

1792

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

MICROFILM
Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
for Single Track Embankment.

DEC 29 1964

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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1792

Handwritten notes and calculations in pencil, including numbers like 51, 25.5, 15, 25.5, 22.5, and some illegible scribbles.

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Sewer - Hornet Tract 1 -
X-Sec. 42nd + Canterbury Dr. 25-32
" Locust Wharfed to Xenophon - 46

20

Proposed Sewer Line
Hornet Tract.

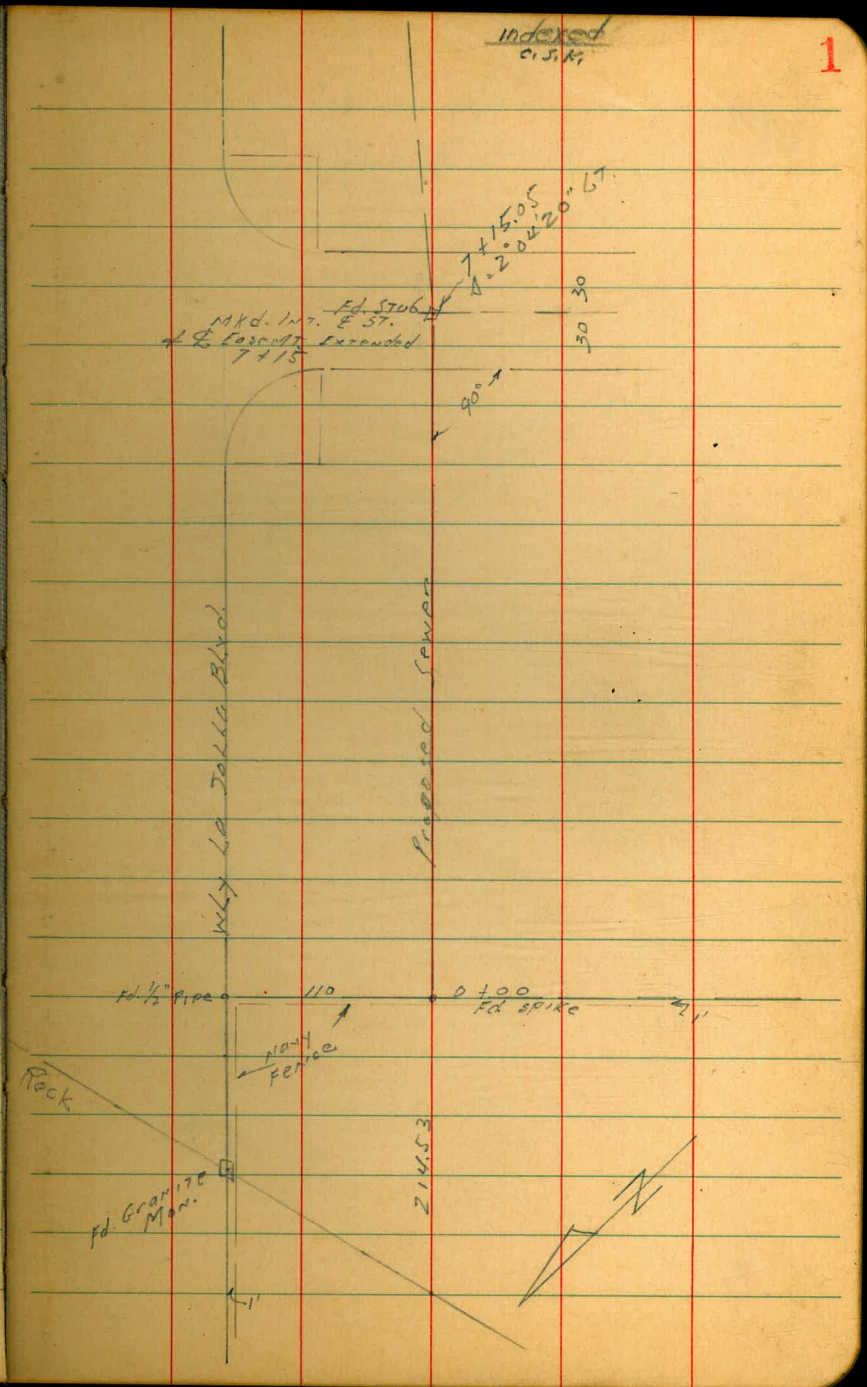
Mason
Begg
Gardner
Roberts

W.O. 23046

7-17-47

Ref. 1650 P. 9

To Main
Sewer



Fd. 2x2 stub
MKd. & sewerline

1940.6.17
 $\Delta = 32^{\circ} 48' \text{ LT.}$

Fd. 2x2 108 wily MKd.
& easmt.
1940.9.54

Fd. 2x2 MKd.
300.49 & sewerline

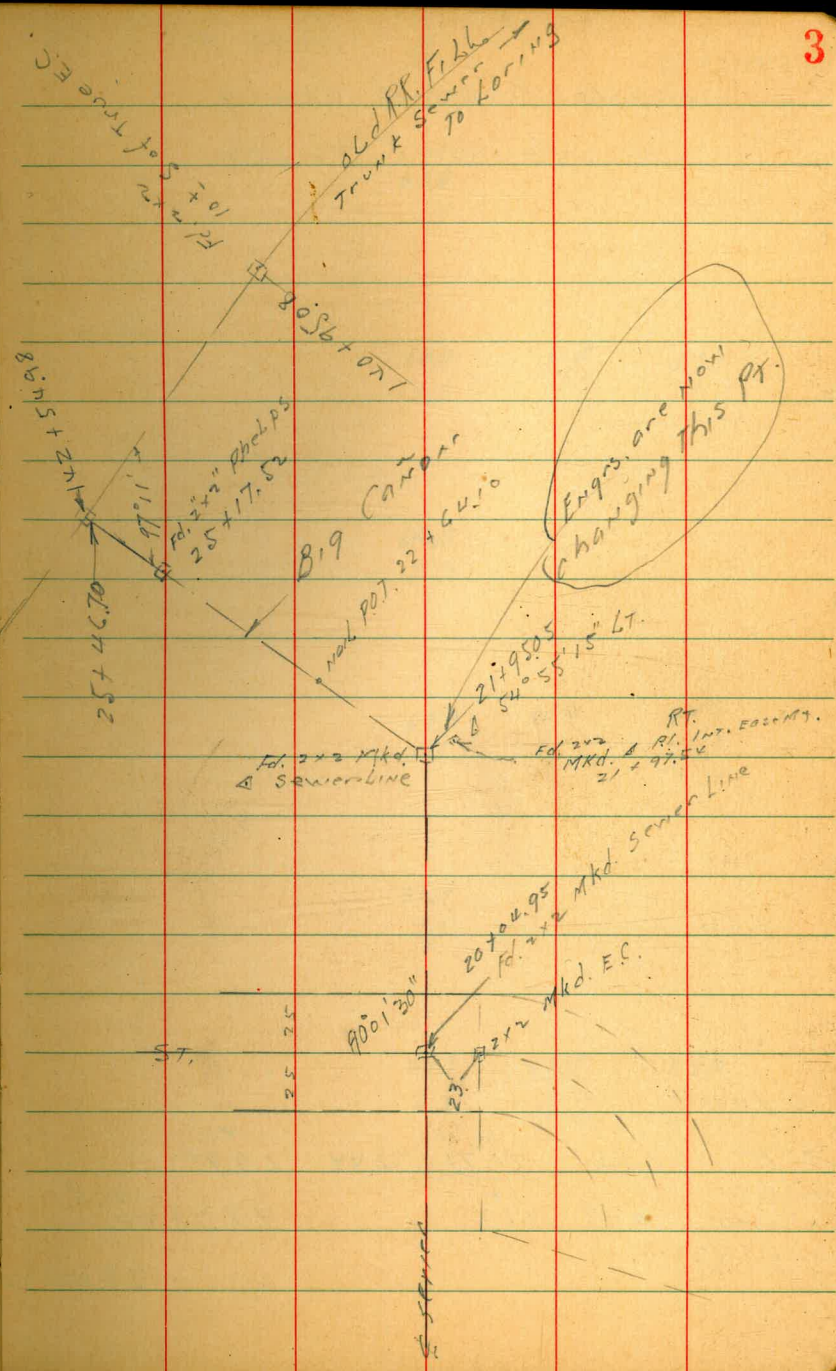
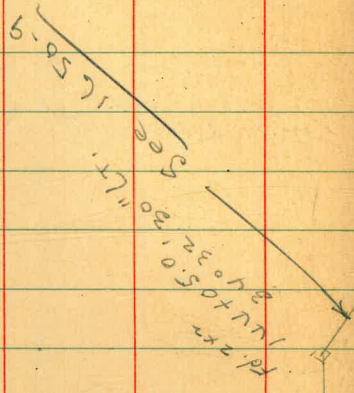
14 + 60.69
 $\Delta = 12^{\circ} 15' 45'' \text{ RT.}$

Fd. 100.53 & easmt.
MKd. & sewerline
100.53

Fd. 2x2 stub
MKd. & pt. of easmt.
11 + Co. 02
Fd. 100.53 stub
MKd. NOT MKd

11 + Co. 12
 $\Delta = 3^{\circ} 14' \text{ LT.}$

Service, Hannel Tract



Sketch P.1
Levels Proposed Sewer
in Hornumel Tract

+19

2

+50

1

+50

0/00

T.P. 1.80 71.71 8.44 69.91

SW.B.P. Colima 0.37 78.35 77.98 = CITY

La Jolla Blvd.

78.02 = E.B. 1650-43

2

Rt = WEST 4

63.8

7.9

64.0

7.7

61.5

$\frac{10.2}{100}$

59.1

$\frac{12.6}{200}$

64.5

7.7

65.9

5.8

63.2

$\frac{8.5}{100}$

59.7

$\frac{12.0}{200}$

66.3

5.4

66.9

4.8

2

71.71

63.5

$\frac{8.2}{100}$

58.2

$\frac{13.5}{200}$

11

+ P 3.93 66.89 8.75 62.96

+ 50

3

+ 63

+ 57

+ 27

+ 23

71.71

62.3
4.6

59.0
7.9
100

65.3
11.6
182

5

S. PIM CAÑON

66.89

62.1
9.6

62.3
9.4

59.5
12.7
100

57.5
14.7
200

62.9
8.8

62.1
9.6

64.4
7.3

62.8
8.9

71.71

T.P. 5706
7+15.05 6.00 68.51 4.38 (2.51)

7+15.05 A 2°00'20" 17

7

+50

6

+50

5

4+50

66.89

6

R

6

62.51

4.38

62.5

4.4

58.2

8.7

100

53.9

13.0

200

62.1

4.8

61.9

5.0

57.4

9.5

100

54.0

12.9

200

61.9

5.0

61.9

5.0

58.1

8.8

100

53.2

13.7

200

62.0

4.9

66.89

E

R

57.9
10.6

57.9
10.6

63.5
5.0

63.5	59.5	56.2
5.0	9.0	12.3
	<u>100</u>	

62.4
6.1

62.0	58.4	55.0
6.5	10.1	13.5
	<u>100</u>	<u>200</u>

62.4
(.)
68.51

728

725 wash

715

7

750

8

7150

68.51

T.P.
11+60.12
57.6 8.40 75.12 17.9 66.72

11+60.12 A 3'14'17

+50

11

+50

10

+50

9+32

68.51

8

RT

8

66.72

17.9

66.5

2.00

66.0

2.5

63.3

5.7

1.00

61.8

6.7

1.40

57.1

11.4

2.00

65.1

3.4

64.7

3.8

61.7

1.8

1.00

59.4

9.1

2.00

64.2

4.3

64.2

4.3

68.51

BM. H66
14+60.69

4.36 70.76 ✓ Hub

14+60.69 A 12°15'45"R

+50

14

+50

13

+50

12

75.12

8

17

9

70.76
4.36

70.5
4.6

70.9 66.7 64.0
4.7 $\frac{8.1}{100}$ $\frac{11.1}{200}$

70.8
4.3

69.6 67.1 63.1
5.5 $\frac{9.0}{100}$ $\frac{12.0}{200}$

68.3
6.8

67.4 64.8 61.8
7.7 $\frac{10.3}{100}$ $\frac{13.3}{200}$

75.12

18

67.7	72.4	87.576
5.7	10.6	15.4
	70.0	20.0

+ 50

68.0
5.0

17

68.7	65.1	58.5
4.3	7.9	14.5
	70.0	20.0

+ 50

69.0
4.0

16

69.6	66.3	57.2
3.4	5.7	15.8
	70.0	20.0

I.P.

