

1787

1787

Pages.

Index :

1-44 - Prop Storm Drain - Hawley to Mandell - <sup>Adams</sup> N. side  
45-50 - Ext. Prop Drain - Mission Valley  
51-73 - Add. Notes - Adams Ave Drain

Levels + Location for Prop. Storm  
Drain - on N. side of Adams - from  
Hawley to N. of Mondell Terrace

#1176

W.O. 60126

6-13 to 20-47

Osborne  
Hardin  
Smith  
Worrell

Indexed  
C.S. & R.

34<sup>th</sup>

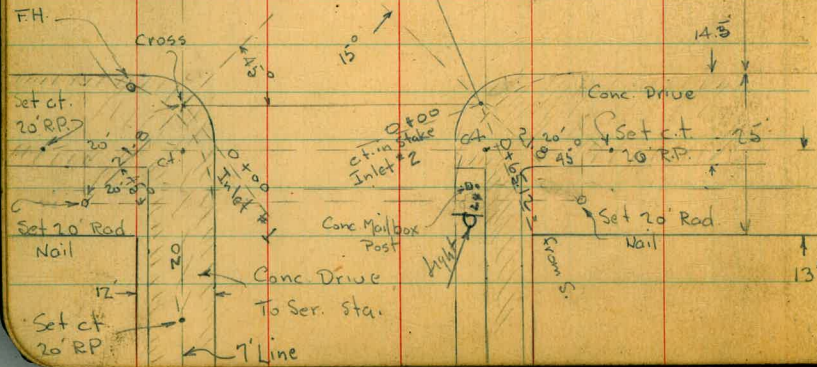
see P. 54 for Poles  
lights etc.

Note: Returns are  
To scale 1" = 30'  
Positions of some  
Tops shown  
by scale hoc.

Hue  
Adams

See Page 51

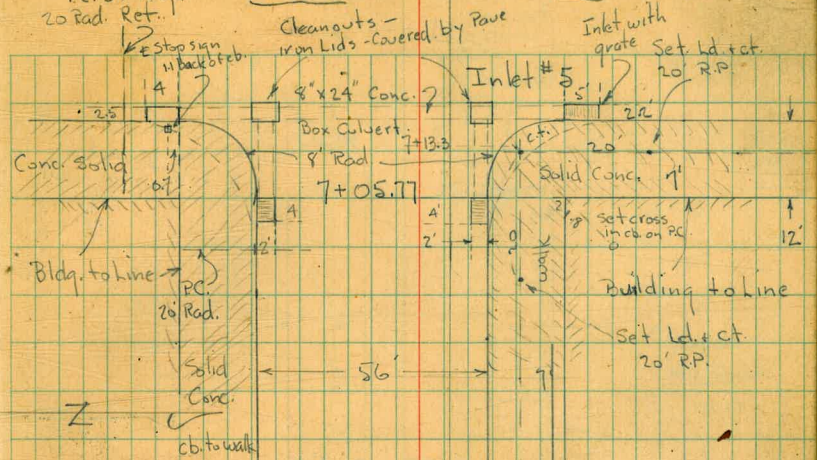
Sec P. 51



P.C. of Prop.  
20 Rad. Ret.

Felton

St. 60' 2



Water Main in Hawley, 10' E of G.  
Water Dept found top of pipe  
20" below paving at point  
C/S of 72' curb of Adams.  
By Phone. 7-11-47

Thomas' Office.

See P. 54 for  
Poles - etc.  
+ P15

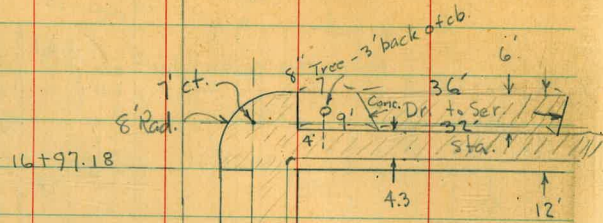
34<sup>th</sup>

St. - 60'



32<sup>nd</sup>

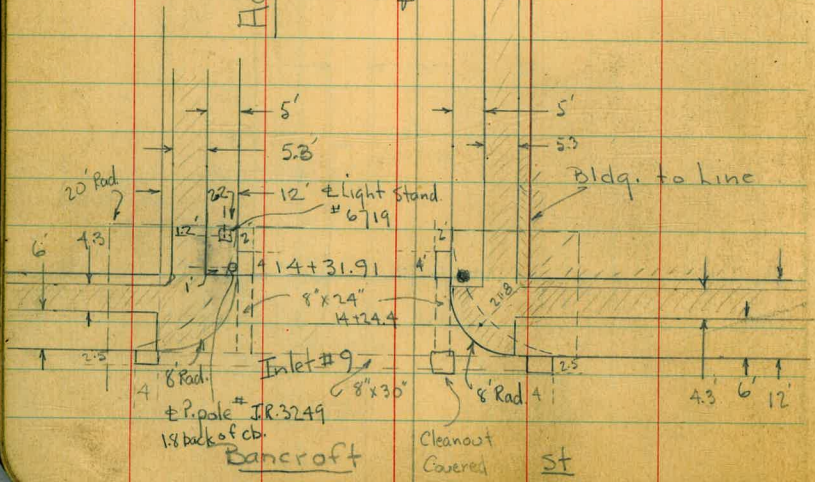
st



Adams Ave

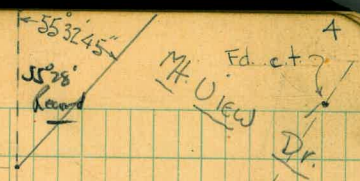
Prop. Culvert

Adams Ave



Bancroft

Cleanout Covered st



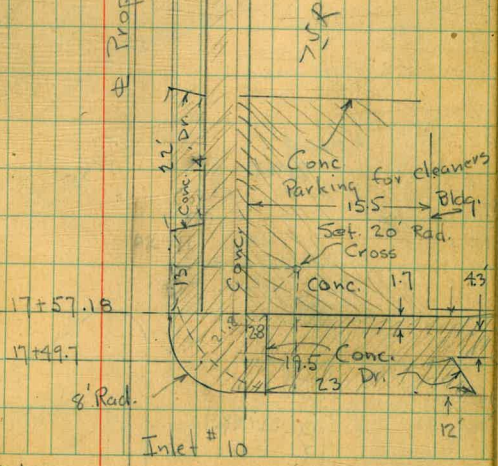
22+27.60 spike

21+98.90

Adams Ave

Prop. Culvert

Adams Ave



17+57.18

17+49.7

Inlet #10

32<sup>nd</sup>

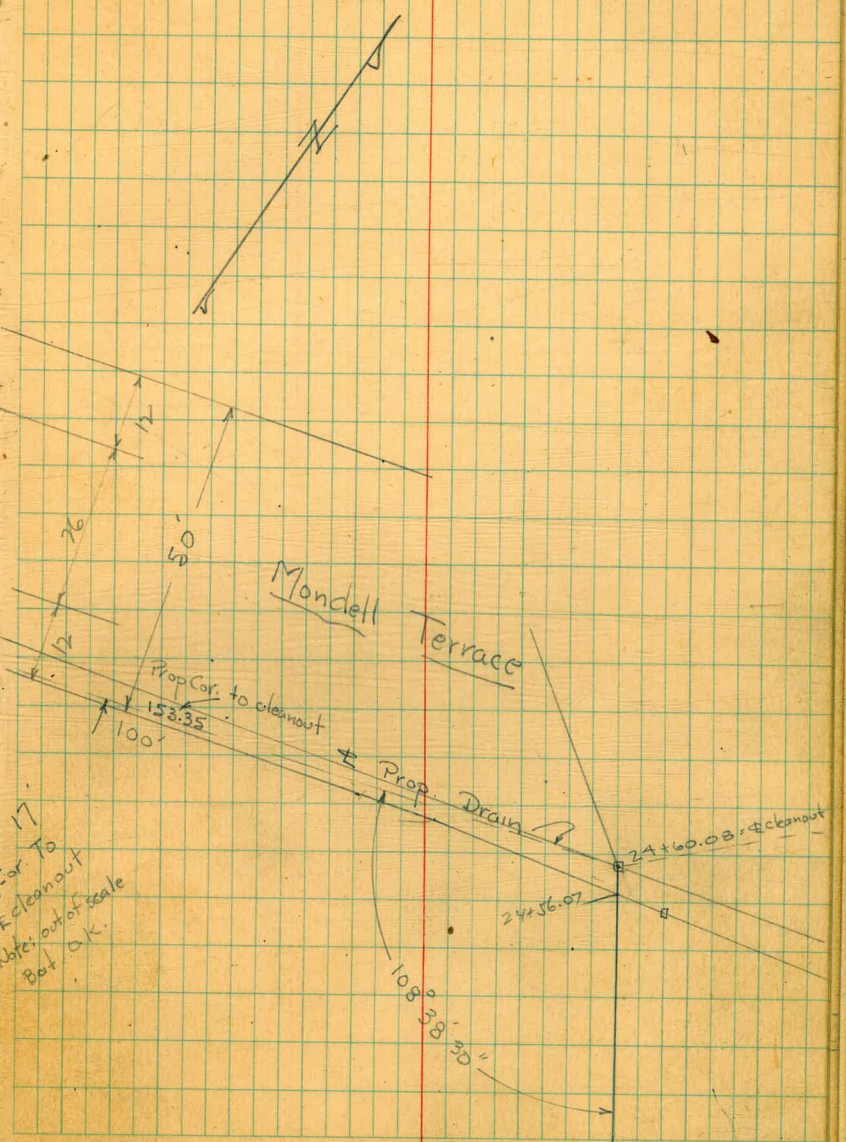
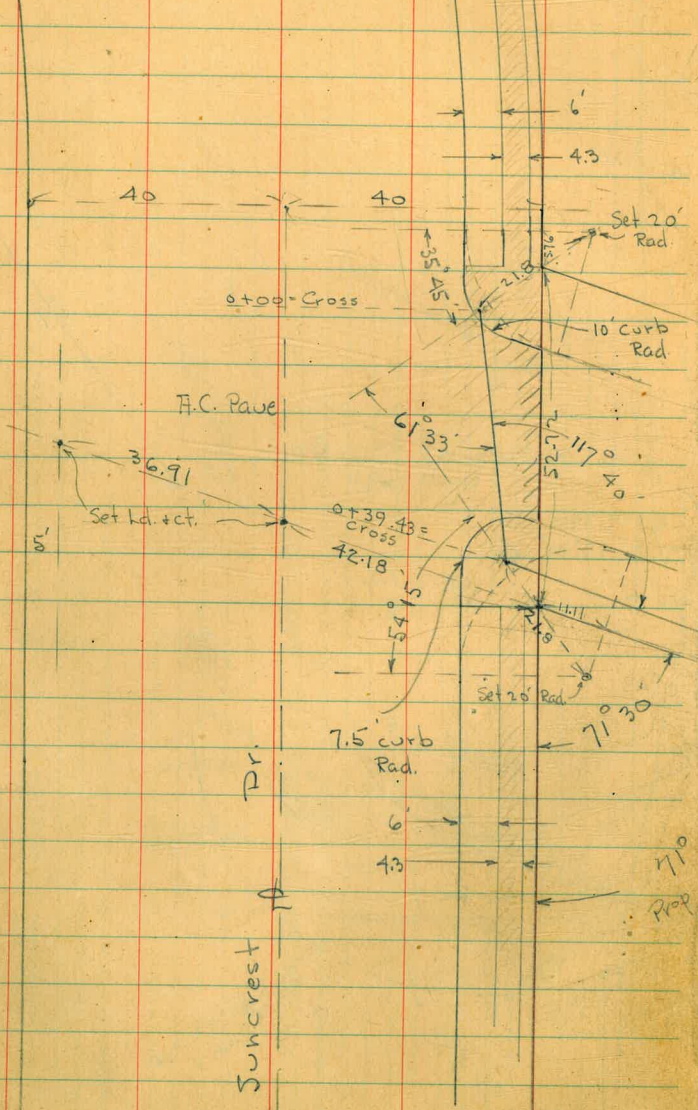
st







31 - 31.3  
26 - 27.4

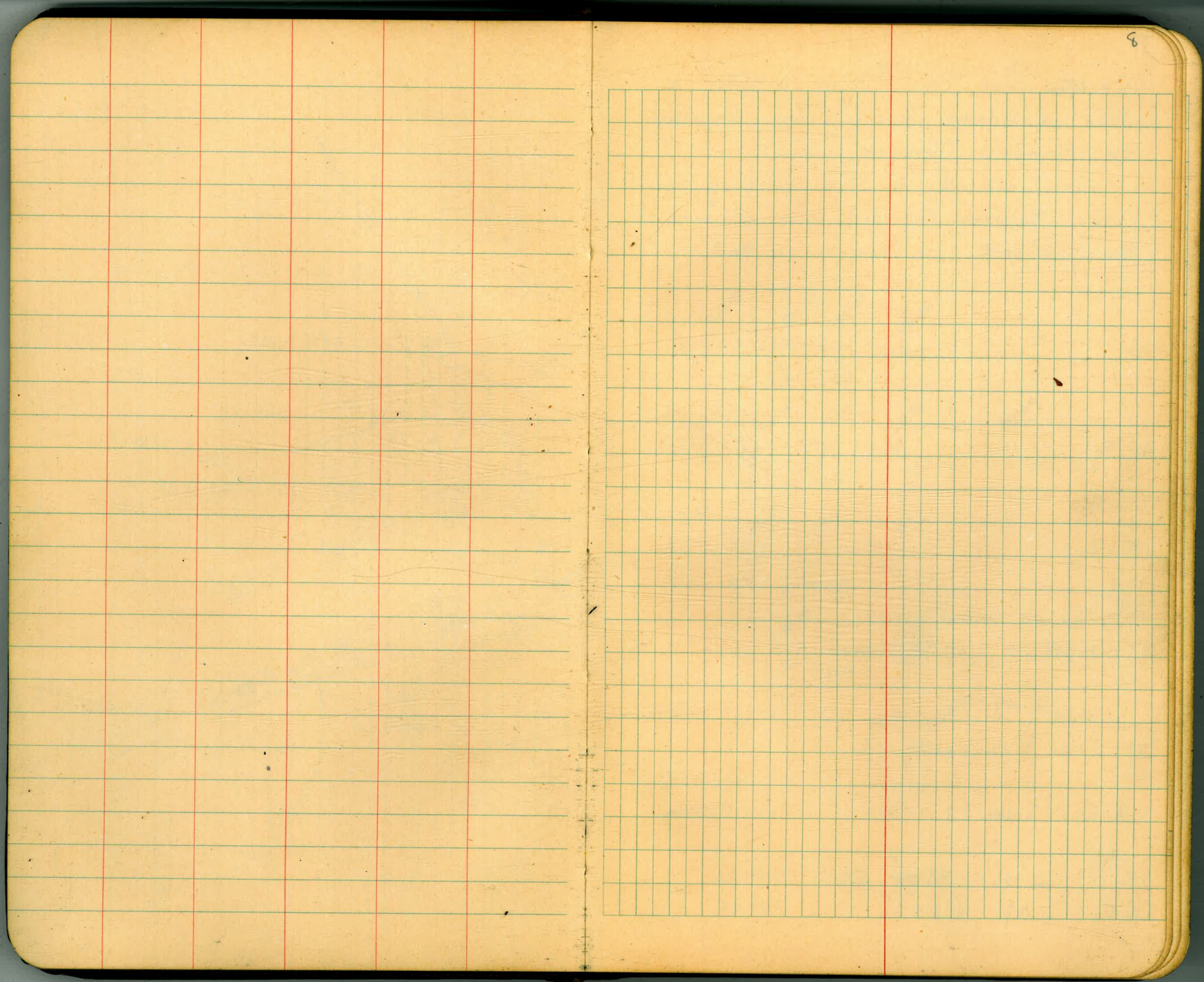


17  
Prop. Cor. to  
cleanout  
Note: out of scale  
Bot. O.K.

Mondell Terrace

Prop. Drain

108° 38' 30"





E.C. = N. end = 8' N. of N.L. Adams

3/4

⊕

1/4

P.C. = E. end

40' E. along N. cb. Adams

Ret. Inlet #2 - N.E. Cor. Hawley + Adams

50' E. along S. cb. Adams

E. end = S.W. of E.L. Hawley = P.C. 20' Ret.

Lt.

Rt.

	391.97 4.57 5		391.23 4.31 got. in Dr.		391.80 4.24 14.7 = edge Dr.
	391.32 4.72 67	391.14 4.90 1.7 gut.	391.63 4.36 1.7 Top		391.74 4.36
	390.99 5.05 10.1	391.02 5.02 5.1 gut.	391.68 4.36 5.1 Top		391.80 4.24
	391.07 4.97 69	390.94 5.10 1.9 gut.	391.02 4.60 1.9 Top		391.62 4.42
		391.09 4.95 5	391.42 4.60 Top		391.81 4.23 10 = on Ret.
			390.95 5.11 gut.		391.63 4.41 5 walk
			391.77 4.27 10.3		
			391.61 4.43 Top		391.12 4.90 gut.
			391.13 4.91 Top		390.63 5.41 gut.
		390.96 5.08 5	391.58 5.46 gut. in Drive		391.60 4.44 10.4 = edge of Dr.

396.04 ✓

50' W. along N. cb. Adams

E.C. = W. end. = 5' E. of W.L. Hawley

3/4

⊕

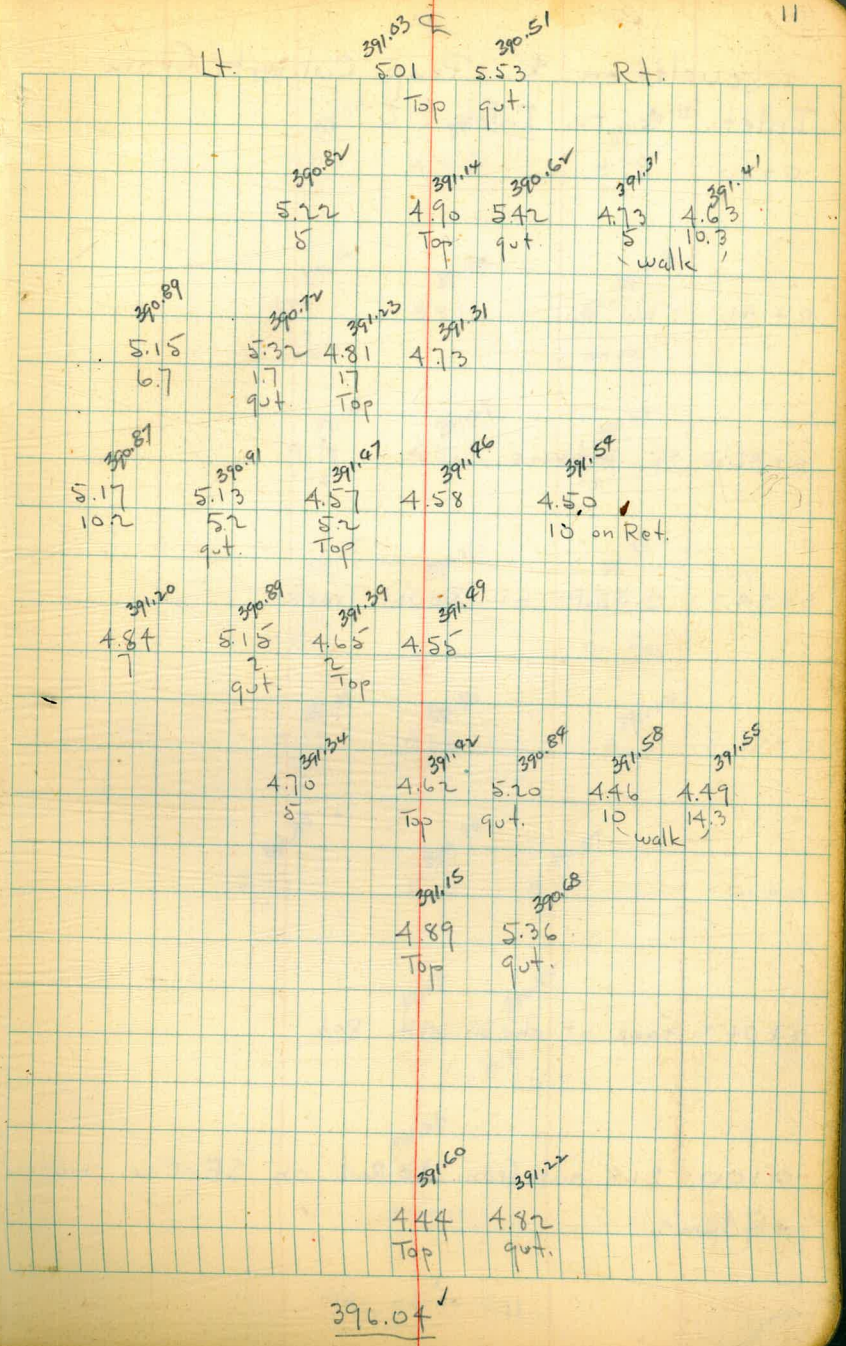
1/4

P.C. = N. end. - 8' N. of N.L. Adams

50' N. along W. cb. Hawley

Ret. - Inlet #3 = N.W. Cor. Adams + Hawley

40' N. along E. cb. Hawley



Levels on  $\Phi$  Prop. Culvert from  
Inlet # 1 to Inlet # 2

0+50

0+41 = N. Rail

0+32.5  $\Phi$  Adams

0+24.3 = S. rail of Doub Track

0+20

0+10

0+04 = face of cb. on ext. Ret.

