

1786

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

MICROFILMED

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

DEC 29 1964

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \times 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.
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1786

Mission Valley Sewer
Construction

30 x 4
#

CITY ENGINEER'S OFFICE

INDEXED
to page #69

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

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to b
of r
exar
30.6

M. Valley Sewer Construction 1 to 19

" " #3 "

20 to 34

Alignment Mission Valley Trunk Sewer
No 3 Construction

INDEXED
W.K.

DEC 6 1949

40+55.13 Δ $3^{\circ}49'30''$ Rt.

40+30 = Fly Jacking Operation

39+73 = Fly Jacking Operation

37+70 = Fly Jacking Operation

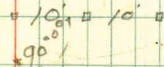
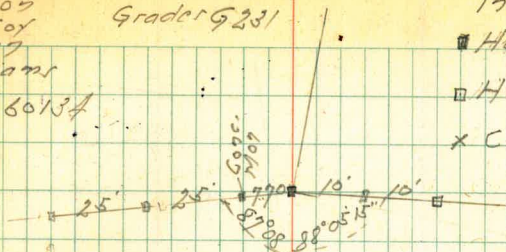
36+10 = Fly Jacking Operation

35+45.28: Existing Sewer Man Hole

July 1-47 Levels 1788
Sisson
McCoy Grader 9231
Riley
Williams
W.O # 60134

Indicator 1

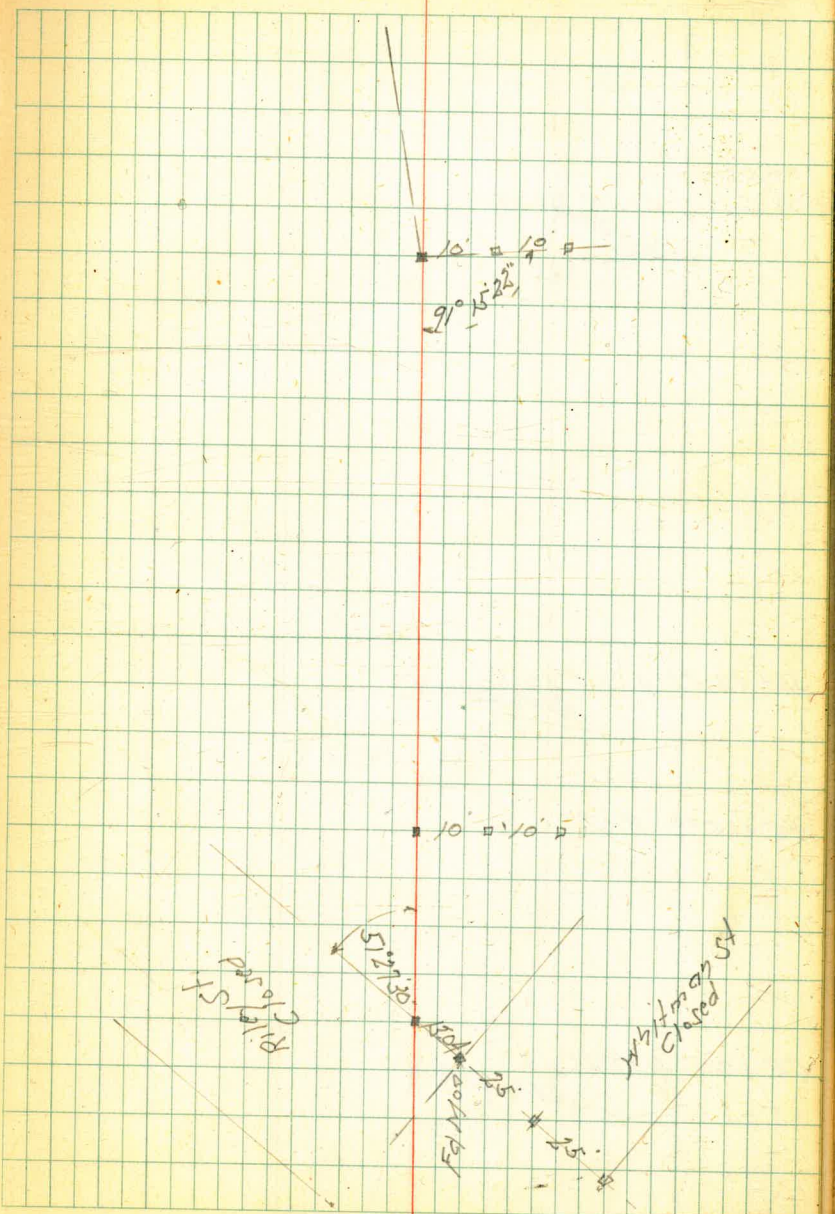
▣ Hub Found
▣ Hub Set
x Chisel/Cross x



51700 J
5173842 A 2'30" 45" Lt

46700 P.O.T.

4479730



6070500 ↗
6070646 ↘ $\Delta 10^{\circ} 25' R$

5674842 $\Delta 14^{\circ} 10' R$

5576500 P.O.T.

55700 $\Delta 19^{\circ} 26' L$

3

6070500 $\Delta 11.16^{\circ}$
87.97

6070646 $\Delta 82.55^{\circ}$
10.08

5674842 $\Delta 98.43^{\circ}$
10.12

74760.00 P.O.T.

69761.05 J
69759.15 J

68756.62 Δ 0° 45' 6"

63753.56 Δ 7° 03' 11"

4

10' 10'

Grass
Stem
Bark
90° 22' 30"
Stem
Bark

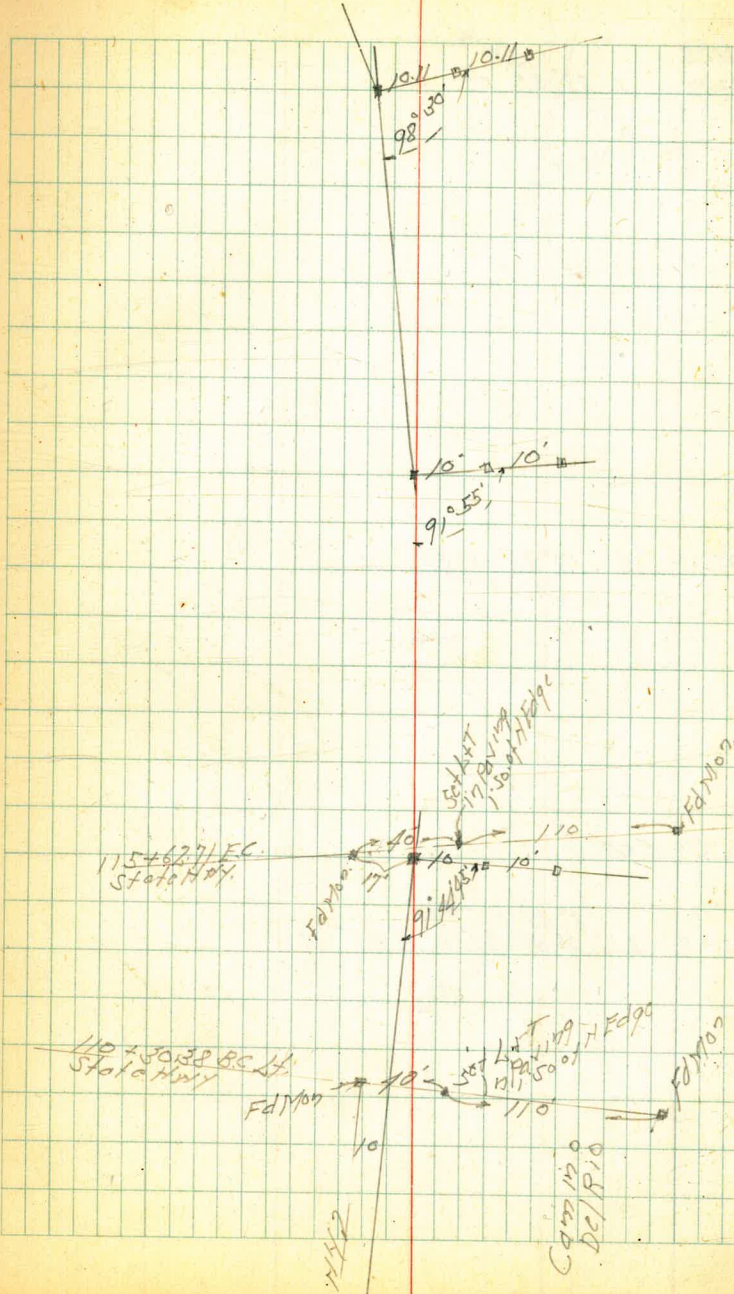
1002' 1002'
86° 28' 30"

89+06.00 Δ 17°00' Lt.

84+46.05 Δ 3°50' Lt.

81+01.25 Δ 3°29'30" Lt.

79+21.11



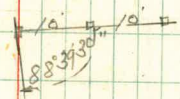
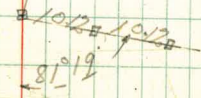
105+33.32

103+28.39 Δ 22° 52' RT

97+87.02 Δ 17° 22' 15" RT

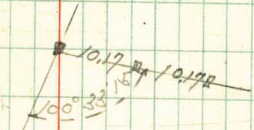
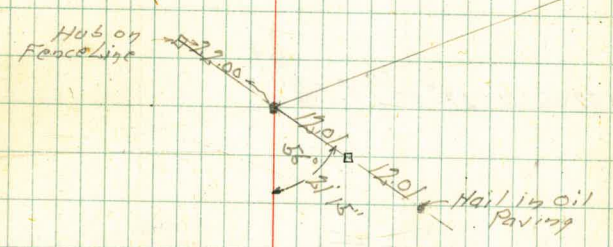
95+66.61 P.O.T.

93+65.00 Δ 1° 49' 50" RT
2° 41' RT MH # 13



112+42.59 $\Delta 67^{\circ} 17' 30''$ Rt.

109+50.00 $\Delta 21^{\circ} 06' 30''$ Lt.

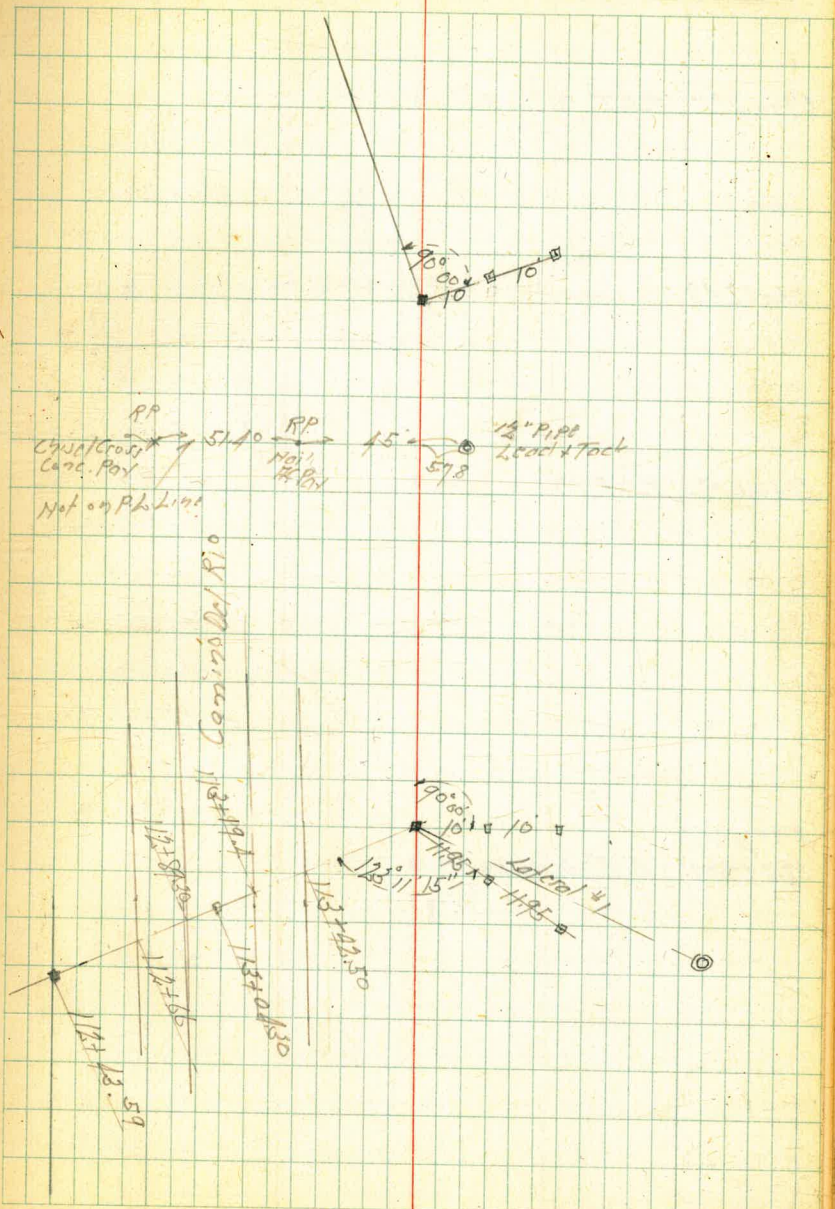


118+92.56 Δ 18° 10' 47"

118+5662

113+92.70 Δ 66° 22' 30" Lt

112+42.59 Δ 67° 17' 30" Rt



37+32.00 P.O.T.

35+62.48

31+40.00 P.O.T.

25+46.68

123+91.41 12° 36' N

9

10' 10'

1885

50' Chicago Coast
14' of S.S. West
Bound Strip

50' Chicago Coast
17' of S.S. Coast
Strip

1885
1885
1885

17.00 18.85
17.45
15.98-41

Ed. 1707
City

10' 10'

10' 10'
91° 18'

54+15.78 Δ 17°22'30" Rt

51+89.96 = Mon

49+15° Δ 0°34'30" Rt

48+21°° P.O.T

39+68.92

10

Fd Mon
"C"

Satellite → 1000 → Fd City
Mon

10' 10' \square
89°
14245

10 \square 10 \square

Fd Mon

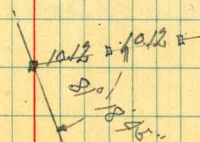
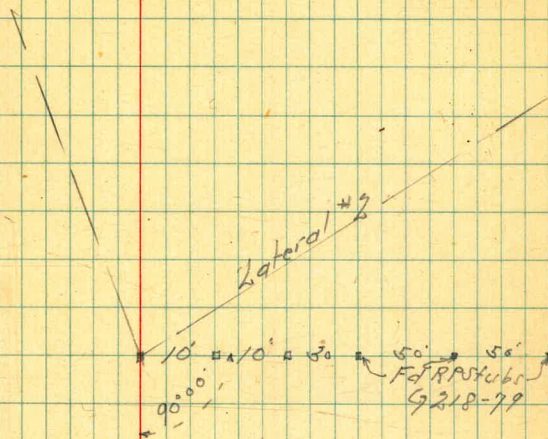
18' Fd State
Mon

Sketch
1/19/52
1/21/52

61+06.48 Δ 20°06'30" Lt.

54+15.78 Δ 17°22'30" Rt.

11



73+66° POT

67+51.86 Δ 12° 05' RE

66+75.29 = Ely Fainting Server

July 11-47
Sisson
McCoy
Robert
Williams

12

□ 10' □ 10' □

□ 10.06' □ 10.06' □
58° 10' 50"

Ely Fainting Server

101470⁰⁰ P.O.T. $\Delta 0^{\circ} 24'$ Rt.

9670150 $\Delta 5^{\circ} 05'$ Rt.

100' 10' 10'

Constructed

100' 10' 10'

Center of

118+50° Δ 12° 22' Lt.

112+90° P.O.T.

107+30° P.O.T.

15

10.06 10.06
96 11

10 10

10 10

129+00 A 6°47'30" Rt.

123+75 POT

Ed Crony
of Concord
1005 1302
8
15

139+8850 Δ 14°26' RT

13A+45° P.O.T

1005 199
829 47
Had six
offshore
house

10' 10'

155+70° P.O.T.

150+90 Hwy EC.

150+0132
149+99967

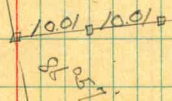
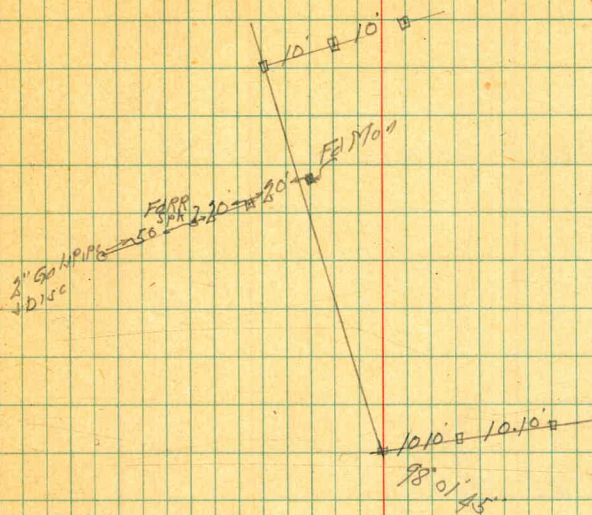
149+5864
150+1190 Δ 16° 03' 30" Lt.

147+24 Hwy BC.

144+00 Δ 6° 06' Rt.

July 17, 47
S. 8807
McCoy
Haddal

18

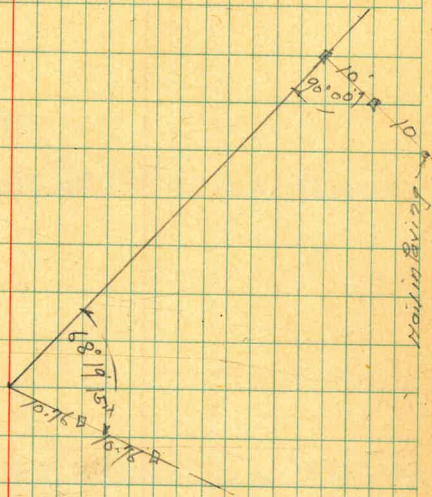


169+40.75 = End of Contract $\Delta 30^{\circ} 13' \text{ Rt}$

165+75.68 $\Delta 43^{\circ} 21' 30'' \text{ Rt}$

161+90.00 $\Delta 42^{\circ} 55' \text{ Lt}$

19



Alignment Mission Valley Trunk Sewer No. 3
East of City Line - As Constructed.

