

1790

1790

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

1 sec alleys Blk 95 Palomar Hrs 1-1x

Swamy " " 94 " " " "

" " " 93 " " " "

1 Camino de La Costa 21-25

X sec Dowling Drive 26

" Palomar Ave Electricity 41

" LANDIS Texas to Louisiana 54

X-Sect Landis - Arizona to Ulla Terr. 60-67

Levels - spur track 2nd to 4th

between J+K Sts. 72-75

Location of IMPRINTS, etc.

BLK 95 Pt Loma Hts

" " Ocean Beach

Sketch P. 1

4 + 99.3

4 + 51

4 + 01

4 / 00

2 + 52.5

2 + 52.30 = Δ 0° 40' 45" RT

1 + 50

0 + 00 w. L. Guizot

Lt = South ~~£~~

PT

2

Contd. P. 3

PP. A4585
8.1

Exp. 8" wall
and fence 10.7

8" Con.
wall
Beg. and
18.5 Bamboo
Fence

Beg. 8" Con. Per. wall
and Bd. Fence
11

PP. A4560 RE. 469
8.2 7.40

PP. A4534
9

RE. 469
10.25 = add. line

PP. A4524
10

curb Per.
10

curb Per.
9.90

alley

Blk 95 Mr. Landa Hrs

" Ocean Beach

Lt

d

Pr.

3

6100.00 E.L. Freude

curb Ret.
10.10

6. Ret.
9.90

5100.3

End 8" wall + Bamboo
18.5 fence

5100

RE. 469
8.90

Survey of alley

Blk 94 Pt. Loma Hts

" 10 Ocean Beach

Moore
Bc99
Gager
Roberts
7-17-47

W.O. 21001

Ref. F.B. 567-62

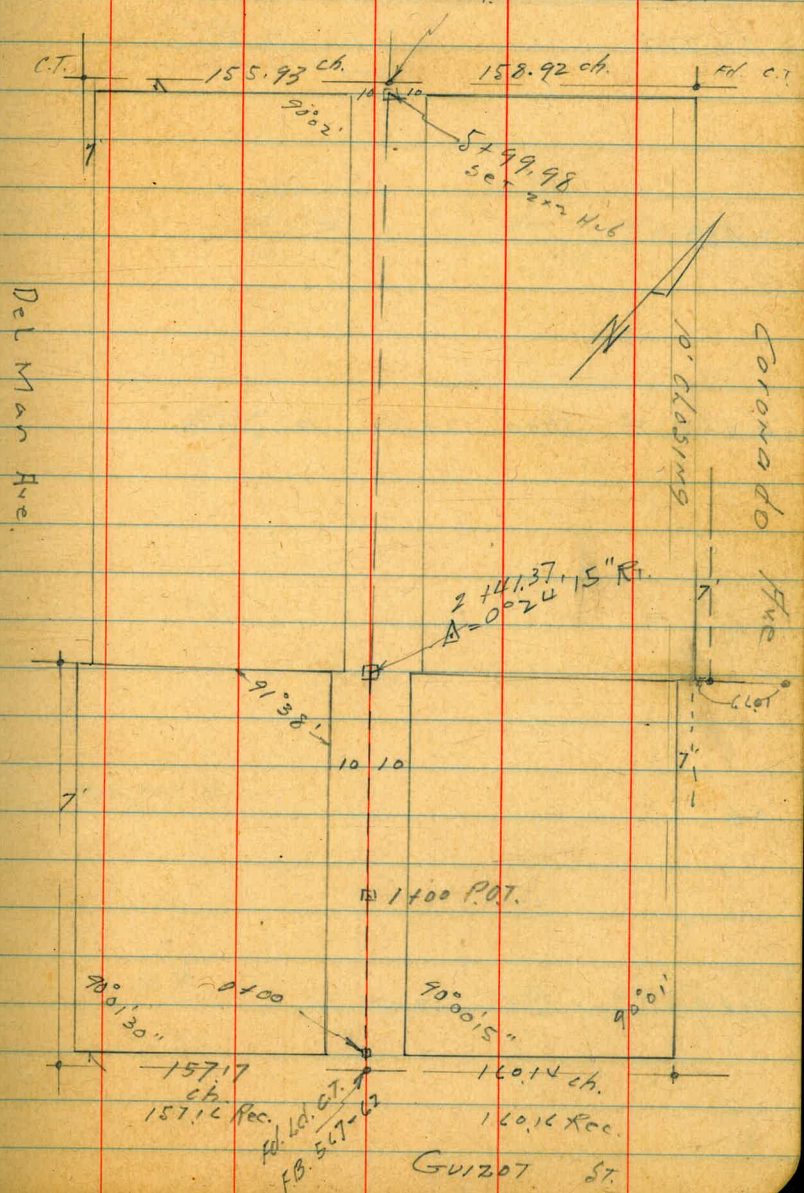
• fd. ld. cts
• 507 2x2 Hubs

Used Ties for Pt. Loma Hts.
any correction will be in O.B.

Indexed map
8-14-47
Fraude

fd. ld. cts.
fb. 567-62

ST



BLK 94 PT LOMA HTS
LOCATION OF IMPRINTS " 10 O.B.

Lt = South

±

Rt

5

0+99.5

End Bd. Fence and Beg. Wire Fence
14

0+50

Beg. Bd. Fence
12.7

R.P.
J.P.H. 4508
10

End Brick Wall
10.3

0+45 ± shed stable, 10' wide

shed
12.7

0+

End Rail Fence

0+

Beg. rail fence

0+00 w/6 Guizot

c.b. Ret.

c.b. Ret.

Beg. 12" Brick Wall
4' High

2100

1799

1795

1753.5 Beg. wire fence

1731 end wire fence

1711 E 15' Con. drive

LT

E

RT

6

End wire
fence
9.7

pp. H453x
8.7

Beg. Bd. Fence
70.5

Fence
9.8

Fence
14

E drive
14

Bk 94 P. Lanta Hrs
" 10 Ocean Beach

Lt

E

R

7

5 + 99.98 E.L. Froude

End Picket fence Curb
11 70

81
70

5 + 11

End Wall Beg. Picket
21.5 71.7
Fence

5 + 00

93

4 + 50 Beg. Con. Blk. Wall

Wall
31.5

3 + 51 P.P. 40 #

P.P.
97

2 + 41.37 Δ 0°24'15" RT.

2 + 40

1/2" Pipe & End Bd.
11.08 FENCE

Survey of Alley

Blk 93 Pt. Loma Hrs
 " 9 Ocean Beach

Moore
 8499
 Green
 Roberts
 7-24-27.

W.O. 21001

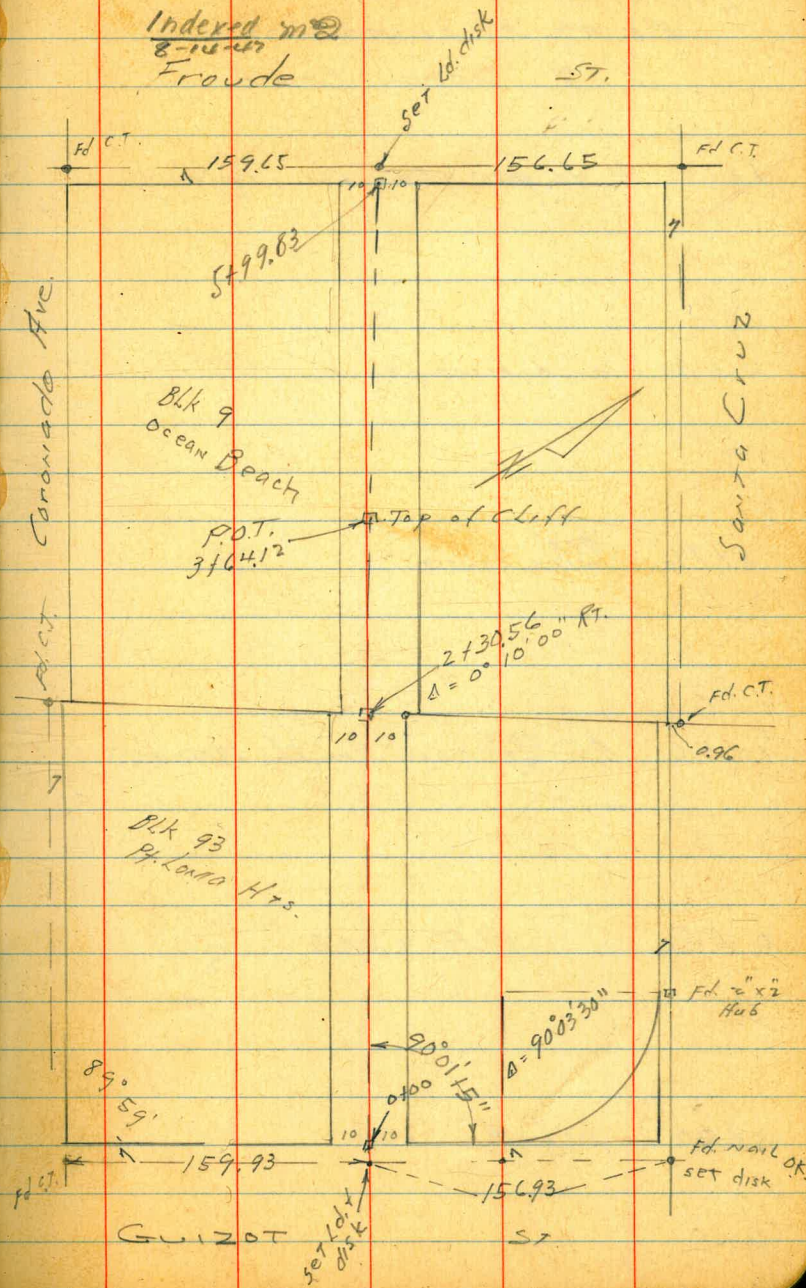
Used the P.M. for Pt. Loma Hrs.
 any correction will only
 affect Ocean Beach.

Take and check bet. rocks N & S
 2 + 30.56 to Pueblo Line

30 276

8

Indexed m²
 8-14-27
 Froude



Coronado Ave.

Santa Cruz

Blk 9
 Ocean Beach

P.O.T.
 3 + 4.12

Blk 93
 Pt. Loma Hrs.

89° 59'

GUIZOT

set 6d. disk

Fd. 2" x 2"
 Hub

Fd. nail
 set disk OK

Locations of Imprints in Alley
Blk 93 Pt Loma Hts
" 9 Ocean Beach

Lt \$ Ft

5+

1+10 E do gar. con fl. 17 wide

gar.
20

5+1

0+90 end wire fence

fence
9

5+0

0+76 3rd wire fence

fence
9

4+

0+56 E do gar. con. fl. 19.2 wide

gar.
14.9

3+

0+50 PA v 508

P.P.
8.5

2+

0+00 W.L.G. 1207

curb
10

curb
10

2+

	Lt	E	Rt
	2 + 38 end lattice fence	Fence 8.6	
5	2 + 30.56 $\Delta = 0^{\circ} 10'$ Rt.	"x2" Hub. disk	3/4" Pipe L.S. 2201 9.73
5 + 11	2 + 29 Beg. Lattice fence	Fence 8.41	
5 + 10	1 + 76 P.P. P.M. 4528	P.P. 8.8	
4 + 8	1 + 50 end wire fence	Fence 8.8	
3 +	1 + 46.3		3/4" Pipe L.S. 2201 9.75
2 +	1 + 18 Beg. wire fence	fence 9	

LT

¢

RT

3425 E 10' Bd. gar.

5

garage
9.3

3420 end last fence

5+

fence
9.3

510

3400 { also Beg last fence
9.4 LT. NW Cor. Con. floor
RP 8.9 Lt. H 4550

3/4" Pipe RE 2748
9.30

4+

2462 L Beg. Con. Floor

N.E. Cor. Con. Floor
9.2

3x

2457.6 E 32' wide oil drive

drive
18

240

2+

2451 E do gar. Con

gar.
20

LT

E

R

12

5 + 15 Beg. of 8' High Con. Pct. Wall

Wall
9.7

4 + 93.5 E 11' Con. slab

slab
11.64 + 88 N.W. Cor. Wood Bldg.
work shopBldg.
11.4

4 + 61.6 N.E. Cor. Wood Bldg.

Bldg.
10.7

3 + 99 P.P. A 4560

P.P.
8.2

3 + 64.2 P.O.T. 2' x 2' H.S.

