

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide Side Slopes 1 on 1.
For Single Track Embankment.

MICROFILMED

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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130
1794

INDEXED

to page # 74

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Pages	
1-11	Vsec Bangor (Cresta Real) / Sub.
12-19	" " Golden Park Ave.
20-23	" " Wabaska Row. - Macauley
25-31	" " Midway St. - LaJolla Blvd. to Ocean
32-46	" Bangor INDEXED to 600' North " John - Bangor to 300' west JUL 12 1948
47-50	" Golden Park ave So line Lucinda to Cresta Real (Sub)
51	Location water valves Jennings & Bangor

76 Ties Linda Vista Rd. & Ulrich

X sec Banger ST
 S.L. P.L. 179 to Jennings St.

INDEXED

W.O. 25001

Morse
 Begg
 Gosse
 Roberts

7-23-47

Ref. F.B. 1565-14

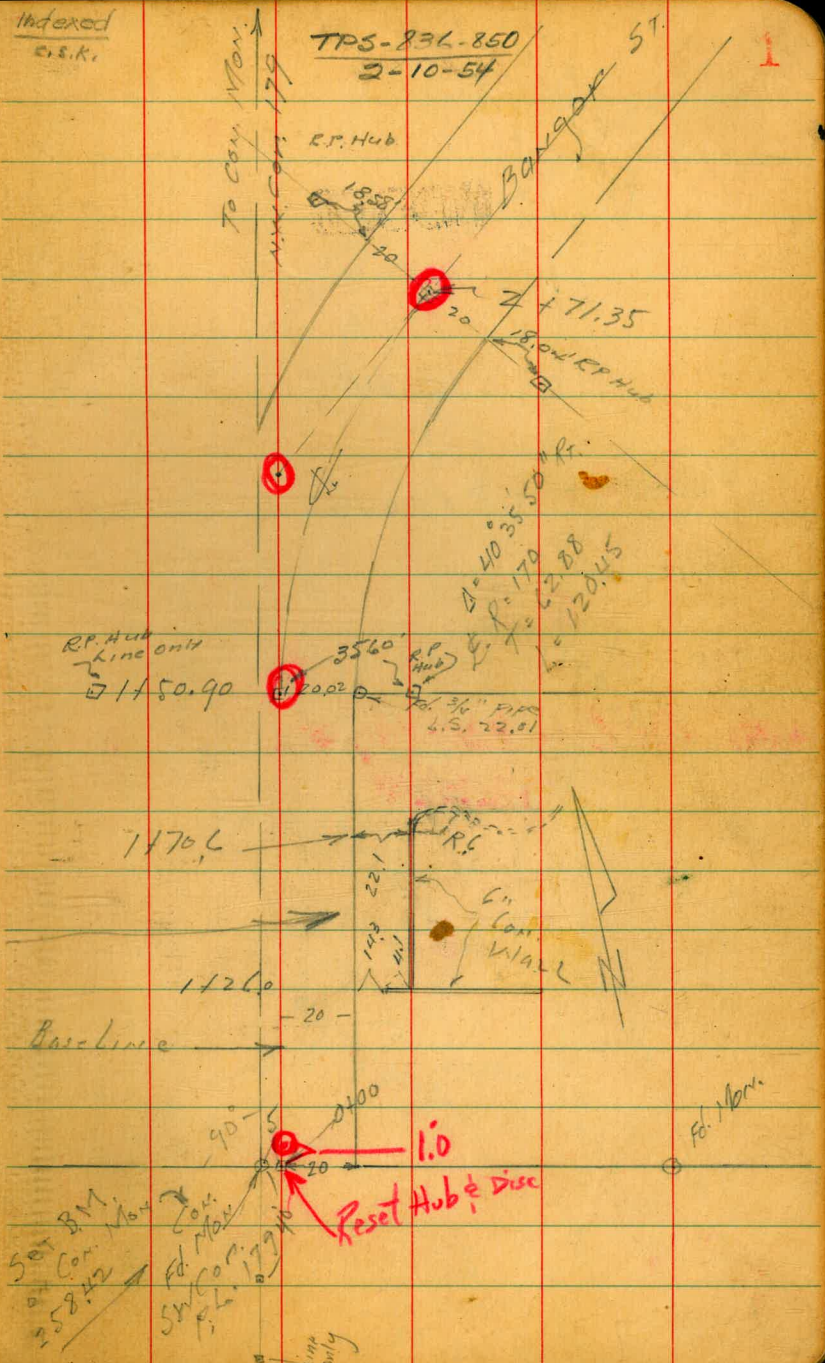
= set 2"x2" Hubs.