178+28.95 28°-50' RT. Invert
178+41.89 M.H. #50 37.61

175+86.83 Δ 25°-51'-30" LH M.H. 49 37.10

173+58.66 Δ 41°-20'-30" LH M.H. 48 38.64

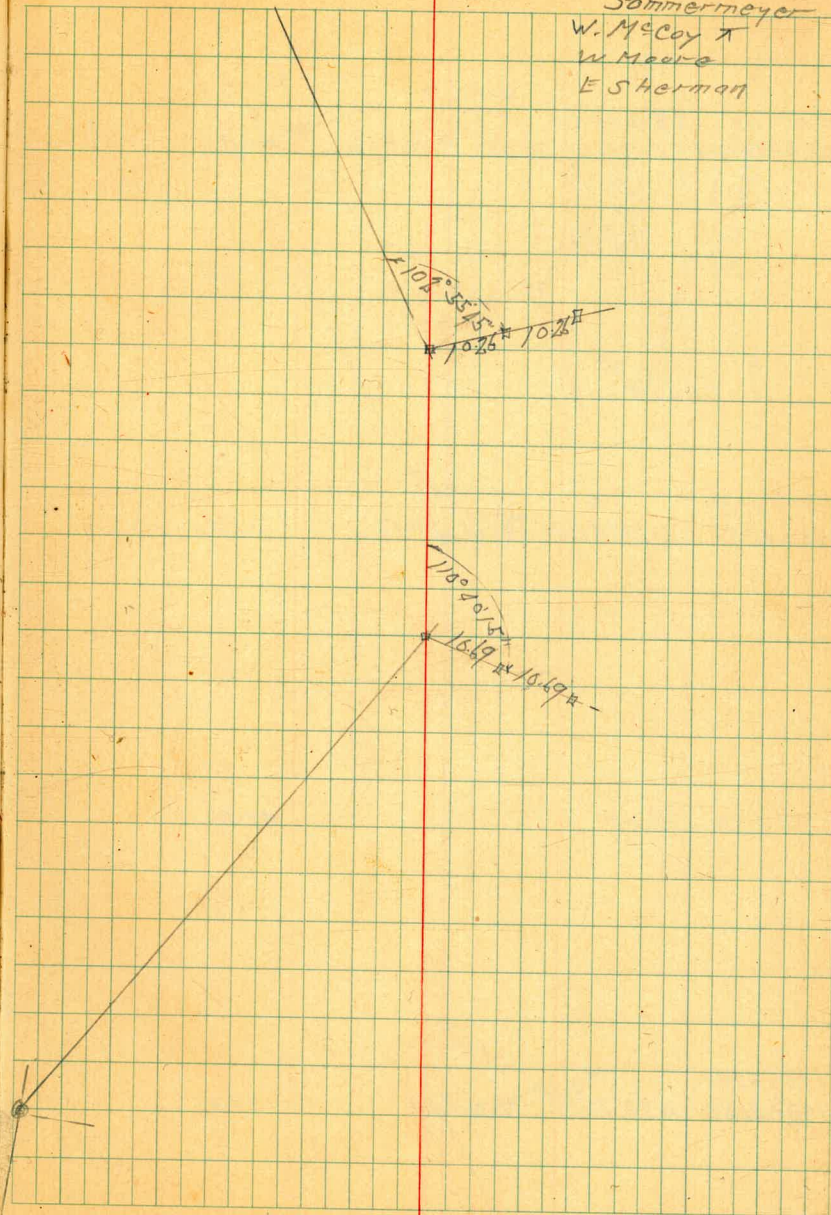
169+47.4 Contract Begins 37.80

169+40.73 Existing Man Hole

Jan-20-1948 W.O. 60162

20

Sommermeier
W. McCoy &
W. Moore
E. Sherman



INVERT

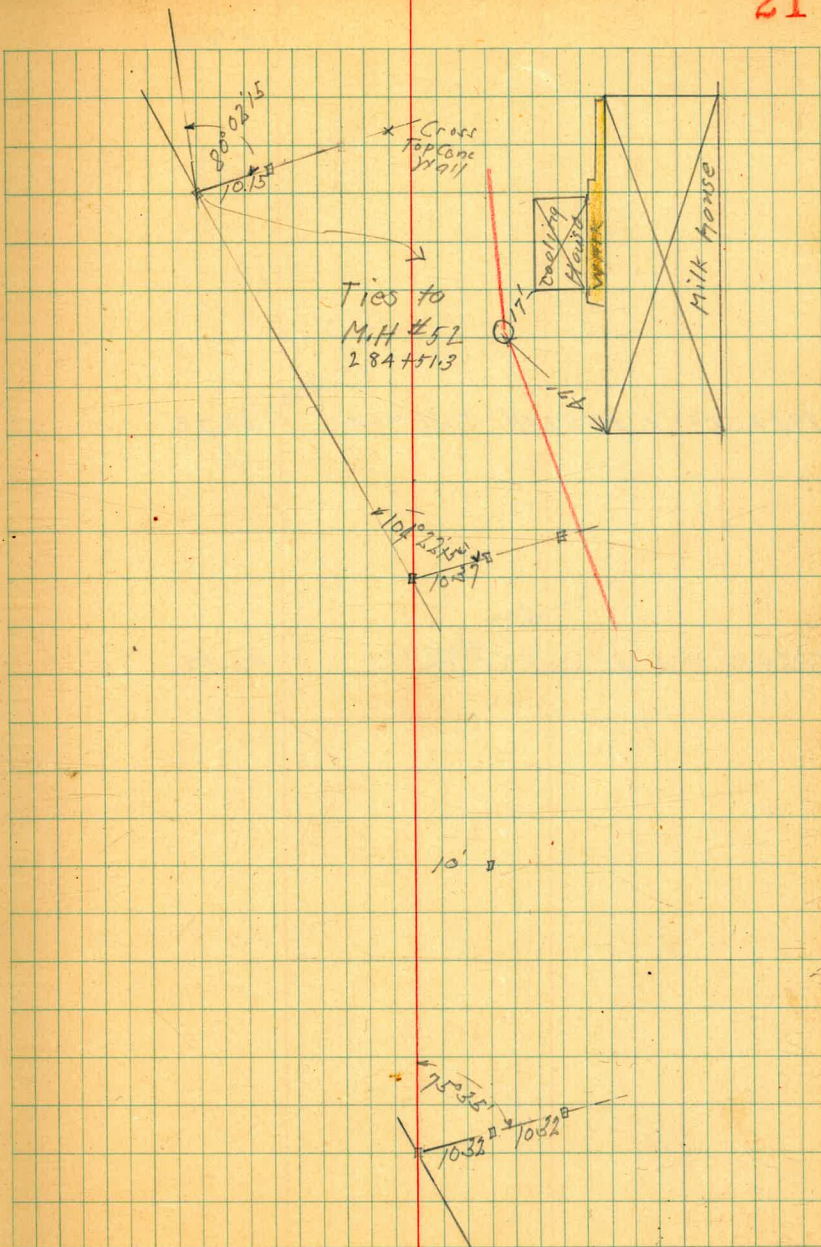
Set. at 284+51.3
284+50.04 = Δ 19° 53' 30" R/L M.H. #52 41.97

279+83.20
185+42.86 Δ 28° 44' 30" L M.H. #51 41.04

181+80 P.O.T 40.31

178+28.94
178+41.89 Δ 28° 50" R/L M.H. #50 39.61

21

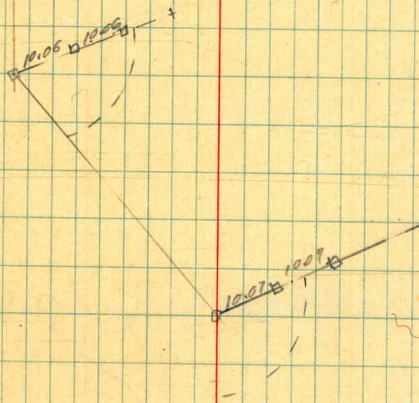


INVERT

294 + 55° Δ 38° 57' RL M.H. #54 43.98

296 + 58° 35' Δ 41° 07' RL M.H. #53 43.59

22



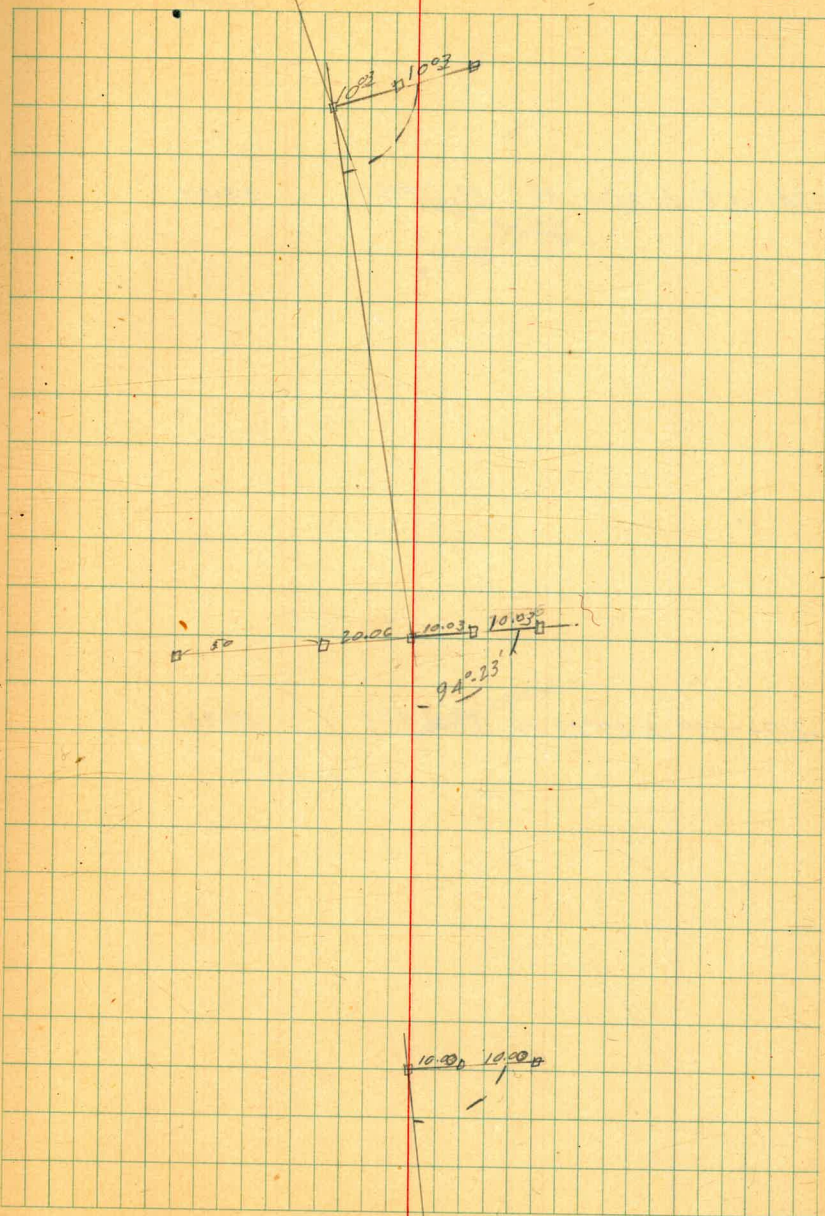
Invert

312+00.5
3107.3599 $\Delta 8^{\circ}45'30''$ L. M.H.#57 48.41

304+00 $\Delta 8^{\circ}46'$ L. M.H.#56 45.89

299+43.72 $\Delta 2^{\circ}12'30''$ R. M.H.#55 44.96

23



Invert.

324+15.31 Δ 21°31' Rt. M.H. #59 56.17

317+76.87 Δ 37°22' Rt. M.H. #58 50.72

24

10.18 # 10.18
79°43'

10.96 # 10.96
37°22'

Invert

$\Delta 40^{\circ}-57'$ Rt. M.H.#62

$341+32^{\circ}00'$ $\Delta 39^{\circ}25'$ Rt. 63.49 Ahead

$341+32^{\circ}82'$ 63.36 Back

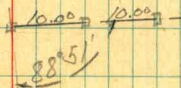
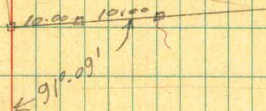
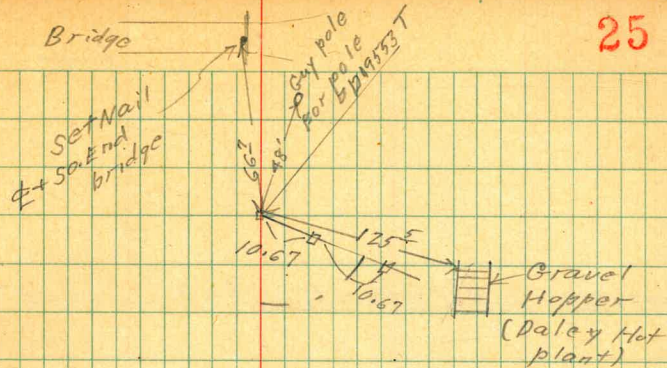
M.H.# 61

$335+60^{\circ}$ $\Delta 2^{\circ}-18'$ Lt. 61.01

$329+90^{\circ}00'$

$329+80^{\circ}03'$ $\Delta 2^{\circ}18'$ Rt. M.H.# 60 58.73

25



invert

348+96.86 Δ 5°16'30" N M.H. #64 66.55

66.04 Ahead

343+86.10 Δ 45°51'30" N M.H. #63 65.94 Back

348+76.97

341+32.00

10.0 10.0

10.0 10.0

Invert

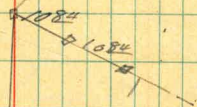
365+65.72 Δ 32° 38' 11" M.H. # 67 68.13

362+80.00 Δ 45° 15' 20"
 367+88.60 Δ 45° 50' 11" M.H. # 66 67.84

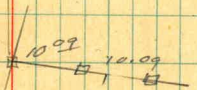
359+40 Δ 0° 50' - 40" Rt. No. man hole.
Line moved 2.50 Left. in order
to miss water well.

357+00 Δ 13° 27' 30"
 Δ 13° 41' 36" Lt. M.H. # 65 67.05

27



10° 10' - 10.09



Invert

1+20 $\Delta 33^{\circ}07'30''$ Lt. 71.05

0+00 Fairmount 69.13 Ahead

370+50.00 $\Delta 73^{\circ}30''$ Rt. M.H. #68 69.10 Back

370+44 "Y" for Fairmount line 69.13 Y to Fairm-
cont.

Fairmount line does not run
through man hole.

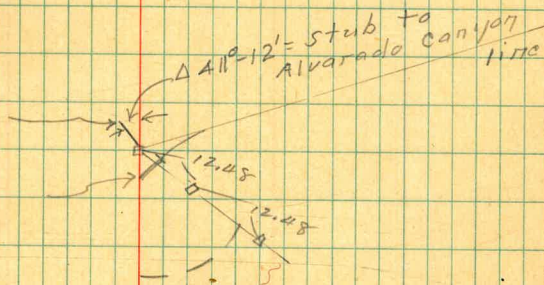
365+65.72 $\Delta 32^{\circ}38''$ Lt. M.H. #67 68.13

28

Stub = 0+07

EL. = 69.24

370+44 = Y

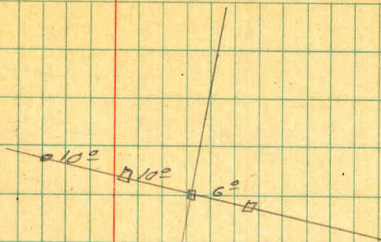


Inquiry

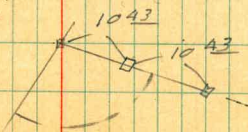
10+80⁰⁰ P.O.T. M.H. #71 85.77

6+38.54 19°32' Rt. M.H. #70 78.00

1+20⁰⁰ 43°07'30" Lt. M.H. #69 71.05



Nail
in Pav

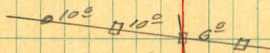
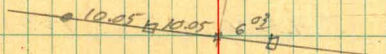
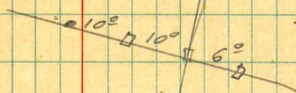