Top of Chiff

LT

¢

R

13

5+99.83 E.L. Froude

 $\frac{\text{cb. Ret.}}{9.9}$ $\frac{\text{cb. Ret.}}{10.05}$

5+99.6 End. Cou. Ret. walk

 $\frac{\text{walk}}{9.9}$

5+49 P.P. A 4592

 $\frac{\text{P.P.}}{9.4}$

Sketch P1

Cross sec. alley Blk 95 Pt. Loma His

Moore " " " " " Ocean Beach
Green " " " " " "
Roberts W.O. 2/001

LT = South

R7

0-06

186.32
5.43
10
C6
186.01
5.74
10
186.78
4.97
10
187.73
4.02
10
3.68
10
C6

182.69
9.06
50
C6

182.09

185.93

185.46

186.65

187.79

188.25

190.98

191.49

0-12 WC6

9.66
50
C6
5.87
13
C6
6.29
13
5.10
13
3.98
13
C6
3.50
13
C6
0.77
50
C6
0.26
50
C6

0-30 E Guisot

183.04
87
50
187.42
4.33
191.71
0.04
78

T.P. 10.105 191.75 0.225 181.645
T.P. T.CT. 9.72 181.87 0.73 172.15
T.P. 12.36 172.88 0.84 160.52
T.P. 10.76 161.36 0.14 150.60
T.P. 11.55 150.74 0.41 139.19
T.P. 11.14 139.60 0.25 128.46
T.P. 12.25 128.71 0.12 116.46
T.P. 12.165 116.58 0.45 104.415
B.M. S.W.B.P.
Pescadero 10.265 104.865 94.60
and
Froude

191.75
Set B.M. S.W. T.C.T. Orchard & Guisot

1400

0775

0741

T.P. 201 182.36 1140 180.35

0723

0708

0700 W.L. Guizot

191.75

121
50

174.7
107

7.7
50

176.9
5.9
50

183.0
8.8
50

186.36
5.39
10
66

170.3
8.5
10

171.7
174.6
7.8
10

177.5
4.9
10

178.8
183.3
182.36
187.1
7.5
4.7
10

187.6
4.2
7.0

185.94
5.81
10

175.0
7.4
10

176.2
178.8
6.2
10

180.0
2.8
10

187.6
187.1
1.5
10

187.4
4.4
10

187.62
4.13
10

191.75

176.0
6.4
10

177.2
178.8
1.6
10

180.8
1.6
20

185.3
182.8
6.5
30
36

184.9
4.9
33

188.08
3.67
10
66

177.6
4.8
50

180.2
182.1
2.1
50

182.4
0.3
50

183.4
1.5
50

186.2
5.2
50

188.08
3.67
10
66

2 + 55

2 + 52.3 Δ 0° 40' 45" R

+ 50

2 + 11

T.P. 125 175.87 774 174.62

2 + 00

1 + 75

1 + 33

182.36

	166.2	169.2	169.7	170.7	171.6	174.1
9.7	6.7	6.2	5.7	4.3	1.8	
<u>50</u>	<u>30</u>	<u>10</u>	<u>10</u>	<u>10</u>	<u>50</u>	
	170.3	172.7	173.2	173.4	174.9	
5.0	3.2	2.7	2.5	1.0		
<u>50</u>	<u>10</u>	<u>10</u>	<u>10</u>	<u>50</u>		
	170.2	172.1	173.7	174.2	175.6	
12.2	10.3	8.7	8.2	8.2	1.8	
<u>50</u>	<u>40</u>	<u>10</u>	<u>10</u>	<u>10</u>	<u>50</u>	
	171.0	174.8	175.6	175.2	176.5	
11.4	7.6	6.8	7.2	1.9		
<u>50</u>	<u>10</u>	<u>10</u>	<u>10</u>	<u>50</u>		
	170.4	173.5	173.6	174.7	177.4	
12.0	8.9	8.8	7.7	5.0		
<u>50</u>	<u>10</u>	<u>10</u>	<u>10</u>	<u>50</u>		

182.36

T.P. 9.78 173.97 40x 164.99
 +85 159 152.3
 57 55 156.9

+60

3+29

3+23

T.P. 4.95 168.23 1259 163.28

3+07

3/00

175.87

160.8
 7.2 161.5
 31 18 163.4
 6.9 161.3
 8 161.7
 5.5 163.2
 5.0 165.7
 5.5

154.0
 14.2 156.3
 7.0 10.0 158.2
 28 10 8.6 159.6
 7.5 160.7
 7.0 7.0 161.2
 2.2 4.8 163.4
 5.0

155.4
 5.2 159.2
 0.8 7.0 160.2
 161.8
 6.0 164.9
 0.0 5.0

156.2
 12.0 159.9
 5.0 10 7.4 160.8
 7.1 161.1
 3.1 165.1
 10 0.2 168.0
 5.0

158.4
 17.5 162.0 168.23
 5.0 13.9 12.8 163.1
 12.0 12.0 166.4
 7 9.5 9.7 166.7
 10 6.9 169.0
 5.0

162.1
 13.8 165.7
 5.0 10.2 9.6 166.3
 9.1 166.8
 10 5.0 169.6
 5.0

175.87

497

455

4451

T.P. 2.88 170.20 6.59 167.38

4425.5 9 5' Con Walk

4401

3795

173.97

158.8
163.2
157.8
161.4
50

162.7	164.4	165.8	164.0	168.7	169.8	171.6
11.3	9.6	8.2	10.0	5.3	15.2	2.4
31	19	14	10	10	10	10
165.8	167.3	165.9	166.2	169.4	171.1	171.5
8.2	6.7	8.1	17.8	4.6	2.9	2.5
19	14	14	8	4	10	11
161.8	164.9	167.0	167.6	168.5	170.21	171.57
12.2	9.1	7.0	6.4	5.5	3.7	2.80
48	22	19	10	5	10.6	25
160.5	163.7	165.6	165.8	166.3	166.8	169.68
9.8	6.6	4.7	4.5	4.0	3.5	0.58
50	20	16	10	10	6	107
160.3	163.1	165.1	165.3	165.6	166.7	169.0
10.0	7.2	5.3	5.0	4.7	3.0	2.6
50	20	10	10	10	10	19
158.3	158.3	161.8	162.0	161.3	161.9	165.9
5.0	5.0	8.5	8.3	9.0	5.8	4.4
50	10	10	8	8	5	18

TOP Wall
TOP Wall to West

Walk

TOP Wall

173.97

T.P. 327 154.3 8.40 151.16

5+97

+80

+68

5+50

T.P. 0.69 159.50 11.39 158.87

5+18

16.1
50
14.5
35

5+00.3 end wall on Rt

170.26

154.6
21.0

154.7
1.9
5

153.0
4.0
10

151.6
8.0
20

151.7
7.9
10

152.5
7.1
10

155.3
4.3
10

157.2
2.1
12

158.0
1.6
20

154.3
2.9
25

154.7
1.9
10

154.0
6.0
20

153.0
5.8
10

154.4
5.7
10

156.0
2.8
10

158.6
1.0
20

154.6
2.0
25

155.3
1.3
10

155.6
4.0
10

156.0
1.0
10

158.0
1.6
10

159.4
1.0
20

155.9
3.7
25

156.4
1.4
10

156.9
2.7
10

158.3
1.3
10

159.6
2.0
10

159.6
0.0
20

158.4
11.9
27

159.5
10.8
10

159.9
10.4
10

159.3
11.0
4

159.56
11.3
10

159.6
10.7
5

160.9
9.4
7

160.9
9.4
10

162.1
8.4
25

154.1
12.7
80

161.3
9.0
10

161.0
8.5
7

160.9
9.0
10

161.6
8.7
10

163.0
7.3
10

164.0
9.3
18

166.01
4.25
18.5

170.26

Top
Wall

check to starting B.M. 12.57 94.56 94.60

T.P. 0.45 107.13 12.64 106.68

T.P. 0.64 119.30 12.29 118.66

T.P. 0.44 130.95 12.27 130.51

T.P. 0.41 142.78 12.06 142.37

6+30 E Froude

6+12 E C6

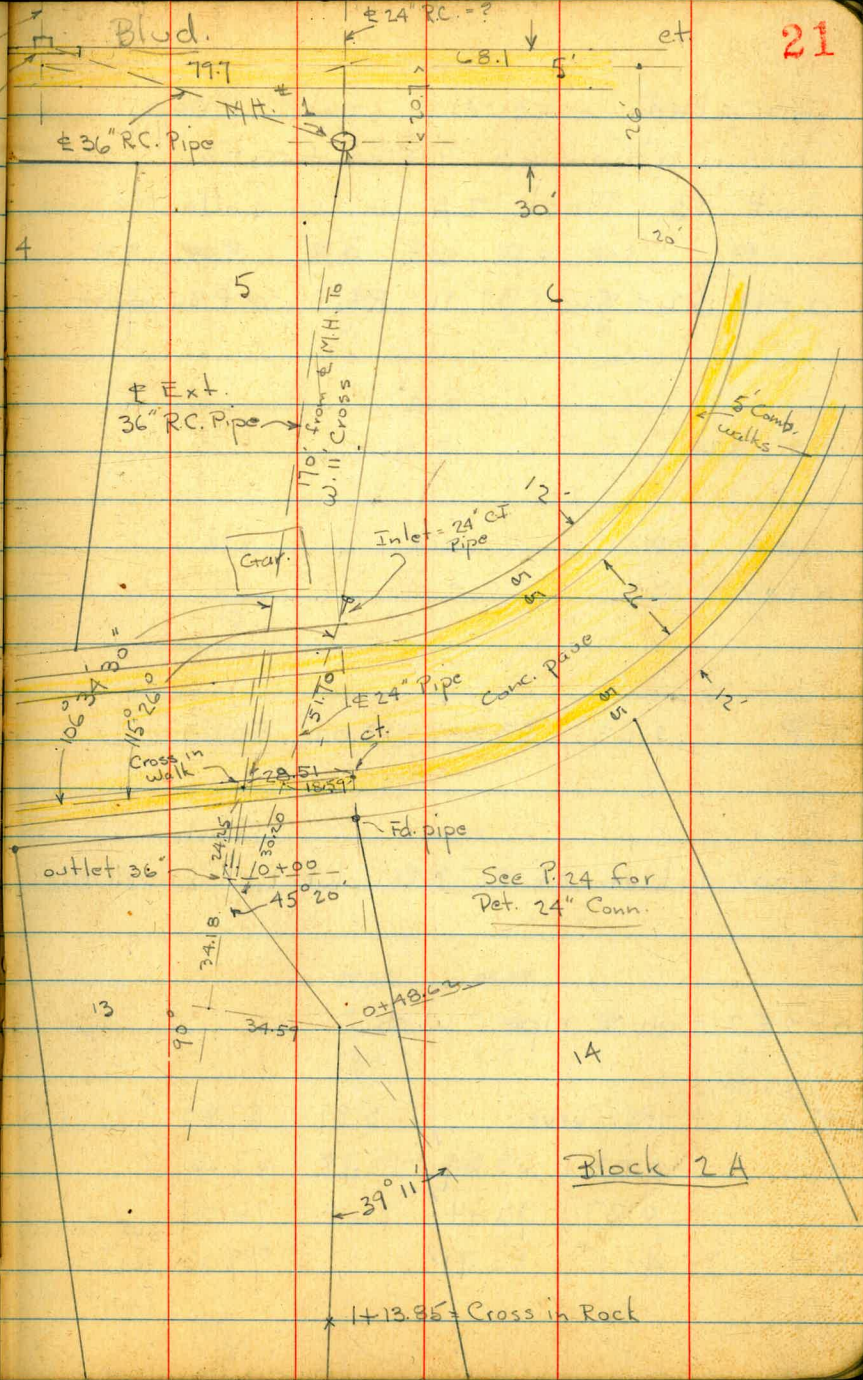
6+00 E.L. Froude

154.43

				147.68	149.32	150.23	151.12	152.16	
		6.75	5.11						
		25	10	4.20	3.31	2.27			
147.73	147.23	149.63	149.18	150.35	151.48	151.99	153.79	154.26	
6.70	7.20	4.83	5.25	2.08	2.95	2.44	0.64	0.17	
30	30	13	13		13	13	5.0	5.0	
06		26			06	06		06	
	150.05	149.92	150.53	151.55	151.90				
	4.38	4.51	3.90	2.88	2.53				
	10	10		10	10				
	06				06				
				154.43					

indexed
c.s.k.

La Jolla $\pm 24"$ R.C. To
Inlet opp.
20' curb Inlet



Block 13

Camino De La Costa
et.

Costa Place

12

13

14

Block 2A

See P. 24 for
Det. 24" Conn.

1+13.85 = Cross in Rock

10-20-47

22

7.0

Lt.

+

Rt.

Location + Levels for Prop.

Drain - Camino De La Costa

Lot 13 - Block 2A in La Jolla Hermosa

0+48.62 - Ang. 39° 11' Rt. - Sect. on split

52.8	55.2	36.0	36.0	36.0	41.1	48.0
0.5	7.9	17.3	17.3	17.3	12.2	5.3
17	7	3		3	5	15

0+22

36.5
14.8

0+10

53.2		41.0	41.0	51.8
0.1		12.3	12.3	15
.13			12	15
				Top

T.P. 2.63 53.30 13.02 50.67

53.30 ✓

Trash

0+00 - outlet of 36" RC. Culvert - Covered by

44.89
18.70 = Flow line outlet.

0-25.2 - on + Pipe = w. cb.

56.68 56.28

w. side

B.M. on 11 ct. - P.C. Curve 5.89 57.80 ✓

7.01 7.21
Top cut.

0.03 63.69 12.78 63.66

0.37 76.44 7.64 76.07

63.69 ✓

B.M. 4.65 83.71 79.06

sw Bird Pond
aka Jolla Blvd.

19.74

Lt.

Rt.

#1
M.H. on W. side La Jolla Blvd. - See sketch

76.44 = H.I.

Top - M.H. #1

9.86 66.58

Flowline

17.80 58.64 ✓

1+50 = Base of cliff on Rocky Beach

2.80

37.5

1+45 = edge of cliff above Beach

27.3 25.8 20.0 20.0 35.2

13.0 14.9 20.3 20.3 4.9

20 7 4 6

1+25

36.0 26.8 27.0 37.0 43.1

T.P. - Hand level

13.00 40.30 ✓

4.3 13.5 13.3 3.3 + 2.56

12 6 8 18

0+90

45.7 35.8 40.30 30.0 42.9

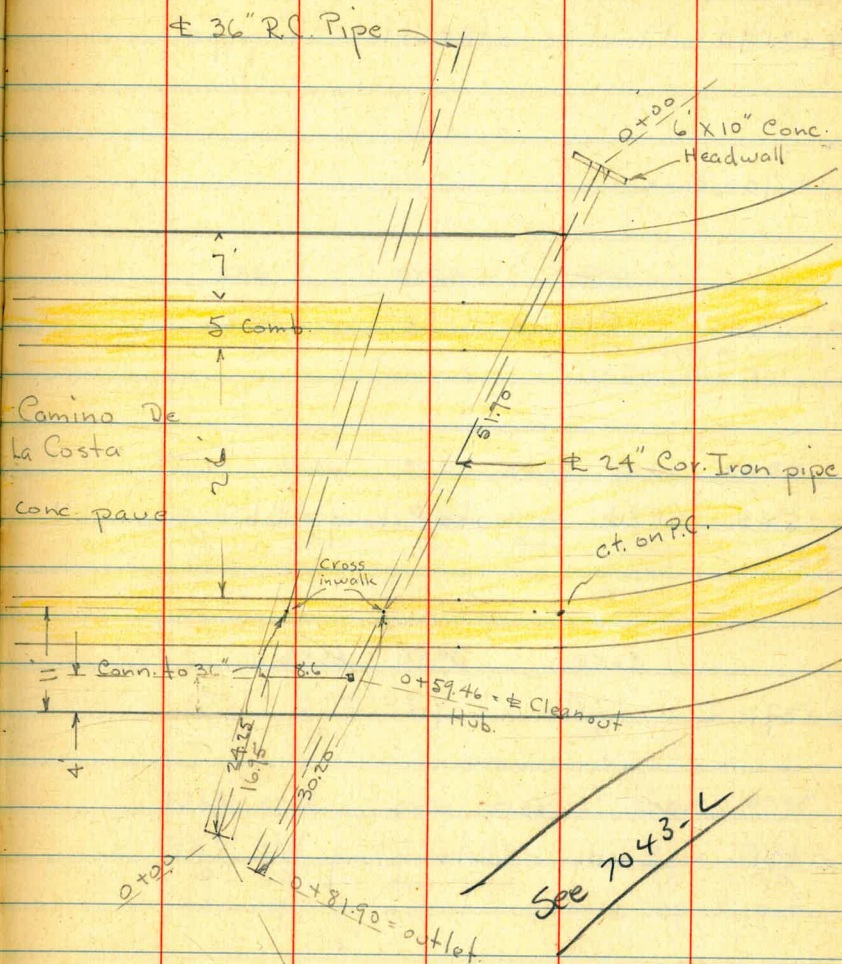
7.6 17.5 23.8 23.3 10.4

15 2 7 15

53.30

Detail of 24" + Connection
to 36" See P. 21

24



± Prop.
Culvert →
See P. 21

0+81.90 = Flowline of outlet 24" pipe

0+70 = Bank

0+59.46 = ± Cleanout

0+50.5 = W. cb. - outs along cb.