Points Marked \odot - Reset L.d. & Disc in Conc. Pav.
 Feb. 1954

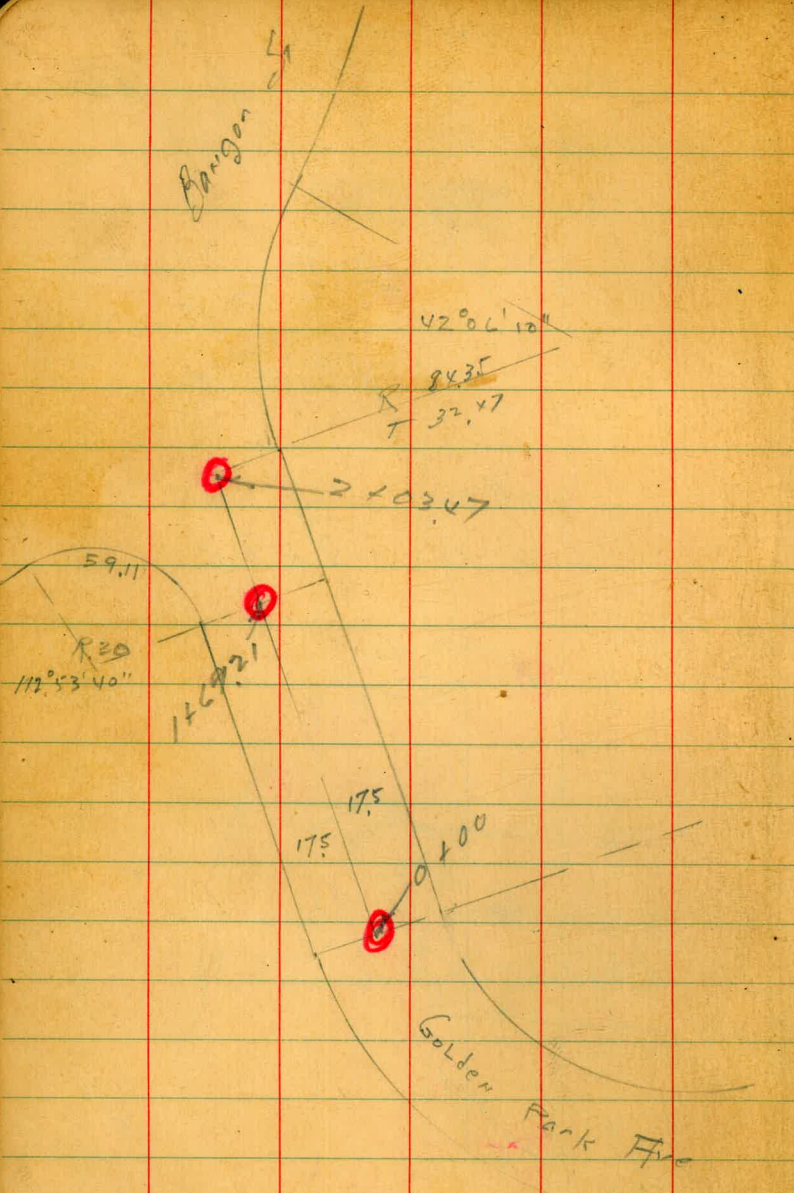
Levels on Wall
 Page 52

Indexed
 C.S.K.

TPS-236-850
 2-10-54



Bangor



42°06'10"

8435

T 32.47

2 x 0347

59.11

RED

112°53'40"