invert

24+00 $\Delta 1^{\circ}17'30''R$ M.H. # 74 111.72

18+98.48 $\Delta 1^{\circ}32'R$ M.H. # 73 100.69

15+26.79 $\Delta 1^{\circ}01'30''R$ M.H. # 72 93.63



Invert

35+44.56 $\Delta 11^{\circ} 42' R$ M.H. # 77 138.83

31+90.00 P.O.T. M.H. # 76 127.32

29+05 P.O.T. M.H. # 75A. 123.05 Ahead
120.23 Back

28+41.91
38739.02 $\Delta 51^{\circ} 15' 30'' L$ M.H. # 75 119.18

31

• 201 □ 201 • 603

• 200 □ 200 • 6

M.H. 75A - put in to
avoid 36" water line

• 6" •

• 1109 • 1109 • 606

• 1109 •

• 606 •

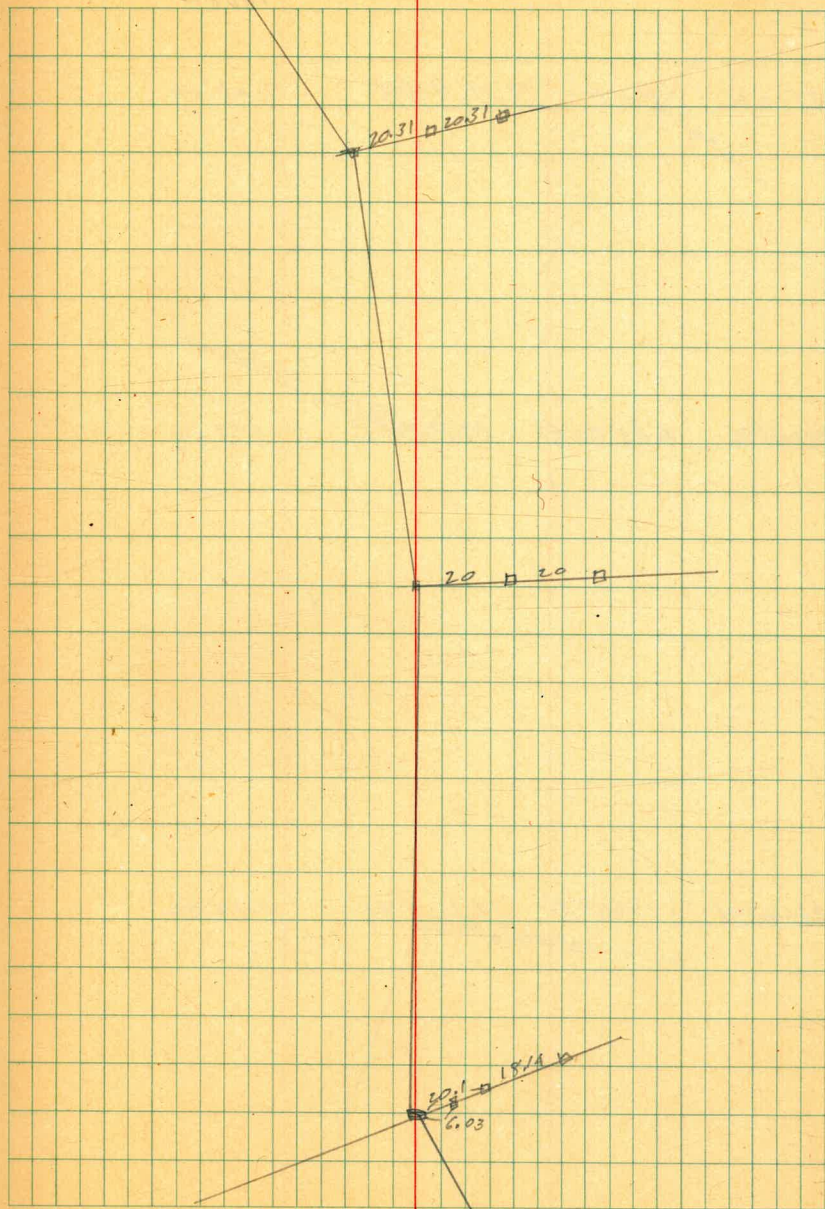
invert

20+00
4877.58 $\Delta 19^{\circ}56' L$ M.H. #80 168.85

44+00 $\Delta 4^{\circ}04' L$ M.H. 79 159.30

38+36.80 $\Delta 11^{\circ}42' R$ M.H. 78 144.09

32

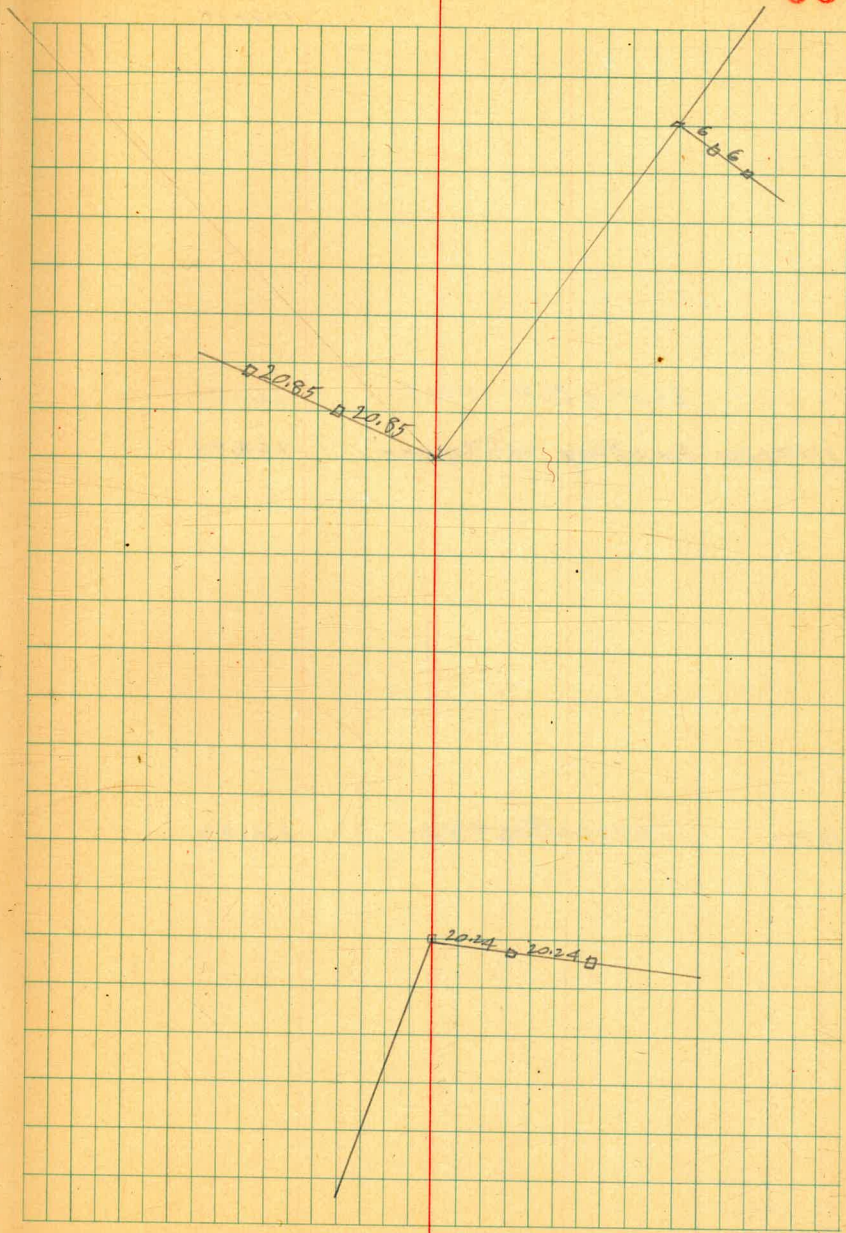


Invert

34+00 P.O.T M.H. # 83 204.89

29+63.96 $\Delta 33^{\circ}00'$ M.H. # 82 193.12

22+95.96 $\Delta 17^{\circ}35'$ M.H. # 81 178.92



Invert

Existing M.H. Inlet 227.61

41+86.60 Existing 10" Sewer 224.94

38+00 2196' M.H. # 8A 214.89

34

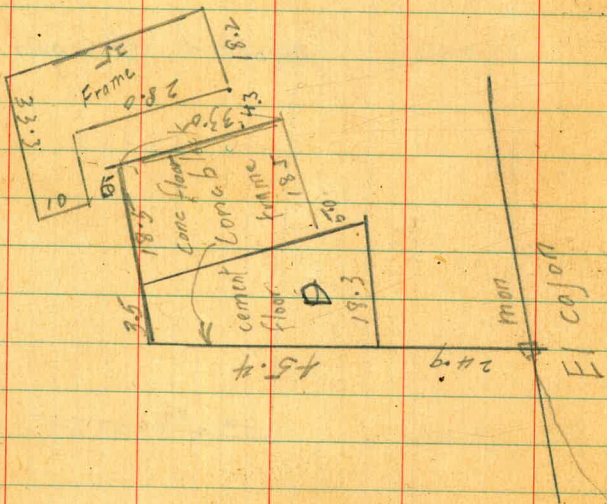
End of Contract

20 20

Levels for Proposed Sewer &
8' Easement Lots 5 & 10
La Mesa Colony

Beeg
Sherman
Bench

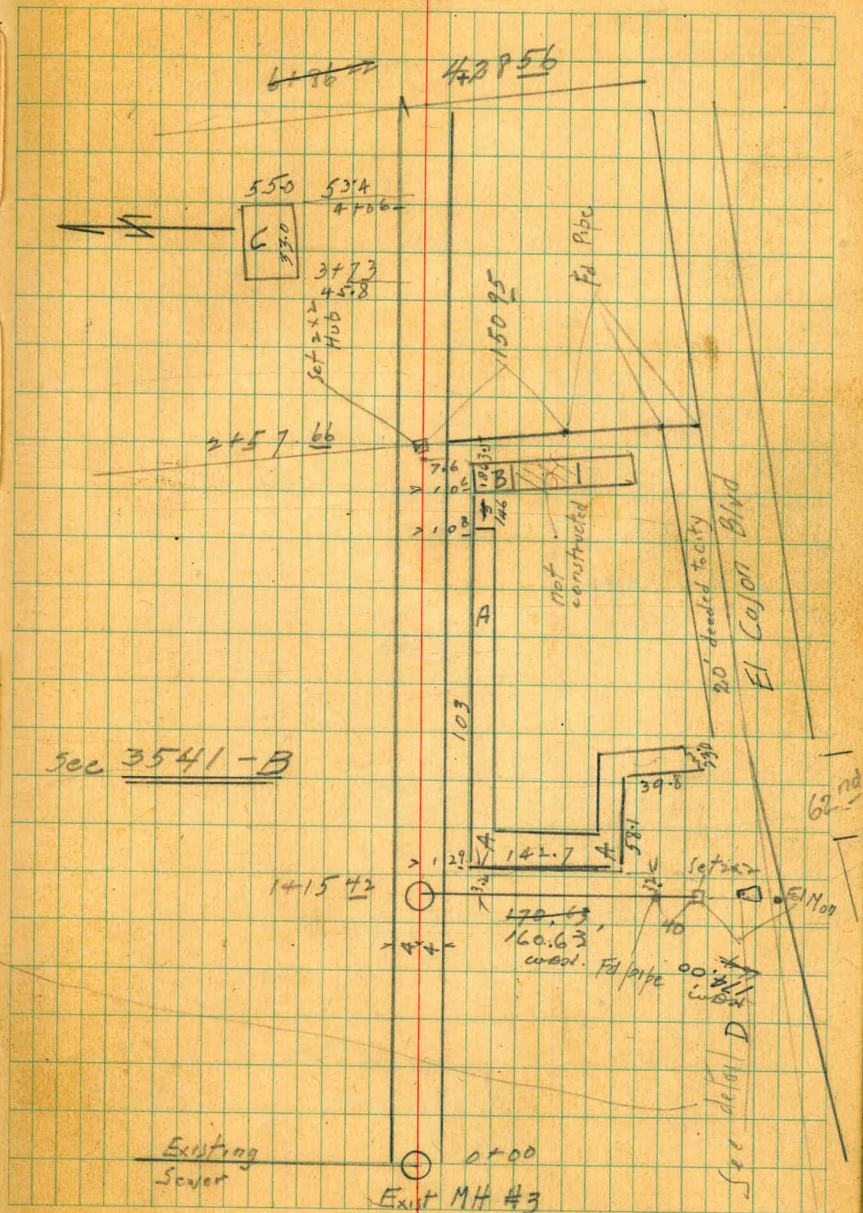
W0 80113



TP	3.17	469.83	3.11	466.66 ✓
	3.50	468.77		465.37 BM

TP	3.16	478.81	7.47	467.65 ✓
	3.85	469.12		465.27 NW BP College & El Cajon

Indexed
C.S.K.



Sec 3541-B

Existing Sewer
Exit MH #3

See detail D

	464.7								
2+57	5.1								
		465.51							
		4.32	Bldg B						
		conc							
	464.2								
2+00	5.6								
	463.9								
1+50	5.9								
	465.0								
1+18	4.80								
	conc floor								
	12.9 ft								
		outlet is located here							
		bldg ft. but not accessible							
	463.8	463.7	464.0	463.6	465.0				
1+15 ⁴²	6.0	6.1	5.8	6.2	4.81				
		50	150	150	150				
		463.8	463.6	floor					
		6.0	6.2	conc					
		210	170						
	463.4								
1+00	6.4								
	463.3								
+50	6.5								
	463.8								
+15	6.0								
	463.99	456.23							
0+00	MH Run	5.84	13.60 ft.						
			470 ft						
	469.83								
	470.81								

469.83

~~470.81~~

469.83

~~470.81~~

461 468.60
 2.51 466.09
 463.99 MTH3 Rim

TP 5.62 470.37 5.08 464.75
 4.75 465.62 465.66
 0.4

TP 6.47 472.16 5.08 465.73
 5.58 466.58 465.66
 all along

469.83

floor level - Bldg. D

6354 B.P. NW

end of line 466.3
 4+28.56 3.5

4+06 466.6
 floor Bldg C 469.4 3.2
 0.4

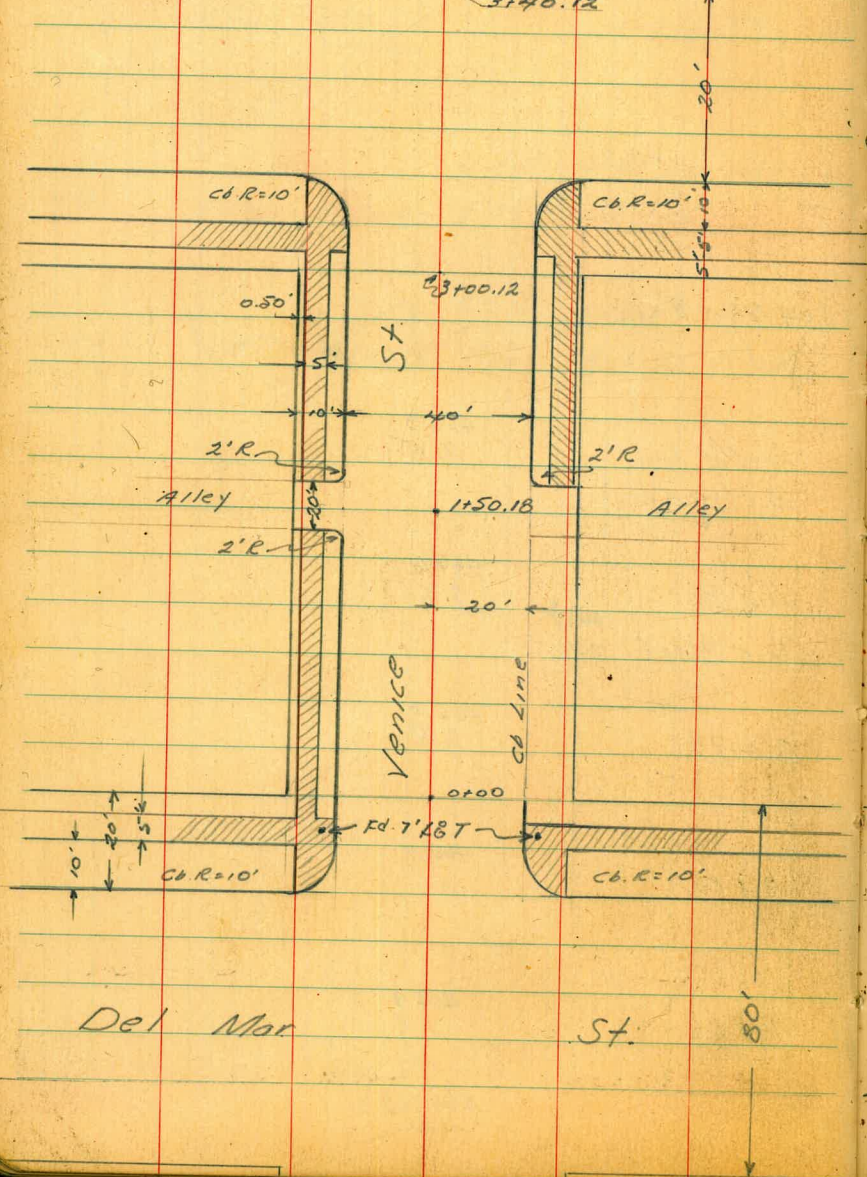
3+73 466.0
 3.8

3+50 465.7
 4.1

3+00 464.9
 4.9

469.83

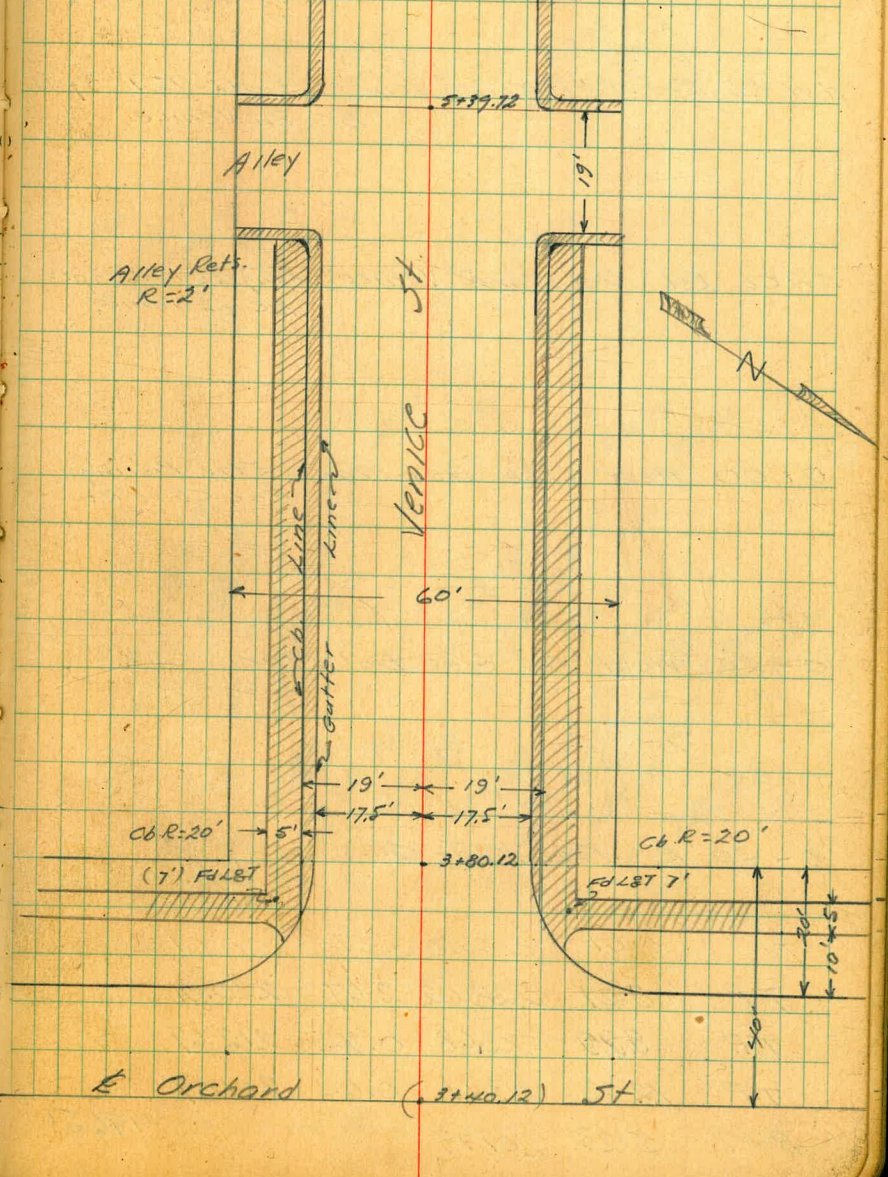
9-17-48 X Sect. Venice St.
 Hendricks Del Mar to Sky Line Block 75
 Roberts Point Loma Hts.
 Rorer
 WO#31629 E Orchard St.



SEP 20 1948

INDEXED

Fd L& Disc. City Engrs.
 6+03.15 BC



SEP 30 1948

INDEXED

0+50

NW Cb Ret. Del Mar & Venice Length = 15.9 3pts.
BC on Venice

SW Cb Ret. Del Mar & Venice Length = 15.6 3pts.
BC on Venice

0+100 West Line Del Mar Edge Paving
End Cb on Rt

0-20 West Cb Line Del Mar

0-40 E Del Mar St.

T.P. 8.01 228.02 2.67 220.01

TP 9.99 222.68 0.72 212.69

TP 12.32 213.41 0.64 201.09

B.M 5.23 201.73 196.50

221.17
 685 220.5
 20 20
 221.82
 22.1
 222.8
 224.0

222.27
 475 222.93
 407 223.32
 470 223.91
 444 223.43
 459 224.00
 402 223.54
 448 224.20

G Cb G Cb G Cb G Cb
 BC. (1) (2) G Cb BC

221.60
 636 221.07
 624 221.78
 669 221.33
 613 221.89
 653 221.49
 577 222.03
 650 221.52

G Cb G Cb G Cb G Cb
 BC. (2) (1) BC

221.98
 604 221.42
 650 222.57
 20 20
 223.12
 223.76
 224.62

G Cb G Cb
 BC

219.17
 218.57
 220.69
 220.23
 221.60
 221.07
 221.61
 222.70
 223.28
 223.54
 224.20
 224.36
 224.94
 226.44
 227.00

885 945 713 779 642 685 641 522 474 448 382 324 308 158 02
 84 84 50 50 30 30 20 20 30 30 50 50 100 100
 Cb G Cb G Cb G Cb G Cb G Cb G Cb G Cb

BC

217.82
 218.57
 220.80
 222.19
 222.89
 223.66
 224.11
 226.72

1020 945 722 583 513 430 321 130
 100 88 50 20 20 50 100

BC

228.02
T

NW BP Catalina & Orchard

1760.18 West Line Alley Beg. Cb on Rt.

219.25	218.7	219.17	218.7	218.4	219.5	220.1	220.5	221.12	221.1	221.25
877	77	885	93	96	85	79	75	690	69	677
30	30	22	22	20	20	22	22	20	30	30
cb	G	cb	G			G	cb.	G	cb	cb

1750.2 E MH

219.72
830
Rim

1740.18 East Line Alley

219.70	219.3	219.50	219.4	218.9	220.0	220.5	221.4
822	87	822	86	91	89	75	66
30	30	22	22	20	19	30	
cb	G	cb	G				

1738.18 B.C. Alley Ret. Lt.

219.49
218.9
853
71
20 20
cb

1700

220.26
219.7
220.9
221.0
222.6
776
83
71
70
54
20 20
17 30
cb

0188 E 14' Conc. Drive Lt.

220.52
219.90
750
812
245 20

22802

22802
*

3+80.12 West Line Orchard

For sections Intersection of Orchard &

TP. 5.95 223.02 10.95 217.07 217.09

2100.12 East Line Orchard

2150

2+11 & 17 Conc Drive LF

2+00

1+62.18 EG Alley Refs.

