

1785

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \times 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.  
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1785

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Vernon Park, Locate Bldg's 8-  
Cresta Real } Sewer 10 to 56  
Cuesta Loma } Profiles 57 to 64

X Section Alley 26

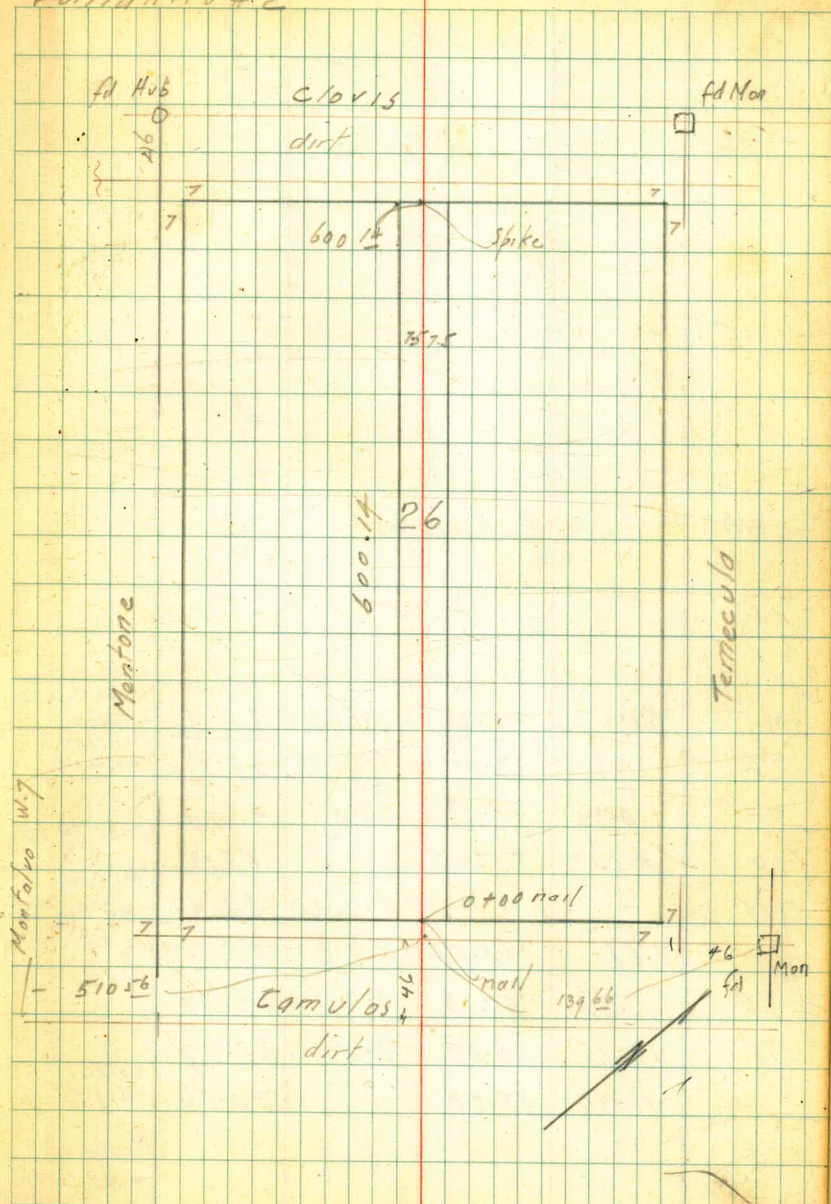
W25001

Begg  
Greer  
Roberts

Loma Alto #2

Indexed  
C.S.R.

1



	+	#1	-	E1	
- 06					
- 15					
- 30		Camutos			
set B.M.	695	<u>31.05</u>	8.96	<u>24.10</u>	Spike on Pole N side Corn Way between Mentone & Terrecola
TP	1.18	33.06	12.25	31.88	
TP	0.39	44.13	11.51	43.74	
TP	+ 0.17	55.25	10.43	55.08	Spike PP SW clovis & Mentone
B.M.			3.20	<u>62.31</u>	62.32 -01
	7.68	65.51	1.23	57.83	
TP	11.26	59.06	0.22	47.80	
TP	12.75	48.02	0.49	35.27	
	11.70	35.76		24.06	Spike SW PP Mentone & W.P. Loma Blvd

2

L	R	R
29.05	22.75	17.75
4.0	9.3	13.3
5.0		4.0
25.65	20.35	15.15
5.4	18.7	15.9
5.0		5.0
25.75	20.65	15.25
5.3	10.4	15.8
5.0		5.0

31.05

set by Moore on sewer survey  
old lat found marked 62.32

	+	#1	-	
TP	11.27	46.12	1.61	34.85
1+50		<u>46.12</u>		

1+00				
TP	8.62	36.46	3.21	27.84
+75	7.04	4 PPole	PA 4310	
+51	7.04	end chic house		
+51		chic wire	across Alley	

+ 50

+ 40	7.04	chic House	beg	
+ 40		chic wire	across alley	
+26 <sup>5</sup>	7.8 P.	end chick wire		
0+10 <sup>5</sup>	7.2 P.	chick wire	fence	

+ 02

0+00

31.05

Alley 26 Loma Alta #2 3

33.86	33.16	32.76	32.11	31.46
2.6	3.3	3.7	4.3	5.0
20	75		75	20
31.36	30.76	29.96	29.56	29.06
5.1	5.7	6.5	6.9	7.4
20	75		75	15
		36.46		
	27.65	27.65	27.05	26.85
	3.4	3.4	4.0	4.2
	75		75	15
	25.35	26.35	25.85	25.45
5.7	4.7	5.2	5.6	6.4
5	75		75	15
25.05	25.55	25.25	25.05	24.35
6.0	5.5	5.8	6.0	6.7
15	75		75	15
		31.05		

	T	H1	
2+99	6.8	Lt	end shed, beg chic wire
2+93	6.8	Lt	beg shed
2+93	7.1	Lt	end hd fence

+85

+82 8.1 Rt end Picket

2+75

2+75 7.1 Lt Beard Fence

2+50 7.9 Rt Picket fence

2+38 7.7 Lt PR JPA 4340 434613#

2+00

46.12

	T	H1		
	0.7		45.42	
	20			
	0.7		45.42	
	7.5			
	3.2		42.92	
	3.8		42.32	
	7.5			
	4.8		41.32	
	7.6			
	5.7		40.42	
	20			
	1.6		44.52	
	15			
	3.3		42.92	
	7.5			
	4.2		41.92	
	5.1		41.02	
	7.5			
	6.0		40.12	
	15			
	4.8		41.32	
	5.6		40.52	
	7.5			
	6.2		39.92	
	6.7		39.42	
	7.5			
	7.5		38.62	
	18			
	8.7		37.42	
	20			
	9.7		36.42	
	7.5			
	10.3		35.82	
	11.0		35.12	
	7.5			
	12.2		33.92	
	20			

46.12





+ H1 -

+95 8.6 Rt end eugenia hedge

5+75

5+69 8.7 Lt end Picket

9.2 Rt beg eugenia hedge

5+50 8.1 Rt end chic wire fence

5+50

5+15

7.3 Rt end of Lath beg. chic wire

5+00 7.1 Lt P.P. A4384

+95 7.1 Lt

+95 10.0 Lt beg Picket

H+50

60.34

Alley 26 Loma Alto #2

6

H H Rt

2.5  
10 57.84

2.5  
8 57.84

3.2 57.14

4.3  
7.5 56.04

4.4 55.94

4.6  
7.5 55.74

1.9  
10 58.54

2.5  
7.5 57.84

3.7  
5.0 56.64

4.0 56.34

4.3  
7.5 56.04

4.8 55.54

2.2  
10 58.14

2.8  
7.5 57.54

3.8  
5.5 56.54

4.1 56.24

4.6  
7.5 55.74

5.0 55.34

58.04

57.24

56.34

57.34

2.3  
7.5

3.1

4.0  
7.5

3.0  
2.0

56.44

56.04

55.24

54.74

3.9  
1.5

4.3  
7.5

5.1

5.6  
7.5

60.34

+ H1 -

BM 4.47 65.11 2.80 62.31 62.92  
 TP -1.13 60.64 -01

6+30<sup>14</sup> q clovis

6+14<sup>14</sup>

6+00<sup>14</sup> South line clovis

7.53 61.77  
 TP 6.10 54.24

60.34

Clovis +  
 Mentone

Alley 26 Land Alto #2

L RT

7

59.57  
 4.2 12.0  
 50 50

57.27  
 4.5 12.7  
 50.0 50.0

56.27  
 5.5 7.2 7.6  
 20 75 50 75 15

54.07  
 7.7 49.07  
 53.47 49.07

54.37  
 7.4 7.6  
 7.9

61.77

60.34

Vernon Park.  
Locate Buildings.

Work Order # 25001

Sammermeyer  
W Marc  
Sherman  
8-11-47

- = Fd. conc. Mon.
- = Fd. Hub + City disk.
- ① = Building Number

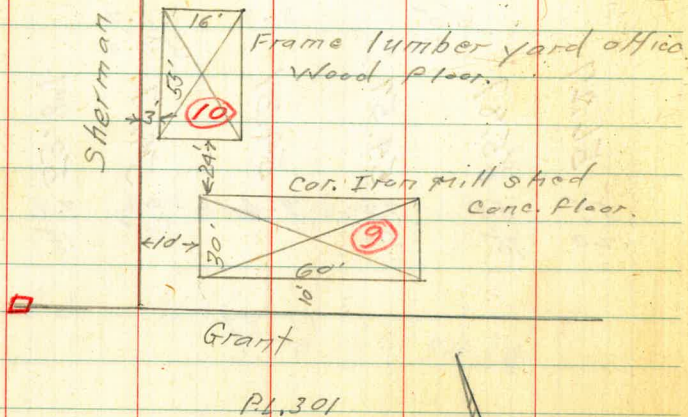
see  
1693-147  
871-50  
T.P. #1  
Map 569

#1-2-3-4-5+6 are Cor. Iron Bldgs.

#7 is Conc. Milk House

#8 is Frame dwelling

#11 - " " "

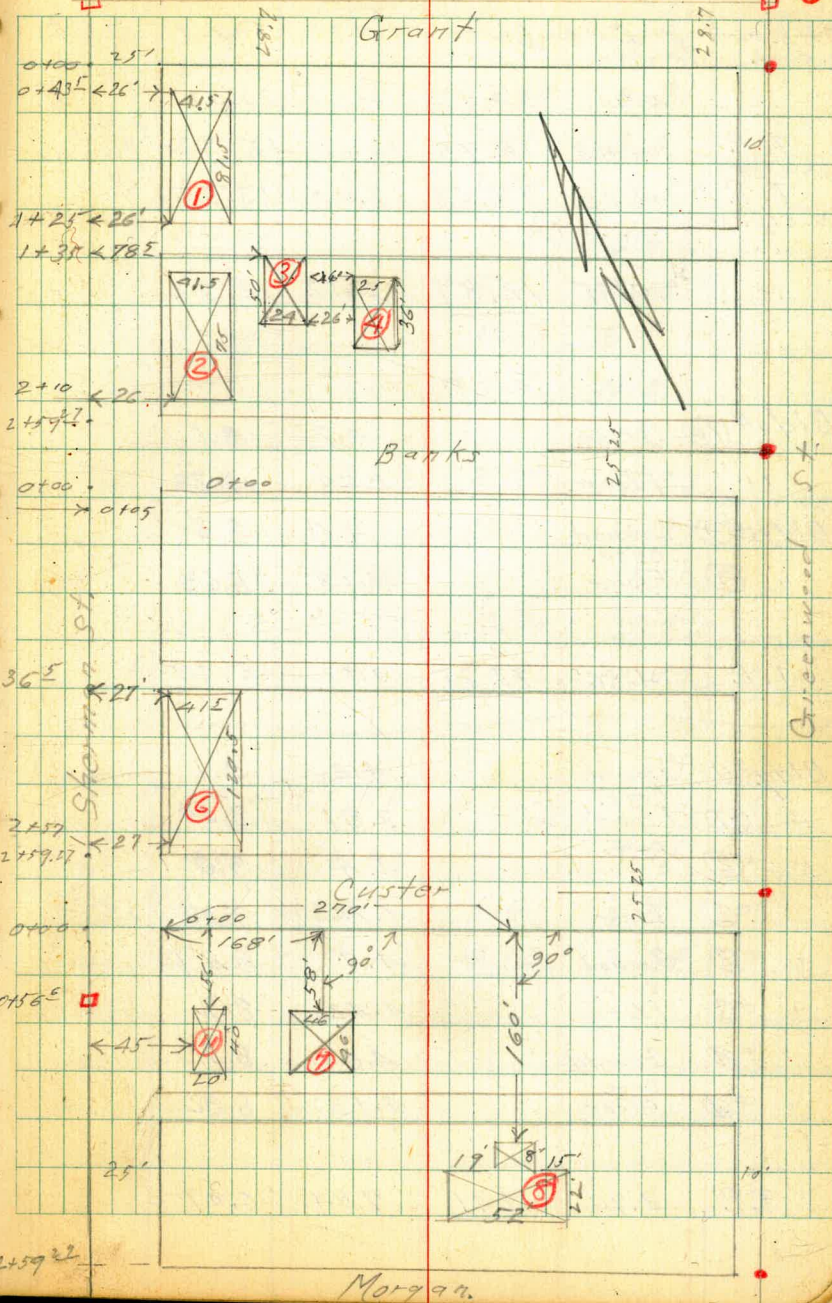


Indexed  
8-13-49

See opposite page

INDEXED

8



R.P.S. end. Sand Diego River bridge Taylor +  
w. curb. Morena.

	4.85	24.92	—	20.07
T.P.	4.43	16.75	12.60	12.32
T.P.	4.93	18.68	3.00	13.75
N. Ely. Mon R.L. 301)				
	0.45	12.81	6.32	12.36

Bldg #10	Ground	4.7	8.1
"	Floor	2.52	10.29
Bldg. #9	Ground conc.	4.5	8.3
"	Floor	4.18	8.63
T.P.	4.86	13.35	4.32 8.49

Bldg. #10	Ground	4.2	9.1
"	conc. Floor	3.81	9.54
"	Ground	4.4	9.0
"	conc. Floor	3.96	9.39
"	Ground	4.7	8.6
"	conc. Floor	4.42	8.9
"	Ground	4.6	8.7
"	conc. Floor	4.53	8.82
T.P.	3.90	9.91	7.34 6.01

π  
9.91

Bldg #5	Grd	7.6	2.3
"	conc. Floor	7.60	2.31
"	Ground	1.5	5.4
"	conc. Floor	1.58	8.33
"	Ground	3.3	6.6
"	conc. Floor	+ 0.53	10.44
"	Ground	0.2	9.7
"	Wood Floor	+ 1.6	11.5
T.P.	6.41	13.74	2.58 7.33
S.S.		1.39	12.35
T.P.	5.24	16.96	2.02 11.72
T.P.	11.24	24.85	3.35 13.61
or 17. B.M.			3.55 13.41
Long shot. →		4.81	20.04

BM = Floor Bldg #6			
	4.83	13.16	— 8.33
Bldg. #10	Ground	6.6	6.6
"	Floor	4.82	8.34

9

CRESTA REAL and  
CUESTA LOMA.

SEWER PROFILES.

11-18-47

Work Order 80072

Sommertmeyer  
W Moore  
E Sherman.

LINES IN RED = Run profiles.

" " Blue = Existing sewers.

■ = Fd. Man.

● = Fd. Lat.

■ = Set 2x2x Disk

● = " Nail

✕ = cut chisel cross

INDEXED

WK  
DEC 17 1948

Bldg T.P. 0.18 193.06 12.85 192.88

Correction to B.P. Evergreen + Talbot B.II =

Chise □

T.P. 0.28 205.73 12.98 205.45

S.E. Cb.  
Lucinda  
Golden  
Park Huc

T.P. 0.13 218.43 12.94 218.30

Bldg T.P. 0.34 231.24 13.21 230.90

T.P. 0.13 244.11 13.12 243.98

T.P. 0.29 257.10 13.16 256.81

N.E. 10' tie

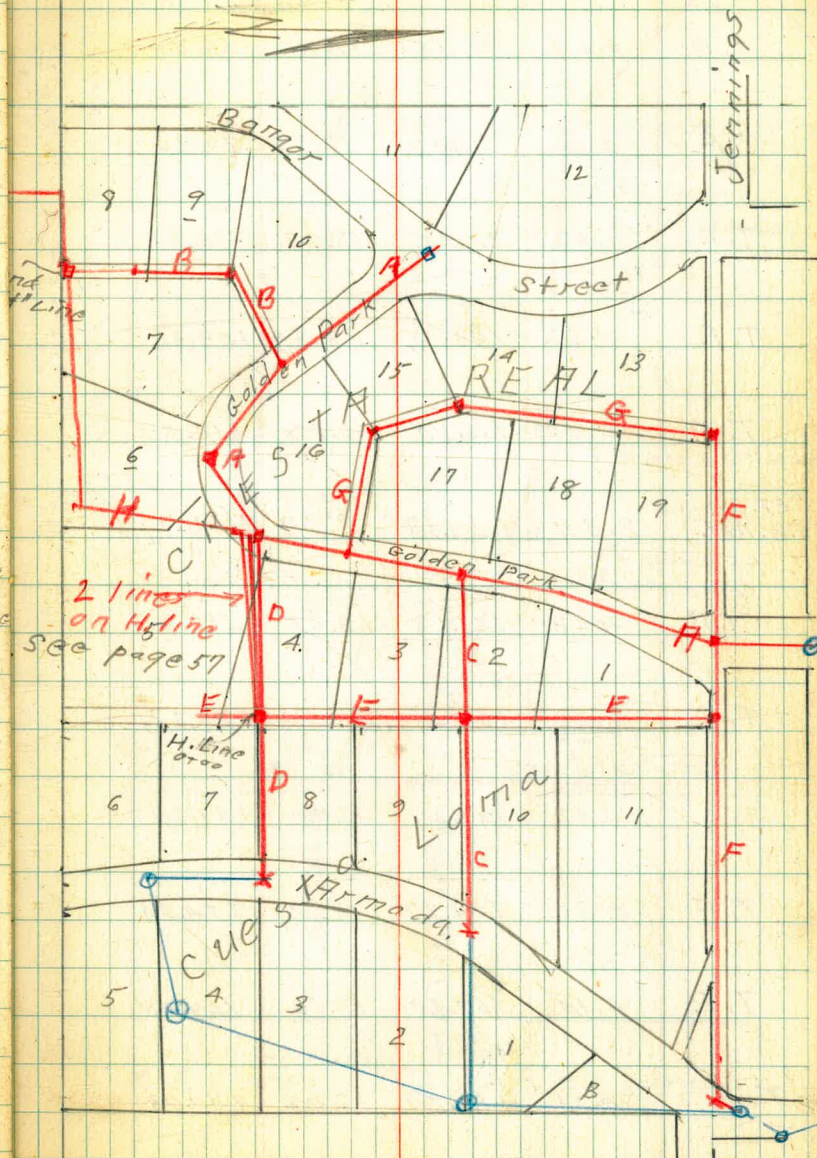
back. Banger  
+ Lucinda

0.49 269.97 — 269.48

shows 269.30 from  
Evergreen + Talbot.