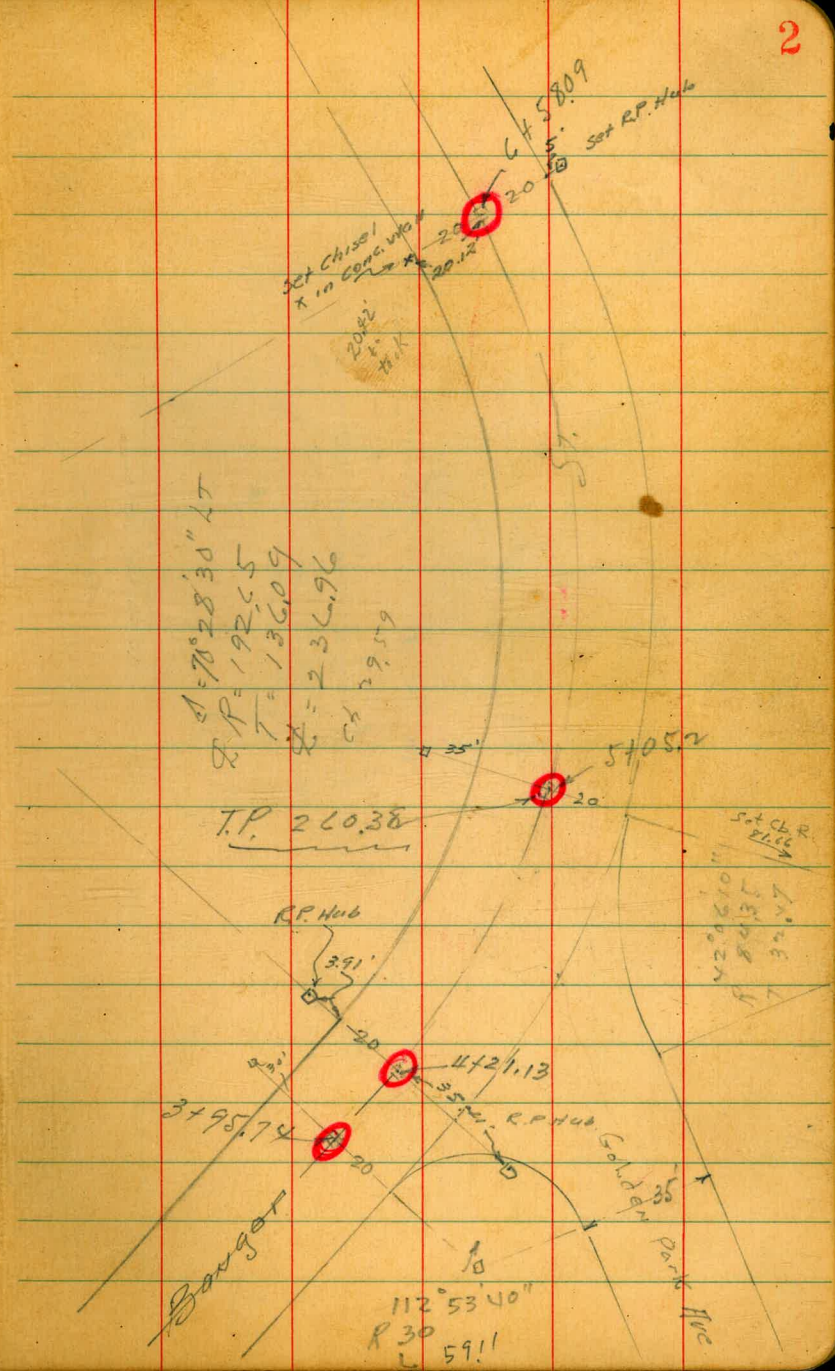
146921

175

175

0 x 00

Golden Park Ave



Set Chisel
X in Conc. w/

2042
T
41K

645809

Set RP Hub

d = 70°28'30" LT

R.P. = 192.55

T = 136.09

X = 236.96

Ch 29.19

T.P. 26038

RP Hub

391

3795.74

4721.13

Bangor

112°53'40"

R 30

L 59.11

Set CLR
P.L.C.C.

429610
R 8435
T 32.47

5405.2

Golden Park Ave

S. L. Jennings

PL. 119
Mon.
PL. 119

Reset Mon.
Feb. 1954

x 3

93.45
14.38
23.14

130.97

93.45
93.33
Rec.