222

72.96

438

70.7472.96

+ 50

70.1
5.0

70.5
4.6

67.0
8.1
100

64.0
11.1
200

75.1275.12

$$\begin{array}{r} 69.3 \\ 6.3 \end{array}$$

$$\begin{array}{r} 28.7 \\ 6.9 \end{array}$$

$$\begin{array}{r} 68.1 \\ 7.5 \end{array}$$

$$\begin{array}{r} 62.9 \\ 10.1 \\ \hline 700 \end{array}$$

$$\begin{array}{r} 59.9 \\ 13.1 \\ \hline 200 \end{array}$$

$$\begin{array}{r} 75.60 \\ \hline \end{array}$$

$$\begin{array}{r} 67.4 \\ 5.6 \end{array}$$

$$\begin{array}{r} 66.9 \\ 6.1 \end{array}$$

$$\begin{array}{r} 66.9 \\ 6.1 \end{array}$$

$$\begin{array}{r} 64.4 \\ 8.6 \\ \hline 700 \end{array}$$

$$\begin{array}{r} 59.6 \\ 13.4 \\ \hline 200 \end{array}$$

$$\begin{array}{r} 67.3 \\ 5.7 \end{array}$$

$$\begin{array}{r} 72.96 \\ \hline \end{array}$$

+ 90

+ 50

20

T.P. 727 $\overset{\vee}{75.60}$ 4.63 $\overset{\vee}{68.33}$

+ 50

19 + 06.67 Δ 34° 48' LT

19

+ 18 + 50

$$\begin{array}{r} 72.96 \\ \hline \end{array}$$

21 + 95.05 A 54° 55' 15" LT.

174

150

138

128

115

21

75.60

12

68.6

70

68.8

73

56.6

19.0

50.5

25.1

56.6

19.0

56.8

18.8

66.6

90

75.60

L 41 in wash

+35

+33

23 + 10

TP 2.38 67.40 10.58 65.02

+65

+50

22

75.60

~~40.2~~
27.2

41.0
26.4

42.9
24.5

42.9
24.5

67.40

72.3
33

71.9
3.7

69.7
5.9
75.60

~~4~~46.7
20.745.3
22.144.1
23.343.1
24.341.9
25.543.3
24.142.8
24.64
67.40

+19

+17

24

+87

+81

+78

23+65

v
67.40

check to spike T.P. on RP
1.60 R₂ of 146+00 11.3 86.45 86.53
1650-42

25 + 46.7 Proposed trunk sewer

+110

T.P. 1329 87.57 108 74.28

25 + 17.5 = P.O.T. 2x2 "Phelps"

T.P. 9.53 75.36 157 65.83

25

+75

24 + 50

67.40

15

82.1

5.5

82.4

5.2

87.57

67.8

7.6

75.36

58.4

9.0

51.4

16.0

49.6

17.8

67.40

Proposed change #1 on
 Sewer line in
 Hurdle Tract,
 to avoid Cañon.

Fd. 2x2
 Mk'd. P.I.

50' ST. 296-80

16x22x3
 5100' LT.

16x22x3
 5100' LT.

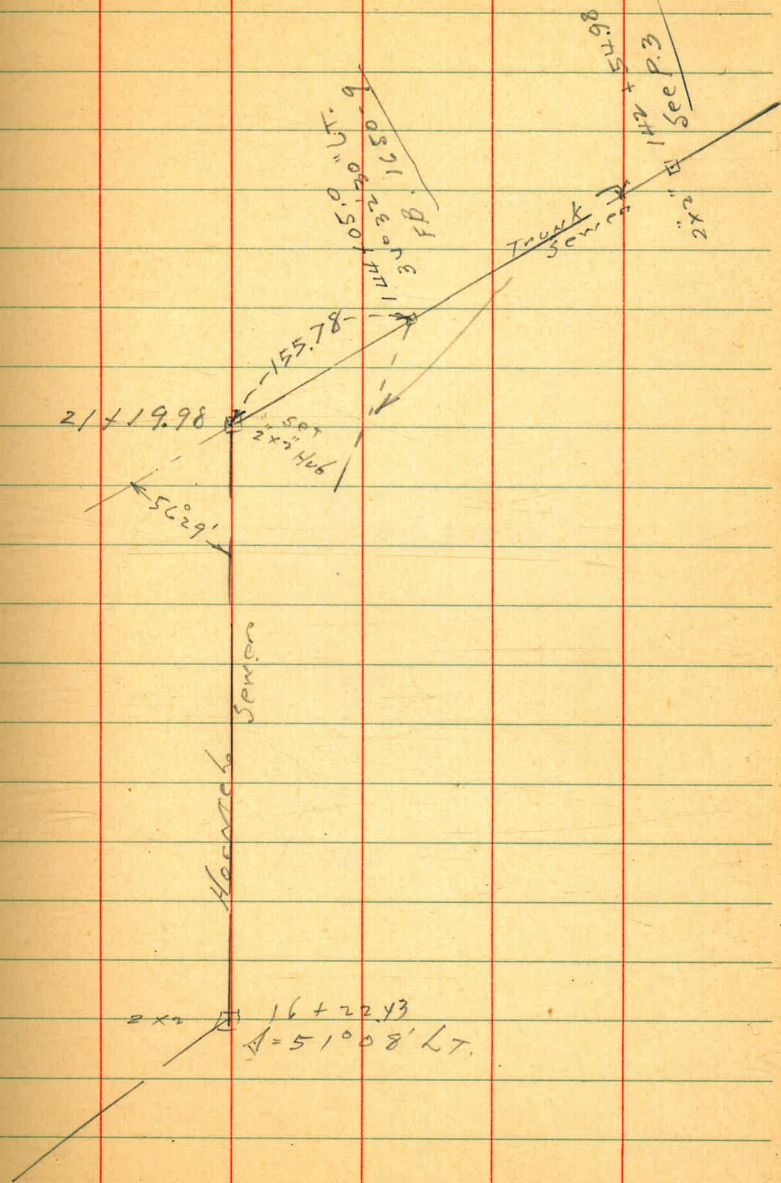
13°07' 15934

Fd. 2x2
 P.I.

14160.69 P.I.

Proposed
 Sewer

11160.17
 3014' LT.



Some levels on change #1

17

+50

16+22.43 Δ 51°08'47"

16

+50

15+00

B.M. 2x2 Hub

14+60.69

8.13

78.89

70.76

P. 9

§

18

72.9

60

71.7

7.7

71.0

7.9

70.8

8.1

70.6

8.3

70.4

8.5

78.89

+50

20

+50

T.P. 10.85 88.22 1.52 77.37

19

+50

18

17+50

78.89

~~82.4~~
5.8

81.5
6.7

80.2
8.0

88.22

78.8
0.1

77.2
1.7

75.5
3.4

73.9
5.0

78.89

19

Check to SPIKE
 F.P. P.15

176 86.46 86.53

21719.98

85.2
 3.0

21700

84.7
 3.5

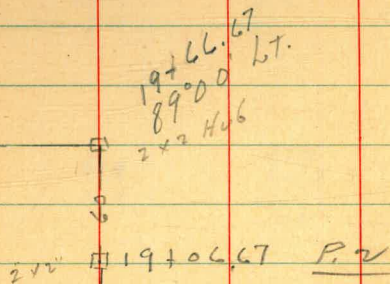
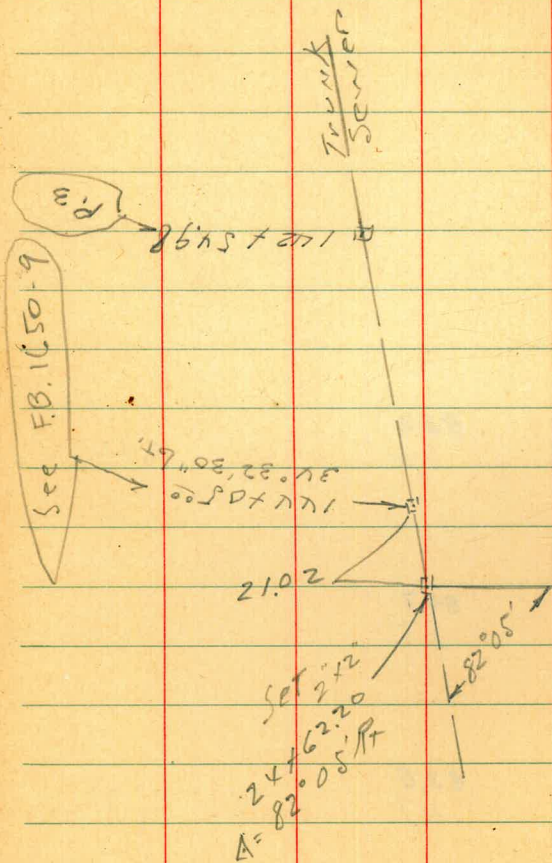
21761

83.5
 4.7

88.22

88.22

change # 2 to avoid canyon
in Hooded Tract



Sewer levels on change #2

22

+50

21

+50

20

19+6667 A 89° LT.

B.M. 282
146069
P. 9

74.0

78.16

70.76

75.1
3.1

74.4
3.8
20

72.7
5.5

72.0
6.2
20

70.8
7.4

70.8
7.4
20

69.2
9.0

69.0
9.2
20

67.4
16.8

67.5
10.7
20

66.6
11.6

66.4
11.8
20

78.16

22

+35

81.8
6.9

80.1

8.6

70

F.M.
CANYON

73.2

15.5

20

WASH

+20

82.0
6.7

78.9

9.8

20

24

81.3
7.4

80.3

8.4

20

+50

80.3
8.4

79.6

9.1

20

23

78.2
10.5

78.3

10.4

20

T.P.

