |        | 330.12 |       |         |        |        |       |
| 324.2   | 324.83     | 324.0  | 324.6  | 324.7  | 324.1 | 323.6   | 324.24 | 324.8  |       |
| 0.3     | 0.63       | 1.5    | 0.9    | 0.8    | 1.4   | 1.9     | 1.22   | 0.7    |       |
| 40      | 25.9       | 25.9   | 13     | 13     | 25.9  | 25.9    | 40     | 40     |       |
|         | Top        | got.   |        |        | got.  | Top     |        |        |       |
| 324.83  | 324.77     |        |        |        |       |         |        |        |       |
| 0.63    | 0.69       |        |        |        |       |         |        |        |       |
| 38.1    | 33.1       |        |        |        |       |         |        |        |       |
| endwalk |            |        |        |        |       |         |        |        |       |
|         | 324.56     | 323.8  | 324.1  | 324.1  |       | 323.8   | 323.7  | 323.24 | 324.6 |
|         | 0.9        | 1.7    | 1.4    | 1.4    | 1.7   | 2.3     | 1.52   | 0.9    |       |
|         | 26         | 26     | 13     |        | 13    | 25.8    | 25.8   | 40     |       |
|         | Top broken | got.   |        |        |       | got.    | Top    |        |       |
|         | cb.        |        |        |        |       |         |        |        |       |
|         |            |        |        |        |       |         |        |        | 324.9 |
|         |            |        |        |        |       |         |        |        | 1.55  |
|         |            |        |        |        |       |         |        |        | 25.8  |
|         |            |        |        |        |       |         |        |        | Top   |
|         |            |        |        |        |       |         |        |        | cb.   |
| 324.6   | 324.37     | 324.24 | 324.09 | 323.6  | 323.6 | 323.5   | 323.2  | 322.7  | 322.3 |
| 0.9     | 1.09       | 1.22   | 1.37   | 1.9    | 1.9   | 2.0     | 2.3    | 2.8    | 2.2   |
| 40      | 38.1       | 33.1   | 25.9   | 25.9   | 13    | 13      | 26     | 30     | 40    |
|         |            | Top    | got.   |        |       |         |        |        |       |
|         |            | broken |        |        |       |         |        |        |       |
|         |            | cb.    |        |        |       |         |        |        |       |
|         |            |        |        |        |       |         |        |        |       |
|         |            |        |        |        |       | 322.16  |        | 322.2  |       |
|         |            |        |        |        |       | 2.30    |        | 2.24   |       |
|         |            |        |        |        |       | 33      |        | 38     |       |
|         |            |        |        |        |       | endwalk |        |        |       |

Cont. on P. 17

TP. on BM. 2.76 <sup>✓</sup> 328.85 4.03 <sup>✓</sup> 326.09 326.11 NW Van Dyke

80' E = EL Van Dyke - 0+00 ahead.  
= edge of H.C. Pave

66' E = F.cb

53' E.

40' E. = ±

27' E.

14' E. = W.cb.

Edge of H.C. Pave  
1+99.51 = W.L. Van Dyke also ± of 2' broken  
out cb. on Both sides

Lt.

Rt.

13

| Station | Top  | Gut  | Top    | Gut  | Top  | Gut    | Top  | Gut  | Top    | Gut  | Top  | Gut    | Top  | Gut | Top    | Gut  | Top | Gut    | Top  | Gut  | Top    | Gut  | Top  | Gut    | Top  | Gut  | Top    | Gut  | Top  | Gut    | Top  | Gut  |     |
|---------|------|------|--------|------|------|--------|------|------|--------|------|------|--------|------|-----|--------|------|-----|--------|------|------|--------|------|------|--------|------|------|--------|------|------|--------|------|------|-----|
| 326.09  | 4.08 | 26   | 325.81 | 4.71 | 26   | 325.91 | 4.51 | 13   | 325.64 | 4.48 | 13   | 325.43 | 4.69 | 13  | 325.07 | 5.05 | 26  | 325.8  | 4.3  | 40   | 325.84 | 4.28 | 40   | 325.86 | 4.26 | 40   | 325.86 | 4.26 | 40   | 325.86 | 4.26 | 40   |     |
| 326.10  | 4.02 | 40   | 325.55 | 4.57 | 40   | 325.47 | 4.65 | 26   | 325.47 | 4.65 | 13   | 325.34 | 4.80 | 13  | 325.25 | 4.87 | 13  | 325.20 | 4.92 | 26   | 325.07 | 5.15 | 40   | 325.07 | 4.58 | 40   | 325.07 | 4.58 | 40   | 325.07 | 4.58 | 40   |     |
|         | 4.17 | 40   |        | 4.30 | 26   |        | 4.39 | 13   |        | 4.56 | 13   |        | 4.64 | 13  |        | 4.63 | 26  |        | 4.76 | 40   |        |      |      |        |      |      |        |      |      |        |      |      |     |
|         | 4.02 | 40   |        | 4.15 | 26   |        | 4.26 | 13   |        | 4.33 | 13   |        | 4.47 | 13  |        | 4.53 | 26  |        | 4.68 | 40   |        |      |      |        |      |      |        |      |      |        |      |      |     |
|         | 4.15 | 40   |        | 4.20 | 26   |        | 4.23 | 13   |        | 4.31 | 13   |        | 4.55 | 13  |        | 4.75 | 26  |        | 4.94 | 40   |        |      |      |        |      |      |        |      |      |        |      |      |     |
| 326.06  | 4.06 | 40   | 325.59 | 4.53 | 40   | 325.71 | 4.41 | 26   | 325.83 | 4.29 | 13   | 325.79 | 4.33 | 13  | 325.52 | 4.60 | 13  | 325.18 | 4.94 | 26   | 324.89 | 5.23 | 40   | 325.52 | 4.60 | 40   | 325.52 | 4.60 | 40   | 325.52 | 4.60 | 40   |     |
| 325.31  | 3.75 | 38.1 | 325.21 | 3.91 | 37.8 | 325.09 | 4.13 | 25.8 | 325.42 | 4.70 | 25.8 | 325.6  | 4.51 | 13  | 325.17 | 4.63 | 13  | 325.09 | 5.02 | 25.8 | 325.10 | 4.58 | 25.8 | 325.54 | 4.44 | 32.9 | 325.66 | 4.35 | 38.2 | 325.66 | 4.35 | 38.2 |     |
|         | walk |      | Top    | Top  | Top  | Top    | Top  | Top  | Top    | Top  | Top  | Top    | Top  | Top | Top    | Top  | Top | Top    | Top  | Top  | Top    | Top  | Top  | Top    | Top  | Top  | Top    | Top  | Top  | Top    | Top  | Top  | Top |

330.12



Indexed  
a.s.k.

Lt. = W.      #

Rt. = E.      14

Levels on Van Dyke - 100' Each way from  
Prop Lines of Myrtle - 80' St. 14' cbs  
Paved. A.C.

1+00 = end.

0+50

0+25

0+00 = N.L. Myrtle

1+00 = S.L. Myrtle. - See P. 13 for Int.

0+75

0+50

0+00 = 100' S. of S.L. Myrtle on # Van Dyke

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 2.24<br>26<br>Top | 2.82<br>26<br>gut. | 2.42<br>13 | 2.23 | 2.41<br>13 | 2.78<br>26<br>gut. | 2.22<br>26<br>Top |
| 3.29<br>26<br>Top | 3.79<br>26<br>gut. | 3.34<br>13 | 3.18 | 3.34<br>13 | 3.70<br>26<br>gut. | 3.18<br>26<br>Top |
| 3.76<br>26<br>Top | 4.23<br>26<br>gut. | 3.79<br>13 | 3.65 | 3.82<br>13 | 4.21<br>26<br>gut. | 3.68<br>26<br>Top |
| 4.06<br>26<br>Top | 4.53<br>26<br>gut. | 4.15<br>13 | 4.02 | 4.17<br>13 | 4.57<br>26<br>gut. | 4.02<br>26<br>Top |
| 4.60<br>26<br>Top | 5.23<br>26<br>gut. | 4.94<br>13 | 4.68 | 4.76<br>13 | 5.15<br>26<br>gut. | 4.58<br>26<br>Top |
| 5.37<br>26<br>Top | 5.94<br>26<br>gut. | 5.00<br>13 | 5.38 | 5.50<br>13 | 5.79<br>26<br>gut. | 5.31<br>26<br>Top |
| 5.99<br>26<br>Top | 6.59<br>26<br>gut. | 6.26<br>13 | 6.01 | 6.18<br>13 | 6.53<br>26<br>gut. | 5.96<br>26<br>Top |
| 7.40<br>26<br>Top | 7.98<br>26<br>gut. | 7.67<br>13 | 7.44 | 7.52<br>13 | 7.92<br>26<br>gut. | 7.44<br>26<br>Top |

330.12

Rods Around Returns - Van Dyke + Myrtle  
 N.W. Ret. - from Prop. to prop. 239 ground - 4 - 6' each

330.12 - P. 14

|                                       |      |          |
|---------------------------------------|------|----------|
| Beq. W.L. Van Dyke +<br>N. cb. Myrtle | 4.13 | Top = T  |
|                                       | 4.69 | g = gut. |
| 6' E.                                 | 4.12 | T        |
|                                       | 4.50 | g.       |
| "                                     | 4.06 | T        |
|                                       | 4.50 | g.       |
|                                       | 4.02 | T        |
|                                       | 4.53 | g.       |
| 6' end = N.L. Myrtle                  | 4.05 | 4.52     |

Note: Ret. in Poor Cond.

N.E. Ret. - 239 ground - 4 - 6'

|                        |      |    |
|------------------------|------|----|
| Beq. N.L. Myrtle       | 4.02 | T. |
|                        | 4.57 | g. |
| 6' S.                  | 4.01 | T  |
|                        | 4.56 | g. |
| "                      | 4.05 | T  |
|                        | 4.62 | g. |
| "                      | 4.02 | T  |
|                        | 4.62 | g. |
| 6' end = E.L. Van Dyke | 4.07 | T  |
|                        | 4.71 | g. |

Ret. in poor Cond.

330.12

SE Ret. - 239 ground - 4 - 6'  
 Ret. in Very poor Cond. curb entirely broken out  
 on N. side. - See P. 2

|                               |      |                  |
|-------------------------------|------|------------------|
| Beq. E.L. Van Dyke            | 5.05 | No curb.<br>gut. |
| 17 W. = edge of Ret. - No cb. | 4.40 | 0.5' Lt. on Ret. |
|                               | 5.03 | g.               |
| 6' W. - No cb.                | 4.41 | 0.5' Lt. on Ret. |
|                               | 4.98 | g.               |
| 3.3' ahead. = end of cb.      | 4.52 | T                |
|                               | 4.95 | g.               |
| 6' = Ret.                     | 4.53 | T                |
|                               | 5.01 | g.               |
| "                             | 4.54 | T                |
|                               | 5.01 | g.               |
| 6' end = S.L. Myrtle          | 4.58 | T                |
|                               | 5.15 | g.               |

over

330.12

|                               |      |   |
|-------------------------------|------|---|
| S.W. Ret. 24" around - 4 - 6' |      |   |
| Beq. SL Myrtle                | 4.59 | T |
|                               | 5.23 | g |
| 6' N.                         | 4.60 | T |
|                               | 5.07 | g |
| 6' ±                          | 4.58 | T |
|                               | 5.06 | g |
| "                             | 4.53 | T |
|                               | 5.00 | g |
| 6' end. = WL Van Dyke         | 4.58 | T |
|                               | 5.03 | g |
| Ret. o.k.                     |      |   |

Cont. from P. 13

1+38 - 27.9' Rt. = # P pole # P 4275

1+04 - 26' Lt. = End. broken cb.

1+00

0+92 - 25.9' Lt. = Beg. Broken cb.

0+75

0+70 - End. of Walk on Lt.

0+50

0+36 - 26' Rt. = end. Broken cb.

0+25

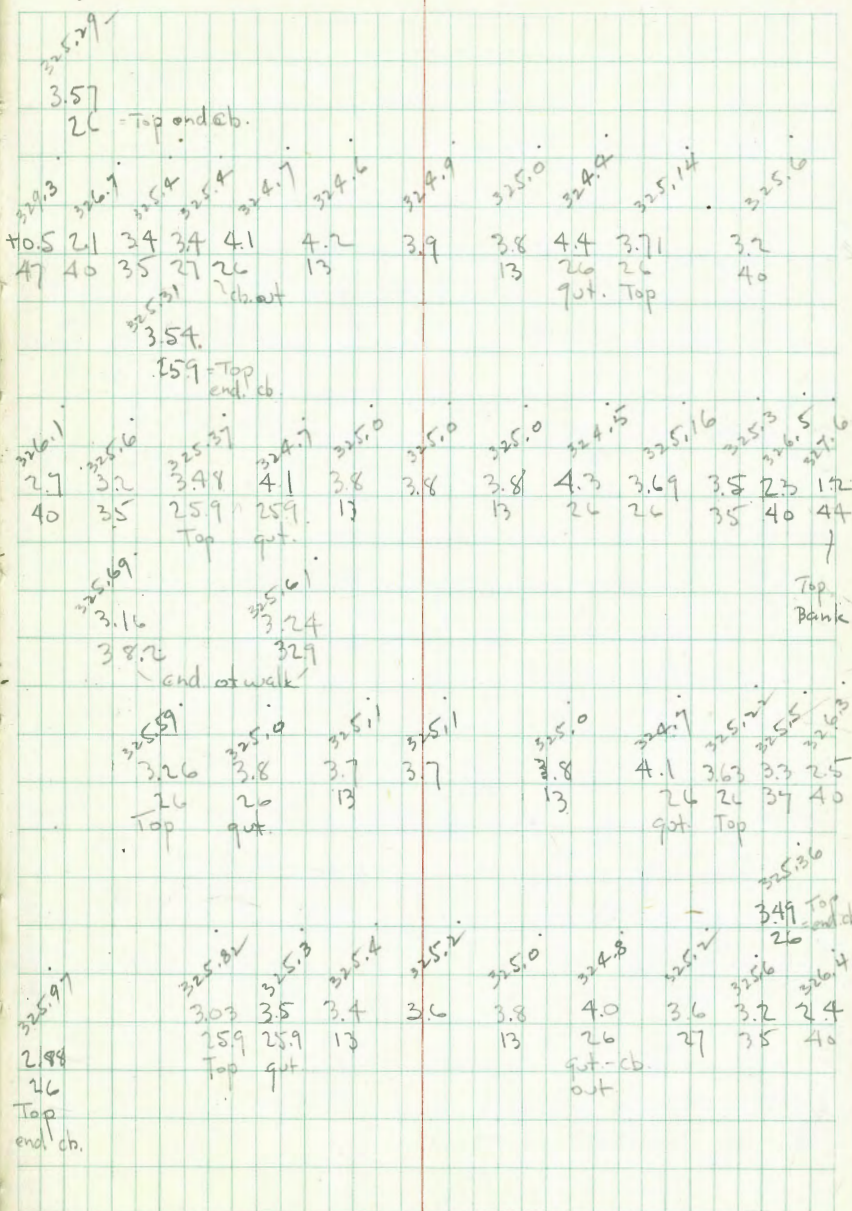
0+08 - 26' Lt. = end Broken cb.

0+00 = E.L. - Von Dyke - 26' Lt. = Beg. Broken curb.

Lt.

Rt.

17



324.85 - P 13

2+98-28.1 Rt. = ± P. pole # 4299

2+78 = Brk. in cb. on Lt.

2+45

2+40-26 Rt. = ± 9' Dirt Dr. to Gar. curb broken out

2+10

1+99 - End of walk on Lt.

1+80

1+72-259 Lt. = ± 3' broken cb.

1+61-28' Rt. = ± F.H.

T.P. 1.53 325.35 5.03 323.82

1+60 = E.L. Alley

1+40 = W.L. 20' Alley

Lt

Rt

|         |          |        |        |       |       |       |        |        |        |         |        |         |
|---------|----------|--------|--------|-------|-------|-------|--------|--------|--------|---------|--------|---------|
| 321.8   | 320.65   | 319.9  | 319.6  | 319.9 | 319.5 | 319.2 | 319.90 | 319.5  | 319.9  |         |        |         |
| 3.5     | 4.70     | 5.4    | 5.5    | 5.4   | 5.8   | 6.1   | 5.45   | 5.8    | 5.4    |         |        |         |
| 40      | 26       | 26     | 13     | 13    | 13    | 26    | 26     | 36     | 40     |         |        |         |
|         | Top      |        |        |       |       | gut.  | Top    |        |        |         |        |         |
| 322.3   | 321.77   | 321.0  | 321.0  | 321.1 | 320.7 | 320.5 | 321.17 | 321.1  | 321.6  |         |        |         |
| 3.0     | 3.54     | 4.3    | 4.3    | 4.2   | 4.6   | 4.8   | 4.18   | 4.2    | 3.7    |         |        |         |
| 40      | 26       | 26     | 13     | 13    | 13    | 26.1  | 26.1   | 35     | 40     |         |        |         |
|         | Top      | gut.   |        |       |       | gut.  | Top    |        |        |         |        |         |
| 322.11  | 322.97   | 322.1  | 322.3  | 322.5 | 322.0 | 321.8 | 322.55 | 322.4  | 322.3  |         |        |         |
| 2.2     | 2.38     | 3.2    | 3.0    | 2.8   | 3.3   | 3.5   | 2.80   | 2.9    | 2.0    |         |        |         |
| 40      | 26       | 26     | 13     | 13    | 13    | 26.1  | 26.1   | 32     | 40     |         |        |         |
|         | Top      | gut.   |        |       |       | gut.  | Top    |        |        |         |        |         |
| 323.59  | 323.40   |        |        |       |       |       |        |        |        |         |        |         |
| 1.76    | 1.95     |        |        |       |       |       |        |        |        |         |        |         |
| 38.3    | 33       |        |        |       |       |       |        |        |        |         |        |         |
|         | end walk |        |        |       |       |       |        |        |        |         |        |         |
|         | 324.01   | 323.5  | 323.8  | 323.9 | 323.5 | 323.0 | 323.76 | 323.3  | 324.6  |         |        |         |
|         | 1.34     | 1.8    | 1.5    | 1.4   | 1.8   | 2.3   | 1.59   | 2.0    | 0.7    |         |        |         |
|         | 25.9     | 25.9   | 13     | 13    | 13    | 26.1  | 26.1   | 33     | 40     |         |        |         |
|         | Top      | gut.   |        |       |       | gut.  | Top    |        |        |         |        |         |
|         | 324.95   | 325.4  | 324.53 | 324.1 | 324.4 | 324.5 | 324.3  | 324.0  | 324.51 | 325.4   | 324.83 |         |
| 3.90    | 3.4      | 4.32   | 4.7    | 4.4   | 4.3   | 4.5   | 4.8    | 4.34   | 3.4    | 4.02    |        |         |
| 40      | 40       | 26     | 26     | 13    |       | 13    |        | 25.9   | 25.9   | 40      | 40     |         |
| Top     | ground   | Top    | Rad.   | gut.  |       |       |        | gut.   | Top    | ground  | Top    | end cb. |
| end cb. |          |        |        |       |       |       |        | Rad    |        |         |        |         |
| 325.21  | 326.1    | 325.06 | 324.3  | 324.7 | 324.9 | 324.7 | 324.1  | 325.00 | 325.17 | 325.6   |        |         |
| 3.58    | 2.7      | 2.79   | 4.5    | 4.1   | 3.9   | 4.1   | 4.7    | 3.85   | 3.63   | 3.2     |        |         |
| 39.8    | 39.8     | 26     | 26     | 13    |       | 13    | 25.9   | 25.9   | 37.5   | 40      |        |         |
| Top     | ground   | Top    | gut.   |       |       |       | gut.   | Top    | Top    | end cb. |        |         |
| end cb. |          | Rad.   | Ret.   |       |       |       | Rad.   | Ret.   |        |         |        |         |

328.85

60' E = E.L. 43<sup>rd</sup> = 0+00 ahead.

⊥ NE. Ret.

66' E = E. cb.

53' E.

40' E = ⊥

27' E.

14' E = W. cb. - S. edge of FC. pave 40' Lt.

Rod on ⊥ of S.W. Ret.

2+99.25 = W.L. 43<sup>rd</sup>

Lt.

⊥

Rt.

|        |           |        |       |       |       |       |       |         |
|--------|-----------|--------|-------|-------|-------|-------|-------|---------|
| 319.4  | 319.70    | 318.9  | 319.0 | 319.1 | 319.1 | 319.2 | 319.8 | 319.5   |
| 4.9    | 5.57      | 6.4    | 6.3   | 6.2   | 6.2   | 6.1   | 5.5   | 6.0     |
| 40     | 25.8      | 25.8   | 13    |       | 13    | 24    | 27    | 40      |
|        | Top       | got.   |       |       |       |       |       |         |
| 319.70 | 319.26    | 318.7  | 318.7 | 318.7 | 318.8 | 318.9 | 318.4 |         |
| 5.52   | 6.09      | 6.6    | 6.6   | 6.6   | 6.5   | 6.4   | 6.9   |         |
| 40     | 40        | 26     | 13    |       | 13    | 26    | 40    |         |
| Top    | got.      |        |       |       |       |       |       |         |
|        | edge pave |        |       |       |       |       |       |         |
| 319.66 | 319.0     | 318.9  | 318.8 |       | 318.5 | 318.5 | 318.2 |         |
| 5.69   | 6.3       | 6.4    | 6.5   |       | 6.8   | 6.8   | 7.1   |         |
| 40     | 26        | 13     |       |       | 13    | 26    | 40    |         |
|        | edge pave |        |       |       |       |       |       |         |
| 319.75 | 319.4     | 319.1  | 319.0 | 318.8 | 318.9 | 318.6 |       |         |
| 5.60   | 5.9       | 6.2    | 6.3   | 6.5   | 6.4   | 6.7   |       |         |
| 40     | 26        | 13     |       | 13    | 26    | 40    |       |         |
|        | edge pave |        |       |       |       |       |       |         |
| 319.67 | 319.2     | 319.0  | 318.9 |       | 318.7 | 318.8 | 318.5 |         |
| 5.68   | 6.1       | 6.3    | 6.4   |       | 6.6   | 6.5   | 6.8   |         |
| 40     | 26        | 13     |       |       | 13    | 26    | 40    |         |
|        | edge pave |        |       |       |       |       |       |         |
| 319.55 | 319.16    | 318.8  | 318.9 | 318.8 | 318.5 | 318.6 | 318.4 | 318.61  |
| 5.80   | 6.19      | 6.5    | 6.4   | 6.5   | 6.8   | 6.7   | 6.9   | 6.74    |
| 40     | 40        | 26     | 13    |       | 13    | 26    | 40    | 40      |
| Top    | got.      |        |       |       |       | got.  | Top   |         |
|        |           |        |       |       |       |       |       | 318.72  |
|        |           |        |       |       |       |       |       | 6.43    |
|        |           |        |       |       |       |       |       | Top cb. |
|        |           |        |       |       |       |       |       | ⊥ Ret.  |
| 320.6  | 320.2     | 319.29 | 319.3 | 319.2 | 319.2 | 318.7 | 318.9 | 318.9   |
| 4.7    | 5.1       | 6.06   | 6.0   | 6.1   | 6.1   | 6.6   | 6.4   | 6.4     |
| 40     | 32        | 26     | 26    | 13    |       | 13    | 26    | 40      |
|        |           | Top    | got.  |       |       |       | got.  | Top     |
|        |           |        |       |       |       |       |       |         |
|        |           |        |       |       |       |       |       |         |

325.35

Indexed  
C.S.P.

Levels on 43<sup>rd</sup> - 100' Each way from  
Prop. Lines of Myrtle - 80' st. / 14' obs.

1+00 = end.

0+50

0+25

0+00 = N.L. Myrtle = S. edge of AC pave

See P. 19 for Int.

1+00 = S.L. Myrtle

0+75

0+72 - 20' Lt. = 8' broken cb.

0+50

0+00 = 100' S. of S.L. Myrtle on 43<sup>rd</sup>

W  
Lt. = E

Rt. = E 20

|              |                  |             |                 |                 |                  |            |
|--------------|------------------|-------------|-----------------|-----------------|------------------|------------|
| 104          | 180              | 150         | 139             | 152             | 186              | 113        |
| 30.7<br>walk | 26<br>9.4<br>Dr. | 13          |                 | 13              | 26<br>9.4        | 26<br>Top  |
| 321.21       | 321.42           |             | 321.77          |                 | 321.76           | 321.14     |
| 354          | 393              | 367         | 358             | 365             | 399              | 320        |
| 26<br>Top    | 26<br>gut        | 13          |                 | 13              | 26<br>9.4<br>Top | 26<br>Top  |
| 320.48       | 320.25           | 320.66      | 320.75          |                 | 320.71           | 320.29     |
| 4.87         | 5.10             | 4.69        | 4.60            | 4.64            | 5.03             | 4.26       |
| 26           | 26               | 13          |                 | 13              | 26<br>9.4<br>Top | 26<br>Top  |
|              | 319.58           | 319.10      | 319.67          | 319.75          | 319.66           | 319.40     |
| 47           | 56.6             | 57.5        | 58.0            | 6.19            | 56.8             | 56.0       |
| 40           | 35.7<br>end.walk | 35.7<br>Top | 26<br>26<br>Top | 26<br>26<br>gut | 13               | 56.9<br>13 |
|              | 318.61           | 318.2       | 318.5           | 318.6           | 318.2            | 318.4      |
| 6.4          | 6.74             | 6.9         | 6.8             | 6.7             | 7.1              | 6.9        |
|              | 26<br>Top        | 26<br>gut   | 13              |                 | 13               | 26         |
| 317.9        | 317.68           | 317.4       | 317.9           | 318.0           | 317.7            | 317.8      |
| 7.4          | 7.67             | 7.9         | 7.4             | 7.3             | 7.6              | 7.5        |
| 40           | 26<br>Top        | 26<br>gut   | 13              |                 | 13               | 26         |
| 317.0        | 316.70           | 316.6       | 317.1           | 317.1           | 316.8            | 317.1      |
| 8.3          | 8.68             | 8.7         | 8.2             | 8.2             | 8.5              | 8.2        |
| 40           | 26<br>Top        | 26<br>gut   | 13              |                 | 13               | 26         |
| 316.8        | 314.95           | 314.8       | 315.1           | 314.9           | 314.8            | 314.8      |
| 10.5         | 10.40            | 10.5        | 10.2            | 10.4            | 10.5             | 10.5       |
| 40           | 26<br>Top        | 26<br>gut   | 13              |                 | 13               | 26         |
|              | 315.3            | 315.3       | 314.3           |                 |                  |            |
|              | 10.0             | 10.0        | 11.0            |                 |                  |            |
|              | 36               | 36          | 40              |                 |                  |            |
|              | Top              | cb.         |                 |                 |                  |            |

325.35 P. 19

Cont. from P. 19

1+87 - Brk. in cb. on Lt. - Beg. good walk on Lt.