0+00 = 21.8 out from 20' Rad. on SE. Cor. Hawley  
& Adams

12

Lt.

$\Phi$

Rt.

391.14 4.90 10	391.19 4.85	391.26 4.78 10
391.16 4.88 10 on rail	391.24 4.80	391.28 4.76 10 on rail
391.25 4.79 10	391.29 4.76	391.34 4.70 10
391.14 4.90 10 on Rail	391.21 4.83	391.31 4.73 10 on Rail
391.33 4.71 10	391.38 4.66	391.44 4.60 10
390.87 5.17 10	390.99 5.10	391.07 4.97 10
	391.13 4.91 Top	390.57 5.50 Gut
	391.23 4.81 on Cross	

396.04 - P-11

0+74.73 RT -  $\Phi$  P. pole # J.R. 3436

0+62.5 - 22.5 RT. =  $\Phi$  12" Acacia

0+61.8 = opp.  $\Phi$  inlet # 3

0+50

0+21.18 = Ang.  $29^{\circ}57'$  RT

0+10

0+03.4 = face cb. on Ext. Ret.

0+00 = 21.8 out from 20' Rad. on N.E. Cor. (0+65.12 Below)  
Begin Levels on Prop. Drain along Adams

0+65.12 =  $\Phi$  Inlet #2 - 21.8 out from 20' Rad. on N.E. Cor. Hawley + Adams = 0+00 ahead. on Line along Adams. to west.

0+60.8 = cb. face on Ext. Ret.

Adams +34 7.65 396.90 — 389.25 S.W.R.P.

Red = Top of Pav. after

completion of Job.

A =  $\Phi$  drain c. out from curb

C = gutter of 100' on movement

7-13-49 C.H.S.

Lt.

Rt.

390.97 390.85  
5.93 6.05  
 $\Phi$  6

390.93  
5.11

390.89  
5.15  
6.4  
gut.

391.42  
4.62  
6.4  
Top

391.47  
4.57  
10.4 = 21.8  
out on  
 $\Phi$  Ret.

391.03  
5.01  
10

390.98  
5.06

390.88  
5.16  
10  
gut.

391.09  
4.95  
10

391.18  
4.86  
10

391.04  
5.00

390.93  
5.11  
7  
ingut.

391.02  
5.02  
10 - on split

on split of Ang.

391.14  
4.90  
10

390.98  
5.06

391.34  
4.72  
10

391.69  
4.35  
Top

391.05  
4.99  
gut.

391.80  
4.24

391.80  
4.24

391.85  
4.48  
Top

390.98  
5.06  
gut.

396.70

396.04 ✓





Cont. on P. 17

6+50

6+00

5+50

5+00

T.P. 5.59 395.17 7.32 389.58

4+50

4+31.3 - 8.1 Rt. = \$ Lamp Standard # 67 34

4+25 - 7.5 Rt. = \$ P. pole # J.R. 3398

4+24.25 = W.L. 34<sup>11</sup>

4+16.8 = \$ cleanout - opp. \$ Inlet # 4 - 2.8 out  
from 20' Rad.

3+76.25 = E. cb.

396.90

Cont. P. 17

E

15

Lt.

Rt.

388.53 <u>6.64</u> E	388.04 <u>7.13</u> G	388.89 6.08 10	388.49 6.48	387.96 7.01 6 gut.	388.45 6.52 6 Top.
388.61 <u>6.52</u> E	388.34 <u>6.83</u> G	389.03 5.94 10	388.70 6.27	388.29 6.68 6 gut.	388.77 6.20 6 Top
388.70 <u>6.38</u> E	388.56 <u>6.61</u> G	389.16 5.81 10	388.81 6.16	388.44 6.53 6 gut.	388.97 6.00 6 Top
388.91 <u>6.26</u> E	388.68 <u>6.49</u> G	389.24 5.73 10	388.95 6.02	388.57 6.40 6 gut.	389.19 5.78 6 Top
		<u>395.17</u>			
389.19 <u>7.71</u> E	388.98 <u>7.92</u> G	389.37 5.60 10	389.19 5.78	388.88 6.09 6 = gut. in Dr.	
389.23 <u>7.67</u> E	389.11 <u>7.77</u> G	389.42 5.55 10	389.27 5.70	389.03 5.94 6 gut.	389.95 5.52 6 Top
389.22 <u>7.68</u> E	389.07 <u>7.83</u> G	389.42 5.55 10	389.27 5.70	389.11 5.86 6.4 gut.	389.57 5.40 6.4 Top
					389.57 5.40 10.4 = \$ Inlet.
389.46 <u>7.44</u> E	389.33 <u>7.57</u> G	389.60 5.37 10	389.45 5.52	389.19 5.78 6	389.24 5.73 16 gut.
					389.91 5.06 16 Top - P.C.
		<u>396.90</u>			
			<u>394.97</u> ✓		



T.P. 4.96 393.91 7.12 388.05

Cont. on P. 20

7+66.5 - 7.2 Rt. =  $\pm$  P. pole - No #

7+65.77 = w.L. Felton

7+58.2 =  $\pm$  Lug.

7+13.3 =  $\pm$  Cleanout

7+35.77 =  $\pm$  Felton

7+17.77 = E. cb.

7+05.77 - 8' Rt. =  $\pm$  Light Stand # 6730

7+05.77 = E.L. Felton = w. end Inlet.

7+01.77 = opp E. end cb inlet = 4'x2' Box + Grate

check B.M. - NW. Felton + Adams 5.26 388.26 388.32 = Book

T.P. 4.27 392.52 5.72 389.25

Cont. from p. 15

395.17  
From P. 15

Cont. on  
P. 20

17

Lt.		Rt.	
388.01 <u>7.16</u> $\pm$	387.57 <u>7.60</u> $\pm$	388.48 5.04 10	388.02 5.50 6 gut.
388.10 <u>7.07</u> $\pm$	387.70 <u>7.47</u> $\pm$	388.5v 5.00 10	388.1v 5.40 6.01 6.4 gut.
388.32 <u>6.85</u> $\pm$	388.05 <u>7.12</u> $\pm$	388.67 4.95 10	387.51 5.72 6.4 Top
388.42 <u>6.75</u> $\pm$	388.45 <u>6.72</u> $\pm$	388.6v 4.90 10	388.10 5.22 10.4 = 21.8 out.
388.94 6.54 62	388.08 5.44 62	388.6v 4.90 10	388.37 5.15 6 gut.
FL. Outlet of Culvert at S.L. Adams	Top cb.	388.45 5.07 6	388.3v 5.20 6 Top
388.21 <u>6.96</u> $\pm$	387.94 <u>7.23</u> $\pm$	388.70 4.82 10	388.43 5.09 6 Top cb
388.20 <u>6.97</u> $\pm$	387.96 <u>7.21</u> $\pm$	388.3v 5.20 6 Top Inlet	388.27 5.25 6 Top cb
FL. Inlet	FL. Inlet	388.38 5.24 6 4: Cor. Inlet	388.44 5.08 18 Top
		387.94 5.58 6 gut. = FL inlet	388.24 6.40 19 Top
			387.1v 5.10 23 Top
			388.4v 5.60 23 FL
			387.9v 5.60 6 FL Culvert
			388.5v 5.00 6 Top
			387.18 6.34 6 FL Culvert
			388.50 5.02 6 Top cb.

395.17

393.52

Levels around prop. 20' Rad. Ret.  
at Felton + Adams

50' N. along E. cb. Felton

E.C. = 8' N. of N.L. Adams

3/4

±

1/4

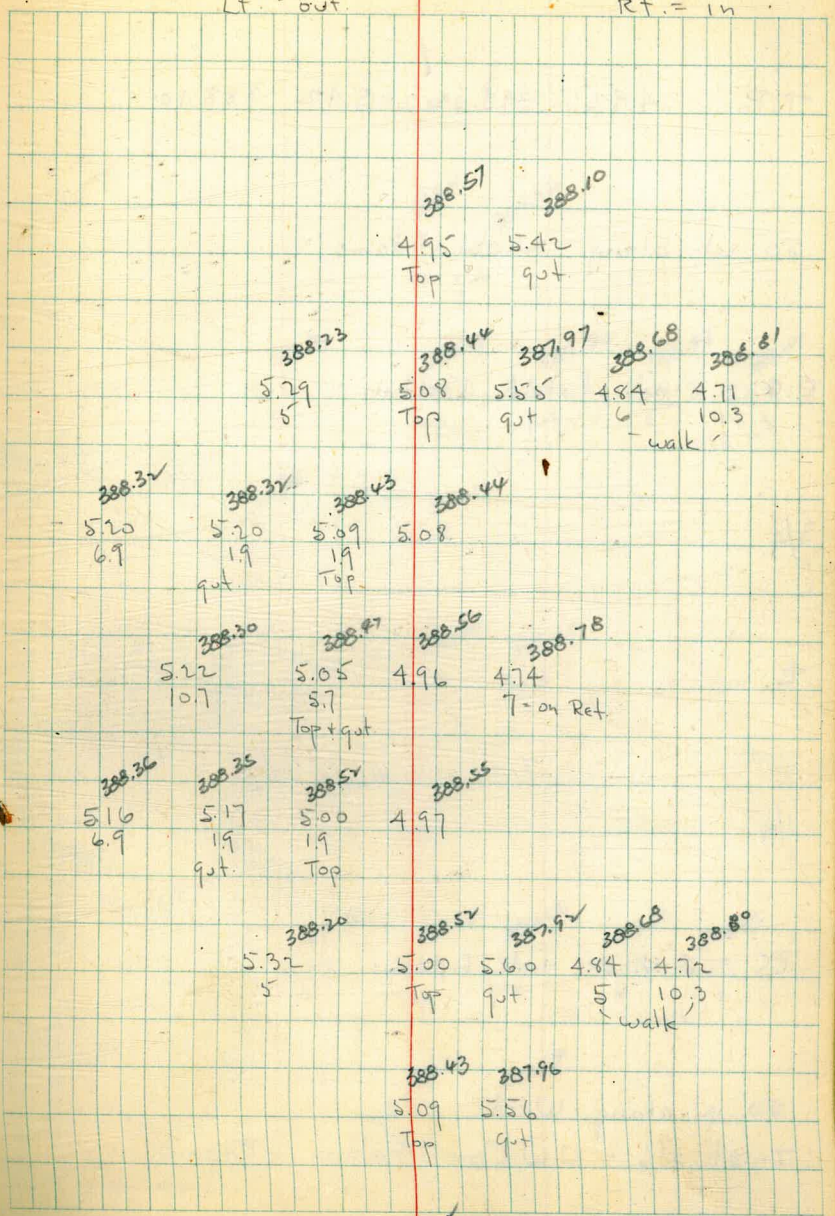
P.C. = 8' E. of E.L. Felton

50' E. along N. cb. Adams

Inlet #5 - N.E. Cor.

Lt. - out.

Rt. = in



393.52 - P.17

T.P. 4.92 393.02 ✓ 5.42 388.10

50' W. along N.cb. Adams

E.C. - 8' W. of W.L. Felton

3/4

±

1/4

P.C. = 8' N. of N.L. Adams

50' N. along W.cb.

Inlet #6 - N.W. Cor. Felton + Adams

393.02 ✓

388.11  
387.26  
5.41 6.26  
Top gut.

387.87  
5.65  
5  
388.09  
5.43  
Top  
387.96  
6.06  
gut.  
388.43  
5.09  
5  
walk  
388.44  
5.08  
10.3

387.93  
5.59  
6.9  
387.48  
6.04  
1.9  
gut.  
388.00  
5.52  
1.9  
Top  
388.14  
5.38

387.94  
5.58  
10.2  
387.56  
5.96  
5.2  
gut.  
388.18  
5.34  
5.2  
Top  
388.29  
5.13  
388.29  
5.13  
7 = on Ret.

387.87  
5.65  
6.9  
387.59  
5.93  
1.9  
gut.  
388.20  
5.32  
1.9  
Top  
388.34  
5.18

387.98  
5.54  
5  
388.23  
5.29  
Top  
387.66  
5.86  
gut.  
388.33  
5.19  
6  
walk  
388.46  
5.06  
10.3

388.21  
5.31  
Top  
387.59  
5.93  
gut.

393.52 ✓

Cont. P. 22

T.P. 6.14 392.94 6.22 386.86

10 + 99.2 =  $\pm$  Cleanout

10 + 76.72 =  $\pm$  33<sup>rd</sup>

10 + 46.72 = E.L. 33<sup>rd</sup>

10 + 00

9 + 50

9 + 00

8 + 50

9 + 00

From P. 17

Cont. from P. 17 393.01

Cont.  
P. 22

20

Lt			Rt		
386.63 <u>6.38</u> $\pm$	386.27 <u>6.24</u> $\pm$	386.90 6.12 10	386.73 6.29	386.16 6.86 6.5 9ut.	386.73 6.29 6.5 Top
386.78 <u>6.23</u> $\pm$	386.52 <u>6.19</u> $\pm$	386.97 6.05 10	386.76 6.26	386.52 6.48 6	386.82 6.20 10.5 = 21.8 cut.
386.86 <u>6.15</u> $\pm$	386.54 <u>6.07</u> $\pm$	387.34 5.68 10	386.88 6.14	386.54 6.48 6 9ut.	387.17 5.85 6 Top
387.08 <u>6.23</u> $\pm$	386.19 <u>6.22</u> $\pm$	387.57 5.45 10	387.16 5.86	386.79 6.23 6 9ut.	387.50 5.52 6 Top
387.25 <u>5.76</u> $\pm$	386.88 <u>6.13</u> $\pm$	387.79 5.23 10	387.26 5.76	386.82 6.18 6 9ut.	387.60 5.42 6 Top
387.53 <u>5.48</u> $\pm$	387.16 <u>5.85</u> $\pm$	388.02 5.00 10	387.99 5.53	387.07 5.95 6 9ut.	387.72 5.30 6 Top
387.72 <u>5.29</u> $\pm$	387.29 <u>5.72</u> $\pm$	388.17 4.85 10	387.73 5.29	387.15 5.87 6 9ut.	387.93 5.09 6 Top
387.81 <u>5.20</u> $\pm$	387.93 <u>5.58</u> $\pm$	388.37 4.65 10	387.84 5.18	387.35 5.67 6 9ut.	388.19 4.83 6 Top

393.01

393.02  $\checkmark$

Levels Around Prop. 20' Rad. Ret.  
 Inlet #7 - N.W. Cor. Adams + 33<sup>rd</sup>

50' W. along N. eb. Adams

E.C. = 8' W. of W.L. 33<sup>rd</sup>

3/4

⊕

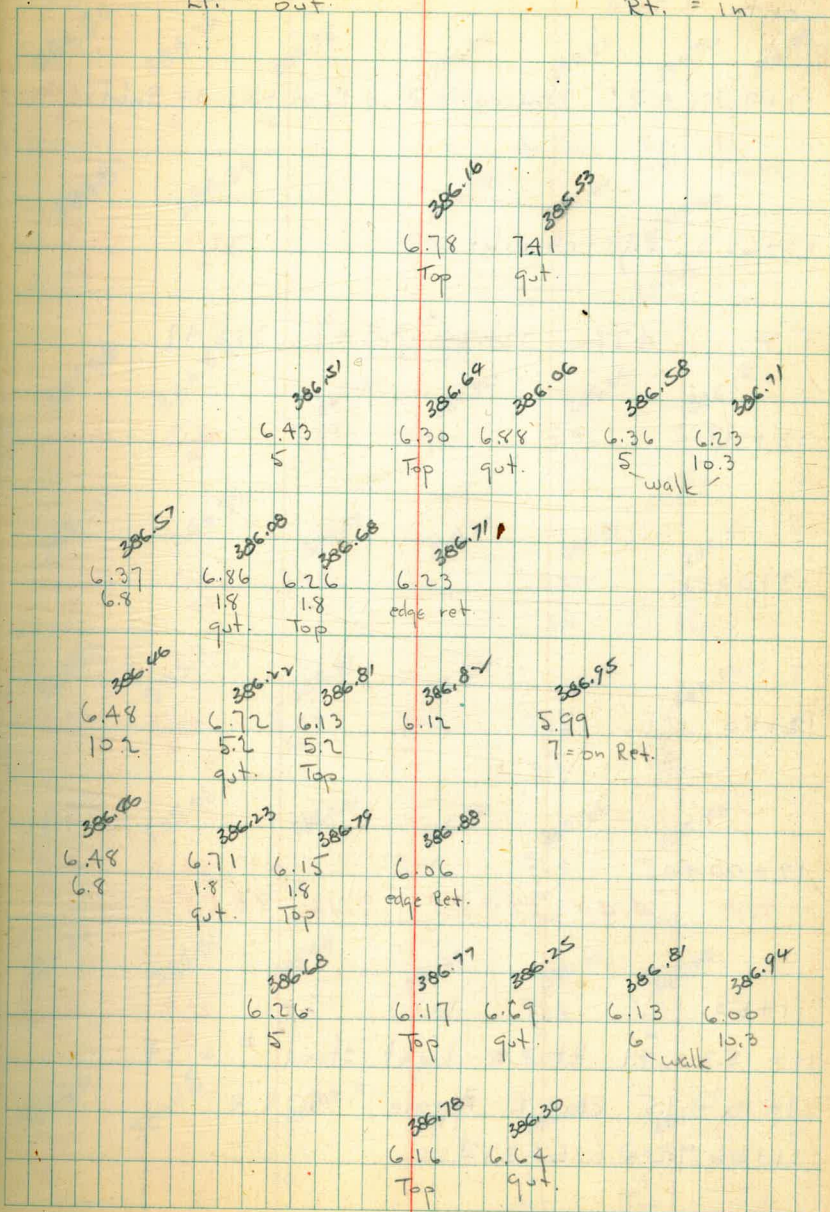
1/4

P.C. = 8' N. of N.L. Adams

50' N. of P.C. along W. eb. 33<sup>rd</sup>

Lt. = out

Rt. = in



√ 392.94 - P. 20

Cont. P. 25

13+71.91 = EL Bancroft = .4 E. of Headwall Inlet.