Key sketch.

10



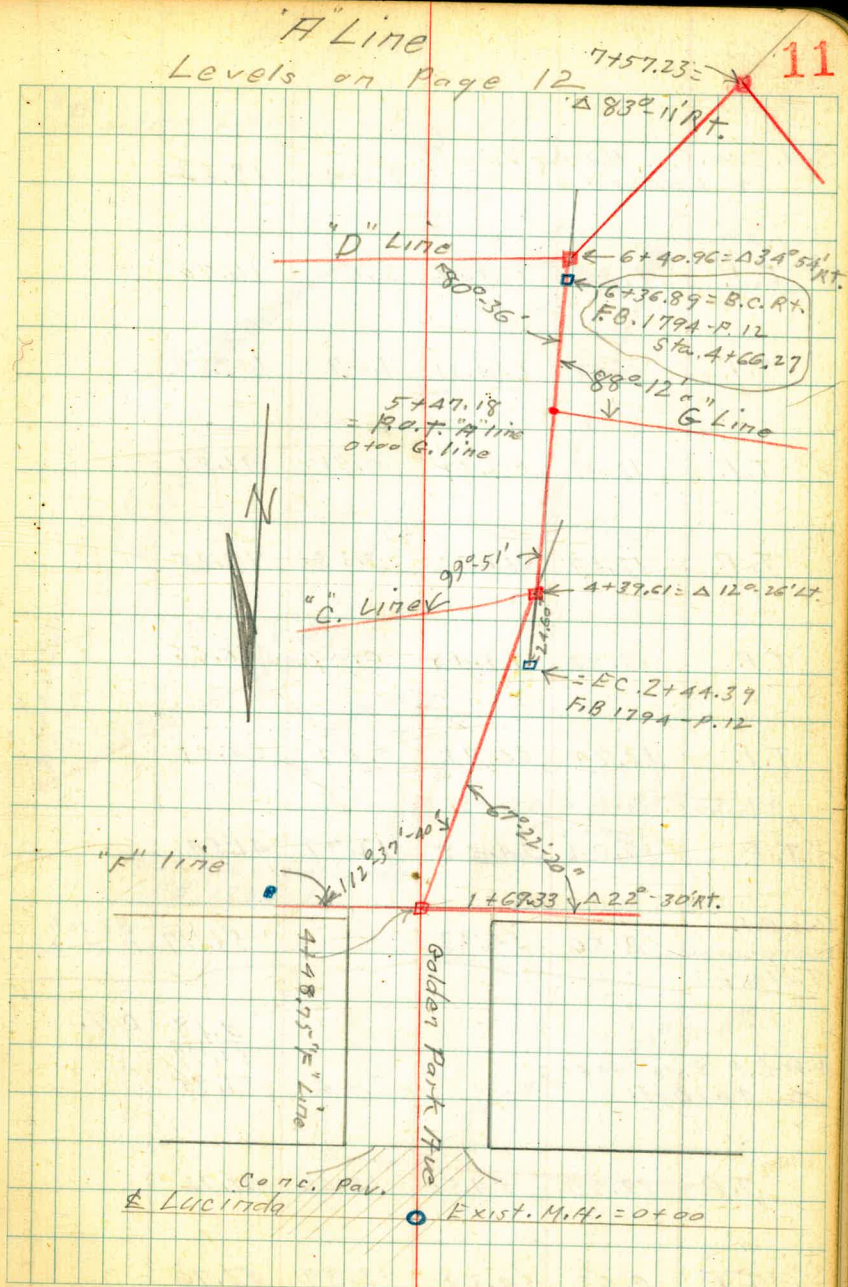
T.P.	0.29	66.65	13.11	66.36
T.P.	0.11	79.47	12.99	79.36
T.P.	0.34	92.35	13.07	92.01
T.P.	0.82	105.08	12.64	104.26
T.P.	0.10	116.90	4.38	116.80
SET. B.P. in S.W. Ret.	2.39	121.18	2.39	118.79
T.P.	4.38	121.18	12.65	116.80
T.P.	0.22	129.45	13.04	129.23
T.P.	0.88	142.27	13.00	141.39
T.P.	0.35	154.39	13.14	154.04
T.P.	0.10	167.18	13.16	167.08
T.P.	0.21	180.24	13.03	180.03

193.06

case Elevation of  
 page 12 = 118.62

Harbor View  
Dr. + Lucinda

"A" Line  
Levels on Page 12



Set, S.W.B.P. Harbor View Pl.  
+ Lucinda 2.44 118.62

T.P. 9.36 121.06 2.61 111.70

T.P. 11.44 114.31 1.07 102.87

T.P. 12.43 103.94 0.31 91.51

T.P. 12.57 91.82 0.23 79.25

T.P. 12.82 79.48 0.09 66.66

T.P. 12.74 66.75 0.57 54.01

T.P. 13.04 54.58 12.79 41.54

N.W.B.P.  
Evergreen & Talbot 2.56 54.33 — 51.77 Bench  
Book Et.

N.W.B.P. Evergreen  
& Talbot. 2.56  $\frac{0.18}{51.77}$  Diff.  
51.95

T.P. 12.79 54.51 12.67 41.72

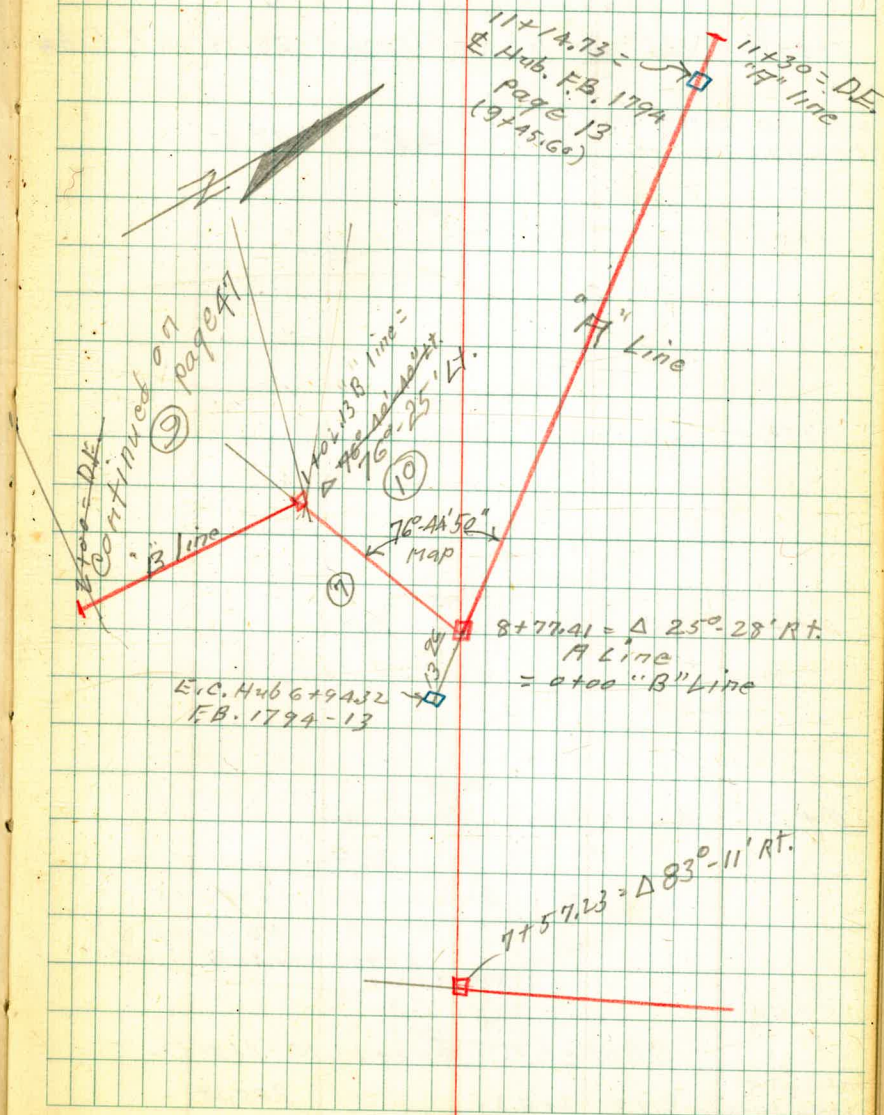
T.P. 0.63 54.39 12.89 53.76

66.65

"A" LINE.

12

"B" Line Levels - Page 19



Taken on split of Δ

1+69<sup>33</sup> = Δ 22°-30' Rt. (Also = 4+78.75 on <sup>or</sup>F Line

2x2 = Δ 22°-30' Rt.  
1+69.33      9.S.      4.65      209.61

1+00

0+50

0+20

0+25<sup>E</sup> = End Conc. Pav.

Note:

Ground to right is higher than E. No long cuts needed.

0+00

Sketches Pages 10-11+12

Chisel D  
3 Esc. Lucinda 8.98      214.26      —      205.28  
+ Golden Park  
Page 101

±

209.9  
 $\frac{12.1}{50}$      $\frac{8.3}{25}$      $\frac{4.7}{14}$     4.4     $\frac{3.9}{10}$

208.6  
 $\frac{9.9}{50}$      $\frac{5.7}{10}$     5.7     $\frac{5.7}{4}$      $\frac{1.9}{10}$

208.0  
6.3     $\frac{2.8}{7}$      $\frac{2.4}{10}$   
 $\frac{5.5}{10}$

207.9  
6.4     $\frac{5.6}{5}$      $\frac{5.4}{10}$   
 $\frac{6.8}{10}$

207.91  
6.35    6.14  
Pav    Pav    Pav

201.95    208.72  
12.31    5.57  
Invert Riff  
±



4+39<sup>el</sup> = 2x2Δ S.S. 3.90 219.58

Taken as split of Δ

4+39<sup>el</sup> = Δ 120-26' Lt. also = 3+67.85 on "C" wire

4+00

3+50

3+00

2+50

T.P. 9.45 223.48 0.23 214.03

2+00

214.26

$\frac{3.3}{10}$  219.9  
3.6  $\frac{4.1}{10}$

$\frac{20.6}{100}$   $\frac{144}{67}$   $\frac{5.7}{48}$   $\frac{1.5}{10}$  219.2  
4.3  $\frac{4.8}{10}$

$\frac{5.6}{10}$  218.0  
5.9  $\frac{5.6}{10}$

$\frac{22.8}{90}$   $\frac{15.8}{47}$   $\frac{8.2}{30}$   $\frac{7.1}{10}$  216.7  
6.8  $\frac{9.6}{10}$

$\frac{9.1}{26}$   $\frac{8.7}{10}$  214.8  
8.7  $\frac{9.1}{10}$   
223.48

$\frac{17.6}{20}$   $\frac{9.2}{32}$   $\frac{1.8}{18}$  212.1  
2.2  $\frac{4.0}{10}$

214.26



"A" Line

shots not needed.

road from here on long side

8+00 Ground on left. higher than

1/2 Δ 7+57.23 S.S. 10.19 224.91

7+57.23 = Δ 83°-11' RT. Taken on split.

T.P. 11.61 246.33 0.38 234.72

7+40

7+25

7+00

6+50

235.10

238.2  
 $\frac{9.7}{10}$  8.1  $\frac{8.5}{6}$   $\frac{5.5}{8}$   $\frac{1.5}{18}$   
 top bank

236.2  
 $\frac{15.7}{142}$   $\frac{17.3}{142}$   $\frac{10.9}{133}$   $\frac{7.3}{42}$   $\frac{7.7}{10}$  10.1 10.5 12.0 5.7  
 House Floor 246.33 10 28 37  
 top. Bank

234.1  
 $\frac{24.1}{140}$   $\frac{8.6}{94}$   $\frac{4.4}{80}$   $\frac{0.2}{28}$   $\frac{0.5}{10}$  1.0  $\frac{0.9}{10}$   $\frac{0.9}{22}$   
 toe of bank

232.0  
 $\frac{2.6}{10}$  3.1  $\frac{3.5}{12}$   $\frac{1.0}{17}$   
 top of bank

229.2  
 $\frac{208.1}{150}$   $\frac{214.1}{95}$   $\frac{228.2}{67}$   $\frac{3.8}{40}$   $\frac{5.2}{10}$  5.9  $\frac{6.2}{7}$   $\frac{0.4}{12}$   
 top bank

226.6  
 $\frac{8.1}{10}$  8.5  $\frac{7.2}{10}$

235.10

10+00

9+50

9+00

Also = 0+00 "B" line

8+77.4 = Δ 25°-28' Rt. Taken on split of Δ

8+60

T.P. 12.52 258.66 0.19 246.14

E.C. 6.12.26+94.32  
FB 179A-13  
P. 12 this wk

8+30

246.33

254.4

$\frac{4.2}{10}$  4.3  $\frac{4.9}{10}$   $\frac{4.8}{10}$   $\frac{3.7}{21}$   $\frac{8.8}{75}$

252.3

$\frac{6.6}{10}$  6.4  $\frac{6.7}{10}$   $\frac{6.9}{19}$   $\frac{5.0}{25}$   $\frac{10.4}{75}$

249.3

$\frac{9.3}{10}$  9.4  $\frac{9.6}{10}$

247.8

$\frac{11.2}{10}$  10.9  $\frac{10.8}{10}$   $\frac{11.4}{19}$   $\frac{7.2}{29}$   $\frac{14.7}{75}$

245.9

$\frac{12.7}{10}$  12.8  $\frac{13.4}{10}$   $\frac{11.7}{12}$   $\frac{8.7}{20}$   
258.66 top bank

240.8

$\frac{4.2}{10}$  5.5  $\frac{5.5}{1}$   $\frac{2.3}{4}$   $\frac{+1.7}{12}$   
246.33 top of bank

"A" Line

N.E.				<u>0.03</u>
10' tie back	Banyon			269.30
	Lucinda	5.34		269.33

T.P.	6.78	274.77	1.60	269.99
------	------	--------	------	--------

11+30 = D.E. "A" Line

11+00

T.P.	11.16	<u>269.59</u>	0.23	258.43
------	-------	---------------	------	--------

10+50

258.66

18

	260.0	
$\frac{8.4}{10}$	9.6	$\frac{9.7}{10}$

	259.0			
$\frac{10.2}{10}$	10.6	$\frac{11.2}{10}$	$\frac{11.8}{50}$	$\frac{18.5}{100}$
	<u>269.59</u>			

	256.6			
$\frac{1.9}{10}$	2.1	$\frac{2.6}{10}$	$\frac{2.7}{15}$	$\frac{2.3}{25}$
				$\frac{7.4}{7.5}$

258.66

"B" Line  
Sketch - Page 12

1+25

1+02.13 =  $\Delta$  76°-40'40" Lt. Taken on split of  $\Delta$

0+50

T.P. #2 11.00 269.86 0.10 258.86

0+32

0+24

0+00 = 8+77.41 on A. Line  $\Delta$  76°-44'-50" Lt

2x2 - T.P.  
Page 17

12.82 258.96 246.14

±

19

268.4  
 $\frac{4.8}{10}$  1.5  $\frac{0.9}{10}$

264.1  
 $\frac{8.7}{50}$   $\frac{7.1}{10}$  5.8  $\frac{5.5}{10}$

259.0  
 $\frac{10.8}{10}$  10.9 269.86  $\frac{11.1}{10}$

256.3  
 $\frac{2.8}{10}$  2.7  $\frac{2.3}{10}$

248.4  
 $\frac{11.3}{10}$  10.6  $\frac{9.9}{10}$

247.8  
11.2

258.96

"B."  
LINE

See Page 49 for  
additional Levels

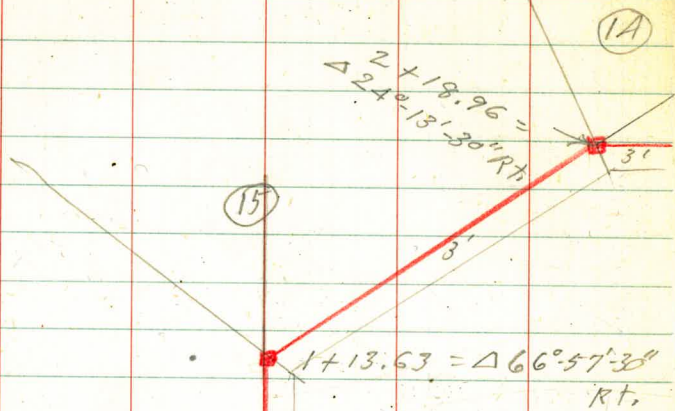
0517	T.P.				
				$\frac{-0.01}{294.14}$	
		12.95		294.13	

T.P.	0.22	259.08	11.00	258.86
------	------	--------	-------	--------

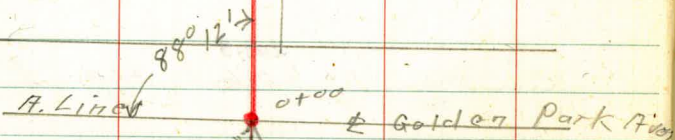
2400	P.E.							
					$\frac{7.6}{50}$	$\frac{1.5}{10}$	$\frac{269.3}{0.6}$	$\frac{+0.8}{10}$

1765	74°	Rt. = N.E. Cor Double Bar.	West. Ent					
				$\frac{7.9}{50}$	$\frac{2.0}{10}$	$\frac{269.3}{0.6}$	$\frac{+1.0}{10}$	$\frac{262.8}{7.1}$
		269.86				<u>269.86</u>		Bar. Flt

"G" LINE.