Conc. apron from floor extends over Reg. walk  
1+56 = 257 Lt. = 13' Conc. Dr. to Sing. Gar - Conc. floor

over the cb. - walk in poor Cond.  
1+45 = E.L. Alley - Ret. on Lt. is low - walk extends

is exposed.  
Broken down + Covered up - end of Ret. on Rt.  
1+25 = W.L. 20 Alley - cb. on Both sides are

1+24 - 27.8 Rt. = ± P. pole # P 4325

1+00

I.P. 11.98 334.30 3.03 322.32

0+60 = Brk. in cb. on Lt.

See P. 24 for tops of cbs. - dug out later.

0+25

X-Sect. Myrtle

21

| Lt.                  |               |                  |         |        | Rt.   |       |       |         |                 |
|----------------------|---------------|------------------|---------|--------|-------|-------|-------|---------|-----------------|
| 328.39               | 328.31        | 328.34           | 327.2   | 327.5  | 327.6 | 327.0 | 326.3 | 327.1   | 327.0           |
| 5.91                 | 5.99          | 5.96             | 7.1     | 6.8    | 6.7   | 7.3   | 4.0   | 7.19    | 7.3             |
| 37.8                 | 32.8          | 25.7             | 25.7    | 13     | 13    | 13    | 26.2  | 26.2    | 40              |
| Walk                 |               | Top              | Gut     |        |       |       | Gut   | Top     |                 |
| 327.20               | 326.59        | 326.10           | 325.86  |        |       |       |       |         |                 |
| 7.10                 | 7.71          | 7.60             | 8.44    |        |       |       |       |         |                 |
| 40                   | 34.0          | 32.9             | 25.7    |        |       |       |       |         |                 |
| Top of apron + floor | edge of apron | edge of sidewalk | Dr.     |        |       |       |       |         |                 |
| 324.1                | 323.6         | 325.16           | 324.01  | 325.69 | 325.1 | 325.7 | 325.2 | 324.9   | 325.39          |
| 10.2                 | 9.69          | 8.54             | 8.29    | 8.61   | 9.1   | 8.8   | 8.6   | 9.1     | 8.91            |
| 40                   | 39.6          | 39.9             | 32.9    | 26     | 26    | 13    | 13    | 26.2    | 26.2            |
| Top end cb.          |               | end of walk      | Top cb. | Gut    |       |       |       | Gut Top | Rad.            |
|                      |               |                  |         |        |       |       |       |         | Top end ret.    |
| 324.0                | 325.1         | 325.0            | 324.2   | 324.4  | 324.7 |       |       | 324.3   | 324.0           |
| 10.3                 | 9.2           | 9.3              | 10.1    | 9.9    | 9.6   |       |       | 10.0    | 10.3            |
| 40                   | 37            | 26               | 25      | 13     |       |       |       | 13      | 24              |
|                      |               |                  |         |        |       |       |       |         | 26              |
|                      |               |                  |         |        |       |       |       |         | 40              |
|                      |               |                  |         |        |       |       |       |         | Top-cb + ground |
| 324.0                | 323.7         | 323.0            | 323.3   | 323.5  |       |       |       | 323.1   | 322.6           |
| 10.3                 | 10.6          | 11.3             | 11.0    | 10.8   |       |       |       | 11.2    | 11.7            |
| 40                   | 26            | 24               | 13      |        |       |       |       | 13      | 23              |
|                      |               |                  |         |        |       |       |       |         | 26              |
|                      |               |                  |         |        |       |       |       |         | 40              |
| 322.6                | 322.33        | 321.2            | 321.7   | 321.8  | 321.3 | 320.9 | 321.2 | 321.4   |                 |
| 2.7                  | 3.02          | 4.1              | 3.6     | 3.5    | 4.0   | 4.6   | 4.1   | 3.9     |                 |
| 40                   | 25.7          | 25.7             | 13      |        | 13    | 23    | 26    | 40      |                 |
|                      | Top           | Gut              |         |        |       |       |       |         |                 |
| 321.3                | 320.88        | 320.8            | 320.1   | 320.3  | 320.0 | 319.8 | 320.1 | 320.0   |                 |
| 4.0                  | 4.47          | 5.5              | 5.2     | 5.0    | 5.3   | 5.5   | 5.2   | 5.3     |                 |
| 40                   | 25.8          | 25.8             | 13      |        | 13    | 23    | 26    | 40      |                 |
|                      | Top           | Gut              |         |        |       |       |       |         |                 |

325.35



check B.M.

2.29 326.08

Nw. Van Dyke  
326.09-P.13

I.P. 6.76 328.37 12.69 321.61

Nw. B.P.  
Myrtle  
Fairmount

B.M. 2.20 332.00

30' E = Fairmount

20' E

10' E = w. cb. Fairmount

2+68.90 = w.l. Fairmount + edge of H.C. Pave

2+53 = Brk. in cb. on Lt.

2+30

2+02-262 Rt. = 11' Conc. Dr.

Lt.

Rt.

Rt. 22

0.95 1.30 1.75 2.09 2.40 2.74 3.04 3.36 3.69 5.21  
90 65 40 26 13 13 26 40 90

1.34 1.76 2.18 2.41 2.61 2.86 3.16 3.53 3.94 5.23  
90 65 40 26 13 13 26 40 90

332.24 331.41 331.39 332.01 331.50 331.50 331.54 331.40 330.94 330.20 329.83 330.14 329.37 328.95  
204 189 241 229 274 280 276 290 336 410 447 388 593 533  
90 65 65 40 40 26 13 13 26 40 40 90 90 90  
gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top

331.91 331.29 331.27 331.20 330.72 330.17 330.42 330.50 330.57 330.9  
239 310 303 310 358 413 388 380 373 410  
257 257 13 13 26.3 26.3 30.7 35.7 40  
Top gut. Top gut. Top end. walk

331.21 3109 2571 Topcb.  
330.32 330.23 330.14 329.3 329.3 329.3 328.6 327.9 328.0 326.7  
398 407 416 50 50 50 57 64 550 5.6  
27.4 328 15.7 25.7 13 13 26.4 26.4 40  
walk Top gut. Top Top

327.14 327.11 327.29  
7.16 6.59 6.51  
26.2 33.2 40  
Dr. on Dr.

334.30

Levels around Returns on W. side of  
Fairmount at Myrtle.

334.30 - P. 22

N.W. Ret. 21.4 ground. - 4 parts 5.3 each

|                          |      |        |
|--------------------------|------|--------|
| Beq. W.L. Fairmount      | 2.39 | T=Top  |
|                          | 3.10 | g=gut. |
| 5.3 - E,                 | 2.42 | T      |
| "                        | 2.96 | g      |
| "                        | 2.40 | T      |
| "                        | 2.91 | g      |
| "                        | 2.35 | T      |
| "                        | 2.82 | g      |
| 5.3 = end. = N.L. Myrtle | 2.39 | T      |
|                          | 2.74 | g      |

S.W. Ret. - 19.8 ground. - 4 parts - 4.9

|                             |      |   |
|-----------------------------|------|---|
| Beq. S.L. Myrtle            | 3.88 | T |
|                             | 4.47 | g |
| 4.9 N.                      | 3.82 | T |
| "                           | 4.34 | g |
| "                           | 3.84 | T |
| "                           | 4.25 | g |
| "                           | 3.84 | T |
|                             | 4.10 | g |
| 4.9 = end. = W.L. Fairmount | 3.88 |   |
|                             | 4.12 |   |

Levels on Curbs found Covered up  
 From 43<sup>rd</sup> to Alley E. on Myrtle - for the  
 ground sections See P. 21  
 Used same stations

1+25 = W.L. Alley

1+00

0+60

0+25-

80' E. = E.L. 43<sup>rd</sup> = 0+00 ahead.

67.5' E. of W.L. 43<sup>rd</sup> - end of cb. on Ret. on Rt.

T.P. 3.78 326.10 322.32 T.P.-P.21

Lt. = N

⊕

Rt = S. 24

|  |   |  |  |
|--|---|--|--|
| 322.06<br>2.65<br>39 = end.<br>Ret. (broken) | 322.81<br>2.28<br>25.7<br>Top Rad.<br>Ret. (broken) | 322.12<br>2.68<br>26.2<br>Top Rad.<br>Ret. | 324.80<br>1.30<br>40<br>Top-end.         |
| 322.9<br>3.16<br>25.7<br>Top cb.             |   |  | 321.91<br>4.19<br>26.3<br>Top cb.        |
|  |   | 322.09<br>6.01<br>26.5<br>Top cb.          |  |
|  |   | 318.28<br>7.82<br>26.2<br>Top cb.          | 319.12<br>6.98<br>26.5<br>Top cb.        |
|  |   |  | 318.44<br>7.66<br>31.6<br>Top-end<br>Cb. |

326.10

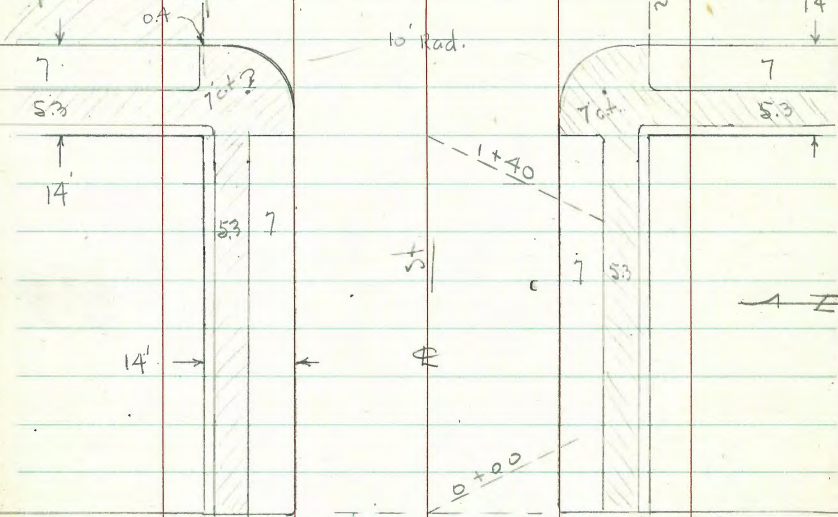


H.C. Pave  
To 115' N.

0+00  
on E. Main

6+00.72  
on E. - P. 51'

Marlborough 80'



St

R

Dwight

20' Alley

41<sup>st</sup> 80'

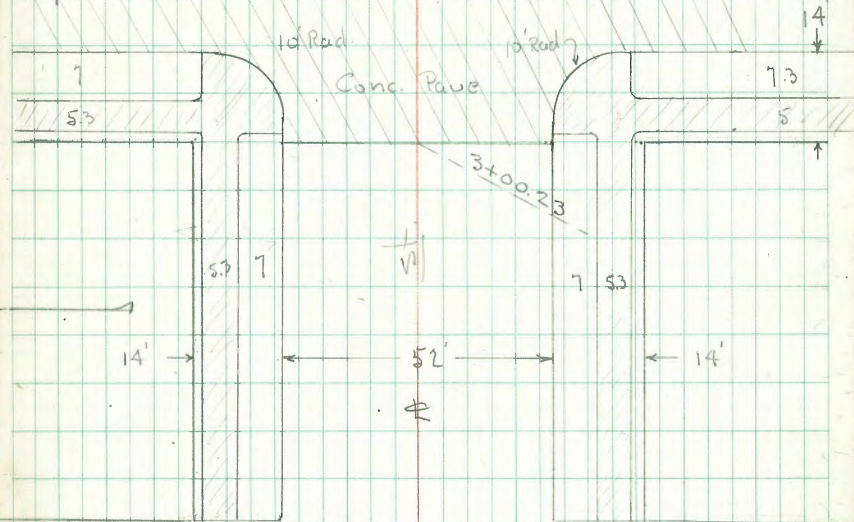
St.

X-Sect. Dwight - 41<sup>st</sup> to Fairmount

7.0 - 7-21-47 - W.O. 31385

42<sup>nd</sup> - 80'

St



10' Rad.

Conc. Pave

10' Rad.

St

R

Dwight

20' Alley

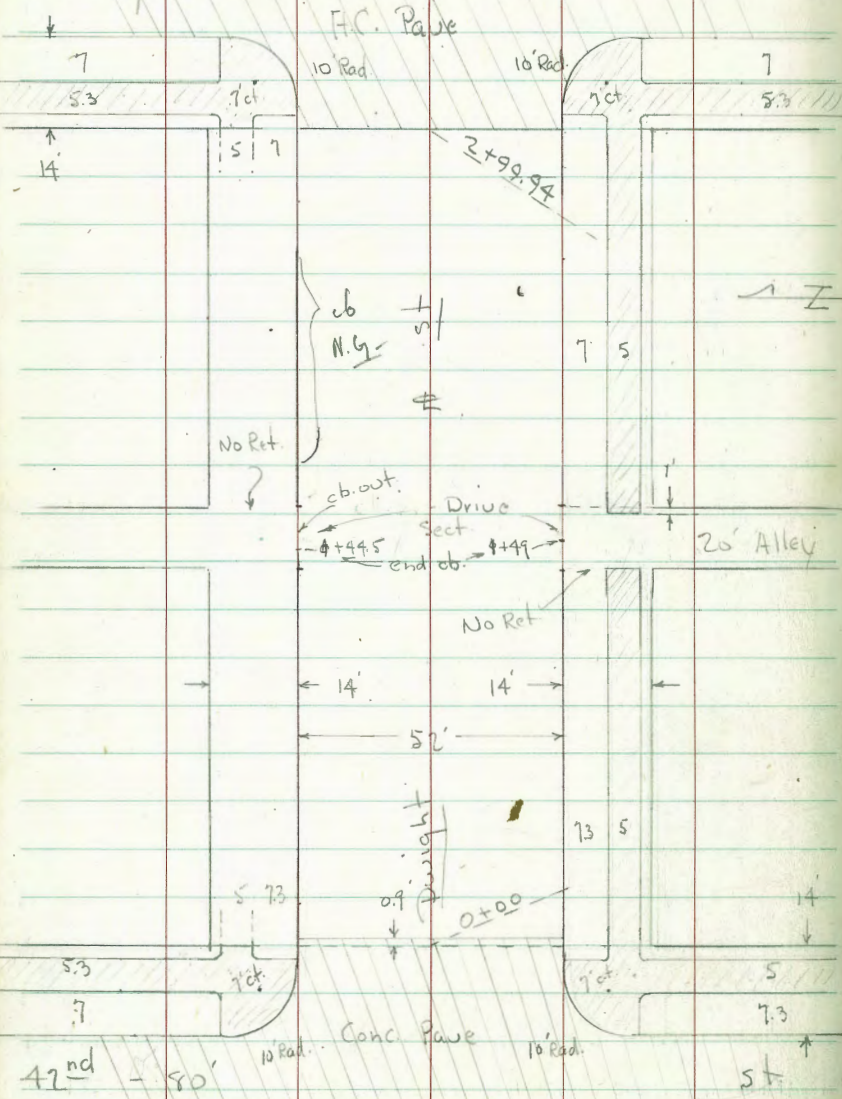
Marlborough 80'

St.

H.C. Pave

Van Dyke - 80'

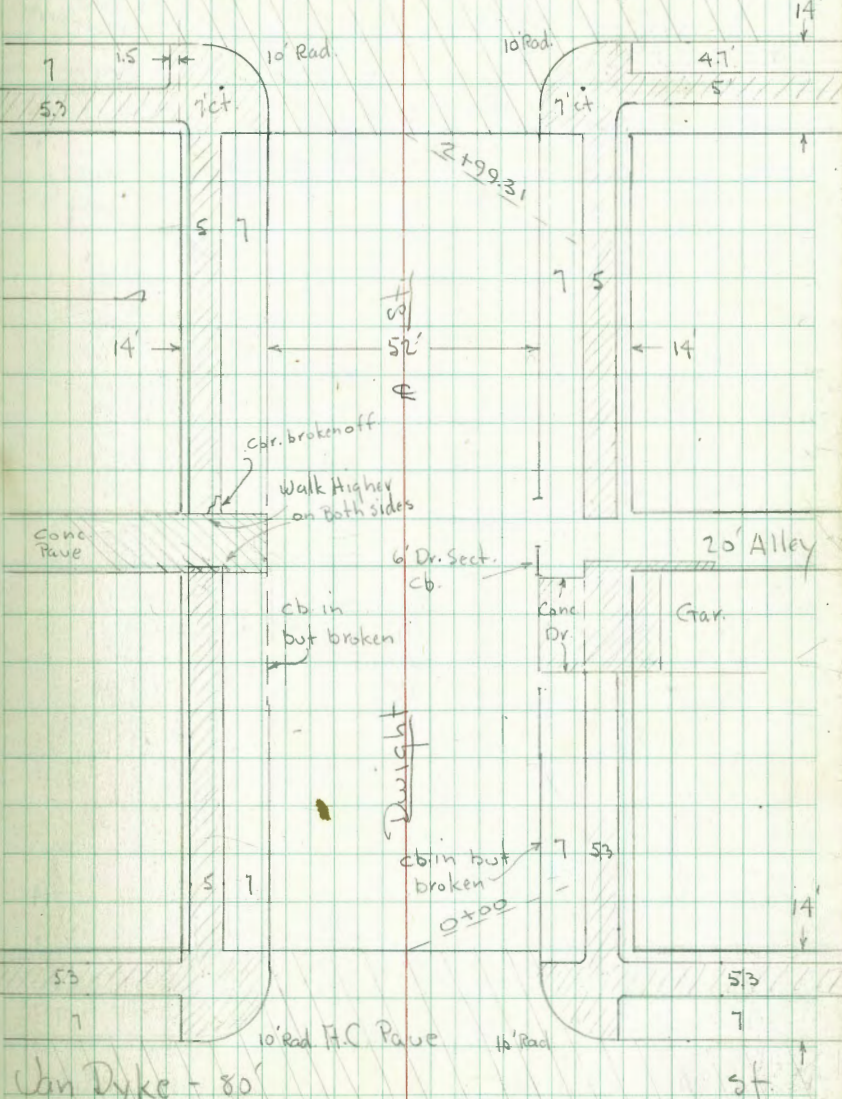
st.



43rd - 80'

H.C. Pave

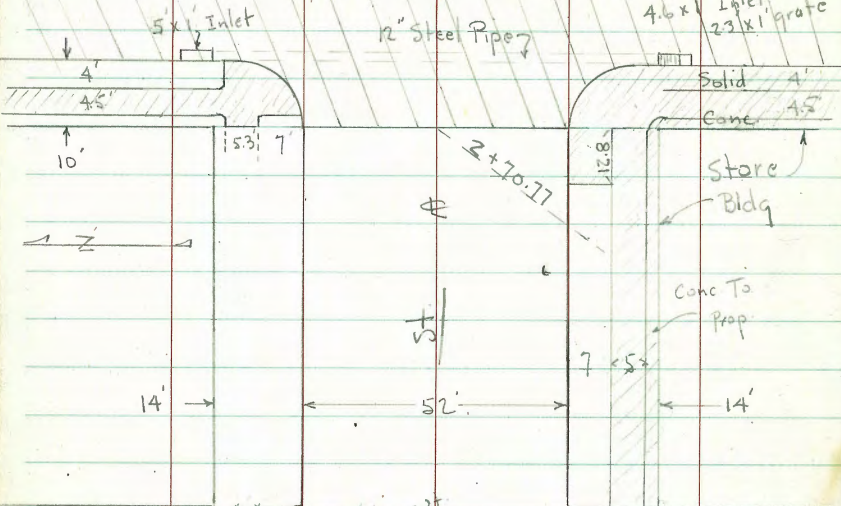
st.



Fairmount - 60' AC. Pavc

12" Steel Pipe

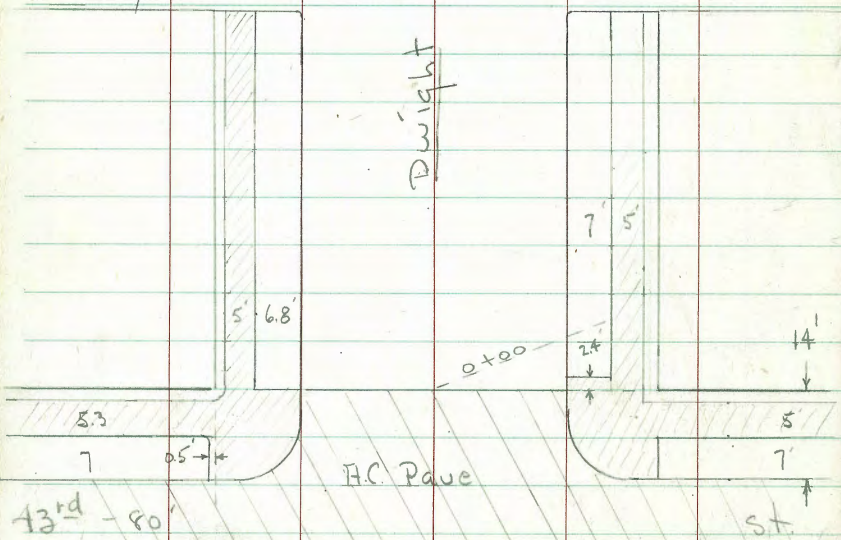
4.6 x 1 Inlet grate  
23 x 1 grate



20' Alley

Ret broken out

Dwight



13<sup>rd</sup> - 80'

AC. Pavc

st

Indexed  
C.S.R.

X-Sect. Dwight St. - from E.L. Alley  
E. of 41<sup>st</sup> to ± Fairmount.

80' st. 14' cbs. - See sketch - P. 26 for  
location of cbs. & walks.

0+90

0+74 - 26' Rt. = ± 9' Conc. Dr.

0+60

0+37 - 25.8' Lt. = ± 9' Conc. Dr.

0+30

0+06 - 26' Rt. = ± 10' Conc. Dr.

0+00 = E.L. of 20' Alley Bet. 41<sup>st</sup> & Marlborough.

B.M. 4.94 335.93

330.99

N.W.  
Marlborough  
& Dwight

7-21-47

70.

Lt. = N.

±

Rt. = S.

29

|           |                |       |       |       |        |            |
|-----------|----------------|-------|-------|-------|--------|------------|
| 330.07    | 330.2          | 330.2 | 330.6 | 330.2 | 329.6  | 330.24     |
| 5.06      | 5.7            | 5.5   | 5.3   | 5.7   | 6.3    | 5.69       |
| 25.9      | 25.9           | 13    |       | 13    | 26     | 26         |
| Top       | cut            |       |       | cut   | cut    | Top        |
|           |                |       |       |       | 329.68 | 330.30     |
|           |                |       |       |       | 6.25   | 5.63       |
|           |                |       |       |       | 26     | 33.1       |
|           |                |       |       |       | Dr.    | walk       |
| 330.12    | 330.2          | 330.2 | 330.5 | 330.1 | 329.5  | 330.13     |
| 5.21      | 5.7            | 5.7   | 5.4   | 5.8   | 6.4    | 5.80       |
| 25.8      | 25.8           | 13    |       | 13    | 26     | 26         |
| Top       | cut            |       |       |       | cut    | Top        |
| 330.2     | 330.09         |       |       |       |        |            |
| 5.11      | 5.84           |       |       |       |        |            |
| 33        | 25.8 = Dr.     |       |       |       |        |            |
| walk      |                |       |       |       |        |            |
| 330.56    | 330.3          | 330.1 | 330.2 | 329.9 | 329.5  | 330.05     |
| 5.37      | 5.6            | 5.8   | 5.7   | 6.0   | 6.4    | 5.88       |
| 25.7      | 25.7           | 13    |       | 13    | 26     | 26         |
| Top       | cut            |       |       |       | cut    | Top        |
|           |                |       |       |       | 329.42 | 330.04     |
|           |                |       |       |       | 6.51   | 5.89       |
|           |                |       |       |       | 26     | 33         |
|           |                |       |       |       | Dr.    | walk       |
| 330.63    | 330.47         | 330.1 | 330.2 | 330.1 | 329.9  | 329.4      |
| 5.30      | 5.46           | 5.8   | 5.7   | 5.8   | 6.0    | 6.5        |
| 40        | 26             | 26    | 13    |       | 13     | 26         |
| Top & cut | Top & Rad. cut |       |       |       | cut    | cut        |
| end. ret. |                |       |       |       |        | 26         |
|           |                |       |       |       |        | 26         |
|           |                |       |       |       |        | Top        |
|           |                |       |       |       |        | cut        |
|           |                |       |       |       |        | 2 Rad. Ret |
|           |                |       |       |       |        | 6.1        |
|           |                |       |       |       |        | 40         |
|           |                |       |       |       |        | 40         |
|           |                |       |       |       |        | Top        |
|           |                |       |       |       |        | cut        |
|           |                |       |       |       |        | end Ret    |
|           |                |       |       |       |        | 6.02       |
|           |                |       |       |       |        | 335.93     |



80' E. = E.L. Marlborough = 0+00 ahead.