11.09

88.71

0.54

77.62

88.71

22/50

76.6
1.6

76.4

1.8

20

78.16

78.16

check to T.P.
SPIKE P.P.
P. 15

226 8645 8653

24 + 220

+ 50

24 + 45

8871

4

R.

24

851
3,0

845
4,2

824
6,3

8871

848
3,9
20

815
7,2
20

P.M
Canon

Cross Section A2nd at Canterbury Drive Indexed-8-4-47 M²

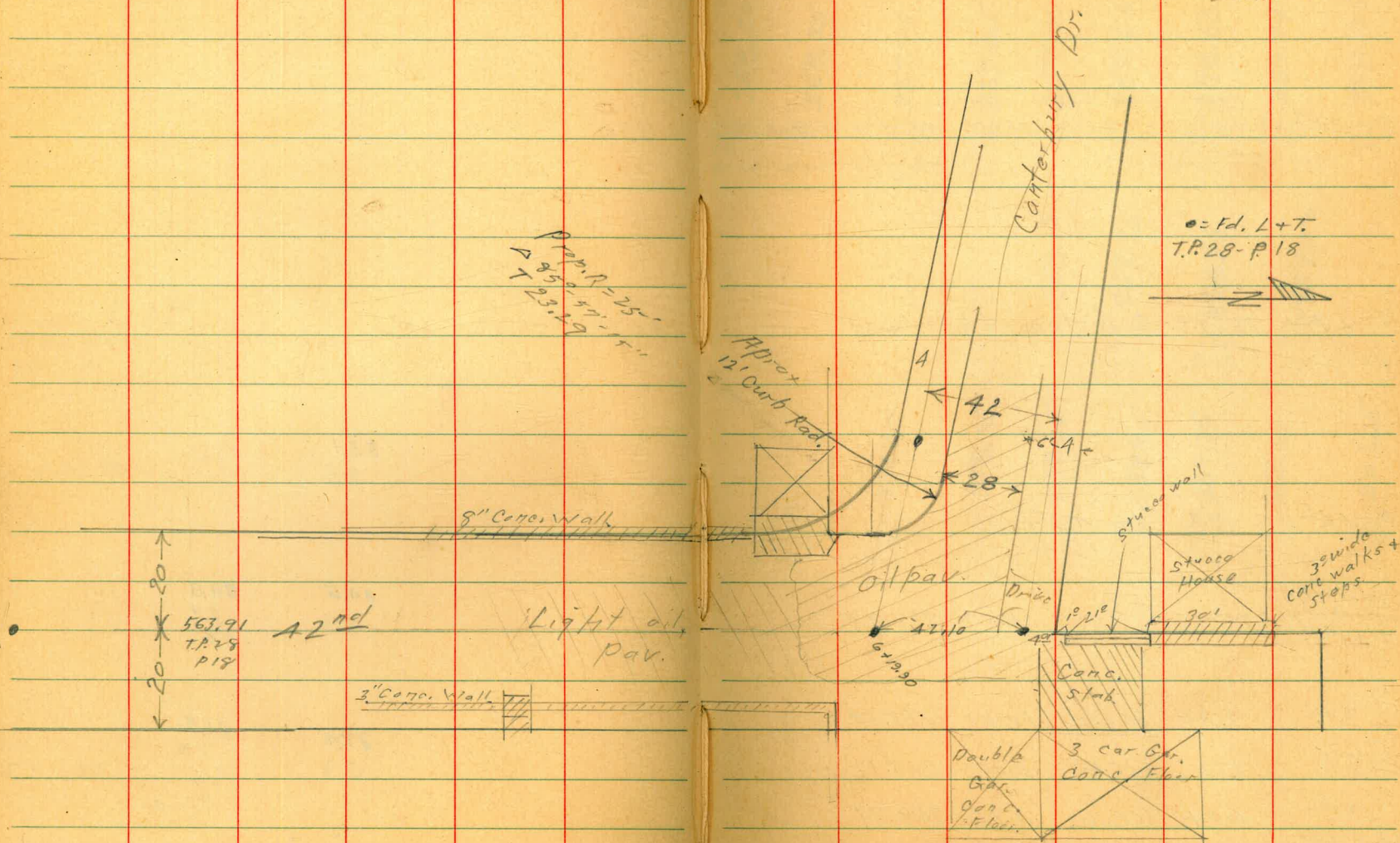
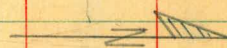
8-1-47

X.O. # 25001

Sammermeyer
W Moore
Sherman
Lamora

PROP. R=25'
A 85.57'-1'-11"
T 23.29

o = Id. L+T.
T.P. 28-P. 18



0-20^A 19^L = End conc. walk
 15^E LT. = Start conc. Apron + Doub. Car.

0-29^G 15^E RT. = 3' steps thru. wall

0-56^E 90° to 42nd

Set S.W. BR
 Canterbury Drive
 + Apron

SS

5.57 357.38

J.P. 7.45 362.95 10.00 355.50

J.P. 2.37 365.50 2.00 363.11

TP 6.24 365.11 5.91 358.87

S.E. 6' LT.

Adams St.
 Edgewood Rd.

6.28 364.78 — 358.50

358.50	358.25	357.79	357.65	357.95	357.65	358.55	359.74	360.25
4.45	4.7	5.16	5.3	5.0	5.3	4.4	3.21	2.7
19.1	19.1	15.8	10	oil	oil	15.7	15.8	20
Apron	dirt	Edge Apron + 8'rd.	oil	oil	oil	8'rd	Top wall	

362.95

0-01^s End point of Apron. (90° to 42nd)

357.85

0-02^s 18² Lt. start 6" Curb.

5.10
22.6
Edge Apron
+ ground

0-03^s Cont.

0-03^s

0-06^s 16² Lt. End N. + S. wall also ♀ E + W. wall.

362.95

4" curb.

5.26
18.3
Top Cl.

357.69

5.67
18.3
Apron

357.26

5.25
18.3
Apron - Top End
Ground + Curb

357.70

5.61
16.7
Edge Apron

357.34

3.88
22.6
at floor

359.07

4.60
18
Ork in
Apron

358.35

357.38

5.57
15.8
Edge Apron

357.25

5.7
15.9
Ord

357.35

357.55

357.25

5.6
10
oil

357.55

357.35

358.35

359.62

359.85

5.4
5.6
10
oil

362.95

4.6
16
Ord

3.33
16.7
Top wall

3.10
20
End
E + W wall

LT

RT

RT

27

0+18 = 1/4

0+11 Cont

0+11 Wly. Cb Canterbury Dr.

0+01 18² Lt. = Curb. Ret. B.C 12' Rad.

Sections taken parallel to Canterbury Dr.

0+00 = Sil. Canterbury drive (start oil Pav.)

362.95

						356.48	356.91	357.01	357.05	356.65	358.25
						6.47	6.04	5.74	5.90	6.30	4.7
						100	20	10	10	10	20
						26.					
						7.41	355.99	357.01	357.05	356.65	358.25
						100					
						26.					
						6.00	356.95	357.01	357.05	356.65	358.25
						6.65					
						60					
						10					
						Pav					
						357.38	356.70	356.93	357.06	357.18	356.81
						5.57	6.25	6.02	5.89	5.77	6.14
						30	30	20	10	10	10
						Top. Pav	Pav				oil
						Curb. EC					20
						357.18	357.18	357.18	357.18	357.18	357.18
						5.30	5.30	5.91	5.91	5.91	5.91
						18.3	18.3	18.3	18.3	18.3	18.3
						20	20	20	20	20	20
						Pav.					
						357.18	357.13	357.25	357.45	357.15	359.25
						5.27	5.87	5.7	5.5	5.8	3.7
						18.3	18.3	9	0.1	11	20
						Top. Pav	oil		oil	oil	
						362.95	362.95	362.95	362.95	362.95	362.95

214. = End Drive opening Drive
100 cc

0+39 = Nly Cb. line Canterbury Dr.
start E.W. Curb to west only

0+32 1/4

0+27 20³ Rt. = Start double Gar. Conc. floor

0+25 = Rough Corrid. walk (3' wide - E.W. walk)

362.95

355.16 7.79 100 Pav 355.19 6.76 60 cc 355.51 7.39 60 Pav 356.45 6.50 21 Top cl. 356.43 6.52 8 357.25 5.7 20

355.83 7.12 20 Pav. 356.07 6.88 10 Drive in drive 355.88 7.07 10 Pav. 355.89 7.06 Pav 356.49 6.46 10 Top cl.

356.46 6.49 20 356.45 6.50 10 356.41 6.54 356.35 6.6 10 oil 357.15 5.8 20 3rd

357.34

5.61
20.7 Gar. floor

355.92 7.03 100 356.30 6.65 60 356.72 6.23 20 356.79 6.10 10 356.80 6.15 356.44 6.51 10.7 oil 357.50 5.45 16 End walk 358.11 4.84 20 on walk

362.95

0+24² 20² Rt. = End Car.

357.16
5.79
on walk
357.16
5.79
on walk
357.16
6.0
Bar.
356.95
7.0
8
356.75
6.2
20
356.85
6.10
20.3
Bar Floor

start, Conc. landings + steps
0+22 1' Rt. = End N+S, Conc. Wall

357.16
5.79
on walk
357.16
5.79
on walk

0+20 1' Lt. = End. N+S, Hedge

356.33

1' Rt. = Base Conc. wall, + W. edge
13⁵ = End Conc. slab. Conc. Slab.

6.62
on slab
356.62
6.33
10
356.87
6.08
20
Bar Floor

0+01 1' Rt. = start 6" Conc. N+S. Wall
Sections at 90° to 42nd

356.75

356.68

357.79

356.92

0+100

0+50¹ 1' Lt. = E 6' ^{wide} N+S. Hedge
Nly. line Canterbury Drive

6.2
Bar.

6.27
slab.

6.16
10

6.03
20 - Bar Floor
also slab.

0+46⁵ 1⁰ Rt. = End 4' E+W. walk to west
Start Conc. slab. 90° to 42nd

356.71
6.24
10

356.71
6.24
10

356.79
6.16
10

356.87
6.08
16
Edge
oil

356.92
6.03
20.3
End slab
+
Edge Bar Floor

362.95

362.95

0+54 1⁶ Rt. End stairs.

0+50 1⁶ = wall.
1⁰ Rt. End landing start stairs

0+42 1⁵ start. N+S. 6" Conc wall
1⁰ Rt End stairs start landing

0+32⁵ End landing start stairs 1⁵ Rt.