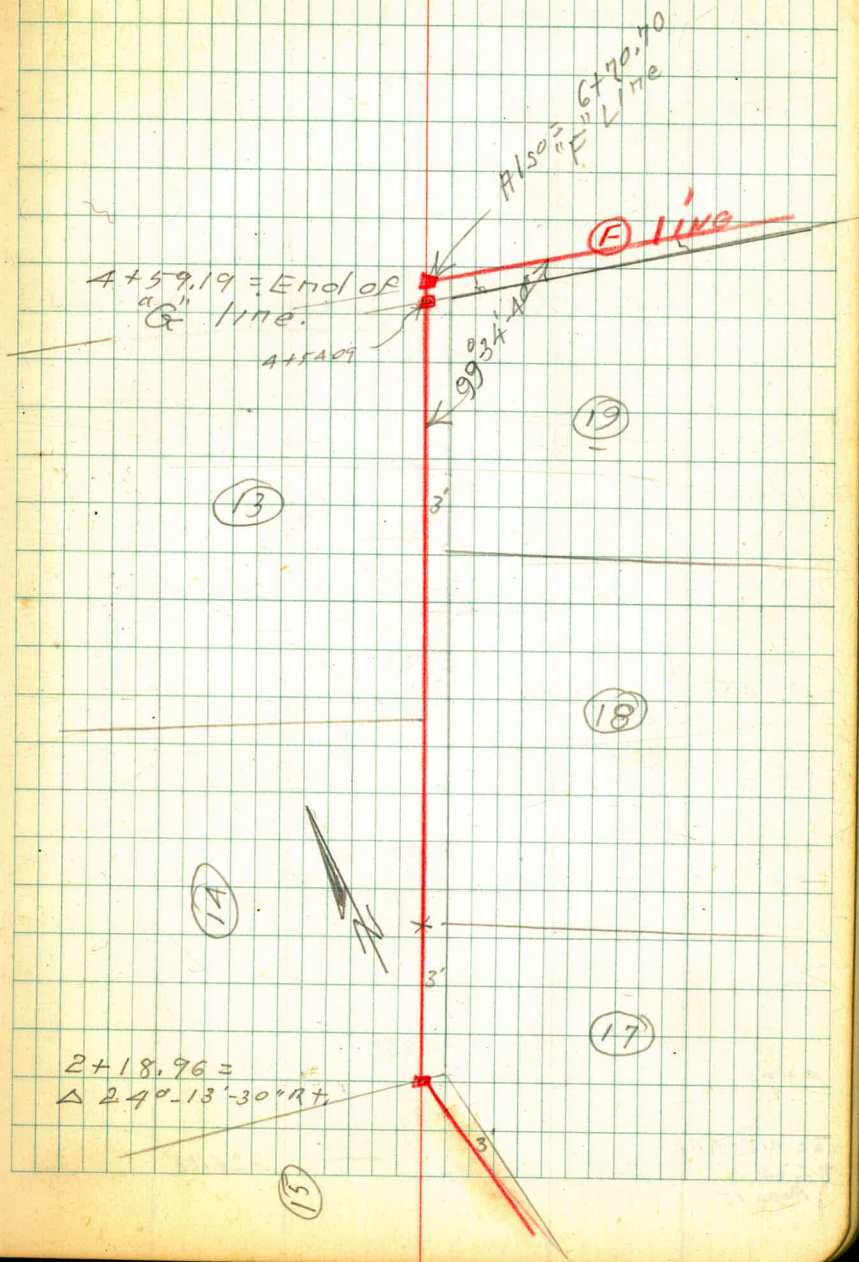
Run according to  
Map # 2170



$5 + 47.18 = 52'$   
 Line Sta.

"G" LINE  
Levels - P. 22

21





"G"  
LINE

T.P. 9.76 254.21 2.58 244.45

1+50

1+13<sup>33</sup> =  $\Delta 66^{\circ}57'30''$  RT Taken on Split of A

1+00

T.P. 12.28 247.03 0.09 234.75

0+45

0+27

0+00

2x2  $\Delta 67^{\circ}40'96''$   
7 line  
Page 15

8.69 234.84 — 226.15

243.7

$\frac{2.6}{10}$

3.3

$\frac{4.0}{10}$

$\frac{9.6}{30}$

243.1

$\frac{1.9}{15}$

3.9

$\frac{5.3}{15}$

241.6

$\frac{5.4}{10}$

5.4

$\frac{5.7}{10}$

247.03

233.6

$\frac{1.1}{10}$

1.2

$\frac{1.5}{10}$

222.8

$\frac{12.0}{10}$

12.0

$\frac{12.3}{10}$

222.4

12.4

"G"  
Line

A+59.19 = 1/2 Hub = G+70.70 on "F" Line.

A+00

3+50

3+00

2+60

2+18<sup>96</sup> = Δ 24°-13'-30" Rt.

taken  
on split of A

2+00

254.21

£

23

247.41

$\frac{6.80}{10}$   
HVB

246.7

$\frac{6.2}{10}$

7.5

$\frac{8.4}{10}$

$\frac{15.5}{60}$

245.4

$\frac{7.4}{10}$

8.8

$\frac{10.0}{10}$

245.5

$\frac{6.9}{10}$

8.7

$\frac{10.4}{10}$

238.2

$\frac{16.0}{50}$

244.8

$\frac{8.5}{10}$

9.8

$\frac{10.4}{10}$

244.4

$\frac{8.6}{10}$

9.8

$\frac{11.0}{10}$

244.8

$\frac{8.4}{10}$

7.4

$\frac{11.3}{10}$

$\frac{15.5}{50}$

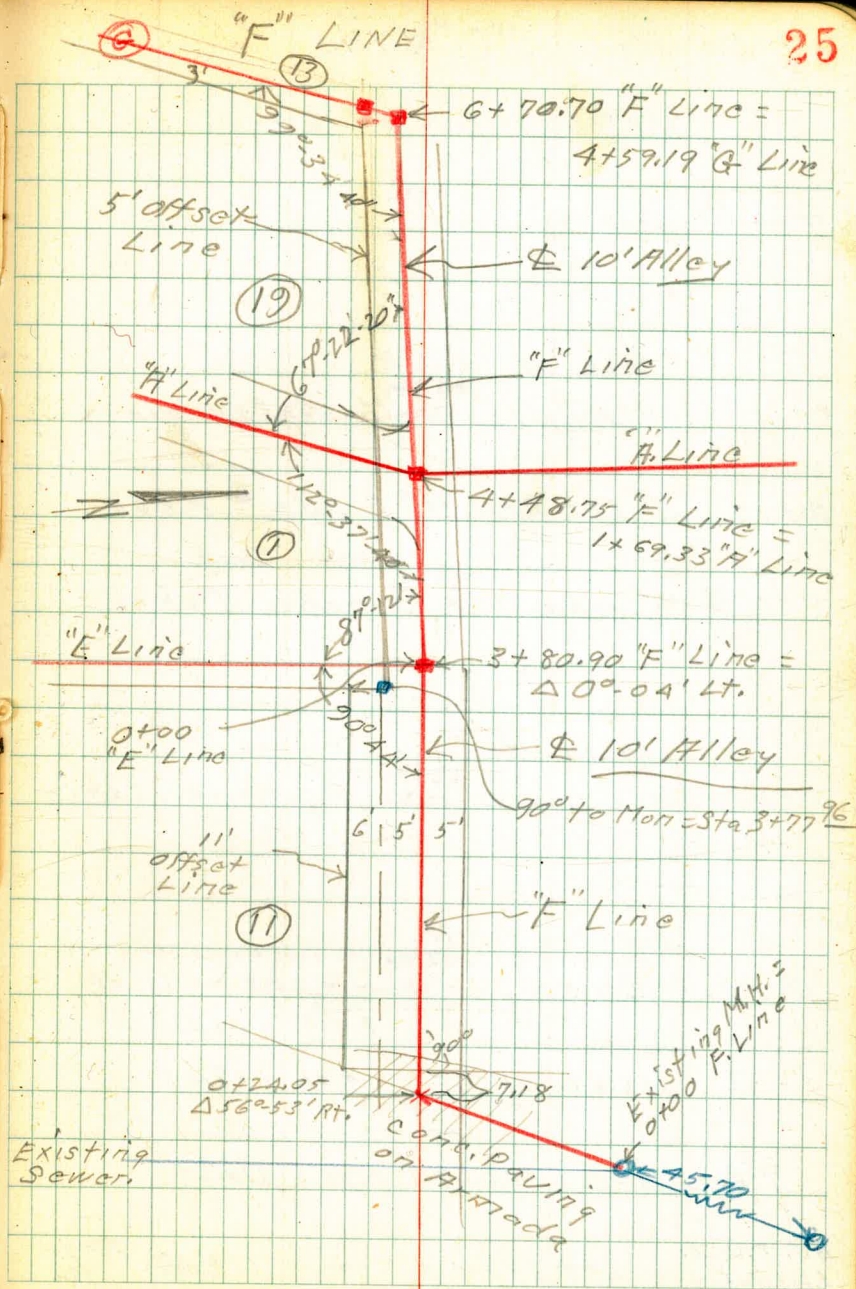
254.21



# "F" Line

Levels on P-38

Run according to  
Maps 1910 & 2170  
and T.P. 25



Levels "C" Line

sketches P. 19 + P. 24

0+21<sup>t</sup> Grdn

edge of walk.

0+21<sup>e</sup> Wly. Edge walk. taken along

0+19 3<sup>5</sup> Lt. = Ctr. 14" P. pole # P. 860  
along curb.

0+15<sup>25</sup> Wly Ch. line Armada. Taken

in gutter

0+15<sup>t</sup> Wly Gutter line Armada. taken

South line lot 10.

0+00 = Dead end cap. line run 3' North of  
chisel + in par. 1' west + 0.8 North of

7.05 148.30

T.P. 12.69 155.35 0.62 142.66

T.P. 13.01 143.28 0.33 130.27

B.P. S.W. Ch.  
Lucinda  
Harbor View Pl.

11.98 130.60 — 118.62

Page  
12

1502

5.2

2.0

9

2.0

10

top of  
bank

149.56

5.44

5.79

6.10

3

149.17

5.86

6.18

6.50

3

148.85

6.36

6.70

6.97

3

148.30

6.79

7.05

7.30

3

155.35

"C"  
line

1+40

T.P. 11.97 192.45 0.07 180.48

0+90

0+75

T.P. 12.84 180.55 0.15 167.71

0+50

0+32

T.P. 12.58 167.86 0.07 155.28

0+27

155.35

27

181.5  
 $\frac{10.9}{10}$  10.8  $\frac{10.6}{10}$   
192.45

173.1  
 $\frac{9.8}{10}$  9.5  $\frac{7.2}{10}$

188.2  
 $\frac{12.6}{10}$  12.4  $\frac{11.7}{10}$   
180.55

161.1  
 $\frac{7.4}{10}$  6.8  $\frac{6.9}{10}$

156.3  
 $\frac{11.6}{10}$  11.6  $\frac{11.2}{10}$   $\frac{8.8}{50}$   
167.86

155.0  
 $\frac{4.5}{10}$  0.4  
top of  
bank  
155.35  $\frac{0.4}{10}$

T.P.	9.24	<u>224.62</u>	0.34	215.38
3+03				
3+00				
2+95				
T.P.	11.13	215.72	0.10	204.59
2+50				
P.O.T. 1499 <sup>45</sup>				
T.P.	13.04	<u>204.69</u>	0.80	191.65
1+99A = P.O.T. =		2+50.52	on "E" line	
1+75				
		<u>192.45</u>		

		213.3	
	$\frac{5.2}{10}$	2.4	$\frac{0.3}{10}$
	Toe of bank		
		210.3	
	$\frac{5.5}{10}$	5.4	$\frac{2.6}{10}$
	Toe of bank		
		209.5	
	$\frac{6.6}{10}$	6.2	$\frac{5.8}{10}$
			Toe of Bank
		200.9	
	$\frac{4.3}{10}$	3.8	$\frac{4.1}{10}$
		<u>204.69</u>	
		191.6	
	$\frac{1.2}{10}$	0.80	$\frac{0.5}{10}$
		on line	
		187.6	
	$\frac{4.8}{10}$	4.9	$\frac{5.1}{10}$
		<u>192.45</u>	

+0.03

219.59

219.61

Check 1/2 Hk.

3+67.85 "C" line

4+39.61 "A" line Page 14

5.01

3+67.85 = Int. "A" line at sta 4+39.61

3+62

3+50

3+32 = Elev. Edge Traveled Road

3+25

3+11

224.62

221.8

7.8

Grd.

220.2

4.4

220.0

4.6

219.1

5.5

219.7

 $\frac{5.2}{10}$ 

4.9

 $\frac{5.4}{10}$ 

217.3

 $\frac{7.3}{10}$ 

7.3

 $\frac{6.7}{10}$ 224.62



"D" Line - Levels

Sketches Page 10 + Page 24

T.P. 12.87 184.22 0.41 171.35

0+71E 20 RT - 18" Diam tree.

0+70

169.3  
2.5  
3  
171.76  
3.3  
10

T.P. 11.73 171.76 0.60 160.03

0+25

158.0  
2.4  
3  
158.0  
2.6  
5  
155.4  
2.4  
10

along lot line.

0+18 = 3' Lt. = start 1' wide conc. block wall 158.2  
Wly. Edge walk.

2.4  
3  
Top wall

155.0  
5.6  
3  
Base of wall  
4.6  
3  
Ord  
4.96  
3  
walk.  
155.66  
4.97  
3  
walk  
4.93  
3  
Ord

0+14 4' Lt. = Ctr. P. pole # P. 832 (15" pole)

0+13 1/2 Wly. Curb Armada

155.59  
5.06  
3  
5.04  
5.05  
3

0+13 = Wly. Gutter Armada.

155.25  
5.40  
3  
5.38  
5.39  
3

0+00 lot # 18 Also = D.F. Exist sewer  
= Armada + 3 North of South line

155.51  
5.14  
3  
5.12  
5.09  
3

Chise x in Pav.

0+00 "C" line 12.33 160.63 — 148.30

Page 26

160.63

1+52 8" wide N+S wall  
 3<sup>5</sup>Lt = End 1' wide CONC. wall also = E

T.P. 12.74 196.84 0.12 184.10

1+31

1+24 3<sup>5</sup>Lt = Face of wall at step up in  
 top of wall. (12 step)

1+17<sup>E</sup> 3.8 Lt = End Bar.  
 3.5 Lt = start 1' wide CONC. block wall

Bar. CONC floor East door.

0+95<sup>E</sup> 2<sup>8</sup>Lt = End wall, 4<sup>0</sup> Lt = start stucco

0+84 2<sup>8</sup>Rt = Break in wall grade

0+82 10<sup>0</sup>Rt = ctr. 10' diam tree  
 184.22

185.3	180.3		184.9	
11.5	16.5	11.9	11.9	11.9
3.5	3.5	3.5		10
Top wall	Base wall	Grd	<u>196.84</u>	

	181.8		
2.2	2.4	2.9	2.6
3.4		10	20
HT wall			

178.5	179.9
5.7	4.3
3.5	3.5
Base wall	Grd

6.2	182.1	7.0	6.0	178.3
4.0	2.1	3.5	3.5	5.9
Grd	Top wall	Base wall	Grd	

170.8	169.6	173.8	178.7	
13.4	14.6	10.4	10.8	10.3
N. E. Bar Floor	Base of wall	Top wall	Grd	10

13.4	173.8	169.6	12.3	171.8
4.0	10.4	14.6	12.4	12.7
Grd	Top wall	Base wall	Grd	10

"D" Line

T.P. 8.75 229.88 0.07 221.13

3+05

2+80

T.P. 12.06 221.20 0.21 209.14

2+50

T.P. 12.60 209.38 0.06 196.78

2+00

1+60 E 1<sup>st</sup> Rt. = ctr. 5" Holly Tree.

1+56.02 = Int. "E" Line

2nd Hub  
1+56.02 S.S. 11.54 185.30

1+53

196.84

☉

32

215.3

$\frac{5.3}{10}$

5.7

$\frac{6.0}{10}$

212.1

$\frac{9.1}{10}$

9.1

$\frac{9.3}{10}$

221.20

204.8

$\frac{4.8}{10}$

4.6

$\frac{4.5}{10}$

194.5

$\frac{2.3}{10}$

2.3

$\frac{2.5}{10}$

185.9

$\frac{10.7}{10}$

10.9

$\frac{10.5}{10}$

185.0

$\frac{11.7}{10}$

11.8

$\frac{11.5}{10}$

196.84

"D" Line

$\frac{0.04}{226.15}$   
 226.19  
 222 6+40.96 "A" Line  
 page 15.      3.69      226.19

222  
 3+57.31 = End "D" line + Int. "A" line at 6+40.96

3+49 = Ely. Edge traveled road

3+36

3+25

229.88

4

33

226.4  
 $\frac{3.5}{10}$

226.7  
3.2  
 $\frac{3.8}{10}$

225.9  
2.0  
 $\frac{2.5}{10}$

223.8  
6.1  
 $\frac{6.5}{10}$

229.88

"E" Line  
Sketches P. 10 + 24

1+00

0+85

0+50

0+07

0+00 = 212 3+80<sup>20</sup> on "F" Line

Rat. Hub.  
"C" Line 199<sup>22</sup>  
page 28 9.40 201.11 — 191.65

±

34

$\frac{18.5}{75}$

$\frac{7.6}{10}$

195.6  
5.5

$\frac{3.5}{10}$

$\frac{8.3}{10}$

195.0  
6.1

$\frac{3.8}{10}$

$\frac{9.0}{10}$

194.3  
6.8

$\frac{4.3}{10}$

$\frac{8.1}{10}$

195.7  
5.4

$\frac{3.1}{10}$

$\frac{5.9}{10}$

198.25  
2.86  
Hub

$\frac{4.4}{10}$

201.11

"E" Line

3750

T.P. 2.90 191.06 12.75 188.16

3715

3700

2+50<sup>5</sup> P.O.T. = 1994 "C" Line

2700

1750

201.11

4

35

4.6  
10  
188.0  
3.1  
191.06  
9.0  
10

11.9  
10  
191.4  
9.7  
7.8  
10

22.0  
75  
11.2  
10  
191.5  
9.6  
7.9  
10

11.2  
10  
191.6  
9.5  
7.6  
10

20.8  
75  
11.2  
10  
192.2  
8.9  
6.9  
10

8.7  
10  
194.6  
6.5  
4.9  
10

201.11

4+54 4' Lt. = start 8" Concr. Wall

10.1	5.7	10.7	6.1	185.7
50	4.0	4.0	4.0	5.4
Grd	Top	Base	Grd	
inside	wall	wall		
wall				

4+50.52 = P.O.T. = 1+56.02 "D" Line.