66' E. = E. cb.

53' E.

40' E. = ⌀

27' E.

14' E. = W. cb.

1+40 = W.L. Marlborough

I.P. 4.62 335.61 4.94 330.99

1+20

30

|  | Lt.                    |                        |                      |  | Pt.                  |                      |                      |                      | Rt.                   |                       |                       |  |
|--|------------------------|------------------------|----------------------|--|----------------------|----------------------|----------------------|----------------------|-----------------------|-----------------------|-----------------------|--|
|  | <sup>330.97</sup> 4.64 | <sup>330.2</sup> 5.4   | <sup>330.0</sup> 5.6 |  | <sup>330.0</sup> 5.6 | <sup>329.8</sup> 5.8 | <sup>329.7</sup> 5.9 |                      | <sup>330.3</sup> 5.26 | <sup>330.5</sup> 5.26 |                       |  |
|  | Top 25.8               | put. 25.8              | 13                   |  | 13                   | 13                   | put. 25.9            |                      | 25.9                  | 25.9                  |                       |  |
|  | <sup>330.90</sup> 4.81 | <sup>330.01</sup> 5.54 | <sup>330.1</sup> 5.5 |  | <sup>330.2</sup> 5.4 | <sup>330.1</sup> 5.5 |                      | <sup>329.8</sup> 5.8 | <sup>329.8</sup> 6.2  | <sup>329.9</sup> 6.2  | <sup>330.5</sup> 5.26 |  |
|  | Top 40                 | put. 40                | 26                   |  | 13                   |                      | 13                   | 26                   | 26                    | 40                    | 40                    |  |
|  | <sup>330.93</sup> 4.68 | <sup>330.6</sup> 5.0   | <sup>330.5</sup> 5.1 |  | <sup>330.3</sup> 5.3 | <sup>330.1</sup> 5.5 |                      | <sup>329.8</sup> 5.8 | <sup>329.8</sup> 6.2  | <sup>329.8</sup> 6.2  | <sup>330.5</sup> 5.26 |  |
|  | edge pave. 40.3        | 26                     | 13                   |  | 13                   | 13                   | 26                   | 26                   | 40                    | 40                    |                       |  |
|  | <sup>331.11</sup> 4.50 | <sup>330.7</sup> 4.9   | <sup>330.5</sup> 5.1 |  | <sup>330.3</sup> 5.3 | <sup>330.1</sup> 5.5 |                      | <sup>330.0</sup> 5.6 | <sup>330.0</sup> 5.6  | <sup>329.7</sup> 5.9  | <sup>330.5</sup> 5.26 |  |
|  | edge pave. 40.7        | 26                     | 13                   |  | 13                   | 13                   | 26                   | 26                   | 40                    | 40                    |                       |  |
|  | <sup>330.91</sup> 4.70 | <sup>330.6</sup> 5.0   | <sup>330.4</sup> 5.2 |  | <sup>330.2</sup> 5.4 | <sup>330.0</sup> 5.6 |                      | <sup>329.9</sup> 5.7 | <sup>329.9</sup> 6.0  | <sup>329.6</sup> 6.0  | <sup>330.5</sup> 5.26 |  |
|  | edge pave. 40.5        | 26                     | 13                   |  | 13                   | 13                   | 26                   | 26                   | 40                    | 40                    |                       |  |
|  | <sup>330.94</sup> 4.67 | <sup>330.28</sup> 5.33 | <sup>330.0</sup> 5.6 |  | <sup>330.1</sup> 5.5 | <sup>330.0</sup> 5.6 |                      | <sup>329.9</sup> 6.2 | <sup>329.9</sup> 6.4  | <sup>329.8</sup> 5.63 | <sup>330.5</sup> 5.26 |  |
|  | Top 40                 | put. 40                | 26                   |  | 13                   | 13                   | 26                   | 26                   | 40                    | 40                    |                       |  |
|  |                        | on edge of pave        |                      |  |                      |                      |                      |                      |                       | cb                    |                       |  |
|  | <sup>330.87</sup> 4.74 | <sup>330.3</sup> 5.3   | <sup>330.3</sup> 5.3 |  | <sup>330.3</sup> 5.3 | <sup>330.0</sup> 5.6 |                      | <sup>329.7</sup> 5.9 | <sup>329.7</sup> 5.40 | <sup>330.2</sup> 5.40 | <sup>330.5</sup> 5.26 |  |
|  | Top 25.7               | put. 25.7              | 13                   |  | 13                   | 13                   | 25.9                 | put. 25.9            | 25.9                  | Top 25.9              |                       |  |
|  |                        |                        |                      |  |                      |                      |                      |                      |                       |                       |                       |  |
|  | <sup>330.94</sup> 4.99 | <sup>330.1</sup> 5.8   | <sup>330.5</sup> 5.4 |  | <sup>330.6</sup> 5.3 | <sup>330.1</sup> 5.8 |                      | <sup>329.8</sup> 6.3 | <sup>329.8</sup> 5.62 | <sup>330.3</sup> 5.62 | <sup>330.5</sup> 5.26 |  |
|  | Top 25.8               | put. 25.8              | 13                   |  | 13                   | 13                   | 24                   | put. 26              | 26                    | Top 26                |                       |  |
|  |                        |                        |                      |  |                      |                      |                      |                      |                       |                       |                       |  |
|  |                        |                        |                      |  |                      |                      |                      |                      |                       |                       |                       |  |
|  |                        |                        |                      |  |                      |                      |                      |                      |                       |                       |                       |  |

335.93

1+40 = WL. 20' Alley  
end cb. on Lt. leaning out.

1+00 - 1' W. of  $\pm$  9' Conc. Dr. on Rt. - 23'  
of 12" Corr. Iron pipe laying along gut at Drives

0+89 - 26' Rt. =  $\pm$  10' Conc. Dr.

Req. cb. on Lt. leaning out.

0+76 - 25.9 Lt. =  $\pm$  9' Conc. Dr.

0+66 - 25.8 Lt. =  $\pm$  9' Conc. Dr.

0+50

0+45 - 26' Rt. =  $\pm$  9' Conc. Dr.

0+43 - Brk. in cb. on Lt.

0+20

Lt.

$\pm$

Rt.

31

|                                     |  |                              |                    |                    |                             |                                    |   |                                     |
|-------------------------------------|--|------------------------------|--------------------|--------------------|-----------------------------|------------------------------------|---|-------------------------------------|
| 332.89<br>2.72<br>40<br>Top<br>gut. | 332.69<br>2.92<br>25.8<br>Top<br>2' read<br>gut. | 331.9<br>2.7<br>25.8<br>gut. | 332.0<br>3.6<br>13 | 332.0<br>3.6<br>13 | 331.8<br>3.8<br>13          | 331.6<br>4.0<br>26<br>gut.         | 332.06<br>3.55<br>26<br>Top<br>2' read. | 332.25<br>3.36<br>40<br>Top<br>gut. |
| 332.11<br>3.50<br>25.8              | 331.3<br>4.3<br>25.8<br>gut.                     | 331.3<br>4.3<br>13           | 331.6<br>4.0       |                    | 331.5<br>4.1<br>13          | 331.20<br>4.41<br>26<br>gut in Dr. | 331.10<br>3.91<br>33<br>walk            |                                     |
|                                     |  |                              |                    |                    | 331.17<br>4.44<br>26<br>Dr. | 331.61<br>4.00<br>33<br>walk       |   |                                     |
| 332.06<br>3.55<br>32.9<br>walk      | 331.69<br>3.92<br>25.9<br>Dr.                    | 331.0<br>4.6<br>13           | 331.9<br>4.2       | 331.1<br>4.5<br>13 | 331.0<br>4.6<br>26<br>gut   | 331.36<br>4.25<br>26<br>Top        |   |                                     |
| 331.96<br>3.65<br>32.9<br>walk      | 331.21<br>4.32<br>25.8<br>Dr.                    |                              |                    |                    |                             |                                    |   |                                     |
|                                     | 331.69<br>3.92<br>25.9<br>Top                    | 330.9<br>4.7<br>25.9<br>gut. | 330.7<br>4.9<br>13 | 331.1<br>4.5       | 330.9<br>4.7<br>13          | 330.5<br>5.1<br>26<br>gut          | 331.04<br>4.57<br>26<br>Top             |                                     |
| 331.61<br>4.00<br>25.9<br>Top       | 331.21<br>4.32<br>25.8<br>Dr.                    |                              |                    |                    |                             | 330.61<br>5.00<br>26<br>Dr.        | 331.04<br>4.57<br>33<br>walk            |                                     |
| 331.21<br>4.34<br>25.9<br>Top       | 330.3<br>5.3<br>25.9<br>gut.                     | 330.6<br>5.0<br>13           | 330.6<br>5.0       | 330.5<br>5.1<br>13 | 330.0<br>5.6<br>26<br>gut.  | 330.57<br>5.04<br>26<br>Top        |   |                                     |
|                                     |  |                              | 335.61             |                    |                             |                                    |   |                                     |

27'E

14'E = w. cb.

3+00.23 = w.L 4<sup>th</sup> + Edge of Conc. Pavc

T.P. 4.58 339.30 0.86 334.75

2+60

2+26

2+05 - 258' Lt. = Brk. in cb.

2+00 - 258' Lt. = ± 10' Conc. Dr.

1+83 = Brk. in cb. on Lt.

1+60 = E.L. Alley

|  | Lt.                                  |  |                                  |            | Rt.        |                     |                     |   |                                     |
|--|--------------------------------------|--|----------------------------------|------------|------------|---------------------|---------------------|---|-------------------------------------|
|  | 334.82                               | 334.73                                 | 334.65                           | 334.42     | 334.27     | 334.15              | 334.02              | 32  |                                     |
|  | 4.48<br>40                           | 4.57<br>26                             | 4.65<br>13                       | 4.88       | 5.03<br>13 | 5.15<br>26          | 5.28<br>40          |   |                                     |
|  | 334.80                               | 334.72                                 | 334.34                           | 334.35     | 334.28     | 334.05              | 333.74              | 334.07  |                                     |
|  | 4.50<br>40<br>Top                    | 4.98<br>40<br>gut                      | 4.96<br>26                       | 4.95<br>13 | 5.02       | 5.25<br>13          | 5.54<br>26          | 5.85<br>40<br>gut                             | 5.23<br>40<br>Top                   |
|  | 334.66                               | 334.11                                 | 334.29                           | 334.19     | 333.88     | 333.54              | 334.13              |   |                                     |
|  | 4.64<br>26<br>Top                    | 5.19<br>26<br>gut                      | 5.01<br>13                       | 5.11       | 5.42<br>13 | 5.76<br>25.9<br>gut | 5.17<br>25.9<br>Top |   |                                     |
|  | 334.12                               | 333.9                                  | 333.5                            | 334.30     | 333.6      | 333.4               | 332.1               | 333.69  |                                     |
|  | 1.97<br>25.9<br>Top                  | 2.6<br>25.9<br>gut                     | 2.1<br>13                        | 2.0        | 2.2<br>13  | 2.5                 | 2.8<br>25.8<br>gut  | 1.92<br>25.8<br>Top                           |                                     |
|  | 333.78                               | 332.8                                  | 332.9                            | 333.0      | 332.9      | 332.6               | 332.25              |   |                                     |
|  | 1.83<br>25.9<br>Top                  | 2.8<br>25.9<br>gut                     | 2.6<br>13                        | 2.6        | 2.7<br>13  | 3.0<br>25.8<br>gut  | 2.36<br>25.8<br>Top |   |                                     |
|  | 333.56                               | 332.66                                 | 332.90                           | 332.7      | 332.6      | 332.4               | 332.1               | 332.93  |                                     |
|  | 2.05<br>25.8<br>Top                  | 1.95<br>33<br>walk                     | 2.71<br>25.8<br>gut in<br>Dr.    | 2.9<br>13  | 3.0        | 3.2<br>13           | 3.5<br>25.9<br>gut  | 2.68<br>25.9<br>Top                           |                                     |
|  | 333.25                               | 332.99                                 | 332.1                            | 332.3      | 332.2      | 332.0               | 331.9               | 332.27  |                                     |
|  | 2.36<br>25.8<br>Top                  | 2.51<br>25.8<br>Top + gut<br>end. ret. | 3.5<br>25.8<br>Top + Rad.<br>gut | 3.3<br>13  | 3.4        | 3.6<br>13           | 3.7<br>26           | 3.34<br>26<br>Top + gut<br>2 Rad.<br>end. Ret | 3.00<br>40<br>Top + gut<br>end. Ret |
|  | 333.19                               | 332.99                                 | 332.1                            | 332.3      | 332.2      | 332.0               | 331.9               | 332.27  |                                     |
|  | 2.51<br>40<br>Top + gut<br>end. ret. | 2.62<br>25.8<br>Top + Rad.<br>gut      | 3.5<br>25.8<br>Top + Rad.<br>gut | 3.3<br>13  | 3.4        | 3.6<br>13           | 3.7<br>26           | 3.34<br>26<br>Top + gut<br>2 Rad.<br>end. Ret | 3.00<br>40<br>Top + gut<br>end. Ret |



indexed  
O.S.R.

Levels on 42<sup>nd</sup> - 100' Each way from  
Prop. Lines of Dwight - Paved - Conc.

80' St 14' cbs.

1+00 = 100' N. of N.L.

0+50

0+25

0+00 = N.L. Dwight.

1+00 = S.L. Dwight. - P 32 + 33 for Int.

0+75

0+50

0+00 = 100' S. of S.L. Dwight.

Lt. = W

±

Rt. = E 34

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 3.47 | 3.90 | 2.43 | 3.36 | 3.62 | 4.04 | 3.43 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 4.09 | 4.50 | 4.06 | 3.79 | 4.12 | 4.58 | 4.00 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 4.44 | 4.82 | 4.31 | 4.26 | 4.44 | 4.85 | 4.42 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 4.50 | 4.98 | 4.48 | 4.39 | 4.61 | 5.12 | 4.69 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 5.23 | 5.86 | 5.29 | 5.17 | 5.38 | 5.88 | 5.21 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. |      |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 5.76 | 6.32 | 5.83 | 5.66 | 5.90 | 6.32 | 5.76 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 6.32 | 6.83 | 6.38 | 6.28 | 6.35 | 6.89 | 6.30 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 7.27 | 7.83 | 7.42 | 7.35 | 7.46 | 7.87 | 7.23 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

339.30

Levels around Returns - Dwight + 42<sup>nd</sup>

339.30 - P. 34

N.W. Ret. - 24' around - 4 parts - 6'

Req. W.L. 42<sup>nd</sup> 4.64 T = Top

5.19 q = gut.

6' E. 4.63 T

5.18 q

+ 4.5 = cb. broken out 4.65 T

5.10 q

+ 6 = ± Ret. - .5 Lt = edge Ret. 4.57 T

5.09 q

+ 3' = end. cb. broken 4.54 T

5.08 q

+ 6 = 3/4 4.43 T

5.02 q

6 = end. = N.L. Dwight 4.50 T

4.98 q

Ret. in poor Cond.

N.E. Ret. - 23.7' around - 4 - 5.9

Req. N.L. Dwight 4.69 T

5.12 q

6' S. 4.67 T

5.21 q

" 4.69 T

5.26 q

339.30

35

6' - 4.70 T

5.23 q

6' = end. = E.L. 42<sup>nd</sup> 4.63 T

gut. = 0.9 E. 5.22 q

Ret. in poor Cond.

S.E. Ret. 24' around - 4 - 6'

Req. E.L. 42<sup>nd</sup> 5.18 T

5.70 q

6' W. 5.12 T

5.68 q

" 5.10 T

5.73 q

" 5.17 T

5.83 q

6 = end. = S.L. Dwight. 5.21 T

5.89 q

Ret. in poor Cond.

S.W. Ret. - 24' around - 4 - 6'

Req. S.L. Dwight. 5.23 T

5.87 q

6' N. 5.18 T

5.77 q

" 5.15 T

5.70 q

S.W. Cont.

339.30

6-3/4

5.18

T.

5.69

9

6-End. = W.L. 4<sup>2nd</sup>

5.18

T

5.77

9.

Ret. in Poor Cond.

Cont. from P. 33

1+62 - 273 Rt. = ± F.H.

1+60 = E.L. Alley - Beg. cb. on Lt

1+59 = End. of cb. + walk on Rt.

1+49 = end of cb. - Dr. Sect. on Rt.

1+445 = .end of cb. - Drive Sect. on Lt.

sides - Some broken out on Both sides

The curb makes like a Drive. across Alley on Both

1+40 = w.L. 20' Alley - No Returns at Alley -

1+39 - 273 Rt. = ± P. pole # P 4225

1+15

1+10 - 259 Rt. = ± 7.5' Dirt Dr. - cb. broken out -

0+94 - 258 Lt. = Brk. in cb.

0+89 - 259 Lt. = ± 9' Conc. Dr.

0+80

Lt

±

Rt.

Dwight  
X-587

|             |         |            |       |       |       |         |          |          |         |       |
|-------------|---------|------------|-------|-------|-------|---------|----------|----------|---------|-------|
| 336.2       | 335.97  | 335.3      | 335.4 | 335.5 | 335.5 | 335.1   | 335.49   | 335.78   | 335.94  | 335.9 |
| 4.1         | 4.29    | 5.0        | 4.9   | 4.8   | 4.8   | 5.2     | 4.77     | 4.48     | 4.32    | 4.4   |
| 40          | 26      | 26         | 13    |       | 13    | 26      | 26       | 33       | 38      | 40    |
|             | Top-end | cut        |       |       |       | cut     | Top      | walk     |         |       |
|             | cb.     |            |       |       |       |         |          |          |         |       |
|             |         |            |       |       |       | 335.46  | 335.76   | 335.93   |         |       |
|             |         |            |       |       |       | 4.80    | 4.50     | 4.33     |         |       |
|             |         |            |       |       |       | 26      | 33       | 38       |         |       |
|             |         |            |       |       |       | end cb. | end walk |          |         |       |
| 335.13      |         |            |       |       |       |         |          |          | 334.97  |       |
| 5.13        |         |            |       |       |       |         |          |          | 5.29    |       |
| 26          |         |            |       |       |       |         |          |          | 26      |       |
| Top cb.     |         |            |       |       |       |         |          |          | Top-end |       |
| in Dr.      |         |            |       |       |       |         |          |          | in Dr.  |       |
| 336.1       | 335.75  | 335.3      | 335.3 | 335.3 | 335.3 | 334.9   | 335.39   | 335.64   | 335.72  | 335.8 |
| 4.2         | 4.51    | 5.0        | 5.0   | 5.0   | 5.0   | 5.4     | 4.87     | 4.62     | 4.54    | 4.5   |
| 40          | 26      | 26         | 13    |       | 13    | 25.9    | 25.9     | 133      | 38      | 40    |
|             | Top-end | cut        |       |       |       | cut     | Top      | end walk |         |       |
|             | cb.     |            |       |       |       |         | end cb.  |          |         |       |
|             |         |            |       |       |       |         | Req. Dr. |          |         |       |
| 336.0       | 335.49  | 334.9      | 334.9 | 335.0 |       | 334.8   | 334.7    | 335.19   |         |       |
| 4.3         | 4.77    | 5.4        | 5.4   | 5.3   |       | 5.5     | 5.6      | 5.07     |         |       |
| 40          | 25.9    | 25.9       | 13    |       |       | 13      | 25.9     | 25.9     |         |       |
|             | Top     | cut        |       |       |       |         | cut      | Top      |         |       |
|             |         |            |       |       |       |         |          |          |         |       |
| 335.36      |         |            |       |       |       |         |          | 335.40   |         |       |
| 4.90        |         |            |       |       |       |         |          | 4.86     |         |       |
| 25.8        |         |            |       |       |       |         |          | 33       |         |       |
| Top         |         |            |       |       |       |         |          | on walk  |         |       |
| cb.         |         |            |       |       |       |         |          | (Broken) |         |       |
| 335.57      |         | 334.73     |       |       |       |         |          |          |         |       |
| 4.69        |         | 5.53       |       |       |       |         |          |          |         |       |
| 33          |         | 25.9 = Dr. |       |       |       |         |          |          |         |       |
| edge of Dr. |         |            |       |       |       |         |          |          |         |       |
| End.        |         |            |       |       |       |         |          |          |         |       |
| 335.7       | 335.17  | 334.9      | 334.7 | 334.7 |       | 334.5   | 334.4    | 334.33   |         |       |
| 4.6         | 5.09    | 5.4        | 5.6   | 5.6   |       | 5.8     | 5.9      | 5.43     |         |       |
| 40          | 25.9    | 25.9       | 13    |       |       | 13      | 25.9     | 25.9     |         |       |
|             | Top     | cut        |       |       |       |         | cut      | Top      |         |       |

340.26 - P. 33



LT.

⊕

RT.

38

2+99.94 = W.L. Van Dyke - edge of AC Pave

NW Van Dyke

TP. 4.74 342.00 3.00 337.26 337.27

2+81 - End Broken cb. on Rt.

2+65 - end Broken cb. on Lt. ✓

2+25

2+20 = Ely Conc. Dr. on Lt.

2+19 - 25.9 Rt. = Beg Broken cb.

2+05 - 25.8' Lt. = Wly. Conc. Dr. - Back to prop.

2+08 - 26' Rt. = Brk. in cb.

1+99 - 26' Rt. = ⊕ 10' Conc. Dr.

1+90

1+80 - Beg Broken cb. on Lt.

0+66 - 25.9 Rt. = Brk. in cb.

| Station | LT. (ft) | RT. (ft) | Notes                          |
|---------|----------|----------|--------------------------------|
| 2+99.94 | 4.52     | 5.24     | edge of AC Pave                |
| 2+81    | 4.72     | 5.24     | End Broken cb. on Rt.          |
| 2+65    | 4.1      | 3.62     | end Broken cb. on Lt. ✓        |
| 2+25    | 4.5      | 3.94     |                                |
| 2+20    | 4.5      | 3.94     | Ely Conc. Dr. on Lt.           |
| 2+19    | 4.5      | 3.94     | Beg Broken cb.                 |
| 2+05    | 4.67     | 4.16     | Wly. Conc. Dr. - Back to prop. |
| 2+08    | 4.67     | 4.16     | Brk. in cb.                    |
| 1+99    | 4.67     | 4.16     | ⊕ 10' Conc. Dr.                |
| 1+90    | 4.7      | 4.16     |                                |
| 1+80    | 4.7      | 4.16     | Beg Broken cb. on Lt.          |
| 0+66    | 4.7      | 4.16     | Brk. in cb.                    |

342.00 ✓

340.26

Cont. on P. 42

0+50 - 25.8 Lt. = ± 14 Conc. Dr.

0+25

T.P. 5.48 342.74 4.74 337.26

Curb on Rt. in poor cond. from Here to Alley  
80' E = E.L. Van Dyke = 0+00 ahead = edge H.C. Pav.

66' E = E. cb.

53' E.

40' E = Φ

27' E.

14' E = W. cb.

|                     | Lt.                 | ±          | Rt.                 |
|---------------------|---------------------|------------|---------------------|
| 338.15              | 337.31              |            |                     |
| 4.89<br>33<br>walk  | 5.43<br>25.8<br>Dr. |            |                     |
| 337.17              | 337.1               | 337.0      | 337.2               |
| 4.97<br>25.9<br>Top | 5.6<br>25.9<br>Cut  | 5.7<br>13  | 5.5                 |
|                     |                     |            | 336.9               |
|                     |                     |            | 5.8<br>13           |
|                     |                     |            | 336.7               |
|                     |                     |            | 6.0<br>25.9<br>Cut  |
|                     |                     |            | 5.60<br>15.9<br>Top |
|                     |                     |            | 337.4               |
|                     |                     |            | 342.74 ✓            |
| 337.64              | 337.06              | 337.08     | 336.92              |
| 4.36<br>25.9<br>Top | 4.94<br>25.9<br>Cut | 4.92<br>13 | 337.07              |
|                     |                     |            | 5.08<br>13          |
|                     |                     |            | 336.65              |
|                     |                     |            | 5.35<br>25.8<br>Cut |
|                     |                     |            | 4.95<br>25.8<br>Top |
|                     |                     |            | 337.05              |
| 337.65              | 337.01              | 336.90     | 336.88              |
| 4.35<br>40<br>Top   | 4.99<br>40<br>Cut   | 5.10<br>26 | 5.20<br>13          |
|                     |                     |            | 336.67              |
|                     |                     |            | 5.33                |
|                     |                     |            | 336.56              |
|                     |                     |            | 5.44<br>13          |
|                     |                     |            | 336.78              |
|                     |                     |            | 5.52<br>26          |
|                     |                     |            | 336.31              |
|                     |                     |            | 5.69<br>40<br>Cut   |
|                     |                     |            | 4.97<br>40<br>Top   |
|                     |                     |            | 337.03              |
| 337.32              | 337.09              | 337.00     | 336.87              |
| 4.68<br>40          | 4.91<br>26          | 5.00<br>13 | 5.13                |
|                     |                     |            | 336.88              |
|                     |                     |            | 5.12<br>13          |
|                     |                     |            | 336.70              |
|                     |                     |            | 5.30<br>26          |
|                     |                     |            | 336.60              |
|                     |                     |            | 5.40<br>40          |
| 337.41              | 337.24              | 337.03     | 337.02              |
| 4.59<br>40          | 4.76<br>26          | 4.92<br>13 | 4.98                |
|                     |                     |            | 336.94              |
|                     |                     |            | 5.06<br>13          |
|                     |                     |            | 336.86              |
|                     |                     |            | 5.14<br>26          |
|                     |                     |            | 336.76              |
|                     |                     |            | 5.24<br>40          |
| 337.24              | 337.10              | 336.91     | 336.82              |
| 4.78<br>40          | 4.90<br>26          | 5.09<br>13 | 5.18                |
|                     |                     |            | 336.65              |
|                     |                     |            | 5.35<br>13          |
|                     |                     |            | 336.60              |
|                     |                     |            | 5.40<br>26          |
|                     |                     |            | 336.47              |
|                     |                     |            | 5.53<br>40          |
| 337.17              | 336.76              | 336.67     | 336.47              |
| 4.83<br>40<br>Top   | 5.30<br>40<br>Cut   | 5.33<br>26 | 5.53<br>13          |
|                     |                     |            | 336.39              |
|                     |                     |            | 5.61                |
|                     |                     |            | 336.29              |
|                     |                     |            | 5.71<br>13          |
|                     |                     |            | 336.23              |
|                     |                     |            | 5.77<br>26          |
|                     |                     |            | 336.97              |
|                     |                     |            | 6.03<br>40<br>Cut   |
|                     |                     |            | 5.26<br>40<br>Top   |
|                     |                     |            | 336.72              |
|                     |                     |            | 342.00              |

indexed  
C.S.R.