228.02

216.60	216.33	216.1	217.2	217.81	218.06
6x2	6x9	6x8	5x8	5x21	4x9
19	175	175		175	19
4	E			G	C6

Venice see FB 1870

Rim M.H. Orchard & Venice 223.02

216.53	216.8	217.0	217.4	218.53
11x9	12x2	11x2	10x5	9x9
20	20		20	20
C6				C6

217.43	216.6	218.0	218.3	219.43
10x9	11x4	10x9	9x7	8x9
20	20		20	20
C6				C6

218.21	217.54	217.3
9x1	10x8	10x7
24.5	20	20
	Drive Dirt	

218.37	217.5	218.8	219.3	220.41
9x2	10x5	9x3	8x7	7x1
20	20		20	20
C6				C6

219.12	218.3	220.1	221.03
8x9	9x7	7x9	6x9
20	20	20	20
C6	G	G	C6

228.02

5+39.72 West Gutter Line Alley

5+20.72 East Gutter Line Alley

5+19.22 East Gb Line Alley

5+17.22 B C Alley Retn

5+100

4+50

4+100

223.02

218.87	218.78	219.2	219.29	219.37
415	434	38	372	365
20	21		21	20
G	G		G	G

218.47	218.39	218.86	219.04
455	463	416	398
30	21	21	20
G	G	G	G

218.74	218.70	218.8	219.15	219.28
428	422	42	387	374
30	21		21	20
G	G		G	G

218.67	218.39	218.89	219.14
425	463	413	388
19	17.5	17.5	19
G	G	G	G

218.42	218.16	218.5	218.77	219.04
460	486	45	425	398
19	17.5		17.5	19
G	G		G	G

217.81	217.52	217.3	217.9	218.36	218.63
521	550	57	51	466	439
19	17.5	17.5		17.5	19
G	G			G	G

217.14	216.78	216.6	217.5	217.97	218.22
588	524	54	55	505	480
19	17.5	17.5		17.5	19
G	G			G	G

223.02

595 217.07 217.09

6703.15 B.C.

5743.22 E.C. Alley Ret's. Reg. Asp. Paving

5741.22 West Co. Line Alley

223.02

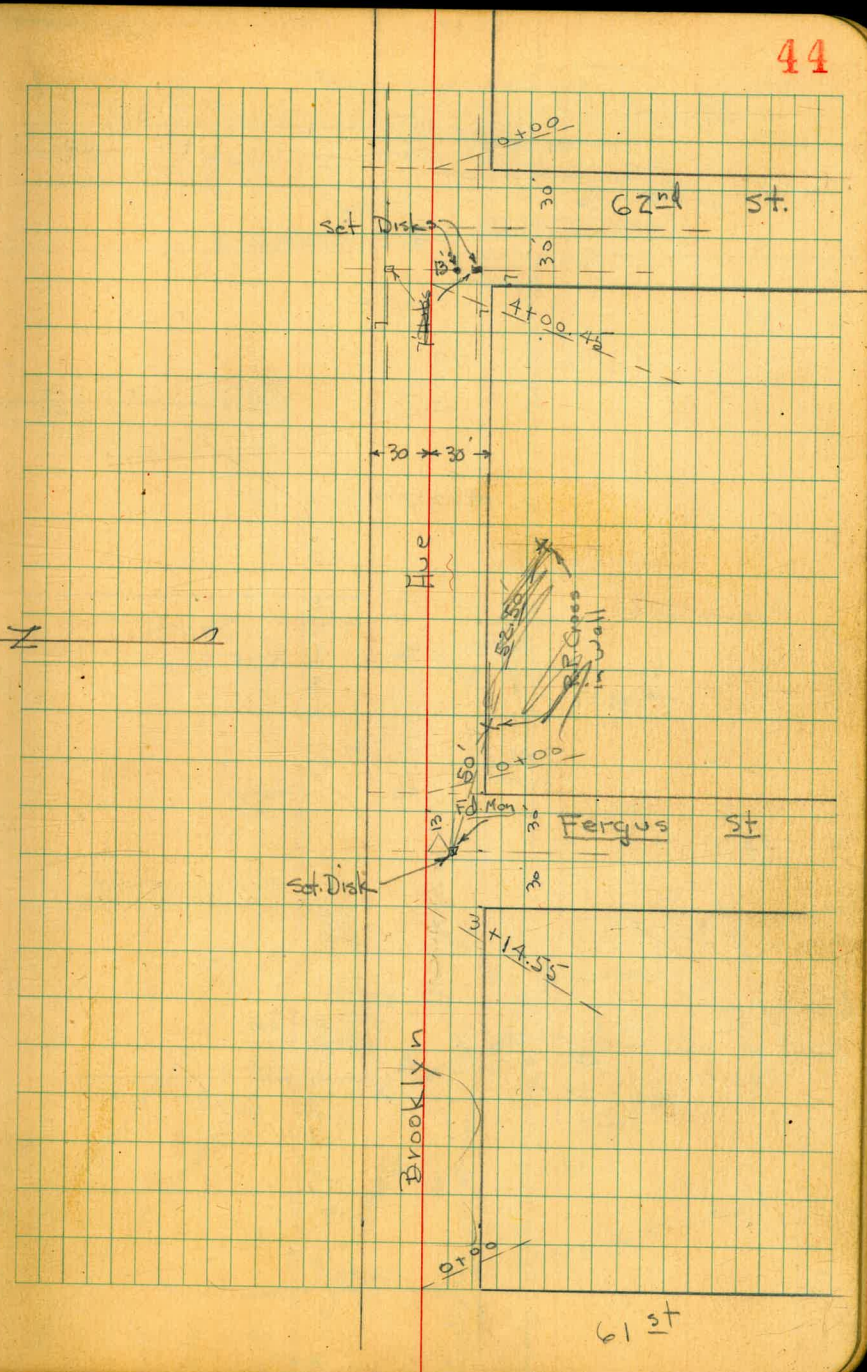
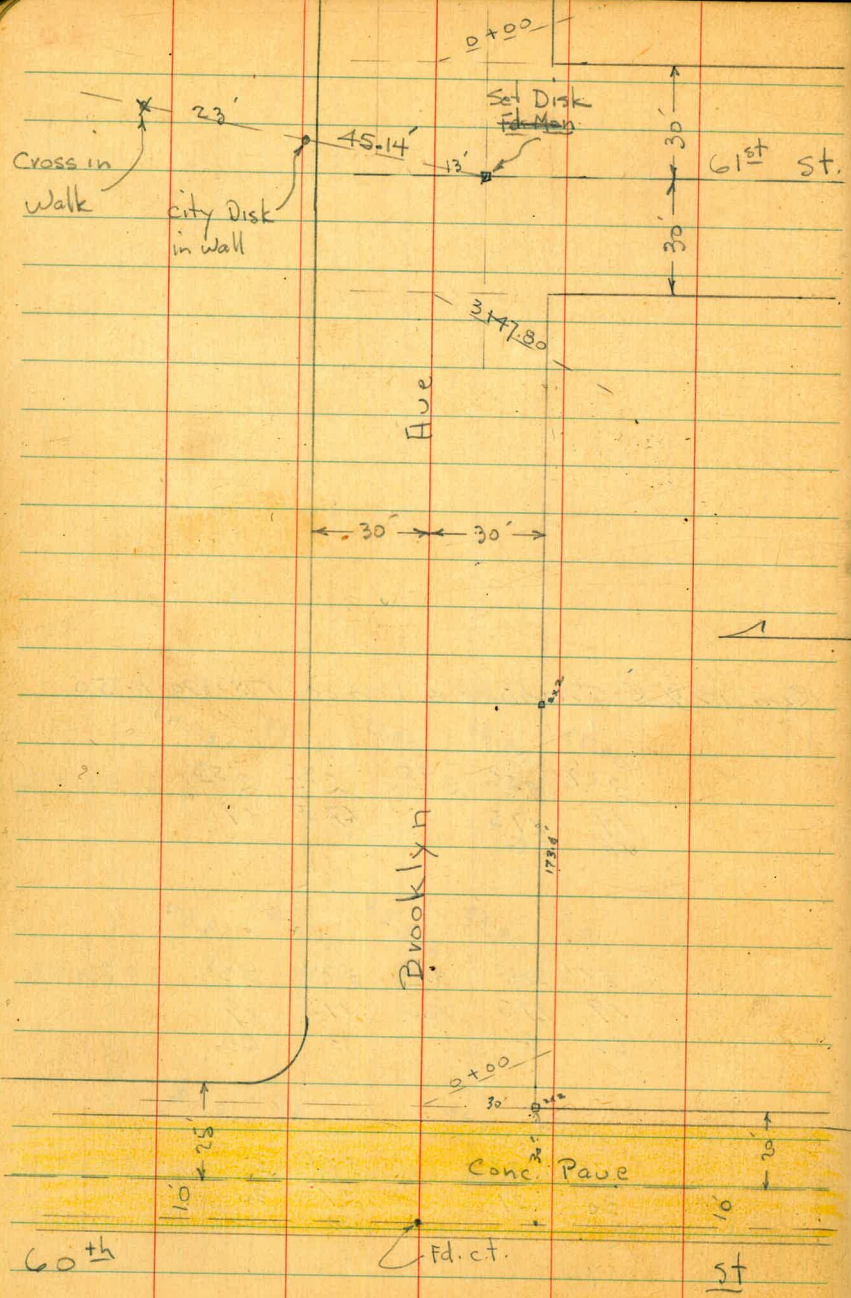
Rim 17H & Orchard & Venice 151870 P-50

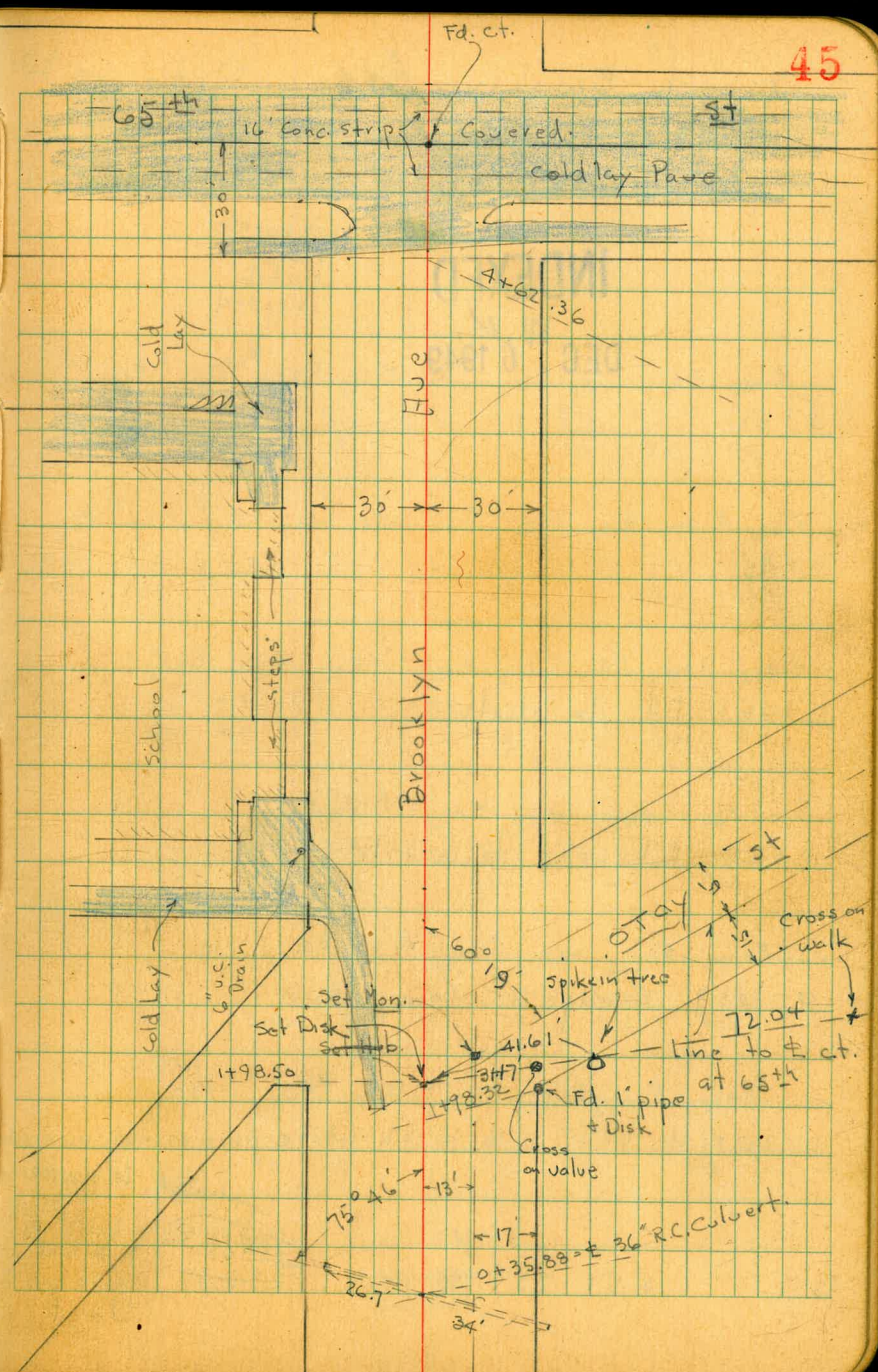
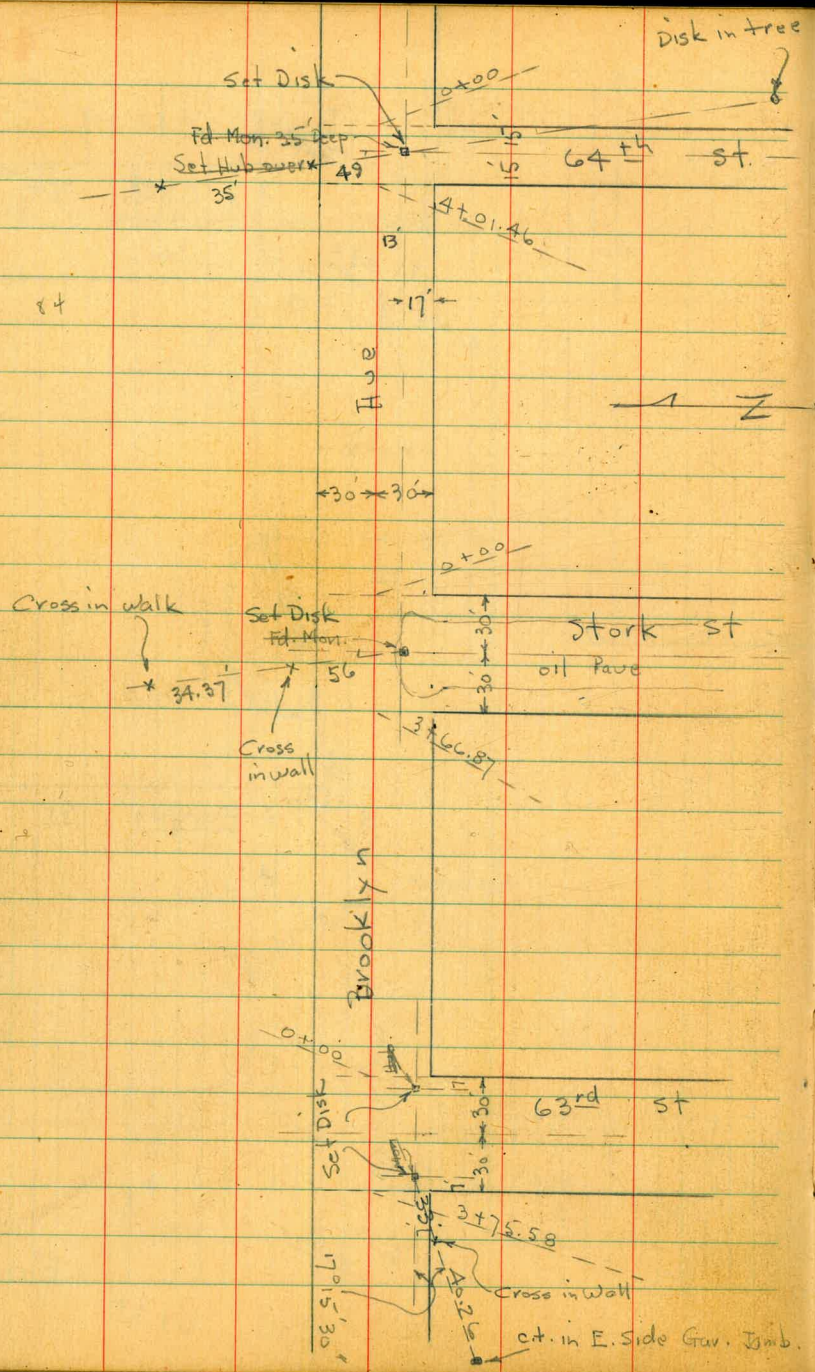
219.73	219.46	220.17	220.20	220.44
329	356	295	282	258
19	175		175	19
Cb	G			

219.08	218.80	219.26	219.28	219.54
394	422	376	374	348
19	175	Par.	175	19
Cb	G		G	Cb.

219.12	219.08	219.56	219.62
390	384	346	340
30	21	21	30
		Cb.	Cb.

223.02





X-Sect. Brooklyn Ave. 60th to 65th

4102

W.O. 31337

11-28-49

Osborne
Hardin
Hatch
Sheperd

INDEXED

W.K.

DEC 6 1949

0+55

0+45

0+55 = E.L. to North

0+00 = E.L. 60th to South

0-03.9 = E. edge of Conc pave

0-20 = ϕ 60th (To South - Note pave is not in center)

Contracted to agree

B.M. 5.51 229.98 ✓

234.53 E Brooklyn
234.47 + w. 10' 60th
Ld + c.t.

Lt.

Rt.

Rt.

46

Note: check B.M.'s at 63rd + Brooklyn
(63rd St. Sections) Before Reducing

233.1	232.8	232.3	231.6	231.8	231.1	231.7	232.1	232.3
6.9	7.2	7.7	8.4	8.2	8.9	8.3	7.9	7.7
40	30	13	11		18	20	30	40

235.4	235.0	234.7	233.0	232.1	232.2	231.4	232.0	232.8	232.7
4.6	5.0	5.3	7.0	7.9	7.8	8.6	8.0	7.2	7.3
40	30	24	17	11		19	20	30	40

236.5	235.6	234.7	234.1	233.6	233.1	234.1	233.7
3.5	4.4	5.3	5.9	6.4	6.9	5.9	6.3
40	30	15		15	25	30	40

235.8	234.9	234.4	233.8	233.2	233.1
4.2	5.1	5.6	6.2	6.8	6.9
30	15		15	30	40

240.06	235.85	235.13	234.57	233.94	233.38	231.43
+0.02	4.19	4.91	5.47	6.10	6.66	8.61
80	30	15		15	30	80

240.12	235.94	235.27	234.73	234.13	233.57	231.71
+0.08	4.10	4.77	5.31	5.91	6.47	8.33
80	30	15		15	30	80

with
B.M.

@ 63rd + Brooklyn

240.04

239.98

Brooklyn.

1' E. - 21.9 Rt. = ± P. pole # J.P. 171035
3+47.80 = w.L. 61st St. = along wly. of Dirt Dr.

2+00

2+55 - 30.3 Lt. = ± 6.6 Drive - 2-2' conc. strips

2+50

T.P. 11.69 242.87 8.80 231.18

2+00

1+95 - 21.4 Rt. = ± P. pole # ? 171034

1+62 = 11.6 Lt. = ± of 10' A.C. Drive

1+40

1+00

0+75 - 21.6 Rt. = ± P. pole # J.P. 79725

Lt.

±

Rt.