23.14

Mon. Oct. 7 1948

Mon. Feb. 12 1949

Set Hub (on PL. Line)

d = 59.49'
R = 25
T = 14.38

7+22.2

Chisel
20'

6+87

Set Chisel
X in Con. Mon. 20.12

6+58.09

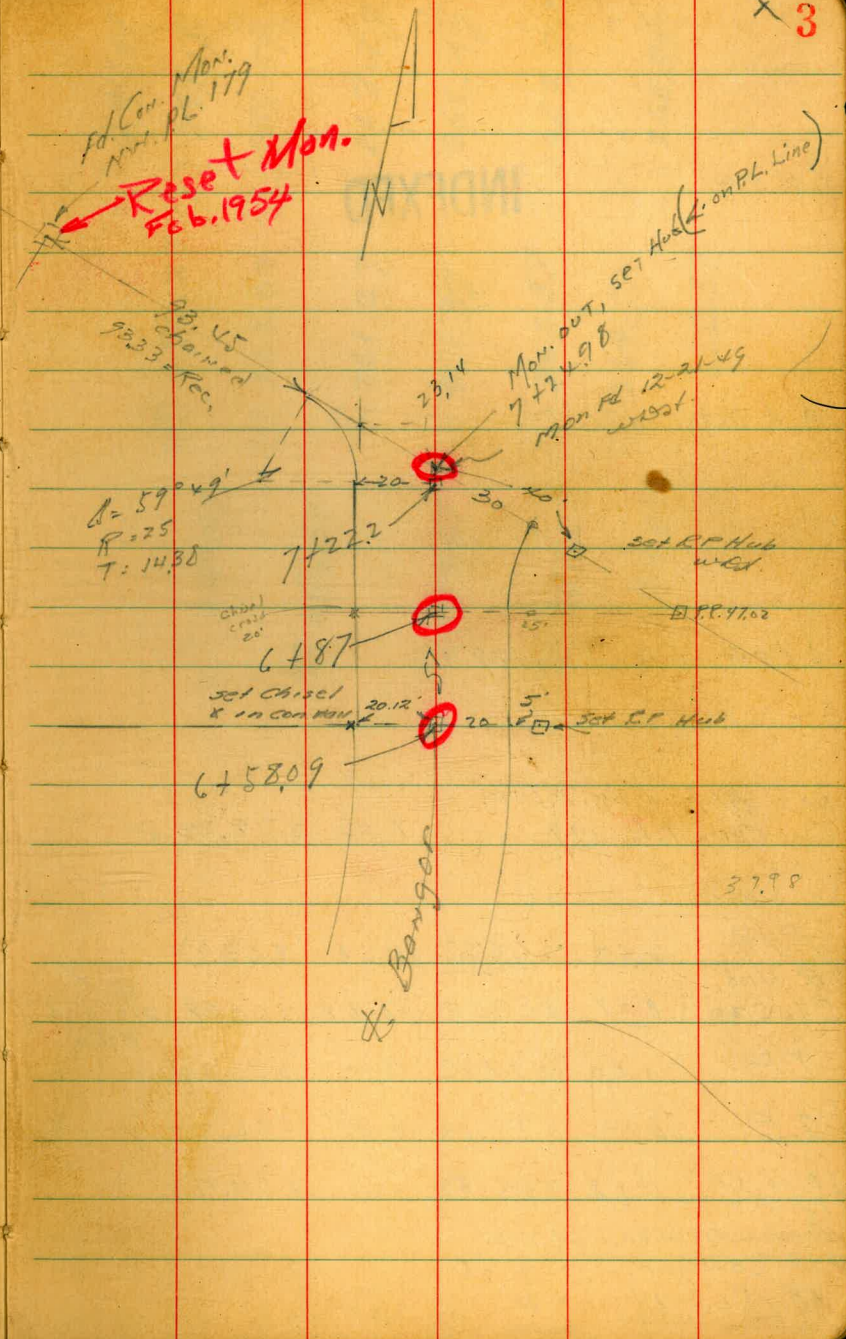
Bangor

Set R.P. Hub
w. Ed

Set P.P. 10.2

Set R.P. Hub

37.98



Levels on Bangor St.

INDEXED

1.00

0.750

0.700 S.L. P.L. 179

Set B.M. Con. Mon.
Sw Cor. P.L. 179

8.15 258.42 ✓

T.P. 2.60 266.57 4.68 263.97

T.P. Hub 5.105.20 8.27 268.65 10.88 260.38 $\frac{212}{100}$ Hub P.O.C. ✓

T.P. 0.52 271.26 4.16 270.74

T.P. 8.32 274.84 0.37 266.54

S.E. 10' R.P. 12.18 266.89 254.71

Ed. C.T.
Harbor View Dr. Ed. C.T.
and Bangor. 17' E of

FB. 1565-14 7' Pt. on S.E. Cor.