Levels on Van Dyke - 100' Each way from  
Prop Line Dwight. - 80' st. 14' obs. Paved - A.C.

1+00 = 100' N. of N.L.

0+50

0+25

0+00 = N.L. Dwight.

1+00 = S.L. Dwight. - for Int. See P. 39

0+75

0+50

0+00 = 100' S. of S.L. Dwight

LT. = W.

RT = E. 40

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 3.64 | 4.18 | 3.67 | 3.37 | 3.41 | 3.85 | 3.30 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 4.26 | 4.76 | 4.32 | 4.02 | 4.04 | 4.40 | 3.74 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 4.57 | 5.10 | 4.58 | 4.30 | 4.39 | 4.72 | 4.12 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 4.83 | 5.30 | 4.78 | 4.59 | 4.68 | 4.99 | 4.25 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
|      | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 5.26 | 6.03 | 5.53 | 5.24 | 5.40 | 5.69 | 4.97 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 5.73 | 6.30 | 5.89 | 5.66 | 5.76 | 6.03 | 5.46 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|
| 6.16 | 6.72 | 6.28 | 6.11 | 6.20 | 6.52 | 5.88 |
| 26   | 26   | 13   |      | 13   | 26   | 26   |
| Top  | gut. |      |      |      | gut. | Top  |

|      |      |      |      |      |            |
|------|------|------|------|------|------------|
| 7.08 | 7.63 | 7.16 | 6.93 | 7.03 | 7.40       |
| 26   | 26   | 13   |      | 13   | 26         |
| Top  | gut. |      |      |      | gut in Dr. |

342.00 P. 39

342.00 P.40

Levels around Returns - Van Dyke + Dwight

N.W. Ret. - 24' around - 4 parts - 6'

Beg W.L. Van Dyke 4.89 T=Top

5.33 q=got.

W.E. 4.90 T

5.32 q

" 4.86 T

5.29 q

" 4.82 T

5.30 q

6'-end = N.L. Dwight. 4.82 T

5.30 q

Ret. in Good Cond.

N.E. Ret. - 23.8 around. 4 - 5.9

Beg N.L. Dwight 4.35 T

5.00 q

59' S 4.39 T

5.03 q

" 4.41 T

5.03 q

" 4.47 T

5.01 q

59' = end = E.L. Van Dyke 4.36 T

4.94 q

Ret. in Fair Cond.

T = 342.00

41

S.E. Ret. - 23.8 around - 4 - 5.9

Beg E.L. Van Dyke 4.95 T

5.35 q

59 W. 5.04 T

5.41 q

4.93 T

5.52 q

4.97 T

5.58 q

59'-end = S.L. Dwight. 4.98 T

5.70 q

Ret. in Fair Cond.

SW Ret - 24' around - 4 - 6'

Beg S.L. Dwight 5.26 T

6.03 q

6 N. 5.31 T

5.88 q

" 5.34 T

5.80 q

" 5.78 T

5.70 q

6'-end = W.L. Van Dyke 5.24 T

5.80 q

Ret. in Poor Cond.

Cont. from P. 39

7-25-47

70.

Lt.

R

Rt.

42

1+44 = end of cb. - Dr. sect. in Alley

1+40.8 = end of walk on Rt. + Conc Dr.

1+40.6 = end of walk on Lt.

Lt. extends over pave

Pave on Lt. extends out to cb. line - walk on

1+40 = w.l. 20' Alley - No Returns. - Alley Conc.

1+39 = 27.2 Rt. =  $\Phi$  P. pale # P 4275

1+38 = 29.2 Lt. =  $\Phi$  18" Acacia - for alley - on Rt. Beg. cb. - Drive Sect.

1+37.5 = 25.8 Rt. = Ely. Conc. Dr.

1+12 = Beg. cb. broken on Lt.

1+11 = 15.8 Rt. = Wly. Conc. Dr.

1+03 = 25.8 Rt. = cb. completely broken out

1+00

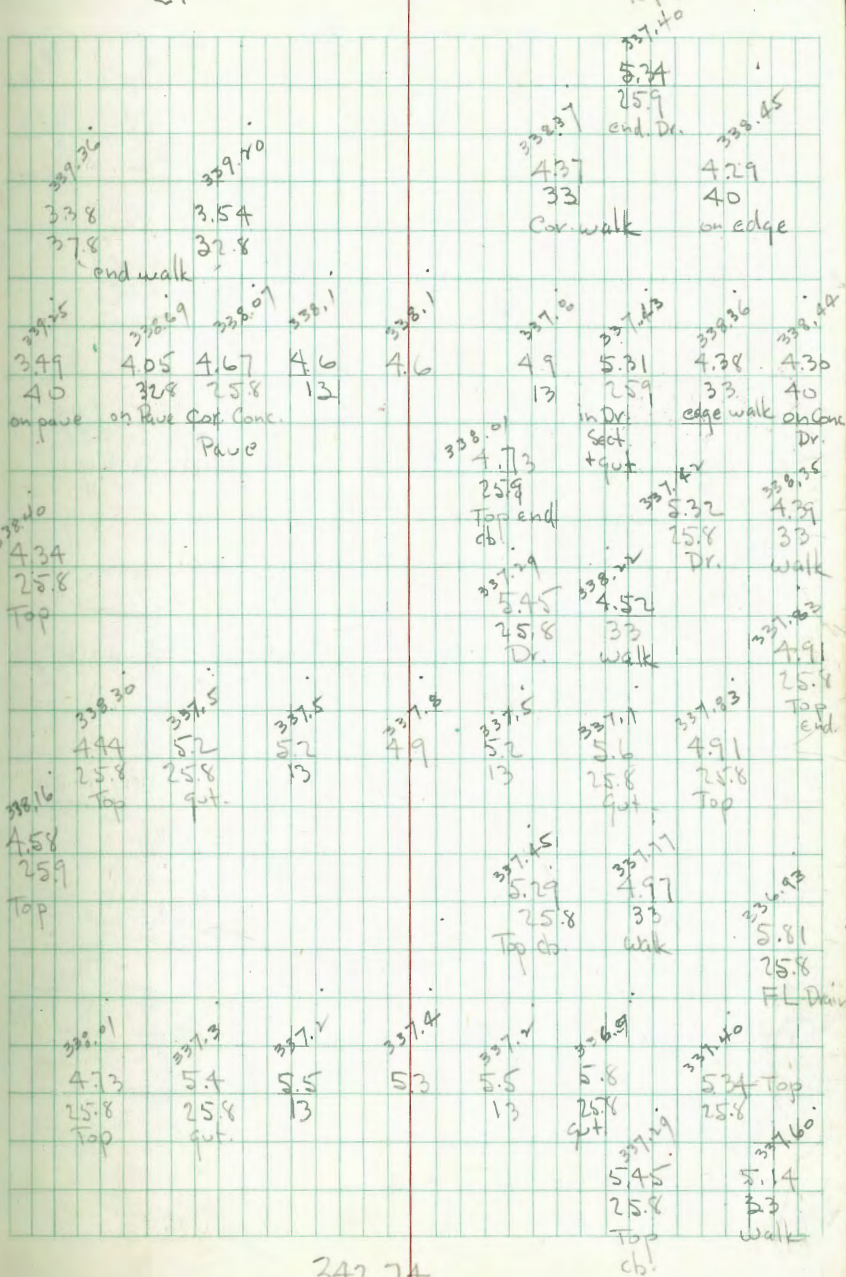
0+85 = Brk. in cb. on Lt.

0+70 = 4' Conc. walk on Rt. - cb. to walk

0+64 = 25.8 Rt. =  $\Phi$  4" C.I. Drain in cb.

0+60

0+51 =  $\Phi$  4' Conc. walk on Rt. - cb. to walk



342.74

2+40

2+15 = ± 3' Conc. walk on Lt.

2+00 - ± 11' Conc. Dr. on Lt.

cb. in on Lt in places - but poor Cond. Alley  
E to WL. 43rd

1+92.5 - 25.7 Rt. = ± 10' Conc. Dr.

1+87 - 25.9 Rt. = Brk. in cb

1+78 - ± 3' Conc. walk on Lt. - cb. to walk

1+75 = ± 4' Conc. walk on Rt. - cb. to walk

1+65 - 26' Rt. = Beg. cb. (broken) cb in poor cond.  
from here to Cor. 43rd

1+62 - 28' Rt. = ± F.H.

Cor. Broken off

1+60 - Beg. Walk on Lt. - Higher than pave -

1+60 = E.L. Alley

1+59 - Beg. Walk on Rt.

1+50 = ± Alley on Lt. - Dip

Lt.

Rt.

43

|        |        |       |       |       |       |       |        |        |
|--------|--------|-------|-------|-------|-------|-------|--------|--------|
| 339.39 | 339.16 | 338.7 | 338.7 | 338.7 | 338.5 | 338.1 | 338.19 | 338.97 |
| 335    | 3.58   | 4.0   | 4.0   | 4.0   | 4.2   | 4.6   | 3.95   | 3.77   |
| 33     | 25.9   | 25.9  | 13    |       | 13    | 25.9  | 25.9   | 33     |
| walk   | Top    | gut   |       |       |       | gut   | Top    | walk   |

|        |        |
|--------|--------|
| 339.26 | 339.00 |
| 3.48   | 3.74   |
| 32.9   | 25.9   |
| walk   | Top cb |

|        |             |       |       |       |       |        |
|--------|-------------|-------|-------|-------|-------|--------|
| 339.11 | 338.28      | 338.9 | 338.4 | 338.2 | 338.0 | 338.64 |
| 3.63   | 4.36        | 4.3   | 4.3   | 4.5   | 4.7   | 4.10   |
| 32.9   | 25.8        | 13    |       | 13    | 25.9  | 25.9   |
| walk   | gut. in Dr. |       |       |       | gut   | Top    |

|        |        |
|--------|--------|
| 337.96 | 338.11 |
| 4.78   | 4.03   |
| 25.7   | 33     |
| Dr     | walk   |

|        |          |
|--------|----------|
| 339.18 | 338.91   |
| 3.56   | 3.83     |
| 33     | 26.4     |
| walk   | Top walk |
|        | cb. out  |

|         |        |
|---------|--------|
| 338.21  | 338.54 |
| 4.43    | 4.20   |
| 25.8    | 33     |
| Top cb. | walk   |

|        |        |
|--------|--------|
| 338.97 | 338.09 |
| 4.27   | 4.65   |
| 25.9   | 26     |
| Top    | cb     |

|        |          |
|--------|----------|
| 339.21 | 339.06   |
| 3.43   | 2.68     |
| 37.8   | 37.8     |
|        | end walk |

|        |        |         |           |       |       |       |       |       |
|--------|--------|---------|-----------|-------|-------|-------|-------|-------|
| 339.37 | 338.66 | 338.04  | 338.3     | 338.1 | 338.0 | 337.7 | 331.9 | 338.7 |
| 3.42   | 4.08   | 4.70    | 4.4       | 4.6   | 4.7   | 5.0   | 4.8   | 4.0   |
| 40     | 33     | 25.8    | 13        |       | 13    | 26    | 27    | 40    |
|        |        | on pave | Cor. pave |       |       |       |       |       |

|        |        |
|--------|--------|
| 339.01 | 337.93 |
| 3.73   | 4.81   |
| 40     | 25.8   |
|        | edge   |

|        |          |
|--------|----------|
| 338.44 | 338.55   |
| 4.30   | 4.19     |
| 32.9   | 37.9     |
|        | end walk |

342.74

Lt. Rt.

53' E

40' E = E

27' E

14' E = w.cb.

2 + 99.31 = w.l. 43<sup>rd</sup> = edge H.C. Pavc

I.P. on BM. 4.47 344.22 2.99 339.75 339.77 NW. 43<sup>rd</sup>

2 + 79 = 25.9 Rt. = Brk. in cb.

2 + 70

|                              |                             |                             |                      |                      |                      |                               |                                      |                              |
|------------------------------|-----------------------------|-----------------------------|----------------------|----------------------|----------------------|-------------------------------|--------------------------------------|------------------------------|
| 339.53<br>4.71<br>40         | 339.35<br>4.92<br>26        | 339.19<br>5.05<br>13        | 339.08<br>5.16       | 339.63<br>5.21<br>13 | 338.89<br>5.35<br>26 | 338.13<br>5.51<br>40          |                                      |                              |
| 339.58<br>4.66<br>40         | 339.39<br>4.85<br>26        | 339.86<br>4.98<br>13        | 339.74<br>5.10       | 339.24<br>5.10<br>13 | 338.92<br>5.32<br>26 | 338.78<br>5.46<br>40          |                                      |                              |
| 339.56<br>4.68<br>40         | 339.38<br>4.86<br>26        | 339.29<br>4.95<br>13        | 339.09<br>5.15       | 339.05<br>5.19<br>13 | 338.84<br>5.40<br>26 | 338.74<br>5.52<br>40          |                                      |                              |
| 339.70<br>4.54<br>40<br>Top  | 339.16<br>5.08<br>40<br>gut | 339.12<br>5.12<br>26        | 339.05<br>5.19<br>13 | 338.86<br>5.38       | 338.73<br>5.51<br>13 | 338.65<br>5.59<br>26          | 338.58<br>5.66<br>40<br>gut          | 339.26<br>4.98<br>40<br>Top  |
| 339.79<br>4.45<br>33         | 339.64<br>4.60<br>26<br>Top | 339.21<br>5.03<br>26<br>gut | 339.70<br>5.04<br>13 | 339.25<br>4.99       | 339.03<br>5.21<br>13 | 338.64<br>5.60<br>25.8<br>gut | 339.25<br>4.99<br>25.8<br>100        | 339.49<br>4.75<br>33         |
| 339.61<br>3.13<br>33<br>walk | 339.79<br>3.45<br>26<br>Top | 338.8<br>3.9<br>26<br>gut.  | 338.9<br>3.8<br>13   | 338.9<br>3.8         | 338.7<br>4.0<br>13   | 338.91<br>3.83<br>26<br>Top   | 339.09<br>3.65<br>25.9<br>Top<br>cb. | 339.13<br>3.61<br>33<br>walk |
|                              |                             |                             |                      | 342.74               |                      |                               |                                      |                              |

Cont. P.48

1+16 - Brk. in cb. on Rt.

1+02 - Brk. in cb. on Lt.

0+85

0+81 - 259 Lt. =  $\Phi$  9' Conc. Dr.

0+78 - 26 Rt. =  $\Phi$  10' Dirt Dr. (cb. broken out)

0+76 - 259 Lt. = Brk. in cb.

0+70 - 259 Lt. =  $\Phi$  10' Conc. Dr.

0+63 - 259 Rt. =  $\Phi$  9' Conc. Dr.

0+55

0+25

80' E = EL 43<sup>d</sup> = 0+00 ahead = edge F.C. Pave.

66' E = E cb.

Lt

$\Phi$

339.84 Rt. 45

|        |        |  |  |  |  |  |        |  |
|--------|--------|--|--|--|--|--|--------|--|
| 339.90 | 340.06 |  |  |  |  |  | 339.84 |  |
| 4.34   | 4.18   |  |  |  |  |  | 4.40   |  |
| 259    | 259    |  |  |  |  |  | 259    |  |
| Top    | Top    |  |  |  |  |  | Top    |  |
|        | 339.3  |  |  |  |  |  | 339.8  |  |
|        | 4.9    |  |  |  |  |  | 5.2    |  |
|        | 259    |  |  |  |  |  | 259    |  |
|        | 9ut    |  |  |  |  |  | 9ut    |  |
|        | 340.14 |  |  |  |  |  | 339.55 |  |
|        | 4.10   |  |  |  |  |  | 4.69   |  |
|        | 32.7   |  |  |  |  |  | 25.9   |  |
|        | walk   |  |  |  |  |  | Top    |  |
|        | 339.40 |  |  |  |  |  | 339.13 |  |
|        | 4.84   |  |  |  |  |  | 4.51   |  |
|        | 259    |  |  |  |  |  | 33     |  |
|        | Dr.    |  |  |  |  |  | walk   |  |
|        | 340.20 |  |  |  |  |  |        |  |
|        | 4.04   |  |  |  |  |  |        |  |
|        | 32.7   |  |  |  |  |  |        |  |
|        | walk   |  |  |  |  |  |        |  |
|        | 339.40 |  |  |  |  |  |        |  |
|        | 4.84   |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | Dr.    |  |  |  |  |  |        |  |
|        | 339.74 |  |  |  |  |  |        |  |
|        | 4.50   |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | Top    |  |  |  |  |  |        |  |
|        | 339.1  |  |  |  |  |  |        |  |
|        | 5.1    |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.5  |  |  |  |  |  |        |  |
|        | 4.7    |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 339.7  |  |  |  |  |  |        |  |
|        | 4.5    |  |  |  |  |  |        |  |
|        | 339.6  |  |  |  |  |  |        |  |
|        | 4.6    |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 339.0  |  |  |  |  |  |        |  |
|        | 5.2    |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | Dr.    |  |  |  |  |  |        |  |
|        | 339.64 |  |  |  |  |  |        |  |
|        | 4.60   |  |  |  |  |  |        |  |
|        | 33     |  |  |  |  |  |        |  |
|        | walk   |  |  |  |  |  |        |  |
|        | 339.44 |  |  |  |  |  |        |  |
|        | 4.50   |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | Top    |  |  |  |  |  |        |  |
|        | 339.69 |  |  |  |  |  |        |  |
|        | 4.55   |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | Top    |  |  |  |  |  |        |  |
|        | 339.00 |  |  |  |  |  |        |  |
|        | 5.24   |  |  |  |  |  |        |  |
|        | 259    |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.9  |  |  |  |  |  |        |  |
|        | 4.8    |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 339.6  |  |  |  |  |  |        |  |
|        | 4.6    |  |  |  |  |  |        |  |
|        | 5.0    |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 338.8  |  |  |  |  |  |        |  |
|        | 5.4    |  |  |  |  |  |        |  |
|        | 26     |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.21 |  |  |  |  |  |        |  |
|        | 4.93   |  |  |  |  |  |        |  |
|        | 26     |  |  |  |  |  |        |  |
|        | Top    |  |  |  |  |  |        |  |
|        | 339.02 |  |  |  |  |  |        |  |
|        | 5.22   |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 338.65 |  |  |  |  |  |        |  |
|        | 5.59   |  |  |  |  |  |        |  |
|        | 25.9   |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.18 |  |  |  |  |  |        |  |
|        | 5.06   |  |  |  |  |  |        |  |
|        | 25.9   |  |  |  |  |  |        |  |
|        | Top    |  |  |  |  |  |        |  |
|        | 339.74 |  |  |  |  |  |        |  |
|        | 4.50   |  |  |  |  |  |        |  |
|        | 40     |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.25 |  |  |  |  |  |        |  |
|        | 4.99   |  |  |  |  |  |        |  |
|        | 40     |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.09 |  |  |  |  |  |        |  |
|        | 5.15   |  |  |  |  |  |        |  |
|        | 26     |  |  |  |  |  |        |  |
|        | 338.99 |  |  |  |  |  |        |  |
|        | 5.25   |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 338.81 |  |  |  |  |  |        |  |
|        | 5.43   |  |  |  |  |  |        |  |
|        | 338.68 |  |  |  |  |  |        |  |
|        | 5.56   |  |  |  |  |  |        |  |
|        | 13     |  |  |  |  |  |        |  |
|        | 338.58 |  |  |  |  |  |        |  |
|        | 5.66   |  |  |  |  |  |        |  |
|        | 26     |  |  |  |  |  |        |  |
|        | 338.92 |  |  |  |  |  |        |  |
|        | 5.80   |  |  |  |  |  |        |  |
|        | 40     |  |  |  |  |  |        |  |
|        | 9ut    |  |  |  |  |  |        |  |
|        | 339.09 |  |  |  |  |  |        |  |
|        | 5.15   |  |  |  |  |  |        |  |
|        | 40     |  |  |  |  |  |        |  |
|        | Top    |  |  |  |  |  |        |  |

344.20



Levels on 43<sup>rd</sup> - 100' each way from  
Prop. Lines of Dwight - 80' st. - 14' lbs. - Paved AC

1+00 = 100' N. of N.L. Dwight.

0+50

0+25

0+00 = N.L. Dwight.

1+00 = S.L. Dwight. - For Int. See P. 44

0+75

0+50

0+00 = 100' S. of S.L. Dwight.

Lt. = W

±

Rt. = E 46

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 3.25<br>26<br>Top | 3.90<br>26<br>gut. | 3.33<br>13 | 3.32 | 3.38<br>13 | 3.82<br>26<br>gut. | 3.17<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 3.90<br>26<br>Top | 4.49<br>26<br>gut. | 3.96<br>13 | 4.06 | 4.08<br>13 | 4.49<br>26<br>gut. | 3.84<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 4.21<br>26<br>Top | 4.80<br>26<br>gut. | 4.29<br>13 | 4.27 | 4.36<br>13 | 4.79<br>26<br>gut. | 4.21<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 4.54<br>26<br>Top | 5.08<br>26<br>gut. | 4.68<br>13 | 4.66 | 4.71<br>13 | 4.99<br>26<br>gut. | 4.50<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 4.98<br>26<br>Top | 5.66<br>26<br>gut. | 5.51<br>13 | 5.46 | 5.51<br>13 | 5.80<br>26<br>gut. | 5.15<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 5.62<br>26<br>Top | 6.35<br>26<br>gut. | 5.95<br>13 | 5.85 | 5.81<br>13 | 6.15<br>26<br>gut. | 5.49<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |            |            |      |            |                    |                   |
|-------------------|------------|------------|------|------------|--------------------|-------------------|
| 6.12<br>26<br>Top | 6.77<br>26 | 6.75<br>13 | 6.33 | 6.36<br>13 | 6.84<br>26<br>gut. | 6.11<br>26<br>Top |
|-------------------|------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 7.17<br>26<br>Top | 7.89<br>26<br>gut. | 7.49<br>13 | 7.43 | 7.62<br>13 | 7.89<br>26<br>gut. | 7.16<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

344.22 - P. 45

Levels around Returns - 43<sup>rd</sup> + Dwight.

|                                       |      |          |
|---------------------------------------|------|----------|
| N.W. Ret. - 24' around - 4 parts - 6' |      |          |
| Beq. W.L. 43 <sup>rd</sup>            | 5.03 | T = Top  |
|                                       | 4.60 | g = gut. |
| 6' E.                                 | 4.52 | T        |
|                                       | 4.99 | g        |
| " = E                                 | 4.50 | T        |
|                                       | 5.01 | g        |
| 6'                                    | 4.57 | T        |
|                                       | 5.06 | g        |
| 6' end = N.L. Dwight.                 | 4.54 | T        |
|                                       | 5.08 | g        |

Ret. in fair Cond.

|                                 |      |   |
|---------------------------------|------|---|
| N.E. Ret. = 24' around - 4 - 6' |      |   |
| Beq. N.L. Dwight.               | 4.50 | T |
|                                 | 4.99 | g |
| 6' S.                           | 4.99 | T |
|                                 | 5.03 | g |
| "                               | 4.47 | T |
|                                 | 5.03 | g |
| "                               | 4.48 | T |
|                                 | 5.05 | g |
| 6' end = E.L. 43 <sup>rd</sup>  | 4.62 | T |
|                                 | 5.12 | g |

Ret. in poor Cond.