47

237.9	236.3	234.5	234.2	233.5	232.9	229.7
5.0	6.6	8.4	8.7	9.4	10.0	13.2
50	30	15		15	30	80
Dr.						
233.9	233.0	231.6	231.5	230.9	230.5	229.9
9.0	9.9	11.3	11.4	12.0	12.4	13.0
40	30	15		15	30	40
231.71		231.29				
11.22		11.64				
50		30.3				
Dr.		Dr.				
231.4	230.5	229.9	229.7	229.1	228.0	227.2
11.5	12.4	13.0	13.2	13.8	14.9	15.7
40	30	15		15	30	40
			93			
			242.87			
231.1	229.6	229.3	229.0	228.4	226.9	226.0
8.9	10.4	10.7	11.0	11.6	13.1	14.0
40	30	15		15	30	40
231.14	230.3	229.17	228.7	228.2	227.0	226.6
8.90	9.73	10.87	11.3	11.8	13.0	13.4
50	30	11.6		15	30	40
Dr.	Dr.	Dr.				
229.7	229.6	229.1	229.0	228.5	227.2	226.9
10.3	10.4	10.9	11.0	11.5	12.8	13.1
40	30	15		15	30	40
230.4	230.1	229.9	229.8	229.2	229.2	229.4
9.6	9.9	10.1	10.2	10.8	10.8	10.6
40	30	15		15	30	40

240.04

239.98

1+65-30' Lt. = Beg. Picket fence
 1+50 = wly. of Dirt Dr. on Lt.

1+25

1+06-22.7 Rt. = \pm P. pole # J.P. 171044
 1+00

0+75

0+63-22.9 Lt. = E P. pole # 277618
 0+50

0+09-30.7' Lt. = end wall

60' E. = E.L. 61st = 0+00 ahead.

30' E. = \pm 61st to S. - Dirt Graded.

25' E. = 32' Lt. = Beg 10" Conc wall

244.0	242.9	241.7	240.8	240.5	239.8	238.8	238.1
+1.1	0.0	1.2	2.1	2.4	3.1	4.1	4.8
40	30	19	13		15	30	40
	Dr	Dr					
244.2	242.9	242.2	241.1	240.9	240.2	240.3	239.6
+1.3	0.0	0.7	1.8	2.0	2.7	2.6	3.3
40	30	19	12		15	30	40
243.2	242.3	242.0	241.2	240.9	240.4	240.3	239.8
+0.3	0.6	0.9	1.7	2.0	2.5	2.6	3.1
40	30	20	14		15	30	40
242.8	242.2	241.5	240.7	240.4	239.9	240.6	239.5
0.1	0.7	1.4	2.2	2.5	3.0	2.3	3.4
40	30	20	15		15	30	40
242.1	241.6	240.7	239.6	239.5	238.8	239.1	238.5
0.8	1.3	2.2	3.3	3.4	4.1	3.8	4.4
40	30	18	15		15	30	40
242.27	239.9						
0.66	3.0						
30.7	30.7 = ground						
Top wall							
239.6	239.6	238.9	237.4	237.3	236.4	236.1	232.5
3.3	3.3	4.0	5.5	5.6	6.5	6.8	10.4
31.1	30	23	15		15	30	80
along wall							
238.9	238.6	237.5	236.1	235.7	234.9	233.8	230.4
4.0	4.3	5.4	6.8	7.2	8.0	9.1	12.5
31.8	30	22	15		15	30	80
along wall							
0.69	4.2						
32	32						
Top wall	ground						
		242.87					

T.P. 10.60 258.13 2.10 247.53⁴
 walk on diag. to house
 also- 29.8' Rt. = Beg. Nly. of Conc. wall + Cor. of Conc.
 60' E. = E.L. Fergus = 0+00 ahead. = wly of 2.5' Conc
 walk on Lt.

30' E. = Φ - 21.5' Lt. = Φ 18" Pepper

3+14.55 = wly. Fergus to S. - Rough Graded

3+14.5 = 23.4' Rt. = Φ P. pole J.P. 171046

3+04 = 20.7' Lt. = Φ 14" Pepper

2+70

2+64 = 21.8' Lt. = Φ 12" Pepper

2+49 = 29.7' Lt. = Φ 4.5' Conc walk

2+43 = 20.6' Lt. = Φ 14" Pepper

2+35.

2+11 = 22.6' Rt. = Φ P. pole # J.P. 171045

T.P. 9.59 249.62 2.83 240.04 # JP 171045
 40.10 - Nail in Pole

2+00 = wly. of dirt Dr on Lt.

1+96 = 30.2' Lt. = end fence

1+78 = 30.3' Lt. = Φ 3' Conc. walk

Lt. Φ Rt.

49

250.45	249.74	249.1	247.0	246.6	246.0	245.4	245.74	245.25	242.2
+0.76	+0.05	0.6	2.7	3.1	3.7	4.3	3.95	4.44	7.5
40	30.3	30	10		15	29.8	29.8	30.4	80
wly. of walk	walk					ground	Top wall	Cor. NE Walk Cor.	
250.7	248.1	247.2	245.0	245.1	244.9	244.3	244.4	241.4	
+1.0	1.6	2.5	4.7	4.6	4.8	5.4	8.3	8.3	
40	30	27	11		15	30	80		
248.3	246.0	244.1	243.6	243.6	243.2	243.1	240.6		
1.4	3.7	5.6	6.1	6.1	6.5	6.3	9.1		
40	30	14	11		15	30	80		
244.5	243.3	242.5	241.8	241.9	241.2	240.1	239.3		
5.2	6.4	7.2	7.9	7.8	8.5	9.6	10.4		
40	30	15	12		15	30	40		
245.62		244.11							
4.07		5.58							
50.8 at Porch		29.7 = walk							
244.0	242.6	241.7	241.3	241.0	240.3	239.3	238.4		
5.7	7.1	8.0	8.4	8.7	9.4	10.4	11.3		
40	30	16	13		15	30	40		
					249.69				
					249.65				
242.2	241.9	241.3	240.7	240.3	239.6	238.7	238.1		
0.7	1.0	1.6	2.2	2.6	3.3	4.2	4.8		
40	30	20	13		15	30	40		
244.23		242.88							
+1.30		0.05							
53 at Porch		30.3 walk							
					242.89				

Brooklyn

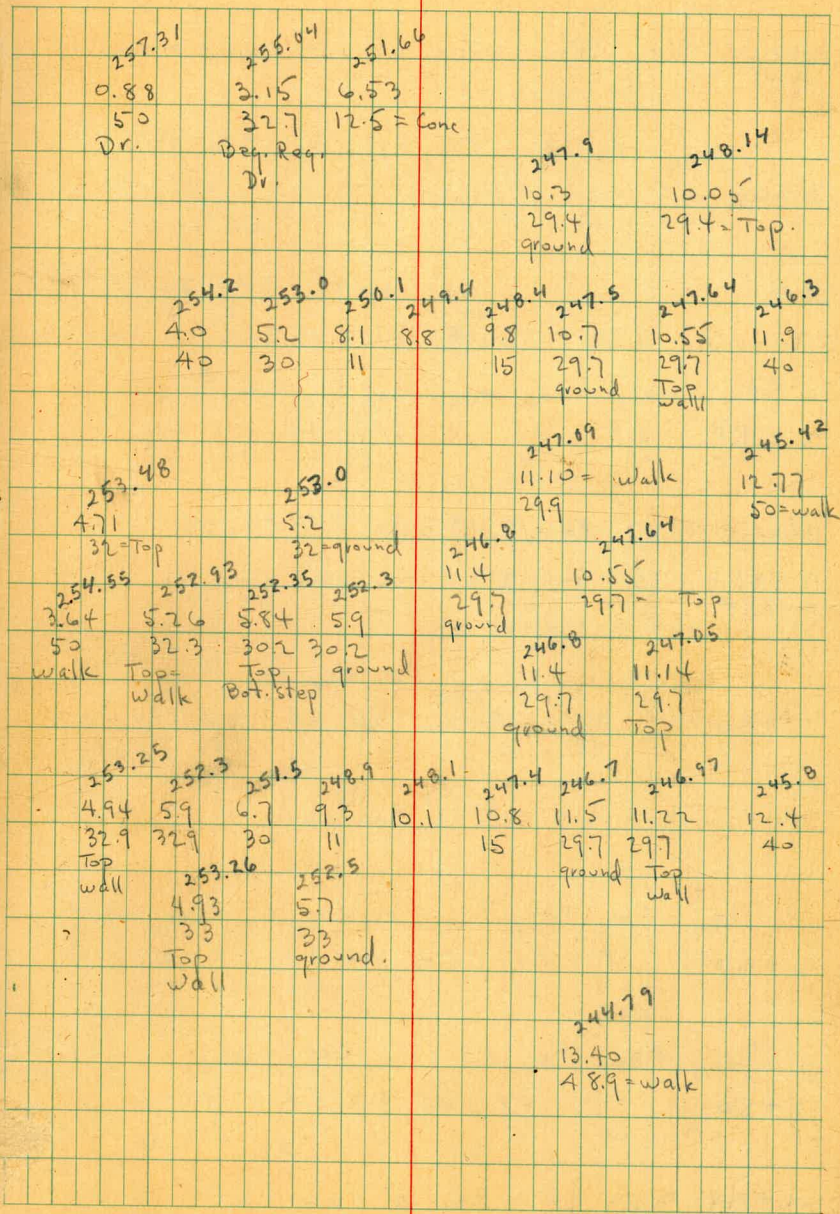
- 1+42- 12.5 Lt. = sly. # of Rough Conc. Slab to
13' Conc. Dr. to Sing Gar. Conc. floor
- 1+33 - 22.6 Rt. = # P. pole # P 77157
29.4 Rt. = end wall
- 1+00
- 0+90- 29.9 Rt. = # 3' Conc. walk thru wall
- 0+88 - 32' Lt = end Conc. wall
- 0+77 - 29.7 Rt. = Beg. 6" Conc. wall
- 0+72 - 30.2 Lt. = # 3' Conc. Steps + walk thru wall
- 0+67 - 29.7' Rt. = end wall
- 0+57 - 23.2 Rt. = # 6" Acacia
- 0+50
- 0+37 - 33' Lt. = Beg. 6" Conc. wall
- 0+49 - 23' Rt. = # P. pole # J.P. 171054
- 0+34 - 23.5' Rt. = # 4" Acacia
- 0+19 - 48.9 Rt. = N.Ely. Edge of walk (shows angle)
- 0+13 - 26.4 Lt. = # 30" Pepper
- 0+12 - 23.8 Rt. = # 6" Acacia
- 0+07 - 23.6 Rt. = # F.H.

Lt.

#

Rt.

50



258.19

Brooklyn

3+16- 50' Rt. = Wly. of Conc porch + House

3+00

B.M. 10.85 244.56 spike in
T.P. 9.59 255.41 12.31 245.82 Nail in SW Pole - 62nd

2+75-

2+65-22.7' Rt = \pm P. pole # P 77188

2+50- 30' Rt. = \pm 3' Conc walk

2+40- Wly. of 9' Conc Dr. on Lt

2+36- 30' Lt. = end (8') Conc. wall

2+00

1+50

256.6
1.6
40

1+48-30.3' Lt. = Beg. 4" Conc. wall

Lt

\pm

Rt

51

247.1 247.72
8.4 7.75
50 ground 50 = Porch

254.8 254.4 253.1 251.7 251.3 250.2 248.9 248.2
0.7 1.1 2.4 3.8 4.2 5.3 6.6 7.3
40 30 20 11 15 30 40

255.47
255.41

256.7 255.6 254.1 252.2 251.9 250.7 249.4 248.3
1.5 2.6 4.1 6.0 6.3 7.5 8.8 9.9
40 30 20 12 15 30 40

249.56 248.30 248.57
8.63 9.89 9.62
30 walk 41.9 at porch 45.5 = House

257.74 255.91 255.19 254.6 252.7 252.2 251.1 249.4 248.4
0.45 2.28 3.00 3.6 5.5 6.0 7.1 8.8 9.8
40 Dr. 30 Dr. 20 Cor. Dr. 15 30 40

257.44 256.2
0.75 2.0
30 Top wall 30-gr.

257.6 257.15 255.9 254.6 252.8 252.0 250.9 249.1 248.1
0.6 1.4 2.3 3.6 5.4 6.2 7.3 9.1 10.1
40 29.9 29.9 20 12 15 30 40

Top wall

255.84 254.8 253.5 251.6 250.8 249.7 248.3 247.7
2.35 3.4 4.7 6.6 7.4 8.5 9.9 10.5
30.3 Top wall 30 20 11 15 30 40
255.82 254.9 30.3
2.37 3.3
30.3 Top ground 19
258.12

30' Lt. = Φ Natural drainage to N.
 60' E. = E.L. 62nd = 0+00 ahead.

45' F

30' E = Φ

15' F

S E - 22.7 Rt. = Φ P. pole # J.P. 178811

T.P. 4.67 250.49 9.59 245.82

4+00.45 = w.L. 62nd to S. - Rough Graded

3+75

3+50

3+40 18.2 Lt. = Φ 8' Conc. Dr

3+25

52

244.2 6.4 50 Φ Drain	Lt 30 Φ Drain	243.4 7.2	243.4 7.1	243.8 6.7	Φ 7.2	243.4 7.0	241.6 10.6	240.0 Rt 30	235.0 14.7 80
245.0 5.6 40	244.4 6.2 30	243.6 7.0 15	243.2 7.4	241.6 8.9 18	240.6 9.9 30	238.6 12.0 40			
246.4 4.2 40	246.3 4.3 30	245.7 4.9 20	244.0 6.6 11	243.6 6.9	243.0 7.6 10	241.4 9.2 20	239.6 10.9 30	235.6 15.0 80	
248.2 2.4 40	247.8 2.8 30	246.8 3.7 20	244.6 5.9 11	244.4 6.2	243.6 7.0 10	242.4 8.1 17	242.6 7.9 30	242.0 8.6 40	
				250.49 55					
249.0 6.5 40	248.4 7.1 30	247.6 7.9 20	245.7 9.8 11	245.3 10.2	244.3 11.2 16	244.9 10.6 23	244.0 11.5 30	240.3 15.2 80	
252.4 2.1 40	252.1 3.4 30	251.4 4.1 21	247.7 7.8 11	247.2 8.3	246.4 9.1 15	246.4 9.1 30	246.0 9.5 40		
252.9 2.6 40	252.4 3.1 30	251.7 3.8 19	249.5 6.0 11	249.0 6.5	248.1 7.4 15	247.5 8.0 30	246.8 8.7 40		
253.98 1.49 50 Dr.	252.35 2.12 30 Dr.	251.29 4.18 18.2 = Dr.							
253.9 1.6 40	253.1 2.4 30	252.3 3.2 19	250.9 4.6 11	250.4 5.1	249.3 6.2 15	248.0 7.5 30	247.3 8.2 40		
				255.44					

Brooklyn

3+50

3+30

3+29- 26.7 Lt. = sly. of 12" stone wall

3+24- 33.2 Rt. = Beg. Wly. of 6" cb. along Conc. Dr.

3+13- 33' Rt. = Fly Conc. apron

3+07- 11' Lt. = \pm oil Drive.

T.P. 6.14 278.36 1.79 272.22

3+00

2+94- 33.4 Rt. = Wly. of Conc. apron to Doub. Gar. ^{Conc. floor}

2+83 - 29.6 Rt. = end wall

2+80

2+70 - 24.4' Rt. = \pm P. pole # J.P. 113851

2+61- 27.4 Rt. = \pm 4.5' ^{+step} Conc. walk thru wall

2+40

278.1 0.3 40	277.7 0.7 30	277.0 Lt. 1.4 20	274.7 3.7 15	274.1 \pm 4.3 11	273.4 5.0 50	272.3 6.1 15	270.7 Rt. 7.7 20	270.23 8.19 30	269.70 8.72 30	54 9.25 41.2 Dr.
277.6 0.8 40	277.2 1.2 30	277.0 1.4 28	275.1 3.3 26	273.1 5.3 20	271.8 6.6 12	271.5 6.9 15	270.8 7.6 15	269.4 9.0 30	268.94 9.48 33	
278.08 0.34 44.8 Top-by House		277.30 0.92 26.7 Top	275.1 3.3 26.7 ground		268.4 10.0 33.2 ground	265.76 12.66 33 Conc.	268.43 9.99 33.2 Top cb.	267.76 10.66 33.7 Conc. Dr.	267.67 10.75 41.7	
275.0 3.4 40 Dr.	273.5 4.9 30 Dr.	270.4 8.0 18 Dr.	269.3 9.1 11 Dr.	278.36				12.62 44.9 = floor		
274.1 +0.7 40	273.9 0.2 30	270.0 4.1 18	268.5 5.6 9	268.4 5.7	267.8 6.3 15	265.7 8.4 30	265.65 8.42 33.3 = Apron			
					265.58 8.49 33.4 Conc.	264.69 9.38 45.2 = floor Gar.	264.6 9.5 29.6 ground	265.01 9.06 29.6 Top-wall		
269.3 4.8 40	268.1 6.0 30	267.2 6.9 20	266.3 7.8 11	266.3 7.8	265.7 8.4 15	264.5 9.6 29.5 Top wall	264.90 9.17 29.5 Top wall	262.3 11.8 40 = Level		
				262.94 11.13 27.4 Top	261.9 12.2 15	261.9 12.7 29.2 Top wall	261.59 12.48 30.9 Beg. walk	261.17 12.90 44.6 - at House		
265.5 8.6 40	264.9 9.2 30	264.1 10.0 19	262.4 11.7 11	262.4 11.7	261.9 12.2	261.9 12.7 29.2 Top wall	263.22 10.85 29.2 Top wall	260.6 13.5 40 Level		

Brooklyn

0+58-25 Rt. = \pm P. pole # J.P. 171066

0+50

0+36-20.1' Lt. = \pm P. pole # 77803

60' E. = E.L. Stork = 0+00 ahead

30' E. = \pm

13' E. - 20.5' Lt. = \pm Gray Pole

9' E. - 28.4' Lt. = \pm 2' Conc. walk

J.P. 171065 67.12
Set B.M. - Spike in S.W. Pole 5.92 267.06

3+66.87 = W.L. Stork St. to S. Rough Graded.

3+64-21' Lt. = \pm 30" Palm

3+64-25.1 Rt. = \pm P. pole # J.P. 171065

3+35

3+14-21.3 Lt. = \pm 42" Palm

3+00-29.7 Lt. = end wall

2+50

2+48-29.9 Lt. = \pm 4' Conc. walk - Thru wall

Lt.

\pm

Rt.

56

269.9	269.0	268.4	267.4	267.0	266.3	265.1	264.1
3.1	4.0	4.6	5.6	6.0	6.7	7.9	8.9
40	30	19	15	15	15	30	40

270.8	269.8	269.0	267.8	267.4	266.7	265.6	261.7
2.2	3.2	4.0	5.2	5.6	6.3	7.4	11.3
40	30	20	16	15	30	30	80

270.6	270.0	269.3	268.2	267.8	267.0	266.0	262.1
2.4	3.0	3.7	4.8	5.2	6.0	7.0	10.9
40	30	22	16	15	30	30	80

oil Pavc

270.85	270.21
2.19	2.83
40	28.4 = walk

271.0	270.0	269.3	267.9	267.9	266.7	266.0	262.1
2.0	3.0	3.7	5.1	5.1	6.3	7.0	10.9
40	30	20	16	15	30	30	80

270.7	269.8	269.1	267.8	267.8	266.9	266.0	265.6
2.3	3.2	3.9	5.2	5.2	6.1	7.0	7.4
40	30	20	15	15	30	30	40

270.3	272.12	269.7	269.0	267.9	267.7	266.7	265.7	266.1
2.7	0.92	3.3	4.0	5.1	5.3	6.3	7.3	7.9
40	29.7	29.7	22	16	14	30	30	40

Top wall

270.6	272.57	269.8	269.0	267.8	267.3	266.8	264.9	264.2
2.4	0.47	3.2	4.0	5.2	5.7	6.2	8.1	8.8
40	29.9	29.9	23	15	13	13	30	40

Top wall

270.64	270.13
2.40	2.91
40	29.9

walk

273.04
~~272.98~~

Brooklyn

T.P. 13.09 256.⁸⁴/₈₅ 109 243.⁷⁵/₇₆

0+77- 24.3' Rt. = \pm P. pole \neq J.P. 171 040
0+75

0+55

0+35.88 = \pm + \pm of 36" RC. Culvert under fill
see sketch - P. 45 for angle - Note: inlet is covered
by fill over top of pipe

0+30

0+18 Cont.