186.0  
5.1

4+49 4' Rt. = Ctr. 5" Diam Holly Tree.

4+25

6.3	187.1	2.1
10	4.0	10

3+93 = S. bank Wash

17.0	186.0	2.8
55	5.1	10
7.2		
10		

3+91 Bottom of Wash

10.3	183.8	5.4
10	7.3	10

3+89 = North bank of wash (Turns E+W)

7.5	185.9	3.1
10	5.2	10

191.06

191.06

"E" Line

♀

37

check to  
1x2 p.a.t.  
1+56.02  
"D" Line page 32

$\frac{0.01}{185.30}$   
5.75 185.31

5+05 = D.E. + 3<sup>rd</sup> Lt = 8" N. + S. Conc. Wall <sup>Face.</sup>

$\frac{11.0}{3}$   $\frac{5.9}{3}$   $\frac{6.0}{3}$  5.6  $\frac{5.2}{10}$   
Base top wall

4+94 3<sup>rd</sup> Lt. = Small Eucalyptus

191.06

191.06



"F" Line  
Levels

Sketches P-10 & P-25

T.P.  
Nail in Pole  
#935924

11.6    136.07    0.09    124.91

0+35

0+29 on dirt

0+28<sup>9</sup> = Curb 1170 Armada No side walk

0+28<sup>9</sup> = Gutter line Armada

1" Gas line runs 15' south of E Alley.

5' Lt. on Δ split = Ctr. 2" x 2" Gas Co. box

0+24<sup>05</sup> = Δ 56°-53' Rt. Taken on split of Δ

0+00 = Existing M.H. (Page 25)

S.W.B.P. Lucinda

+ Harbor

Vien Place

P-12

6.38    125.00

118.62

±

38

$\frac{5.7}{10}$

122.4  
2.6

$\frac{+4.4}{10}$

118.9  
6.1

$\frac{6.8}{10}$

118.59  
6.41  
top of

117.97  
7.03  
gutter

$\frac{6.70}{50}$

118.13  
6.87

$\frac{7.10}{3}$

109.5    117.10  
15.5    7.90  
INVERT    RITI

±

F LINE

45 RT.

1+43 = End wire fence start picket fence

1+35

$\frac{9.0}{50}$	$\frac{13.8}{33}$	7.5	143.4	$\frac{+0.2}{10}$
			1.8	

1+27

1+24 2<sup>8</sup> Rt. = start wire + wood fence

1+22 4<sup>9</sup> Lt. = Ctr. 16" P. pole P3124

		8.0	141.8	$\frac{4.5}{10}$
			6.4	

1+00

0+95 4' Lt. = P. pole Dead man.

	$\frac{13.3}{10}$		137.7	$\frac{6.4}{10}$
			10.5	
			<u>148.19</u>	

T.P. 12.22 148.19 0.10 135.97

0+75

$\frac{7.0}{35}$	$\frac{2.8}{10}$		135.0	$\frac{+1.3}{10}$
			1.1	

0+45

	$\frac{7.0}{10}$		130.2	$\frac{3.7}{10}$
			5.9	

0+38

	$\frac{14.8}{10}$		129.1	$\frac{4.9}{10}$
			7.0	

136.07

136.07

1+85

155.2  
 $\frac{6.2}{5}$  5.5  $\frac{3.0}{5}$

1+80

152.7  
 $\frac{7.6}{75}$   $\frac{8.2}{48}$   $\frac{7.0}{5}$  8.0  $\frac{6.0}{5}$

1+79

152.1  
 $\frac{1.0}{5}$  8.6  $\frac{8.1}{5}$   
160.69

← 5 →

T.P. 1256 160.69 0.06 148.13

1+69

← 7.3 →

Conc. & brick steps.

1+69 7<sup>2</sup> Rt. = 3' wide brick + Conc. steps.

1462  
 1+62 ← 5' →  
 24.7

1+62<sup>5</sup> = Int. fence + alloy line

1+62 4<sup>3</sup> Rt. = Δ in fence →

1+60

149.6

$\frac{1.0}{50}$   $\frac{5.0}{20}$   $\frac{0.0}{10}$  11.4  $\frac{14.0}{10}$

1+49 6<sup>2</sup> Rt. = 18" Diam. Pepper tree.

148.19

148.19

2+58

2+57<sup>E</sup> = Cross 1" Water line (Private)2+57 4<sup>o</sup> Rt. = ctr. 4" poplar2+54 4<sup>4</sup> Lt. = ctr. 4x8 clothes line post.2+50 4<sup>3</sup> Rt. = ctr. 2-5" poplars

2+45

2+45

2+44 2<sup>1</sup> Lt. = 1' Diam pine2+41 4<sup>o</sup> Rt. = 2-4" <sup>1/2</sup> diam. poplars2+35 2<sup>2</sup> Rt. = 14" Diam pine tree2+33 1<sup>5</sup> Lt. = 5' High Cateniaster

2+25

2+24 3<sup>E</sup> Rt. = 2" Diam Lemon tree

2+14 3' Rt. = ctr. 10" Eucalyptus

T.P. 12.49 172.99 0.19 160.50

2+00

160.69 $\frac{2.1}{5}$ 

171.0

2.0 $\frac{1.6}{5}$ 

170.7

 $\frac{2.4}{5}$ 2.3 $\frac{2.3}{5}$  $\frac{4.2}{5}$ 

169.0

4.0 $\frac{3.6}{5}$  $\frac{2.8}{5}$ 

165.2

2.8 $\frac{2.7}{5}$ 172.99 $\frac{0.8}{50}$  $\frac{3.1}{5}$ 

158.0

2.7 $\frac{0.4}{5}$ 160.69

"F" LINE.

3+00

2+76 1  $\frac{1}{2}$  Lt. =  $\Phi$  start E+W. Hedge <sup>3' wide</sup>

2+75 = Cross  $\frac{3}{4}$  wide Hedge

$\Phi$  = Cross wire fence

2+72 3  $\frac{3}{4}$  Lt. = start E+W wire fence.

2+69 3  $\frac{1}{2}$  Lt. = Ctr. P. pole #3162 - P3162

2+68 5.5 Rt. = End brick work

2+67 3  $\frac{1}{2}$  Rt. = Ctr. 14" poplar tree

T.P. 13.26 185.46 0.79 172.20

2+61 on Ground

2+59.1

2+58.1 = start brick work on  $\Phi$

172.99

$\Phi$

180.1

$\frac{5.6}{5}$  5.4  $\frac{5.3}{5}$

175.0

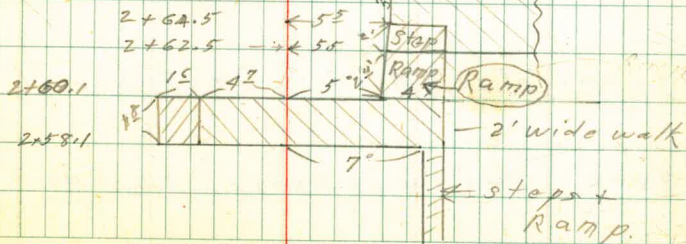
$\frac{10.4}{50}$   $\frac{10.3}{5}$   $\frac{10.2}{185.46}$   $\frac{10.0}{5}$   $\frac{10.7}{5.5}$   $\frac{10.5}{70}$   
on Bricks

171.9

$\frac{1.3}{5}$  1.1  $\frac{0.9}{5}$

172.1

$\frac{1.9}{6.4}$   $\frac{1.3}{6.3}$   $\frac{0.9}{4.7}$  0.9 0.8 0.7  
Grd End stop End walk E walk E walk End walk



172.99

"F" line

T.P. 12.95 210.50 0.43 197.55

3+74 Cross Wash

3+66

3+43

T.P. 12.68 197.98 0.16 185.30

3+22 Start of fill on lot on Rt.

3+15 5° Rt. = line of wire fence

3+10 0° Lt = Δ in wire fence

3+08 End 3' wide hedge on line

185.46

±

43

				195.1		
43	40	45	55	2.9	+3.6	+3.5
25	15	8	5	wash	11	20
			Δ in wash			

				198.0		
5.0	5.0	7.2	6.3	0.3	+3.0	+3.0
25	12	11	7		6	20
		wash				

				193.7		
11.3	10.6	6.7	4.3		2.2	+2.0
50	11	5		197.98	5	20
						+2.3
						50

				188.5		
	1.8	2.0	1.9			1.9
	5		5			20

185.46

4+23

4+18 3<sup>rd</sup> Lt. = P. pole # P 3198

4+15

4+02

4+00

3+82

3+80<sup>20</sup> = Δ 0°-04' Lt. Also = 0+00 on E. line210.50

205.7

$\frac{5.5}{15}$	$\frac{5.1}{5}$	4.8	$\frac{4.6}{3}$	$\frac{5.6}{5}$	$\frac{4.6}{10}$	$\frac{2.5}{4.9}$
------------------	-----------------	-----	-----------------	-----------------	------------------	-------------------

207.4

$\frac{7.6}{15}$	$\frac{6.7}{5}$	6.1	$\frac{7.2}{3}$ wash	$\frac{5.7}{5}$	$\frac{6.5}{9}$	$\frac{5.9}{15}$
------------------	-----------------	-----	-------------------------	-----------------	-----------------	------------------

200.3

$\frac{9.8}{5}$	10.2 wash	7.5	7.5	$\frac{7.2}{8}$	$\frac{6.9}{12}$
-----------------	--------------	-----	-----	-----------------	------------------

202.5

$\frac{11.2}{30}$	$\frac{10.2}{7}$	$\frac{11.1}{5}$ wash	8.0	$\frac{7.6}{3}$	$\frac{2.6}{7}$	$\frac{7.2}{12}$	$\frac{6.8}{30}$
-------------------	------------------	--------------------------	-----	-----------------	-----------------	------------------	------------------

197.8

$\frac{14.8}{8}$	10.7	$\frac{10.1}{3}$	$\frac{14.0}{8}$	$\frac{8.7}{15}$	$\frac{8.4}{30}$
------------------	------	------------------	------------------	------------------	------------------

198.26

12.24  
HVB210.50

"F" LINE

5+27 3<sup>rd</sup> RT. = End same

5+15 - 3<sup>rd</sup> RT. = start Frame Gar. 1st floor

4+95

4+72

4+67

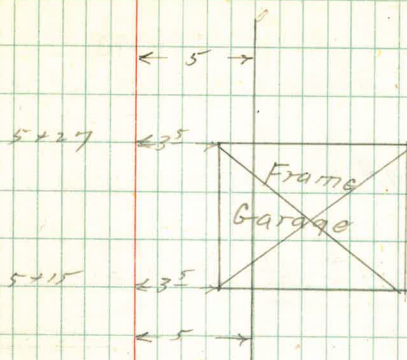
4+64

T.P. 12.95 222.61 0.84 209.66

4+37 = Edge traveled road  
210.50

4.

45



218.1  
 $\frac{5.0}{5}$  4.5  $\frac{4.1}{5}$

214.8  
 $\frac{7.7}{5}$  7.8  $\frac{7.7}{5}$

212.6  
 $\frac{10.2}{5}$  10.0  $\frac{9.3}{5}$

210.4  
 $\frac{12.1}{5}$  12.2  $\frac{12.4}{5}$   
222.61

209.9  
 $\frac{0.3}{5}$  0.6  $\frac{0.6}{5}$   
210.50



"F" Line

Also = 4 + 59.19 on "G" line

6 + 70.70 4<sup>E</sup> Rt = Line of wire fence

6 + 30<sup>E</sup> 4<sup>●</sup> Rt. = Start wire fence

6 + 30 = 4<sup>A</sup> Rt = End brick patio + wall

6 + 20 4<sup>A</sup> Rt. = start brick patio + wall

6 + 19 4<sup>A</sup> Rt. = End 6' wide hedge

T.P. 12.98 248.01 0.20 235.03

5 + 75

5 + 44 - 5' Rt. = Start 6' wide hedge

Level or higher to Lt. & Rt.

No long outs needed. Ground

5 + 40 4<sup>L</sup> Lt. = Ctr. P. pole # P3230

T.P. 12.68 235.23 0.06 222.55

222.61

⊕

247.9

$\frac{0.56}{5}$   
0.112

0.1

$\frac{+0.4}{5}$

243.2

$\frac{5.0}{5}$

4.8

$\frac{4.9}{5}$   
0.98

5.6

1.12

Bottom of wall.

242.4

$\frac{5.7}{5}$

5.6

$\frac{5.3}{5}$   
1.06  
on Bricks

5.6

1.12

Base of patio + wall

248.01

233.5

$\frac{4.7}{10}$

$\frac{2.1}{5}$

1.7

$\frac{1.2}{5}$

227.3

$\frac{8.3}{5}$

1.9

$\frac{7.7}{5}$

235.23

222.61

"B" Line - Cont.  
 N. 1/2 P.L. 173 + Por. P.L. 174.

6+18.04  
 P.O.T.

$\Delta 89^{\circ}56'20''$  Lt.  
 4+58.43 =

~~Not used.~~

4+55.43 = P.O.T.

Map 2170 + F.B. 1794

Sec. R. of S. 767

15 15

Fd. 1/2  
 Hub

2+84.05  
 $\Delta 90^{\circ}10'$  Rt.

P.L. 173

P.L. 179

3+57.28  
 $\Delta 89^{\circ}56'20''$  Lt.

(8)

(7)

(9)

1+02.13  
 $\Delta 76^{\circ}25'$  Lt  
 From Page 12

(10)

"B" Line. Cont.

47

9+32.17 =  $\Delta 37^{\circ}50'$  Rt.