S.E. Ret. = 24' around - 4 - 6'

|                            |      |   |
|----------------------------|------|---|
| Beq. E.L. 43 <sup>rd</sup> | 5.06 | T |
|                            | 5.59 | g |
| 6' W.                      | 5.03 | T |
|                            | 5.58 | g |
| "                          | 5.03 | T |
|                            | 5.64 | g |
| "                          | 5.07 | T |
|                            | 5.67 | g |
| 6' end = S.L. Dwight       | 5.15 | T |
|                            | 5.79 | g |

Ret. - fair Cond

S.W. Ret. = 24' around - 4 - 6'

|                                |      |   |
|--------------------------------|------|---|
| Beq. S.L. Dwight.              | 4.98 | T |
|                                | 5.66 | g |
| 6' N.                          | 5.02 | T |
|                                | 5.61 | g |
| "                              | 4.99 | T |
|                                | 5.65 | g |
| "                              | 4.99 | T |
|                                | 5.56 | g |
| 6' end = W.L. 43 <sup>rd</sup> | 4.99 | T |
|                                | 5.60 | g |

Ret. in fair Cond.

Cont. from P. 45

2+70.77 = w.l. Fairmount + edge H.C. Pave

2+67.7 = cb. Brks down to w.l. Fairmount.

2+35

T.P. on BM. 5.01 345.93 330 340.92 340.89

2+00

1+88-26.1 Lt. = Brk in cb.

1+75

1+58 - Brk in cb. on Rt. at E. side of Dr.

1+52 - 259 Rt. = 10' Conc. Dr.

1+47 - 26' Lt. = Beg cb.

1+45 - E.L. Alley, - Ret. on Lt. Broken out.

1+32 - 82 Lt. 5-1/2' x 37' Gas Co. M.H.

1+25 = W.L. 20' Alley

1+23.5 - 27.3 Rt. = E P. pole # P. 4325

48

|  |             |              |        |          |        |         |        |          |            |         |  |     |  |        |      |      |
|--|-------------|--------------|--------|----------|--------|---------|--------|----------|------------|---------|--|-----|--|--------|------|------|
|  | Lt.         |              |        |          |        |         |        |          |            |         |  | Rt. |  |        |      |      |
|  | 340.9       | 340.96       | 340.92 | 340.87   | 340.81 | 340.89  | 340.74 | 340.61   | 340.80     |         |  |     |  |        |      |      |
|  | 5.0         | 4.97         | 5.01   | 5.16     | 5.12   | 5.04    | 5.19   | 5.32     | 5.13       |         |  |     |  |        |      |      |
|  | 40          | 38.2         | 32.9   | 26.1     | 13     |         | 13     | 25.9     | 40         |         |  |     |  | 340.99 | 4.94 | 25.9 |
|  |             |              |        | end walk | Ret    | Top cb. |        | Top+gut. | on Conc.   |         |  |     |  |        |      | Top  |
|  | 5.4         | 5.58         | 6.1    | 5.4      | 5.4    |         |        | 5.5      | 5.6        | 5.30    |  |     |  |        |      |      |
|  | 40          | 26.2         | 26.2   | 13       |        |         |        | 13       | 25.9       | 25.9    |  |     |  |        |      |      |
|  |             |              | Top    | gut      |        |         |        |          | gut        | Top     |  |     |  |        |      |      |
|  | 339.8       | 339.97       | 339.6  | 340.1    | 340.9  | 340.2   | 339.9  | 340.37   | 340.16     |         |  |     |  |        |      |      |
|  | 4.4         | 4.27         | 4.6    | 4.0      | 3.8    | 4.0     | 4.3    | 3.87     | 4.08       |         |  |     |  |        |      |      |
|  | 40          | 26.2         | 26.2   | 13       |        | 13      | 25.8   | 25.8     | 33         |         |  |     |  |        |      |      |
|  |             | Top          | gut    |          |        |         | gut    | Top      | walk       |         |  |     |  |        |      |      |
|  | 339.9       | 339.5        | 340.1  | 340.1    | 339.9  | 339.8   | 340.32 |          |            |         |  |     |  |        |      |      |
|  | 4.2         | 4.30         | 4.7    | 4.1      | 4.0    | 4.3     | 4.4    | 3.92     |            |         |  |     |  |        |      |      |
|  | 40          | 26.1         | 26.1   | 13       |        | 13      | 25.9   | 25.9     |            |         |  |     |  |        |      |      |
|  |             | Top          | gut    |          |        |         | gut    | Top      |            |         |  |     |  |        |      |      |
|  | 340.17      |              |        |          |        |         | 340.27 |          |            |         |  |     |  |        |      |      |
|  | 4.12        |              |        |          |        |         | 4.02   |          |            |         |  |     |  |        |      |      |
|  | 26          |              |        |          |        |         | 25.9   |          |            |         |  |     |  |        |      |      |
|  | Top         |              |        |          |        |         | Top    |          |            |         |  |     |  |        |      |      |
|  | 339.8       | 339.9        | 339.5  | 339.9    | 340.1  | 339.9   | 339.9  | 339.81   | 339.97     | 339.64  |  |     |  |        |      |      |
|  | 4.4         | 4.3          | 4.7    | 4.3      | 4.1    | 4.3     | 4.8    | 4.43     | 4.27       | 4.60    |  |     |  |        |      |      |
|  | 40          | 26           | 26     | 13       |        | 13      | 26     | 26       | 33         | 40      |  |     |  |        |      |      |
|  |             | i Rad.       | gut    |          |        |         | gut    | Top      | Brk in     | Top+gut |  |     |  |        |      |      |
|  |             | Top broken   |        |          |        |         | i Rad. | Ret      | Ret        | end ret |  |     |  |        |      |      |
|  | 340.13      | 340.19       |        |          |        |         |        |          |            |         |  |     |  |        |      |      |
|  | 4.11        | 4.05         |        |          |        |         |        |          |            |         |  |     |  |        |      |      |
|  | edge - 13.3 | 82 = edge MH |        |          |        |         |        |          |            |         |  |     |  |        |      |      |
|  | 340.28      | 340.11       | 339.4  | 339.9    | 339.9  | 339.7   | 339.3  | 339.11   | 340.02     |         |  |     |  |        |      |      |
|  | 3.96        | 4.13         | 4.8    | 4.3      | 4.3    | 4.5     | 4.9    | 4.53     | 4.22       |         |  |     |  |        |      |      |
|  | 40          | 26           | 26     | 13       |        | 13      | 26     | 26       | 40         |         |  |     |  |        |      |      |
|  | Top+gut     | Top          | gut    |          |        |         | gut    | Top      | Top+gut    |         |  |     |  |        |      |      |
|  | end Ret.    | i Rad.       |        |          |        |         | i Rad. | Ret      | end of Ret |         |  |     |  |        |      |      |
|  |             |              |        |          |        |         |        |          |            | 344.22  |  |     |  |        |      |      |

7-23-47  
7.0.

30' E = Fairmount - end.

|     |     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 332 | 395 | 426 | 450 | 465 | 483 | 493 | 512 | 526 | 541 | 572 | 601 | 651 |
| 140 | 90  | 65  | 40  | 26  | 13  |     | 13  | 26  | 40  | 65  | 90  | 140 |

20' E. of W.L.

|     |     |     |     |     |     |     |     |     |     |     |      |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|
| 366 | 428 | 455 | 470 | 472 | 483 | 495 | 503 | 519 | 533 | 553 | 559  | 588 | 617 | 679 |
| 140 | 90  | 65  | 45  | 40  | 26  | 13  |     | 13  | 26  | 40  | 44.6 | 65  | 90  | 140 |

10' E. Cont.

|     |     |     |     |     |     |            |               |           |           |           |           |           |           |
|-----|-----|-----|-----|-----|-----|------------|---------------|-----------|-----------|-----------|-----------|-----------|-----------|
| 436 | 375 | 490 | 441 | 529 | 474 | 573        | 633           | 567       | 642       | 602       | 663       | 673       | 733       |
| 40  | 140 | 90  | 90  | 65  | 65  | 45         | 44.6          | 65        | 65        | 90        | 90        | 140       | 140       |
| got | Top | got | Top | got | Top | got = FL   | got = FL      | got = Top | got = Top | got = Top | got = Top | got = Top | got = Top |
|     |     |     |     |     |     | Inlet end. | FL Inlet end. |           |           |           |           |           |           |

10' E. of W.L. = W.cb. Fairmount

|          |        |        |        |        |        |        |        |          |
|----------|--------|--------|--------|--------|--------|--------|--------|----------|
| 593      | 503    | 502    | 505    | 503    | 519    | 536    | 536    | 636      |
| 40       | 40     | 26     | 13     |        | 13     | 26     | 40     | 40       |
| got = FL | Top cb | Top cb | Top cb | Top cb | Top cb | Top cb | Top cb | got = FL |
| Culvert  | + Top  | + Top  | + Top  | + Top  | + Top  | + Top  | + Top  | Culvert  |
|          |        |        |        |        |        |        |        |          |

Rodson & Returns - N.W. + S.W.

Rave meets top of cb around Ret.

Ret N.W.  
Ret Top cb  
+ got

Ret S.W.  
Ret Top cb  
+ got

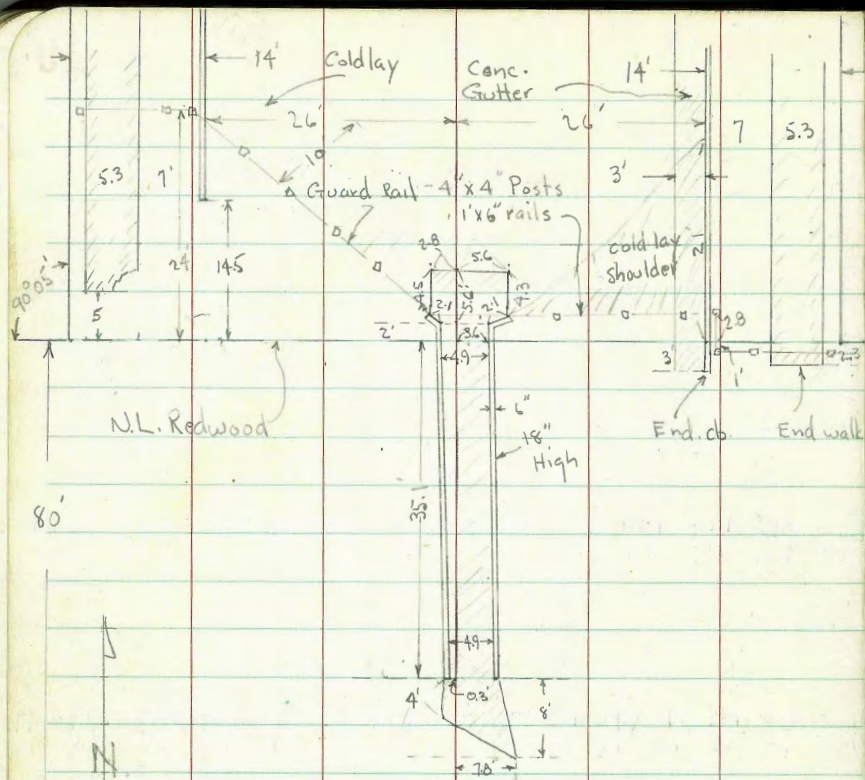
345.93

Lt.

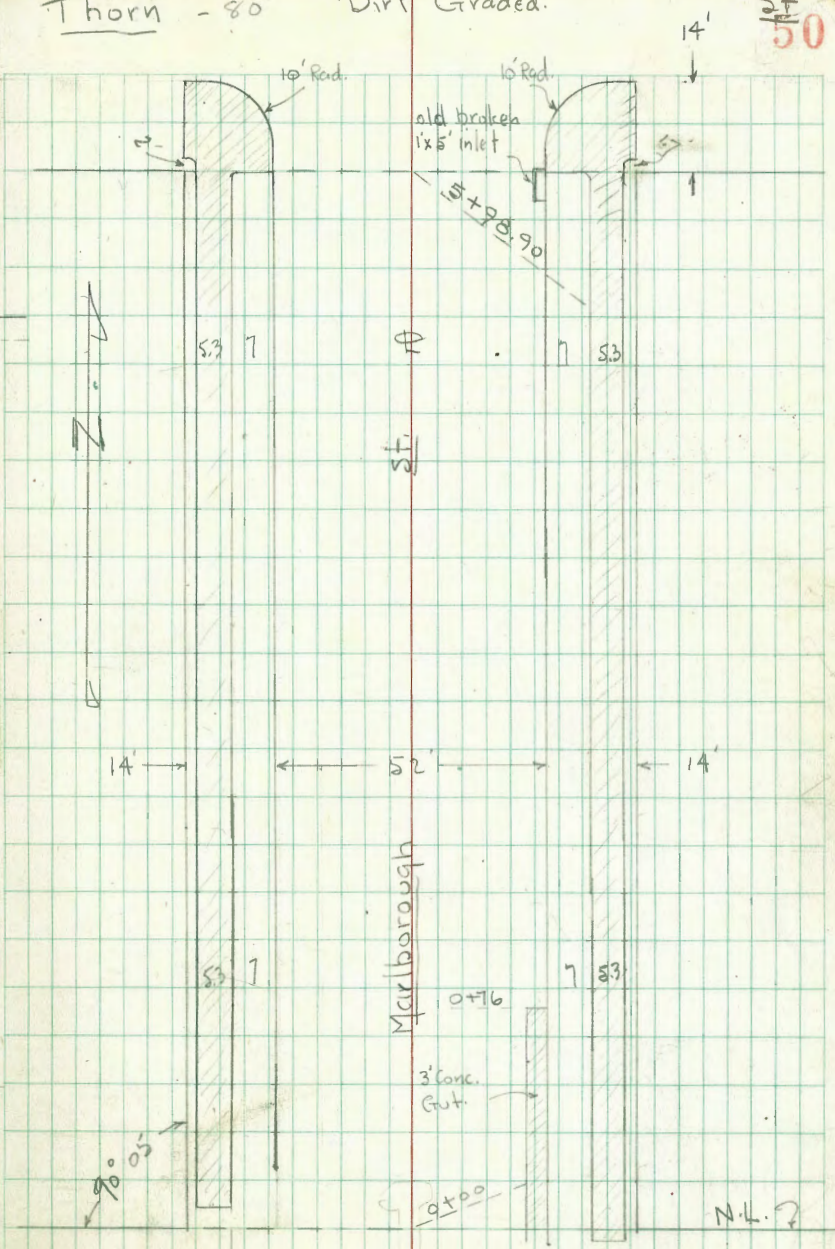
±

Rt.

49



Thorn - 80' Dirt Graded.



St 50

Redwood - 80' St

± Marlborough

Ed. Hub

Detail of open Conc. Box Culvert at Redwood + Marlborough

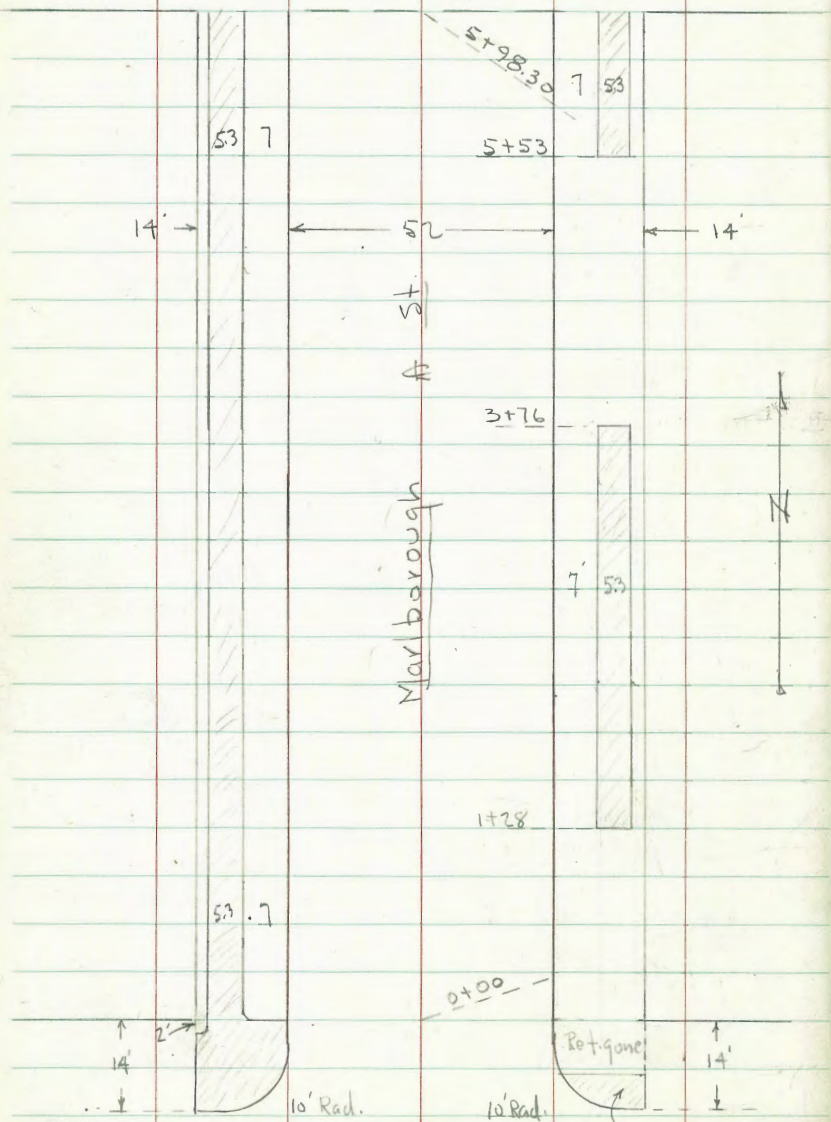
X-Sect. Marlborough - Redwood To N. of Dwight - 7-14-47 W.O. 31385 F.O.

Redwood Not Graded. See Detail other side St.

Myrtle - 80' st.

st

For Int. See P. I.



Thorn 80' st.

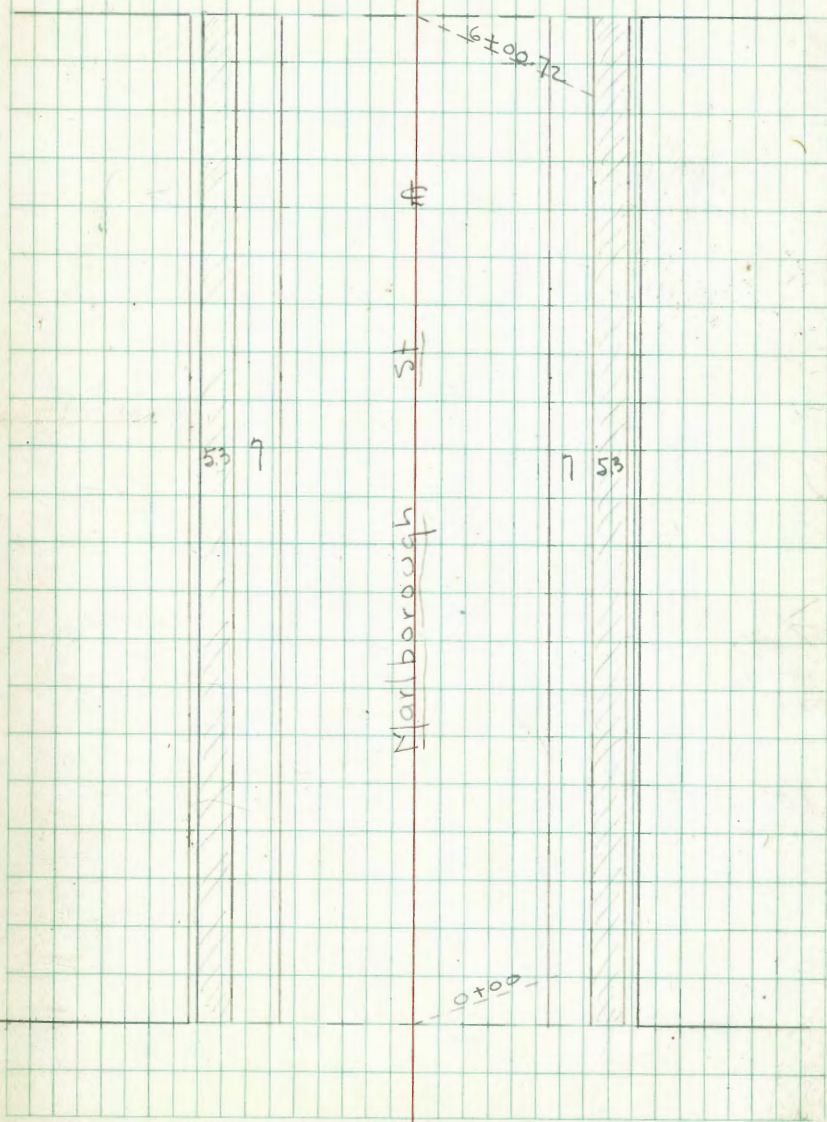
Poor Cond.

st

Dwight - 80'

st 51

See P. 26 for Int



Myrtle = 80'

st

A table with 5 columns and 20 rows. The columns are defined by vertical red lines, and the rows are defined by horizontal green lines. The table is currently empty.

A table with 1 column and 20 rows. The column is defined by a vertical red line, and the rows are defined by horizontal green lines. The table is currently empty.





0+07.6 = Edge Conc. slab inlet  
 0+06 = 29' Rt. = ± 14" Acacia  
 T.P. 5.98 298.19 5.54 292.21

0+05 = Beg. walk on Lt. - Cor. broken

0+03.2 = on end of wing walls

0+02 = Ang. in wing walls

0+00 - Cont.

Conc. gutter is under the Cold lay.  
 0+00 = NL. Redwood - End<sup>3</sup> - Conc. gutter - Broken Down to rd of cb.

0-02.3 = Beg. Walk on Rt. - Poor Cond.

| Station | Left                                   | Center                                   | Right                                       |
|---------|--|--|---|
|         |  | 290.68<br>7.31<br>28<br>Cor.             | 290.94<br>7.25<br>5.0<br>Cor.               |
|         |  | 298.19 ✓                                 |   |
|         | 292.79<br>49L<br>38.3<br>Cor. end walk |  |   |
|         | 299.6<br>8.1<br>5.0                    | 292.3<br>5.4<br>4.0                      | 292.1<br>5.6<br>4.6                         |
|         |  | 292.3<br>5.4<br>1.3                      | 292.1<br>5.0<br>1.3                         |
|         |  | 292.01<br>5.74<br>3.1<br>Top-end<br>wall | 291.9<br>6.00<br>2.88<br>Top cb<br>+ CL     |
|         |  | 291.87<br>5.88<br>1.4<br>Top<br>wall     | 291.75<br>6.00<br>2.88<br>Top<br>wall       |
|         |  | 291.43<br>7.32<br>1.4<br>Bot             | 291.19<br>5.80<br>3.5<br>Bot                |
|         | 291.3<br>8.4<br>5.0                    | 291.4<br>6.1<br>4.0                      | 291.71<br>6.04<br>3.1<br>walk               |
|         |  |  | 291.60<br>6.15<br>3.84<br>walk              |
|         |  |  | 291.4<br>6.3<br>4.0                         |
|         |  |  | 289.9<br>7.8<br>5.0                         |
|         | 291.8<br>5.9<br>2.6                    | 291.5<br>6.2<br>1.3                      | 290.1<br>7.6<br>2.0                         |
|         |  | 290.67<br>7.08<br>1.3<br>Top<br>wall     | 290.57<br>6.68<br>1.3<br>Bot                |
|         |  |  | 291.9<br>8.46<br>3.6<br>Bot                 |
|         |  |  | 290.77<br>6.98<br>3.6<br>Top<br>wall        |
|         |  |  | 290.8<br>7.9<br>4.0<br>Top                  |
|         |  |  | 292.5<br>5.7<br>1.3<br>Grand. Conc.<br>gut. |
|         |  |  | 292.0<br>7.16<br>2.59<br>Top<br>cb.         |
|         |  |  | 290.54<br>5.99<br>2.59<br>Top<br>cb.        |
|         |  |  | 291.9<br>6.28<br>3.1<br>end walk            |
|         |  |  | 291.69<br>6.36<br>3.84<br>end walk          |
|         |  |  | 297.75                                      |

1+04 - 26' Rt. =  $\pm$  9' Dirt Dr. - cb. broken

1+00

0+76 = End. of Conc gutter on Rt.

0+68 - 22.9 Rt. =  $\pm$  16' Conc. Dr.

0+57 - 29.8 Rt. =  $\pm$  18" Acacia

0+50

0+39 - 30' Rt. =  $\pm$  8' Acacia

0+36 = Brk. in cb. on Lt.

0+29 =  $\pm$  10' Conc. Dr. on Rt.

0+23

0+20 - 30' Rt. =  $\pm$  18" Acacia

0+14.5 = Beg. cb. on Lt.

0+10

Lt.

+

Rt.