0+37 = ± - outs at 90°

0+21.6 = E. cb. - outs along cb.

Conc. wing wall
0+00 = ± Inlet 24" Cor. Iron pipe + ± 6'x10"

3.36 61.16

57.80
C.T. - P.C.
P. 22

Lt. = S ± Rt. = N. 25

85.08

16.08

56.3

4.9

57.6

57.22

57.0

3.6

3.92

4.2

10

on Hub.

8.6 along 4' from P.L.
= Conn. to 36" pipe

57.12

57.50

57.01

56.66

56.67

56.87

4.04

3.66

4.15

4.50

4.49

4.69

10
gut.

10
Top

Top

gut.

10
Top
about
± 36"

10
gut.

57.88

57.96

57.53

3.28

3.70

3.63

10

10

57.63

57.98

57.60

57.35

57.55

57.25

3.53

3.18

3.56

3.81

3.61

3.91

10
gut.

10
Top

Top

gut.

20
Top

20
gut.

58.56

57.53

6.60
Top Conc.
wall

9.63
FL. inlet

61.16 ✓

Xsec Dowling Drive
Electric to Palaman

Moore
Begg
Green
Roberts

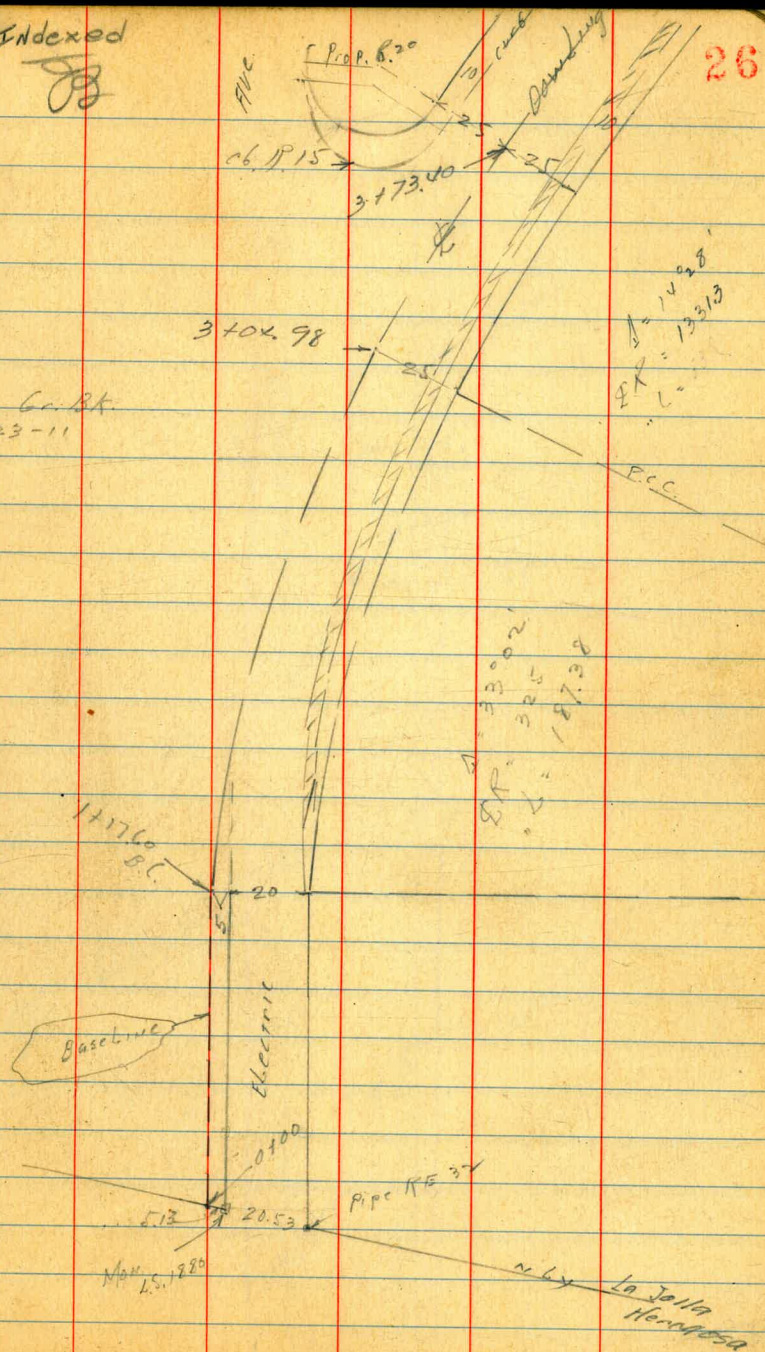
W.O. 31410

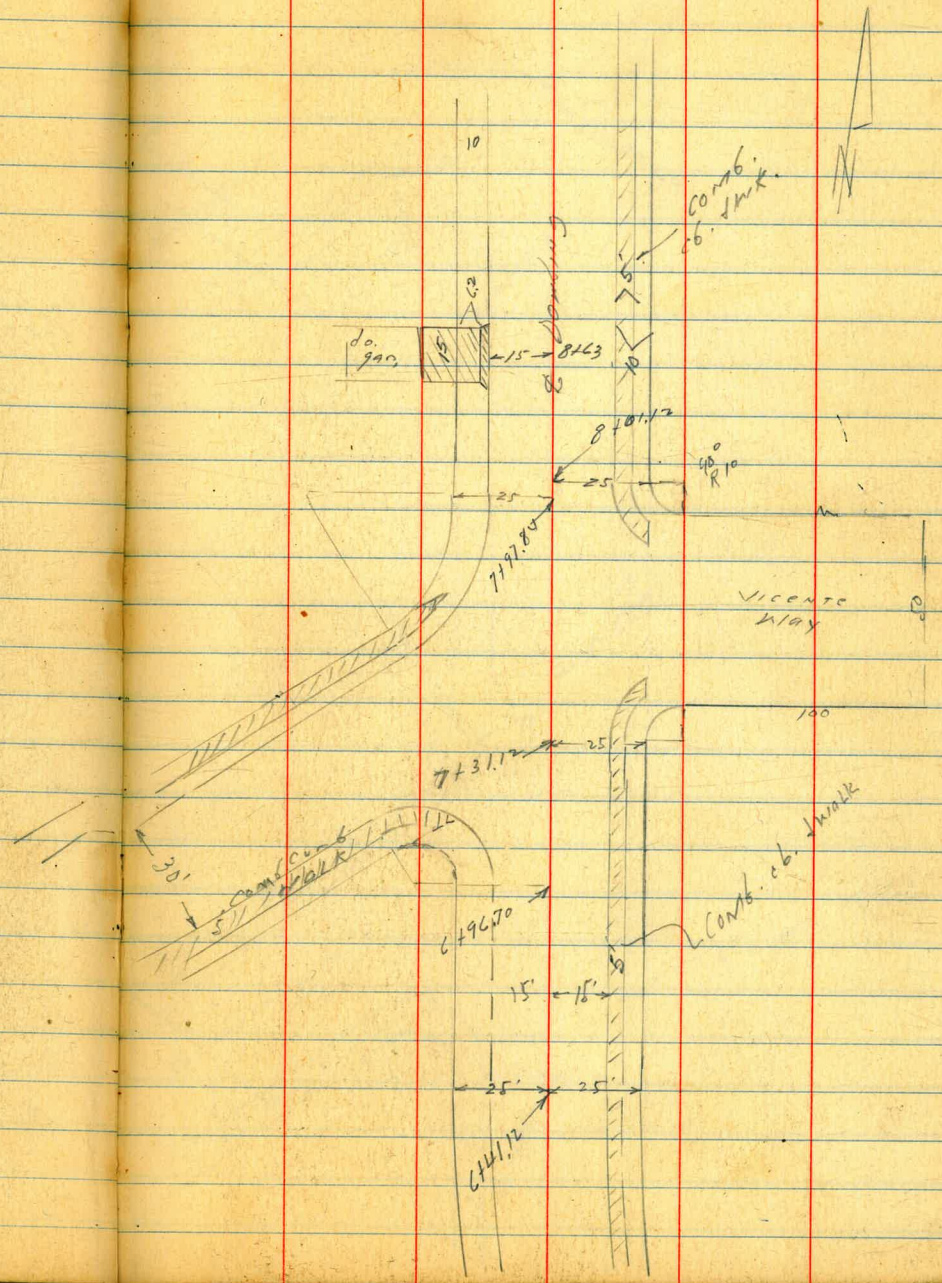
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Ref. G.B. 123-11

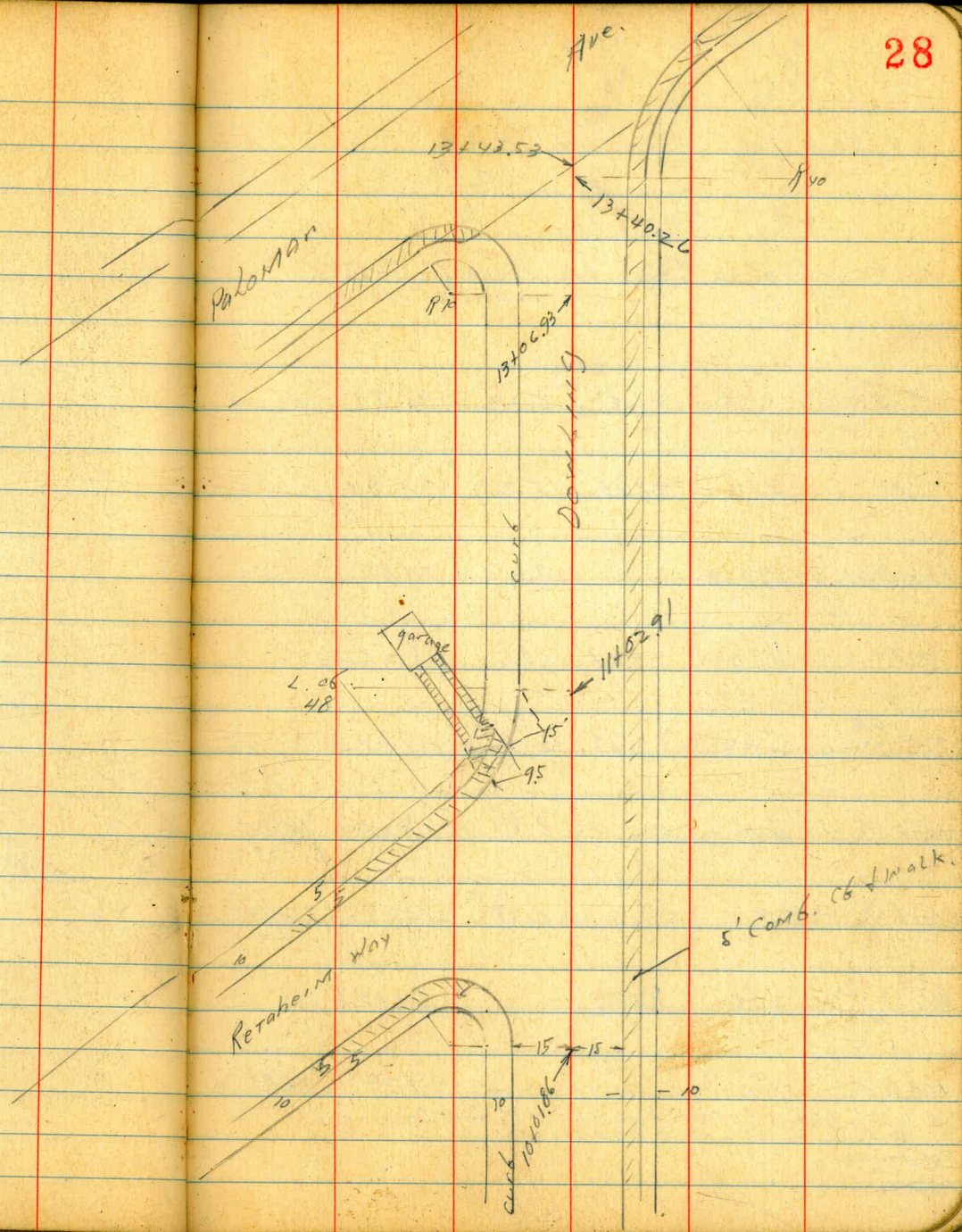
Indexed

JB

See G.B. 123-11







Doubling Dr.