247.47 19.1 40 17.4 27 14.0 20 249.17 4.8 4 252.57 4.1 20 262.27 2.7 20 263.87 1.0 35 265.57

250.27 16.3 35 14.5 20 252.07 5.3 9 261.27 7 261.37 4.2 17 262.37 2.0 20 264.57 0.0 35 266.57

254.67 11.9 35 10.7 20 256.37 6.9 20 259.67 4.3 20 262.27 2.1 35 264.47

266.57

2 + 71.35 F.C.

2 + 41.24

T.P. 7.98 270.99 3.5C 263.01

2 + 11.13

1 + 81.02

1 + 50.9 B.C.R.

266.57

264.69	264.69	263.99	263.39	263.69	263.49	263.89	267.69
6.3 30	6.3 24	7.0 20	7.6 17	7.3 16	7.5 16	7.1 20	6.3 30
		263.59	263.39	263.19	263.19	264.19	266.69
		7.6 30	7.6 20	7.8	7.8 15	6.8 20	4.3 27
	263.07	262.97	270.99	262.87	264.47	266.17	267.07
	3.5 33	3.6 20	3.6 20	3.7 17	2.1 20	0.8 25	4.0 35
250.57	251.17	254.67	257.47	263.37	262.77	263.07	265.27
16.0 40	15.4 35	11.9 20	9.1 17	3.2 14	3.8	3.5 20	1.3 35
249.87	250.87	253.27	262.57	262.57	263.67	265.87	
16.7 40	15.7 25	13.3 20	4.0 2	4.0	2.9 20	0.7 35	
			266.57				

4 + 5075

4 + 2113 BC L7

3 + 95.74

3 + 50

3 + 00

270.99

$\frac{11}{30}$	265.99	$\frac{7.9}{30}$	263.09	$\frac{10.8}{12}$	260.19	$\frac{11.2}{12}$	259.79	$\frac{12.2}{20}$	258.79	$\frac{12.9}{30}$	258.09
$\frac{11}{30}$	265.99	$\frac{7.2}{30}$	263.79	$\frac{10.2}{13}$	260.79	$\frac{10.5}{13}$	260.49	$\frac{11.0}{20}$	259.39	$\frac{12.8}{30}$	258.19
$\frac{11.5}{30}$	265.59	$\frac{7.6}{20}$	263.39	$\frac{9.0}{16}$	261.99	$\frac{9.7}{16}$	261.29	$\frac{11.0}{16}$	259.99	$\frac{9.8}{20}$	261.19
$\frac{11}{30}$	266.99	$\frac{7.4}{20}$	263.59	$\frac{7.8}{16}$	263.19	$\frac{7.8}{16}$	263.19	$\frac{7.5}{20}$	263.49	$\frac{6.4}{25}$	264.59
$\frac{11}{30}$	265.99	$\frac{7.1}{20}$	263.89	$\frac{7.0}{20}$	263.19	$\frac{7.8}{16}$	263.19	$\frac{7.5}{20}$	263.49	$\frac{6.3}{30}$	264.69
$\frac{11}{30}$	263.99	$\frac{7.0}{20}$	263.99	$\frac{7.0}{20}$	263.99	$\frac{7.0}{20}$	263.99	$\frac{6.7}{20}$	264.29	$\frac{6.1}{30}$	267.89

270.99

5+9885

5+6973

5+3961

T.P. 1219 272.57 10.61 260.38 260.38 E.H. 6

5+052

4+8037

270.99

3.0 30	4.5 24	6.8 20	7.9 18	8.0 80	7.9 5	7.3 20	8.3 30	269.57	268.07	265.77	264.17	262.87	263.17	263.17	263.67	262.87	264.27
8.5 30	9.4 20	10.9 11	10.8 10.8	10.8 10.8	11.3 20	13.0 30		264.07	263.17	261.67	261.77	261.67	261.37	259.57			
7.4 30	9.5 20	10.4 11	10.6 10.6	11.3 20	11.8 30			263.59	261.49	260.59	260.39	259.69	259.69	259.19			
5.6 30	9.6 20	11.0 11	11.2 11.2	12.2 20	12.6 30			265.39	261.39	259.99	259.79	258.79	258.39				

270.99

7+24.98 Sec. on S6, Jennings

7+22.30

6+87.0 BC on P7.

6+58.09 E.C.