55

|  |  |  |  |  |  |  |           |            |        |
|--|--|--|--|--|--|--|-----------|------------|--------|
|  |  |  |  |  |  |  | 293.1     | 293.12     | 293.81 |
|  |  |  |  |  |  |  | 5.1       | 4.97       | 4.38   |
|  |  |  |  |  |  |  | 26        | 26         | 33.1   |
|  |  |  |  |  |  |  | got.      | Top        | walk   |
|  |  |  |  |  |  |  | 293.0     | 293.55     |        |
|  |  |  |  |  |  |  | 5.2       | 4.64       |        |
|  |  |  |  |  |  |  | 26        | 26         |        |
|  |  |  |  |  |  |  | got.      | Top        |        |
|  |  |  |  |  |  |  | 292.72    | 292.45     | 293.13 |
|  |  |  |  |  |  |  | 5.47      | 5.64       | 5.06   |
|  |  |  |  |  |  |  | 23        | 26         | 26     |
|  |  |  |  |  |  |  | Gr. gut   | got.       | Top    |
|  |  |  |  |  |  |  | 292.54    | 292.41     | 293.12 |
|  |  |  |  |  |  |  | 5.65      | 5.78       | 5.07   |
|  |  |  |  |  |  |  | 22.9      | 22.9       | 33.1   |
|  |  |  |  |  |  |  | edge gut. | got in Dr. | walk   |
|  |  |  |  |  |  |  | 293.0     | 293.51     |        |
|  |  |  |  |  |  |  | 5.2       | 4.68       | 5.50   |
|  |  |  |  |  |  |  | 40        | 38.4       | 33.1   |
|  |  |  |  |  |  |  | walk      | Top        | walk   |
|  |  |  |  |  |  |  | 292.7     | 292.7      |        |
|  |  |  |  |  |  |  | 6.0       | 5.5        | 5.5    |
|  |  |  |  |  |  |  | got.      | 13         |        |
|  |  |  |  |  |  |  | 292.5     | 292.5      |        |
|  |  |  |  |  |  |  | 5.7       | 6.16       | 5.68   |
|  |  |  |  |  |  |  | 13        | 22.9       | 25.9   |
|  |  |  |  |  |  |  | edge gut. | got        | Top    |
|  |  |  |  |  |  |  | 291.86    | 291.45     | 292.26 |
|  |  |  |  |  |  |  | 6.63      | 6.74       | 5.93   |
|  |  |  |  |  |  |  | 22.8      | 25.9       | 33.1   |
|  |  |  |  |  |  |  | edge gut. | in Dr.     | walk   |
|  |  |  |  |  |  |  | 292.23    | 291.9      | 292.6  |
|  |  |  |  |  |  |  | 5.36      | 6.3        | 6.01   |
|  |  |  |  |  |  |  | 6.3       | 6.4        | 5.93   |
|  |  |  |  |  |  |  | 25.7      | 25.7       | 33.1   |
|  |  |  |  |  |  |  | Top       | got        | Top    |
|  |  |  |  |  |  |  | 292.32    | 291.91     | 292.26 |
|  |  |  |  |  |  |  | 5.87      | 6.73       | 6.83   |
|  |  |  |  |  |  |  | 25.7      | 22.8       | 25.9   |
|  |  |  |  |  |  |  | Top       | edge Conc  | got    |
|  |  |  |  |  |  |  |           | got.       | Top    |
|  |  |  |  |  |  |  | 292.6     | 292.95     | 292.04 |
|  |  |  |  |  |  |  | 5.6       | 5.37       | 6.00   |
|  |  |  |  |  |  |  | 40        | 38.3       | 38.4   |
|  |  |  |  |  |  |  | walk      | 33         | 38.4   |
|  |  |  |  |  |  |  | 292.82    | 292.8      | 292.14 |
|  |  |  |  |  |  |  | 5.8       | 5.6        | 6.05   |
|  |  |  |  |  |  |  | 26        | 13         | 6.1    |
|  |  |  |  |  |  |  | 292.6     | 291.3      | 292.1  |
|  |  |  |  |  |  |  | 6.7       | 7.2        | 6.1    |
|  |  |  |  |  |  |  | 8         |            |        |
|  |  |  |  |  |  |  | 291.0     | 291.3      | 292.19 |
|  |  |  |  |  |  |  |           |            | 6.0    |
|  |  |  |  |  |  |  | 6.9       | 6.5        | 6.05   |
|  |  |  |  |  |  |  | 13        | 16         | 38.4   |
|  |  |  |  |  |  |  | on c.l.   | Top        | walk   |
|  |  |  |  |  |  |  |           | 25.9       | 33.1   |
|  |  |  |  |  |  |  |           | Top        | cb     |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |
|  |  |  |  |  |  |  |           |            |        |

298.19

+C.L.

T.P. 7.41 304.16 1.44 296.75

3+50

2+26 = ± 7' cb. broken out for Dirt Dr. on Rt.

3+00

2+56 = ± 10' Conc. Dr. on Rt.

2+54 = ± 7' cb. broken out for Dirt Dr. on Rt.

2+50

2+07 - 26' Rt. = ± 8' Broken out cb. for Dirt Dr.

2+00

1+50

Lt.

±

Rt.

56

|                              |                             |                    |              |                            |                            |                                |
|------------------------------|-----------------------------|--------------------|--------------|----------------------------|----------------------------|--------------------------------|
| 297.59<br>0.60<br>26<br>Top  | 296.8<br>1.4<br>26<br>gut.  | 297.3<br>0.9<br>13 | 297.3<br>0.9 | 296.7<br>1.5<br>13         | 296.2<br>2.0<br>26<br>gut. | 297.06<br>1.13<br>26<br>Top    |
| 296.93<br>1.26<br>26<br>Top  | 296.2<br>2.0<br>26<br>gut.  | 296.7<br>1.5<br>13 | 296.5<br>1.7 | 295.9<br>2.3<br>13         | 296.0<br>2.2<br>26<br>gut. | 296.37<br>1.32<br>33.1<br>walk |
| 296.47<br>1.72<br>33<br>walk | 296.83<br>2.36<br>26<br>Dr. |                    |              | 295.2<br>3.0<br>26<br>gut. |                            | 295.89<br>2.30<br>33.1<br>walk |
| 296.24<br>1.91<br>26<br>Top  | 295.6<br>2.6<br>26<br>gut.  | 296.1<br>2.1<br>13 | 295.8<br>2.4 | 295.4<br>2.8<br>13         | 294.9<br>3.3<br>26<br>gut. | 295.67<br>2.52<br>26<br>Top    |
| 295.53<br>2.66<br>26<br>Top  | 294.8<br>3.4<br>26<br>gut.  | 295.4<br>2.8<br>13 | 295.3<br>2.9 | 294.6<br>3.6<br>26<br>gut. | 294.4<br>3.8<br>26<br>gut. | 295.15<br>2.94<br>33.1<br>walk |
| 294.27<br>3.32<br>26<br>Top  | 294.1<br>4.1<br>26<br>gut.  | 294.6<br>3.6<br>13 | 294.6<br>3.6 | 294.2<br>4.0<br>13         | 293.6<br>4.6<br>26<br>gut. | 295.05<br>3.14<br>26<br>Top    |

298.19

T.P. on BM 5.07 306.89 2.3f 301.82 NW. Thorn

5+59- ± 9' Conc. Dr. on Rt.

5+50

5+14- ± 9' Conc. Dr. on Rt.

5+00

4+79 = ± 9' Conc. Dr. on Rt.

4+50

4+07- ± 9' cb. broken out for Dirt Dr. on Rt. (not used)

4+00

Lt. ± Rt.

57

306.89 ✓

300.45

299.6

300.0

299.9

299.7

299.2

299.88

3.71

4.6

4.2

4.3

4.5

5.0

4.28

26

26

13

13

26

26

Top

gut.

Top

gut.

Top

298.98

5.18

25.9

Dr.

299.58

4.58

33

walk

299.74

299.0

299.3

299.3

298.8

298.6

299.14

4.42

5.2

4.9

4.9

5.4

5.6

5.02

26

26

13

13

26

26

Top

gut.

Top

gut.

Top

298.34

5.82

25.9

Dr.

299.07

5.09

33

walk

299.01

298.4

298.6

298.7

298.4

297.6

298.43

5.15

5.8

5.6

5.5

5.8

6.6

5.73

26

26

13

13

26

26

Top

gut.

Top

gut.

Top

297.3

6.9

26

gut.

298.01

6.15

33

walk

298.40

297.5

297.9

298.0

297.5

297.1

297.16

5.76

6.7

6.3

6.2

6.7

7.1

6.40

26.1

26.1

13

13

13

26

26

Top

gut.

Top

gut.

Top

304.6 ✓

80' N. = N.L. Thorn = 0+00 ahead

Reds on  $\Phi$  of N.E. & N.W. Returns  
curbin on N.E. But most of walk gone - see sketch

66' N. = N. cb.

53' N.

40' N. =  $\Phi$  Thorn

27' N.

14' N. = S.cb Thorn

Rodson  $\Phi$  of S.E. & S.W. Returns

5+98.90 = S.L. Thorn

5+93.9 = S. end 5' x 1' outlet for 12" Corr. Iron pipe  
abandoned

| Lt.                     |       |       |       | RT                      |                  |          |               |
|-------------------------|-------|-------|-------|-------------------------|------------------|----------|---------------|
| 301.75                  | 301.1 | 301.5 | 301.7 | 301.5                   | 300.87           | 301.7    | 58            |
| 5.14                    | 5.8   | 5.4   | 5.2   | 5.4                     | 6.02             | 5.2      |               |
| 26                      | 26    | 13    |       | 13                      | 26               | 40       |               |
| Top                     | gut.  |       |       |                         | Topcb.           | gut.     |               |
| 301.10                  |       |       |       | 300.98                  |                  |          |               |
| 5.19                    |       |       |       | 5.91                    |                  |          |               |
| Topcb. $\Phi$ N.W. Ret. |       |       |       | Topcb. $\Phi$ N.E. Ret. |                  |          |               |
| 301.16                  | 301.2 | 301.0 | 301.4 | 301.6                   | 301.4            | 300.9    | 300.7         |
| 5.13                    | 5.7   | 5.9   | 5.5   | 5.3                     | 5.5              | 6.0      | 6.2           |
| 40                      | 40    | 26    | 13    |                         | 13               | 26       | 46            |
| Top-end                 | gut.  |       |       |                         |                  | gut.     | Top           |
| cb.                     |       |       |       |                         |                  |          | end cb.       |
| 301.4                   | 301.0 | 301.2 | 301.4 | 301.4                   | 301.2            | 301.1    |               |
| 5.5                     | 5.9   | 5.7   | 5.5   | 5.5                     | 5.7              | 5.8      |               |
| 40                      | 26    | 13    |       | 13                      | 26               | 40       |               |
| 301.5                   | 300.9 | 300.9 | 301.3 | 301.3                   | 301.2            | 301.2    |               |
| 5.4                     | 6.0   | 6.0   | 5.6   | 5.6                     | 5.7              | 5.7      |               |
| 40                      | 26    | 13    |       | 13                      | 26               | 40       |               |
| 301.1                   | 300.6 | 300.8 | 301.1 | 301.0                   | 301.0            | 300.9    |               |
| 5.8                     | 6.3   | 6.1   | 5.8   | 5.9                     | 5.9              | 6.0      |               |
| 40                      | 26    | 13    |       | 13                      | 26               | 40       |               |
| 301.19                  | 300.6 | 300.3 | 300.7 | 300.9                   | 300.8            | 300.4    | 300.55        |
| 5.70                    | 6.3   | 6.6   | 6.2   | 6.0                     | 6.1              | 6.5      | 6.34          |
| 40                      | 40    | 26    | 13    |                         | 13               | 26       | 40            |
| Top-end                 |       |       |       |                         |                  |          | Top-end       |
| cb.                     |       |       |       |                         |                  |          | cb. + ground. |
| 301.02                  |       |       |       |                         | 300.53           |          |               |
| 5.87                    |       |       |       |                         | 6.36             |          |               |
| Top ch.                 |       |       |       |                         | Topcb.           |          |               |
| $\Phi$ S.W. Ret.        |       |       |       |                         | $\Phi$ S.E. Ret. |          |               |
| 301.10                  | 300.2 | 300.6 | 300.7 | 300.5                   | 300.56           | 300.53   |               |
| 5.79                    | 6.7   | 6.3   | 6.2   | 6.4                     | 6.33             | 6.36     | 6.59          |
| 26                      | 26    | 13    |       | 13                      | 26               | 26       | 26            |
| Top                     | gut.  |       |       |                         | Top head         | Topcb.   | 7.30          |
|                         |       |       |       |                         | well             | + ground | 26            |
|                         |       |       |       |                         |                  |          | gut = Inlet.  |

306.89

1+60 = Brk. in cb. on Rt.

1+50 = walk still Low

1+37 = Dirt Dr. over cb. (mud need Dr.)

1+28 = Beg walk on Rt.

1+20

1+00

0+83 = Brk. in cb. on Rt.

0+65 = Brk. in cb. on Rt.

0+50

0+43 = Brk. in cb. on Rt.

0+25 = Brk. in cb. on Rt.

Lt

+

Rt

302.48

50.40

341

349

26 = Top 33

ch.)

303.66

302.8

303.1

303.4

302.1

301.6

303.16

303.13

303.11

303.11

3.23

4.1

3.7

3.5

3.8

4.3

3.73

3.76

3.60

259

259

13

13

26.1

26.1

33

walk

38.3

Top

gut

gut

Top

walk

302.67

302.87

302.95

4.22

4.07

3.94

26.1

33.1

38.4

Top cb.

walk

+Dirt

302.53

302.68

4.36

4.21

33.1

38.4

end walk

303.30

302.3

302.8

303.0

302.7

301.9

302.15

302.9

302.9

3.59

4.6

4.1

3.9

4.2

5.0

4.74

4.0

4.0

259

259

13

13

26.1

26.1

33

40

Top

gut

gut

Top

303.05

302.1

302.5

302.7

302.5

301.7

302.14

302.3

303.0

3.84

4.8

4.4

4.2

4.4

5.2

4.75

3.6

3.9

26

26

13

13

26.1

24.1

33

40

Top

gut

gut

Top

302.36

301.5

301.9

302.7

301.8

301.7

301.67

302.0

301.85

4.53

5.4

5.6

4.7

5.1

5.7

5.22

3.9

4.0

259

259

13

13

26.1

26.1

33

40

Top

gut

gut

Top

306.89

301.59

301.2

5.39

5.77

26.1

26.2

Top

Top cb.

3+85

3+76 = End of walk on Rt.

3+61 - Beg Broken walk on Rt.

T.P. 7.06 312.80 1.15 305.74

3+50

3+00

2+50

2+00

1+81 = 9" Dr. Dirt over reg. cb. - used.

| LT.                           | ±                            | RT.                                      |
|-------------------------------|------------------------------|--|
| 306.80<br>6.00<br>26<br>Top   | 305.9<br>6.9<br>26<br>gut.   | 306.3<br>6.5<br>13                       |
|                               |                              | 306.4<br>6.4                             |
|                               |                              | 306.2<br>6.6<br>13                       |
|                               |                              | 305.6<br>7.2<br>26.1                     |
|                               |                              | 306.39<br>6.41<br>26.1                   |
|                               |                              | 306.3<br>6.5<br>40                       |
|                               |                              | 306.31<br>6.49<br>26.1<br>Topcb.         |
|                               |                              | 306.47<br>6.33<br>25<br>Cor. broken      |
|                               |                              | 306.30<br>6.50<br>38.3                   |
|                               |                              | 306.18<br>6.62<br>26.1<br>Topcb.         |
|                               |                              | 306.26<br>6.54<br>33<br>walk             |
|                               |                              | 306.33<br>6.47<br>28.3                   |
|                               |                              | 312.80 ✓                                 |
| 306.28<br>0.61<br>26<br>Top   | 305.5<br>1.4<br>26<br>gut.   | 305.9<br>1.0<br>13                       |
|                               |                              | 306.1<br>0.8                             |
|                               |                              | 305.8<br>1.1<br>13                       |
|                               |                              | 305.2<br>1.7<br>26<br>gut.               |
|                               |                              | 306.44<br>0.85<br>26<br>Top              |
| 305.64<br>1.25<br>25.9<br>Top | 304.7<br>2.2<br>25.9<br>gut. | 305.3<br>1.4<br>13                       |
|                               |                              | 305.4<br>1.5                             |
|                               |                              | 305.1<br>1.8<br>13                       |
|                               |                              | 304.7<br>2.2<br>26<br>gut.               |
|                               |                              | 305.34<br>1.55<br>26<br>Top              |
| 304.07<br>1.92<br>25.8<br>Top | 304.0<br>2.9<br>25.8<br>gut. | 304.2<br>2.5<br>13                       |
|                               |                              | 304.8<br>2.1                             |
|                               |                              | 304.6<br>2.3<br>13                       |
|                               |                              | 304.1<br>2.8<br>26<br>gut.               |
|                               |                              | 304.66<br>2.23<br>26<br>Top              |
| 304.3<br>2.58<br>26<br>Top    | 303.8<br>3.5<br>26<br>gut.   | 303.7<br>3.2<br>13                       |
|                               |                              | 304.1<br>2.8                             |
|                               |                              | 303.8<br>3.1<br>13                       |
|                               |                              | 303.3<br>3.4<br>25.9<br>gut.             |
|                               |                              | 304.07<br>2.87<br>25.9<br>Top            |
|                               |                              | 304.16<br>2.82<br>33<br>walk             |
|                               |                              | 303.13<br>3.16<br>26<br>Topcb.<br>+ Dirt |
|                               |                              | 303.91<br>3.48<br>33<br>walk             |
|                               |                              | 303.91<br>2.98<br>38.3                   |
|                               |                              | 306.89                                   |

5+50

5+46 - Brk. in cb. on Lt.

5+42 - Brk. in cb. on Rt.

5+37 - Brk. in walk on Lt.

5+32 - ± 10' Conc. Dr. on Lt.

5+20

4+96 - ± 10' Conc. Dr. on Lt.

4+90

4+60

4+30

|         |        |        |        |        |        |           |        |        |       |        |
|---------|--------|--------|--------|--------|--------|-----------|--------|--------|-------|--------|
| 308.76  | 308.11 | 308.50 | 307.7  | 308.2  | 308.4  | 308.3     | 307.9  | 308.00 | 309.0 | 309.7  |
| 1       | 4.09   | 4.30   | 5.1    | 4.6    | 4.4    | 4.5       | 4.9    | 4.80   | 3.8   | 3.6    |
| walk    | 33     | 259    | 259    | 13     |        | 13        | 26     | 26     | 33    | 40     |
| 308.50  |        | Top    | gut    |        |        |           | gut    | Top    |       |        |
| 4.30    |        |        |        |        |        |           |        |        |       | 307.67 |
| 25.9    |        |        |        |        |        |           |        |        |       | 5.3    |
| Top cb. |        |        |        |        |        |           |        |        |       | 26     |
|         | 308.69 |        |        | 308.76 |        |           |        |        |       | Top    |
|         | 4.11   |        |        | 4.04   |        |           |        |        |       | cb.    |
|         | 383    |        |        | 33     |        |           |        |        |       |        |
| 308.37  |        |        |        |        |        |           |        |        |       |        |
| 4.43    |        |        | 307.83 |        |        |           |        |        |       |        |
| 33      |        |        | 4.97   |        |        |           |        |        |       |        |
| walk    |        |        | 259    |        |        |           |        |        |       |        |
|         |        |        | Dr.    |        |        |           |        |        |       |        |
| 308.14  |        |        |        |        |        |           |        |        |       |        |
| 4.66    | 307.94 | 307.4  | 307.8  | 307.9  | 307.8  | 307.3     | 307.60 | 308.5  | 309.0 |        |
| 33      | 4.96   | 5.4    | 5.0    | 4.9    | 5.0    | 5.5       | 5.20   | 4.3    | 3.8   |        |
| walk    | 259    | 259    | 13     |        | 13     | 26.1      | 26.1   | 30     | 40    |        |
|         | Top    | gut    |        |        |        | gut       | Top    |        |       |        |
| 308.24  |        |        |        |        |        |           |        |        |       |        |
| 4.56    | 307.52 |        |        |        |        |           |        |        |       |        |
| 33      | 5.28   |        |        |        |        |           |        |        |       |        |
| walk    | 259    |        |        |        |        |           |        |        |       |        |
|         | Dr.    |        |        |        |        |           |        |        |       |        |
| 308.13  | 308.10 | 307.4  | 307.2  | 307.4  | 307.3  | 307.13    | 307.1  | 308.1  |       |        |
| 4.7     | 4.70   | 5.4    | 5.6    | 5.4    | 5.5    | 5.67      | 4.9    | 4.7    |       |        |
| 33      | 259    | 259    | 13     |        | 13     | 26.2      | 30     | 40     |       |        |
| walk    | Top    | gut    |        |        |        | Top cb.   |        |        |       |        |
|         |        |        |        |        |        | + ground. |        |        |       |        |
| 307.13  | 307.1  | 306.9  | 307.1  | 306.9  | 306.9  | 306.4     | 306.10 | 307.1  | 307.4 |        |
| 5.07    | 5.7    | 5.9    | 5.7    | 5.9    | 6.4    | 6.70      | 5.7    | 5.4    |       |        |
| 26      | 26     | 13     |        | 13     | 26.3   | 26.3      | 35     | 40     |       |        |
| Top     | gut.   |        |        |        | ground | Top       | cb.    |        |       |        |
| 307.30  | 306.2  | 306.8  | 306.9  | 306.5  | 306.16 | 306.8     | 307.6  | 306.1  |       |        |
| 5.50    | 6.6    | 6.0    | 5.9    | 6.3    | 6.64   | 6.0       | 5.2    | 6.1    |       |        |
| 25.9    | 25.9   | 13     |        | 13     | 26.3   | 36        | 38     | 40     |       |        |
| Top     | gut.   |        |        |        | Top    | gut.      |        |        |       |        |
|         |        |        |        |        |        |           |        |        |       |        |
|         |        |        |        | 312.80 |        |           |        |        |       |        |



983  
130

4 # Rt 62

0+20

0+00 = N.L. Myrtle

BM.  
I.P. on 11.47 321.52 2.75 310.05 N.W. Myrtle

See P. 5 + 6 for Int.

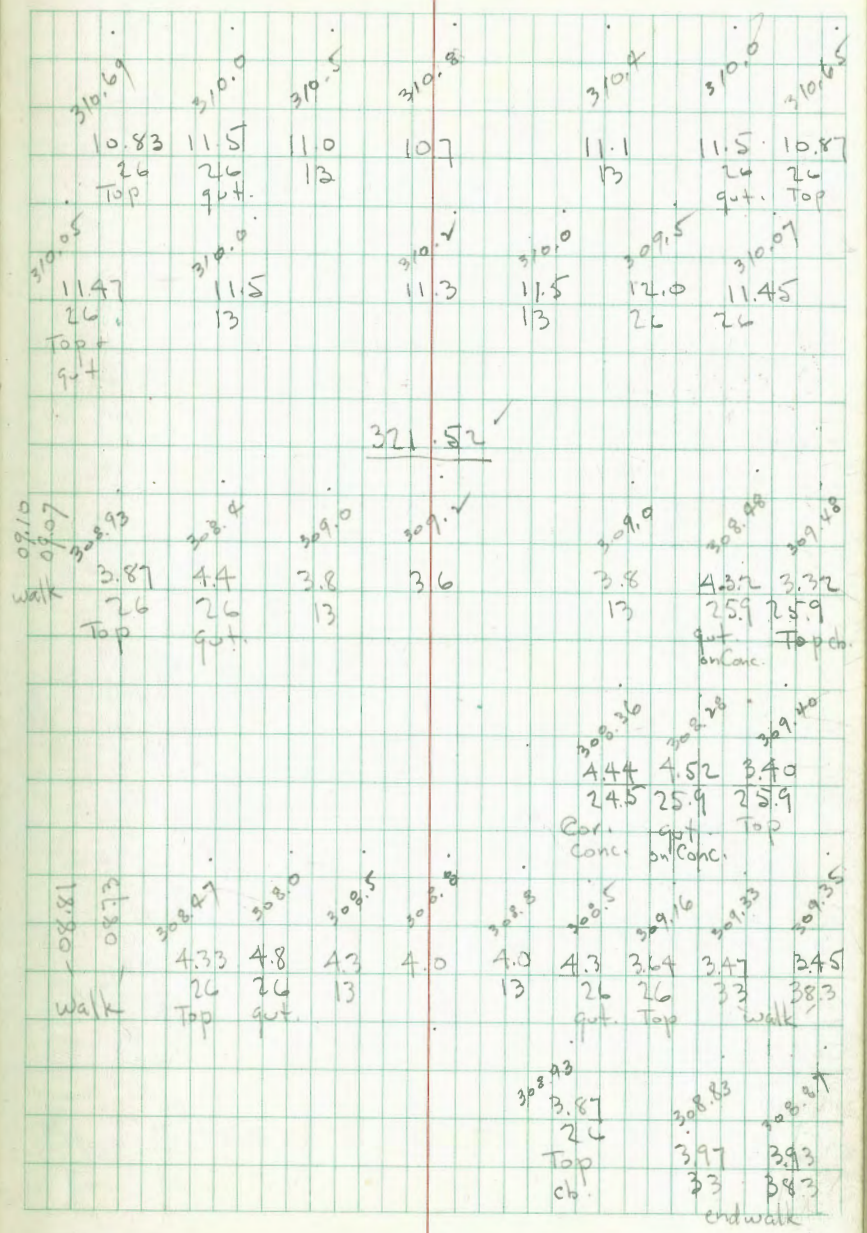
5+98.30 = S.L. Myrtle

5+98.30 = S. end of Conc. slab from inlet  
See sketch - P. 3

5+75

5+61 - Brk. in cb. on Rt.

5+53 - Beg Walk on Rt - Poor Cond.



312.80

3+50

T.P. 11.80 333.14 0.18 321.34

3+00

2+50

2+00

1+60

1+50

1+00

0+50

11.80

333.14

0.18

321.34

± 9' cb. broken out for Dirt Dri

(Not Used)

Lt.

±

Rt.