0+18- 16' Rt. = inlet of $\frac{1}{2}$ -18" Corr. Iron Culvert. (open)

30 E. = E.L. 64⁺¹ = 0+00 ahead

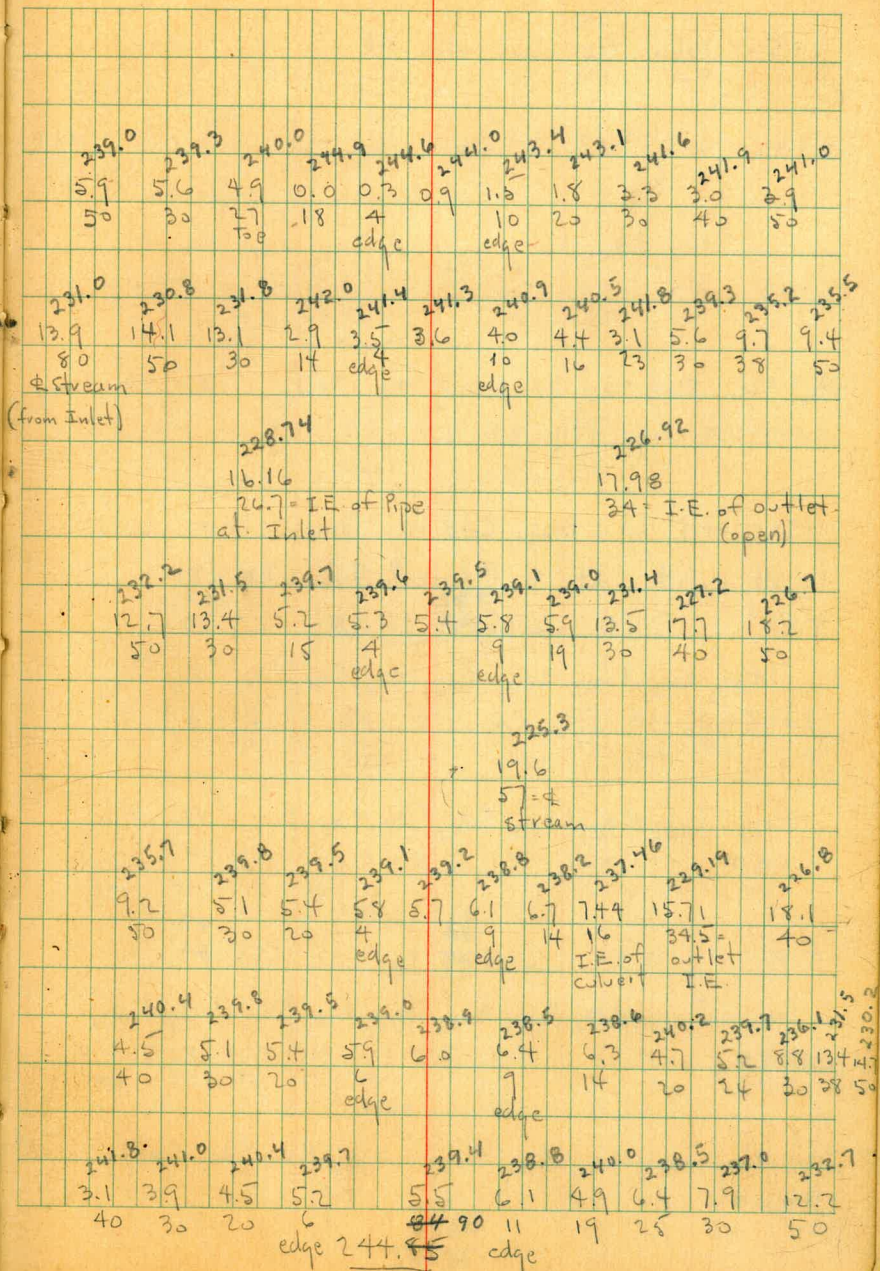
15 E. = \pm 64⁺⁵ - Not Graded.

Lt

C

Rt

59



Brooklyn

2+56 = opp Prop. Cor. on Rt.

2+42 = Wly of 8' L. walk on Lt

2+25

2+15 = end oil pave strip

1+98.32 = opp. Prop cor.

1+92 = 11.7' Lt. = Beg. Cold lay Drain from school

1+84 = 24' Rt. = P. pole # J.P. 278 681

T.P. 7.50 275.33 0.90 267.83

1+75

1+50

T.P. 12.84 268.75 0.96 255.89

1+25

1+00

60

	Lt.				±	Rt.			
	270.78	270.09	269.13	269.72	270.3	270.2	270.0	269.3	268.4
	4.6	5.79	6.25	5.66	5.1	5.2	5.4	6.1	7.0
	45	33.5	29.2	25.5	15	15	15	30	50
	27.15	27.15	27.15	27.15	27.15	27.15	27.15	27.15	27.15
	4.23	5.21	5.56	6.45	5.90				
	50	30	26.6	22.5	19.3				
	walk	walk	walk + walk	edge	edge Drain				
				IE					
	271.1	270.8	270.6	269.72	268.43	269.02	269.1	269.2	269.3
	4.3	4.6	4.8	6.06	6.95	6.36	6.3	6.2	6.1
	40	30	25	20.3	16.6	13.3		15	30
				edge	±	edge Drain			
	270.1	270.2	269.8	266.76	267.0	267.1	269.9	269.9	267.3
	7.3	5.2	5.6	8.62	8.4	8.3	8.5	8.5	8.1
	40	30	20	12.5	10	10	10	17	20
				± Drain edge	edge	edge			30
				265.88	± Drain edge				267.4
				9.50					267.2
				11.7					
				IE of		38			
				Drain		32			
						275.33			
	268.3	267.9	267.3	263.2	263.5	263.7	263.5	262.9	264.2
	0.5	0.9	1.5	5.6	5.3	5.1	5.3	5.9	4.6
	40	30	16	15	edge		10	15	21
					edge		edge		30
	262.8	263.2	262.9	258.6	259.2	259.3	259.1	258.8	261.6
	6.0	5.6	5.9	10.2	9.6	9.5	9.7	10.0	7.2
	40	30	16	15	5	5	9	15	30
					edge		edge		40
						78			
						72			
						268.73			
	256.9	257.1	257.8	253.5	254.2	254.4	254.0	253.5	256.7
	0.0	0.2	0.9	3.4	2.7	2.5	2.9	3.4	0.2
	40	30	16	15	4	4	9	15	30
					edge		edge		40
	248.9	249.6	248.6	244.1	244.1	248.7	247.9	250.9	250.8
	8.0	7.3	8.3	7.4	7.8	8.2	9.0	6.0	6.1
	40	30	15	4	8	9	17	27	30
				edge		edge			40
						256.85			

3+82 - 33.3 Lt. = S.E. ly. Cor. of C.L.

3+62 - 33.3' Lt. = Sly. of C.L.

3+52 - 37.1 Lt. = Beg. C.L. Slab at Root Cor. of Steps

3+20 - 22' Rt. = E P. pole # P - 77386

3+04 - 30.3 Rt. = 3' Conc walk

2+80

2+74 - 30.5 Lt. = S.E. ly. Cor. of C.L.

2+63 - show C.L. on Lt.

2+60 - 21.8' Lt. = outlet 6" U.C. Drain from school
= Beginning of Dip. C.L. Drain to W.

Lt.

Rt.

61

	271.75	271.27							
	3.63	4.11							
	50	33.3 - Cor. C.L.							
	E. edge C.L.								
	271.53	271.44	271.5	271.5	271.5	270.4	269.8	269.4	
	3.85	3.94	3.9	3.9	3.9	5.0	5.6	6.0	
	48.5	33.3	30	15	39	15	30	40	
	at Cor. of School								
	271.55	271.53							
	3.83	3.85							
	45.2	271 = C.L. + steps							
	C.L. along Bldg								
	272.0	271.6	271.5	271.4	270.5	270.2	269.2		
	3.4	3.8	3.9	4.0	4.9	5.2	6.2		
	45.2	30	15	40	15	30	40		
	along Bldg								
						269.96	269.37		
						5.42	6.01		
						30.3 walk	40.8 at Porch		
	270.9	270.8	270.8	270.8	270.1	269.8	269.1		
	4.5	4.6	4.6	4.6	5.3	5.6	6.3		
	37.1	30	15	46	15	30	40		
	along steps								
	270.39	270.37	270.57						
	4.99	5.01	4.81						
	45	37.2	30.5 = C.L.						
	C.L. at Bldg	C.L. at Bot. of Cor. Steps							
	270.51	270.06	269.94						
	4.87	5.32	5.44						
	45	33	29 = sly. of C.L.						
	W. of C.L.								
	C.L.								
		269.04							
		6.34							
		38							
		31.8							
		I.E. of 275.28							
		6" Drain							

check F.H. - 63rd 270.20
14
 11.20 273.⁰⁷₈₈ 10.90 271.¹⁴₈₇ .21
 T.P. 2.63 272.⁷⁷₇₈ 2.01 270.¹⁴₁₅

20' E. = ± 65th = end.

22' E. = approx edge of covered Conc. Strip.

14.5' E. = Gutter = ave. edge of C.L. Pavc

8' E.

T.P. 21
15
 2.01 272.¹⁵₁₆ 5.18 270.20
14
15 F.H. - NE
 65th + Brooklyn

4+62.36 = W.L. of 65th

4+60 - 212' Rt. = ± P. pole # P-70879

4+49 - 26.4 Lt. = ± 6" Pepper

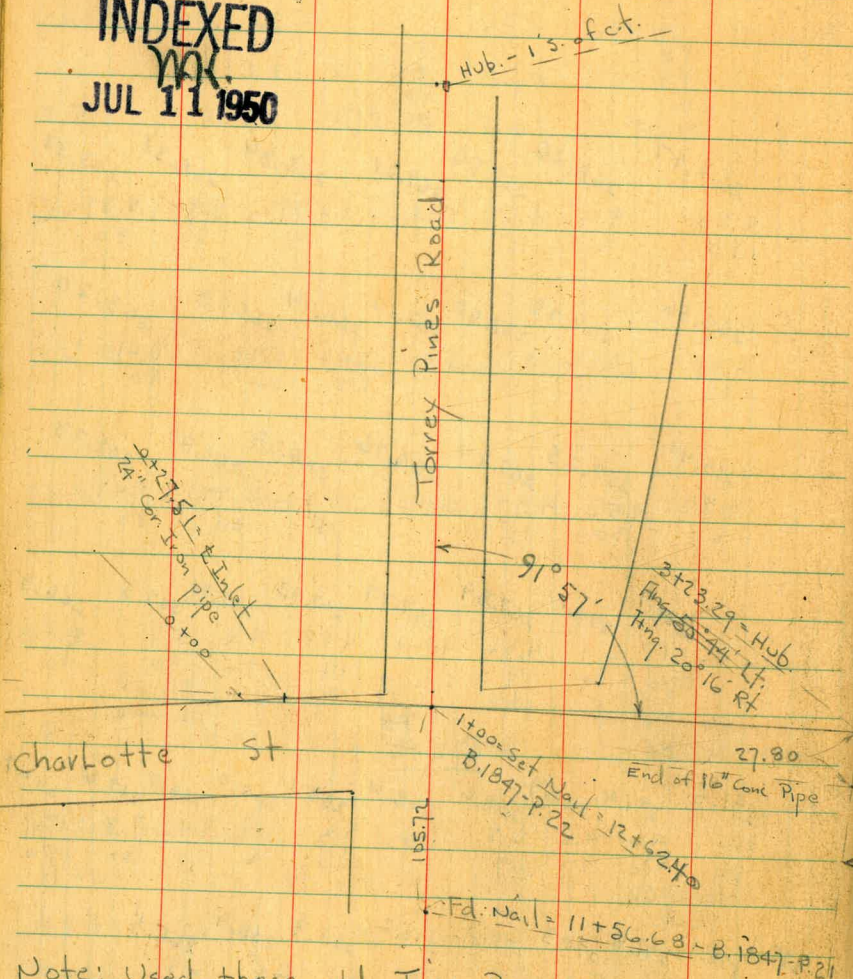
4+35

4+22 - 26.4 Lt. = ± 14" Pepper

4+00 = ± Dirt Dr.

269.97	268.06	267.59	267.21	266.84	266.31	263.32
2.24	4.15	4.62	5.00	5.37	5.90	9.89
80	30	15		15	30	80
269.86	267.95	267.50	267.10	266.74	266.28	263.20
2.35	4.26	4.71	5.11	5.47	5.93	9.01
80	30	15		15	30	80
269.41	267.65	267.24	266.76	266.38	265.80	262.73
2.80	4.56	4.97	5.45	5.83	6.41	9.48
80	30	15		15	30	80
271.1	270.1	267.89	267.77	267.33	267.8	267.5
1.1	2.1	4.32	4.44	4.88	4.4	4.7
30	30	19	C.L.	14	20	30
		edge	21	edge		Ely of
			15			C.L. walk
			272.16			
271.8	271.4	270.9	268.6	268.4	268.1	268.0
3.6	4.0	4.5	6.8	7.0	7.3	7.4
50	30	27	17	15	16	20
edge of C.L.						
walk						
272.1	272.1	271.8	270.3	270.3	270.2	269.3
3.3	3.3	3.6	5.1	5.1	5.2	6.1
40	30	26	19	10		15
						30
						40
273.4	272.5	271.2	271.3	271.3	270.4	269.5
2.0	2.9	4.2	4.1	4.1	5.0	5.9
40	30	21	15	30	15	30
						40
						in Dirt Dr.
				275.33		

INDEXED
 MK
 JUL 11 1950

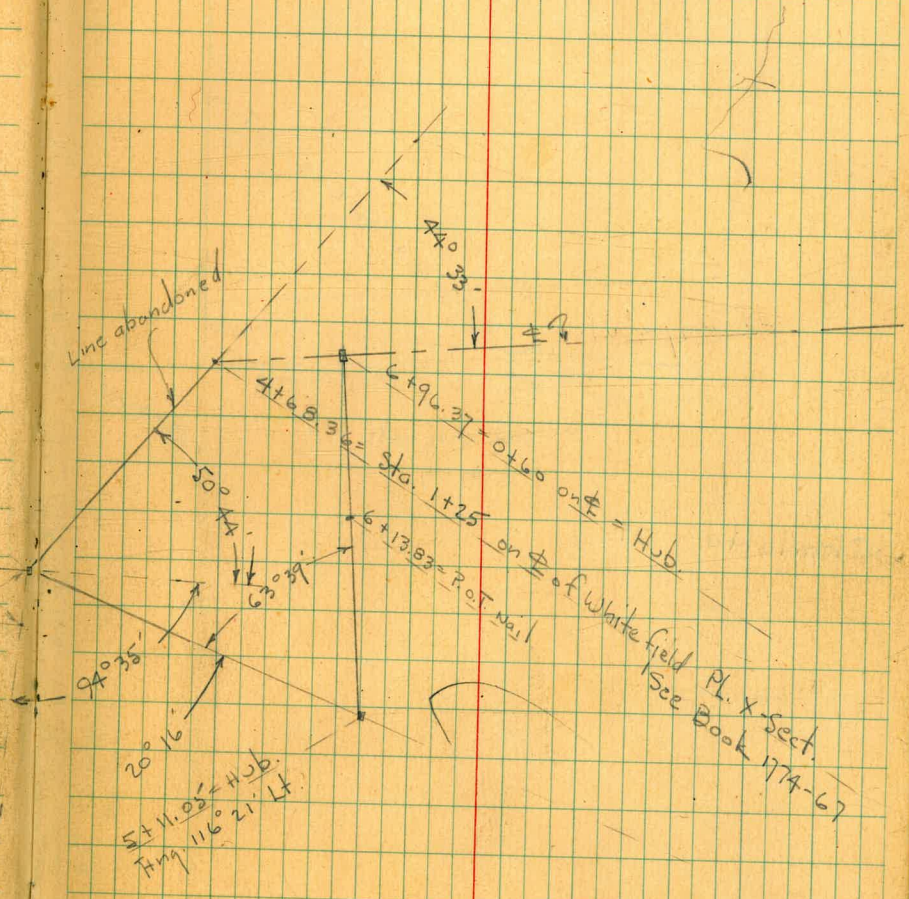


Note: Used these old Ties Because
 Mons. are Covered up. - Prop. Ties on P. 22
 are good.

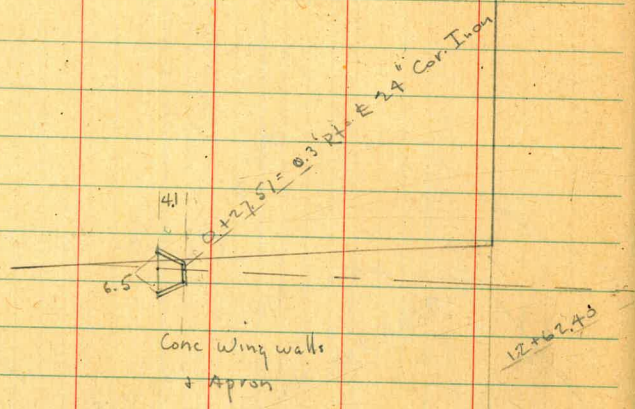
Survey for Prop. Drain - Charlotte + Torrey Pines Rd. 63

4433
 W.O. 20464

7-5-50 - Osborne
 Hardin
 Shepard



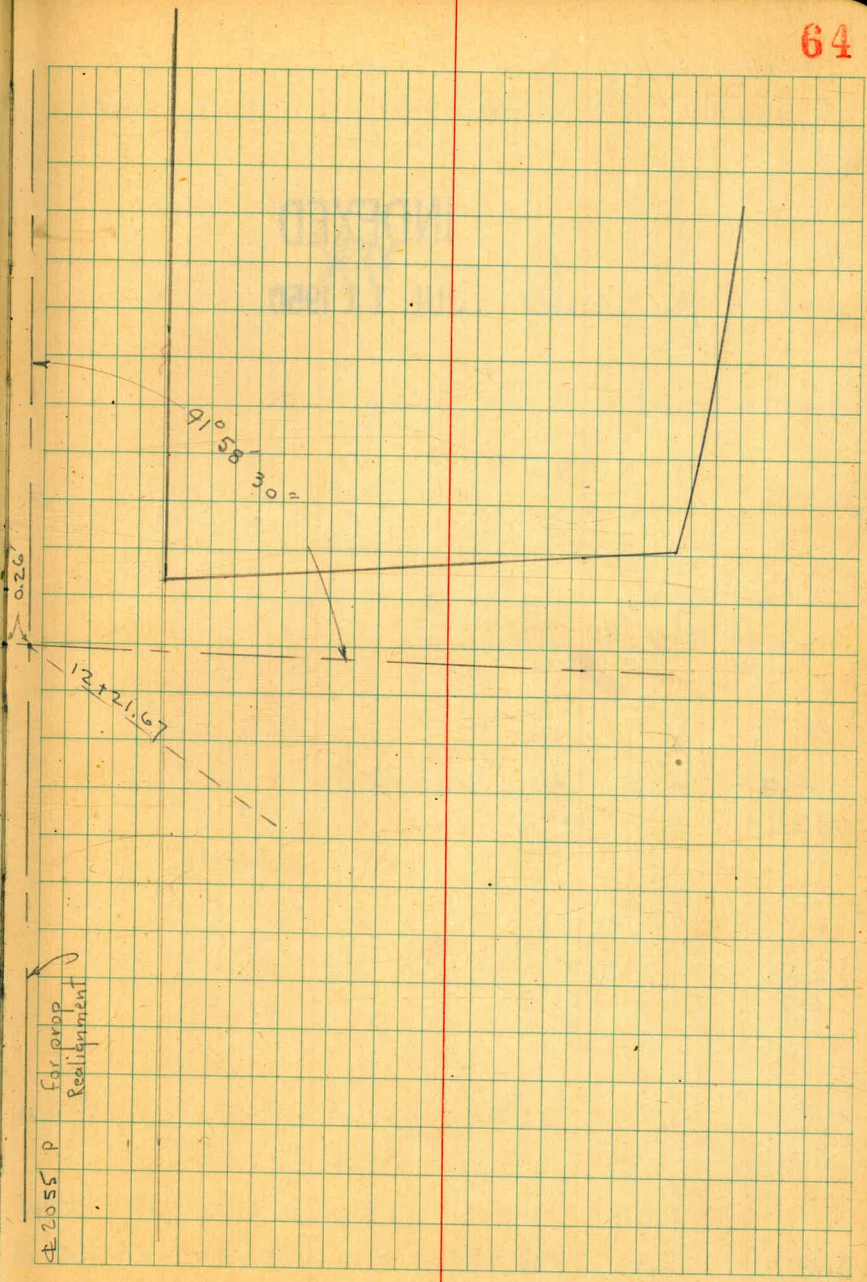
Charlotte st.