0+50

Sketch p. 26

0+00 Pueblo line St. La Jolla Gables
N.H. La Jolla Hermosa

T.P. ^{set} B.M. 4.95 96.84 5.24 91.89

T.P. 3.19 97.13 5.27 93.94

Set B.M. B.M. PLUG
on curb 4.36 94.85

T.P. 10.95 99.21 1.59 88.26

T.P. ^{G.B.} 123-11 5.44 89.85 2.74 84.41

check to N.E.B.P. 8.71 78.44 78.83

check to S.E.B.P. 2.38 83.77 83.80

Ed. 15' R. ^{H.6} 2.74 87.15 84.41

N.E.B.P. This Roman rebuilt 79.22 78.83 =
La Jolla Blvd. in 1929 and old B.P. was destroyed
and at that time
Palomares
G.B. 123-12

Lt

89.94

6.9
30

90.19

6.7
30

Baseline

4.9
30

92.09

4.8
22

92.64

5.2
20

92.19

4.7
22

97.99

2.4
30

99.69

5.2
30

29

96.84
Set B.M. B.P. E. curb Doubling at Electric. 15' Pt. of
Sta. 3+50
± 5' North of F. Hyd.

S.E. Doubling + Retainer about 15' South of F. Hyd.

15' R. Hub. S.E. Cor. Electric + Palomares

La Jolla Blvd + Palomares

Rosemont + Electric

S.E. Cor. Palomares + Electric Ave. G.B. 123-11.

Received from USC+G DATUM
B.P. set by Walker about 1923

1 + 84 Beg. full width walk on Pt

1 + 70 Beg. narrow walk

155.07

1 + 40 E. drive 10' wide

1 + 17.6 B.C. Pt. Beg. curb on Pt.

1 + 00

96.84

27

88.94

$\frac{1.9}{30}$

89.94

$\frac{7.9}{50}$

88.94

$\frac{7.9}{30}$

89.04

$\frac{7.8}{30}$

89.74

$\frac{7.1}{13}$

89.34

$\frac{7.5}{21}$

90.04

$\frac{6.8}{9}$

90.34

$\frac{6.5}{10}$

90.04

$\frac{6.8}{10}$

90.84

$\frac{6.0}{30}$

90.84

$\frac{6.0}{30}$

91.04

$\frac{5.8}{30}$

90.94

$\frac{5.9}{30}$

92.20

$\frac{4.6}{30}$

92.19

$\frac{4.6}{30}$

92.14

$\frac{4.70}{30}$

91.70

$\frac{5.4}{30}$

92.34

$\frac{4.50}{30}$

93.34

$\frac{3.5}{30}$

93.54

$\frac{3.3}{30}$

92.77

$\frac{4.07}{30}$

93.14

$\frac{3.7}{30}$

93.54

$\frac{3.3}{30}$

93.54

$\frac{3.3}{30}$

95.07

$\frac{1.77}{30}$

93.74

$\frac{1.01}{30}$

93.74

$\frac{1.01}{30}$

30

96.84

3+73.4

T.P.
8M, 15' RT
3+50

3+53

3+04.98

PCC.

2+67.5

2+30.03

1+92.55

547

97.36

4.95

91.89

Note! walks & drives

only shown where

Drives dip thru. Curb and walks

96.84

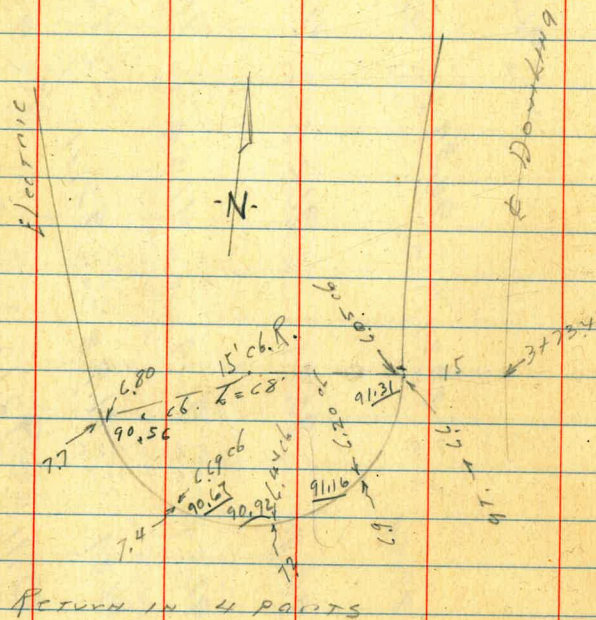
91.96	91.31	90.76	91.56	91.76	91.68	91.91	91.96	31
5.9 25	6.05 15 06	6.6 27	5.8 7.5 9+	5.6 7.5 9+	5.8 15 06	5.45 20 walk	5.4 25 Lawn	
91.06	90.34	90.34	91.34	91.74	91.88	91.93	92.84	
5.78 25.6 7.0 16. 10+	6.5 25		5.5 91.34	5.7 7.5 9+	4.96 7.5 06	4.91 20 walk	4.0 25	
91.14	91.14	91.74	91.54	92.00	92.06	92.74		
5.7 35	5.4 25		5.3 14.9 9+	4.84 14.9 06	4.78 19.9 walk	4.1 25		
90.34	90.34	91.24	91.54	92.11	92.18	92.94		
6.5 30	6.5 30	7.6	5.3 14.8 9+	4.73 14.8 06	4.66 19.9 walk	3.9 25 Lawn		
88.94	90.94	91.14	91.94	92.12	92.64	93.24		
7.9 30	7.9 30	5.7 14.8 9+	5.7 14.8 9+	4.86 14.8 06	4.72 19.8 walk	4.2 25 Lawn		
90.74	91.54	91.84	92.11	92.25	93.24			
6.1	5.3 7	5.0 15.9 06	4.73 15.9 06	4.59 20.9 06 walk	3.6 30			

96.84

Dowling

47490v

47010v



97.36

32

4					
91.96	91.85	91.36	92.00	92.26	92.43
5.2	5.51	5.0	5.6	5.5	4.93
25	15	15	15	15	15
	06				06
91.66	91.53	91.06	91.66	91.86	92.04
5.7	5.83	6.0	5.7	5.5	5.37
25	15	15	15	15	15
	06				06
					WALK
					92.88
					20
					WALK
					92.48
					25
					92.76
					25
					92.06

97.36

6+4112 E.C.

6+09 E 12' Con. Drive to S.W. 900,

5+9310 Note! E.L. or RT.
is on terraced lawn slope

5+V508

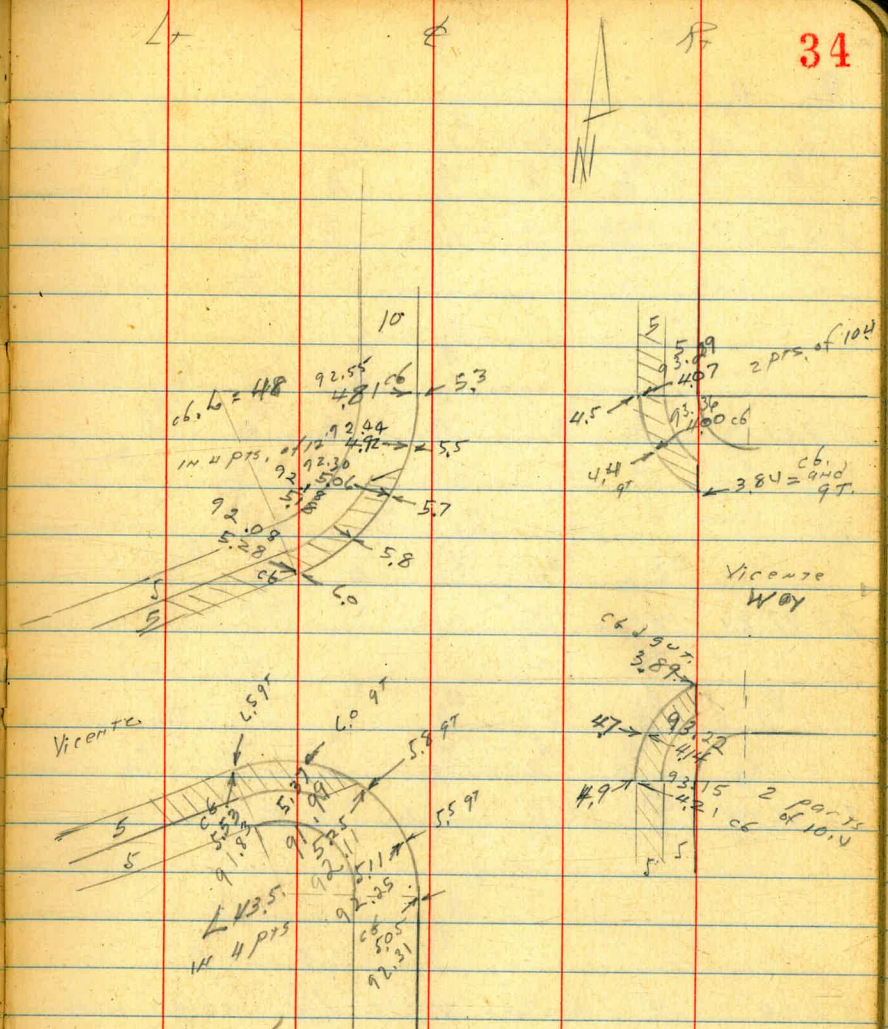
5+324 E 7' Con. Drive

4+970C

9736

3.4	4.16	4.7	4.1	3.8	3.68	3.61	1.3
25	15	15	15	15	15	20	25
cb	cb	cb	cb	cb	cb	wt.	wt.
94.00	93.10	93.00	92.96	93.26	93.52	93.68	93.75
3.36	4.26	4.38	4.90				
25	20	108	15				
Floor	wt.	CON.	CON.				
4.1	4.48	5.0	4.2	4.4	3.98	3.91	3.4
25	15	15	15	15	15	20	25
cb	cb	cb	cb	cb	cb	wt.	wt.
92.06	92.53	92.06	92.76	92.86	93.06	93.45	95.00
4.8	4.83	5.3	4.6	4.5	4.30	4.23	3.0
25	15	15	15	15	15	20	25
cb	cb	cb	cb	cb	cb	wt.	wt.
92.36	92.21	91.96	92.36	92.56	92.72	92.70	91.36
5.0	5.15	5.9	5.0	5.0	4.64	4.55	3.0
25	15	15	15	15	15 = cb on drive	20	25
cb	cb	cb	cb	cb	cb	wt.	wt.

9736



T.P. 509 9860 3.85 93.51
 L+967 B.C. on LT.
97.36

93.36 93.55 93.0 9860 93.46 94.07 94.16 95.36
 4.0 3.81 4.4 3.8 2.9 3.29 3.20 2.0
 25 15 15 15 15 20 25
 cb. cb. cb. cb. cb. cb. cb.
97.36

8 + 50

8 + 01.12

7 + 97.84 BC on LT

7 + 66.12 2 Vicente Way to Rt

7 + 64.12 2 Vicente Way to Lt Sec. 11 with
approach

7 + 31.12 BC, C6 on Rt

98.60

92.10	93.97	93.50	94.10	94.20	94.60	94.70	95.90
4.5 25 Lawn	4.63 15 C6	5.1 15	5.5	4.4 15	4.00 15 C6	3.91 20 Walk	2.7 25 Lawn

99.00	93.81	93.40	93.90	94.1	94.513	93.58	96.20
4.6 25 Lawn	4.79 15 C6	5.2 15	4.7	4.5 15	4.07 15 C6	4.02 20 Walk	2.4 25 Lawn

93.46	92.90	93.30	93.60	94.20	94.56
4.6 25 Lawn	4.81 15 C6	5.3 15	4.8	4.4 15.3 97	4.04 15.3 C6

93.46	92.90	93.30	93.90	94.40	94.90	96.60
5.14 25.5 C6	4.7 25.5 97	5.3 15.3 97	4.7	4.2 15	3.7 25	2.0 50

91.90	93.10	93.90
4.7 80	5.5 31	4.7

93.00	93.80	93.70	94.39	94.79	95.20
5.6 25	4.8	4.7 15	4.21 15 C6	4.11 20 Walk	3.4 25 Lawn

98.60

3.73 98.58

BM. BP
P. 29

3.74 94.86 94.85
P. 29

10 + 01.86 BC. curb on left

9 + 50

9 + 36 Drive way to single garage 8' wide

9 + 05 Power pole 17.6 left 6A.24

9 + 00

8 + 63 @ 17' Condr. thru curb
to db. garage

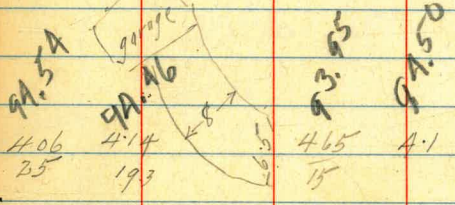
98.60

4.50
33.8
20.5
Floor

drive
15' wide

4.62 4.70 5.07
25 18.8 15
↑ ↑
Con. drive

93.98	94.20	94.21	93.70	94.30	94.30	94.60	94.94	95.40
4.4 25	4.4 25	4.39 25	4.0 15	4.3 15	4.3 15	3.80 20	3.66 20	3.2 25
93.90	94.20	94.21	93.70	94.30	94.30	94.60	94.94	95.40
4.62 25	4.70 25	5.07 15	5.1 15	4.5 15	4.5 15	3.80 20	3.66 20	3.2 25
↑	↑	Con. drive	↑	↑	↑	↑	↑	↑
drive	drive	drive	drive	drive	drive	drive	drive	drive
15' wide	15' wide	15' wide	15' wide	15' wide	15' wide	15' wide	15' wide	15' wide



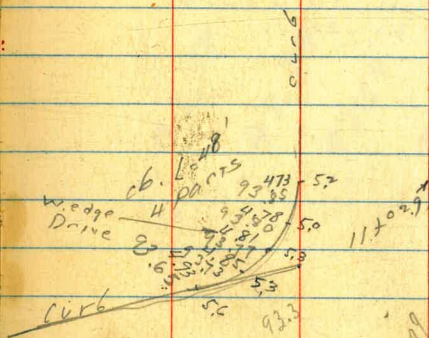
91.20	91.57	93.70	94.30	94.40	95.07	95.16	95.60	
4.4 25	4.03 25	4.9 15	4.3 15	4.2 15	3.53 20	3.44 20	3.0 25	
91.20	91.57	93.70	94.30	94.40	95.07	95.16	95.60	
4.4 25	4.03 25	4.9 15	4.3 15	4.2 15	3.53 20	3.44 20	3.0 25	
91.54	94.26	94.94	93.95	94.50	94.40	94.93	95.03	95.60
4.06 25	4.14 19.3	4.1 19.3	4.65 15	4.1 15	4.2 15	3.67 20	3.57 20	3.0 25

L+ & R+

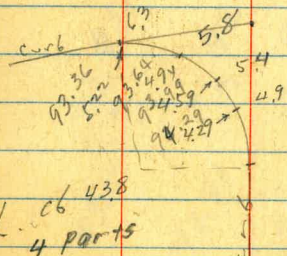
BM
T.P. 1/29 353 9838 3.73 94.85
H 10291 BC Lt.