13+68.3 Ely. - cb. inlet

T.P. 4.77 390.24 7.47 385.47

13+35

13+00

12+50

12+00

T.P. 4.40 390.29 7.12 385.89

11+50

11+15.3 - 8.1 Rt. = £ Light stand. # 6724

11+10 - 7.5 Rt. = £ P. pole # 3538 R

11+06.72 = W.L. 33d

Cont. from P. 20 393.01

Cont. P. 25

22

Lt.				Rt.			
384.80 <u>5.49</u> G	384.36 <u>5.93</u> G	385.13 5.11 10	384.87 5.37	384.93 5.31 Cor. Inlet	384.90 5.34 Top Inlet	383.74 6.50 FL Culvert	
384.83 <u>5.46</u> £	384.34 <u>5.25</u> G		384.78 5.46	384.44 5.80 Cor. Inlet FL	384.30 5.94 6 = Gut. + FL		
384.96 <u>5.33</u> £	384.59 <u>5.20</u> G	385.36 7.58 10	384.96 7.98	384.53 8.41 6 gut.	385.16 7.78 6 Top		
385.23 <u>5.06</u> £	384.85 <u>5.44</u> G	385.59 7.35 10	385.27 7.67	384.81 8.13 6 gut.	385.36 7.58 6 Top		
385.50 <u>4.72</u> £	385.11 <u>5.18</u> G	385.91 7.03 10	385.57 7.42	385.09 7.85 6 gut.	385.62 7.32 6 Top		
385.19 <u>4.50</u> £	385.46 <u>4.83</u> G	386.22 6.72 10	385.80 7.14	385.26 7.68 6 gut.	385.90 7.04 6 Top		
386.26 <u>6.75</u> £	385.80 <u>7.41</u> G	386.69 6.25 10	386.29 6.65	385.70 7.24 6 gut.	386.15 6.79 6 Top		
386.60 <u>6.41</u> £	386.18 <u>6.33</u> G	386.93 6.01 10	386.66 6.28	386.08 6.86 6 gut.	386.67 6.27 6 Top		
		393.01 From P. 20					392.94



Levels Around Prop. 20' Rad. Returns - Inlets  
# 8 + # 9

50' N. - along E. cb Bancroft

E.C. = 8' N. of N.L. Adams

3/4

1/2

1/4

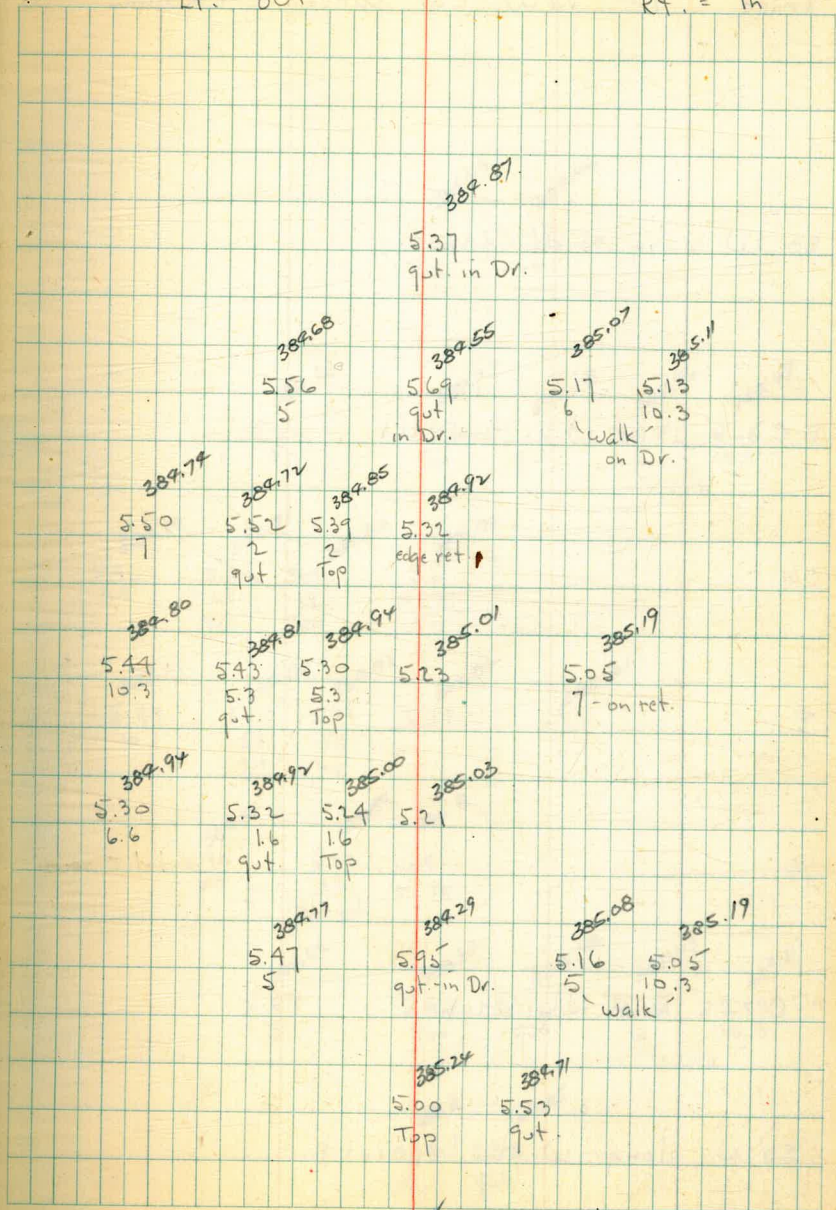
P.C. = 8' E. of E.L. Bancroft

50' E. of P.C. along N. cb Adams

Inlet # 8 = N.E. Cor. Bancroft + Adams

Lt. = out

Rt. = in



390.24 - P.22

Inlet # 9 = N.W. Cor. Bancroft + Adams

50' W. along N. cb Adams

E.C. = 8' W. of W.L. Bancroft.

3/4

⊕

1/4

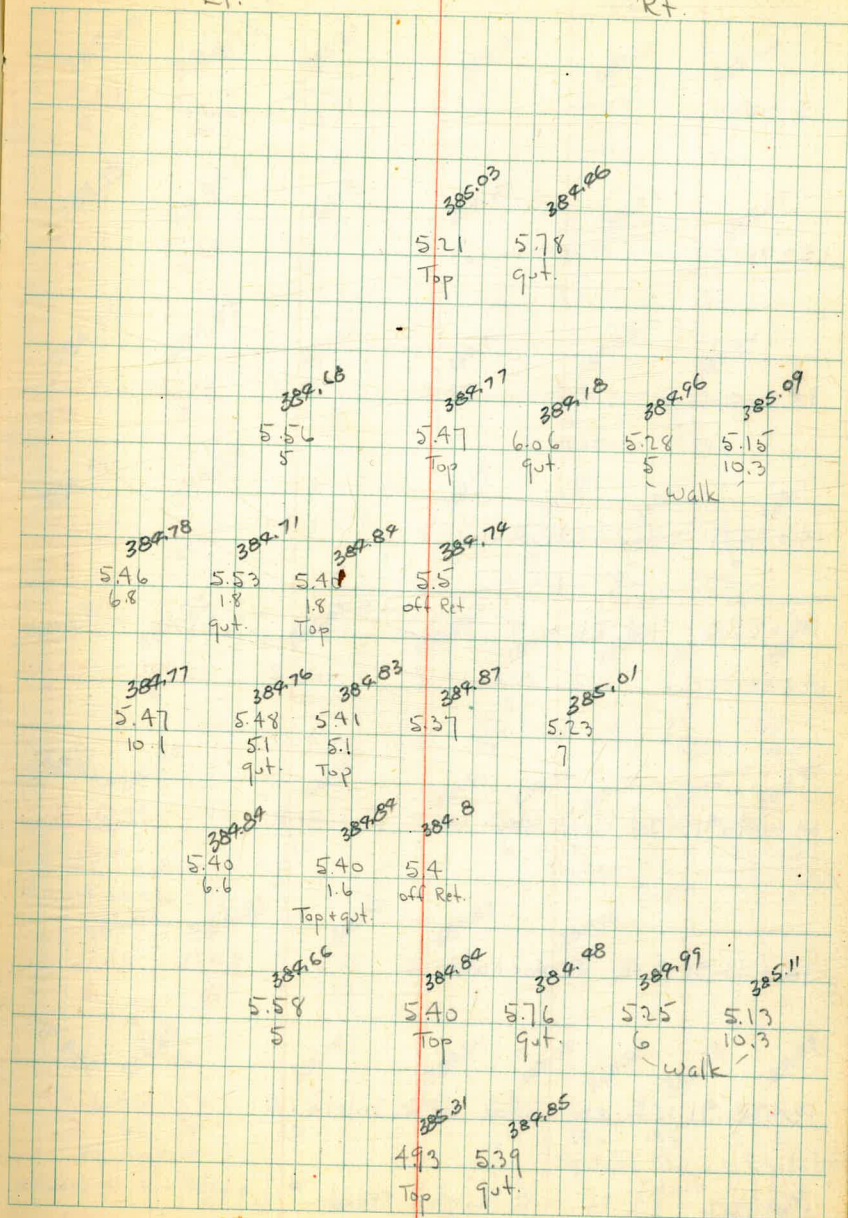
P.C. = 8' N. of N.L. Adams

50' N. along W. cb Bancroft.

24

Lt.

Rt.



390.24 ✓

15+50

15+00

14+60

14+35.91 = for Wly. Inlet.

14+35.2 - 7.4 Rt. =  $\pm$  P. pole # J.R. 3248

14+31.91

14+19.91 = W. cb. = for F.L. Culvert.

14+01.91 =  $\pm$  Bancroft

13+83.91 = E. cb. - for F.L. Inlets

13+72.2 - 8.2 Rt. =  $\pm$  Light stand # 6720

Cont. from P. 22

390.29 From P. 22

Lt.			Rt.		
385.00 <u>5.29</u> $\pm$	384.72 <u>5.57</u> $\pm$	385.31 4.73 10	384.99 5.25	384.61 5.63 6 9ut.	385.24 5.00 6 Top
384.79 <u>5.50</u> $\pm$	384.53 <u>5.76</u> $\pm$	385.19 5.05 10	384.85 5.39	384.97 5.77 6 9ut.	385.02 5.22 6 Top
384.77 <u>5.52</u> $\pm$	384.43 <u>5.86</u> $\pm$	385.12 5.12 10	384.76 5.48	384.33 5.91 6 9ut.	384.92 5.32 6 Top
384.72 <u>5.57</u> $\pm$	384.26 <u>5.03</u> $\pm$		384.79 5.45	384.34 5.90 6 Cor. Inlet.	384.77 5.47 6 Top ch.
384.76 <u>5.53</u> $\pm$	384.33 <u>5.76</u> $\pm$	385.08 5.16 10	384.83 5.41	384.61 5.63 6 Cor. Inlet Top	384.59 5.65 6 Top Inlet.
384.58 <u>5.71</u> $\pm$	383.25 6.99 62 FL outlet Culvert at S.L.	385.07 5.17 10	384.90 5.34	384.75 5.49 6 Top Inlet	383.43 6.81 6 FL Culvert.
384.93 <u>5.36</u> $\pm$	384.81 <u>5.48</u> $\pm$	385.06 5.18 10	384.89 5.35	384.77 5.45 6	384.90 5.84 22=9ut. = FL Inlet.
384.93 <u>5.36</u> $\pm$	384.71 <u>5.57</u> $\pm$	385.09 6.96 62 FL outlet culvert at S.L. Adams	384.94 5.30	384.74 5.45 6	384.54 5.70 22.6 FL Inlet = 9ut.
				384.62 5.60 18.6 Top Inlet	384.53 6.71 18.6 FL Culvert

390.19  
 $\pm$  From P. 22

390.24 ✓

18+50

18+00

17+64.2-8.2 Rt. = \$ Light stand # 6714

17+58-7.6 Rt. = \$ P. pole # P 3338 R

17+57.18 = W.L. 32<sup>nd</sup>

17+49.7 = \$ Cleanout

17+27.18 = \$

16+97.18 = E.L. 32<sup>nd</sup>

16+50

T.P. 5.99 391.62 4.66 385.63

T.P. 5.45 391.08 4.61 385.63

16+00

390.29

386.30 5.32 \$	386.06 5.56 \$	386.58 4.50 10	386.42 4.66	385.99 5.09 9ut.	Rt. 386.55 4.53 6 Top	
386.07 5.55 \$	385.89 5.23 \$	386.29 4.84 10	386.14 4.96	385.85 5.23 6 9ut.	386.36 4.72 6 Top	
385.68 5.74 \$	385.95 6.12 \$	385.88 5.20 10	385.70 5.38	385.39 5.69 6 9ut.	385.95 5.13 6 Top	
385.59 6.03 \$	385.38 6.24 \$	385.85 5.23 10	385.62 5.46	385.37 5.71 6.5 9ut.	385.89 5.19 6.5 Top	385.98 5.10 10.5 = 21.9 out.
385.51 6.11 \$	385.36 6.26 \$	385.76 5.32 10	385.52 5.56	385.37 5.71 5 = in 9ut.	385.58 5.50 10	
385.42 6.20 \$	385.26 6.36 \$	385.70 5.38 10	385.38 5.70	385.19 5.89 6 9ut.	385.84 5.24 6 Top	
385.29 6.33 \$	385.14 6.48 \$	385.60 5.48 10	385.31 5.77	385.08 6.00 6 = 9ut. in Dr.		
	<u>391.62</u>					
385.16 5.13 \$	384.99 5.20 \$	385.48 4.76 10	385.18 5.06	384.92 5.32 6 9ut.	385.48 4.76 6 Top	
	<u>390.29</u>					
			<u>391.08</u> ✓			
					<u>390.24</u> ✓	

Levels Around Prop 20' Rad. Ret at N.W.  
 Cor. Adams + 32<sup>nd</sup> - Inlet # 10

50' W. along N.cb. Adams

E.C. = 8' W. of W.L. 32<sup>nd</sup>

3/4

±

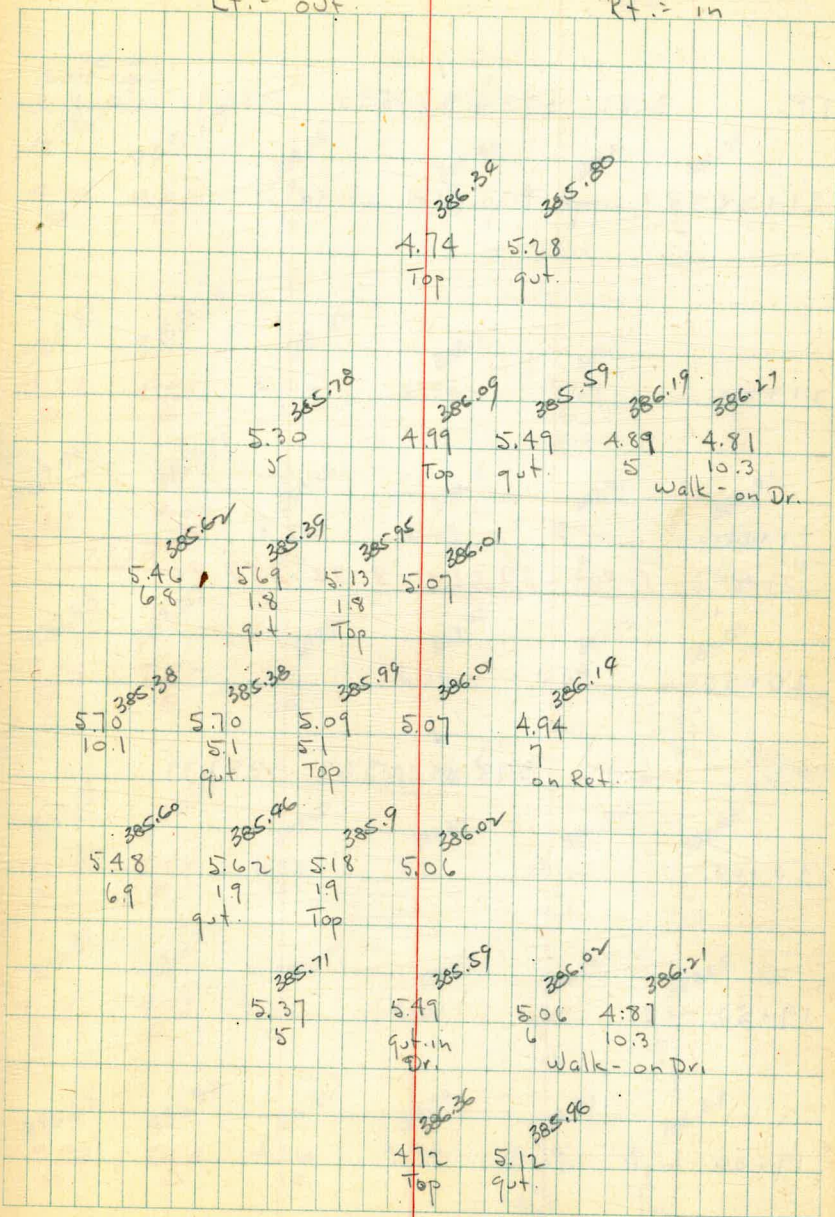
1/4

P.C. = 8' N. of N.L. Adams

50' N. of P.C. along W.cb. 32<sup>nd</sup>

Lt. = out

Rt. = in



T.P. 3.52 392.43 4.90 388.91

N.E. D.P. in  
Light Stand.  
Adams + Mt. View

21 + 88.90 = opp Prop. Cor. at 90°

21 + 50

21 + 00

T.P. 5.30 393.20 3.72 387.90

20 + 50

T.P. 6.42 393.81 3.69 387.39

20 + 00

19 + 50

19 + 00

391.62 From P. 26

L.

R+

388.30 4.90 E	388.25 4.95 G	388.68 5.13 10	392.43 5.34	388.47 5.60 6 gut	388.21 5.03 6 Top
388.21 4.99 E	388.14 5.06 G	388.96 5.35 10	388.27 5.54	388.12 5.69 6 gut. in Dr.	
387.91 5.22 E	387.71 5.49 G	388.25 5.56 10	388.17 5.64	387.91 5.90 6 gut.	388.91 5.40 6 Top
387.68 3.94 E	387.29 4.33 G	387.91 5.90 10	387.61 6.14	387.12 6.69 6 gut.	387.51 6.00 6 Top
387.25 4.37 E	386.95 4.67 G	387.60 3.48 10	393.81 3.71	386.92 4.16 6 gut.	387.63 3.45 6 Top
386.91 4.71 E	386.79 4.83 G	387.22 3.86 10	387.04 4.04	386.70 4.38 6 gut.	387.25 3.83 6 Top
386.62 5.00 E	386.36 5.25 G	386.92 4.16 10	386.74 4.34	386.79 4.79 6 gut.	386.87 4.21 6 Top
<u>391.62</u>		<u>391.08</u>			

23+14 = opp. lot Cor. at 90° - See sketch

23+01.6 = W. edge walk

22 + 97.2 = E. edge of Conc. walk (outs along curved walk)

22+86.2 = cb. face - W. cb. Mt. View (on curve)  
outs along cb. on curve. (see P. 66-67  
for add. outs)

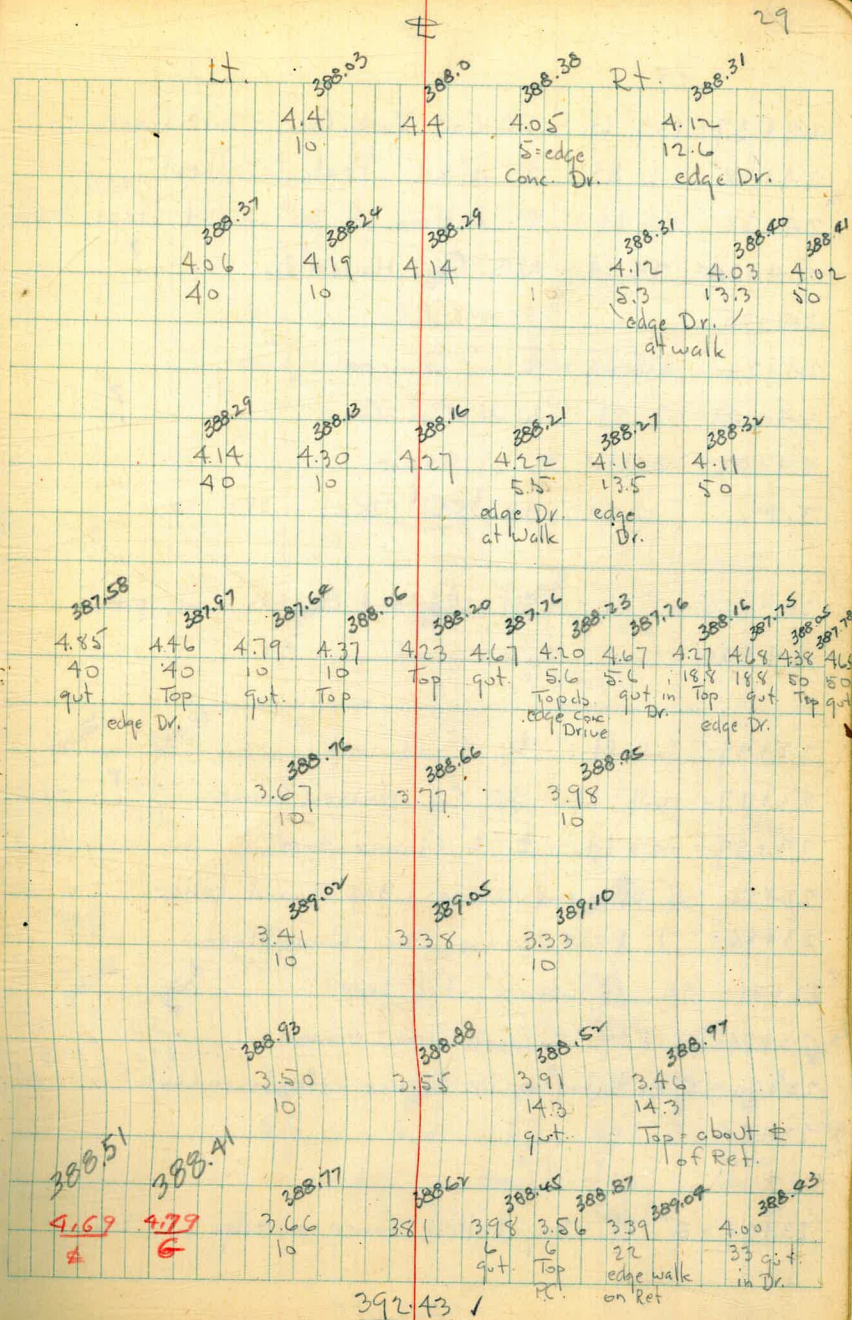
22+70

22+50

22+27.60 = Ang. 55° 32' 45" Rt. (sect. on split)  
Admits + Mt. View 4132 388.88 NE RR in lamp stck

22+10 = Opp. P.C. of 10' Rad. Ret. on Rt.