6+28.47

272.57

271.87	0.7	27.40
272.07	0.5	23.14
272.07	0.5	5
270.77	1.8	22
270.27	2.3	30

272.07	0.5	30
271.97	0.6	20
270.67	1.9	27
268.87	3.7	12
268.87	3.7	20
269.77	3.8	30
271.97	3.0	30

272.37	0.2	30
268.17	4.4	20
267.67	4.9	19
267.37	5.2	20
267.67	4.9	8
269.27	3.3	20
270.67	1.9	20
270.67	1.9	30

271.57	1.0	30
269.47	3.1	25
266.77	5.8	20
266.17	1.4	14
266.27	1.3	10
267.17	5.4	20
267.77	4.8	20
267.07	5.5	30

272.57

check to Orig. B.M.

17th d. C.T. & P. on walk
S. Fly Cor. Bangon +
Harbor View dr.

11.47 254.74 254.71

T.P. 1.42 266.19 10.21 264.77

T.P. 4.37 274.98 1.96 270.61

2x2 Hub
744.98

272.57

Levels on Wby end
of Golden Park Ave.
Sketch P. 2

INDEXED

1730

1700

0750

0700 E.C.

T.P. Hub
5405.2
P. 4

2.54

262.92

260.38

W = West

R

10

257.92	257.72	253.72	254.32	254.22	253.52	254.32	257.62
5.0	8.2	9.2	8.6	8.7	9.4	8.6	8.3
24	17.5	15	13		17.5	20	27
257.32	251.62	253.32	253.12	252.32	252.72	253.72	
5.6	11.3	9.6	9.8	10.6	10.7	9.7	
24	17.5	14		17.5	19	27	
256.72	249.82	250.22	250.22	249.52	250.32	252.42	
6.7	13.1	12.7	12.7	13.4	12.6	10.5	
28	21	17.5		17.5	19	30	
256.72	247.12	246.82	246.32	245.32	246.72	250.22	
6.7	15.8	16.1	16.6	17.6	16.7	12.7	
35	22	17.5		17.5	19	28	

262.92

check to orig. T.P. 254 260.38 260.38

Center Curve on R

+03.47 B.C. on R.

1495

+69.71 B.C. on L.

262.92

L

R

R

11

259.04

258.24

39

4.7

Center Curve

258.32

258.04

257.64

256.84

256.64

257.14

257.14

4.6
30

4.9
17.5

5.3

6.1
17.5

6.3
21

5.8
22

5.8
30

258.22

257.52

257.22

256.22

256.82

256.92

4.7

5.4
17.5

5.7

6.7
17.5

6.1
22

6.0
30

9 Curve

257.62

256.12

255.92

255.42

255.72

256.02

255.72

5.3
27

6.2
17.5

7.0

7.5
16

7.2
17.5

6.9
21

7.2
30

262.92

X Sects Golden Park Ave
(Cresta Real Sub)