10 ± 51.57 Sec at 90° on Rt + Lt

91.58	93.85	93.86	94.06	94.00	94.95	94.90	95.68 ⁸⁷
4.0	4.73	5.2	4.5	4.6	4.13	4.04	2.9
25	15	15	45	15	15	20	25
Lawn	cb				cb	Wt	
93.88	94.38	94.26	94.92	94.90	95.38		
4.7	4.2	4.3	3.76	3.68	3.2		
25		15	15	20	25		
			cb	Wt			



Petahem



98.58

98.58

12 + 41.5251Rt end con. BK wall

+ 35 21.3 Rt PP 6467

12 + 07

12 + 01 24.8 Lt end wire fence

12 + 00 Beg. ^{Block} Con. wall 25.1 Rt

11 + 96 E 10.5 Con. drive thru curb
8' wide at 20 Rt

+ 75

11 + 65 E 14' con. drive thru curb

11 + 50

11 + 28 24.9 Lt Beg. wire fence

10 + 82.07

Back this up.

9838

5.1	5.1	5.9	5.1	5.0	4.65	4.60	4.2	2.50
25	15	15	51	15	15	20	25	25
	06				06	wt		Top
								Walk
93.28	93.22	92.78	93.26	93.38	93.73	93.78	91.14	95.62
93.38	93.39	92.64	93.54	93.38	93.93	93.02	92.66	94.75
5.0	4.99	5.7	4.8	5.0	4.45	4.37	2.8	
24.8	15	15		15	15	20	25	
Fence	06				06	wt	Low	
93.38	93.39	92.64	93.54	93.38	93.93	94.01	95.58	
5.0	4.99	5.7	4.8	5.0	4.45	4.37	2.8	
24.8	15	15		15	15	20	25	
Fence	06				06	wt	Low	
93.38	93.39	92.64	93.54	93.38	93.93	94.01	95.58	
4.7	4.80	5.5	4.6	4.8	4.28	4.20	1.7	
24.9	15	15		15	15	20	25	
Fence	06				06	Walk	Low	
93.64	93.58	92.88	93.78	93.58	94.10	94.18	96.68	
4.49	4.57	5.02	4.2	4.3	3.81	3.72	2.9	
24.6	23.3	19.5		15	15	20	25	
inside	in	gt.		06	06	wt		
edge	drive	drive						
93.64	93.61	93.36	94.16	94.08	94.57	94.61	95.78	
4.49	4.57	5.02	4.2	4.3	3.81	3.72	2.9	
24.6	23.3	19.5		15	15	20	25	
inside	in	gt.		06	06	wt		
edge	drive	drive						
93.64	93.61	93.36	94.16	94.08	94.57	94.61	95.78	

13 + 0693 16. BC on 17

13 + 102 8 8.5 Con. drive show curb
20 Ft. do. Con Ribbon drive
7.3 extra all

12 + 95

12 + 86 4 9.5 Con. drive show curb
7.8 wide Con drive or 20 Ft.

12 + 78

12 + 50

9838

5.9 25	5.83 15 CB	6.6 15	6.0	5.8 15	5.28 15 CB	5.30 20 Wk	4.2 25 Lawn
92.14	92.55	91.78	92.38	92.58	93.10	93.06	91.18
5.9 25	5.77 15 CB	6.5 15	5.9	5.7 15	5.30 15 CB	5.25 20 Wk	4.0 25 Lawn
92.48	92.61	91.88	92.44	92.68	93.04	93.13	91.38
5.71 15 Con	5.19 18 Con	5.15 20 Con	3.85 25 Con	5.71 15 Con	5.19 18 Con	5.15 20 Con	3.85 25 Con
5.8 25	5.53 15 CB	6.6 15	5.8	5.8 15	5.16 15 CB	5.06 20 Wk	3.7 25 Lawn
93.06	92.90	92.14	92.78	92.78	93.27	93.32	91.68
5.3 25	5.48 15 CB	6.2 15	5.6	5.6 15	4.97 15 CB	4.86 20 Wk	3.6 25 Lawn
93.06	92.90	92.14	92.78	92.78	93.27	93.32	91.68

9838

13.4 x 3.53 Sec. on S.L. Polonina

$$\begin{array}{r} 6.33 \\ 32.7 \\ \hline 39.03 \end{array}$$

13.4 x 0.26 c6 BC RT. Sec at 90°

9838

	91.58	91.38	92.18	93.18	93.98	94.58	94.93
	6.8	7.0	5.9	5.2	4.9	3.80	3.45
	32	26	15		20.2	20.2	27.8
	98	dirt	dirt		dirt	ck	WALK
			72.08	93.00	93.06	94.05	94.08
		6.3		5.4	5.4	4.33	4.30
		25		15	15	20	25
		dirt			ck	WALK	LOWN

9838

1 sec of Palomares Ave
 Electric Ave to Ely end.

WD 31410

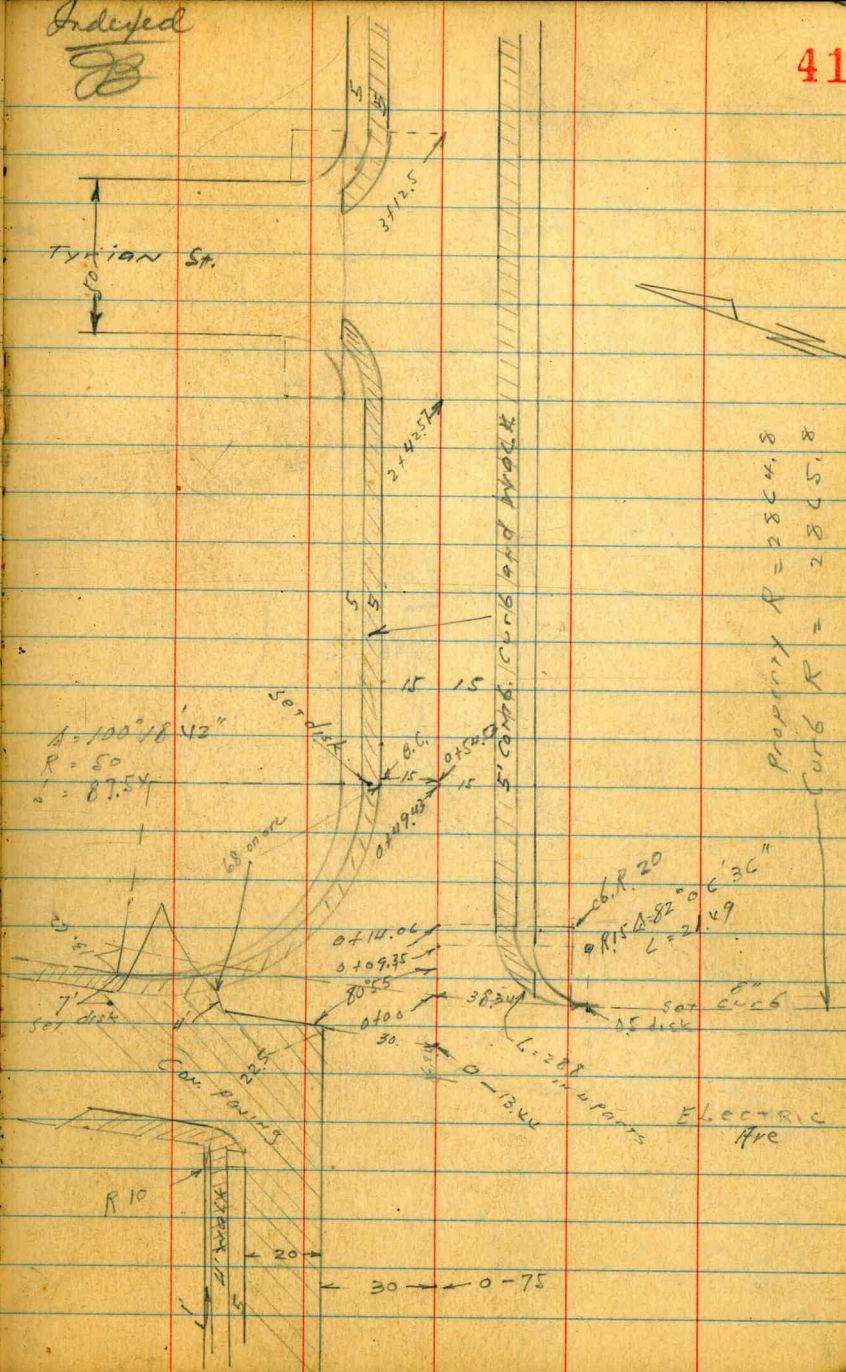
Ref. G.B.K. 123-11 for TIO PTS.

Note: Imprints, walls,
 walk etc. have been
 constructed out to
 inside edge of 5' sidewalks.
 Paving is the improvement
 needed with the exception
 of sidewalk on the wily
 side of Downing Drive

Indexed
 B

41

Tylian St.



$A = 100' 10' 42''$
 $R = 50$
 $S = 87.54$

Property R = 2844.8
 Curb R = 2845.8

ELECTRIC
 Ave

R 10

0-75

0+09.35 Prop Line Radial

0+00 E Line of Electric Ave

- 13.44 Sec p 41 (80° 55' to d)

- 20 E Elec to Right

- 35 E Electric Av to Left and along E

- 50

- 75

3.22 87.63

SE. 15' R. Hub
Palomares
and
Electric
C.D. 123-11

84.41

87.63

4.69	4.37	4.29	4.6	4.6	4.6	4.6	4.6	4.5	3.96	4.2	3.26
52.6	33.8	29.9	33.8	29.9	15	30	30	50	30	100	100
82.99	83.00	83.59	83.03	83.94	82.93	83.03	82.93	83.15	83.67	84.27	83.52
4.43	4.84	4.44	4.7	4.6	4.6	4.7	4.6	3.8	4.6	3.8	3.8
70	49.5	30	15	15	30	30	50	100	50	100	100
83.15	82.61	83.03	82.53	82.73	82.53	82.43	82.23	83.53	82.93	83.03	83.53
4.48	5.02	46.0	51	4.8	4.8	5.2	5.2	3.8	4.6	3.8	3.8
70	50	31	15	15	15	30	30	100	50	100	100
82.96	82.23	82.73	82.33	82.03	82.03	82.23	82.23	83.53	82.93	83.03	83.53
4.67	5.38	4.90	5.3	5.6	5.6	5.4	5.4	3.8	4.6	3.8	3.8
60	50	30	15	15	15	30	30	100	50	100	100
82.43	81.81	82.15	81.23	81.13	81.13	81.33	82.23	83.53	82.93	83.03	83.53
5.20	5.82	5.48	6.4	6.5	6.5	6.3	6.3	3.8	4.6	3.8	3.8
60	50	30	15	15	15	30	30	100	50	100	100

1 + 00

0 + 54.53

0 + 54.53 curb BC

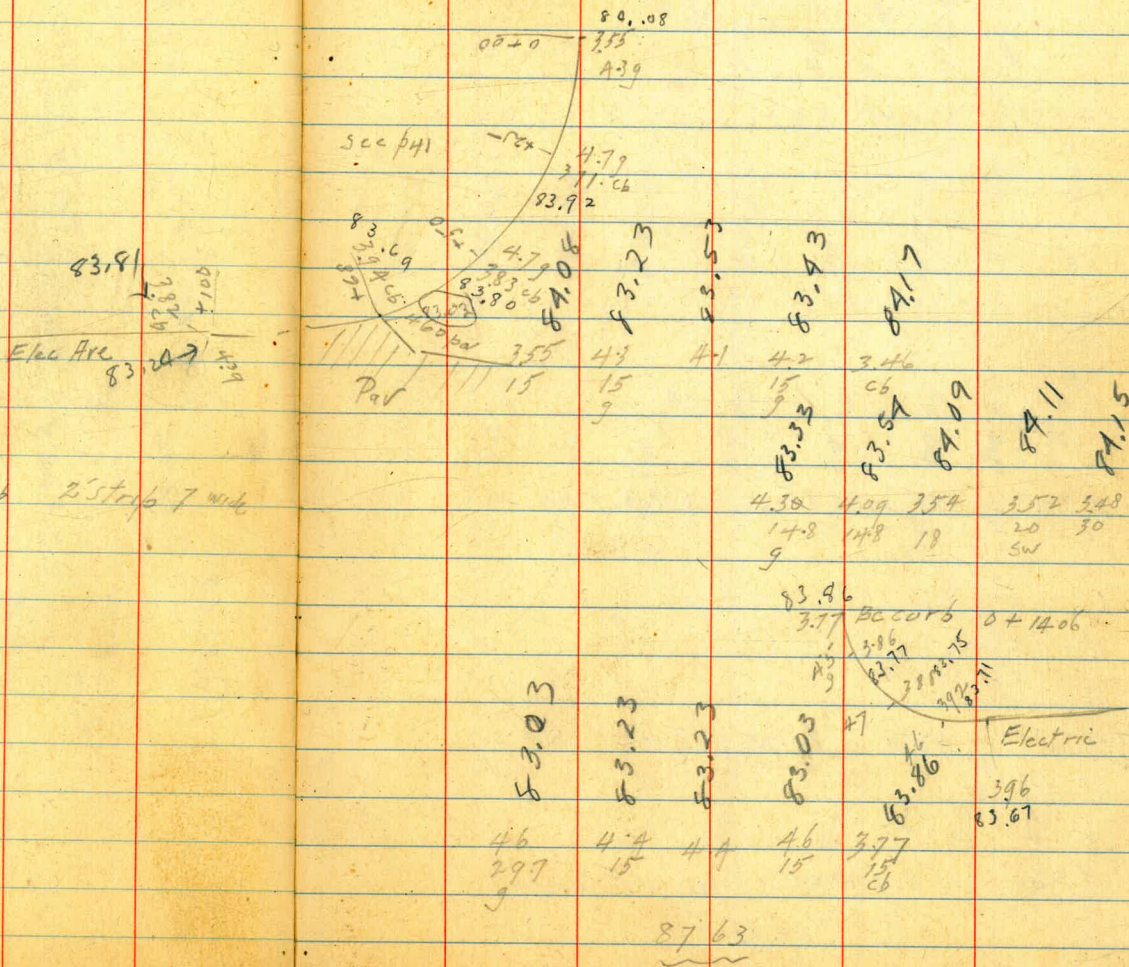
0 + 43 14.8R of drive way 7.3 of 2' strip 7 wide

0 + 14.06

0 + 14.06 BC of curb return

87.63

87.53	87.97	87.38	87.52	87.03	87.93	87.92	87.94	87.63	44
2.8	3.16	3.25	3.8	3.6	3.7	3.21	3.19	3.0	
25	SW	CB	15		15	CB	SW	25	
	20	15					20		



87.63

3+12.50

BC curb to left

2+77.6

Pyran d

2+42.63

BC curb to left

2+00

1+49.5

15' left 85' op 2' strip 7' wide drive

T.P.