T.P. 1.95 357.55 7.35 355.60

0+27 21' Rt. = ~~2~~ 2⁵ 'Conc. Walk

+25 21' Rt. start. 6" Conc. wall.
361.95

Lt.		Rt.	
			31
		349.65	
	7.90 15 on step	349.65	
		351.38	
	6.17 15 at house	351.38	
		351.38	
	6.17 1 top steps	351.38	
		351.84	
	5.71 15 wall	351.84	
		352.15	
	5.4 10	352.15	
		352.25	
	5.3 20	352.25	
		351.88	
	5.67 12 at house	351.88	
		351.88	
	5.67 1 Landing	351.88	
		352.39	
	5.16 16 top wall	352.39	
		353.75	
	3.8 10	353.75	
		353.65	
	3.9 20	353.65	
		356.95	
	0.60 15 at house	356.95	
		356.95	
	0.60 15 top stairs	356.95	
		355.05	
	2.5 10 Grd	355.05	
		355.25	
	2.3 10	355.25	
		355.25	
	2.3 20	355.25	
		357.55	
		356.05	
		356.05	
	6.9 21 Walk + wall	356.05	
		362.95	
		362.95	

X-Sec. 42nd Canterbury Dr.

32

- 0.01

358.50

Orig. B.M. Page 25 5.57 358.49

T.P. 4.23 364.06 4.87 359.83

T.P. 5.72 364.72 8.49 359.00

T.P. 6.37 367.17 0.51 361.10

T.P. 4.89 361.61 0.83 356.72

0+65

0+58

0+57 21' Rt. = End 6" Conc. wall.

362.95
357.55

11.4
20 346.15

8.0
5 349.55

7.9
5 349.65

8.1
3 349.75

7.9
3 349.65

7.2
10 350.35

6.8
10 350.75

6.8
20 350.75

6.3
20 351.25

6.6
30 350.95

1.5
21 356.05

9.9
30 347.65

1.5
30 356.05

362.95
357.55

X-Sect. 42nd - Alder to Canterbury Dr.

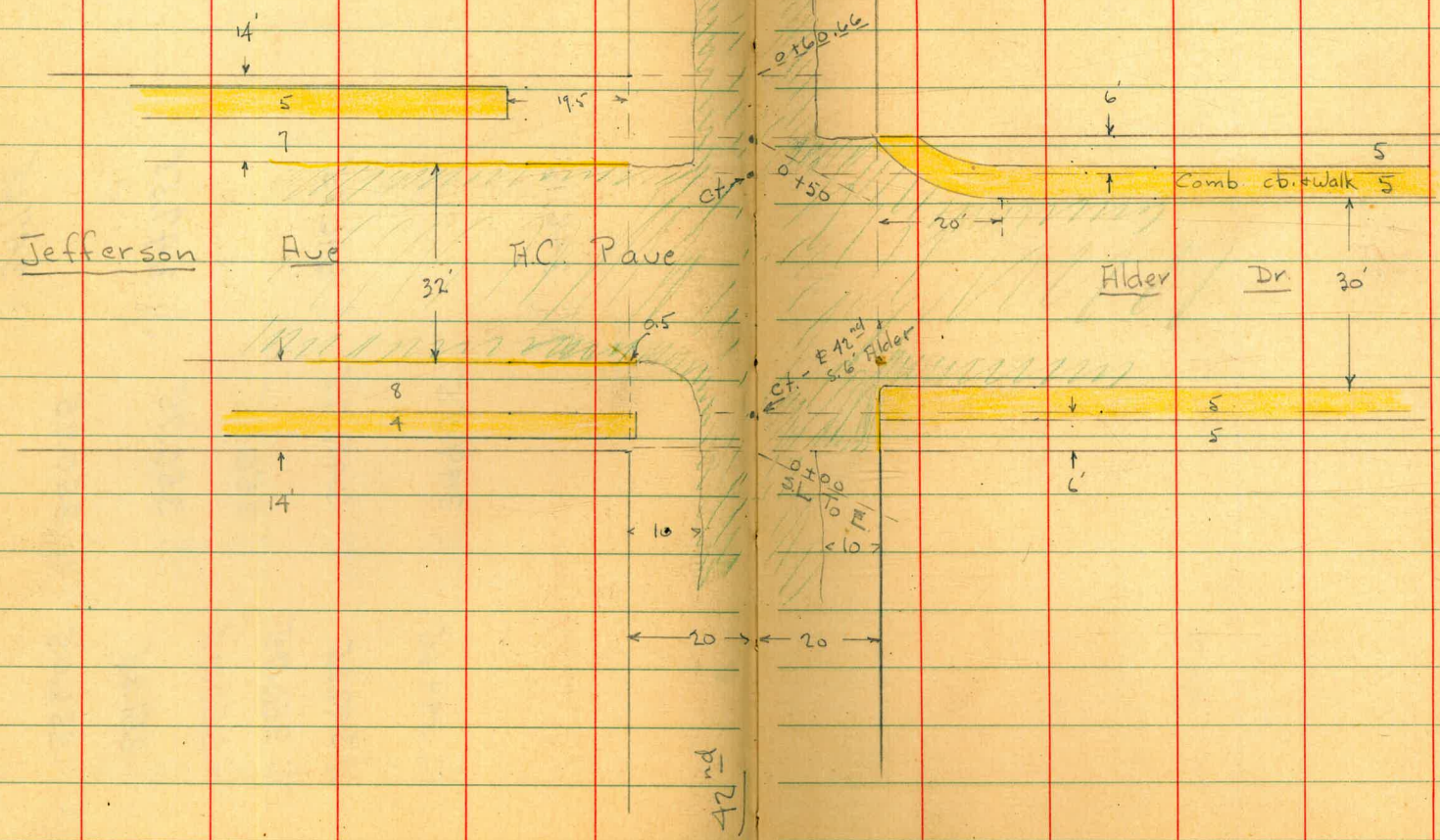
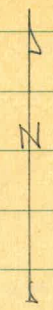
9-18+19-47

1803

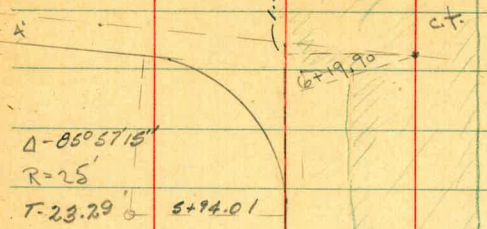
W.O. 25001

See Page 25

Osborne
Hardin
Smith
Worrell



Canterbury Dr.



$\Delta-85^{\circ}57'15''$
 $R=25'$
 $T=23.29'$

5+94.01

< 10 x 10 >

H.C.
Pave

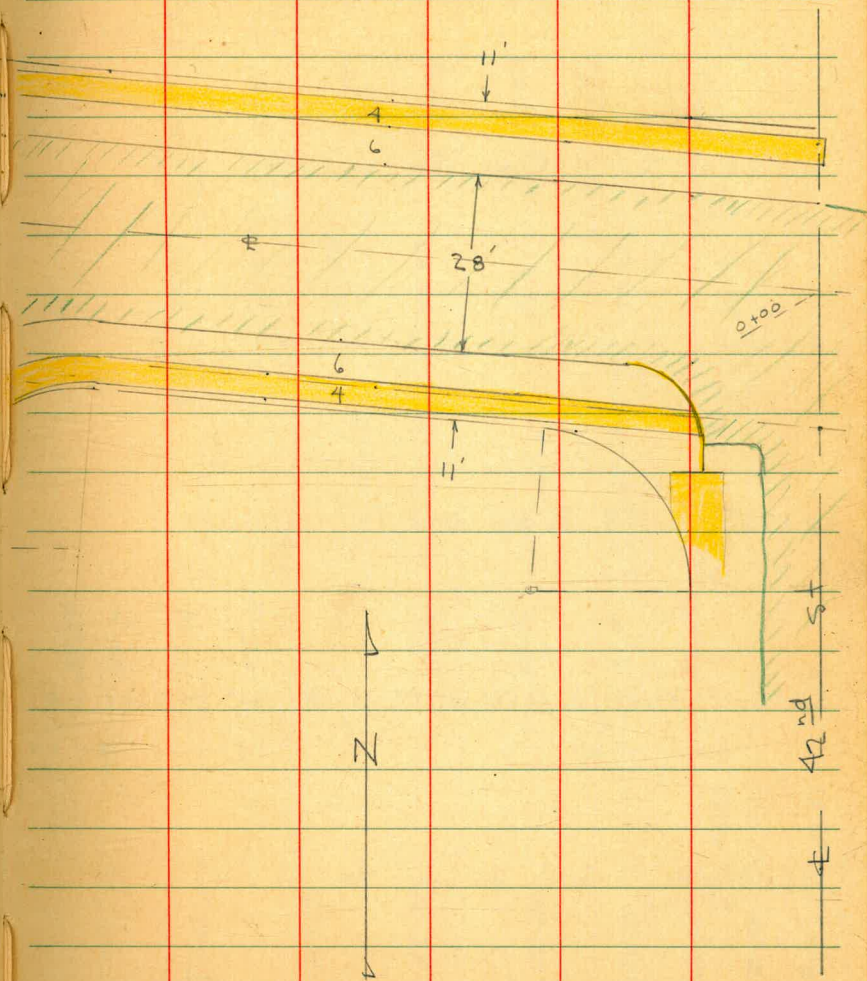
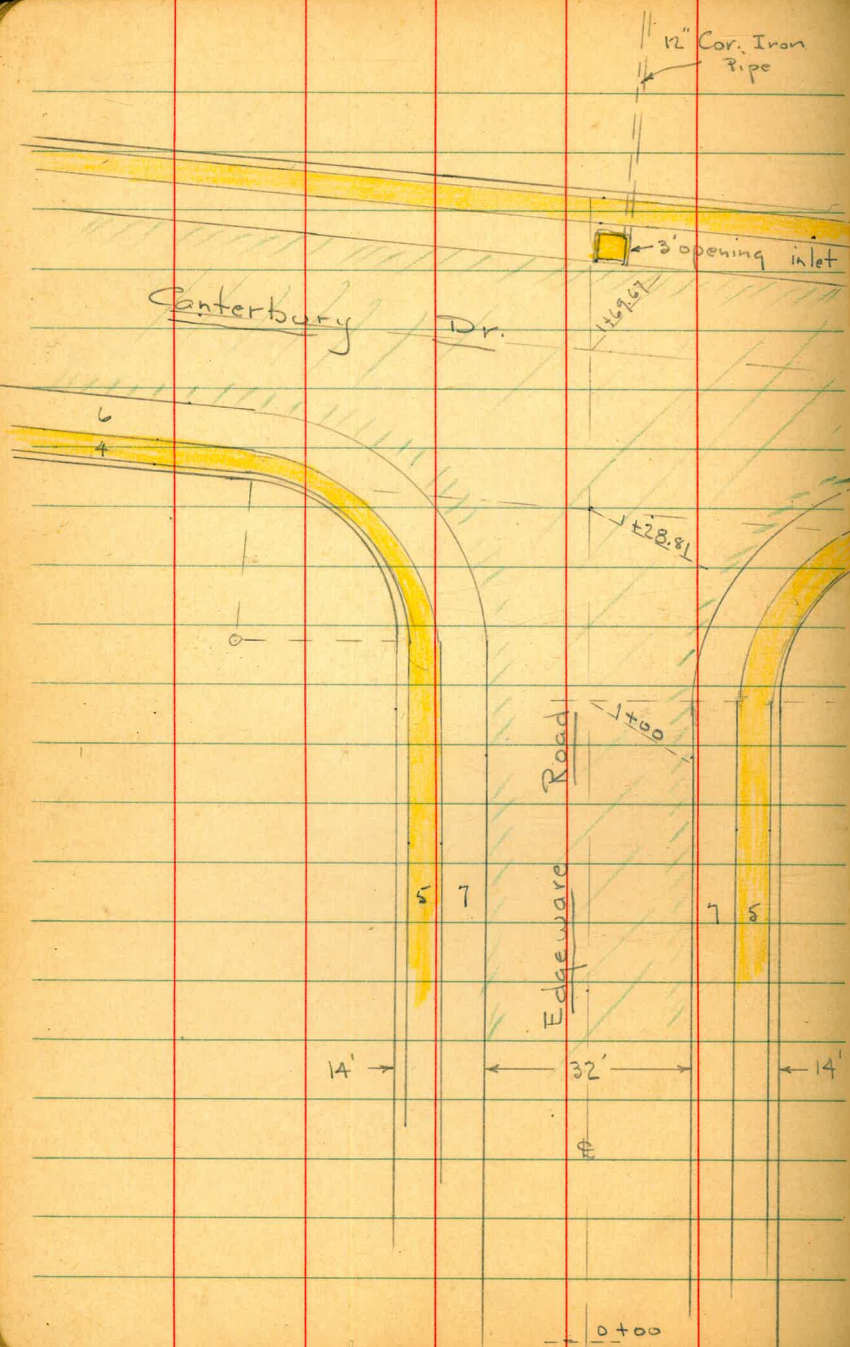
+
5'