393.20



24+37- 13.9' Lt. = S.E. Cor. Doub. Gar. - Dirt floor  
 24+38- 1' Rt. =  $\pm$  4" x 4" Post. (clothes)  
 24+33- 4.9 Lt. =  $\pm$  Bottom of 30" Wood steps from House  
 24+30.5- 9.4 Lt. = N.E. Cor. House ?  
 24+25  
 24+24- 5.5 Lt. =  $\pm$  6" Quince  
 24+07- 7' Rt. = N.W. Cor. Gar. ?  
 24+02- 3' Lt. =  $\pm$  2" Apple  
 T.P. 222 387.52 7.13 385.30

24+00.5- 1' Rt. =  $\pm$  4" x 6" Wood clothes line post.  
 24+00

23+99- 1' Rt. =  $\pm$  4" Quince

23+97- 6.7- Lt. = S.E. Cor. House (frame) ?

23+89- 4.3 Lt. =  $\pm$  6" Quince tree

23+86- 5' Rt. = end Lattice + Beq. Board fence

23+86- 7' Rt. = S.W. Cor. Gar. - Conc. floor

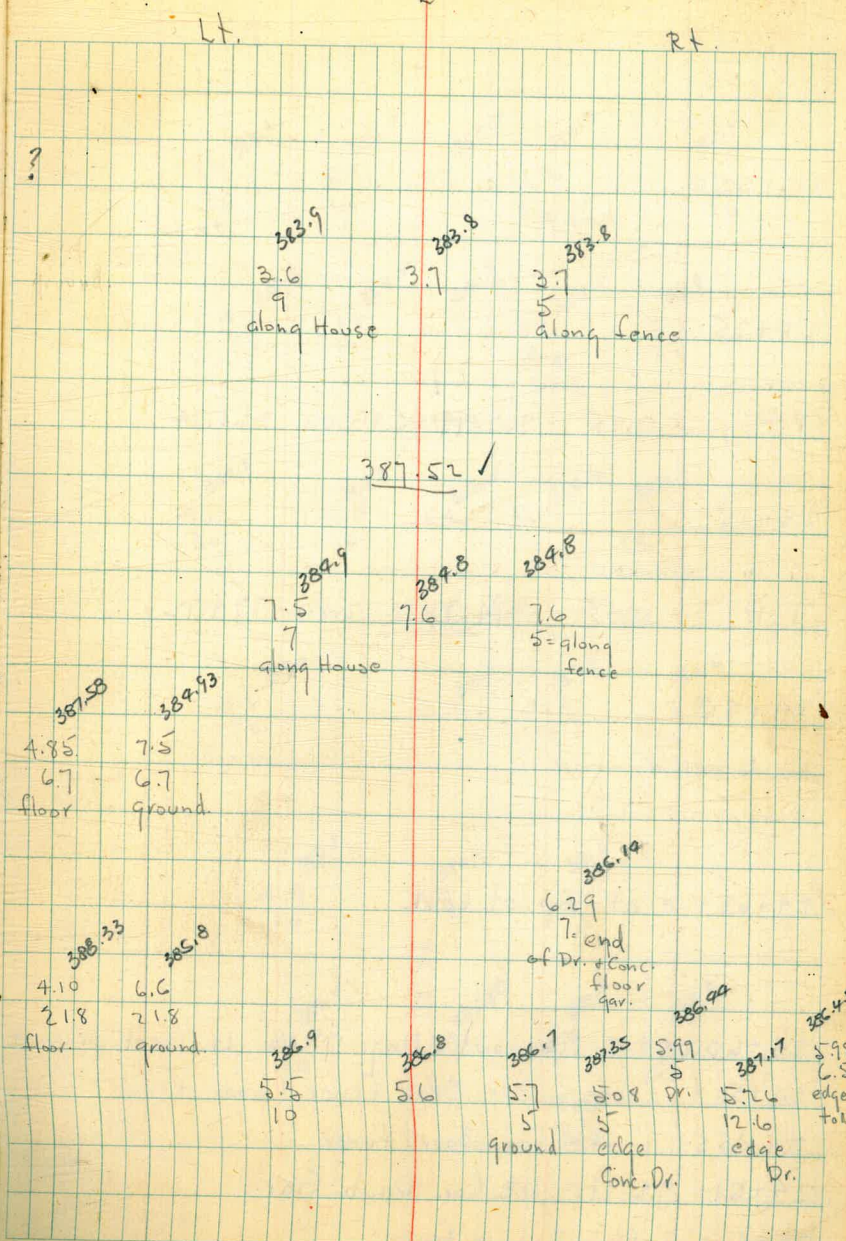
23+81- 9.6 Lt. =  $\pm$  6" fig tree

23+74- 2.18 Lt. =  $\pm$  Small frame house ?

23+70- 5' Rt. = Jog in Dr. - fence extends on Lot Line ?

23+50

23+24- 5' Rt. = Beq. Lattice fence on edge of Dr.



392.43 ✓



25+55

25+35

T.P. 0.25 361.99 13.03 361.74

25+15

T.P. 0.05 374.77 12.80 374.72

24+85

24+63 =  $\pm$  at Top of bank

24+60.08 =  $\pm$  Cleanout Ang. 17° 40' Lt. (sect. on split)

24+56 = Cross-Corr: Iron fence (poor cond.)

24+55 = 1' Rt. = Cor. Board fence

24+51 = 9.2 Lt. = NE Cor. Doub. Gar.

24+46 = 5' Rt. = Ang. in fence

Lt.

Rt.

358.8 355.1 353.7 350.7 361.7  
 3.2 6.9 8.3 11.3 0.3  
 35 10 5  $\pm$  wash 20  
 Toe of new fill

357.3 359.4 355.9 353.1 359.9  
 4.7 7.8 6.1 8.9 2.1  
 20 10 8  $\pm$  Wash 20

361.99 ✓

370.7 363.8 357.4 358.6 357.1  
 4.1 11.0 15.4 16.2 17.7  
 30 10 10 18  $\pm$  Wash

374.77 ✓

363.0 371.5 367.6 361.6  
 4.5 16.0 19.9 25.9  
 20 10 35  
 Top bank Bottom of wash

383.1 382.6 380.3  
 4.4 4.9 7.2  
 10 10

383.4 382.85 382.6 381.9  
 4.3 4.67 4.9 5.6  
 10 on Hub. 7 15  
 Top Bank

383.4  
 4.1  
 9.2  
 floor

387.52 ✓

27+80

27+50

27+20

26+85

T.P. 0.71 337.91 12.86 337.20

26+50

26+30

15+99.74 = Ang. 15° 49' 30"

T.P. 0.42 350.06 12.35 349.64

25+85

336.6 1.3 30	Lt.	333.7 4.2 10	329.4 8.5	323.0 14.9 17 ± wash	Rt.	333.4 4.5 35
336.0 1.9 30 Toe slope		332.8 5.1 10	329.7 8.2	325.2 12.7 14		325.0 2.9 30
334.0 3.9 30		324.4 13.5 18 Toe slope	323.7 14.2	323.8 14.1 7 ± wash		324.5 13.4 15
338.7 10.8 25 on slope		327.3 10.6 5 Toe slope	326.3 11.6	326.1 11.8 5 ± wash		326.0 11.9 13
			337.91 ✓			326.3 1.6 30
			340.8 9.3 20	331.4 14.7 5 Toe slope		328.1 22.0 10 edge wash
			338.7 20.4	329.7 20.4		328.1 22.0 20
			338.6 11.5 20 Toe slope	337.8 12.3 10		334.3 15.8 30
			335.7 14.9	331.7 14.4 12 ± wash		337.1 13.0 30
			345.9 4.2 25 Toe fill	343.4 6.7 10		337.6 12.5 4.5 ± Wash from E
			344.32 5.74 on Hub	342.8 7.3 5 ± Wash		350.0 0.1 20
			348.99 13.2 20 Toe fill	347.8 14.2 10		350.06 ✓
			346.7 13.3	346.7 15.3 6 ± wash		349.5 2.5 30
			361.99 ✓			

			4.91	388.27	388.26	P. 17
T.P.	6.33	393.18	2.79	386.85		
S.E. 7 ct. Bancroft + Adams			5.04	384.60		
	3.93	389.64	6.01	385.71		
T.P. for checking starting BM	2.81	391.72	4.55	388.91		P 28
	10.61	393.46		382.85		P. 31

check - from Hub 24+60.08 to B.M. at Mt. View + Adams

checked back to Hub 24+60.08 with hand level levels o.k.

29+45 =

28+85 - on line produced to show wash.

28+27.80 = Hub. End.

28+10

27.5 50	27.9 30	16.7 15	10.9
315.4	310.0	321.2	327.0
	± wash		
15.8 30	19.8 10	22.1 ± wash	3.1 30
	321.1	318.1	315.8
9.1 30	15.4 10	15.99 on Hub.	16.4 ± wash
	326.8	321.92	321.5
			337.2
6.6 30	12.7 15	15.6	17.9 5
	331.3	325.7	320.3
			320.10
			5.1 30
			332.8
			± wash

337.91 ✓



50' N. along E. cb. Suncrest (on curve)

E.C.

3/4

+

1/4

+2' = end of Ext. Ret.

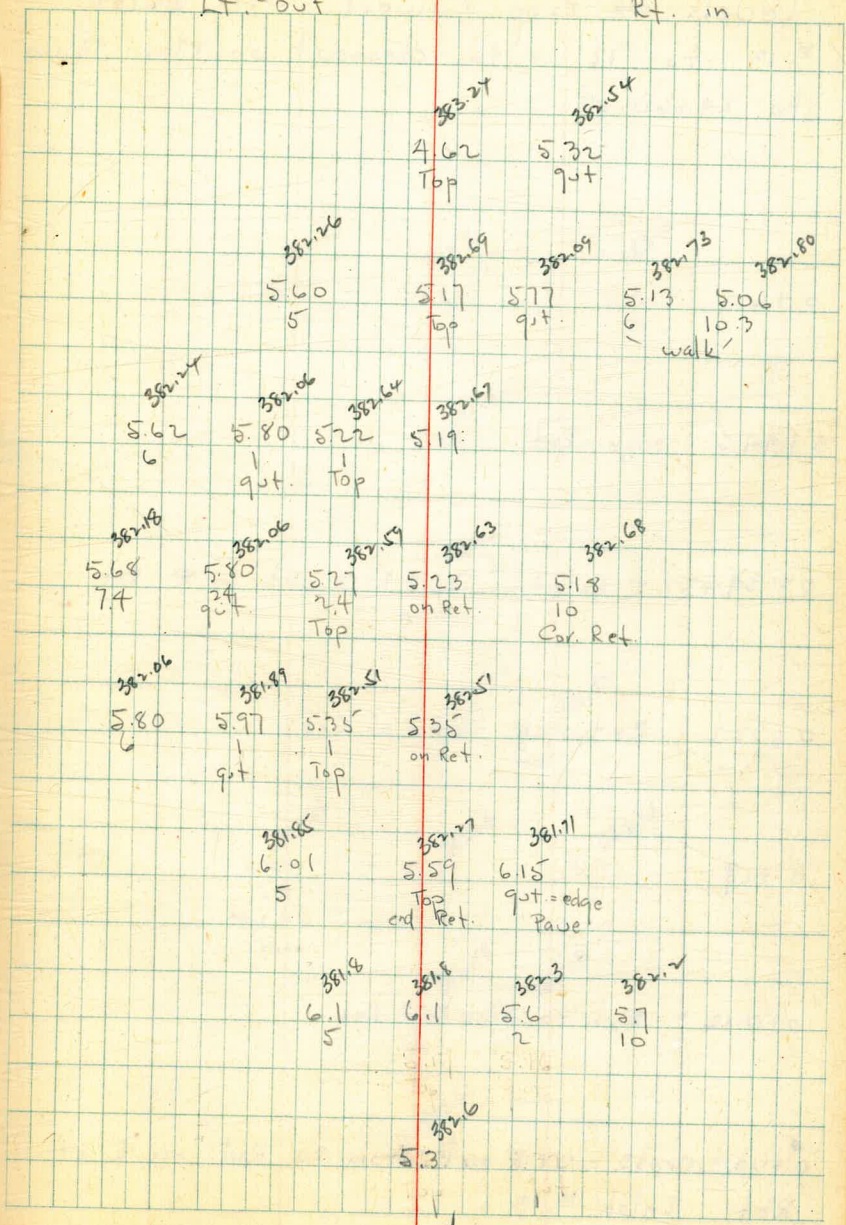
P.C.

30' E. along cb. Line Mondell  
Inlet # 13 = N.E. Cor.  
4 parts about 5.9' on chord.

35

Lt. = out

Rt. in



387.86 - P 34

Levels on Prop. Culvert from Inlet  
 # 13 to #12 + to cleanout on Main Drain  
 sta. 24+60.08

0+60

0+44.6 = edge Ret.

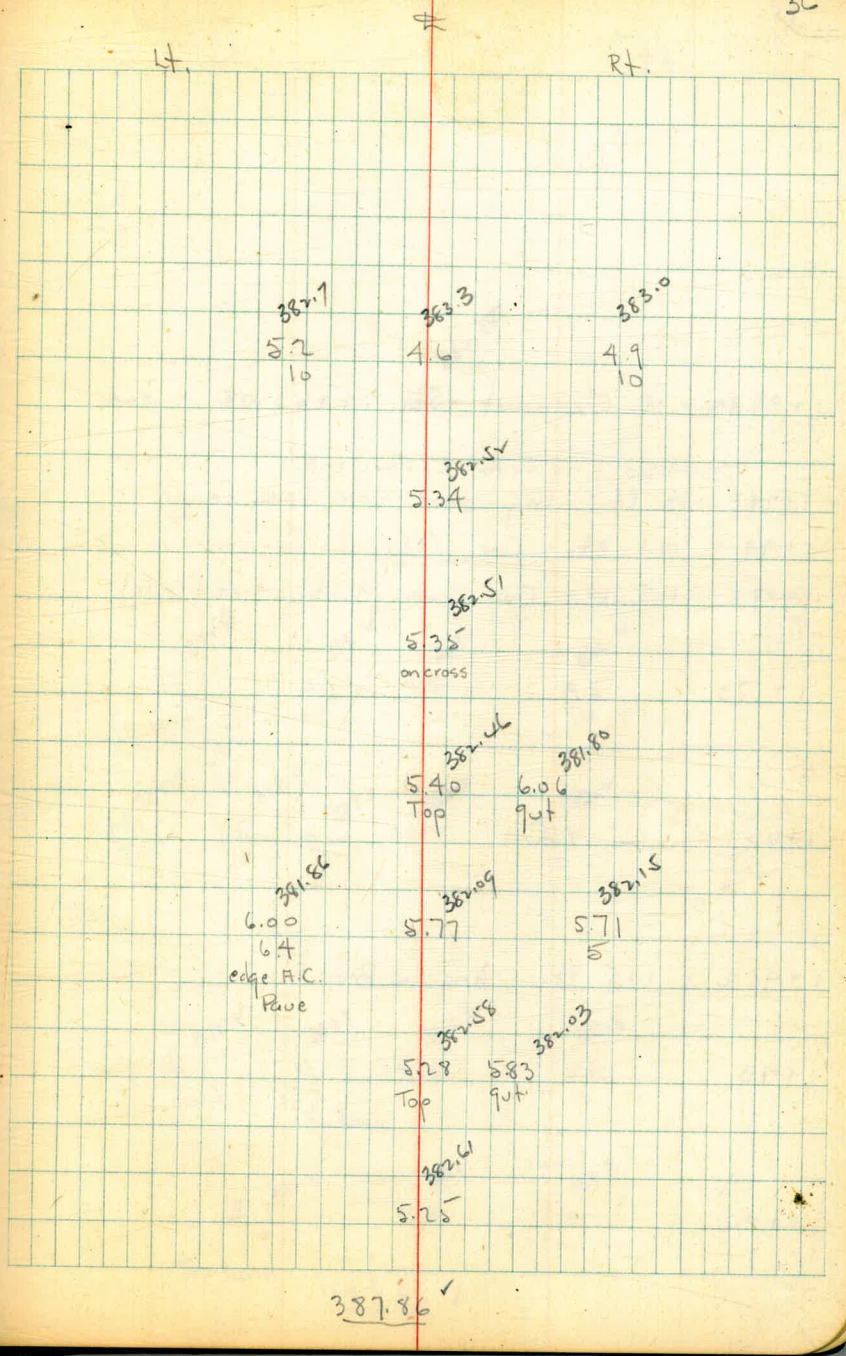
0+39.43 = Inlet # 12 - 21.8 out on Ret.

0+32.2 = Ext. cb. face of Ret.

0+17

0+0.12 = Ext. cb. face on Ret.

0+00 = cross - 21.8 out from 20' Rad. on E of  
 Ret. Inlet # 13



1+99.92 =  $\pm$  Cleanout - Sta. 2+60.08 = end.

(See line from E. for end.)

1+94 - 6.4 Rt. = Beg. poor Corr. Iron fence

1+94 - 11.1 Rt. = Cor. Gar.