6.54 90.75 3.42 84.21

1+27

15 ft driveway 17' open 14.5' driveway
87.63

Handwritten notes and diagrams on the right page of the notebook. The page contains a grid with various numerical entries and two diagrams of triangles.

Diagram 1 (top left): A triangle with vertices labeled 460, 462, and 46. Sides are labeled 46, 48, and 5.1. A value of 85.95 is written near the triangle.

Diagram 2 (top right): A triangle with vertices labeled 460, 462, and 46. Sides are labeled 46, 48, and 5.1. A value of 85.65 is written near the triangle.

Diagram 3 (middle left): A triangle with vertices labeled 538, 541, and 5.41. Sides are labeled 2.5, 2.0, and 1.5. A value of 85.75 is written near the triangle.

Diagram 4 (middle right): A triangle with vertices labeled 578, 5.41, and 5.41. Sides are labeled 5.7, 5.5, and 5.8. A value of 84.97 is written near the triangle.

Diagram 5 (bottom left): A triangle with vertices labeled 6.51, 6.9, and 6.7. Sides are labeled 2.5, 2.0, and 1.5. A value of 87.21 is written near the triangle.

Diagram 6 (bottom right): A triangle with vertices labeled 6.04, 6.00, and 5.7. Sides are labeled 1.5, 2.0, and 2.5. A value of 87.15 is written near the triangle.

Other numerical entries in the grid include: 4.6, 4.8, 5.1, 5.2, 5.5, 5.8, 5.47, 5.45, 5.0, 4.61, 4.58, 4.4, 8.13, 86.35, 85.95, 85.65, 85.25, 85.66, 85.28, 85.30, 85.75, 85.75, 85.95, 85.05, 85.25, 84.95, 85.28, 85.30, 85.75, 85.00, 85.25, 85.75, 85.05, 84.95, 84.67, 85.03, 85.00, 85.25, 84.71, 84.75, 85.05, 84.23, 84.09, 87.57, 87.62, 86.13, 87.63, 3.4, 3.54, 3.06, 3.01, 2.58, 1.5, 1.8, 2.0, 2.5.

+ #1 -
3.51 98.36

94.85
Correction

LT # RT

TP 1.95 94.86 94.85 (oj)

TP 6.93 96.81 0.87 89.88

4+495 9' Dir way 15' ft 8' op 7' strip

4+23 15' ft dbl gorges 2' strip on east side 7'

4+02 to 4+46 Stone & Mortar ret wall 20' ft

4+00

3+64.5 to 3+98 Stone & Mortar ret wall 20' Left

3+60 15' ft drive 9' op 2' strip 7'

3+43 15' ft drive 8.5' op 2x2' strips 7'

90.75

89.55	89.52	89.45	88.75	89.05	88.75	88.55	89.45	89.47	89.55
1.9	1.27	1.20	2.00	1.7	2.0	2.2	1.30	1.28	1.2
25	20	18	cbg	9	15	15	cb	5w 20	25
			15	15					
					88.25	87.95	88.37	88.82	88.83
					2.5	2.8	2.38	1.93	1.92
					14g	cb line	18	20	25
							15		
88.55	88.3	88.23	87.55	87.65	87.65	88.32	88.27	88.95	
2.2	2.45	2.52	3.2	3.1	3.1	2.52	2.47	1.8	
25	20	cb	15	15	15	cb	20	25	
		15							
87.77	87.38	87.43	86.71	86.75	86.55	87.27	87.31	87.45	
2.98	3.77	3.42	4.04	4.0	4.2	3.48	3.44	3.7	
25	20	18	15	cbg	9	15	cb	20	25
						86.37	86.88	86.87	87.05
						4.88	3.89	3.88	3.70
						cbg	18	20	25
						15			

90.75

Saily Return at Dowling

#4 06 E.C.

#3

H2

Part #1

5 + 38.40 = 8.5 Cubic m Ft.

+ 13.5

15 Lt

9' wide do. 2' Con. strip
 2 Con. drive then c. 6

7' overcut
 Ribbons

5 + 0.6

4 + 5.5

98.36

7.0	7.2	7.1	7.5	7.2	7.0	7.7	7.7	7.6	7.7	7.8
25	20	15	15	15	15	15	15	15	20	25
	Walk	06				9.6	Walk			
91.26	91.11	91.06	90.38		90.76	91.6	91.89	91.66	91.96	
7.10	7.25	7.30	7.98		8.2	8.7	8.7	8.7	8.5	
25	20	18	15		15	15	20	25		
	Bag	Con	Con							
	Ribbons									
89.56	89.61	89.52	89.26	88.86	89.56	89.55	89.60	89.86		
8.8	8.75	8.84	9.1	9.5	9.8	8.81	8.76	8.5		
25	20	15	15	15	15	15	20	25		
Walk	Walk	06				06	Walk	06		

98.36

91.76
 91.76
 91.76
 91.56
 91.16
 91.8
 91.76
 92.07
 92.33
 92.55
 91.96
 91.96
 91.96
 91.96
 91.96
 91.96
 91.96

47

#4 6 EC. at Palomares

#3

#2

#1

Return 4 eg, P Ts,
on Dowling
B.C. Curb STA 13 + 40.26 P 28

S.E. by Return at Dowling

6 + 05.53

5 + 93 15' 1/2 E 12.5 Considerable 7' high curb

98.30

95.16 94.46 94.38 93.46 93.96 93.86 93.36

3.2	3.9	3.98	4.9	4.7	4.7	4.7
25	20	15	15	15	15	25
Lawn	Walk edge	cb	cb			

94.06 93.83 93.29 93.16 93.46 93.66 93.26

4.36	4.43	5.07	5.2	4.9	4.7	5.1
25	20	15	15	15	15	25
Can.	cb.	dirt				

↑ in drive
Bag do. Can.
Ribbons 1 1/2 wide
7' over all

98.30

94.86 95.86

3.7	2.50
7.7	2.50
4.1	1.50
9.7	0.06
4.2	3.42
9.7	0.06
4.9	1.40
9.7	0.06
17.3	4.30
9.7	0.06

95.36 94.91 94.50 94.06 93.86 93.36

0+21.68 PRC

0+10.84

0+00 cb and gut levels on Rt.
C+81.87

7+21.55 E "Banjo"

C+81.87 Sketch pvt BC, Rt + Lt. "BANJO"

T.P. 10.95 108.09 1.22 97.14 96.35

C+48.3 15' Lt E 9.2 Cor. drive thru cb 20' 9' wide Cor. drive 92.5

C+39.49 cb E.C. on Rt.

98.36

←

→

99.39
 9.7
 97
 97.79
 10.3
 97
 96.89
 11.2
 15
 99.06
 9.03
 06
 98.39
 9.70
 06
 97.83
 97.91
 98.99
 99.29
 8.8
 S. Line
 Lawn
 98.59
 9.5
 S. Line
 Lawn
 9.1
 25

98.19
 9.9
 25
 Lawn
 10.40
 20
 Walk
 10.50
 15
 97.59
 11.2
 15
 96.89
 10.8
 15
 97.29
 11.2
 15
 96.89
 10.26
 15
 06
 97.83
 10.8
 20
 97.91
 9.1
 25
 Lawn
 96.22
 2.4
 20
 Cor
 96.20
 2.6
 18
 Cor
 95.70
 15
 20
 95.26
 3.1
 14
 108.09
 95.16
 3.2
 15
 95.16
 96.25
 2.1
 15
 06
 96.27
 2.09
 20
 Walk
 97.56
 0.8
 25
 Lawn
 96.21
 2.1
 25
 Lawn
 95.89
 2.50
 20
 Walk
 95.78
 2.58
 15
 06
 97.17
 3.6
 15
 30
 95.36
 3.5
 15
 06
 97.84
 2.50
 15
 06
 95.84
 2.44
 20
 Walk
 95.92
 1.2
 25
 Lawn
 97.26

98.36

0+57.73

0+46.68 PRC

0+39.8 end con drive

0+34.13

0+31.3 2 Con drive

0+23.5 Beg. Con drive

108.09

4

4

101.09

7.0
97

101.99

6.10
26

102.19

5.9
5.2

50

100.39

7.7
97

101.29

6.85
26

101.79

6.3
5.2

100.17

7.92
97
26

100.64

7.45
3 RT of 26

100.59

7.50
5 RT of 26

99.66

8.43
97
26

100.15

7.94
3 RT of 26

100.19

7.90
5 RT of 26

99.72

8.67
26
97

99.92

8.17
3 RT of 26

99.93

8.16
5 RT of 26

98.86

9.29
26, 4 gu, in drive

99.29

8.80
3 RT of 26

99.31

8.78
5 RT of curb

108.09

0+49.6 = Wedge Con drive

101.09
7.0
N.L.
Lawn

100.25
7.84 7.87 8.41
5 LT
of cb 3 LT
of cb 6 in drive

0+21.68 PRC

on drive →

98.57 98.97 98.90 98.09
9.52 9.62 9.69 10.0
10 LT N.L. 5 LT of cb 6 97

+14.24 LT 12.5 Con do. thru cb.

98.47 98.19 98.15 97.67
9.62 9.90 9.94 10.02
Con. N.L. Con 2.5 Con 6 49 in drive

0+10.84

98.39 98.01 97.49
9.7 10.08 10.6
10 LT of cb 5 LT of cb 97 and cb in drive

0+00 = 1481.87 = BC cur cb

98.19 97.69 N.L. 97.59 96.89
9.9 10.40 10.50 11.2
25 20 15 95
Lawn walk cb 97

Levels on cb, etc. on N side of "B4470"

0+68.69 = end cb. on N side old Row 1.

10809

10809

102.55
5.5x
cb 49 ft.
108.09
5.0
5.6

7+61.55 Skerch P42

1+0531 E.C. end of cb + walk

0+954 LT Can drive through 7.3 wide
do. can fit 6.2' wide 7' overcall
at N.L.

0+832 PRC

0+5984 Edge Can drive thru

0+5244

108.09

L +

	103.69	103.18	103.1
4.0	4.91	4.99	
10 LT	5.27	7' + curb	
	of cb.		
4.4	5.30	5.37	5.83
N.L.	5.47	3.5	6.69
	of cb	LT of cb	
	102.79	102.72	102.26
	103.49	102.43	102.3
4.6	5.6	5.79	6.7
N.L.	5.27	6.6	7'
	of cb		
	100.87	100.85	100.3
	101.21	100.3	100.08
6.88	7.22	7.24	7.79
N.L.	5.27	3.17	6.6
drive	of cb	of cb	9.4
	101.19	100.40	100.37
6.9	7.09	7.72	8.27
N.L.	5.47	3.47	6.6
Lawn	of cb	of cb.	in drive

R +

102.59

5.5

108.09

BM 854 94.85 94.85
 T.P. 0.41 103.39 11.54 102.98
 T.P. 0.47 114.52 7.54 114.05

8 + 47

8 + 17

8 + 10 E. edge Emb.

T.P. 3.6 ✓ 121.59 0.64 117.97

7 + 93 W. edge Embankment

7 + 80 Levels over old RR Road

T.P. 12.71 118.61 2.19 105.90

108.09

Lr

Baseline

Rr

53

00 BM 629

120.19
 1.4 38 48 4.9 + 0.7
 75 25 25 75
 116.79 117.79 116.79 116.69 122.29
 5.7 8.1 8.3 11.28 8.6 7.6
 75 25 25 F.C. 25 75
 INLET 24" pipe
 118.69 117.79 117.49 116.99 116.09 113.99
 2.9 3.8 4.1 4.6 5.5 7.5
 75 25 25 25 75
 118.11 117.31 121.59 116.31 115.91
 0.5 1.3 1.9 2.3 2.7
 75 25 25 25 75
 110.31 108.01 108.31 106.17 106.61 106.21
 8.3 10.6 10.3 12.44 12.0 12.4
 75 25 25 F.C. 25 75
 OUTLET 24" pipe
 118.61
108.90

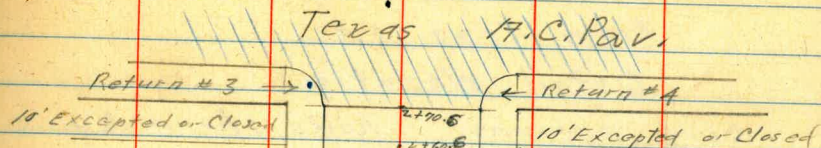
Cross Sec. LANDIS
Texas to Louisiana

~~Indexed~~

12-12-47
V.V.O. # 31400

Sommermeier
W Moore
E Sherman

See FB 2340-52 etc.