← 20' → ← 20' →

4th

6+60.66

Jefferson Ave



N

42' 29' 42'

1+11 = P.C. Ret. on Lt.

1+00 = # Conc Dr. on Rt.

0+60

0+28.4 = E.C. N' Rad.

0+16.2 = face cb at P.C. N' Rad Ret. on Lt.

0+14 = # 17' Conc. Dr. on Rt.

0+00 = # Canterbury Dr. + # 42nd

Sect. on # 42nd

4.31 361.69

357.38

350.8.P
Canterbury
+ 42nd
P. 26

5.31	5.89	5.71	5.85	6.0	6.50	5.83
Top	gut.				gut.	Top
56.44	55.88	56.09	55.94	55.69	55.22	56.01
5.25	5.81	5.60	5.75	6.00	6.17	5.68
Top	gut.				gut.	walk
56.96	56.81	56.43	56.29	56.01	55.57	56.21
4.73	5.38	5.26	5.40	5.68	6.12	5.48
Top	gut.				gut.	Top
57.37	56.72	56.82	56.65	56.41	55.78	56.90
4.32	4.97	4.87	5.04	5.28	5.91	5.29
Top	gut.				gut.	Top
57.69	57.2	57.66	57.05	56.76	55.81	56.56
4.00	4.5	4.03	4.64	4.8	4.93	5.13
Top	gut.	Top cb.	gut.			walk
end cb.		P.C. Ret.				
57.35		57.21	56.79	56.44	55.71	55.82
4.34	4.48	4.90	5.25	5.78	5.20	5.87
25.06 =	14				gut.	Dr.
5.		on H.C. Pave			56.49	56.75
					55.70	56.25
					4.99	4.94
					gut.	walk
					Top	end
					end cb.	

361.69

Cont. N. 36

2+00 = end

2+60

T.P. 3.33 360.71 4.31 357.38

2+21 = opp. P.C. Ret. on Lt.

1+85

1+77 = Brk. in cb. on Rt.

1+68.5 = opp Φ 3' opening curb inlet on Rt.

3' x 3.6' Box - 12" Cor. Iron outlet.

1+69.67 = Φ + Φ Edgeware Rd. Prod.

1+35

Lt.

Φ

Rt.

Cont.

37

2.25 2.83 2.69 3.39 2.77
14 14 14 14
Top gut. Top

3.10 3.75 3.87 4.15 3.55
14 14 14 14
Top gut. Top 360.71

4.89 5.51 5.35 5.39 5.56 6.03 5.38
14 14 7 14 14
Top gut. Top
P.C.

5.83 5.97 6.52 6.67 6.89 6.13
25 14 7 14 14
Top gut. Top

6.20
14
Top.

6.16 7.31 10.90
14 14
Topcb. gut F.L. Box

5.89 6.26 6.82 6.99 7.25 6.15
25 14 7 14 14
on Rim of Sewer M.H. gut. Top

5.31 5.87 5.95 6.24 6.47 6.81 6.02
22.2 22.2 10 7 14 14
Top gut. Top
on Ret. 361.69

Profile Levels on Edgeware Rd.

1+28.81 = ∇ at S.L. Canterbury Dr.
Sect. 90° to ∇ Edgeware

1+07.67 = opp. P.C. 25' Prop. Rad. on Lt.

1+00 = opp. P.C. 25' Prop. Rad. on Rt.

0+75

0+50

0+25

0+00 = 100' S. of 25' Rad. P.C. on E.

Lt. = W.

∇

Rt. = E. Cont.

38

4.22	4.73	4.81	4.90	4.80	4.87	4.33
24.2	24.2	16		16	32.6	32.6
Top	gut.				gut.	Top

4.09	4.54	4.18	4.51	4.07
16	16		17.4	17.4
Top	gut.		gut.	Top

3.84	4.28	3.96	4.31	3.90
16	16		16	16
Top	gut.		gut.	Top

3.00	3.53	3.10	3.64	3.11
16	16		16	16
Top	gut.		gut.	Top

2.05	2.62	2.22	2.75	2.26
16	16		16	16
Top	gut.		gut.	Top

1.33	1.86	1.38	1.92	1.41
16	16		16	16
Top	gut.		gut.	Top

0.70	1.25	0.70	1.19	0.68
16	16		16	16
Top	gut.		gut.	
360.71 P. 37				

Rods around Returns at S.E. + S.W.
Corners of Canterbury + Edgeware

360.71 = P.37

on S. cb. Canterbury			
SE Ret. - Beg. - N. end = EC	4.32	T = Top	
6' around - 10 parts - 6' each	4.90	q = gut	
G.I. W.	4.35	T	
"	4.93	q	
"	4.40	T	
"	4.96	q	
"	4.45	T	
"	4.95	q	
"	4.37	T	
"	4.89	q	
"	4.29	T	
"	4.82	q	
"	4.27	T	
"	4.77	q	
"	4.21	T	
"	4.72	q	
"	4.15	T	
"	4.65	q	

360.71

G.I.	4.04	T	
	4.47	q	
G.I. = S. end. = PC	3.90	T	
on E. cb. Edgeware	4.31	q	
S.W. Ret. - 55' around - 10 parts		S.S. Each.	
W. cb.			
Beg. - S. end. = PC	4.09	T	
	4.54	q	
5.5	4.19	T	
"	4.64	q	
"	4.26	T	
"	4.68	q	
"	4.25	T	
"	4.71	q	
"	4.21	T	
"	4.73	q	
"	4.18	T	
"	4.73	q	
"	4.15	T	
"	4.70	q	

5.5'	4.08	T.
	4.66'	q
"	4.02	T
	4.66'	q
"	4.00	T
	4.56	q
5.5' = W. end. = FC.	3.89	F
	4.52	q.

X- Sect. 42nd - 40' st. - No. cbs. - Paved
 A.C. - from Alder to Canterbury.
 Just for Profile - all Topo. not shown

0+40 Cb Line East

0+30 = Φ Jefferson

0+14 Curb Line West - cb. broken

0+10 Curb Line East

0+00 S. Line Alder Dr.

1.18 362.91 2.15 361.73

BM. 6.50 363.84 357.38

Lt = E Φ

Rt = E 42nd
41

57.64	57.12	57.20	57.64	57.81	57.59	57.82	58.29	57.98
5.78	5.71	5.27	5.10	5.32	5.09	4.62	4.93	
20	10	2	10	20	10	10	10	20
9.04	9.04	9.04	9.04	9.04	9.04	9.04	9.04	9.04
57.09	57.25	57.82	57.72	57.61	57.43	57.18	57.14	57.50
5.27	5.82	5.66	5.09	5.09	5.30	5.78	5.78	5.78
20	20	10	2	10	20	50	50	50
57.18	57.5	56.98	57.14	57.50	57.40	57.43	57.43	57.43
5.73	5.4	5.93	5.77	5.41	5.41	5.48	5.48	5.48
50	20	20	10	2	10	20	20	20
9.04	9.04	9.04	9.04	9.04	9.04	9.04	9.04	9.04
57.8	57.5	57.00	57.49	57.5	57.36	57.71	57.42	57.42
5.1	5.4	5.91	5.42	5.40	5.55	5.20	5.49	5.49
20	15	10	2	10	20	20	50	50
9.04	9.04	9.04	9.04	9.04	9.04	9.04	9.04	9.04
57.1	57.4	56.5	57.29	57.29	57.36	57.41	57.71	57.71
5.2	5.5	6.4	5.62	5.62	5.55	5.50	5.14	5.14
14.5	13	11	10	2	10	20	20	20
at. Garage			Edge Parking			9.04	Top end Ret.	

362.91

1+75

1+50

1+25

1+08 = E Doub. Gar on Lt. - Dirt floor

1+00

0+60.46 = W.L. Jefferson

0+50 = W.L. Alder

0+46.7 = N.cb. Jefferson

42 no
42

	61.8	60.52	60.53	60.29	61.3
	2.12	2.39	2.38	2.62	1.6
	10	10	10	10	20
	edge	edge	edge	edge	
	61.6	59.84	59.91	59.70	60.3
	3.07	3.07	3.00	3.21	2.6
	10	10	10	10	20
	edge			edge	
61.3					
1.6					
20					
floor					
	61.2	59.11	59.21	59.12	60.3
	3.80	3.70	3.79	3.72	2.78
	10	10	10	10	20
	edge				
	60.1	57.75	58.01	58.08	59.4
	5.16	4.90	4.83	3.51	3.51
	10	10	10	20	20
	edge		edge		
	58.2	57.47	57.81	57.84	57.63
	4.7	5.44	5.10	5.07	5.28
	20	10	20	10	20
		edge	Rise	cut	
57.75	57.45	57.22	57.32	57.71	58.15
5.66	5.46	5.69	5.59	5.20	4.76
20	20	20	10	24.3	24.3
cut.	Top	cut		cut.	Top cb.
	end. cb				on Ret.
			362.91		

3+70 - \$ Doub. Gar. on Rt. - Conc. floor + apron.

3+50

3+20 = \$ Doub. Gar. on Rt. - Conc. floor + apron

3+16 = \$ Sing. Gar. on Lt. - Conc. floor + apron

3+00

2+50 - Sing. Gar. on Lt. - Conc. floor + apron

2+21 - \$ Doub. Gar. on Rt. - Conc. floor + apron

2+00 = \$ Doub. Gar. on Rt. - Conc. floor + apron

T.P. 5.75 366.96 1.70 361.21

1+96 - \$ Doub. Gar. on Lt. - Conc. floor + apron

Lt.