1539

40.69

32.89

9+08.28

P.L. 174  
 P.L. 173

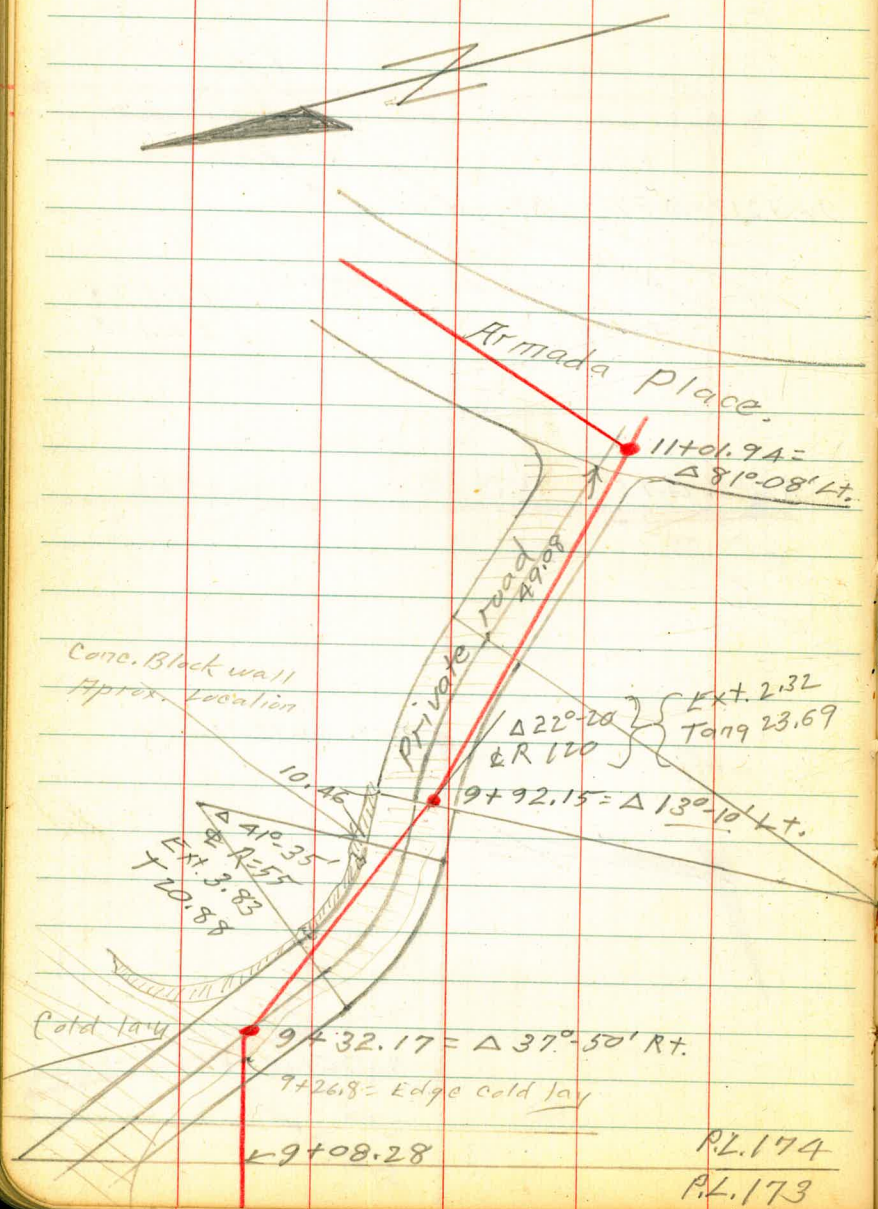
$\Delta 92^{\circ}02'10''$

R.O.P.S. 645

P.O.T. 7+72.01

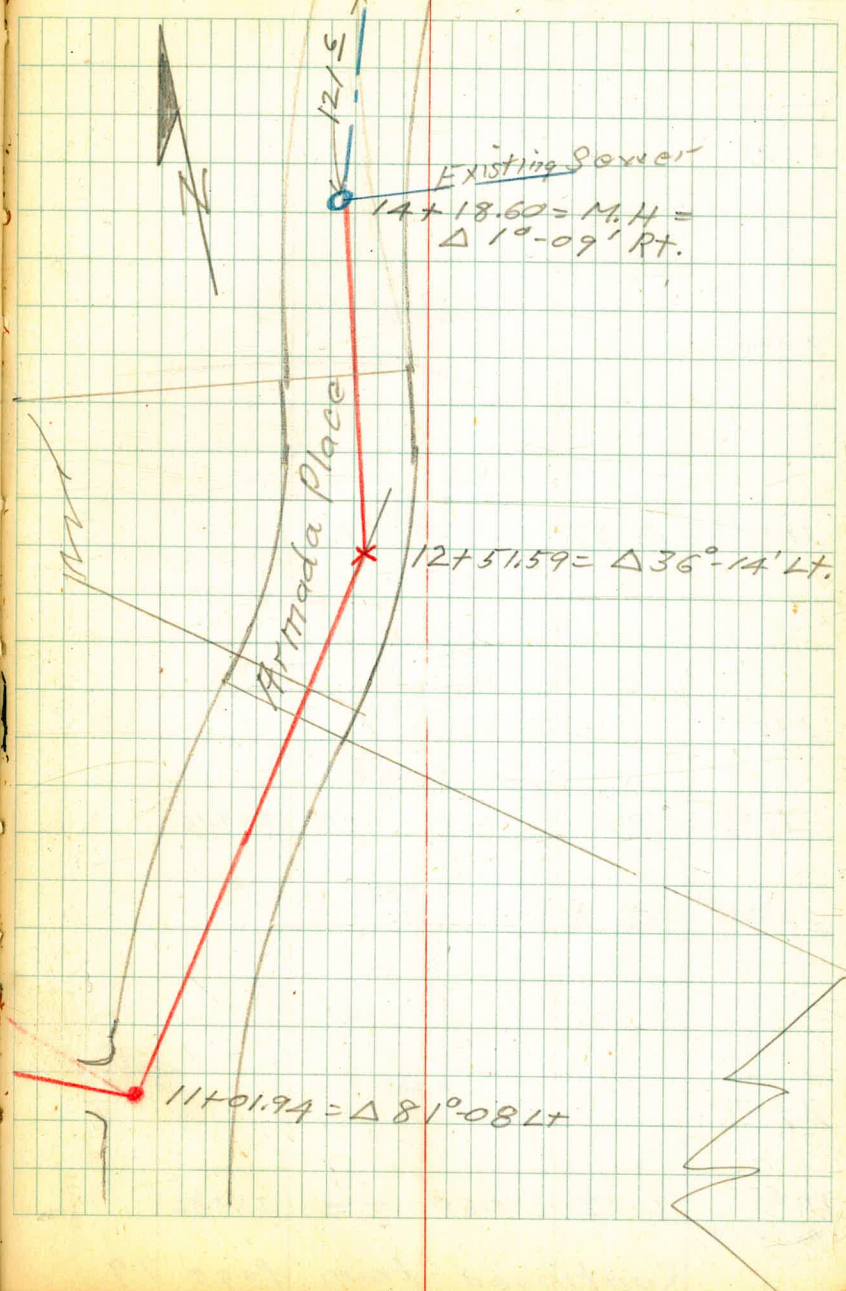
P.O.T. 6+18.04

"B" Line Cont.



"B" Line Cont.  
↑ Exst. D.E.

48



"B"  
Line

3+73

3+45

 $3+39^{28} = \Delta 89^{\circ} 56' - 20'' \text{ Lt.}$ 

3+00

T.P. 5.21 274.37 1.49 269.16

 $2+84^{05} = \Delta 90^{\circ} - 10' \text{ Rt.}$ 

2+50

T.P.#2- 11.79 270.65 ~~11.79~~ 258.86  
Page 19

Continued from page 19

271.5  
2.9

271.4  
3.0

272.3  
2.1

269.7  
1.7  
274.37

268.0  
2.7

268.4  
2.3

"B"  
Line Cont.

♀

50

5+00

268.6  
5.8

4+66

271.3  
3.1

4+63

272.4  
2.2

4+58<sup>43</sup> =  $\Delta 89^{\circ} 56' - 20''$  Rt.

272.5  
1.9

4+55<sup>43</sup> = <sup>Disk in</sup> 2x2. = P.O.T. 1.86 272.51

4+00

272.4  
2.0

3+78

272.5  
1.9

27437

274.37

"B"  
Line

6+75 3<sup>1</sup>/<sub>4</sub> H. = End fence

6+55

6+33

6+21 3<sup>3</sup>/<sub>4</sub> Lt. start wire fence. wood posts  
*set in bone.*

T.P. 0.73 249.26 12.91 248.53

6+18.04 = P.O.F. 2x2

5+85

T.P. 0.00 261.44 12.93 261.44

5+50

274.37

241.0  
7.9  
10  
8.3

243.4  
5.9

248.7  
0.6  
249.30

251.05  
10.39  
07 Hub

256.5  
4.9  
261.44

262.2  
12.2

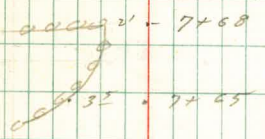
274.37

"B" line

T.P.	1.17	<u>225.76</u>	13.01	224.59
7+75	End of bench			
7+72 <sup>d</sup>	= P.O.T.		11.32	B.M.
7+70	4 <sup>s</sup> Rt. = 9" Diam. Eucalyptus			
7+68	2' Lt. End row of rock in conc. <sup>conc.</sup>			
	3 <sup>s</sup> Lt. = line row of rocks set in			
7+62	2 <sup>s</sup> Lt. = 3/4" water stand pipe			
	in conc.			
7+55	2' Lt. = End row of rocks set			
7+50				
7+32	3' Lt. = start row of rocks set in conc.			
7+30	Φ comes onto bench			
	trees, 11 trunks - 2" Diam.			
7+13	A' Lt. = Ctr. of Clump of Tamarisk			
T.P.	0.97	<u>237.60</u>	12.63	236.63
6+77	start of bench on Lt.			
		<u>249.26</u>		

52

		226.9		
<u>11.7</u>		11.2		<u>11.4</u>
5				5



		228.0		
<u>9.5</u>		9.6		<u>8.6</u>
5				5
				1

		228.5		
<u>9.0</u>		9.1		<u>5.9</u>
5				1
				5

		233.6		
<u>9.4</u>		9.0		<u>2.9</u>
1				10
		<u>237.60</u>		

		240.6		
<u>10.3</u>		10.7		<u>8.7</u>
10				3
				2
		<u>249.20</u>		

T.P. 0.15 187.69 13.16 187.49

9+00

8+75

T.P. 0.07 200.65 13.23 200.58

8+25

8+10

T.P. 1.01 213.81 12.96 212.80

8+05

7+83

225.76

187.9  
12.8

193.0  
7.7  
200.65

204.7  
7.1

207.7  
6.1  
213.81

212.3  
13.5

224.9  
0.7

225.76



T.P. 0.65 162.87 12.94 162.22

10+70

10+30

T.P. 0.72 175.16 13.20 174.44

9+92<sup>15</sup> =  $\Delta$  13°-10' Lt.

Nearest point (Page 48)

9+66 = 3' Lt. = Face of wall at

9+32.17 =  $\Delta$  37°-50' Rt. (on pav)

private road

9+26.8 = start plant mix cold lay on

187.64

164.3  
10.9

170.6  
4.6

175.4  
12.2

178.3  
9.3

183.5  
4.1

184.2  
3.4

187.64

B line

13+00

12+51 <sup>Σ</sup> = Δ 36°-14' Lt.

12+00

11+50

11+01.94 = Δ 81°-08' Lt.

10+96 Start A.C. Pav. on Armada

162.87

55

154.5  
8.4

155.1  
7.8

156.2  
6.7

157.7  
5.2

158.6  
4.3

158.8  
4.1

162.87

"B" Line

$\frac{-0.03}{155.51}$  Page 30,

4.34 155.48

15+40.2 = Exist D.F. = 0+00 on "D" line

14+18<sup>60</sup> Cont.

14+18<sup>60</sup> = Exist M.H. also =  $\Delta 1^{\circ}09'$  RT. to Exist D.F.

14+00

T.P. 4.84 159.82 7.89 154.98

13+50

13+27.6 = End A.C. & start Conc. Pav.

162.87

56

149.10  
10.72  
Invert Exist M.H.

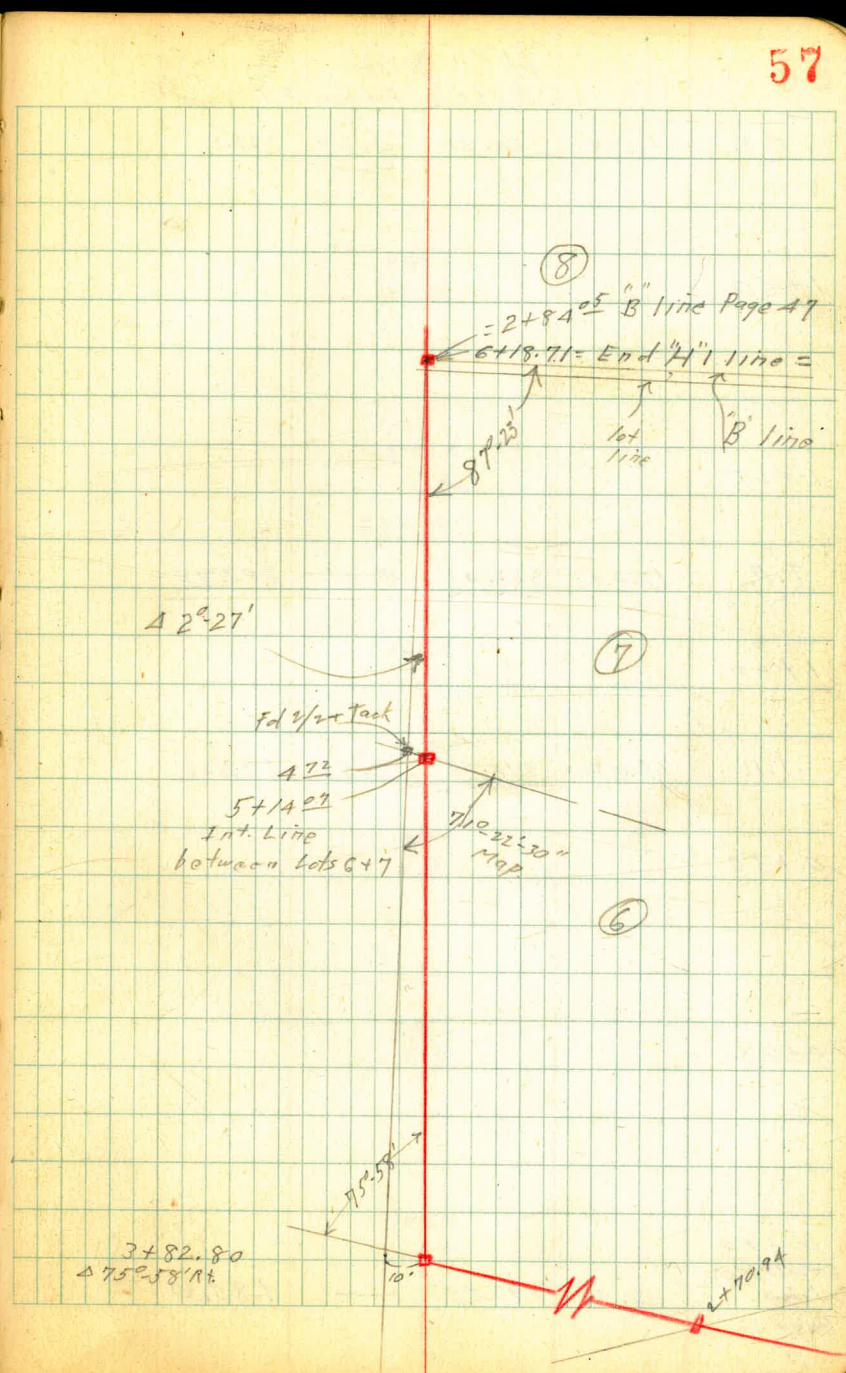
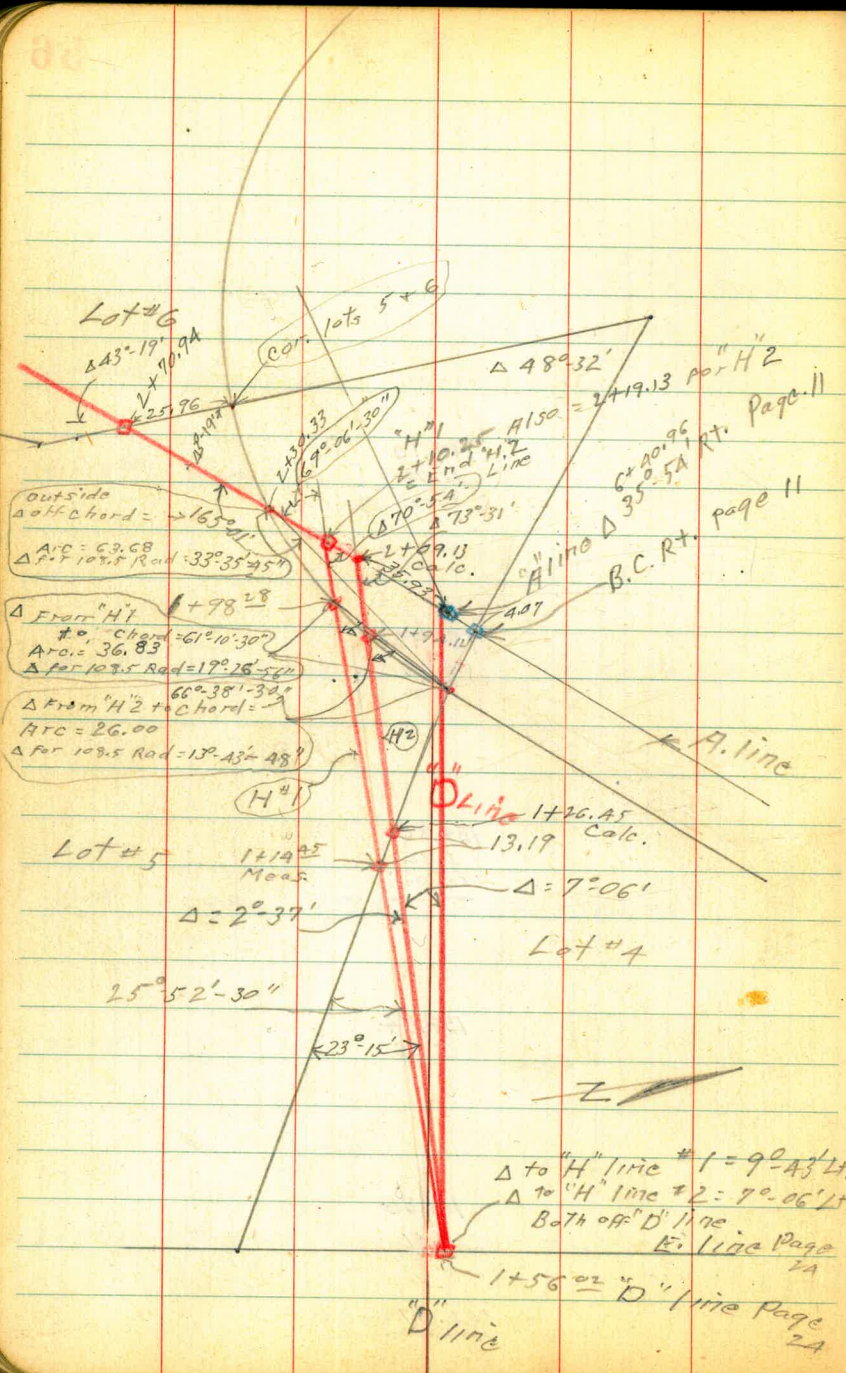
154.92  
4.90  
Rim

154.80  
5.02  
159.82

154.54  
8.33

154.36  
8.51

162.87



"H"<sup>42</sup> Line  
Sketch page 57

T.P. 12.68 234.80 0.29 222.12

1+60

218.1  
4.3

1+25

211.2  
11.2  
222.41

T.P. 12.44 222.41 0.27 209.97

1+00

205.2  
3.0

T.P. 13.02 210.24 0.53 197.22

210.24

0+50

195.7  
2.1

0+08

188.0  
9.8

0+00  
EX 2175602  
D line  
Page 32

12.45 197.75 — 185.30

186.0  
11.8

"H" 2

59

2x2 6+40.96 H line  
Page 15 = 226.15      8.59    226.21    (0.06)

219<sup>13</sup> = End of "H" 2 line  
2+10.25 "H" 1 line

228.1  
6.7

2+09<sup>13</sup>

227.6  
7.2

1+94<sup>13</sup> = Int. street line

228.1  
6.7

234.80

234.80

H#1 Line  
Sketch page 57

\$

60

T.P. 12.68 234.80 0.29 222.12

1+60

211.3 216.2 218.0  
 $\frac{11.1}{100}$   $\frac{6.2}{30}$  4.4

1+25

211.1  
 11.3

222.41

T.P. 12.44 222.41 0.27 209.97

1+00

203.0 205.2  
 $\frac{7.2}{50}$  5.0

210.24

T.P. 13.02 210.24 0.53 197.22

0+50

195.5  
 2.3

1+08

188.0  
 9.8

0+00

186.0  
 11.8

2x2-145602

0' 1170 P.32 12.45 197.75 ~ 185.30

12.3  
 50

3+00

be served - to low

2+70

Property on left can not

+56

2<sup>nd</sup> Lt. = 8" diam. 4' high palm

+40

2+30.33

Int. street line

2+10<sup>25</sup>

Δ 69°-06'-30" Lt.