For E.Ls.
on curb
Returns see P55



LANDIS

Sta. 0100 - 10 ft. Page 56
paving grade. see levets. for
was taken at point to be met for
Elevation shown for point A (opposite page)

Aprox. 12 sq. ft.
Needs .05 top
because of
settlement

10' Excepted or Closed

10' Excepted or Closed

Ret #1

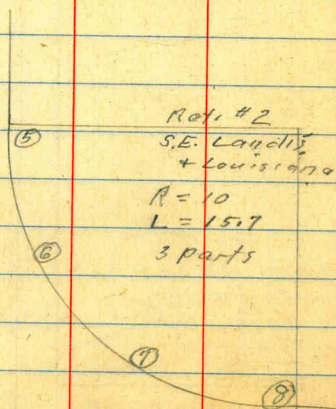
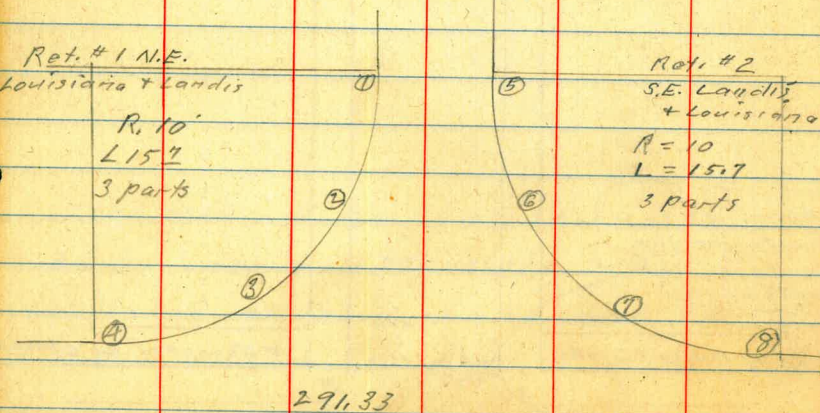
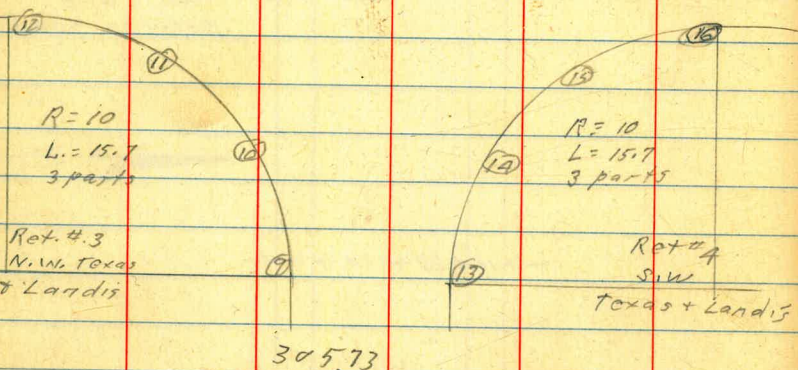
LOUISIANA - H.C. Pav.

Return #2

From Page 54

Detail elevations

Curb Returns. Rods shown by



Numbers

4.24	3.86	4.24	3.86	4.26	3.87	4.41	3.91
13	13	14	14	15	15	16	16
P	C	P	C	P	C	P	C

3.52	2.86	3.55	2.87	3.56	2.90	3.57	2.88
9	9	10	10	11	11	12	12
P	C	P	C	P	C	P	C

305.73 From page 58

285.43	285.91	285.43	285.93	285.44	286.04	285.34	285.95
5.70	5.42	5.85	5.35	5.87	5.29	5.79	5.40
5	5	6	6	7	7	8	8
P	C	P	C	P	C	P	C

285.50	285.90	285.50	285.92	285.45	285.43	285.29	285.34
5.83	5.43	5.83	5.41	5.88	5.39	5.24	5.29
1	1	2	2	3	3	4	4
P	C	P	C	P	C	P	C

291.33 from Page 56

P = Paving C = Top curb

0+25

287.91	286.8	287.2	287.3	287.2	286.6	287.33
3.92	4.5	4.1	4.0	4.1	4.7	4.00
$\frac{20}{cc}$	$\frac{20}{cc}$	$\frac{10}{cc}$		$\frac{10}{cc}$	$\frac{20}{cc}$	$\frac{10}{cc}$

0+10 = old E. Line Louisiana

286.98	286.3	286.3	286.4	286.2	286.1	286.48
4.85	5.0	5.0	4.9	5.1	5.2	4.85
$\frac{20}{cc}$	$\frac{20}{cc}$	$\frac{10}{cc}$		$\frac{10}{cc}$	$\frac{20}{cc}$	$\frac{20}{cc}$

0+00 Cont

285.90	285.50	285.9	285.93	285.91
5.42	5.83	5.4	5.5	5.42
$\frac{20}{cc}$	$\frac{20}{pav}$	$\frac{20}{Ord}$	$\frac{20}{Ord}$	$\frac{20}{cc}$

0+00 Also = End H.C. Pav. = 10' west of old E. line Louisiana

285.79	285.9	285.92	285.72	285.9	285.45
5.54	5.4	5.41	5.61	5.4	5.90
$\frac{10}{pav}$	$\frac{10}{Ord}$	$\frac{10}{Ord + pav}$	$\frac{10}{pav}$	$\frac{10}{Ord}$	$\frac{20}{pav}$

Fit. This (Scootol)

0-10 Cont.

281.09	281.09	283.84	283.18	284.95	285.54	284.78	285.15
10.24	10.24	7.49	8.15	6.38	5.76	6.85	6.20
$\frac{170}{cc}$	$\frac{170}{pav}$	$\frac{80}{cc}$	$\frac{90}{pav}$	$\frac{80}{pav}$	$\frac{80}{cc}$	$\frac{130}{pav}$	$\frac{130}{cc}$

0-10 = East Curb line Louisiana

285.94	285.29	285.52	285.72	285.78	285.70	285.51	285.34	285.93
5.37	6.04	5.81	5.61	5.55	5.63	5.82	5.99	5.40
$\frac{30}{cc}$	$\frac{30}{pav}$	$\frac{20}{cc}$	$\frac{10}{cc}$		$\frac{10}{cc}$	$\frac{20}{cc}$	$\frac{30}{pav}$	$\frac{30}{cc}$

S.E.B.P.
LANDIS &
LOUISIANA

5.45 291.33 — 285.88

291.33

1+75

5.25
20
Cl. 296.83

5.9
20 296.2

5.7
10 296.4

5.6 296.5

5.7
10 296.2

6.5
20 295.6

5.94
20
Cl. 296.14

1+50

6.85
20
Cl. 295.23

7.4
20 294.7

7.2
10 294.9

7.1 295.0

7.5
10 294.6

9.0
20 294.1

7.00
20
Cl. 294.68

1+25

8.85
20
Drive 293.23

8.9
20 293.2

9.7
10 293.4

8.6 293.5

9.0
10 293.1

7.6
20 292.5

8.85
20
Cl. 293.23

1+00

9.97
20
Cl. 292.11

10.8
20 291.3

10.2
10 291.9

10.1 292.0

10.5
10 291.6

11.0
20 291.1

10.36
20
Cl. 291.72

T.P. 11.15 302.08 0.40 290.93

0+75

0.75
20
Cl. 290.58

1.5
20 289.8

0.9
10 290.4

0.8 290.5

1.1
10 290.2

1.7
20 289.6

1.05
20
Cl. 290.28

0+50

2.82
20
Cl. 289.01

3.1
20 288.2

2.7
15 288.6

2.3 289.0

2.6
10 288.7

3.1
20 288.2

2.52
20
Cl. 288.81

291.33

291.33

2+80^g = W. Ol. line Texas.

302.85	302.16	302.29	302.57	302.42	302.05	301.66	301.32
2.88	3.57	3.44	3.22	3.31	3.68	4.07	4.41
30	30	20	10		10	20	30
Cl.	PAV						PAV

2+70^g = Start A.C. PAV. = New. W.L. Texas.

302.87	302.21	302.21	302.20	301.88	301.99	301.87
2.86	3.52	3.52	3.53	3.85	4.24	3.86
20	20	10	PAV	10	20	20
Cl.	PAV	PAV	PAV	PAV	PAV	Cl.

2+60^g = Old. West line Texas

302.18	301.7	301.7	301.7	301.4	300.7	301.22
3.55	4.0	4.0	4.0	4.3	5.0	4.51
20	20	10	305.73	10	20	20
Cl.						Cl.

T.P. 3.94 305.73 0.29 201.79

2+50

301.53	301.1	301.2	301.2	300.9	300.1	300.58
0.55	1.0	0.9	0.9	1.2	2.0	1.50
10	20	10		10	20	20
Cl.						Cl.

2+25

300.03	299.5	299.6	299.7	299.3	299.5	299.14
2.05	2.8	2.5	2.4	2.8	3.6	2.94
20	20	10		10	20	20
Cl.						Cl.

2+00

298.36	297.7	297.9	298.0	297.7	297.1	297.01
3.72	4.4	4.2	4.1	4.4	5.0	5.09
20	20	10		10	20	20
Cl.						Drive

302.08302.08

LANDIS

⊕

59

-0.03
302.87

S.F.B.P.
Texas + Landis

2.89 302.84

2+80^e Cont

2+80^e Cont.

305.73

20108

1.71
130
ob.

25008

5.41
130
pav.

80208

3.65
80
ob.

30141

4.32
80
pav

29937

6.36
130
pav

30182

3.91
30
ob.

30035

5.40
80
pav

28947

5.86
130
ob.

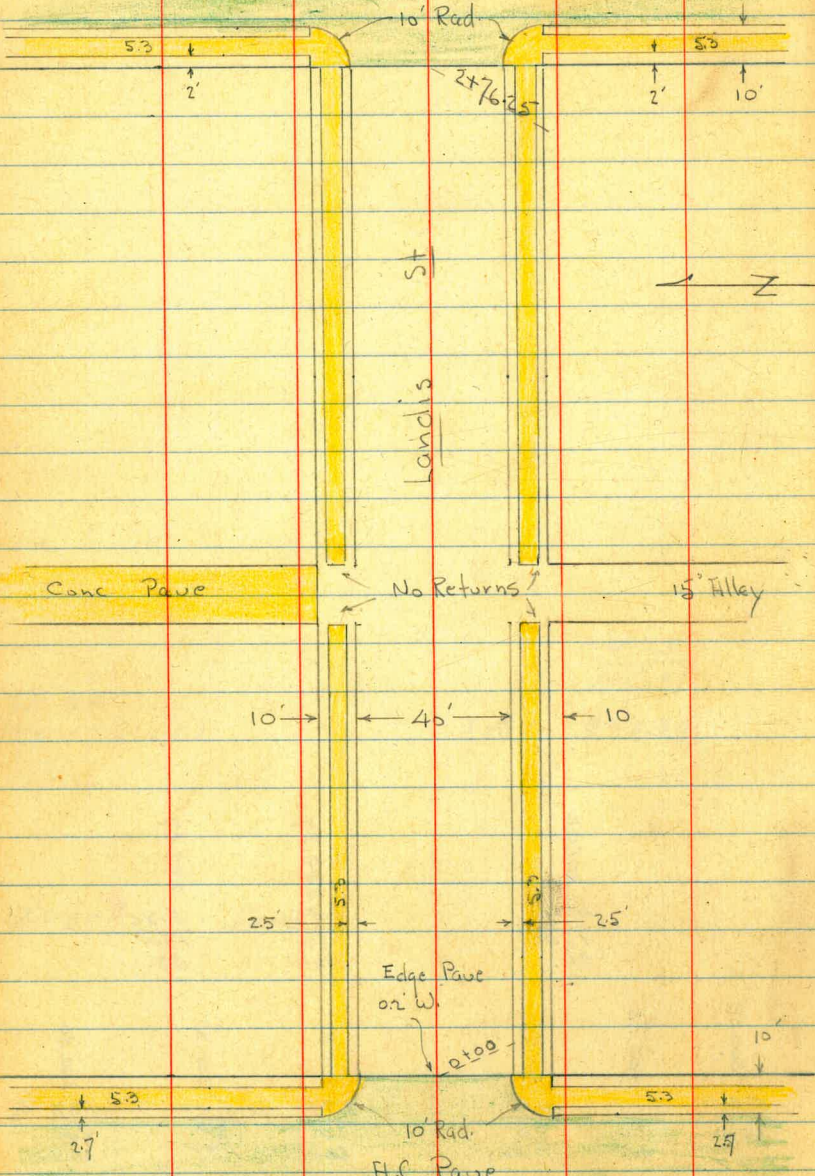
30086

4.87
80
ob.