#

Rt.

42nd
43

Lt.	#	Rt.		
	63.2		61.69	62.05
	3.8	509	5.27	4.91
	20	10	10.9	21.2
		edge	apron	floor
	61.87	514	61.5	5.44
		edge		20.2
	61.82	543	5.68	
		edge	10.5	
	61.53	20	apron	floor
63.4	3.55			
	23			
	61.64			
	5.32			
	97			
	floor			
	apron			
	4.5			
	20			
	62.5			
	5.54			
	10			
	edge			
	61.42			
	5.44			
	61.52			
	61.18			
	5.78			
	10			
	edge			
	61.5			
	5.68			
	10.5			
	apron			
	floor			
	61.86			
	5.10			
	23			
	floor			
	61.78			
	5.18			
	20			
	on			
	Conc.			
	61.23			
	5.73			
	10			
	edge			
	61.45			
	5.51			
	apron			
	61.03			
	5.93			
	10			
	edge			
	61.27			
	5.69			
	20			
	apron			
	61.34			
	5.62			
	20			
	floor			
	62.5			
	4.5			
	20			
	60.98			
	5.98			
	10			
	edge			
	61.20			
	5.76			
	60.85			
	6.11			
	10			
	edge			
	61.27			
	5.69			
	20			
	apron			
	61.34			
	5.62			
	20			
	floor			
	62.52			
	366.96			
62.74	0.17			
	24			
	floor			
	62.52			
	0.39			
	20			
	apron			
	362.91			

5+30

5+16 = ± Sing. Gar. on Lt. - Conc. floor + apron

5+10 = Beg 6" Conc. + rock wall on Rt.

5+00 = ± Doub. Gar. on Rt. - Conc. floor + apron

T.P. 2.06 363.98 5.04 361.92

4+75

4+70 = ± Sing. Gar. on Lt. - Conc. floor + apron

4+50

4+20 = ± Doub. Gar. on Rt. - Conc. floor

4+00

	Lt.	±	Rt.	42nd 44
62.45	61.31	33 20	4.16 10 edge	4.07 59.91
1.53 29.2 floor	26.7 10 apron		4.40 10 edge	59.58
			57.6 16.1 Dirt	60.02
			14.1 Top	26 20 61.4
				61.15
				2.83
		61.4	2.6 20	60.62
			3.36 10 edge	60.72
				60.44
			3.54 10	60.29
			26.9 12.4 apron	21.40 21.2 floor
				16.1 Top
				363.98
				61.34
		63.0	4.0 20	5.62 10 edge
62.96	61.91			5.82 10 edge
39.8 21.2 floor	5.55 7.4 apron			5.82 10 edge
				61.14
				68.0
				20.0
				61.62
		62.5	4.5 20	5.34 10 edge
				5.09 61.87
				5.36 10
				62.4
				4.6 20
				62.26
				4.70 21.9 floor.
				61.86
		63.0	4.0 20	4.99 10 edge
				4.90 62.06
				5.10 10 edge
				5.0 20
				62.0
				366.96

Lt.

E

Rt.

42 nd

45

check starting B.M.

6.59 357.39 357.38

5 + 59.5 = 0 - 56.5 - Page 26

59.8

4.2
19.5

58.81

5.17

9
edge

59.07

4.91

58.94

5.04

11
edge

59.2

4.8

16.3
Dirt

60.25

3.65

16.3
Top

60.6

3.2

20

363.98

X sec Locust St.

Whitson to Kenaphan

Moore

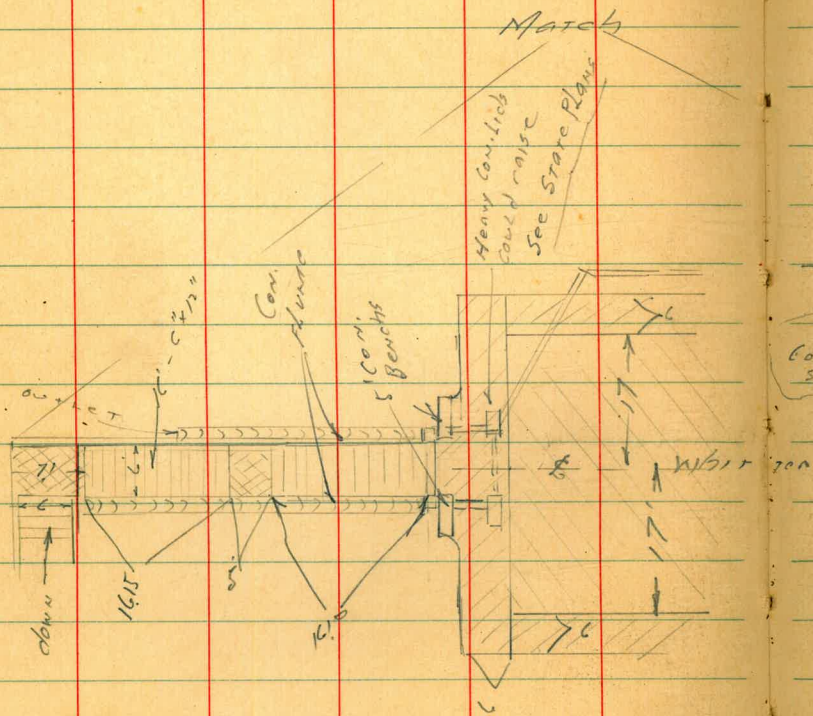
N.O. 25001

Boyer

Green

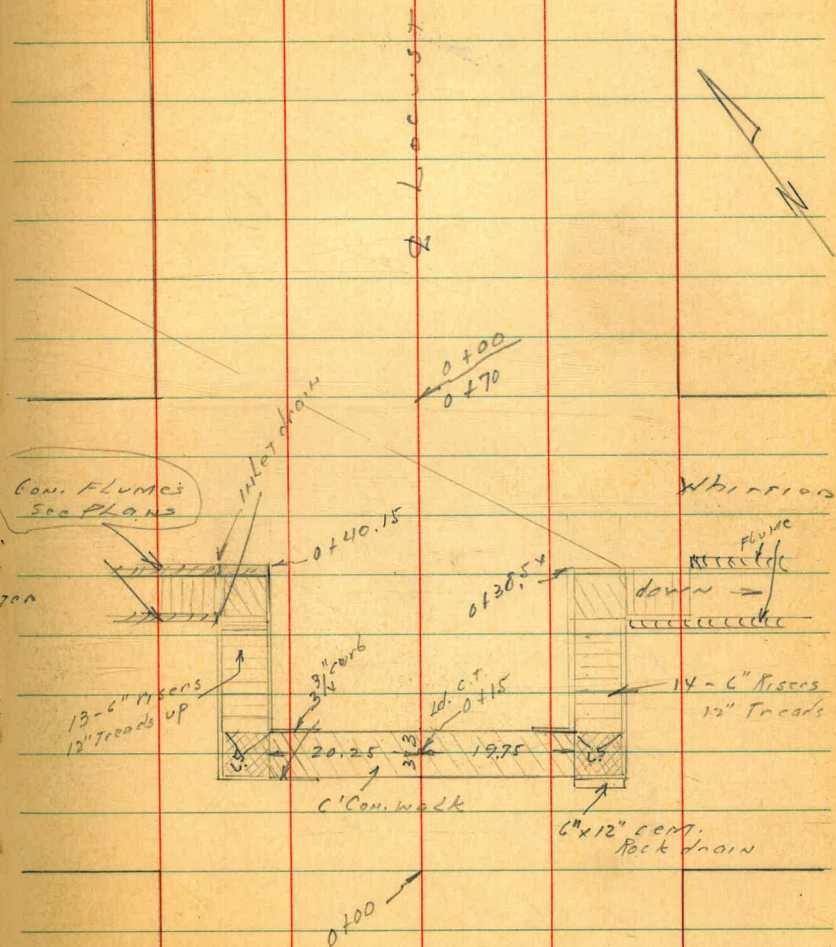
Roberts

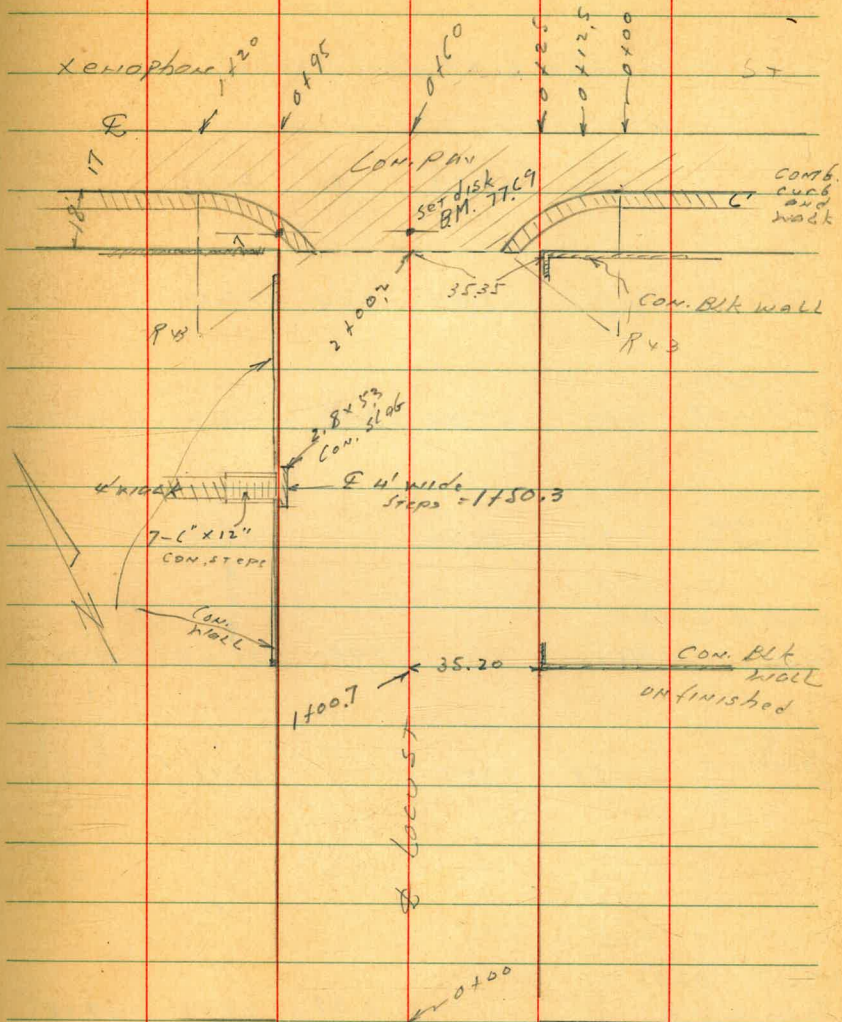
11-4-47



Indexed
818

46





WATER

Levels on Pay, etc

on sly $\frac{1}{2}$ of Xenophon

at Locust

T.P. 1276 57.69 1.94 44.93

T.P. 11.75 46.87 0.68 35.12

Fd.