63

|        |       |       |        |       |       |          |
|--------|-------|-------|--------|-------|-------|----------|
| 321.85 | 321.1 | 321.4 | 321.8  | 321.7 | 320.9 | 321.91   |
| 11.29  | 12.0  | 11.7  | 11.3   | 11.4  | 12.2  | 11.23    |
| 25.9   | 25.9  | 13    |        | 13    | 26    | 26       |
| Top    | gut.  |       |        |       | gut   | Top      |
|        |       |       | 333.14 |       |       |          |
| 320.18 | 319.3 | 319.8 | 320.0  | 319.9 | 319.7 | 320.23   |
| 1.34   | 2.2   | 1.7   | 1.5    | 1.6   | 1.8   | 1.29     |
| 25.9   | 25.9  | 13    |        | 13    | 26    | 26       |
| Top    | gut.  |       |        |       |       |          |
| 318.52 | 317.7 | 318.0 | 318.2  |       | 318.1 | 317.8    |
| 3.00   | 3.8   | 3.5   | 3.3    |       | 3.4   | 3.02     |
| 25.9   | 25.9  | 13    |        |       | 13    | 26       |
| Top    | gut.  |       |        |       |       | gut. Top |
| 316.18 | 315.8 | 316.3 | 316.4  | 316.3 | 316.1 | 316.85   |
| 4.74   | 5.7   | 5.2   | 5.1    | 5.2   | 5.4   | 4.67     |
| 25.9   | 25.9  | 13    |        | 13    | 26    | 26       |
| Top    | gut.  |       |        |       | gut.  | Top      |
| 315.55 | 314.7 |       |        |       |       |          |
| 5.97   | 6.8   |       |        |       |       |          |
| 33     | 25.9  |       |        |       |       |          |
| walk   | gut.  |       |        |       |       |          |
| 315.11 | 314.3 | 314.7 | 314.7  | 314.4 | 314.4 | 315.13   |
| 6.41   | 7.2   | 6.8   | 6.8    | 7.1   | 7.1   | 6.39     |
| 25.9   | 25.9  | 13    |        | 13    | 25.9  | 25.9     |
| Top    | gut.  |       |        |       | gut.  | Top      |
| 313.42 | 312.7 | 313.0 | 313.3  | 313.0 | 312.8 | 313.42   |
| 8.10   | 8.8   | 9.5   | 8.2    | 8.5   | 8.7   | 8.10     |
| 26     | 26    | 13    |        | 13    | 25.9  | 25.9     |
| Top    | gut.  |       |        |       | gut.  | Top      |
| 311.72 | 310.8 | 311.5 | 311.8  | 311.4 | 310.9 | 311.74   |
| 9.80   | 10.7  | 10.0  | 9.7    | 10.1  | 10.6  | 9.78     |
| 26     | 26    | 13    |        | 13    | 25.9  | 25.9     |
| Top    | gut.  |       |        |       | gut.  | Top      |

321.52

7-28-47

7.0

5+75

5+50

5+29 = ± 9' Conc. Dr. on Lt.

5+15 = ± 10' Conc. Dr. on Rt.

5+00

4+92 = ± 10' Conc. Dr. on Lt.

4+60 = ± 11' Conc. Dr. on Rt.

4+50 - cb leans out

4+31 = ± 10' Conc. Dr. on Lt.

4+00

|  | 329.38 | 328.5  | 328.8 | 329.0 | 328.7 | 328.6  | 329.48 |
|--|--------|--------|-------|-------|-------|--------|--------|
|  | 3.76   | 4.6    | 4.3   | 4.1   | 4.4   | 4.5    | 3.66   |
|  | 25.7   | 25.7   | 13    |       | 13    | 25.9   | 25.9   |
|  | Top    | gut.   |       |       |       | gut.   | Top    |
|  | 328.59 | 321.9  | 328.0 | 328.1 | 328.0 | 328.0  | 328.66 |
|  | 4.55   | 5.2    | 5.1   | 5.0   | 5.1   | 5.3    | 4.48   |
|  | 25.7   | 25.7   | 13    |       | 13    | 26     | 26     |
|  | Top    | gut.   |       |       |       | gut.   | Top    |
|  | 328.14 | 321.48 |       |       |       |        |        |
|  | 5.00'  | 5.66   |       |       |       |        |        |
|  | 33     | 25.7   |       |       |       |        |        |
|  | walk   | Dr.    |       |       |       |        |        |
|  |        |        |       |       |       | 327.04 | 327.74 |
|  |        |        |       |       |       | 6.10   | 5.40   |
|  |        |        |       |       |       | 26     | 33.1   |
|  |        |        |       |       |       | Dr.    | walk   |
|  |        |        |       |       |       |        |        |
|  | 326.97 | 326.0  | 326.4 | 326.6 | 326.5 | 326.3  | 326.97 |
|  | 6.17   | 7.1    | 6.7   | 6.5   | 6.6   | 6.8    | 6.17   |
|  | 25.7   | 25.7   | 13    |       | 13    | 26     | 26     |
|  | Top    | gut.   |       |       |       | gut.   | Top    |
|  | 326.83 | 325.89 |       |       |       |        |        |
|  | 6.31   | 7.25   |       |       |       |        |        |
|  | 33     | 25.7   |       |       |       |        |        |
|  | walk   | Dr.    |       |       |       | 324.94 | 325.74 |
|  |        |        |       |       |       | 8.20   | 7.42   |
|  |        |        |       |       |       | 26     | 33.2   |
|  |        |        |       |       |       | Dr.    | walk   |
|  |        |        |       |       |       |        |        |
|  | 325.17 | 324.5  | 324.7 | 325.0 | 324.7 | 324.7  | 325.30 |
|  | 7.97   | 8.6    | 8.4   | 8.1   | 8.4   | 8.4    | 7.84   |
|  | 25.7   | 25.7   | 13    |       | 13    | 26     | 26     |
|  | Top    | gut.   |       |       |       | gut.   | Top    |
|  | 324.68 | 323.95 |       |       |       |        |        |
|  | 8.46   | 9.19   |       |       |       |        |        |
|  | 33     | 25.7   |       |       |       |        |        |
|  | walk   | Dr.    |       |       |       |        |        |
|  |        |        |       |       |       |        |        |
|  | 323.81 | 322.6  | 323.1 | 323.5 | 323.2 | 322.8  | 323.51 |
|  | 9.63   | 10.5   | 10.0  | 9.6   | 9.9   | 10.3   | 9.53   |
|  | 25.9   | 25.9   | 13    |       | 13    | 26     | 26     |
|  | Top    | gut.   |       |       |       | gut.   | Top    |
|  |        |        |       |       |       |        |        |

333.14

1+75 = End

1+25

0+75

0+25

0+00 = NL. of Dwight. = Beg. HC. Pave  
To 175' N. of NL. Dwight.

I.P. on B.M. 7.54 338.53 2.15 330.99 NW Dwight.

for Int. - P 30 - Sketch - P 26

6+00.72 = S.L. Dwight

|                   |                    |            |      |            |                    |                   |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|
| 4.16<br>26<br>Top | 4.81<br>26<br>gut. | 4.20<br>13 | 4.02 | 4.23<br>13 | 4.79<br>26<br>gut. | 4.10<br>26<br>Top |
|-------------------|--------------------|------------|------|------------|--------------------|-------------------|

|                   |                    |            |        |            |                    |                   |
|-------------------|--------------------|------------|--------|------------|--------------------|-------------------|
| 5.13<br>26<br>Top | 5.80<br>26<br>gut. | 5.13<br>13 | 4.94   | 5.16<br>13 | 5.85<br>26<br>gut. | 5.11<br>26<br>Top |
| 332.42            | 331.75             | 332.41     | 332.59 | 332.41     | 331.79             | 332.60            |
| 6.11<br>26<br>Top | 6.78<br>26<br>gut. | 6.12<br>13 | 5.94   | 6.12<br>13 | 6.74<br>26<br>gut. | 5.93<br>26<br>Top |
| 331.47            | 330.84             | 331.44     | 331.54 | 331.40     | 330.68             | 331.41            |
| 7.06<br>26<br>Top | 7.69<br>26<br>gut. | 7.09<br>13 | 6.99   | 7.13<br>13 | 7.85<br>26<br>gut. | 7.12<br>26<br>Top |
| 330.95            | 330.31             | 330.92     | 331.12 | 330.97     | 330.08             | 330.81            |
| 7.58<br>26<br>Top | 8.22<br>26<br>gut. | 7.41<br>13 | 7.41   | 7.56<br>13 | 8.45<br>26<br>gut. | 7.72<br>26<br>Top |

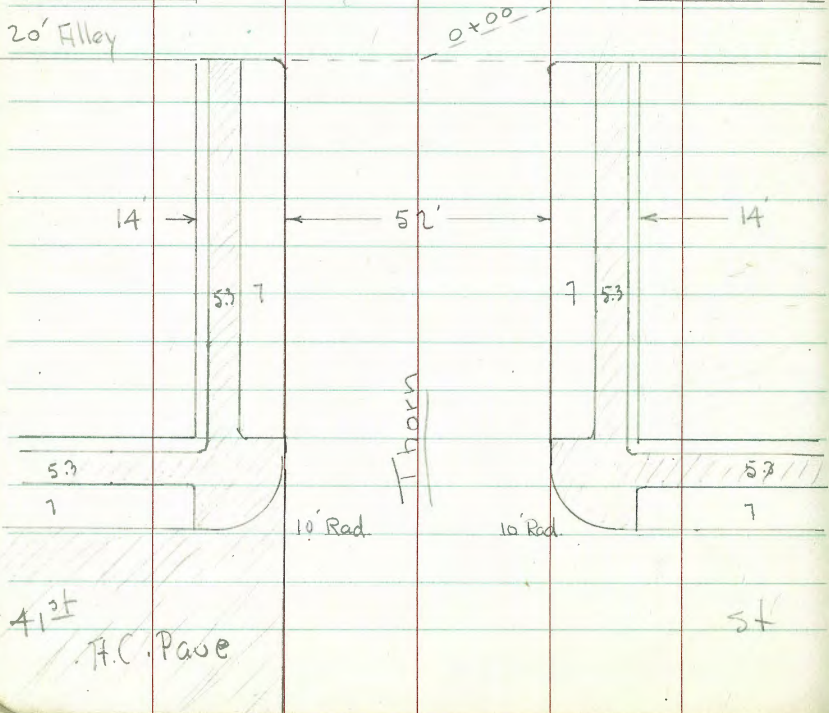
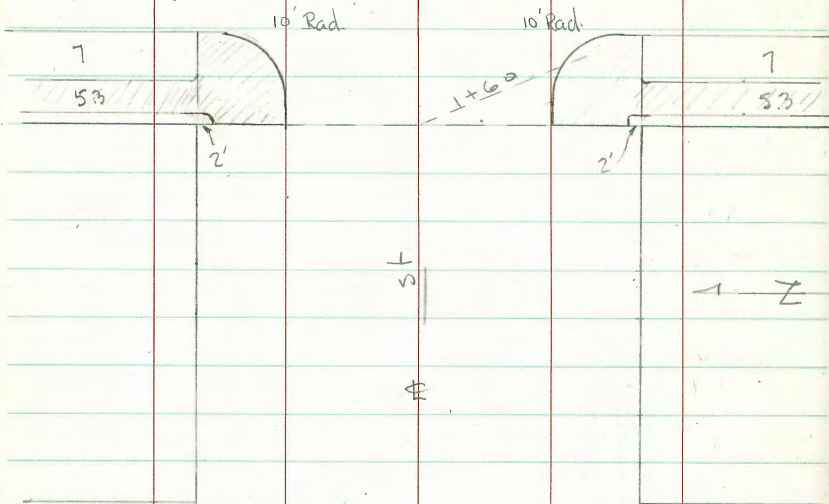
338.53 ✓

|                     |                     |           |       |           |                   |                   |
|---------------------|---------------------|-----------|-------|-----------|-------------------|-------------------|
| 329.97              | 329.1               | 329.5     | 329.7 | 329.4     | 329.3             | 330.36            |
| 3.17<br>25.8<br>Top | 4.0<br>25.8<br>gut. | 3.6<br>13 | 3.4   | 3.7<br>13 | 3.8<br>26<br>gut. | 2.78<br>26<br>Top |

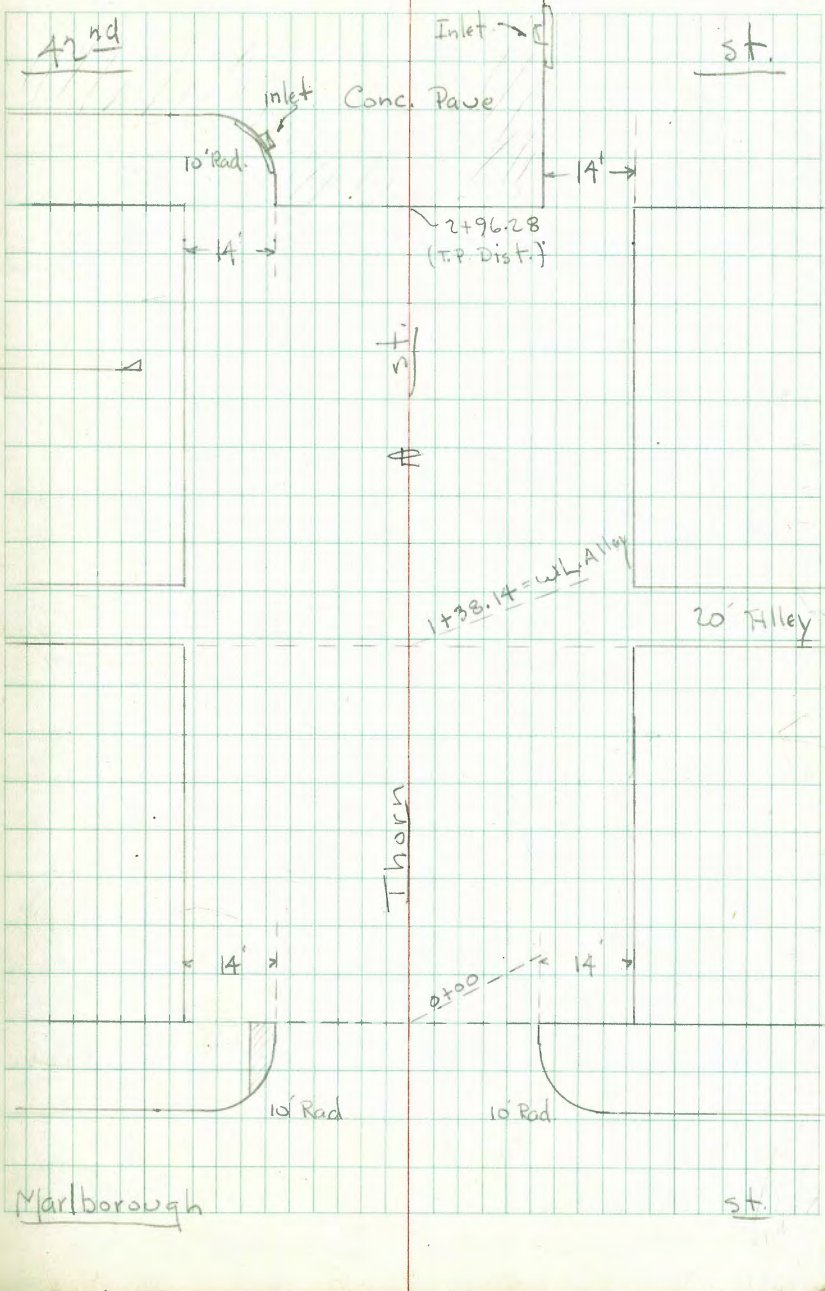
333.14

X-Sect. Thorn - from Hilley to Marlborough  
 Both ways - W.O 31385 - 7-28-47  
 70.

Marlborough Dirt - Graded. st.



41st  
 A.C. Pavement



Marlborough

st.

indexed  
c.s.k.

X- Sect. Thorn - 80' St. - 14' cbs. - from  
W.L. Alley E. of 41<sup>st</sup> to W.L. Alley  
W. of 42<sup>nd</sup>

0+00 = E.L. Marlborough

for Int. - See P. 58

1+60 = W.L. Marlborough

1+59 - 26.8' Rt = ± P. pole # 4149

1+20

0+70

Dirt - Graded - No cbs walk

0+20

0+00 = W.L. of 20' Alley - E. of 41<sup>st</sup> = end of cbs.

B.M. 7.24 309.06

310.82 NW. Thorn  
+ Marlborough

301.82 ?

Lt. = N.

±

Rt. S

67

301.06

|     |      |      |      |     |     |     |             |           |
|-----|------|------|------|-----|-----|-----|-------------|-----------|
| 7.2 | 8.11 | 8.00 | 8.4  | 7.9 | 7.8 | 8.1 | 8.52        | 8.25      |
| 40  | 30.7 | 25.9 | 25.9 | 13  |     | 13  | 26          | 38.3      |
|     | edge | Top  | gut. |     |     |     | Top-end cb. | Cor. Ret. |
|     | Ret. |      |      |     |     |     | gut.        |           |

300.54

301.76

|           |         |      |     |     |     |      |         |           |
|-----------|---------|------|-----|-----|-----|------|---------|-----------|
| 7.10      | 7.30    | 7.8  | 7.7 | 7.6 | 8.0 | 8.5  | 7.87    | 7.68      |
| 38        | 25.4    | 25.8 | 13  |     | 13  | 25.9 | 25.9    | 38        |
| Cor. Ret. | Top     | gut. |     |     |     | gut. | Top     | Cor. Ret. |
|           | end cb. |      |     |     |     |      | end cb. |           |

301.19

302.6

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 6.2 | 6.6 | 7.1 | 6.6 | 6.5 | 6.9 | 7.7 | 6.8 | 6.7 |
| 40  | 26  | 25  | 13  |     | 13  | 25  | 26  | 40  |

303.8

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 4.5 | 5.2 | 6.0 | 5.4 | 5.2 | 5.6 | 6.4 | 5.5 | 5.3 |
| 40  | 26  | 24  | 13  |     | 13  | 25  | 26  | 40  |

|     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 3.2 | 4.0 | 4.6 | 4.2 | 4.0 | 4.3 | 4.7 | 4.1 | 3.8 |
| 40  | 26  | 24  | 13  |     | 13  | 25  | 26  | 40  |

306.31

|         |      |        |      |     |     |      |        |         |           |
|---------|------|--------|------|-----|-----|------|--------|---------|-----------|
| 2.52    | 2.58 | 2.75   | 3.7  | 3.4 | 3.2 | 3.5  | 3.8    | 3.25    | 1.92      |
| 40      | 33   | 26     | 26   | 13  |     | 13   | 26     | 26      | 39.6      |
| Top-end | Brk. | Top    | gut. |     |     | gut. | Top    | Top-end | Ret. gut. |
| cb. r   | inc. | 2 Rad. |      |     |     |      | 2 Rad. |         |           |
| gut.    |      |        |      |     |     |      | Ret.   |         |           |

305.81

309.06

1+38.14 = WL 20' Alley = end.

1+36-27.5 Rt. = ± P. pole # P 4175

1+00

0+60

0+20

Dirt - Graded - No cb. + walk

Lt.

±

Rt.

68

|     |     |     |     |     |     |  |  |  |
|-----|-----|-----|-----|-----|-----|--|--|--|
| 7.9 | 7.5 | 7.8 | 8.9 | 8.5 | 8.6 |  |  |  |
| 40  | 38  | 29  | 24  | 13  |     |  |  |  |

|     |     |     |
|-----|-----|-----|
| 9.0 | 9.4 | 9.7 |
| 13  | 26  | 40  |

|     |                      |     |  |  |  |  |  |  |
|-----|----------------------|-----|--|--|--|--|--|--|
| 7.9 | <sup>301.1</sup> 8.0 | 8.7 |  |  |  |  |  |  |
| 40  | 25                   | 24  |  |  |  |  |  |  |

<sup>300.9</sup>

|     |     |     |     |  |  |  |  |  |
|-----|-----|-----|-----|--|--|--|--|--|
| 8.3 | 8.2 | 8.5 | 9.1 |  |  |  |  |  |
| 13  |     | 13  | 26  |  |  |  |  |  |

<sup>300.0</sup>

|     |
|-----|
| 9.1 |
| 40  |

|     |     |     |     |     |     |  |     |     |     |     |
|-----|-----|-----|-----|-----|-----|--|-----|-----|-----|-----|
| 8.5 | 7.9 | 7.9 | 8.6 | 8.1 | 7.9 |  | 8.1 | 8.8 | 8.7 | 8.3 |
| 40  | 37  | 26  | 25  | 13  |     |  | 13  | 25  | 26  | 40  |

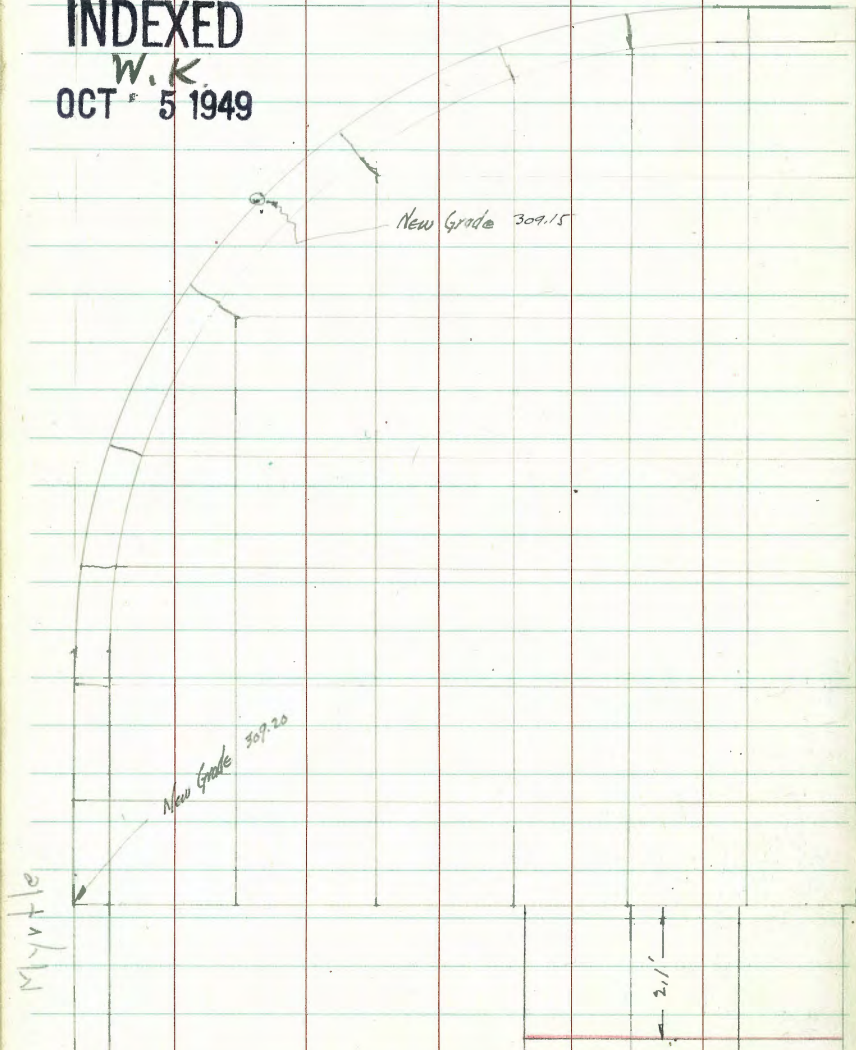
<sup>301.3</sup>

|     |     |     |     |     |     |     |     |  |     |
|-----|-----|-----|-----|-----|-----|-----|-----|--|-----|
| 7.3 | 7.9 | 8.4 | 7.9 | 7.8 | 8.0 | 8.4 | 8.2 |  | 8.0 |
| 40  | 24  | 25  | 13  |     | 13  | 25  | 26  |  | 40  |

309.06

Detail of S.W. Int. - Marlborough +  
Scale = 1" = 3'

INDEXED  
W.K.  
OCT 5 1949



Myrtle

New Grade 309.09

Marlborough



1.9'

Ex. E/ 309.10

Ex. E/ 309.19

W. Line MARLBOROUGH

S-Line Myrtle



Detail N.E. Ret. - 44<sup>th</sup> + Myrtle  
1" = 3'

70

44<sup>th</sup>

↑  
N  
↓

Myrtle

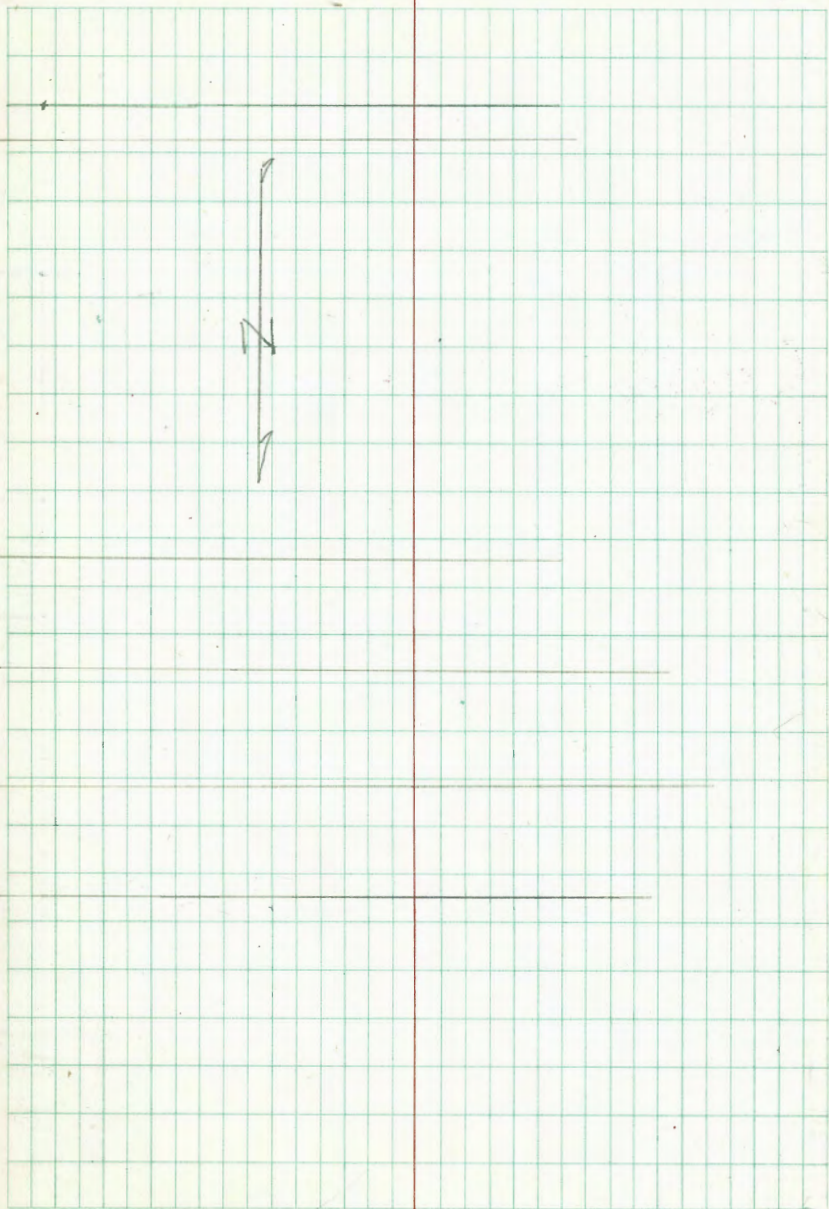
Myrtle

44 ft

N.W. Cor.