1+78 - 11.9 Rt. = Cor. Gar. (doub. - dirt floor)

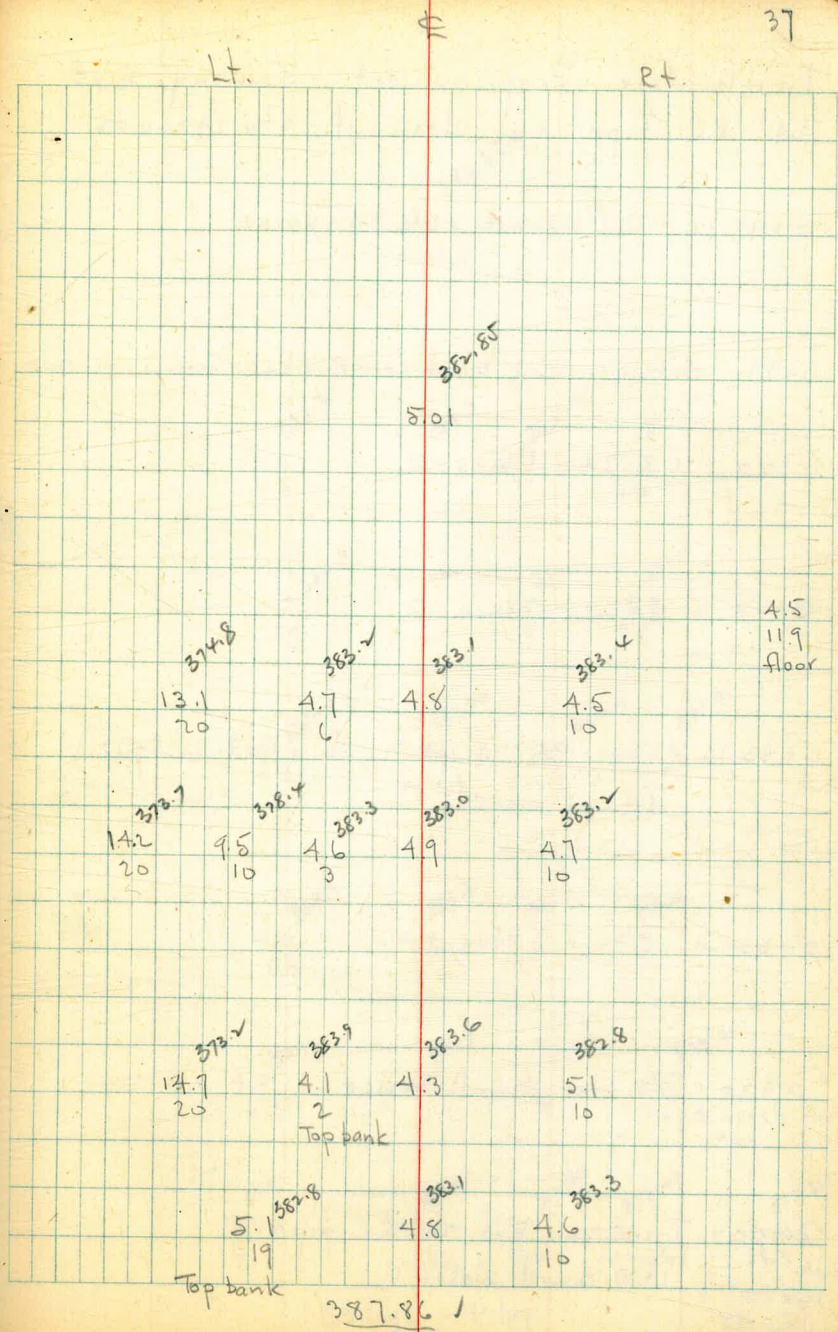
1+70

1+60

1+46.2 - 1.25 Rt. = Ang in Prop. line

1+40

1+00



Levels for Prop. culvert - Joining Ext.  
24" R.C. Pipe to cleanout - Sta. 24+60.08

0+99.72 = Cleanout - Sta. 24+60.08

0+92 - 4.4 Lt. = End Board fence + req. Corr. Iron fence

0+80 - 6.8 Lt. = fence

0+60 - 7.4 Lt. = Fence

0+43.12 = Ang. 34° 34' Rt. = Hub. (sect. on split)  
4.4 Lt. = fence

0+30 - 5.3 Lt. = fence

0+20 - 5.9 Lt. = Board. fence

0+00 = Joint in Ext. 24" R.C. pipe =  
6.7 Lt. = Board fence

Lt.

Rt.

Lt.	Rt.
5.01 on Hub.	382.85
4.6 6.8	383.3
5.2	382.7
5.7 3	382.2
17.6 20	370.3
4.2 7.4	383.7
5.0	382.9
5.8 4	382.1
15.8 25	372.1
3.9 4.4	384.0
4.21 on Hub	383.65
5.3 9	382.6
16.9 25	371.0
4.0 5.3	383.9
4.4	383.2
4.8 3	383.1
18.8 25 ± Wash	369.1
4.0 5.9	383.9
4.5	383.4
5.1 3	382.8
13.7 15 = ± Wash for Pipe	374.2
3.8 6.7	384.1
4.33 on stub.	383.53
7.17 Top Flush Pipe	380.69
9.39 estimated F.L.	378.47
10.05 8.3 along ext. pipe = F.L. outlet	377.81
387.86 - P. 37	



Add. Levels at Returns on S. side of Adams  
at Bancroft - curb culverts to be removed.

S.E. Cor. 0+00 = 50' S. of S.L. Adams  
curb line = base line sketch pg. 387

See P. 61

0+54 = PC of Ret. as Constructed.

0+50 = S.L. Adams = Top of Inlet (note: this Inlet Has grate)

0+46 = S. end Inlet

0+42 = PC Prop 20' Rad Ret.

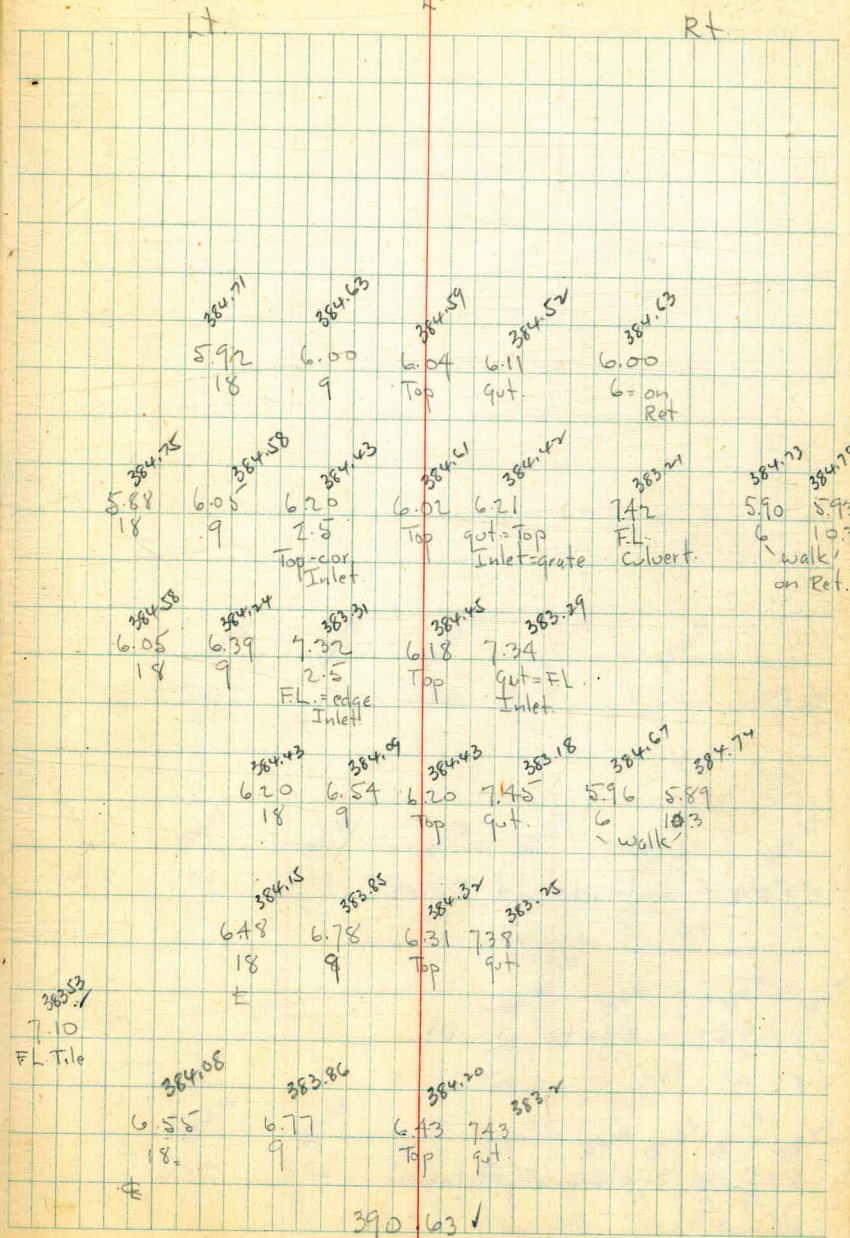
0+25

0+07.3 = outlet of 4" Tile drain in cb.

0+00 = 50' S. of S.L. Adams

B.M. 6.03 390.63

384.60 S.E. 7 ct.  
Bancroft  
Adams  
P. 33



Lt

Rt

Rt

0+70

0+64 = outside of Inlet

0+62 - Cont on Rt.

0+62 = S. cb. Line Adams

<sup>384.96</sup> 5.67 18	<sup>384.91</sup> 5.72 9	<sup>384.83</sup> 5.80 -	<sup>384.84</sup> 5.79 12	<sup>384.91</sup> 5.72 20			
<sup>384.79</sup> 5.84 18	<sup>384.74</sup> 5.89 9	<sup>384.56</sup> 6.07	<sup>384.46</sup> 6.17 12 = Top Cor. Inlet on grate	<sup>384.24</sup> 6.39 15.5 = FL. Inlet on grate	<sup>384.39</sup> 6.24 20		
			<sup>384.56</sup> 6.07 15.5 Top cb	<sup>384.49</sup> 6.14 15.5 FL. Inlet on grate	<sup>384.81</sup> 5.82 50 Top	<sup>384.41</sup> 6.22 50 gut	
<sup>384.74</sup> 5.89 18	<sup>384.68</sup> 5.95 9	<sup>384.52</sup> 6.11	<sup>384.51</sup> 6.12 8 Top	<sup>384.44</sup> 6.19 8 gut	<sup>384.53</sup> 6.10 12 Top	<sup>384.45</sup> 6.18 12 Top	<sup>384.40</sup> 7.23 12 = FL Inlet. Culvert
		<u>390.63</u> ✓	PC	cb.			

S.W. Cor. Adams + Baneroff.  
 0+00 = 50' S. of SL Adams - West cb. line = Baseline

0+62 = S. cb. line Adams

0+54 = P.C. as Const.

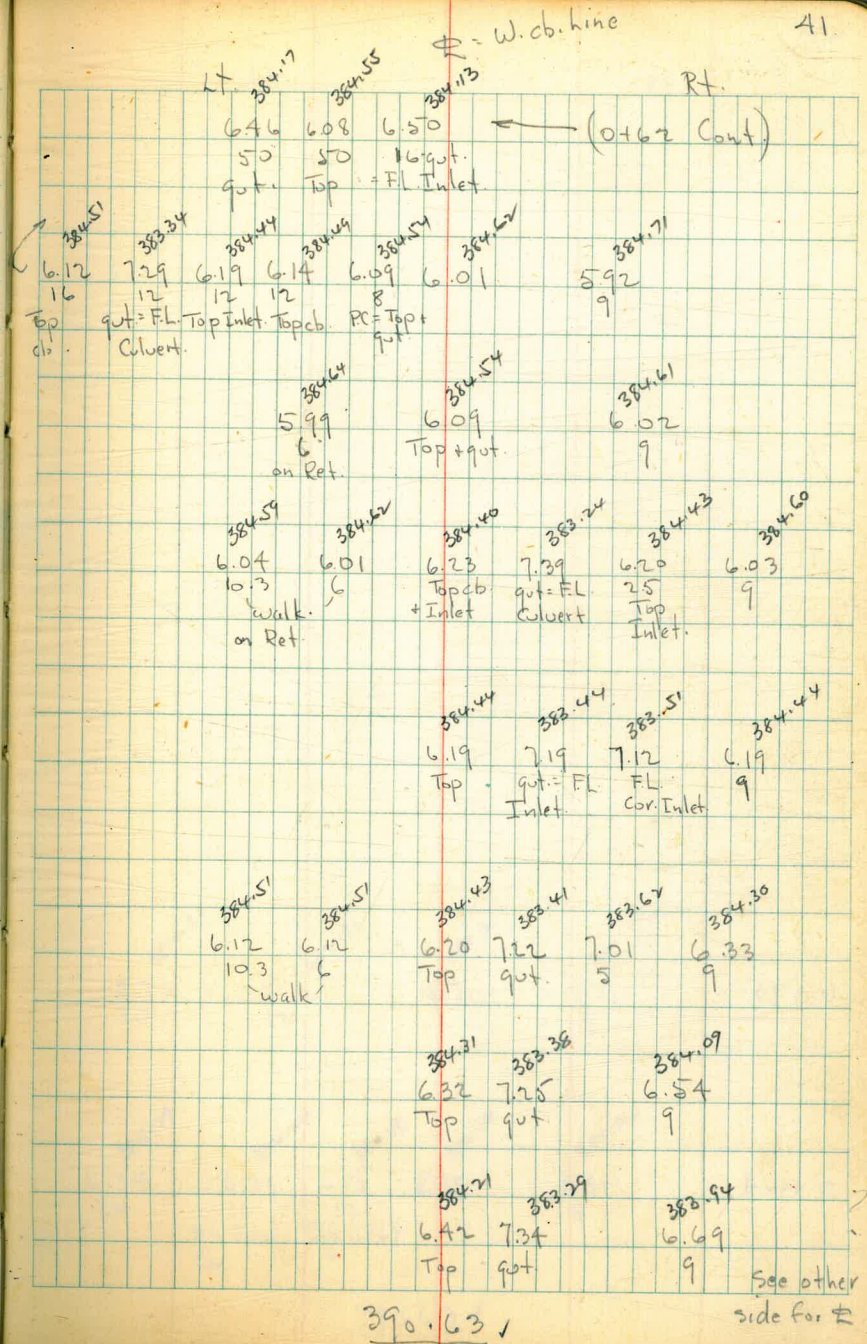
0+50 = SL Adams = Top Inlet.

0+46 = S. end Inlet

0+42 = P.C. Prop. 20' Rad. Ret.

0+25

0+00 = 50' S. of SL Adams along w. cb.



390.63 ✓

See other side for 2

0+70

0+64

Lt.

Rt.

384.87  
5.76  
20

384.91  
5.72  
12

384.91  
5.72

384.92  
5.71  
9

384.79  
6.34  
20

384.24  
6.39  
16  
F.L. Inlet  
Cor.

384.48  
6.15  
12  
Top inlet

384.64  
5.99

384.72  
5.91  
9

390.63 ✓

Add. Levels for S.E. Cor. Adams & Felton - Curb inlets to be removed.  
 0+00 = 50' S. of S.L. Adams - E. cb. = base line

Sec. P. 56

0+50

0+46

0+42 = P.C. Prop. 20' Rad. Ret.

0+25

0+22 =  $\pm$  4" Drain tile in cb.

0+00 = 50' S. of S.L. Adams on E. cb.

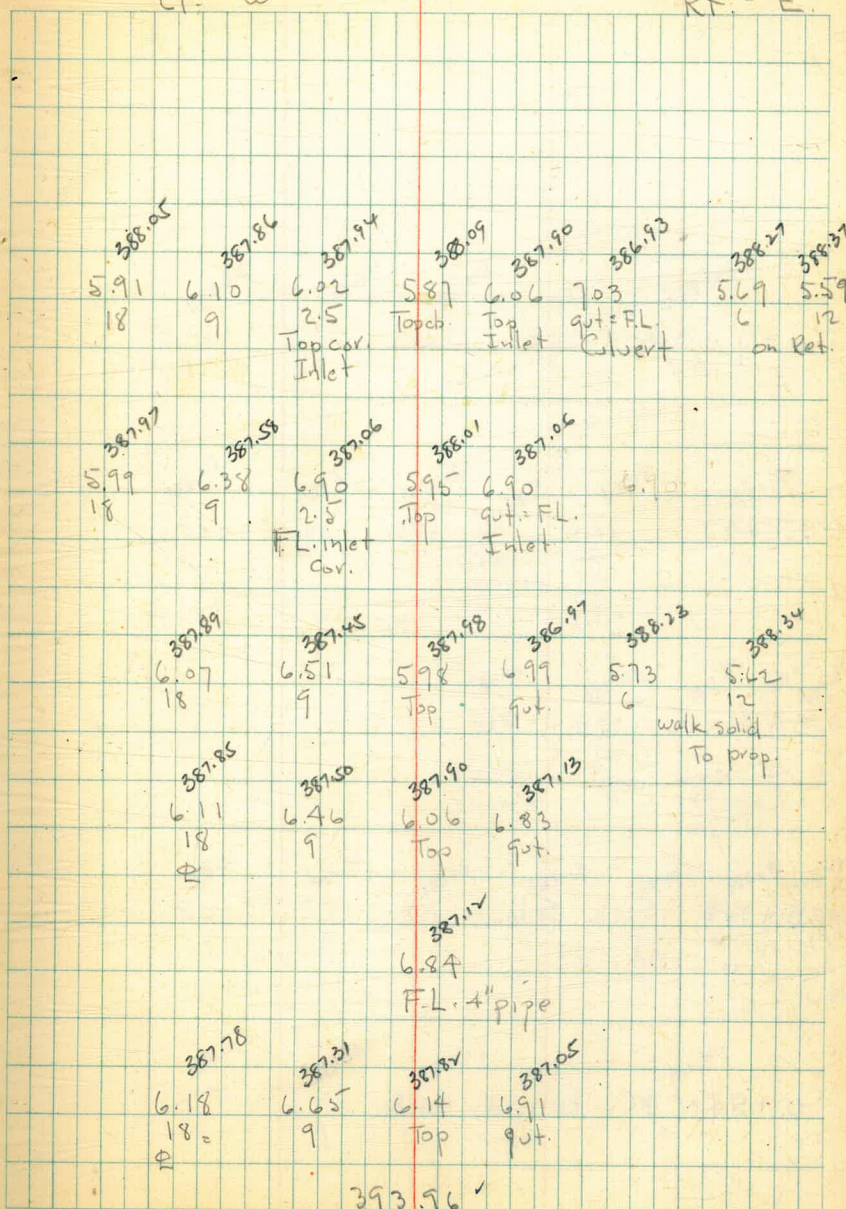
B.M. 5.70 393.96 ✓  
 388.26 ✓ NW Felton + Adams

Lt. - W

$\Phi$  = E. cb. Felton

43

Rt. - E.



0+70 = end.

0+64

0+62 Cont. on Rt.

0+62 = S. cb Adams

0+54 = P.C. Ret. as Const.

Lt.

Rt.

388.55	388.54	388.48	388.41	388.45
5.91	5.42	5.48	5.55	5.51
18	9		12	20

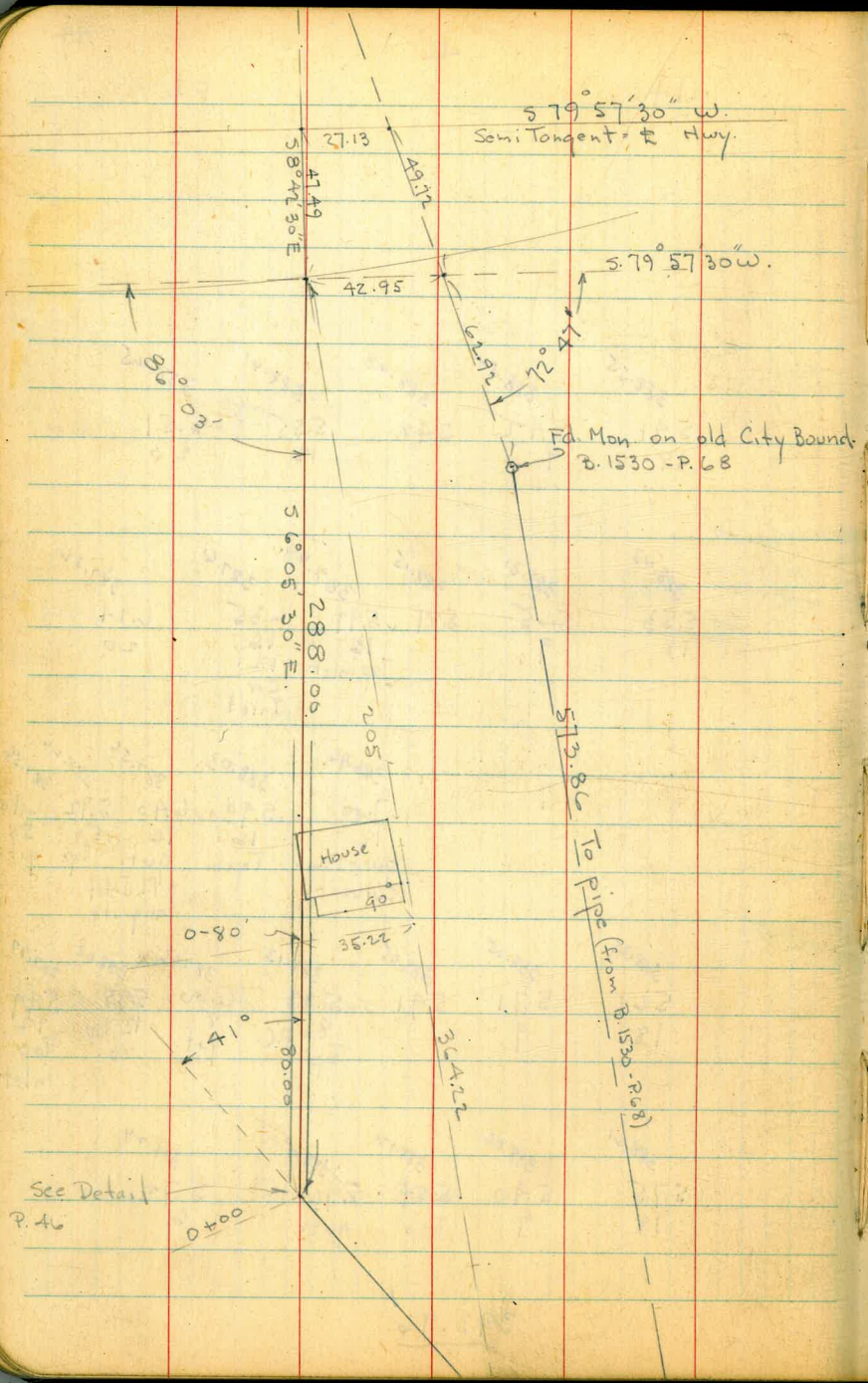
388.43	388.31	388.15	387.99	387.61	387.82
5.53	5.65	5.81	5.97	6.35	6.14
18	9		16	16	20
			Top Inlet	FL. Cov Inlet	

386.96	388.03	387.56	388.24	387.56
7.50	5.93	6.40	5.72	6.20
12	16	16	50	50
Gut. FL. Culvert	Topch.	Gut. = FL Inlet on grate	Top	Gut.