T.P. NWBP 4.34 35.80 7.04 26.46 ?

NWBP

Rosecrans
ALCOTT 1.92 33.50 31.58

check to NWBP

Rosecrans & ALCOTT 7.49 31.58 31.30 ?

NWBP

Rosecrans
Browning 1.59 39.07 37.48 ✓

This may have been moved

check to NWBP

Rosecrans &
Browning 9.39 37.48 37.48 ✓
0.00

SWBP 2.54 46.87 44.33

Rosecrans

↓
CURTIS

Lt.

2

Rosecrans & Zola

5 $\frac{L}{2}$ Xenophora St.
Ketch P47

0 + 45

0 + 35

0 + 25 Ely Locust

0 + 12.5

T.P. 12.75 82.38 0.16 69.63

0 + 00 c6. B.C.

T.P. 12.75 69.79 0.16 57.55

57.69

LT

5.35 77.03

35
edge Pav.

76.80
5.58

5.91 76.47

35
c6. end

74.63

74.16

775
25.1
08

82.2
25.1
97

76.36

70.92

11.92
18.1
08

11.96
18.1
97.

68.55

12.4
17
08

68.09

17
17
97

70.93

11.95
17

71.03

11.85

82.38

12.4
17
97

576.85

17

75.93

6.45
17

73.94

8.44
17

75.72

6.66

75.82

8.56

576.77

Xenophon

1 + 20 c6 EC

LT	1.14	1.14	1.14
	17	17	17
8307	83.51	83.51	83.51
3.84	4.40	4.40	4.40
186	186	17	17
c6	91		

1 + 07.5

Budge
in Line

T.P. on disk
5.71 Xenophon
+ 8 Locust

10.22 87.91 4.69 77.69 Set B17

81.22	80.68	80.82	87.91
1.16	1.70	1.56	
24.9	24.9	17	17
c6	11		

0 + 95 w/L Locust

79.00	78.59	79.19	79.21
3.38	3.79	3.19	3.17
35	35	17	
c6	91		
end			

0 + 85

0 + 75

78.30	78.35	78.29
4.08	4.03	4.09
35	17	
c.d. 1/2 Pan		

0 + 60 & Locust

77.72	77.57	77.52
4.66	4.81	4.86
35	17	
pan.		
colage		

82.38

82.38

Sec Locust St. Sketch p. 26

Whizzing to Kenophon

0 + 38.5x

0 + 18 w/ly edge 6' walk
Cross

0 + 12 Sly edge 6' Com. Cross walk

0 + 07

0 + 00 = Sly Whizzing 50' R.P. # 3095

BM disk
57' Line 9.53 87.22 77.69

L +

83.58
27

83.98

3.24
2.95
Walk and Landing

84.02

3.20
2.75
Landing

96.2

+9.0
35

97.7

+10.5
35

90.5

+3.3
20

90.9

+3.7
23

88.2

+1.0
14

86.5

+1.3
12

87.2

3.0
8

83.9

3.3
9

83.35

3.7
4

83.6

3.6
3

82.9

4.3
20

82.9

4.3
28

77.7

9.5
35

78.7

8.5
35

68.8

18.4
50

68.9

18.3
50

83.33

3.89

Walk and Landing

83.35

3.87

83.5

3.7

82.56

4.66

Walk

82.61

4.61

Walk

82.83

4.39

Landing

82.87

4.35

Landing

3.80
1.70
Top Com.
Ret. Wall

13.5
35
dirt

83.58

83.92

87
66.9

51

0+21 26.4 small Pine
 0+05 26 Lt small Pine
 0+02 24.5 Lt small avocado

0+00
 0+70 nly Whittier St

0+68 25 Lt orange tree

0+59 26.5 Lt small Pine

SMALL
 0+54 25 Lt 909314

0+52

0+43

0+40.5

87.22

93.3
 2.5
 dirt

27

94.9
 92.9
 87.9
 83.5
 83.0
 83.1
 82.9
 73.3
 69.0

+7.7	+5.7	+0.7	3.7	4.2	4.1	4.3	13.9	18.2
35	24	12	10	7		20	35	50

94.3
 92.6
 87.2
 84.3
 83.3
 83.4
 83.2
 73.6
 69.6

+7.1	+5.4	0.0	2.9	3.9	3.8	4.0	18.6	17.6
35	23	13	11	7		20	35	50

93.5
 89.7
 88.6
 84.9
 83.3
 83.5

+6.3	+2.5	+1.4	2.3	3.9	2.7
35	20	10	12	7	

91.64
 86.5
 84.9
 83.4
 83.5

+4.42	0.7	2.3	3.8	2.7
20.1	20	12	7	

Top
 Cor.
 Pet
 Wall

87.22

18

15

52

Lowest
 1+10 31 LT SMALL FIG TREE

1+00.7 25.5 LT P.P. P2258
 and Beg. of 8" Con. Wall on LT.

0+96 28 LT SMALL PINE

0+80 " " " "

0+75

0+62

T.P. 7.55 85.24 9.53 77.69 on disk

0+58 25' LT, Large avocado tree

0+50

0+36 26.5 LT SMALL PINE TREE

87.22

LT # PT 53

91.7	91.2	88.7	86.7	80.9	80.8	80.7	76.1	72.9	77.52	67.1
+65	+60	+35	+15	4.3	14	4.5	4.1	12.3	77.2	18.1
34.7	34.7	21	13	7		19	25	35	35.2	55
Top wall	dist	Base wall							Top unfinished	Con. 8" wall

91.2	90.6	89.5	81.5	81.4	80.2	70.4	63.1
+67	+55	+43	3.7	3.8	5.0	14.8	22.1
35	30	23	7		18	35	55

92.9	91.2	81.8	81.7	80.8	69.4	59.4
+7.7	+6.0	3.4	3.5	4.4	15.8	25.8
35	22	7		18	35	55

85.24

93.5	92.1	86.5	82.1	82.0	81.6	70.9	63.8
+6.3	+4.9	0.7	5.1	5.2	5.0	10.3	23.4
35	25	13	7		18	35	55

87.22

2 + 00.2 SL Xenophon see P. 49
for Pav. & Curbs

82.6	81.0	80.5	78.9	77.6	79.6	77.0
2.6	4.2	4.7	6.8	7.6	10.6	7.5x
35	33	25	15	dirt	35	35 Top
dirt	dirt	dirt	dirt	dirt	dirt	UNFIN WALL

1 + 92 20 L + 1" di. Eucaly. end
WALL

88.9	86.5	82.6	78.5	77.8	76.9	74.4	68.0
13.7	+1.3	2.6	6.7	7x	8.8	10.8	17.2
34.7	34.7	14	9		30	35	55
Top Wall	dirt						

1 + 80

89.74

+4.0
34.9
Top
Wall

86.2	86.9	85.2	82.2	78.4	78.0	77.1	73.1	70.8	67.4	67.4
+1.0	+1.7	0.0	3.0	6.8	7.2	8.1	12.1	14.4	18.8	18.8
34.9	34.9	24	11	7		28	35	41	52	50
Bot. Wall	dirt									

1 + 50.3 4' Con steps

88.6	88.4	86.4	85.2	79.5	79.3	79.0	73.8	68.4
+3.4	+3.2	+1.2	1.0	5.7	5.9	6.2	11.4	16.8
34.8	32	18	12	7		19	35	55
Top Step	Top Step							

+44 32.5 L 4" di. Palm

+29 31 L + small Fir tree

90.74

89.5	89.7	88.8	85.9	80.2	80.1	80.2	76.7	73.8	68.3
+4.3	+4.5	+3.6	+0.7	5.0	5.1	5.2	8.5	11.4	16.9
34.9	34.9	26	12	7		19	25	35	55
Bot. Wall	dirt								

1 + 25

+5.7
34.9
Top

85.24

85.24

check to NW BP
on creek 2.14 37.48 37.48

T.P. 8.04 39.62 1.92 31.58 31.58
7.04 33.50 26.46 P.48

T.P. 8.34 26.45 $\frac{26.46}{.001}$

T.P. 4.00 34.79 11.78 30.79

T.P. 1.26 42.57 12.59 41.31

T.P. 0.37 53.90 12.70 53.53

T.P. 0.10 66.23 12.01 66.13

T.P. disk 0.45 78.14 7.55 77.69
xenophon 7'
& Locust

8524

Rosecrans + Browning

Book says 31.36?

NW BP Rosecrans + ALcott

NW BP Rosecrans + Zolger Look this up please

Sewer Levels
Cont'd. from 1782-5v.

15x

153 + 50, 57 A Lt.

T.P. 4.57 75.36 2.10 70.79

153

+ 50

152

+ 50

151

+ 50

150

149 + 50

72.89

INDEXED
MAR 8 1948

La Jolla Trunk
Sewer

W.O. 66058

56

4x 71.0

4.6 70.8

75.36

2.7 70.2

3.0 69.9

3.5 69.4

3.8 69.1

4.3 68.6

4.9 68.0

5.5 67.4

5.3 67.6

72.89

1784

+50

T.P. 2.03 67.53 9.86 65.50

158

+50

157

+58.95 Δ P

156

+50

155

154 + 50

75.36

8

3.4 64.1

3.0 64.5

67.53

10.6 64.8

10.1 65.3

9.2 66.2

8.6 66.8

7.5 67.9

6.7 68.7

5.0 70.4

4.3 71.1

75.36

162	5.5	62.0
-----	-----	------

161 + 74 ^{1/2} L.R.	5.5	62.0
------------------------------	-----	------

+50	5.2	62.3
-----	-----	------

161	5.1	62.4
-----	-----	------

+50	4.8	62.7
-----	-----	------

160	5.3	62.2
-----	-----	------

+50	4.5	63.0
-----	-----	------

159 + 0	4.1	63.4
---------	-----	------

+95	9.2	58.3
-----	-----	------

+87	8.7	58.8
-----	-----	------

67.53

67.53

+60	+	#1	-
+54			
+50			
165			
+50			
7.36	<u>70.35</u>	4.54	62.99
164			
+50			
163			
162+50			
	67.53		

8.0	62.3
7.6	62.7
7.4	63.0
7.8	62.5
8.2	62.1
<u>70.35</u>	
5.3	62.2
5.4	62.1
5.3	62.2
5.5	62.0
67.53	

+ 38 edge of oil parking old Parking Lot	3.6	66.7
168+1727 E Lt	3.5	66.8
168	3.5	66.8
+50	4.1	66.2
167	5.0	65.3
+50	6.2	64.1
166	6.5	63.8
+96	7.5	62.8
+90	6.2	64.1
+67	6.8	63.5

70.35

70.35

170 + 95⁹⁸ L. RT

+ 50

+ 44

+ 33

170

+ 84

8.31

75.86

2.80

67.55

+ 50

169 + 0

+ 50

70.35

5

70.9

7.5

68.4

8.2

67.7

10.5

65.4

9.5

66.4

9.0

66.9

75.86

3.7

66.6

3.7

66.6

3.8

66.5

70.35

175

+50

17x

+50

173

172 + 910x Δ Lr at Colina 9

+50

172

+67

8.92 ^v 82.40 2.38 ^v 73.48

171 + 50

75.86

8

82

74.2

76

74.8

64

76.0

59

76.5

45

77.9

41

78.3

46

77.8

52

77.2

57

76.7

82.40

2.4

73.5

75.86

+50

T.P. 3.97 65.30 12.27 61.33

+43.3 Navy Fence

178

177 +50

176 +92.30 A Pt = Beg. of Alternate Line

+50

TP 2.99 73.60 11.79 70.61

176

175 +50

82.40

(Cont. on old line)

5.4 59.9

65.30

14.3 59.3

14.4 59.2

11.9 61.7

↓
↓
↓
↓

8.94 ^{2"x2"} H-6 64.66

6.1 67.5

73.60

12.0 70.4

10.8 71.6

82.40

176+92.3 Δ Rt. Beg. ALTERNATE LINE

81

64.6

STUB

175+75.26 12.73 72.76 60.03

72.76

1650-xx

↓

60.03
0.05

176+75.26 Fd. STUB N.L. Midway 5.32 59.98

5.3

60.0

176+49.8178+81.29 Δ RT E 8.