71

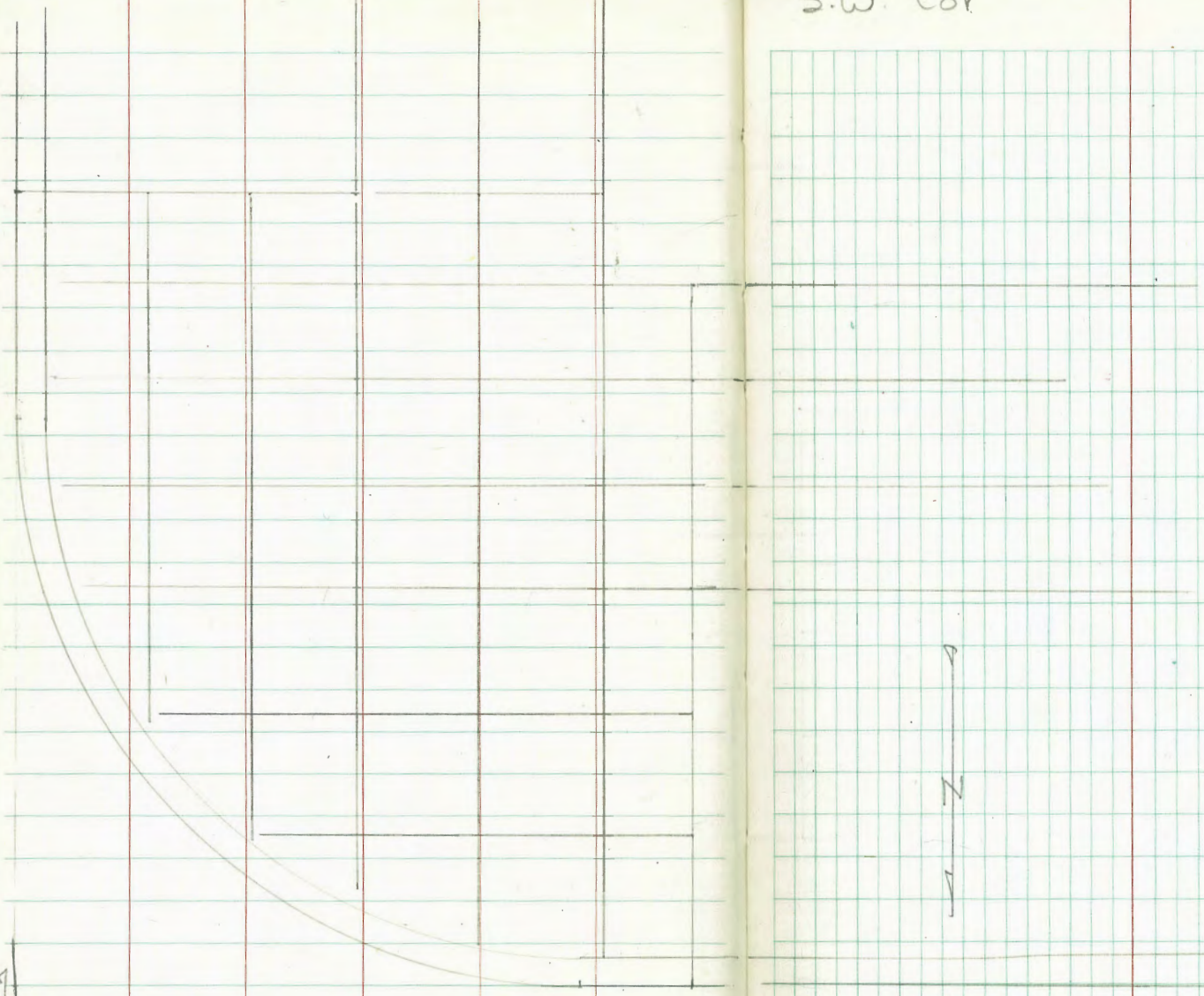
N



S.W. Cor

72

44 1/2



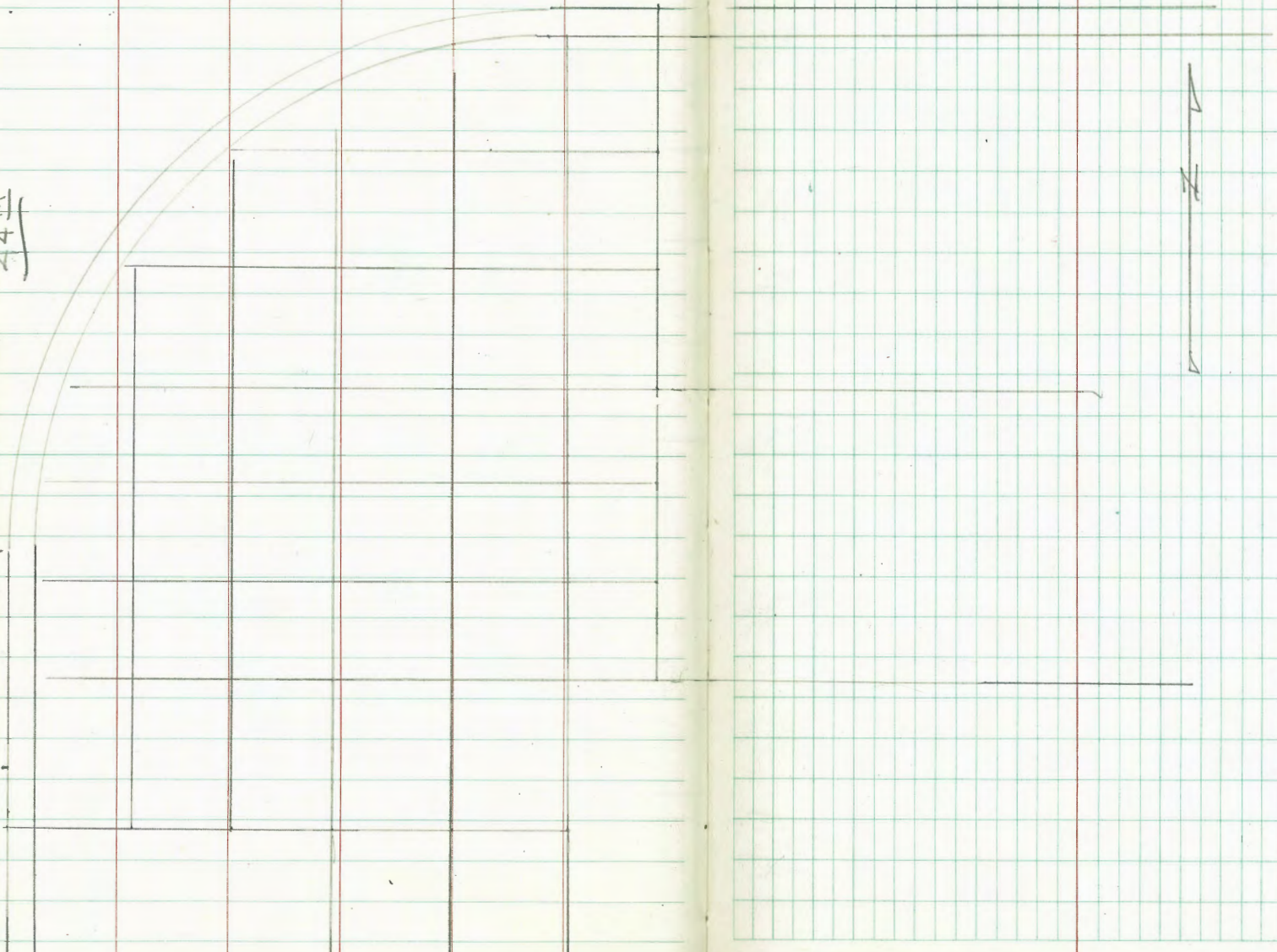
Myrtle

s.E. Cor.

Myrtle

73

4  
4  
4



X-sec portions of Paved Alley Between Van Dyke  
 & 43rd University Ave to Wrightman  
 All 49 City Hts  
 Allen

0+55

0+50

0+45

0+40

0+35

0+30

0+25

0+20 = Man hole (Source)

0+15

0+10

0+05

W/ends pavement

X-sectioning South to only

0+00 = Sky line University Ave

B.M. = NW BP Van Dyke + Wrightman - E.L. = 354.61

INDEXED  
 JER

NOV 24 1954

NT = 214 -

20' alley

RT = W14

74

|                    |                   |                   |                    |                     |
|--------------------|-------------------|-------------------|--------------------|---------------------|
| 5840<br>10         | 5827<br>5         | 5815              | 5822<br>3          | 5840<br>10          |
| 5838<br>10         | 5825<br>5         | 5815              | 5820<br>30         | 5839<br>10          |
|                    | 5841<br>10        | 5827<br>5         | 5815               | 5820<br>35          |
|                    |                   |                   |                    | 5839<br>10          |
| 5844<br>10         | 5834<br>5         | 5823              | 5825<br>35         | 5838<br>10          |
| 5845<br>10         | 5841<br>5         | 5832              | 5838<br>35         | 5841<br>10          |
|                    | 5845<br>10        | 5842<br>5         | 5842<br>35         | 5845<br>10          |
| 5858<br>10         | 5840<br>5         | 5837              | 5848<br>35         | 5846<br>10          |
|                    | 5851<br>10        | 5840<br>5         | 5837<br>Rim<br>SMH | 5848<br>35          |
|                    |                   |                   |                    | 5845<br>10          |
| 5853<br>10         | 5844<br>5         | 5840              | 5851<br>35         | 5847<br>10          |
|                    | 5851<br>10        | 5846<br>5         | 5841               | 5851<br>35          |
|                    |                   |                   |                    | 5845<br>10          |
|                    | 5855<br>10        | 5850<br>5         | 5845               | 5853<br>35          |
|                    |                   |                   |                    | 5851<br>10          |
| 5863<br>99<br>T.C. | 5863<br>99<br>TUT | 5855<br>5<br>Circ | 5851<br>5<br>Circ  | 5878<br>5<br>Circ   |
|                    |                   |                   |                    | 5840<br>99<br>TUT   |
|                    |                   |                   |                    | 5851<br>99<br>Tapel |

Direct elevation Rod used - add 300' to each  
 elevation shown -

X-sec Alley Pavement cont.

2+05

2+00

Pavement from 2+00 to 3+00 is Pavement that does not drain and is origin of Complaint

1+50

1+00 - 10° LT = 2.14' serves stores on side of univ  
wide conc drive to ely

0+95

0+90

0+85

0+80

0+75

0+70

0+65

0+60

LT = ely

20' Alley

RT = W14

75

5773  
10

5762  
5

5758

5784  
5

5811  
10

5774  
10

5762  
5

5758

5780  
5

5786  
10

5795  
10

5786  
5

5781

5795  
5

5812  
10

5819  
10

5808  
5

5799

5817  
5

5822  
10

5814  
10

5806  
5

5799

5815  
5

5829  
10

5815  
10

5809  
5

5802

5818  
5

5830  
10

5818  
10

5808  
5

5800

5811  
3

5836  
10

5820  
10

5813  
5

5804

5814  
3

5832  
10

5824  
10

5813  
5

5807

5820  
3

5834  
10

5828  
10

5821  
5

5813

5821  
3

5832  
10

5834  
10

5825  
5

5815

5822  
3

5837  
10

5841  
10

5839  
5

5815

5823  
3

5838  
10

Direct elev Rod used - add 300' to all elev.

X-sec Alley Pavement Cont

LT=614

X  
20' Alley

RT=614

76

2+50

57<sup>64</sup><sub>10</sub>

57<sup>60</sup><sub>5</sub>

57<sup>63</sup>

57<sup>76</sup><sub>3</sub>

57<sup>87</sup><sub>10</sub>

2+45

57<sup>64</sup><sub>10</sub>

57<sup>62</sup><sub>5</sub>

57<sup>64</sup>

57<sup>78</sup><sub>3</sub>

57<sup>87</sup><sub>10</sub>

2+40

57<sup>71</sup><sub>10</sub>

57<sup>65</sup><sub>5</sub>

57<sup>61</sup>

57<sup>74</sup><sub>5</sub>

57<sup>87</sup><sub>10</sub>

2+35

57<sup>70</sup><sub>10</sub>

57<sup>60</sup><sub>5</sub>

57<sup>56</sup>

57<sup>70</sup><sub>5</sub>

57<sup>90</sup><sub>10</sub>

2+30

57<sup>67</sup><sub>10</sub>

57<sup>58</sup><sub>5</sub>

57<sup>52</sup>

57<sup>67</sup><sub>5</sub>

57<sup>94</sup><sub>10</sub>

2+25

57<sup>67</sup><sub>10</sub>

57<sup>57</sup><sub>5</sub>

57<sup>57</sup>

57<sup>80</sup><sub>5</sub>

58<sup>05</sup><sub>10</sub>

2+20

57<sup>66</sup><sub>10</sub>

57<sup>60</sup><sub>5</sub>

57<sup>60</sup>

57<sup>86</sup><sub>5</sub>

58<sup>13</sup><sub>10</sub>

2+15

57<sup>68</sup><sub>10</sub>

57<sup>60</sup><sub>5</sub>

57<sup>58</sup>

57<sup>85</sup><sub>5</sub>

58<sup>16</sup><sub>10</sub>

2+10

57<sup>68</sup><sub>10</sub>

57<sup>59</sup><sub>5</sub>

57<sup>56</sup>

57<sup>83</sup><sub>5</sub>

58<sup>18</sup><sub>10</sub>

Direct elev reduced - add 300' to each elev.

X-sec Alley Pavement Cont

LT=014

20' Alley

RT=017

17

3+00

5741  
10

5731  
5

5726

5748  
5

5769  
10

2+95

5741  
10

5731  
5

5724

5744  
5

5768  
10

2+90

5741  
10

5735  
5

5727

5746  
5

5765  
10

2+85

5746  
10

5736  
5

5731

5747  
5

5765  
10

2+80

5749  
10

5744  
5

5737

5753  
5

5773  
10

2+75

5755  
10

5747  
5

5738

5757  
5

5774  
10

2+70

5755  
10

5748  
5

5737

5750  
3

5772  
10

2+65

5761  
10

5751  
5

5742

5754  
3

5770  
10

2+60

5765  
10

5756  
5

5750

5761  
3

5773  
10

2+55

5766  
10

5758  
5

5758

5769  
3

5784  
10

Directley Rod used - add 300' to all elev.



X-sec Alley Parc cont

3+65

3+60

3+55

3+50

3+45

3+40

3+35

3+30

3+25

3+20

3+15

3+10

3+05

LT=ely

20' alley

RT=wily

78

57<sup>03</sup>

57<sup>06</sup>  
RIND SMH

57<sup>11</sup>

57<sup>13</sup>

57<sup>07</sup>

57<sup>08</sup>

57<sup>10</sup>

57<sup>14</sup>

57<sup>24</sup>  
10

57<sup>15</sup>  
5

57<sup>15</sup>

57<sup>36</sup>  
5

57<sup>60</sup>  
10

57<sup>25</sup>  
10

57<sup>17</sup>  
5

57<sup>18</sup>

57<sup>40</sup>  
5

57<sup>55</sup>  
8

57<sup>25</sup>  
10

57<sup>27</sup>  
10

57<sup>21</sup>  
5

57<sup>20</sup>

57<sup>42</sup>  
5

57<sup>59</sup>  
8

57<sup>99</sup>  
10

57<sup>35</sup>  
10

57<sup>30</sup>  
5

57<sup>24</sup>

57<sup>44</sup>  
5

57<sup>58</sup>  
8

57<sup>89</sup>  
10

57<sup>35</sup>  
10

57<sup>31</sup>  
5

57<sup>25</sup>

57<sup>42</sup>  
5

57<sup>58</sup>  
8

57<sup>95</sup>  
10

Direct Rod used - add 300' to all elevs.

X-sec Alley Pavement cont

LT = E14

20'  
Alley

RT = W14-

79

Alley drains Sly to Wightman St

4+00

56<sup>50</sup>

3+95

56<sup>61</sup>

3+90

56<sup>65</sup>

3+85

56<sup>67</sup>

3+80

56<sup>70</sup>

3+75

56<sup>79</sup>

3+70

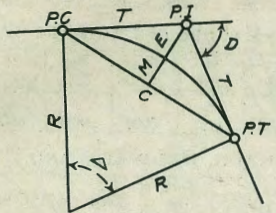
56<sup>80</sup>

2-26-47-

① shall we save gutter - Marlborough & Redwood?

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

- Radius  $= R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve  $= D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)
- Tangent  $= T = R \tan \frac{\Delta}{2}$  (3) Length of Curve  $= L = 100 \frac{\Delta}{D}$  (4)
- Middle ordinate  $= M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)
- External  $= E = T \tan \frac{\Delta}{4}$  (7)  $= R + \cos \frac{\Delta}{2} R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)
- Long Chord  $= C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta$  = Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I. = Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I.  $- T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C.  $+ L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 - Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100) = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^2$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$  and from Table V correction = .10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

3434 - Marlborough

321.52

340

324.92

12.85

312.07

2.35

314.42

4.37

310.05

H

0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0

se to  
ns of  
mple  
43.9.

S A.

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

32.62  
12.32  
20.30

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.2  | 8.3  | 8.5  | 8.6  | 8.8  | 8.9  | 9.1  | 9.2  | 9.4  | 0  |
| 1  | 9.5  | 9.7  | 9.8  | 10.0 | 10.1 | 10.3 | 10.4 | 10.6 | 10.7 | 10.9 | 1  |
| 2  | 11.0 | 11.2 | 11.3 | 11.5 | 11.6 | 11.8 | 11.9 | 12.1 | 12.2 | 12.4 | 2  |
| 3  | 12.5 | 12.7 | 12.8 | 13.0 | 13.1 | 13.3 | 13.4 | 13.6 | 13.7 | 13.9 | 3  |
| 4  | 14.0 | 14.2 | 14.3 | 14.5 | 14.6 | 14.8 | 14.9 | 15.1 | 15.2 | 15.4 | 4  |
| 5  | 15.5 | 15.7 | 15.8 | 16.0 | 16.1 | 16.3 | 16.4 | 16.6 | 16.7 | 16.9 | 5  |
| 6  | 17.0 | 17.2 | 17.3 | 17.5 | 17.6 | 17.8 | 17.9 | 18.1 | 18.2 | 18.4 | 6  |
| 7  | 18.5 | 18.7 | 18.8 | 19.0 | 19.1 | 19.3 | 19.4 | 19.6 | 19.7 | 19.9 | 7  |
| 8  | 20.0 | 20.2 | 20.3 | 20.5 | 20.6 | 20.8 | 20.9 | 21.1 | 21.2 | 21.4 | 8  |
| 9  | 21.5 | 21.7 | 21.8 | 22.0 | 22.1 | 22.3 | 22.4 | 22.6 | 22.7 | 22.9 | 9  |
| 10 | 23.0 | 23.2 | 23.3 | 23.5 | 23.6 | 23.8 | 23.9 | 24.1 | 24.2 | 24.4 | 10 |
| 11 | 24.5 | 24.7 | 24.8 | 25.0 | 25.1 | 25.3 | 25.4 | 25.6 | 25.7 | 25.9 | 11 |
| 12 | 26.0 | 26.2 | 26.3 | 26.5 | 26.6 | 26.8 | 26.9 | 27.1 | 27.2 | 27.4 | 12 |
| 13 | 27.5 | 27.7 | 27.8 | 28.0 | 28.1 | 28.3 | 28.4 | 28.6 | 28.7 | 28.9 | 13 |
| 14 | 29.0 | 29.2 | 29.3 | 29.5 | 29.6 | 29.8 | 29.9 | 30.1 | 30.2 | 30.4 | 14 |
| 15 | 30.5 | 30.7 | 30.8 | 31.0 | 31.1 | 31.3 | 31.4 | 31.6 | 31.7 | 31.9 | 15 |
| 16 | 32.0 | 32.2 | 32.3 | 32.5 | 32.6 | 32.8 | 32.9 | 33.1 | 33.2 | 33.4 | 16 |
| 17 | 33.5 | 33.7 | 33.8 | 34.0 | 34.1 | 34.3 | 34.4 | 34.6 | 34.7 | 34.9 | 17 |
| 18 | 35.0 | 35.2 | 35.3 | 35.5 | 35.6 | 35.8 | 35.9 | 36.1 | 36.2 | 36.4 | 18 |
| 19 | 36.5 | 36.7 | 36.8 | 37.0 | 37.1 | 37.3 | 37.4 | 37.6 | 37.7 | 37.9 | 19 |
| 20 | 38.0 | 38.2 | 38.3 | 38.5 | 38.6 | 38.8 | 38.9 | 39.1 | 39.2 | 39.4 | 20 |
| 21 | 39.5 | 39.7 | 39.8 | 40.0 | 40.1 | 40.3 | 40.4 | 40.6 | 40.7 | 40.9 | 21 |
| 22 | 41.0 | 41.2 | 41.3 | 41.5 | 41.6 | 41.8 | 41.9 | 42.1 | 42.2 | 42.4 | 22 |
| 23 | 42.5 | 42.7 | 42.8 | 43.0 | 43.1 | 43.3 | 43.4 | 43.6 | 43.7 | 43.9 | 23 |
| 24 | 44.0 | 44.2 | 44.3 | 44.5 | 44.6 | 44.8 | 44.9 | 45.1 | 45.2 | 45.4 | 24 |
| 25 | 45.5 | 45.7 | 45.8 | 46.0 | 46.1 | 46.3 | 46.4 | 46.6 | 46.7 | 46.9 | 25 |
| 26 | 47.0 | 47.2 | 47.3 | 47.5 | 47.6 | 47.8 | 47.9 | 48.1 | 48.2 | 48.4 | 26 |
| 27 | 48.5 | 48.7 | 48.8 | 49.0 | 49.1 | 49.3 | 49.4 | 49.6 | 49.7 | 49.9 | 27 |
| 28 | 50.0 | 50.2 | 50.3 | 50.5 | 50.6 | 50.8 | 50.9 | 51.1 | 51.2 | 51.4 | 28 |
| 29 | 51.5 | 51.7 | 51.8 | 52.0 | 52.1 | 52.3 | 52.4 | 52.6 | 52.7 | 52.9 | 29 |
| 30 | 53.0 | 53.2 | 53.3 | 53.5 | 53.6 | 53.8 | 53.9 | 54.1 | 54.2 | 54.4 | 30 |
| 31 | 54.5 | 54.7 | 54.8 | 55.0 | 55.1 | 55.3 | 55.4 | 55.6 | 55.7 | 55.9 | 31 |
| 32 | 56.0 | 56.2 | 56.3 | 56.5 | 56.6 | 56.8 | 56.9 | 57.1 | 57.2 | 57.4 | 32 |
| 33 | 57.5 | 57.7 | 57.8 | 58.0 | 58.1 | 58.3 | 58.4 | 58.6 | 58.7 | 58.9 | 33 |
| 34 | 59.0 | 59.2 | 59.3 | 59.5 | 59.6 | 59.8 | 59.9 | 60.1 | 60.2 | 60.4 | 34 |
| 35 | 60.5 | 60.7 | 60.8 | 61.0 | 61.1 | 61.3 | 61.4 | 61.6 | 61.7 | 61.9 | 35 |
| 36 | 62.0 | 62.2 | 62.3 | 62.5 | 62.6 | 62.8 | 62.9 | 63.1 | 63.2 | 63.4 | 36 |
| 37 | 63.5 | 63.7 | 63.8 | 64.0 | 64.1 | 64.3 | 64.4 | 64.6 | 64.7 | 64.9 | 37 |
| 38 | 65.0 | 65.2 | 65.3 | 65.5 | 65.6 | 65.8 | 65.9 | 66.1 | 66.2 | 66.4 | 38 |
| 39 | 66.5 | 66.7 | 66.8 | 67.0 | 67.1 | 67.3 | 67.4 | 67.6 | 67.7 | 67.9 | 39 |
| 40 | 68.0 | 68.2 | 68.3 | 68.5 | 68.6 | 68.8 | 68.9 | 69.1 | 69.2 | 69.4 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.