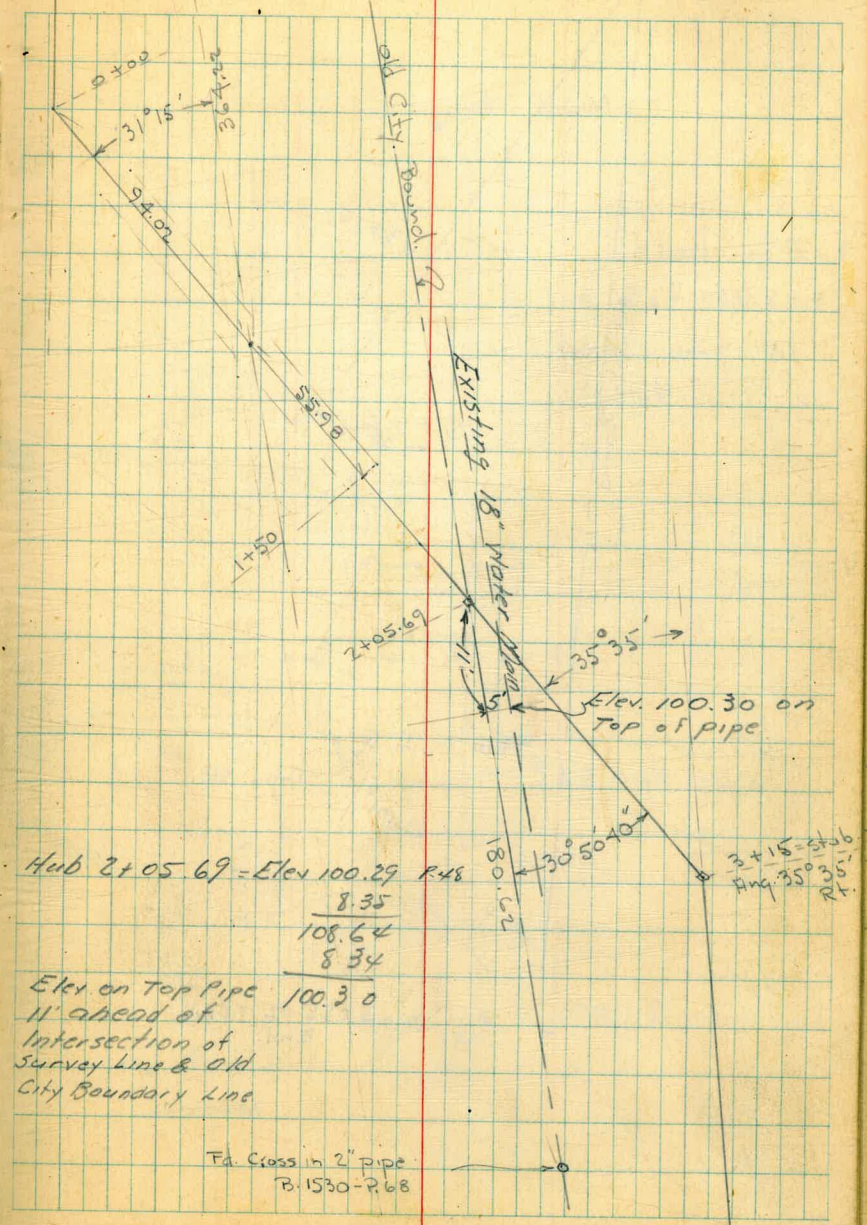
388.35	388.25	388.05	388.13	387.96	388.08	387.97
5.61	5.71	5.91	5.83	6.00	5.88	5.99
18	9		8	8	12	12
			Top PC	Gut.	Top cb	Top Inlet

388.21	388.06	388.12	388.0	388.24
5.75	5.90	5.84	5.96	5.72
18	9	Top	Gut.	6

393.96



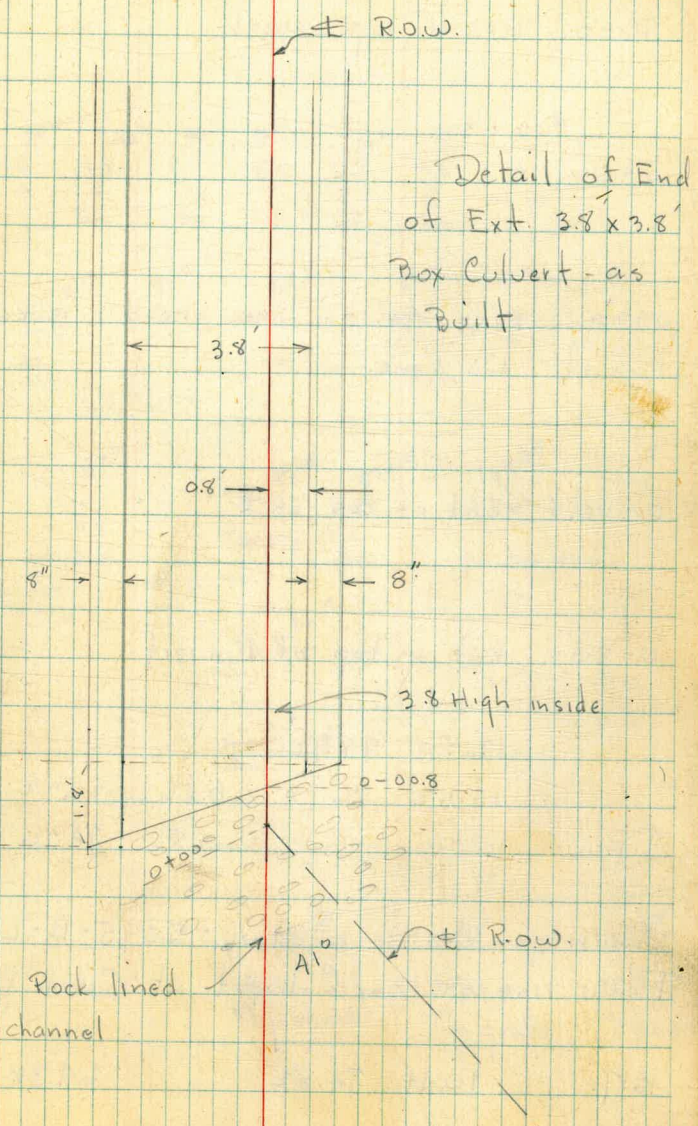
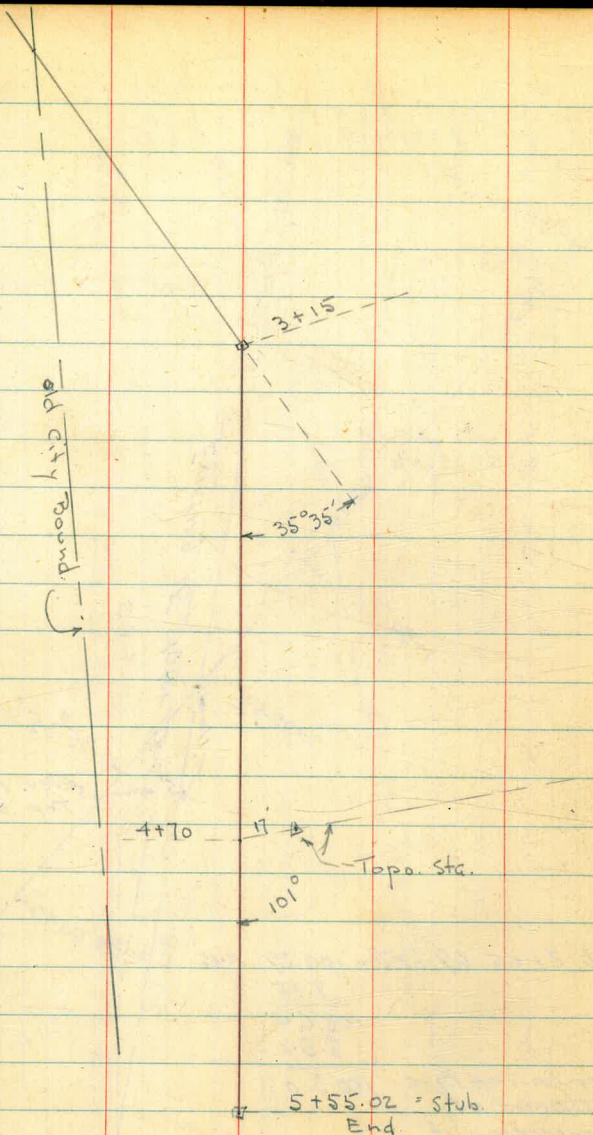
See Detail  
P. 46



Hub 2+05.69 - Elev 100.29 R48  
 8.35  
 108.64  
 8.34  
 Elev on Top Pipe 100.30  
 11' ahead of  
 Intersection of  
 Survey Line & Old  
 City Boundary Line

Fa. Cross in 2" pipe  
 B. 1530 - P. 68

3+15 = stab  
 Ang. 35° 35'  
 Pt.





INDEXED

Levels for Drain Survey - Elev. of  
 Ext Box Culvert and  $\pm$  levels for  
 Prop. Drain up wash.

0+50

0+00 - outs - 90° to Line ahead - in Rock lined  
 channel - No Conc.

0-00.8 = End of Box on  $\pm$

0-80 = Rod on top of Culvert

12.50 98.72

12.52 86.78 0.56 86.22

T.P.

0.56 74.26 ✓

shown on N. side of Hwy - 5095-B-L Sheet 2  
 Flow line of Box Culvert at Catch Basin

B.M.

10.44 74.82

64.38 B.M. 17  
 cross on MH  
 B 1530-P25  
 B-832-35

Lt.  $\pm$  Pt.

94.1	93.9	90.7	90.7	91.0	94.2	94.6
4.6	4.8	8.0	8.0	7.7	4.5	4.1
10	4	0.8		2.7	5	10
	Top	Bot.		Bot.	Top	
91.0	91.3	88.0	88.0	88.7	91.3	91.4
7.7	7.4	10.7	10.7	10.5	7.4	7.3
10	2.5	1		2.7	4	10
	Top	Bot		Bot.		

87.91	91.34	87.92	87.97
10.81	6.33	10.80	10.75
0.8			3
Cor Box	Top box	FL Box	Cor. Box - end
FL.			FL.

85.16  
 13.86

98.72 ✓

55.76	63.92	64.92
19.06	10.90	9.90
FL. Culvert.	Top grate	Top curb

74.82 ✓

T.P. 12.63 122.25 0.51 109.62

2+90

2+50

2+05.69 = Boundary Int <sup>Hub</sup> 9.84 100.29 on Hub

2+00 - in wash

1+70

1+50 - on Hub 12.34 97.79 on Hub

1+43 = end Rock Lined channel

T.P. 11.56 110.13 0.15 98.57

1+00

Lt.

Rt.

122.25 ✓

108.6 10 10	108.6 4	105.9 4.2	104.7 5.4 3 Wash	106.7 3.4 10
	105.0 5.1 10	104.7 5.4	102.9 7.2 10 Wash	
102.8 7.3 10	102.5 7.6 2	100.0 10.1 Wash	100.0 10.1 7	101.9 8.2 10
	101.0 9.1 10	100.1 10.0	99.7 10.4 5	97.8 12.3 8 Wash
99.6 10.5 10	99.6 10.5 4.5 Top	96.9 13.2 1 Bot	96.9 13.2	97.1 13.0 3.3 Bot
				100.1 10.0 6 Top
				101.4 8.7 10
		110.13 ✓		
97.4 13 10	97.0 17 4.3 Top	94.1 4.6 0.5 Bot	94.1 4.6	94.2 4.5 3.2 Bot
				96.9 1.8 6 Top
				97.9 0.8 10
		98.72 ✓		

4+80

T.P. 12.58 134.41 0.42 121.83

4+50

4+30

4+10

3+80

3+50

3+25

3+15 = Ang. 35° 35 Rt. 12.17 110.08 on Hob  
Sect. on split

Lt.

Rt.

5.8 122.6  
15

11.7 122.7  
7

8.5 125.9  
7

14.0 120.4  
15  
wash

134.41 ✓

124.8  
+2.5  
10

14 120.8

0.7 121.6  
10

5.8 116.4  
15

6.9 115.4  
10

4.2 118.0

3.1 119.2  
10

7.4 114.9  
15

8.8 113.4  
5

5.0 117.2

5.7 116.6  
10

8.4 113.8  
26  
wash

10.7 111.6  
10

8.0 114.2

8.0 114.2  
7

11.1 111.2  
10  
wash

8.4 113.8  
15

11.1 111.2  
10

12.8 109.4

11.4 110.8  
5

13.6 108.2  
9  
wash

10.8 111.4  
15

11.9 110.4  
10

14.8 107.4  
5

14.9 107.4

15.4 106.8  
4  
wash

14.0 108.2  
10

11.3 111.0  
10

12.17 110.8

13.3 109.0  
6

15.9 106.4  
11  
wash

122.25 ✓

check starting B.M.		9.95	64.36	64.38
	2.62	74.31	12.97	71.69
	0.20	84.66	13.15	84.46
	0.26	97.61	13.22	97.35
	1.01	110.57	12.31	109.56
T.P.	0.04	121.87	12.58	121.83

5+70 - in wash

5+60

5+55.02 = End = stub. 4.50 129.91

5+30

Lt Rt

126.3	126.4	126.1
8.1	8.0	8.3
6		6

130.7  
37

130.5	131.7	129.91	123.6
3.9	2.7	4.50	10.8
12	8		12 + wash

139.7	139.5	130.7	122.5
+ 5.3	4.9	3.5	11.9
20	5		12 + wash

134.41

Notes Reduced. Pgs. 1-50  
G. 26.46



Levels around S.W. Ret. - Adams +  
 Hawley - on Prop. 20' Rad. Ret. Divided  
 into 4 parts - Base Line or  $\Phi$  = curb face  
 of 20' Rad. Ret. - outs are on Radial Lines

$\Phi$

1/4

PC = 5' E. of W.L. Hawley

5' W. of PC = low spot in cb.

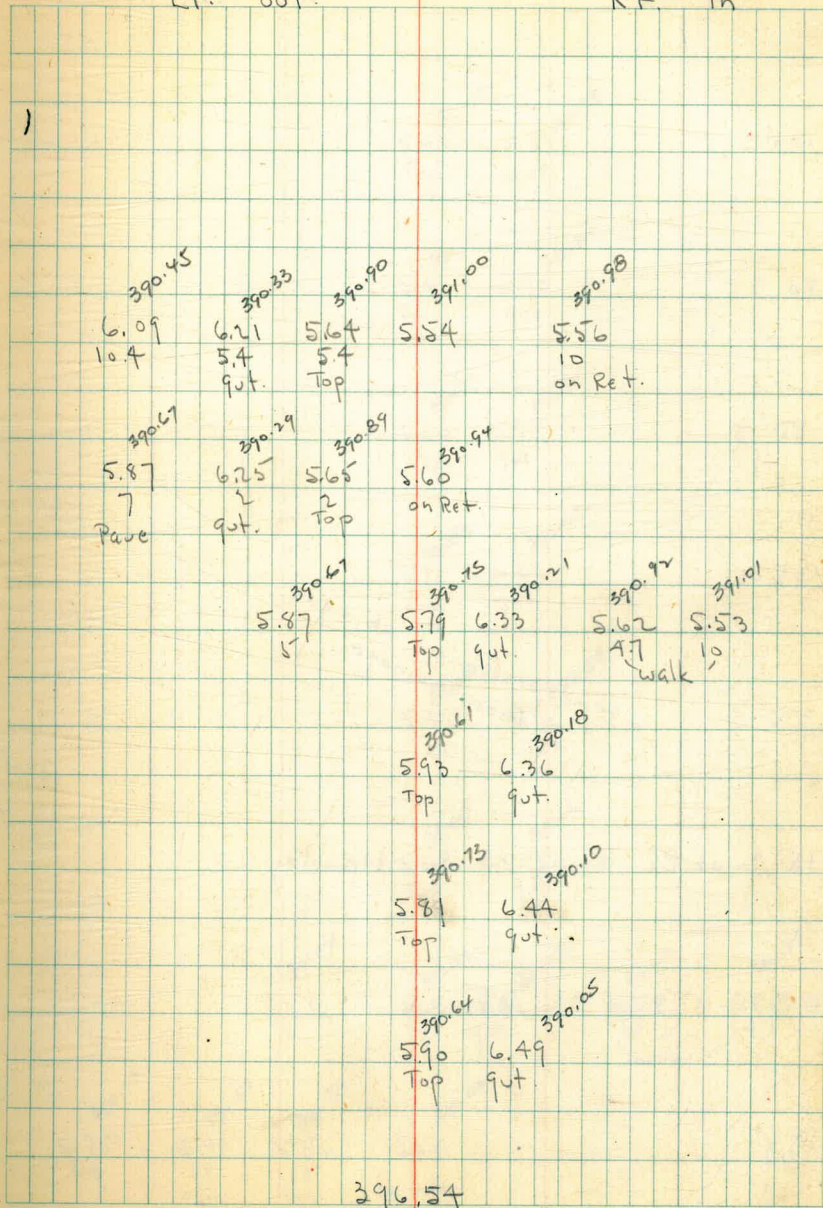
25' W.

50' W. of PC. 20' Rad. along S. cb. Adams.

B.M. 7.29 396.54 389.25

Lt. = out.

Rt. = in





Profile of cb. + Gut. on W. cb. Hawley  
 N. of N.L. Adams. 0+00 = P.C. Prop. 20' Rad.

Going N. 396.54 - P 53

0-08 = N.L. Adams	5.20	391.32	Top
	5.72	390.82	gut.
0+00 = P.C. = 8' N. of N.L.	5.16	391.38	Top
	5.70	390.82	gut.
0+12 = Approx. Brks.	5.27	391.27	Top
	5.80	390.72	gut.
0+23 " "	5.25	391.29	Top
	5.65	390.89	gut.
0+40 " "	5.34	391.20	Top
	5.88	390.66	gut.
0+50	5.41	391.13	Top
	5.87	390.67	gut.
0+65	5.25	391.29	Top
	5.65	390.89	gut.
0+85	5.09	391.25	Top
	5.56	390.98	gut.
1+00	5.09	391.25	Top
	5.58	390.96	gut.