1+98<sup>28</sup>

= Int. street line

234.80

230.2

230.8

4.6

4.0

4

top bank

229.9

231.1

4.9

3.7

10

top bank

230.9

3.9

229.7

5.1

228.1

6.7

228.8

6.0

234.80



12.33 246.49 0.64 234.16

4+17 3<sup>rd</sup> Lt. = 8" diam pine4+04 4<sup>th</sup> Lt. = 8" diam pine

4+00

3+94 4<sup>th</sup> Lt. = 6" diam tree

to existing tank.

Aprox. position of sewer outlet

3+83 65' Lt. = Ctr. front line of house

10<sup>th</sup> Lt = line of 8" conc wall.

12" diam 5' high palm.

3+82<sup>80</sup> 2<sup>nd</sup> Lt at 90° to Fwd tang =  
Cont.

3+82.80 = A. 75°-58' Rt.

3+40.

234.80

234.4

0.4

228.5

230.0

6.3

4.8

6.5  
Cem. Grd.6.5Floor  
level

228.3

231.5

6.5

3.3

10.4

10.4Base of  
wallTop  
wall

+ ground

230.7

231.79

4.1

3.01

12' x 90° to  
Edge of  
bank

2.2

2.2

229.2

230.3

5.6

4.5

7  
Top bank234.80

for sewer

5+53 { 39' Lt. = outlet thru foundation  
37' Lt. = N.E. Cor. house

5+40

T.P. 11.76 270.25 0.21 258.49

5+15

5+11 4<sup>8</sup> Lt. = End 1/4 post + wire fence

4+75

T.P. 12.43 258.70 0.22 246.27

2+57 7<sup>2</sup> Lt. = start 4x4 post + wire fence.

4+45

4+22 9.9 Lt. = end conc. wall - 8" wide

246.49

258.1 261.5 260.3  
12.2 8.8  
39 37  
Apex Invert 8rd.  
Prop. outlet

259.2  
11.1

270.25

254.6 255.2  
4.1 3.5  
50

247.6 248.9  
11.1 9.8  
50

High enough to  
serve on right

258.70

238.7 242.3 242.2  
7.8 4.2 4.3  
50 50

228.9 231.5 237.2  
17.6 8.0 7.3  
10.7 9.9  
Conc. walk top of  
inside wall +  
wall ground 246.49

"Hi" I line

1+34 "B" Line (Sec p 19) Ho. 56' W. Pumping  
this page) =  $267.99 + 0.8 = 268.79$  Ground

what in all means  
maybe I can tell you  
can't write - hands stiff.  
Weather? Feels like zero

Check P.O.T. Hub  
4+55.43 "B" line  
Page 50.

3.73 272.57 (272.51)

T.P. 8.31 276.30 2.26 267.99

Hub

6+18.71 H-1 Line = 2+84.05 "B" line  
~~2+84.05~~

267.99  
2.26  
Hub

5+90

265.1  
5.2

270.25

Outlet 0.8' above Hub (Sta 6+18.71 "H1" Line. see  
2.7 above same Hub = 270.69

Monroe

7' ct

H.C. Pavc

Hue

4.5

5

6 to 0.19

14'

Block 73

Univ. Hts.

St

N

St

Mississippi

Louisiana

cb. + Pavc is 0.5 on W.

Conc wall

0.100

14'

4.5

H.C. Pavc

7' ct

Meade

Hue

X- Sect. 20' Alley in Block 73  
Univ. Hts.

65

# 2330  
W.O. 31421

5-10-48  
Osborne  
Hardin  
Worrell  
Rover

INDEXED

MAY 11 1948

X-Sect. 20 Alley in Blk. 73

0+60 - 77' Ely. P. pole # P.A. 4413

footing 0.2 below ground

0+50 - 10' Rt. = Beg 8" Conc. block wall - 2.5 High

0+47 - 11.1 Lt. = end - Ely. Conc. walk

0+38 = # Sing. Gar. on Rt. = Conc. floor + apron.

0+30 - 10' Lt. = Beg Reg Lattice fence

0+30 - 11.1 Lt. = Ely 2.5 Conc. Walk along House

0+30 - 12.9 Rt. = # 5 Conc. Walk

0+29 - 10.1 Lt. = N.E. Cor. House

0+15

0+09 - 10.2 Lt. = S.E. Cor. House - Pillars.

0+05 - 12.6 Rt. = S.W. Cor. House - Conc. found.

6" Conc. wall - 13 High. - Rods on edge of Pavc  
the E. + 0.4' S of line on W. at base of

0+00 = N.L. Meade - Pavc + cb. end on line on

0-14 = N. cb.

B.M. 6.46 339.16

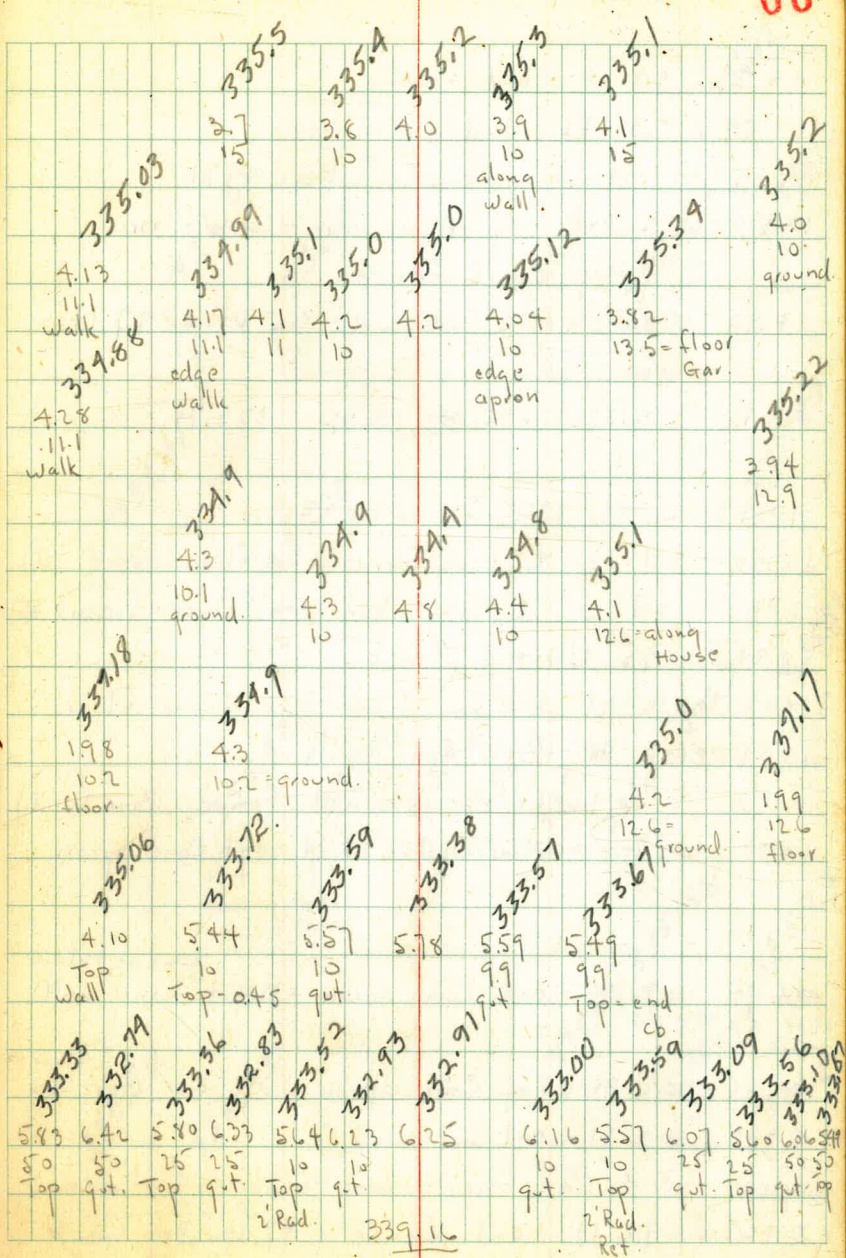
332.70 SE Meade  
+ Louisiana

Lt. = W

#

Rt. = E

66

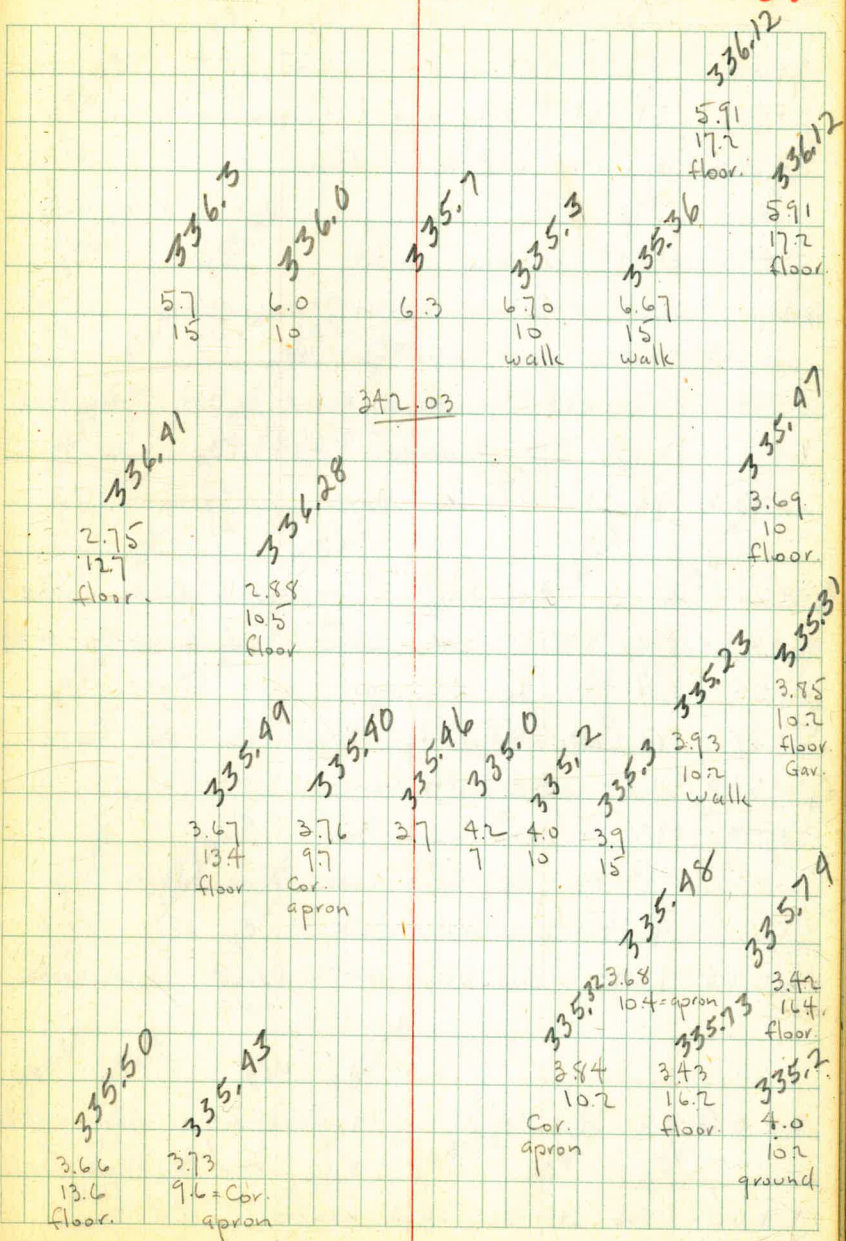


1+99- 9.3 Lt. = end fence  
 1+89- 17.2 Rt. = end 4 car. Gar.  
 1+74- 7' Lt. = Ely. P. pole # P.H. 4431  
 1+53- 17.2 Rt. = Beg. 4 Car. Gar. - Conc. floor.  
     Beg. board fence  
 1+50- N. edge of 2' Conc. walk on Rt. + 9.7 Lt. =  
  
 T.P.      6.29    342.03    3.42    335.74

1+48- 10' Rt. = N.W. Cor. 5 Car. Gar.  
 1+42 12.7 Lt. = 4 Doubl. Gar. - Conc. floor. (opens W)  
 1+30- 10.5 Lt. = 4 Sing. Gar. - Conc. floor. (opens to W)  
 1+21.5- 9.5 Lt. = end fence  
 1+02- 10.2 Rt. = S.W. Cor. 5 Car. Gar. - Conc. floor.  
 1+01- 10.2 Rt. = 18" Conc. Walk  
     + 9.6 Lt. = Beg. board fence (Poor Cond.)  
 1+00- 10.5 Rt. = end Conc. wall + 9.7 Lt. = end Conc. apron

0+92- 6.4 Rt. = end. Conc. apron + Beg. 8" Conc. wall  
     Same as below  
 0+65- 10.2 Rt. = Beg. Conc. apron to 2 car Gar. - Conc.  
     floor.  
 0+65- 10.2 Rt. = end Conc. wall  
 apron to 4 Car. Gar. - Conc. floor.  
 0+63.5- 9.6 Lt. = end fence + 9.7 Lt. = Beg. Conc.

Lt.      \$      Rt.      67



339.16

2+00

2+98.5 - 8.1 Lt. = Beg. board fence

2+98.5 - 9.1 Lt. = end 3 car Gar.

2+93 = end 3 Car. Gar. on Rt.

2+90 - 6.5 Lt. = end Conc. apron

on Lt. - Conc. floor + apron

2+74 - 7.5 Lt. = end Ely. walk at apron + Beg. Car Gar.

2+73 - 7.2 Lt. = Ely. P. pole \* P.A. 4443

2+68.5 - 9.6 Lt. = N.E. Cor. House

2+65 - 7.5 Lt. = Beg. Ely. 2' Conc. walk along House

2+64 = Beg. 3 Car. Gar. - Conc. floor + apron - on Rt.

2+58 - 13.5 Rt. = \$ Sing. Gar. - Conc. floor.

2+50.5 - 9.7 Lt. = S.E. Cor. 2 story. House - Conc. found. <sup>6" below ground.</sup>

2+50 - 9.1 Lt. = end Lath fence

2+48 - 13.8 Rt. = end Doub. Gar.

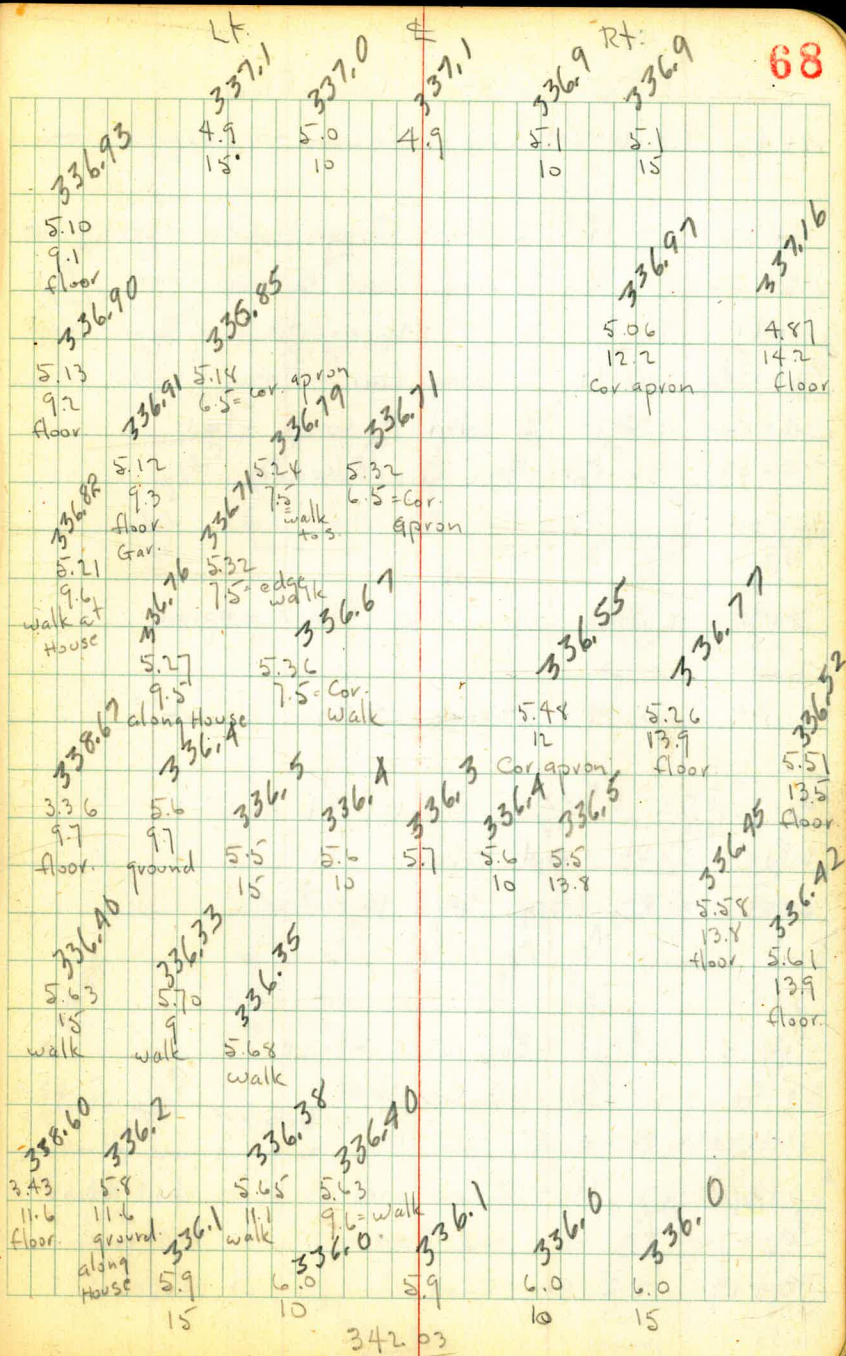
2+30 - 13.9 Rt. = Beg. Doub. Gar. - Conc. floor.