Road

Torrey Pines & Per 1847-P227

42055 P for expp Realignment



Levels along E of Prop Drain in
Charlotte St. - Thru + Sly. of Torrey Pines
Rd.

INDEXED
YJK
JUL 11 1950

0+20 = ± Wash

0+17 = 4 Rt = ± 24" Swamp tree

0+15

0+05 = ± = ± Wash

0+00 = 4 H = ± 2" Water pipe in air

0-20

T.P. 6.19 65.08 ✓ 12.60 58.89 = stake at Head wall

T.P. 0.55 ✓ 71.49 ✓ 13.24 70.94

1.07 ✓ 84.18 ✓ 7.52 83.11 = ± T.P. +

B.M. 5.43 90.63 ✓ 85.20 = ct. in S. db

Lt.

±

Rt.

65

^{61.6} 3.5 20
^{53.3} 11.8 7
^{52.3} 12.8
^{56.9} 8.2 3
^{55.7} 6.9 25

^{60.1} 5.0 17
^{53.9} 11.2 12
^{51.1} 14.0 6
^{55.1} 10.0
^{56.8} 8.3 24
± Wash

^{61.5} 3.6 18
^{49.0} 16.1
^{55.3} 11.8 10
^{54.3} 10.8 23
^{55.5} 2.6 40
± Wash

^{62.0} 3.1 25
^{60.48} 4.0 14
^{51.9} 13.2 7
^{50.0} 15.1
^{48.7} 16.9 6
^{52.1} 12.4 15
^{51.1} 5.4 40
Top bank
Top pipe + bank
± Wash

^{62.4} 2.7 15
^{61.8} 3.3 9
^{58.2} 6.9
^{53.0} 12.1 14
^{45.9} 19.2 19
^{46.6} 18.5 34
^{53.9} 11.2 80
Wash

65.08 ✓

Drain = Gal. spike

Torrey - ± Princess - B. 1847 - P. 23

0+847 = cb. Line - Covered with C.L

0+823 = edge C.L walk

0+75 = Top bank

Set B.M
7.16 90.27 4.25 86.02 = dim
183.11 = spike in E

0+45 = Toe of slope

T.P. 7.57 71.71 0.94 64.14

0+36 = 12' Rt. = ± 6' Clump of Bamboo

0+30.3 = ± at E of 2" pipe

0+28 = 18' Rt. = ± 10' Palm

0+27.51 = 0.3' Rt. = ± outlet 24" C.I. pipe

0+23.4 = edge of Conc. apron

Lt. E Rt.

^{82.63}
7.64
Top

^{82.11}
8.16
9+1

^{82.59}
7.68

^{82.0}
8.3
10

8.5
8.8

^{82.5}
7.8
10

Conc. - NEly. Cor Pump House

P. 65

90.27

^{82.4}
8.3
20

^{82.5}
10.2

^{82.0}
8.7
10

^{82.6}
6.1
20

71.71

^{82.86}
6.22
Top pipe

^{82.4}
2.7
20

^{82.1}
7.0
10

^{82.25}
11.33
1.5
apron at
Cor.

^{82.8}
11.27
I.E. pipe

^{82.33}
7.75
Top
Wall

^{82.9}
11.16
1.9
apron at
Cor.

^{82.0}
6.1
5.3
20

^{82.48}
11.60
2.7
Cor. end
wing

^{82.5}
11.56
65.08

^{82.51}
11.51
3.8 = Cor.
along wing wall

T.P. on Hub. 10.63 96.50 4.40 88.87 3+23.29

2+80

2+50

2+35

2+23 = edge Rd.

2+05 = edge Graded Rd.

2+00 = on Fill

1+50 = on Dump

1+25

1+15.2 = s. cb.

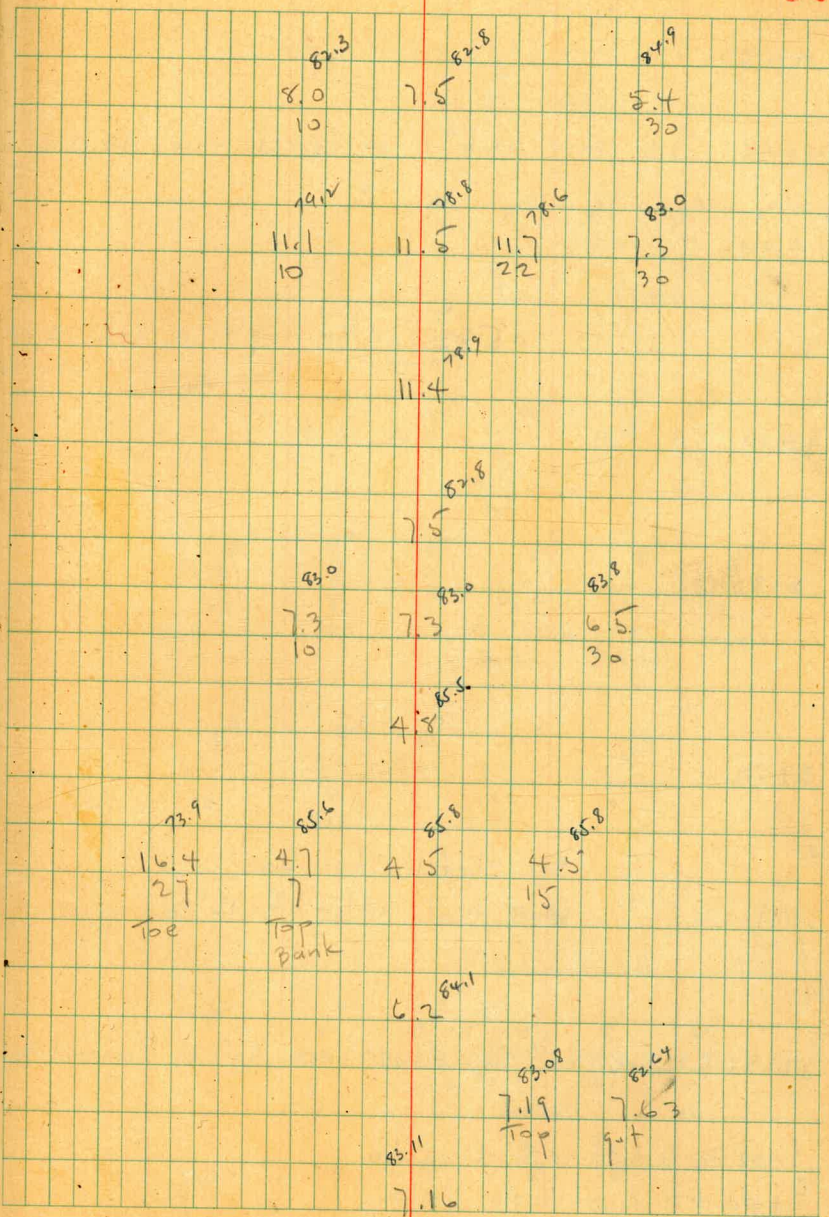
1+00 = †

Lt.

±

Rt.

67



90.27 ✓

4+90

4+48- 3.2 Rt. = stub # 2 on Sewer Line 4+18.8

4+40

T.P. 11.03 105.63 1.90 94.60 = stub # 2

4+10

3+85

3+50

See sketch - for Loc.

3+31-26.7 Rt. = \pm of outlet of 16" Conc. pipe

3+23.29 = Ang 20° 16' Rt. - Sect. 90° to Forward tang

3+08- 7' Lt. = \pm 4' Palm

3+00

Lt.

\pm

Rt.

68

	105.8		100.2	97.8	93.0	91.1		104.8
	+ 0.2		5.4	7.8	12.6	8.5		1.0
	15			4	9	11		25
				Top	\pm Ditch	Top		
						Toe		
	101.9	96.1	94.1	90.4	93.7	94.1	104.1	
	3.7	9.5	11.5	15.2	11.9	11.5	30	
	10		5	12	Top	14	30	
			Toe	\pm 3' Ditch		Toe		
				Bot.				
			105.63					
	97.9	92.7	91.7	89.6	91.6	91.8	102.0	
	+ 1.4	4.3	4.8	6.9	4.9	4.7	+ 5.5	
	15	7	5	5	Top	13	30	
		Toe	\pm 3' Ditch			Toe		
			Bot.					
	94.3	91.0	89.6	88.9	89.9	91.1	98.5	
	2.2	5.5	6.9	7.6	6.6	5.4	+ 2.0	
	15	8	13	13	Top	17	30	
		Toe	\pm 2' Ditch		Bottom (ground)	Toe		
	91.8	86.7	86.7	87.2				
	4.7	9.9	9.9	9.3	5.3	9.2		
	15	4	19	30				
		Toe						
					84.0		86.56	
					12.5		9.94	
					21.7		26.7	
					Bottom at Wash		I.E. end Pipe	
	89.1	85.6	85.87	86.1	83.0	86.1	90.7	
	7.4	10.9	10.63	10.4	13.5	10.4	5.8	
	15	8	on Hub	7	9	20	30	
		Toe		\pm Wash		Toe		
	12.7	83.5	83.5	82.5	84.5	85.1	89.1	
	20			5	13	20	30	
	Toe				\pm Wash	Toe		
					96.50			

6+96.37 = Hub = 0+60 on Φ White field PL.

6+60

T.P. 8.69 161.33 ✓ 0.68 152.64

6+15

T.P. 11.88 153.32 ✓ 0.12 141.44

5+80

T.P. 12.82 141.56 ✓ 0.04 128.74

5+50

T.P. 13.01 128.78 ✓ 0.30 115.77

T.P. 10.87 116.07 ✓ 0.43 105.20

Topo Rods on Tang. prod. ahead. (no angle)

5+11.05 = Ang. $116^{\circ} 21'$ Lt. - Sect. 90° to back Tang.

7.32
0+70
on Φ

154.01 Lt. Φ 156.25 Rt. 158.6

5.08 2.70
0+50 on Φ

157.2 154.3 159.2
10.1 7.0 4.1
10 10

161.33 ✓

10.7 142.6 145.7 148.2 ✓
10 7.6 5.1
10 10

153.32 ✓

6.2 135.4

141.56 ✓

9.0 119.5 122.1 124.6
10 6.7 4.2
10 10

128.78 ✓

5.0 100.6 97.4
15 ahead 82 20' ahead = Φ Ditch

99.99 99.9 95.4 91.4
5.64 5.7 10.2 6.2 + 1.7 107.3
on Hub. 2 Φ 8
105.63 ✓ Top Ditch Top + Toe 20

12+75

12+51 - 15.6 Lt. = Ely. of 10' inlet

12+46 = ± Inlet on Lt. 3.5x 3.5 Box

12+45.3 = E. end 8' opening on Rt.
= end of Cold lay Cover.

12+41 - 15.6 Lt. = W. end 10' opening Inlet

12+40 - 20.5 Rt. = ± F.H.

12+38.3 = ± of 2.2' x 1.8' Box - 1.8' along cb.
(on Rt.)

12+37.3 = W. end of 8' opening inlet on Rt

12+21.67 = ± r 1+00.26 on ± Drain Survey
See P. 64

12+02 - 20.8 Lt. = ± Pipe # P 1698

Lt. E Rt. 72

82.1	83.34	83.14	82.68	82.93	83.20	83.04	82.59	82.99	82.9
8.5	7.25	7.45	7.91	7.66	7.39	7.55	8.00	7.60	7.7
24	19.9		15.2	7.5		7.5	15		25
Top	edge walk	Top	gut.				gut.	Top	
				8.43	9.02	81.57			
				15.6	15.6				
				Top cb.	gut.				
81.4	82.26	78.15	82.26	81.19	82.13	82.63	82.45	82.20	82.61
9.2	8.33	12.44	8.33	9.10	8.46	7.96	7.90	8.39	7.92
25	20	I.E.	Top	15.6	7.5		7.5	14.9	8.5
Top	edge	Box	Ch.	gut.			gut.	Top	25
bank	walk			grate					
							8.45	7.92	82.61
							14.9	14.9	
							gut.	Top cb.	
				82.34	81.4				
				8.25	8.95				
				15.6	15.6				
				Top	gut				
				cb.					
						82.16		82.71	19.91
						8.44		7.88	10.68
						14.9		14.9	I.F. of
						gut.		Top	Box
							82.23		
							8.36		
							gut.		
							14.9		
								7.96	
								14.9	
								Top cb.	
81.5	82.49	82.64	82.12	82.73	83.10	83.04	82.65	83.08	83.39
9.1	8.11	7.95	8.47	7.86	7.49	7.55	7.94	7.51	7.2
25	20.3	16.3	15.9	7.5		7.5	15		25
Top	edge	Top	gut.				gut.	Top	
bank	walk	cl.	cb.						

90.59 ✓

13+50 = End

13+19 - 23.5 Lt. = ± of 6 x 7' Conc. Water M.H.

13+14 - 21 Lt. = ± P. pole # 1720

13+00

12+84 - 16.3 Rt. = ± Tel pole # 307924 - H

Notes Reduced Pg. 45. 73

7-11-50

83.57	83.59	83.20	83.53	83.76	83.55	83.19	83.58	84.5
7.02	6.90	7.29	7.06	6.83	7.00	7.40	7.01	6.1
2.5	19.8	15.2	7.5		7.5	14.9		2.2
on C.L. Dr.	edge walk	cut in Dr.				cut	Top	Top slope

6.85 83.74
23.5
Top M.H.

83.2	83.57	83.39	83.76	83.28	83.51	83.32	82.87	82.28	83.9
7.4	7.02	7.21	7.63	7.31	7.08	7.27	7.72	7.31	6.7
2.4	19.9		15.2	7.5		7.5	14.9		2.5
Top	edge walk	Top	cut				cut Top		