Location of Poles, Trees, Lights +  
 Driveways - Hawley to Mt. View - along  
 N. cb. of Adams  
 Regular Sta. of  $\Phi$  Prop. Drain

0+81 - 8.3 Rt. = $\Phi$ 7" Acacia	
1+02 - 8.5 Rt. = $\Phi$ 9" Acacia	
1+20 - 8.3 Rt. = $\Phi$ 9" Acacia	
1+31 - 6' Rt. = $\Phi$ 5" Conc. walk - cb. to walk + back to house	
1+36 - 8.4 Rt. = $\Phi$ 7" Acacia	
1+38 - 6' Rt. = Beg. Conc. Dr. to Gar.	
1+53 " " End. " " " "	
1+54.5 - 8.4 Rt. = $\Phi$ Light Stand. # 6738	
1+56 - 6' Rt. = Beg. Conc. Dr. to Gar.	
1+90 - " " = End. " " " "	
1+97 - 7.5 Rt. = $\Phi$ P pole # P 3860 R	
2+30 - 6' Rt. = $\Phi$ 10' Conc. Dr.	
2+48 - 8.4 Rt. = $\Phi$ 5" Acacia	
2+64 - 6' Rt. = Beg. Conc. Dr. to Laundry	
2+84 - " " = End. " " " " Beg. Solid Conc. + cb. to prop.	
2+94 - 8.2 Rt. = $\Phi$ Light Stand. # 6736	
3+13 - 7.7 Rt. = $\Phi$ P. pole # J.R. 3408	
4+25 - 20.6 Rt. = $\Phi$ 5" Pipe light pole	
4+78 - 6' Rt. = end Dr. shown in sketch + Beg. Solid Conc. cb. to prop.	
5+01 - " " = End. " " " "	



5+37 - 7.5 Rt. =  $\pm$  P. pole # 3720 R  
5+62 - 9.1 Rt. =  $\pm$  Guy Pole - cable - to N.  
5+65.5 - 8.3 Rt. =  $\pm$  Light Stand. # 6732  
6+20.5 - 6' Rt. = Beg. Solid Conc. - cb. to prop. - to Felton

6+52 - 7.5 Rt. =  $\pm$  P. pole - No. #  
P. 17 - for Felton

8+36.5 - 8.1 Rt. =  $\pm$  Light Stand. # 6728

Note: Entire block Bet. Felton + 33<sup>rd</sup> is  
Solid Conc. - cb. to prop.

8+83.5 - 7.7 Rt. =  $\pm$  P. pole # 3644 R

9+76.5 - 8.2 Rt. =  $\pm$  Light Stand. # 6726

9+94 - 7.6 Rt. =  $\pm$  P. pole # 3606 R

11+81.2 - 6' Rt. =  $\pm$  3.5 Conc. walk

12+09 - 6' Rt. =  $\pm$  2.3 Conc. walk

12+13 - 7.6 Rt. =  $\pm$  P. pole # 3526 R

12+13 - 6' Rt. = beg. solid conc. from cb. to walk

12+20 - 9' Rt. =  $\pm$  5" Palm

12+31 - 9' Rt. =  $\pm$  4" Palm

12+39.5 - 8.2 Rt. =  $\pm$  Light Stand. # 6722

12+47.5 - 9' Rt. =  $\pm$  4" Palm

12+59.5 - 9' Rt. =  $\pm$  4" Palm

12+66 - 6' Rt. = End solid Conc. + Beg. Conc. Dr.

12+96.5 - 6' Rt. = End " "

13+21 - 7.4 Rt. =  $\pm$  P. pole # P3506 R

13+34.5 - 6' Rt. = Beg. Solid Conc. - cb. to walk

13+40 - 6' Rt. = End " " + Beg. Conc. Dr.

13+70 - 6' Rt. = End Conc. Dr.

14+85 - 6' Rt. = Beg. Solid Conc. - cb. to prop.

14+98.6 - 8.2 Rt. =  $\pm$  Light stand. # 6718

15+40 - 7.6 Rt. =  $\pm$  P. pole # J.R. 3224

16+17 - 6' Rt. = end solid conc.

16+21 - 7.4 Rt. =  $\pm$  P. pole # P3408 R

16+31 - 8.2 Rt. =  $\pm$  Lamp stand. # 6716

16+32 - 6' Rt. = Beg. Conc. Dr. To Ser. Sta.

16+68 = 6' Rt. = end " "

18+69 - 7.7 Rt. =  $\pm$  P. pole # P. 3324 R

19+04.8 - 8.3 Rt. =  $\pm$  Light stand. # 6712

19+62 - 7.6 Rt. =  $\pm$  P. pole # P 3312 R

19+71 - 9.6' Rt. =  $\pm$  15" Pepper

19+87.5 - 8.4 Rt. =  $\pm$  Shrub.

20+11.5 - 6' Rt. =  $\pm$  3.2 Conc. walk

20+52.5 - 8.4 Rt. =  $\pm$  Light Stand. # 6710

20+66 - 6' Rt. =  $\pm$  9' Conc. Dr.

20+82.5 - 8.2 Rt. =  $\pm$  P. pole # J.R. 3160

21+13 - 6' Rt. = Beg. Conc. Dr. to Ser. Sta.

21+58 - 6' Rt. = End " " + Beg. Conc. - cb. to walk

21+65 - 6' Rt. = End " " " "

Cont on P. 65

Levels Around S.E. Ret. - Adams + Felton  
Prop. 20' Ret. - 4 parts - outs on Radial Lines

£

1/4

See P. 43 - for Add. notes in Int.

P.C. - 20' Rad. Ret.

25' S.

50' S.

75' S.

100' S. of P.C. of 20' Rad. along.

B.M. 5.02 393.28 ✓ 388.26 ✓ - P. 17

Lt. = out      £      Rt. = in

388.11 5.17 10.2	387.99 5.29 9.2 gut.	388.12 5.16 5.2 Top	388.22 5.06 on ret.	388.34 4.94 7 on ret.
387.98 5.30 6.8	387.95 5.33 9.2 gut.	388.09 5.19 Top 18	388.19 5.14 on ret.	
387.88 5.40	387.41 5.87 9	387.17 6.11 5	387.96 5.32 Top	387.05 6.23 gut.
	387.75 5.53 18	387.43 5.85 9	387.24 6.04 5	387.81 5.47 Top
				387.06 6.22 gut.
	387.73 5.55 18	387.31 5.97 9	387.12 6.16 5	387.77 5.51 Top
				387.03 6.25 gut.
	387.79 5.49 18	387.91 5.87 9	387.20 6.08 5	387.75 5.53 Top
				386.99 6.29 gut.
	387.73 5.55 18	387.91 5.87 9	387.22 6.01 5	387.75 5.53 Top
				387.12 6.16 gut.
			393.28	

PC. 20' Rad. Ret.

25' W.

50' W. of P.C. 20' Rad. Ret. along S.cb. Adams

Adams + Felton  
Levels around Prop. 20' Rad. on S.W. Cor

50' E.

End.

25' E. of P.C. along S.cb. Adams

E.C. - 20' Rad. Ret.

3/4

Lt. = out.

Rt. = in

	388.05	388.05	387.58	388.37	388.44
5.23	5.23	5.70	4.91	4.84	
5	Top	9.4	5	10.3	

	387.99	387.59
5.29	5.69	
Top	9.4	

	387.78	387.44
5.50	5.84	
Top	9.4	

	388.29	387.66
4.99	5.62	
Top	9.4	

	388.19	387.57
5.09	5.71	
Top	9.4	

	388.06	388.03	387.56	388.28	388.37
5.22	5.72	5.72	5.00	4.96	
5	Top	9.4	5	10.3	

	388.16	387.99	388.14	388.18
5.12	5.29	5.14	5.10	
6.8	1.8	1.8		
	9.4	Top		

393.28 ✓

100's = end.

75's.

50's.

39's. - £ 14' Conc. Dr.

25's. along W. cb. Felton

E.C 20' Rad Ret.

3/4

⊕

1/4

	387.68 Lt. 5.60 9	387.59 5.69 5	387.73 5.55 Top	387.91 5.87 gut.					
	387.72 5.56 9	387.62 5.66 5	387.99 5.79 gut. in Dr.	387.91 5.77 6					
	387.72 5.56 9	387.68 5.70 5	387.81 5.47 Top	387.53 5.75 gut.					
			387.57 5.76 gut. in Dr.	387.87 5.41 6 edgewalk					
	387.89 5.44 9	387.70 5.58 5	387.87 5.41 Top	387.61 5.67 gut.					
	387.89 5.39 9	387.78 5.50 5	388.03 5.25 Top	387.66 5.62 gut.	388.17 5.11 6	388.28 5.00 10.3			
	387.88 5.40 6.9	387.81 5.47 1.9 gut.	388.21 5.07 1.9 Top	388.25 5.03 on ret.					
	388.06 5.22 10.2	387.81 5.47 5.2 gut.	388.32 4.96 5.2 Top	388.40 4.88 on ret.	388.54 4.74 7 on ret.				
	387.96 5.32 6.8	387.63 5.65 1.8 gut.	388.17 5.11 1.8 Top	388.27 5.01 on ret.					

393.281

Add. Levels along W. cb. of Felton - N. of N.L. Adams

1+00

0+65

0+50

0+30

0+15

0+00 = RC. 20' Rad. Ret.

0-08 = N.L. Adams

59

Lt. = W ♀

Rt. = E

388.31	387.76	388.32
4.97	5.52	4.96
Top	gut.	5

388.23	387.73	388.06
5.05	5.55	5.22
Top	gut.	5

388.19	387.69	387.99
5.09	5.64	5.29
Top	gut.	5

388.20	387.67	387.96
5.08	5.61	5.32
Top	gut.	5

388.11	387.55	387.94
5.17	5.73	5.34
Top	gut.	5

388.20	387.65	388.00
5.08	5.63	5.28
Top	gut.	5

388.26	387.56	387.90
5.08	5.72	5.38
Top	gut.	5

393.28 - P. 58

Flow line Elev. on Sewer M.H. at  
33<sup>rd</sup> + Adams + 150' N.

B.M. 7.40 392.00 ✓

384.60 ✓ SE 7<sup>th</sup> ct.  
Bancroft +  
Adams  
P. 33

M.H. on ± 33<sup>rd</sup> - 22' S. of N.L. of Adams  
8" Line on Bottom - N. + S. and 8" Line from  
E. along Adams - Live sewer.

8" Line High for Drop from the N.

Seems to be in fair Cond. - Top covered with  
3" of Cold Lay - M.H. built of Conc. rings + Conc

M.H. on ± 33<sup>rd</sup> - 128' N. of N.L. Adams  
8" Line from E. Turns S. to Drop into  
M.H. Shown above - fair Cond.

7-10-47

7.0

60

392.00

Rim of M.H. #65	5.30	386.70 ✓
Flow Line of 8" drop From N.	11.55	380.25 ✓
F.L. Bottom	17.69	374.31 ✓

Rim of M.H. #65A	<del>5.64</del>	387.40
		<del>386.36</del>
FL. M.H. + 8" Sewer	<del>10.97</del>	<del>381.03</del>
		382.06

M.H. 70

Rim	389.60
FL.	383.23

Levels Around Prop. 20' Rad. Ret. at  
S.E. Cor. Bancroft + Adams - also add  
shots in Low gutter to S. - See P. 41  
cb line = base line - outs on Radial Lines

P.C. 20' Rad Ret.

25' S.

50' S

75' S

100' S. of P.C.

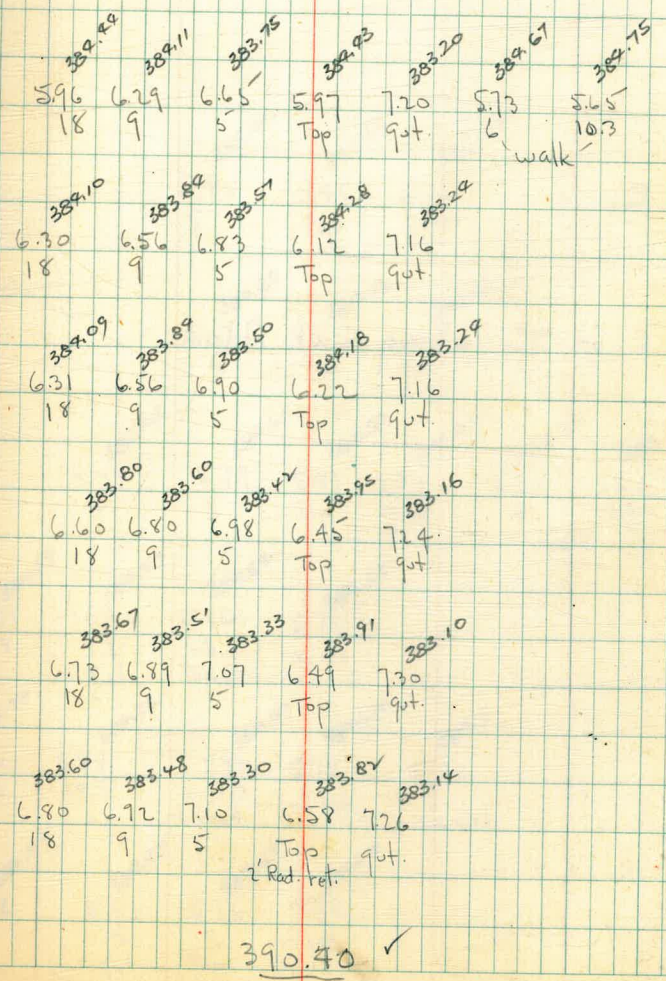
117' S. of P.C. 20' Rad. Ret. along E. ch. of Bancroft  
= N.L. Alley

B.M. 580 390.40 ✓

384.60 ✓ SE 7' ct.  
Bancroft +  
Adams

Lt. = out

Rt. = in



390.40 ✓





Levels around Prop. 20' Rad. Ret. at  
S.W. Cor Bancroft + Adams

EC. 20' Rad. Ret.

3/4

±

1/4

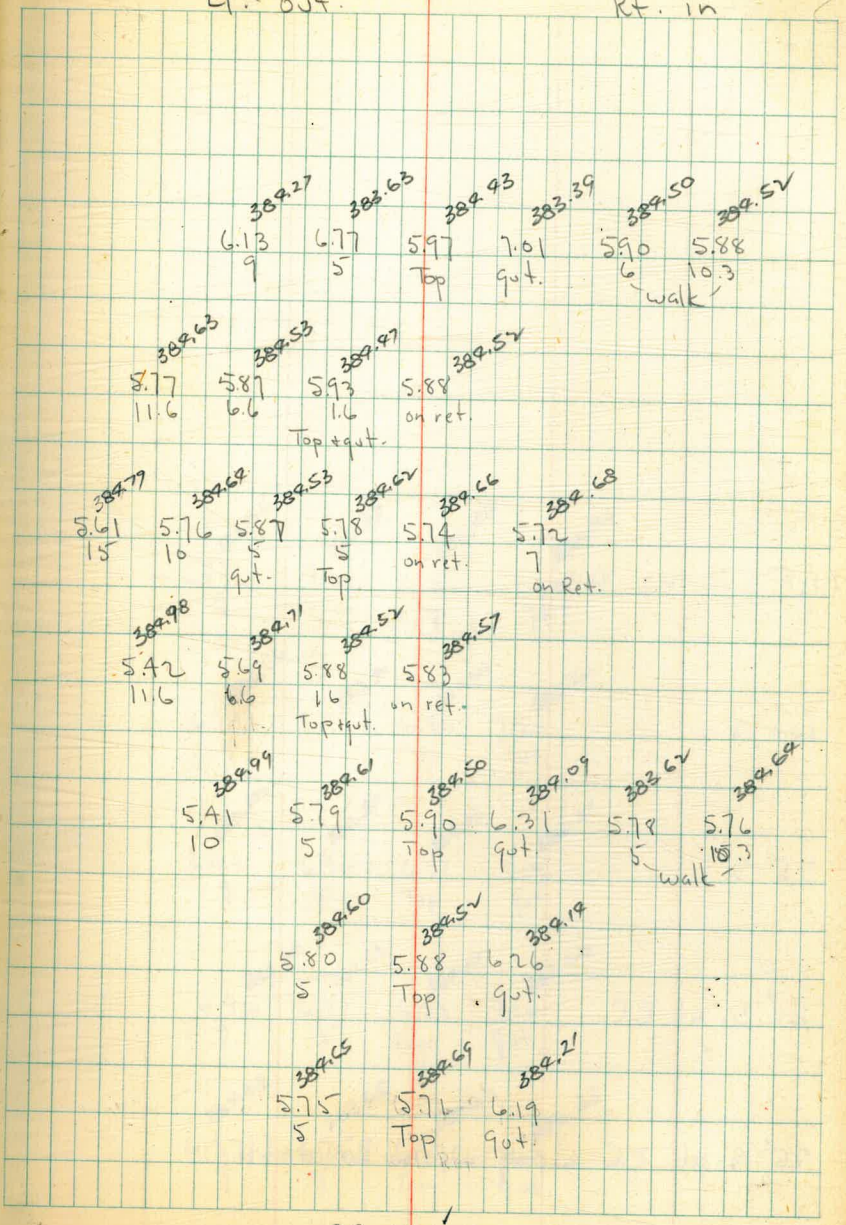
PC 20' Rad. Ret.

25' w. of PC

50' w. of PC 20' Rad. Ret. - along S. cb. of Adams

Lt. out. ±

Rt. in



390.40 - P. 61

117' S. = NL Alley

100' S.

75' S.

50' S. of E.C.

25' S. of E.C. along W. cb. Bancroft.

64

Lt.

E

Rt.

383.56 6.84 9	383.39 7.01	383.82 6.56 Top 2' Rad. ref.	383.20 7.20 9ut.
383.66 6.74 9	383.41 6.99 5	384.00 6.40 Top	383.20 7.20 9ut.
383.80 6.60 9	383.50 6.90 5	384.03 6.37 Top	383.21 7.19 9ut.
383.90 6.46 9	383.63 6.77 5	384.17 6.23 Top	383.24 7.16 9ut.
384.03 6.37 9	383.65 6.75 5	384.23 6.17 Top	383.33 7.07 9ut.

390.40 ✓

Location - Poles - Lights - Trees + Drives  
Cont. from P 55

21+68 - 8.8 Rt. = ± 4" Dia. Shrub.

21+78 - 8.7 Rt. = ± 3' " "

21+87.5 - 8.7 Rt. = ± " " "

21+91 - 9.2 Rt. = ± P. pole # G 3300 R

21+98.5 - 8.2 Rt. = ± Light Stand # 6708

22+00.6 - 8.3 Rt. = ± 4" Steel Mail box post.

Add. Levels along w.cb Mt. View  
 Both ways from int. of  $\Phi$  Prop. Drain  
 + w.cb. Mt. View - sta. 22+86.2 - P. 29  
 cb. Line = Base Line =  $\Phi$

7-11-47  
 7.0.

P. 67 for reeds. to S.

150' N. = end. = opp. Alley on E.

125' N.

100' N.

75' N.

50' N. of  $\Phi$

Going N. along w.cb. (on Curve) = Rt. of  $\Phi$

See P. 29 for outs up to 50'

BM. 5.22 394.13' 388.91'

NE. Adams  
 + Mt. View  
 P. 28

Lt = W

$\Phi$  = w.cb.

66

Rt. = E = in st.

6.12 Top	388.61	6.55 gut.	387.58	5.93 10	388.20
6.57 gut. in Dr.	387.56			5.93 10	388.20
6.19 Top	387.94	6.60 gut.	387.53	5.95 10	388.18
6.16 Top	387.97	6.47 gut.	387.66	5.82 10	388.31
6.08 Top	388.05	6.35 gut.	387.78	5.70 10	388.93

394.13'

147.2's. = E.L. Suncrest. = End.

100's.

70's.

40's. of  $\Phi$  (R. 29 for outs N.)

Going S. along W. cb. = Lt. of  $\Phi$

Lt. = E = in st.