2+26 = 9' Lt. = \$ 2 Conc. Walk

2+25 - 9.6 Lt. = end Ely. Conc. Walk at E.W. walk

2+05 9.6' Lt. = Beg. Ely. 18" Conc. walk along House

2+00 - 8.6 Lt. = Beg. Lath fence



342.03

Sing. Gar - 10' Rt. = Conc. floor.  
 4+43 - 9.4 Rt = € low extension for bumper on  
 - Conc. found.  
 4+32 - 10.9 Lt. = € Glass Green House - Dirt floor.  
 4+22 - 10' Rt. = € Sing. Gar - Dirt floor  
 4+21 - 9 Lt. = € Conc. apron to Sing. Gar. - Conc. floor.  
 4+13 - 10.8 Lt. = € Sing. Gar. - Conc. floor.  
 4+12 - 11.2 Rt. = € Shed - Conc. floor  
 4+09 - 9.6 Lt. = end wire fence  
 4+00

on Rt.  
 3+93 = € Sing. Gar. - Conc. floor + apron

T.P. 6.04 343.66 4.41 337.62

3+76 - 7.6 Lt. = Ely. P. pole # P.A. 4457

3+74 - 10' Rt. = end Porch

3+63 - 10' Rt. = Beg. Porch to House

3+50

3+46.5 - 9.5 Lt. = Beg. wire fence

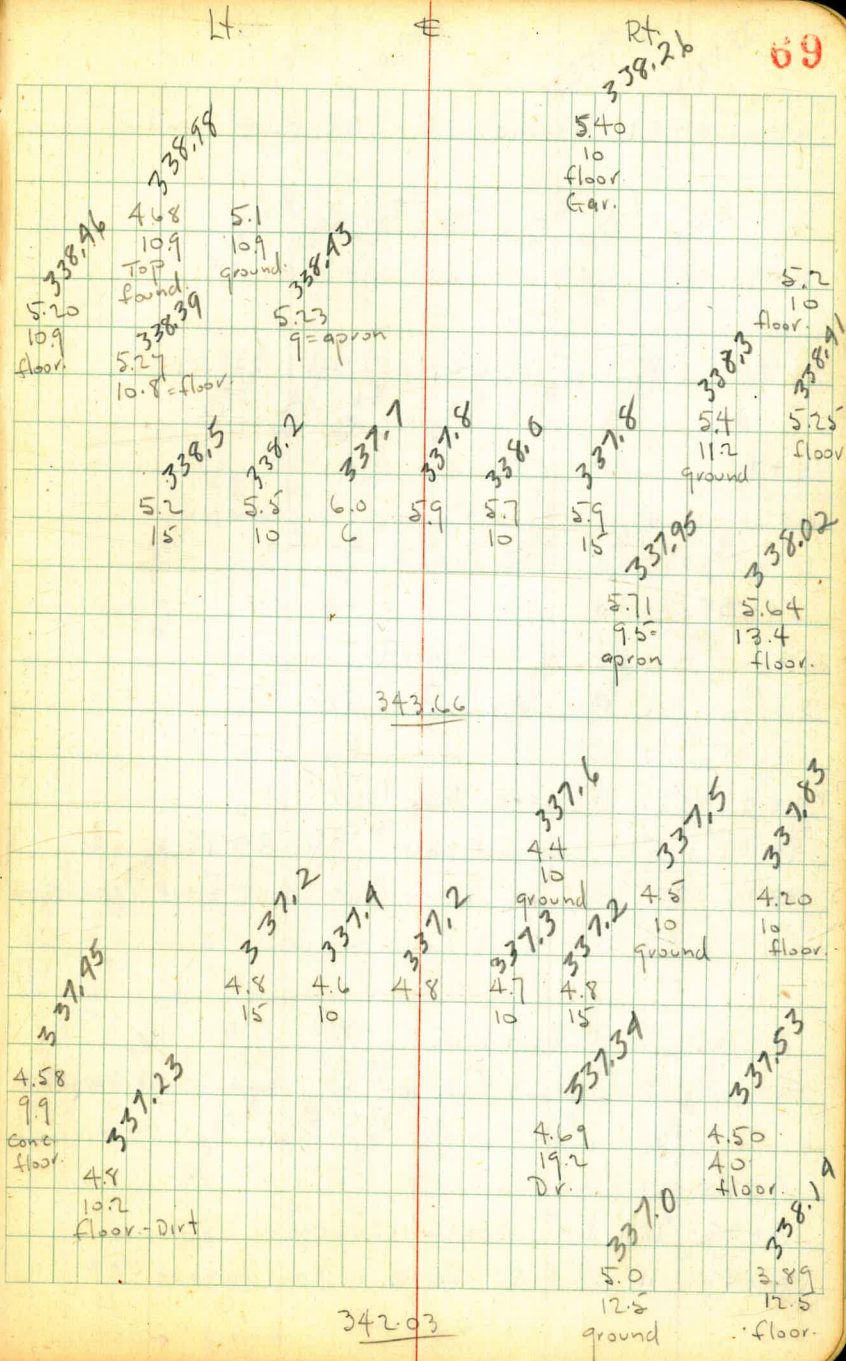
3+46.5 - 9.9 Lt. = N.E. Cor. shed.

3+41 - 19.2 Rt. = € 10.5 Conc. Dr. - to Doub. Gar. - Conc. floor.  
 N. 1/2 is Conc. floor

3+27 - 10.2 Lt. = S.E. Cor. Shed. (S. 1/2 is dirt floor)

3+27 - 8.2 Lt. = end fence

3+19 - 12.5 Rt. = € of Wing (11') of House -





6 + 00.19 = S.L. Monroe = edge A.C. Pauc + end of obs.

5+90

T.P. 5.41 342.62 6.45 337.21

5+70

5+69 - 10.1 Lt. = end fence

5+50

5+32 - 10' Lt. = Beq. Board fence

5+26 - 9.1 Rt. = Beq. Picket fence

5+00

4+95 - 9.6 Rt. = end Doub. Gar.

4+77 - 7.5 Lt. = Ely. P. pole # P.A. 4473

4+75 - 9.4 Rt. = Beq. Doub. Gar - dirt floor - opens to N.

4+73 - 9.9 Lt. = \$ 3' Conc. walk

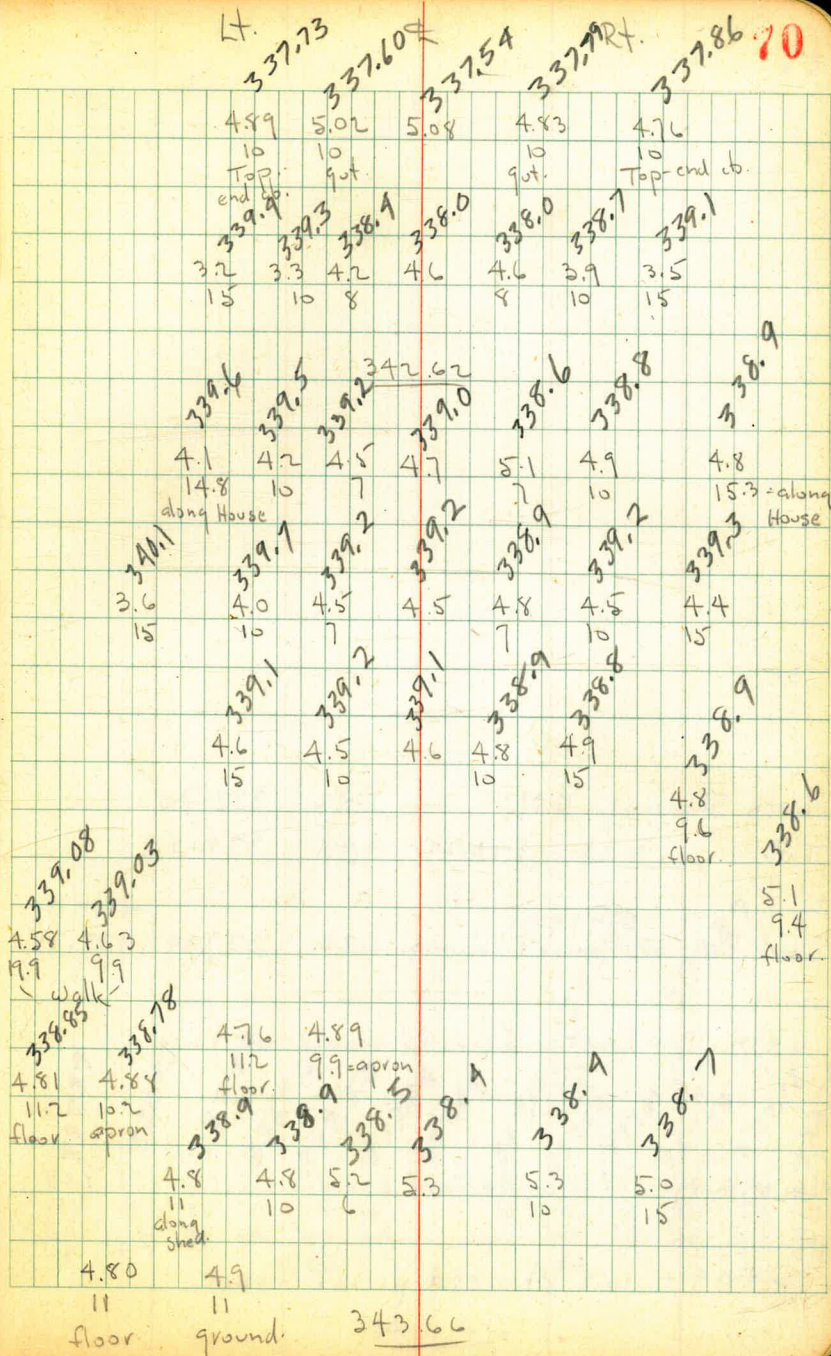
4+765 - end Doub. Gar.

4+57 - Beq. Doub. Gar on Lt. - Conc. floor + apron

4+50

4+49 - 10.1 Rt. = beq. wire fence

4+47 - 11' Lt. = \$ Shed. - Conc. floor



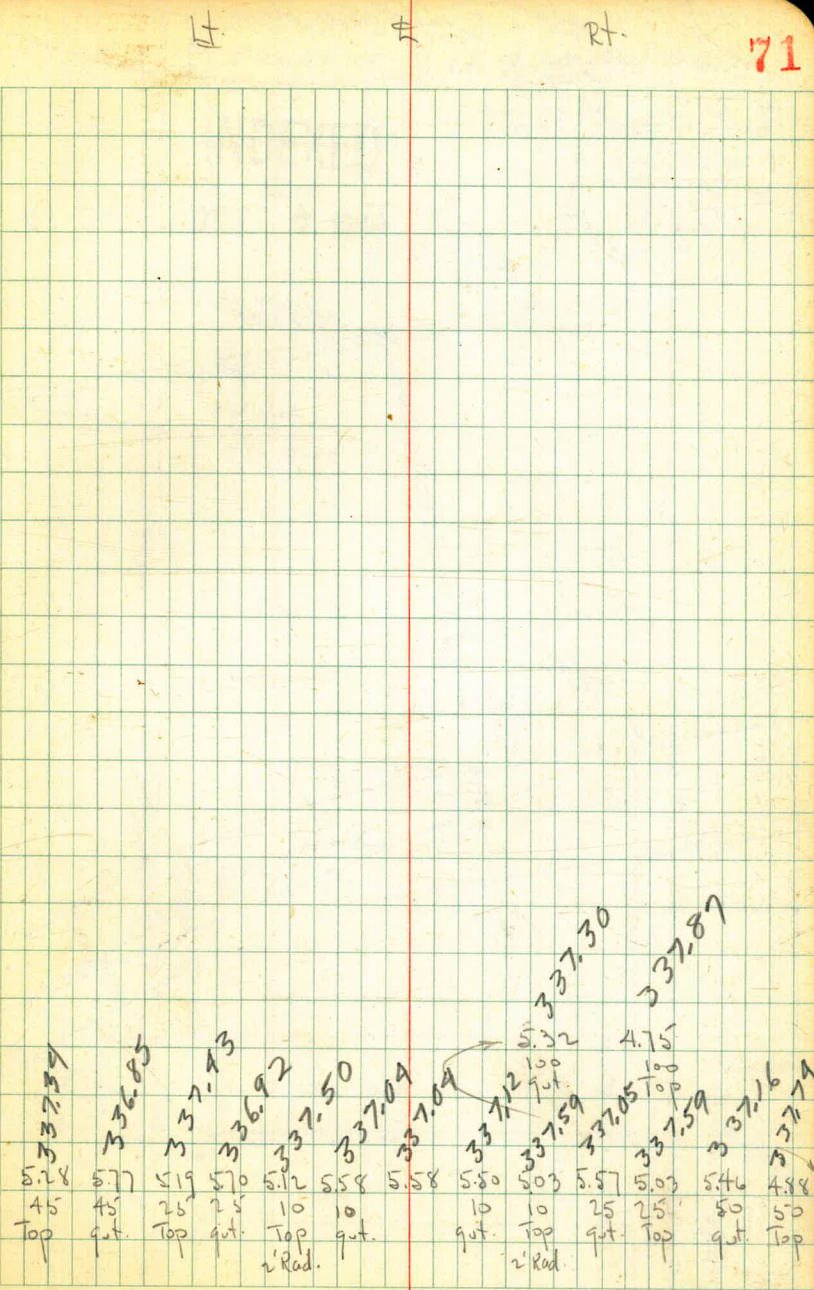
check Starting B.M. 7.52 332.70 ✓  
 T.P. 2.08 340.22 4.48 338.14

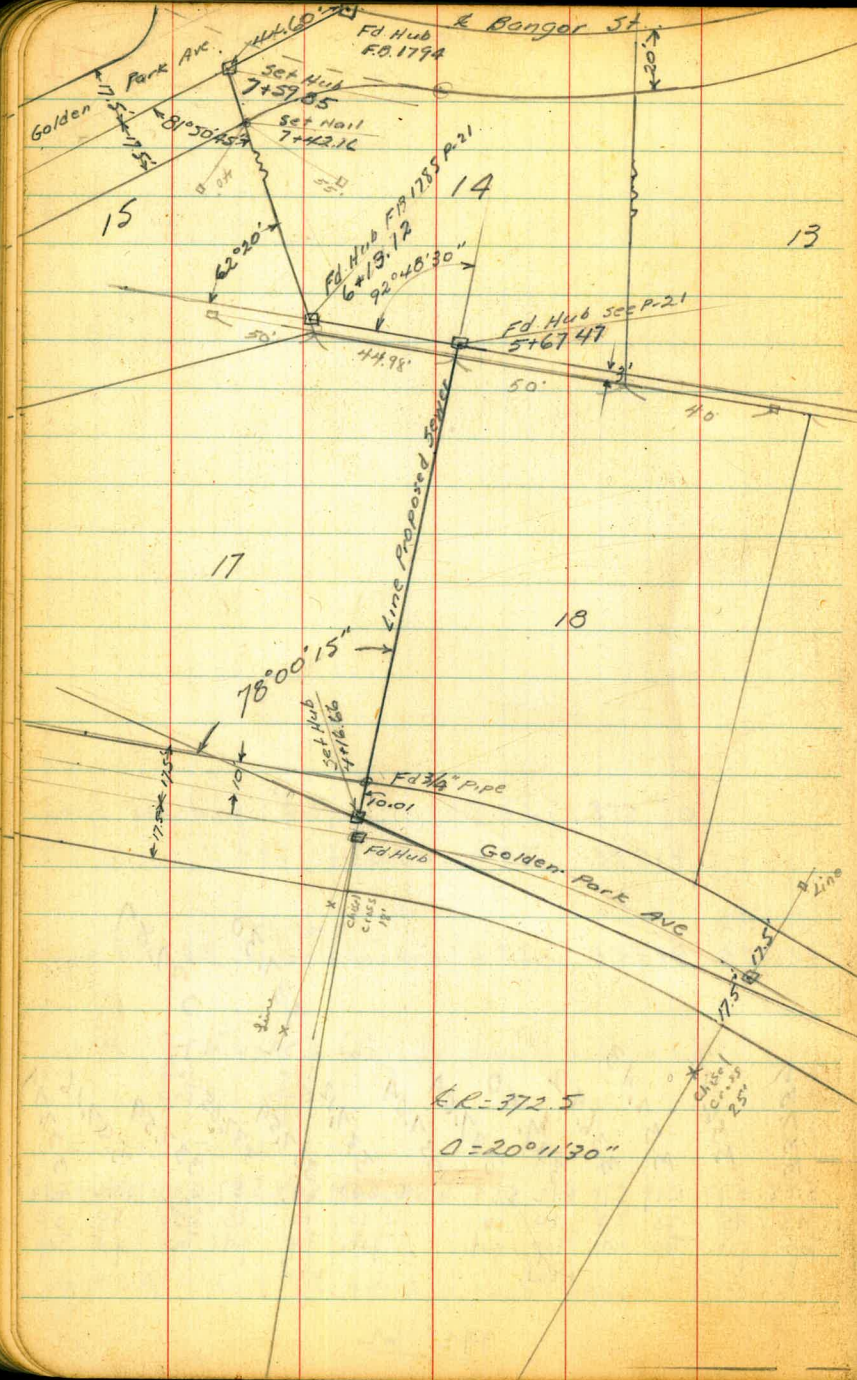
check B.M. <sup>Plug gone</sup> SE. Monroe & Louisiana 5.28 337.34 1543-79 337.35

6+14.19 - Cont. (Grade should fall to w.)