5.9

59.4

+77

5.9

59.4

+76

12.4

52.9

178+60

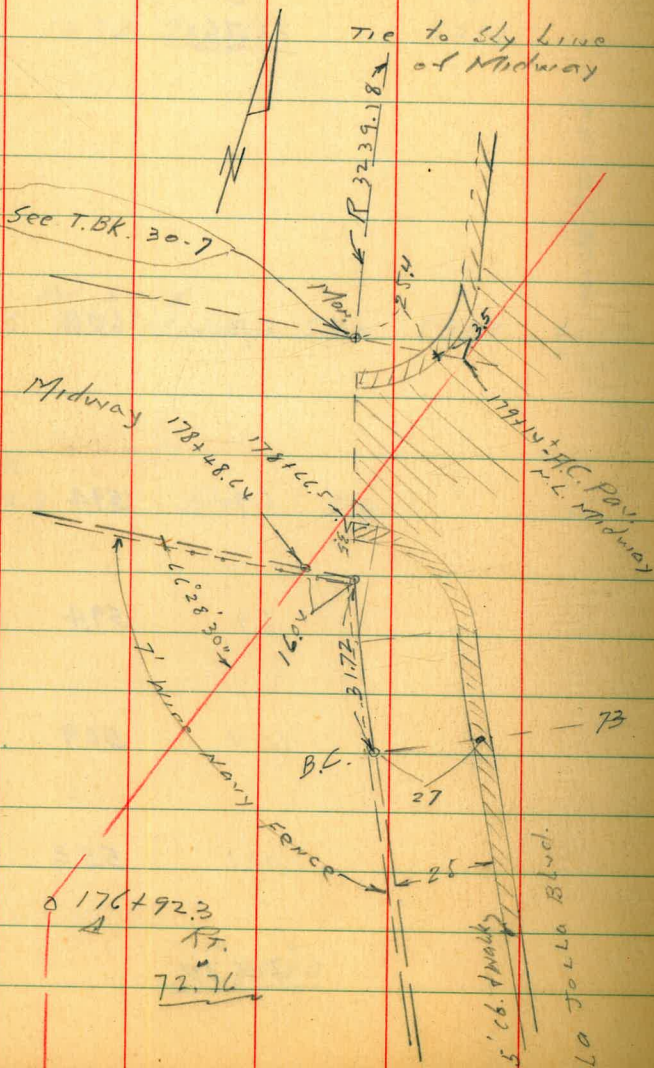
10.1

55.3

65.3065.30

179

178 + 70.7 Beg. 6" A.C. Pav.



+ 48

178

+ 81

+ 50

177

176 + 92.3

Kf.

72.76

65

3.2

69.5

49

67.8

60

66.7

86

64.1

91

63.7

77

65.0

80

64.7

72.76

105

182

+50

181

+50

180

179+95.28 A Lt.

+79.3 E curb La Jolla Blvd

179+31.9+ Inv. sec. Ex. S. line

Fd. SE. BP.

Set B.M.

T.P.

Midway

and
La Jolla
Blvd

5.85

77.72

0.89

71.87

71.80

old City

72.76

Lt

E

R

37

74.0

18

75.9

24

75.3

138

73.9

42

73.5

51

72.6

56

72.1

71.50

71.95

6.22

6.67

curb

SUT.

64.87

73.0A

71.3

70.18

66.18

12.85

4.28

64

7.54

11.54

Inv.

T.M.

T.M.

Inv.

BK. 1782

77.72

+672 edge Con. walk
 +50
 184
 +50
 T.P. 6.08 82.18 1.62 76.10
 183
 +82
 +79
 +57 Con. walk
 182 +50
77.72

£
 6.37 75.81
 6.7 76.0
 5.9 76.3
 5.8 76.4
82.18
 1.7 76.0
 1.8 75.9
 3.2 74.5
 3.4 74.3
 3.6 74.1
77.72

+79.9 drive
Con. walk

+50

187

+50

186

+50

+30.3 edge walk

185 + 151

+99.13 Int. Sewer & Forward
d Rt.

184 +75.5 curb

82.18

5.9 76.3

6.7 76.0

6.1 75.9

5.8 76.4

6.7 76.0

5.9 76.3

75.10
6.45 75.73

75.67 75.23

6.51 6.95
curb gut

63.77 74.97

18.41 7.21
50 50
Inv. Rim
M.H.

75.32

6.86

75.71 75.12

6.47 7.06
68 gut

82.18

M.H. see plan.

+54

+533 end oil Pav.

+126 Beg. oiled park Los

190

+50

189

+50

+063 Con. walk

T.P. 5.88 82.95 5.11 77.07

188

82.18

4

4.9

78.0

5.5

77.4

5.8

77.1

6.1

76.8

6.7

76.7

6.5

76.4

6.6

76.3

6.44

76.51

82.95

5.7

76.5

82.18

69

+65	edge					2.9	80.0
+59.9						79.93	79.35
						302.	360
						curb	947
check to B.M. ^{B.P.} S.W. Ret. Bird Rock Ave. \downarrow 29 Jolly Blvd		3.82	79.13	old City 79.6 79.09 1150-45			
				69.70	79.25		
192 +44.3	A Lt			13.25	3.70		79.3
				24.7	24.7	3.6	M.H. See plan
				1.14	Riv M.H.	79.27	78.58
+ 26.1						3.78	4.37
						curb	947
+31	edge walk					3.73	79.22
192						3.6	79.3
+50						4.6	78.3
191						4.4	78.5
190 +59.1	Can walk					5.13	77.82
						82.95	
						<u>82.95</u>	

194

oil

+ 54.6 Beg. oil drive way
and park Lot

+ 50

195

+ 50

T.P. 2.11 $\overset{\vee}{84.41}$ 0.65 $\overset{\vee}{82.30}$

194

+ 60 Car

+ 50

193

$\overset{\vee}{82.95}$

8

4.9

79.5

71

4.3

80.1

3.8

80.6

3.6

80.8

3.4

81.0

$\overset{\vee}{84.41}$

1.4

81.5

1.34

81.61

1.5

81.4

1.7

81.2

$\overset{\vee}{82.95}$

+50

6.7 77.7

+446 Con walk

6.8 77.6

198

6.1 78.3

+63 Con walk

5.8 78.6

+50

5.7 79.2

197

5.3 79.1

+899 Con walk

5.34 79.07

+613 Con walk

5.1 79.3

+50

4.7 79.7

196+38 end oil pay

4.7 79.7

8441

8441

+82 curb

200 + 588

Int. sec. E Ex. Sewer
approx E of camino

de La Costa

+225 curb

+156 edge walk

200

150

199 400

T.P.
Ft. B.M. B.P.
w. cb. Blvd.
125' S. of
Camino de
La Costa

577

81.73

8.45

75.96

old City
75.84
75.89
1650-46

198 + 7557

N Ly Bird Rock

84.41

73.55 73.27
818 8.50
curb gut

73

7.7 74.0
See 1650-46
for M.H.S

74.76 74.39

6.97 7.34
cb gut.

6.84 74.89

5.9 75.8

4.9 76.8

3.7 78.0

81.73

84.41

+50 Lawn end of till
 +29.4 N. edge dn.
 201+20.8 S. edge Con. dr.
 201
 200+50 Lawn
 200+05.8 N. edge Con. dr.
 BMBP
 W. C6 Blvd 310 78.99
 125 S. of
 Av. de Costa
 199+820.8
 201+5113 E8.
 200+99 con. Walk
 +89.5
81.73

60 73.0

64 72.6

635 72.64

65 72.5

63 72.7

612 72.87

78.99

79 73.8

762 74.11

818 73.55

81.73

Location of Poles & trees

+96 10 ft 12" eucal
 187+24 10 ft 12" eucal
 186+70 11 Lt PP 151
 185+34 4 Lt PP 2398
 +43 70L PP 149
 184+40 6.7 Lt 14" eucal
 183+65 10.3 Lt 9" eucal
 +97 15.3 Lt PP 148
 182+96 9.6 L 12" eucal
 181+72 12.7 Lt P.P 147
 180+40 7.6 Lt P.Pole 146
 +88.2 E. side sidewalk 6.3R 8" Euc.
 +793 East cb La Jolla Blvd
 +31.9 10's existing sewer La Jolla Blvd
 179+14.9 3.4 L ^{to cb} N. line Midway
 89 17 Lt end of cb N side Midway
 70.7 beg pavement
 +665 end of cb S side Midway 3.5 R
 178+61 6 Lt guy pole

La Jolla Sewer

198+496 9.2L PP160
 +28 9 Lt PP159
 197+17 6 Lt 12" eucal
 195+57 9. Lt PP 158
 +92 8.5 Lt 12" eucal
 +40 9 Lt PP157
 +17 8 Lt 18" eucal
 194+05 3" eucal 5 Rt
 +42 8.5 Lt 10" eucal
 193+22 9.5 Lt PP156
 +65 Blvd Stop 4 R
 192+21 (15 Rt) PP1-600-CP 15 R
 +95 9.5 Lt PP 155
 191+00 8.5 Lt 24" eucal
 190+568 10 Lt PP 154
 190+533 end oiled
 190+126 beg oiled Parking area
 189+27 11 Lt PP153
 +75 10.5 Lt 12" eucal
 188+04 11 Lt PP 152

Location of Poles & Trees

La Jolla Sewer

76

200+08 8.2 Lf PP - P5803

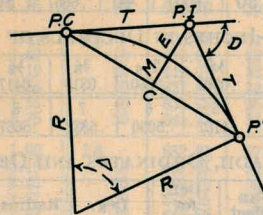
+86 9.5 Lf PP 161

199+42 6.5 Lf 12" eucal

4/11/11

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius= $R = \frac{50}{\sin. \frac{D}{2}}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers } \frac{\Delta}{2}$ (6)
- External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) $\Delta = \text{Central Angle}$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.—Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D$ or = def. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to $41.9 = 43.9$. For slopes of 1 on 1 see inside of front cover.