305.73

Arnold = 65'

st

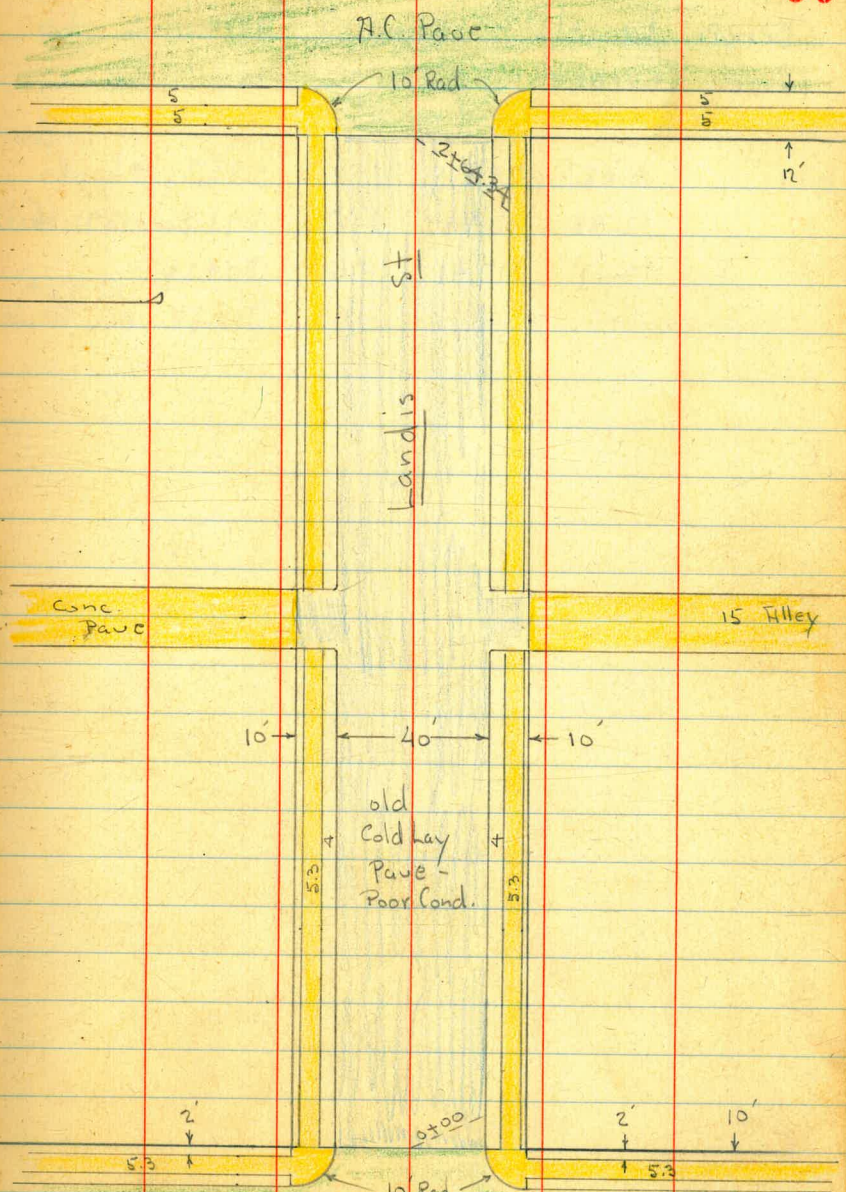


Arizona = 60'

st

Villa Terrace = 65' st

60



Arnold

H.C. Pave

Top broken in gutter

st

Bench Levels - Landis - Arizona to
Villa Terrace.

B.M.	8.88	294.19		285.31	SE Arizona Landis	
	12.88	304.80	2.27	291.92	291.85	SE. BP. Book Arnold.
	13.17	317.41	0.56	304.24		
			1.43	315.98	NW 7'ct. Villa Terrace	

X-Sect - Landis St. - from Arizona
To Villa Terrace - 60' st 10' cbs.

Curbs + Walks in - Dirt - graded

1955

12-23-47

W.O. 313 58

Osborne
Hardin
Worrell

~~Indexed~~

6+20

0+00 = E.L. Arizona St. = edge of T.C. Pavement
is on W. - Rods on edge

Rods on ± 10' Rad. Ret.

10' W. = E. cb.

30' W. = Arizona St.

B.M.

5.70

291.01

285.31

SE. Landis
+ Arizona

291.01

	Lt.	±	Rt.
	5.285.83 10 9.4	5.285.5 20 9.4	5.285.7 10 9.4
	5.285.36 20 9.4	5.284.84 20 9.4	5.285.9 10 9.4
		5.285.80 10 9.4	5.285.77 10 9.4
			5.285.31 10 9.4
			5.284.93 20 9.4
			5.285.39 20 9.4
			5.285.38 10 9.4
			5.284.88 10 9.4
			5.285.36 10 9.4
			5.285.36 10 9.4
			5.284.51 10 9.4
			5.285.36 10 9.4
			5.284.58 10 9.4
			5.285.21 10 9.4
			5.285.13 10 9.4
			5.285.16 10 9.4
			5.285.13 10 9.4

Rods on Φ 10' Rad. Ret

12 F.W. Walk

2+64.34 = W.L. Villa Terrace = edge AC. Pavc

2+50

2+15

2+04 - Φ 14' Conc. Dr. on Lt.

2+00 - Hump in walk on Rt. - Tree

1+90 = Φ 10' Conc. Dr. on Lt.

T.P. 10.26 318.92 0.63 308.66

1+80

N.W.

	LT	Φ	Rt.	
	315.45	315.95	314.95	314.62
	3.47	2.97	2.97	4.30 S.W.
	gut.	Top	Top	gut.
	315.98	315.18	314.89	314.97
	2.94	3.74	4.03	4.51
	20	20	10	20
	Top	gut.	Top	gut.
	314.71	314.1	313.7	313.2
	4.21	4.8	5.2	5.7
	20	20	10	20
	Top	gut.	Top	gut.
	311.53	310.9	310.8	310.53
	7.39	8.0	7.7	8.39
	20	20	10	20
	Top	gut.	Top	Top
	310.65	309.89	310.1	310.53
	8.27	9.33	8.8	8.39
	24	19.9	20	20
	Walk	Dr.	gut.	Top
	308.74	308.74	310.8	310.53
	9.48	10.18	8.1	8.39
	24	20	10	20
	Walk	Dr.	Top	Top
	308.39	307.8	318.92	307.54
	0.90	1.5	1.1	1.75
	20	20	10	20
	Top	gut.	Top	Top
	309.29	307.2	307.7	307.1
	1.6	1.1	1.6	2.2
	10	10	10	20
	Top	gut.	Top	Top

0+94 dirt

0+76 edge Pav

0+99.94 E Blvd

0+24 edge Pav.

0+00

1.0 error on plus Rod.

T.P. 4.74 8.56 6.03 3.84

Fd. spike
P.P. SW Cor
W. Pt Loma
Adrian St

3.50 6.37 ✓

T.P. 4.74 9.87 1.66 5.13

SE spike
P.P.
W. Pt Loma Blvd
Famosa

3.71 6.79 ✓ 3.08

L7

8.7
4.9

R7

69

8.51
5.05

3.61
3.95 ← Please check
to profile

2.79
4.77

0.68
1.634/6.0

-0.11
~~0.23~~ 1.95

8.33
INV. 5.61

TOP hdw.

P 71 for correction 1.96

8.56 ✓

Control P 71

-0.76
9.05
Inv. in let 6.33
TOP hdw.

T.P. 4.44 8.29 6.30 3.85 ✓ 0.01 error

Spike SW PP 3.79 6.36 6.37

T.P. 5.03 10.15 1.69 5.12

B.M. 3.73 6.81 3.08

2+20 CTR. Slough

1+90 Sly edge Slough

1+75

1+53.5

1+32.5

1+00.55 A 3' 30" ft outlet 24" pipe

8.56 ✓

Notes Reduced
3-8-98

19	29	45	49	29	09
9.5	10.5	12.1	11.6	10.5	8.4
25	18	8		70	25

10	34	44	36	0	07
8.6	11.0	12.0	11.2	7.6	7.4
25	12	8		15	25

10	10	29	38	37	30	9.1
6.6	6.6	4.7	11.4	11.3	2.6	4.5
30	21	19	7		11	25

11	16	18.8	13.7	37	36	9.5
6.4	6.0	11.4	11.3	11.3	4.0	4.1
30	18	7	4		15	30

19	16	49	31	9.1
5.7	6.0	9.05	4.5	4.5
20	10		6	12

148 BK 1834/60

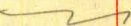
56' Cor. of Wood Bldg.

Correction on H.L. 9-68

3-9-48

1400.55 = out Let 24" pipe

0400 = in Let 24" pipe

8.29


1.51
 9.80
 INV.

0.76
 9.05
 INV.
 INLET

1.96
 6.33
 TOP HDWL.

Levels on spur track
From 2nd to 4th
between J & K Streets.

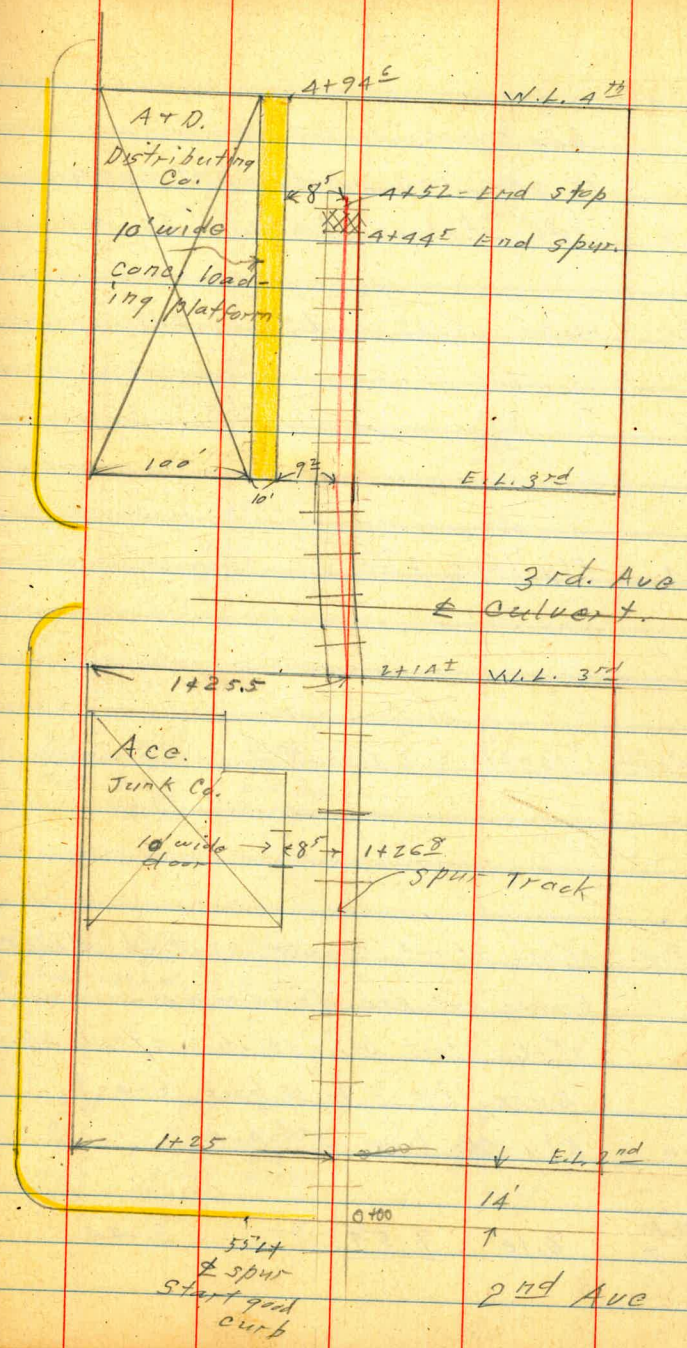
6-29-48
21001

Sommermeyer
L. Melton
W. Duncan
F. Finney

For culvert location
see E.B. 1486 Pages 77 to 79. Inc.
Notes 11/9/43 and 12/8/47 are still
unchanged.

INDEXED
JUN 29 1948

J Street



box cars
to get rail slots between
0+96 odd station taken so as

T.P. 1100 6.13 7.41 2.13

0+25

0+1A = Ely line 2nd

0+00 Cont 125 Lt. = 2 line J

0+00 Cont. 45 Lt. = start regular poured drive
broken out for drive ways.

75 Lt. = start ob. 14 Lt. = start ob.

Base line = E spur track

0+00 = Ely Ob. line 2nd Ave.

SW. B.P.
2.24 + J. 6.10 9.54 — 3.44

17
5.01
24
N. Rail

13
5.00
24
S. Rail

6.13

12
7.82
24
N. Rail

11
7.63
24
S. Rail

11
7.67
24
N. Rail

12
7.52
24
S. Rail

6.58 7.19 6.81 7.44
125 125 65 65
ob. curb start ob. End. Drive
top. ob. gutter

7.47 6.84 7.46
55 45 45
E drive top. ob. gutter

2.38 1.92 2.14
7.11 7.16 7.62 7.51 7.40
14 75 75 24 24
top. curb start ob. + par. N. Rail
ob. par. S. Rail

9.54

platform

8⁵ Lt. = start 10' wide conc. loading2+94 Aprax E. Line 3rd

0.50	4.7	1.00	0.88
85	85	2.00	5.02
platform.	Gro.	N. Rail	S. Rail
			2.00

2+54 Aprax & 3rd

0.91	1.00
5.08	5.05
2.00	2.00
N. Rail	S. Rail

2+14 = Aprax. W. line 3rd

0.18	0.86
0	0
5.27	5.19
2.00	2.00
N. Rail	S. Rail

2+00

0.91	1.01
0	0
5.14	5.04
2.00	2.00
N. Rail	S. Rail

1+75

0.12	1.00
1	1
4.93	4.92
2.00	2.00
N. Rail	S. Rail

1+50

0.15	1.16
1	1
4.90	4.89
2.00	2.00
N. Rail	S. Rail

T.P. 4.91 6.05 4.99 1.14

6.05

1+26⁸ 8⁵ Lt. = 10' wide door.

G.13

0.95	4.18
85	85
Door. Sill	Gord

6.13

S.W.B.P. 4th + J.

3.83

4.93

4.91

W. Line 4th

Platform shot on S.E. cor

of bumpers.

4+44^E = End usable spur. = west side

T.P.

5.79

8.76

4.09

2.77

4+00

3+49

T.P.

5.20

7.06

4.19

1.86

6.05

B.L.1

79

75

5.64

3.12

8^E wt. of B.L. produced.

3.14
8^E
Platform

6.18
8^E
Ord

1.99
6.77
2^E
N.Rail

1.98
6.78
2^E
S.Rail

8.76

1.47
8^E
Platform

5.5
8^E
Ord.

0.63
5.12
2^E
N.Rail

0.64
5.11
2^E
S.Rail

1.50
8
Platform

5.5
8
Ord.

0.31
5.70
2^E
N.Rail

0.35
5.70
2^E
S.Rail

76

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

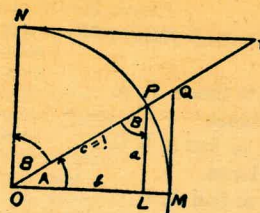


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2 ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2} (A+B)}{\tan \frac{1}{2} (A-B)} \end{aligned}$$

122.6

25

1425.8

157

501

163

394

394

1.47

10
7
17

314 90
17
297.90
158.95

300
790
310