6+14.19 = S. cb. Monroe

6+04 - 10.8 Rt. = end picket fence



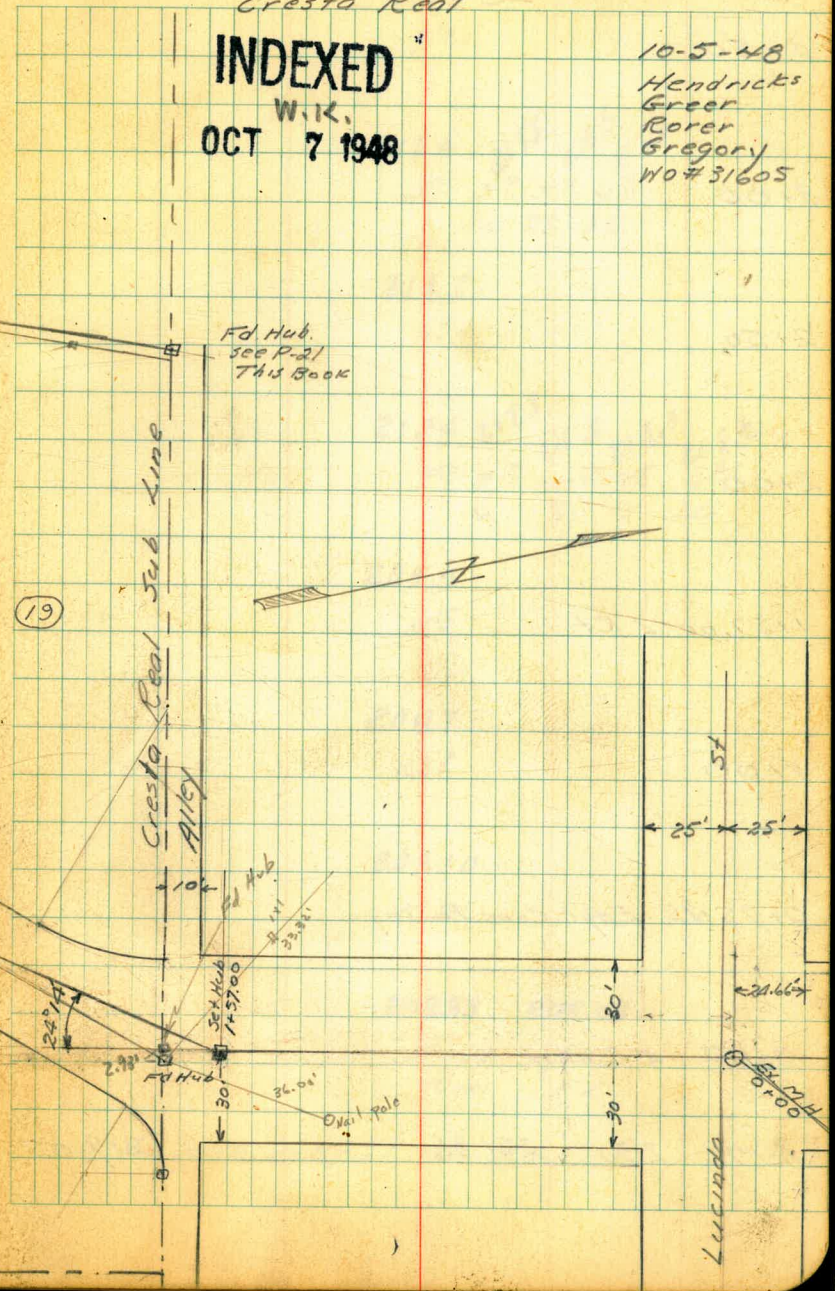


CR-372.5  
 $\theta = 20^{\circ}11'30''$

Proposed Sewer to Serve  
 Blocks 10, 11, 12, 13, 14, 15, 17, 18, & 19 72  
 Cresta Real

**INDEXED**  
 W.K.  
**OCT 7 1948**

10-5-48  
 Hendricks  
 Greer  
 Rorer  
 Gregory  
 WO# 31605



Levels Proposed Sewer  
Cresta Real

2+50

INDEXED

3+00

2+50

2+00

1+57.00 L.Rt.

1+00

0+25.45 Edge Conc. Paving

0+00 Ex. M.H.

B.M. 231 221.36

219.05

217.8

3.6

216.4

5.2

215.5  
216.6  
5.9  
4.8  
24 28 32

214.7

6.7

212.4

9.9

212.3  
211.2  
213.9  
215.2  
9.3  
10.3  
7.5  
6.2  
6 8 11 20

209.9

11.5

208.7

12.7

208.10

13.26

208.89

202.08

12.47

19.28

Rim

FL

on & Hub 2+44.39 FB 1794 P 15

6+13.12 L Rt. Taken Rt. to Forward line

5+67.47 L Lt. Taken Parallel to Lot line

TP 10.47 253.55 1.44 243.08

5+00

T.P. 13.39 244.52 0.15 231.14

4+54

4+40

4+33

4+16.66 L Rt.

TP 12.24 231.29 2.31 219.05

4+00

221.30

243.1 244.2 244.58

10<sup>5</sup> 9<sup>2</sup> 8<sup>9</sup>  
100 50

244.52 245.6 245.6  
9<sup>0</sup> 8<sup>9</sup> 8<sup>9</sup>  
Hub 50 100

236.7 235.5 235.7  
7<sup>8</sup> 9<sup>0</sup> 8<sup>8</sup>  
50 100

230.4 229.5 229.9  
0<sup>9</sup> 1<sup>8</sup> 1<sup>4</sup>  
50 100

221.9  
9<sup>4</sup>

218.3  
13<sup>0</sup>

219.02  
12<sup>2</sup>  
Hub

218.8 217.8 218.1  
2<sup>5</sup> 3<sup>6</sup> 3<sup>3</sup>  
14 20

14

B.M. 266 260.37 260.38

7159.85 & Golden Gate

7127

7100

TP. 9.66 263.03 0.18 253.37

6172

6150

253.55

& Hub 5105.2 FB 1794 P-7

257.46

5.51

Hub

256.9

61

252.7 254.33

10<sup>3</sup> 81

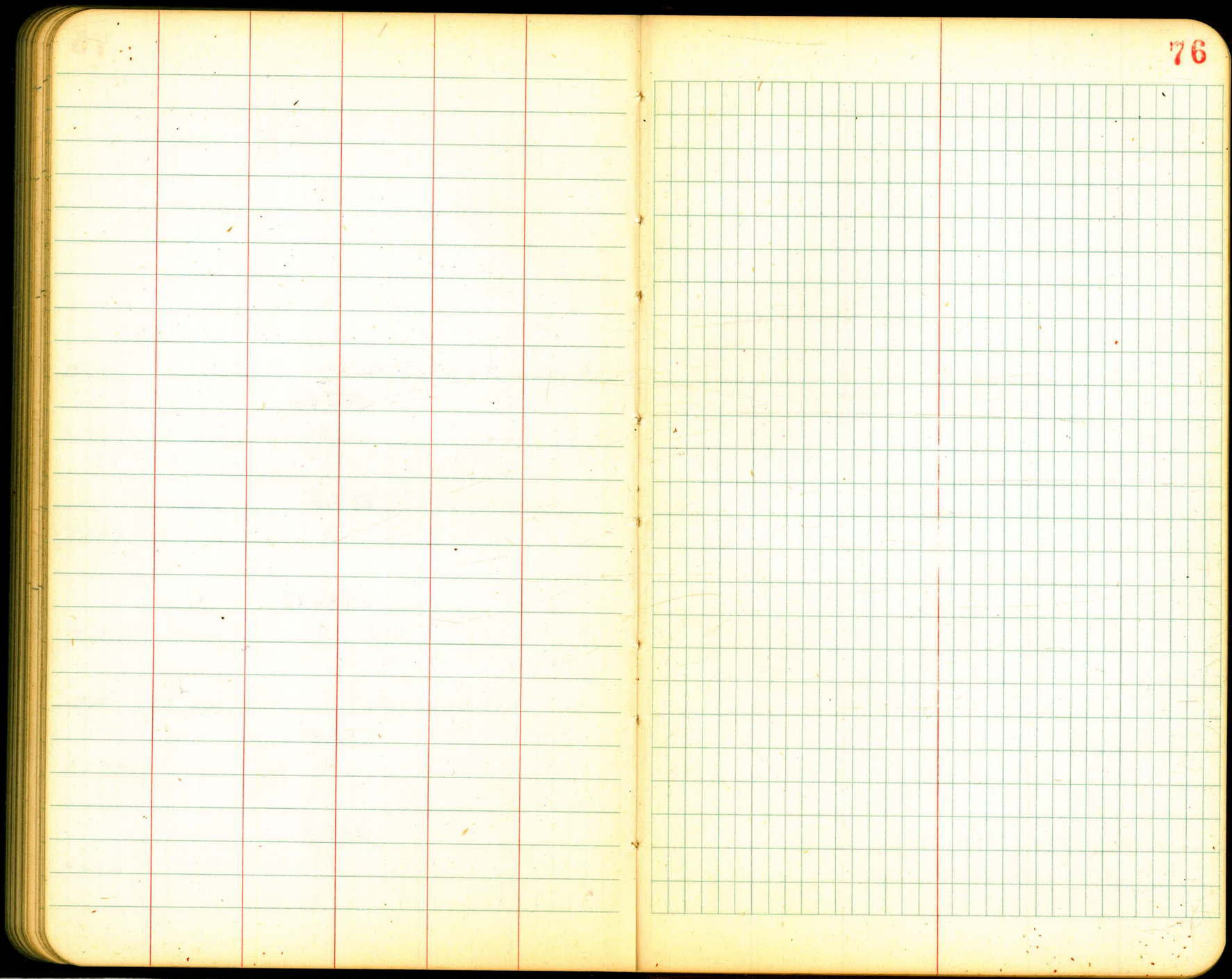
50

251.2

21

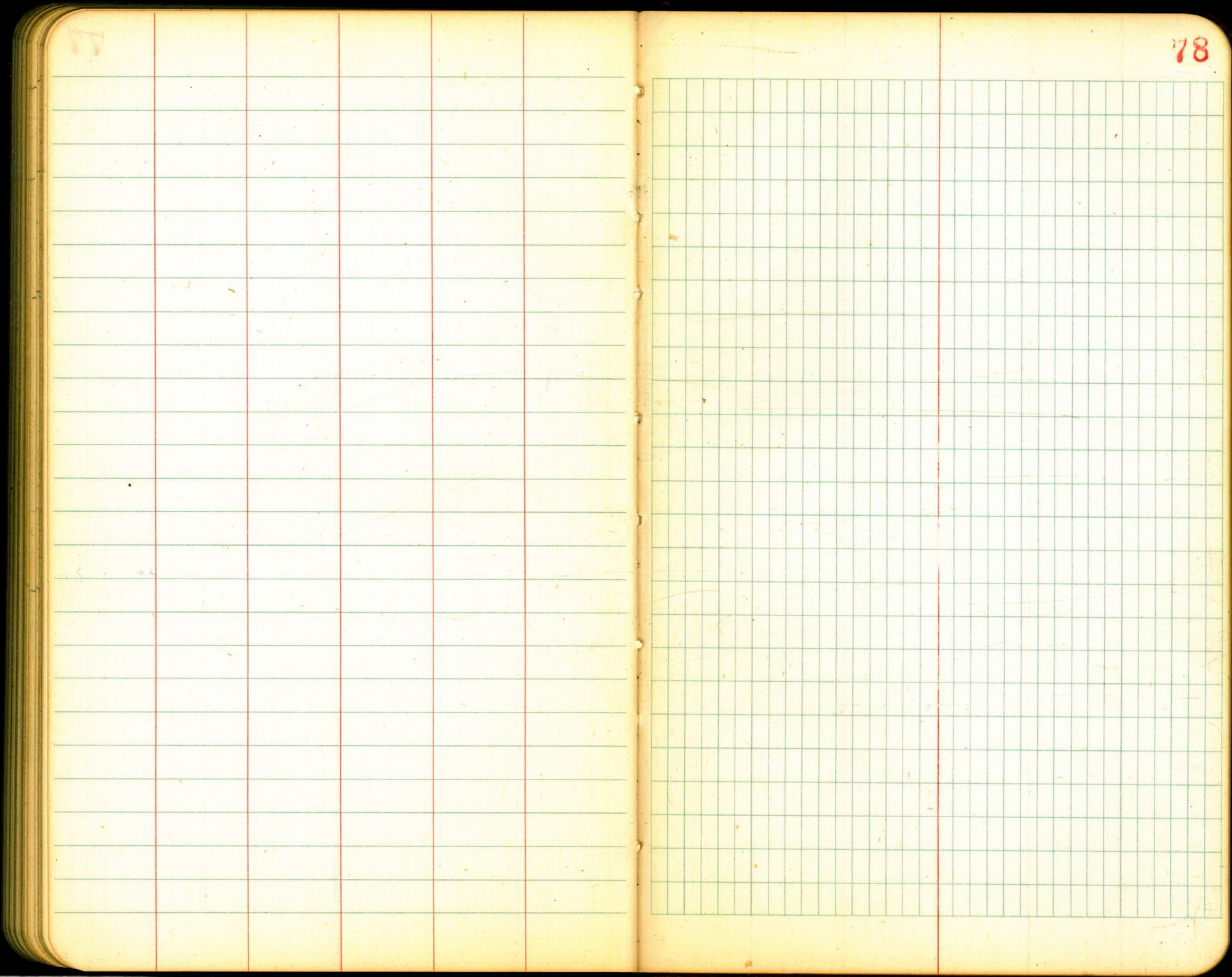
248.3

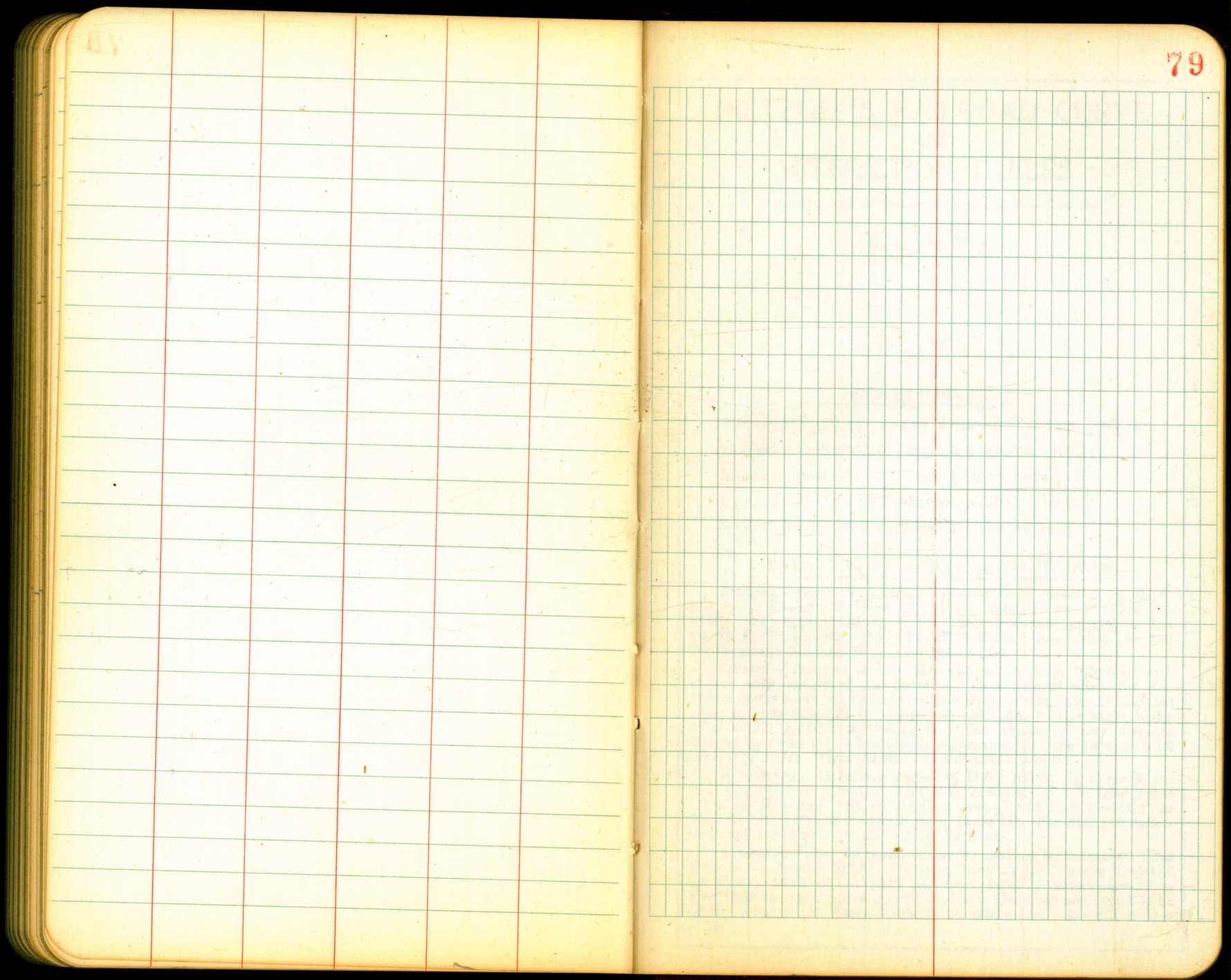
5.3



The image shows an open notebook with two pages. The left page is numbered 87 and features a grid with 5 columns and 20 rows. The right page is numbered 77 and features a grid with 1 column and 20 rows. The pages are yellowed and show signs of use. The notebook is bound in the center, and the pages are slightly curved. The background is a light-colored surface.







79



687  
1247  

---

1928

339.16

3.42

335.74

6.29

342.03

4.41

337.62

6.04

343.66

6.45

337.21

5.41

42.62

342.62

528

4.48

37.34

338.14

547 45 E  
 567 56 30 E  
 47 45  
 20.11 20 11 30  
 280  
 9825

DISTANCES FROM CENTER OF ROADWAY FOR  
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \cdot 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.