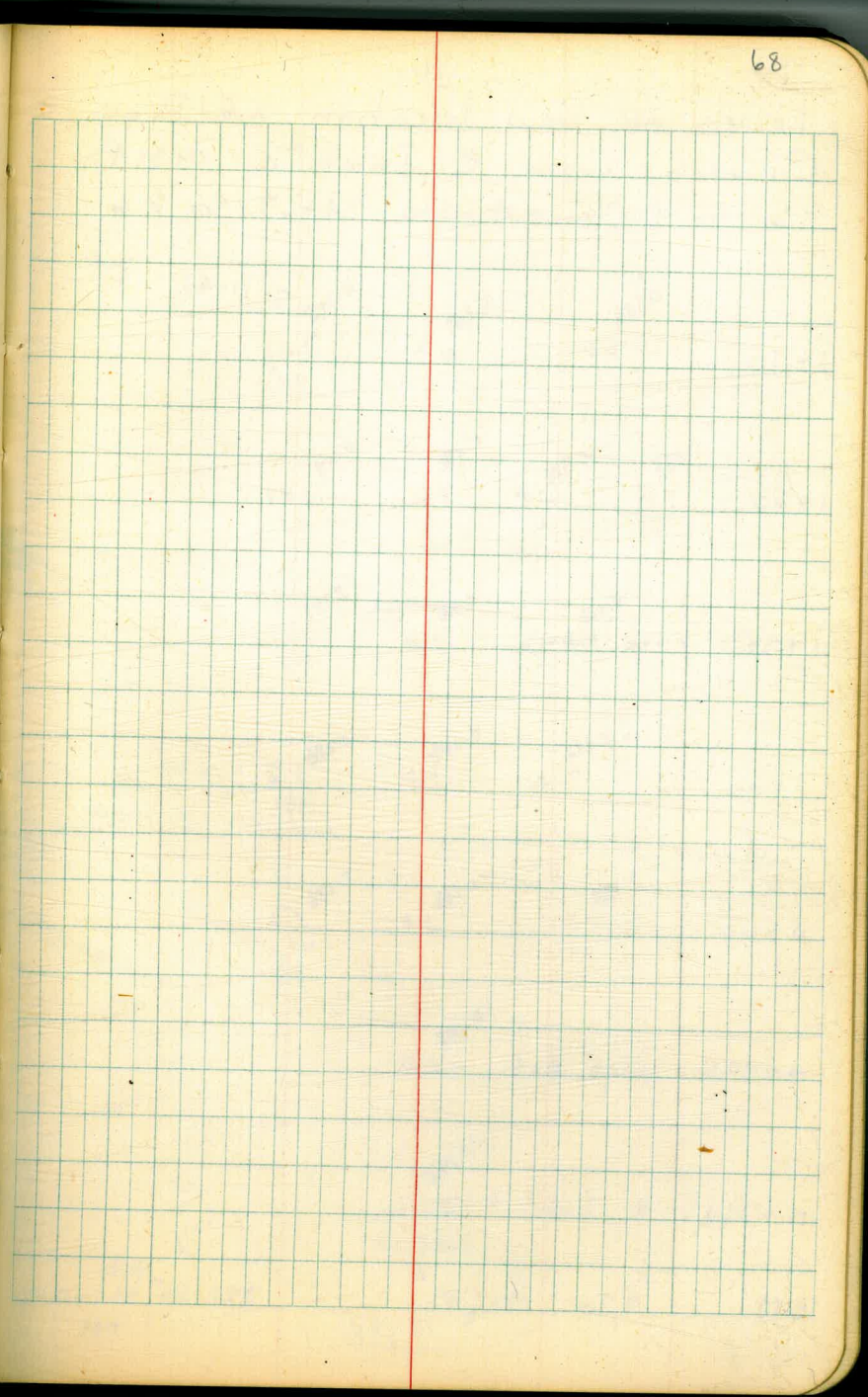
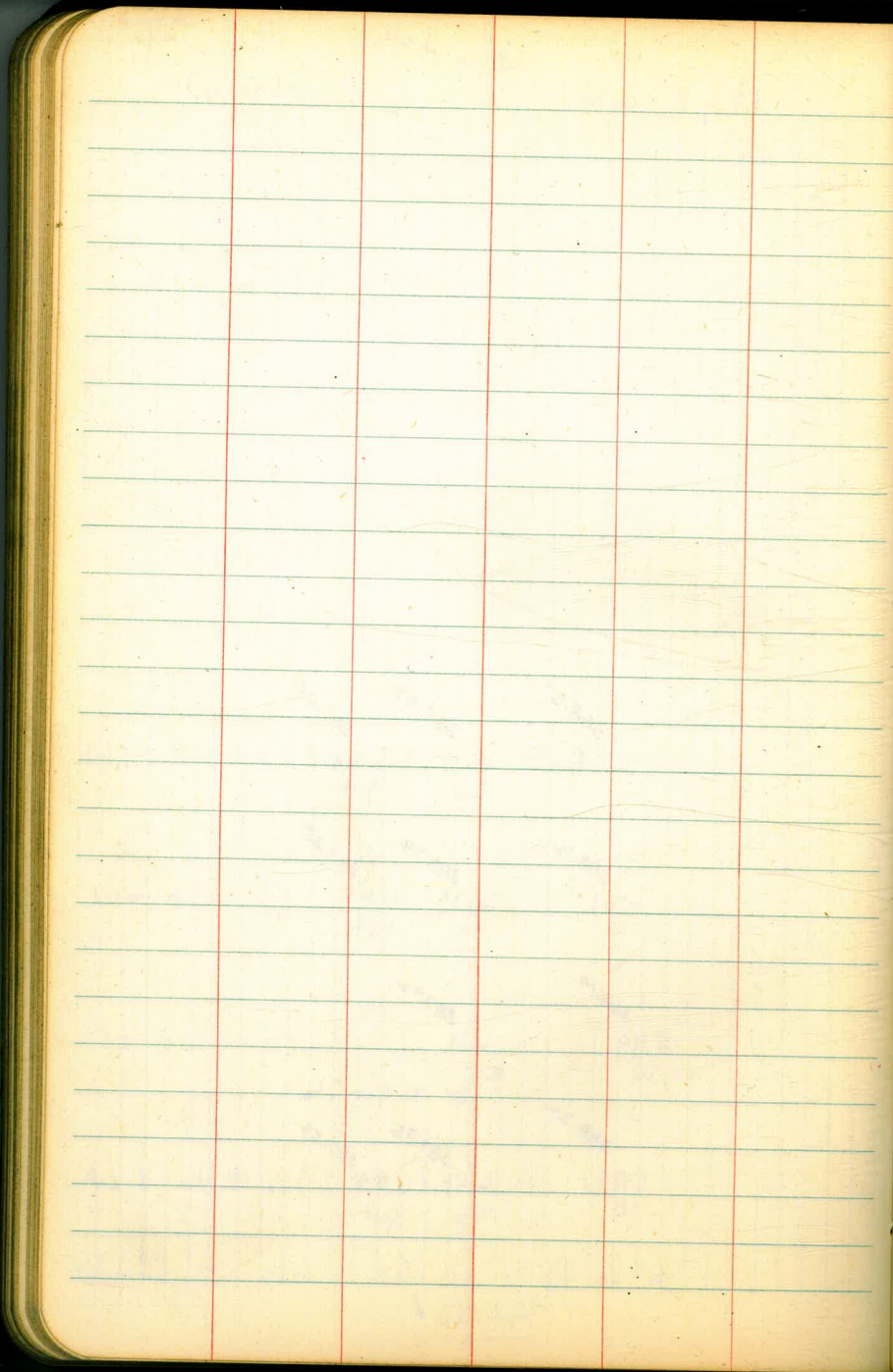
$\Phi$  = w. cb.

67

Rt. = W.

388.39	387.89	387.26
5.74	6.24	6.87
	Top	gut.
388.12	387.74	387.25
6.01	6.39	6.88
10	Top	gut.
388.14	387.92	
5.99	6.71	
10	gut. in	
	Dr. to Set Sta.	
388.24	387.96	387.59
5.89	6.17	6.54
10	Top	gut.

394.13 ✓



Levels on New Location of Prop  
 Culvert - from  $\pm$  Inlet #12 = 0+39.43  
 P. 6 to  $\pm$  Cleanout - Sta. 24+67 - See P. 6

7-11-47 - 7.0

1+70

1+60

1+35 - edge bank

1+00

0+60

0+44.6 = edge Ret.

0+39.43 =  $\pm$  Inlet #12

B.M. 4.96 387.81 ✓

382.85 ✓ Hub  
 24+60.08  
 R31

69

Lt.

$\pm$

Rt.

371.3  
 16.5  
 20

382.8  
 4.0

383.0  
 4.8  
 10

371.9  
 15.9  
 20

382.0  
 5.8

383.2  
 4.6  
 4  
 edge

383.1  
 4.7  
 10

371.9  
 16.0  
 20

383.4  
 4.4

382.9  
 4.9  
 10

382.7  
 5.1  
 18.1  
 Top bank

382.9  
 4.9

383.3  
 4.5

382.7  
 5.2  
 10

383.2  
 4.6

383.1  
 4.7  
 10

382.51  
 5.30

382.52  
 5.29  
 on Cross

387.81 ✓

⊕

70

Lt.

Rt.

1+97.14 = ⊕ Cleanout = Sta. 24+67 on Main line

1+85

379.56  
8.25  
on Hub.

369.11  
18.7  
20

382.1  
57

382.8  
5.0  
5  
edge

383.3  
4.5  
10

387.81 ✓



Levels on new location of Prop  
 Culvert - from end of Existing  
 24" RC Culvert to  $\pm$  Cleanout - Sta.  
 24+67 - P. 5 + P. 6

0+76.23 =  $\pm$  Cleanout = 24+67

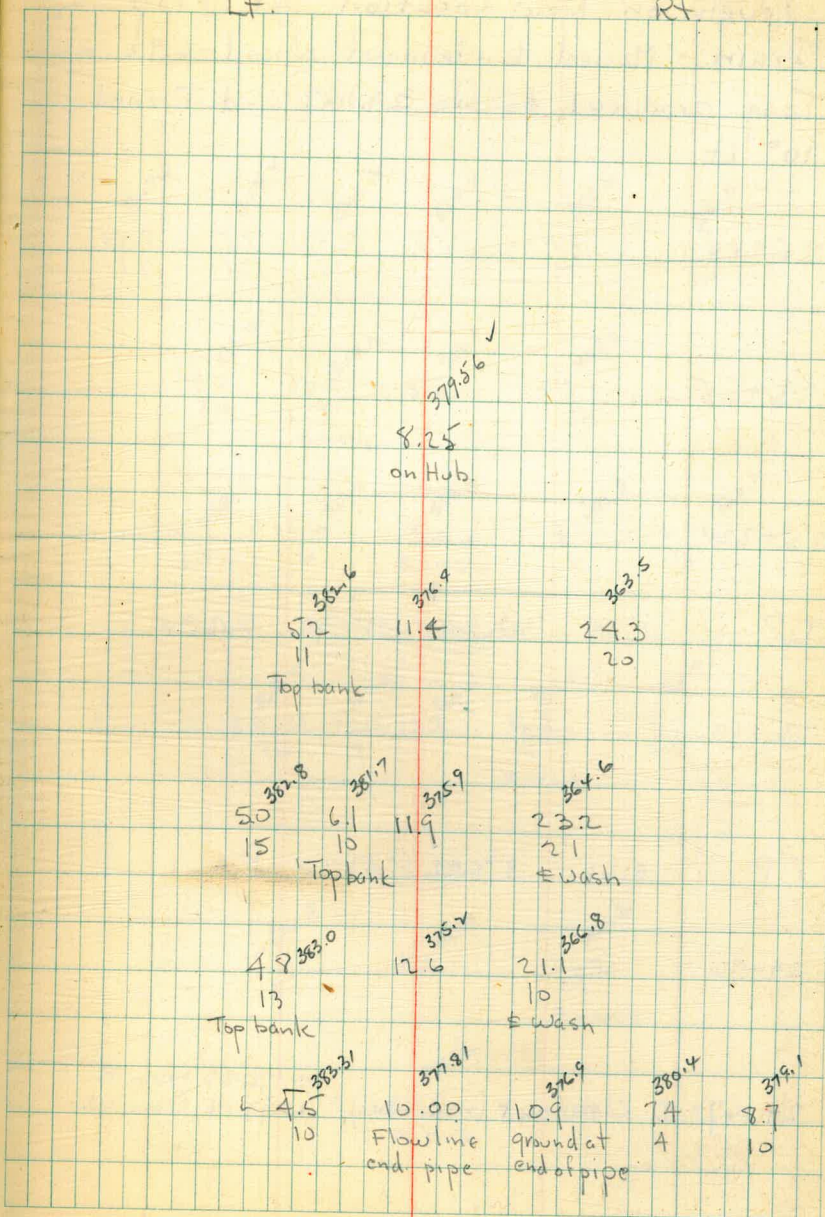
0+55

0+35

0+20

0+00 = F.L. 24" pipe - end.

Lt.  $\frac{R}{L}$  Rt.



387.81 - P. 70

Levels on New Location of Prop  
 Drain = Moved & cleanout ahead -6.92 on  
 Tang. produced to Sta. 24+67 and Turned  
 10° Lt.

25+85

25+65

25+32

T.P. 0.34 362.64 12.92 362.30

25+10

T.P. 0.61 375.22 13.20 374.61

24+90

24+67 =  $\pm$  Cleanout (new loc) =  $\begin{matrix} +76.23 \text{ from E.} \\ +97.14 \text{ from W.} \end{matrix}$

7-11-47  
 70.

Lt.

$\Phi$

Rt.

72

<sup>347.8</sup>  
 14.8  
 25  
 13.2  
 15  
 16.0  
 10  
 $\pm$  wash

<sup>349.4</sup>  
 9.6  
 20  
 13.3  
 8  
 $\pm$  wash  
<sup>354.6</sup>  
 8.2  
<sup>358.2</sup>  
 4.4  
 10  
<sup>361.6</sup>  
 11.0  
 20

<sup>350.0</sup>  
 5.9  
 20  
 5.6  
 6  
 9.0  
 $\pm$  wash  
<sup>357.1</sup>  
 5.5  
<sup>368.7</sup>  
 +6.1  
 20  
<sup>359.3</sup>  
 3.3  
 6  
<sup>363.2</sup>  
 +0.6  
 15

362.64 ✓

<sup>365.2</sup>  
 10.0  
 20  
<sup>372.2</sup>  
 13.0  
 9  
<sup>380.0</sup>  
 15.2  
 $\pm$  wash  
<sup>388.5</sup>  
 16.7  
 9  
<sup>367.1</sup>  
 8.1  
 20

375.22 ✓

<sup>374.9</sup>  
 12.9  
 15  
 19.9  
 $\pm$  wash  
<sup>361.6</sup>  
 26.2  
 24

<sup>379.56</sup>  
 8.25  
 on Hub.

387.81 - P 70

26 + 96.88 = stub = end.

26 + 70

26 + 50

26 + 25

T.P.	0.06	344.36	18.34	344.30	344.32
					25 + 99.74
					P.32

26 + 00

Lt. Rt.

Notes Reduced 7-10-27

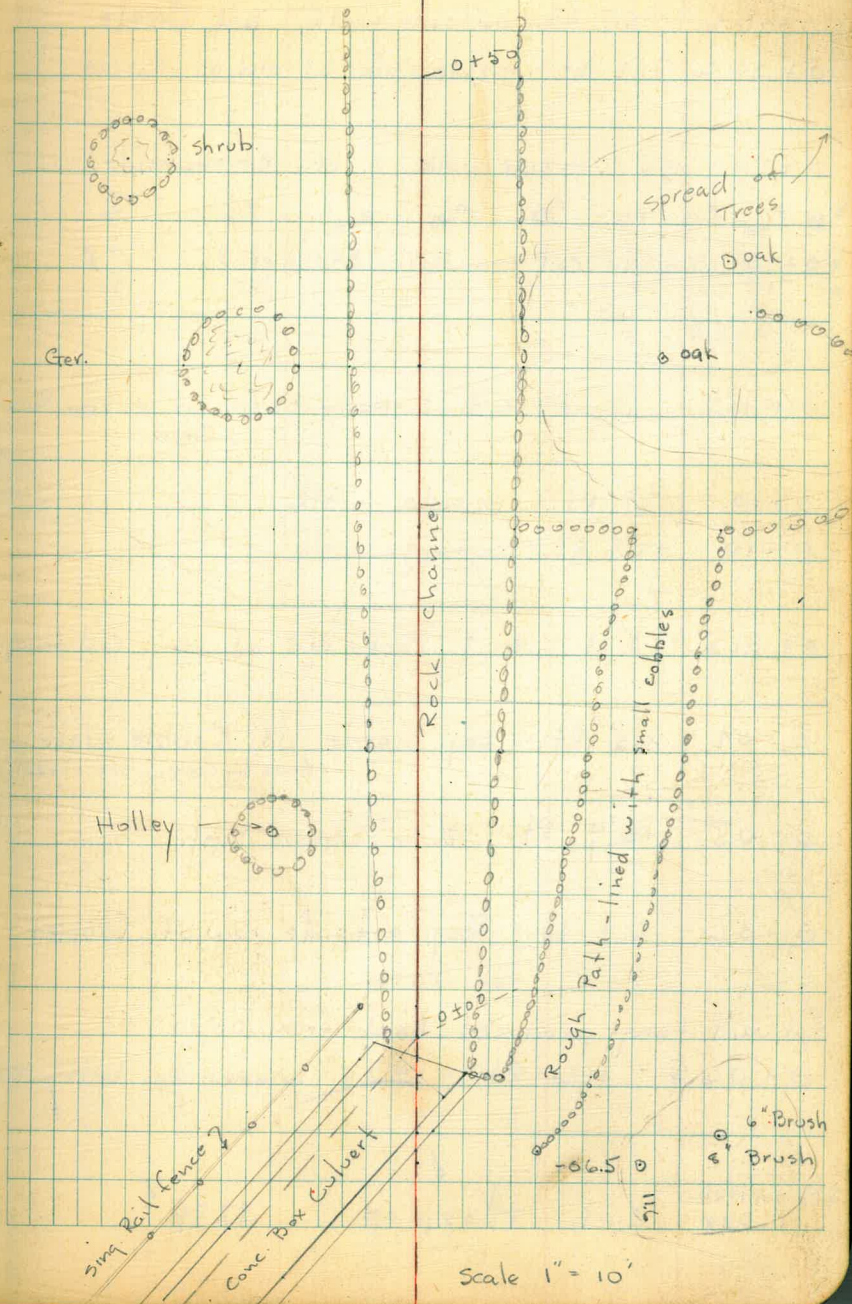
		19.0 14 Toe slope	19.1 wash	19.0 12	11.5 20
		17.0 10 on fill	18.0 6 wash	16.3 6	7.1 20
		11.4 20	16.0 10 Toe slope	17.2 7 wash	7.0 20
		7.8 20	9.0 10	14.3 15 wash from E	6.2 25
		19.3 20	21.2 15 wash	14.0	9.5 10
					8.9 20

344.36 ✓

362.64 ✓

Add Levels + Tops. at end of Conc.  
Box Culvert - Mission Valley - See  
P. 46-47 9-8-47 7.0.

Levels + Tops - Next Page



0+26.6 - 15.7 Rt. = outside walk - beg. Circle

0+26.6 - 11.2 Rt. = inside walk at end at Circle

0+20 - 9.5 = inside walk + 14.7 Rt. = outside

0+15 = add. sect. on Rock channel

0+10.7 - 7.8 Lt. =  $\Phi$  2" Holly bush in 4' Dia. Rock Circle

0+10 - 7.7 Rt. = inside walk

0+10 - 12.7 Rt. = outside walk

0+01.5 = 3' Lt. =  $\Phi$  2" Post = end of Sing. rail fence

0-02 - 4.5' Rt. = Beg. inside of Cobble walk  
Goes to Conc. - see sketch

0-05 - 15.7 Rt. =  $\Phi$  6" Lemon Bush

0-06 - 6.3' Rt. = Beg. outside row of Cobbles  
for Path

forward tang. produced back from 0+00

0-06.5 - 11.6 Rt. =  $\Phi$  8" Lemon side berry Bush

BM. on Hub.

1+50-P48

2.04

99.83 ✓

97.79 ✓

Lt.

$\Phi$

Rt.

75

91.6	91.8	89.0	88.7	88.8	91.6	91.7	92.8	96.7
8.2	8.0	10.8	11.1	11.0	8.2	8.1	7.0	1.6
10	2.7	1		3	4.2	11	20	30
	Top				Top	$\Phi$ Path	Toe slope	

99.83 ✓

o+45.5 - 15.2 Lt =  $\Phi$  of 4' Dia. Rock circle - with shrub

o+40.7 - 16' Rt =  $\Phi$  6" Oak - scrub.

o+35.5 - 12.7 Rt =  $\Phi$  6" Scrub oak

o+35 - 9.4 Lt =  $\Phi$  6' Rock Circle - with Geraniums

o+35

93.2	92.8	90.1	89.9	89.9	93.0	93.6	95.9	98.3
6.5	7.0	9.7	9.9	9.9	6.8	6.2	3.9	1.5
13	3.7	1		2.7	5.4	15	25	30
	Top				Top			

99.83 ✓

82.5  
 25  
 57  
 7320  
 432  
 7899

74  
 26

DISTANCES FROM CENTER OF ROADWAY FOR  
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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