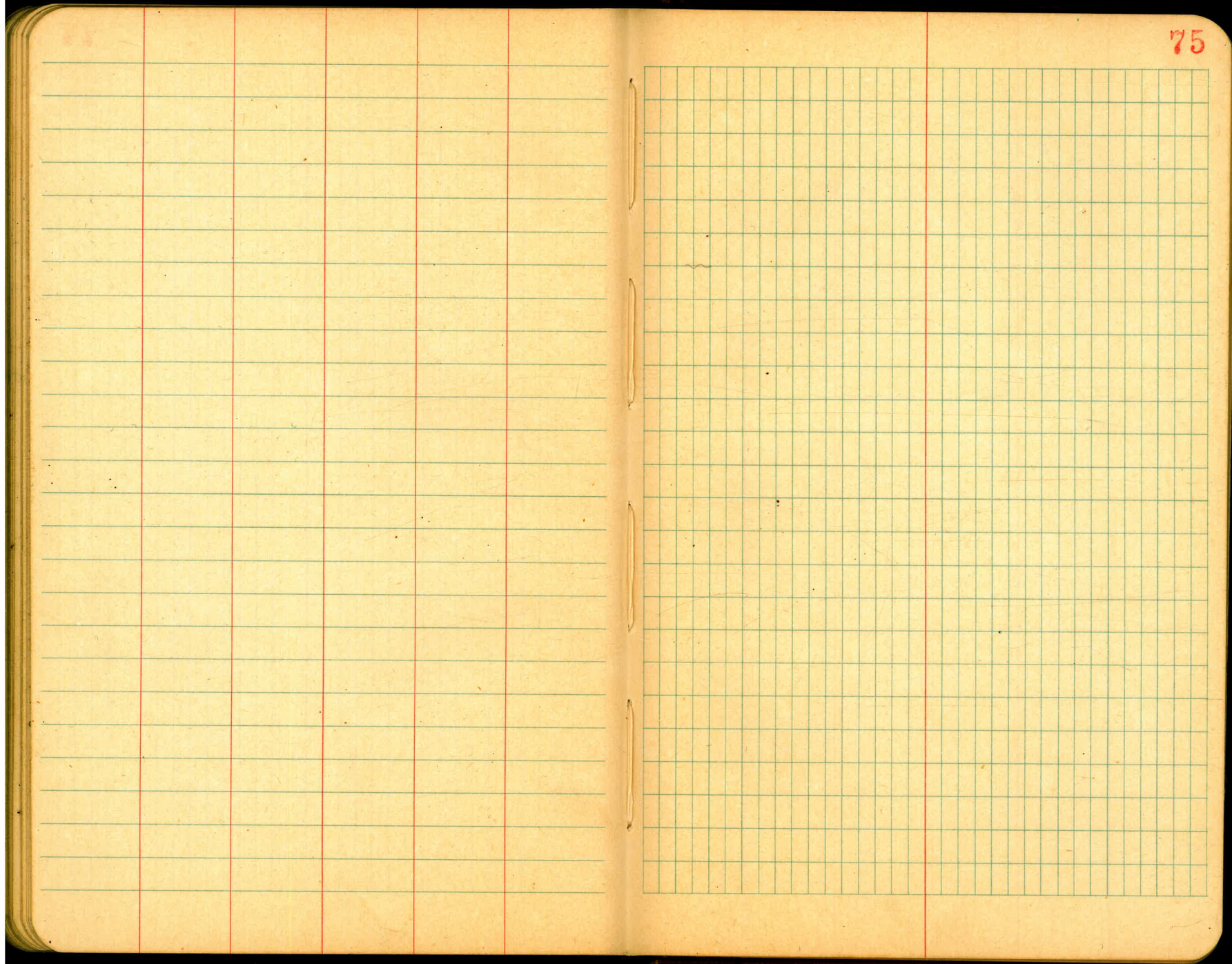
90.59 ✓

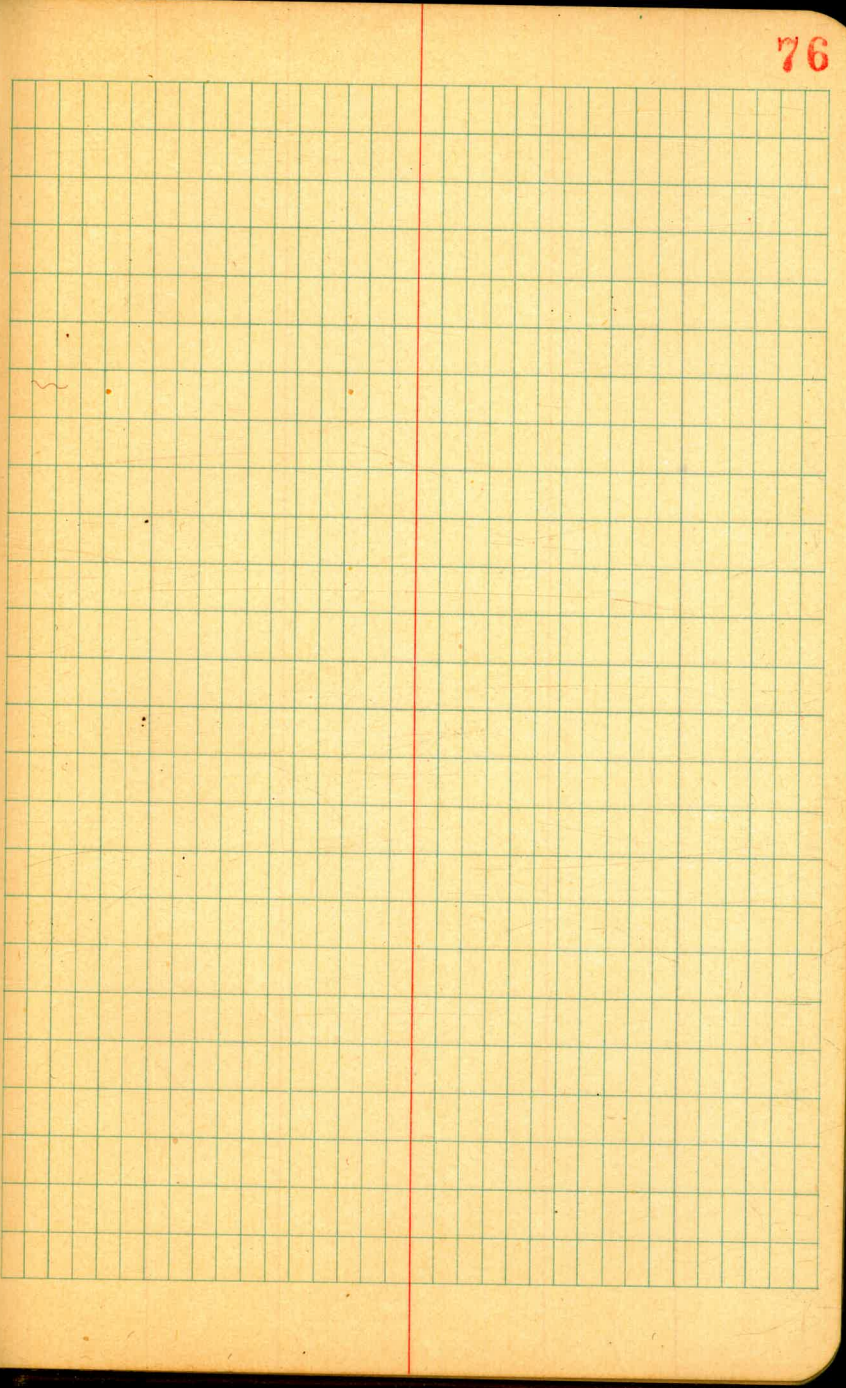
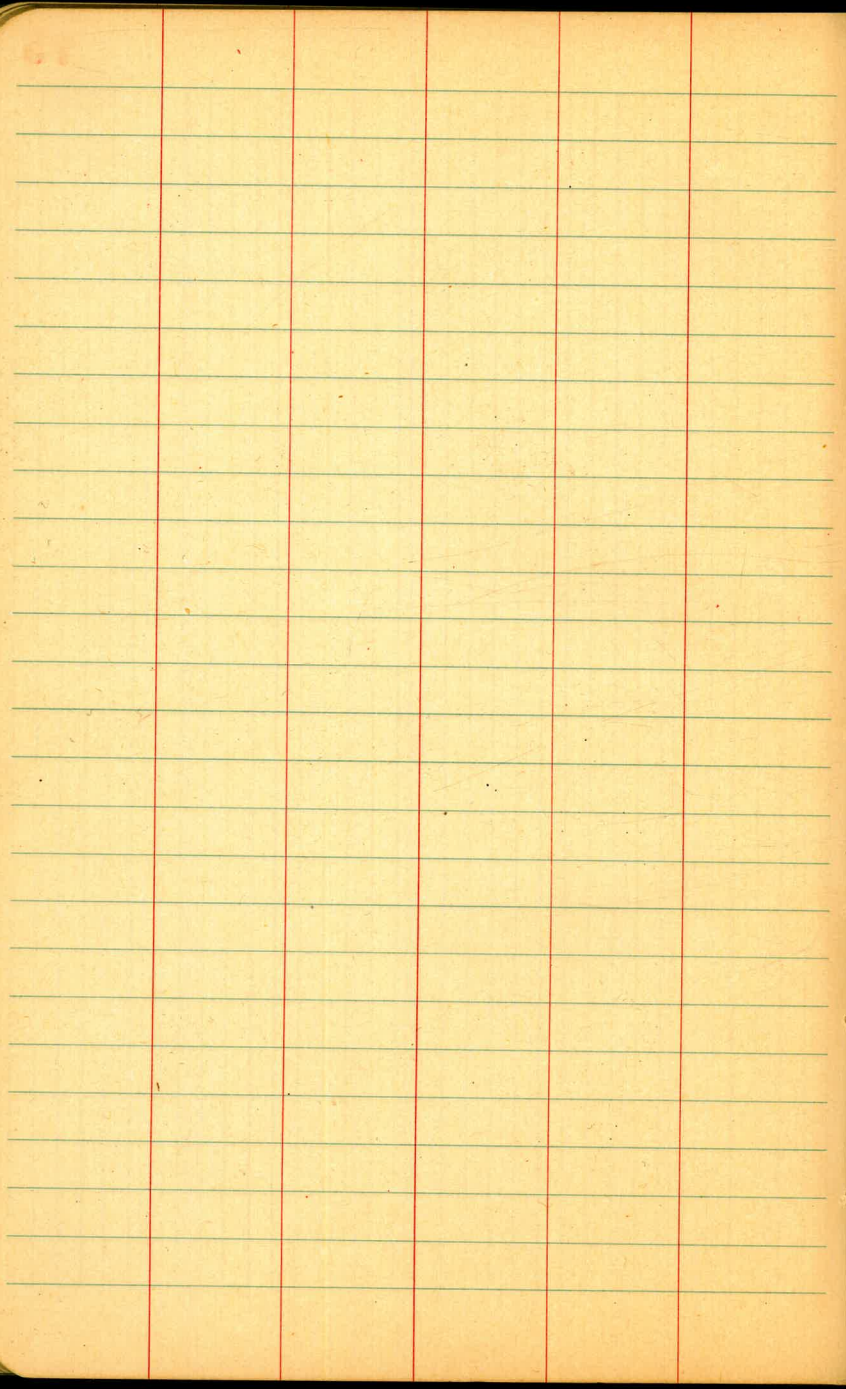
Lt.

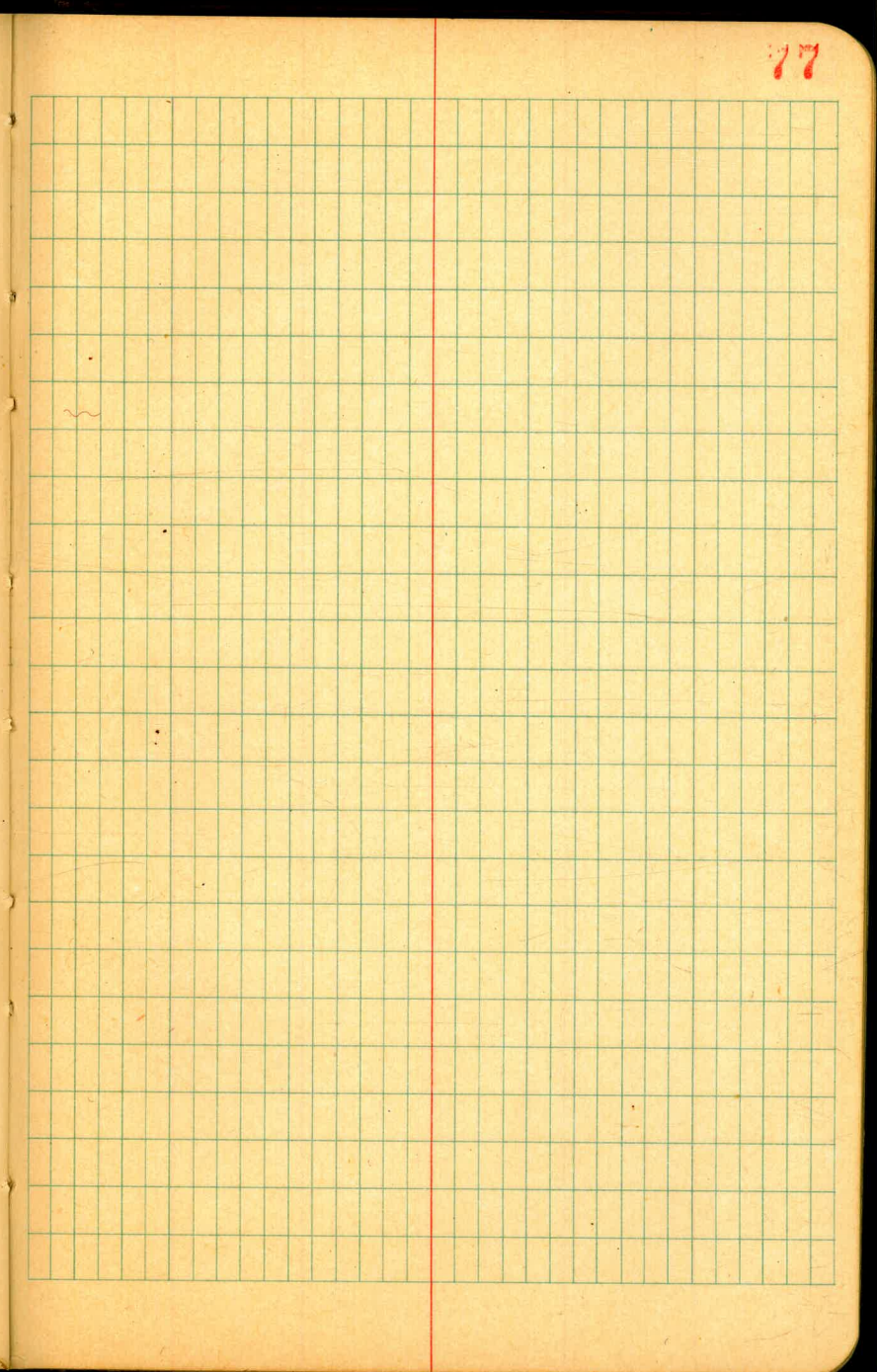
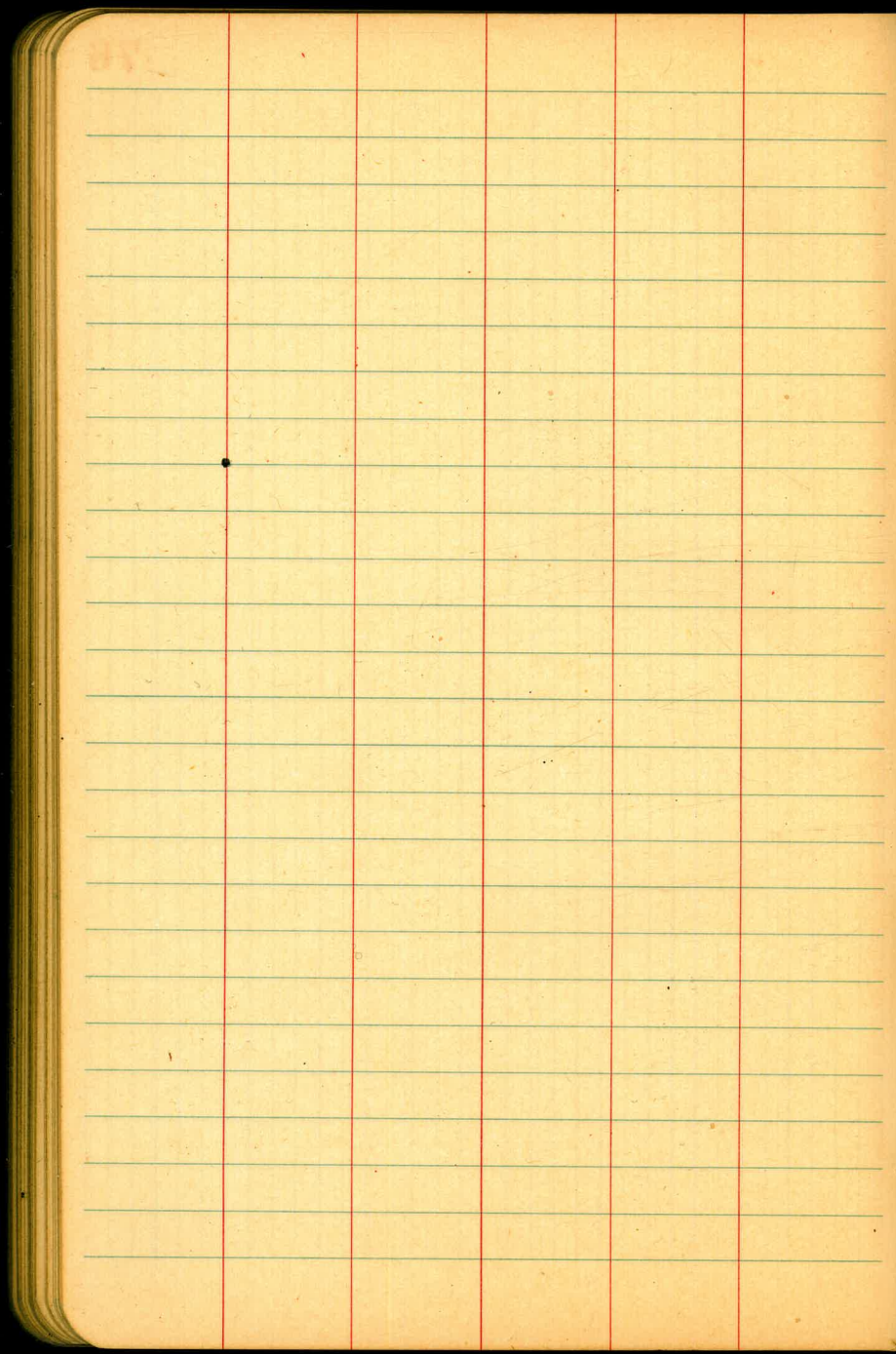
Rt.

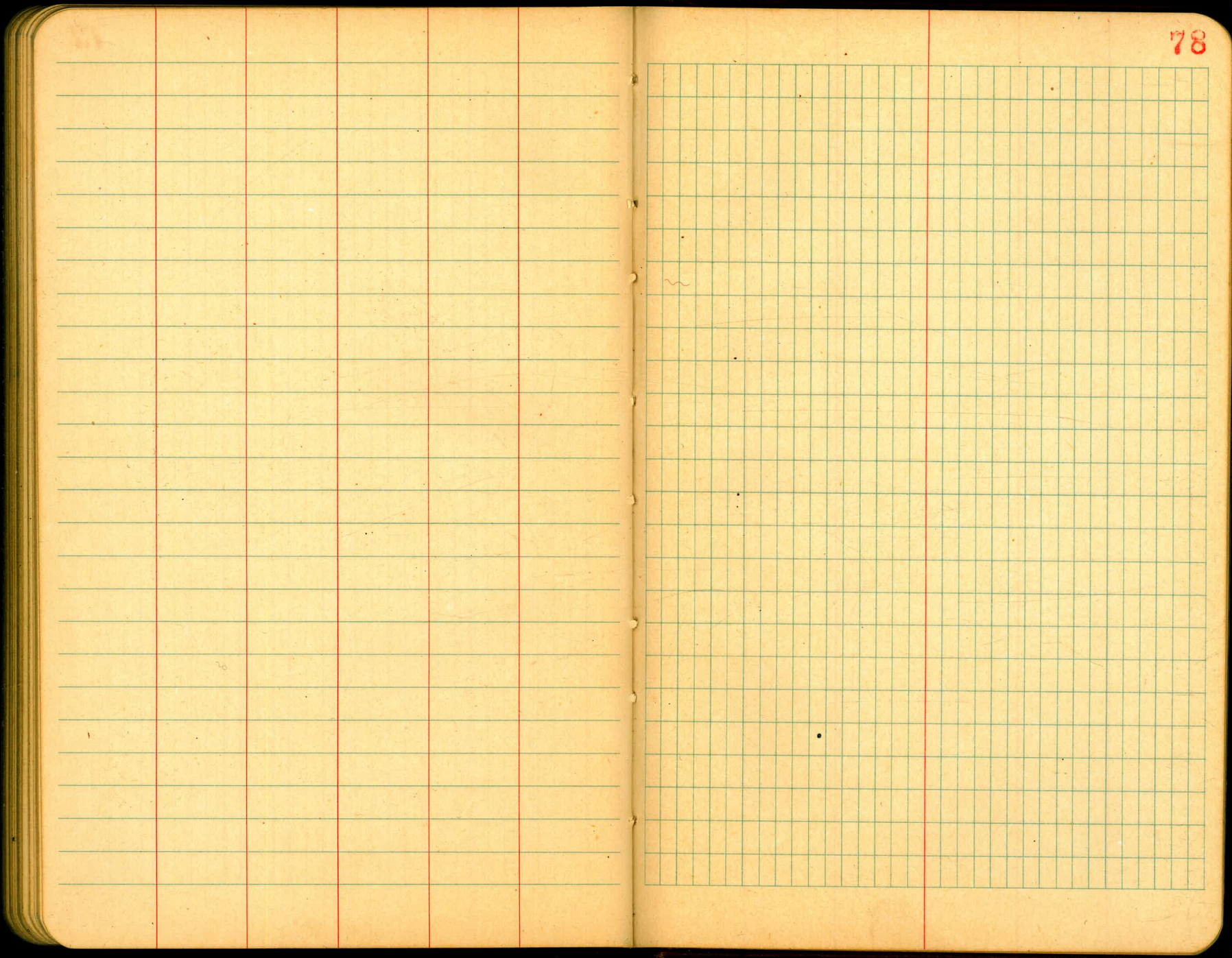
Rt.

73









$$\begin{array}{r} 98.50 \\ 19 \\ \hline 98.32 \end{array}$$

$$\begin{array}{r} 62.4 \\ 35 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 12+21.7 \\ 27.4 \\ \hline 11+94.3 \end{array}$$

271.21 = Top Hyd. - 63rd + Brooklyn B2000 - P.33

271.42 = S.W. 7' Mon

5 + 11.05
3.23.29
1.87.76

13.8
46.2
60.0

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

10.3
4.8
5.5

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 47.9. For slopes of 1 on 1 see inside of front cover.

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