Hendricks

Hardin

Smith

Worrell

Aug 4, 5, 1947

WO # 25001

INDEXED

WK

NOV 19 1948

Points Marked \bigcirc - Reset 11.5" disc in conc. Pav.
Feb. 1954

T.P.S-835

2-10-54

12

Cresta Real Line

R 78.98

$\Delta 30^{\circ} 26' 20''$

Fd $\frac{3}{4}$ " Pipe

32.87

set Hub

34.51

33.37

6767

348

21.18

175 175

set Hub

54 + 13.17 BC

set Chisel X in walk

R = 372.5

$\Delta = 20^{\circ} 11' 30''$

L = 131.27

T = 66.33

Address not check

set Hub

244 + 4.39 EC

set Chisel X in walk

set RP Hub

Ave

set Hub

4 + 66.27 BC

Cont'd Next Page

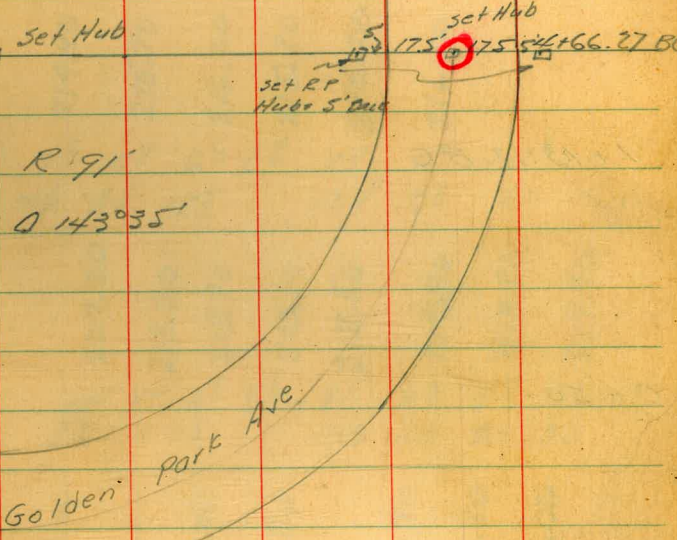
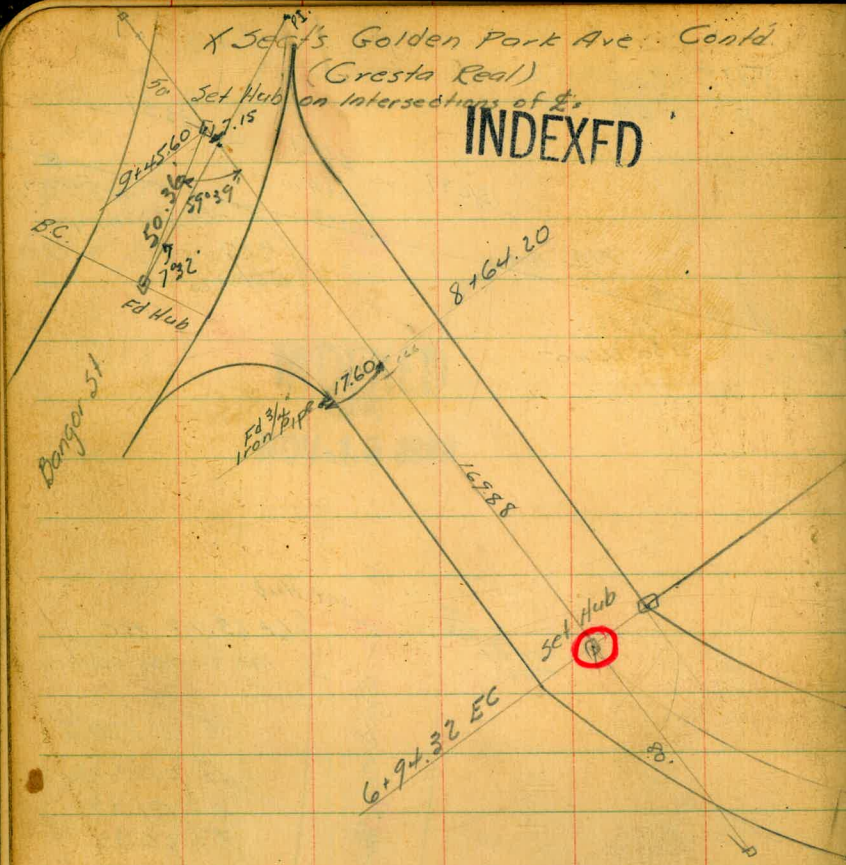
T.P.S. 851 - 2-10-54

X Set's Golden Park Ave. Contd.

(Gresta Real)

Set Hub on Intersections of

INDEXED



X Sects Golden Park Ave

Sta + 41 - Elev B.M.

INDEXED

-1+50

-1+13.12 B.C

0+50

0+00 Taken on Diagonal Sub line

TP. 8.36 222.60 8.54 214.24

TP. 0.77 222.78 11.07 222.01

TP. 0.00 233.08 11.66 233.08

TP. 0.05 244.74 12.48 244.69

B.M. 2.46 257.17 254.71

216.20	217.00	216.50	217.40	217.20	216.40	216.00
4 ⁵⁰	5 ³⁹	6 ³⁶	5 ^{17.5}	5 ^{17.5}	6 ^{17.5}	6 ²⁷
50	39	36	17.5	17.5	27	50

214.80	215.70	216.00	215.70	215.20	216.00
7 ⁸	6 ⁹	6 ⁶	6 ⁹	7 ⁴	6 ⁶
43	25	17.5	17.5	28	50

207.20	213.20	213.70	213.80	213.50	214.30	218.80	219.40
15 ⁴	9 ⁴	8 ⁹	8 ⁸	9 ¹	8 ³	3 ⁸	3 ¹¹
35	20	15	17.5	20	30	35	

203.00	205.20	210.40	210.20	210.40	212.80	216.00
19 ⁶	17 ⁴	12 ²	12 ⁴	12 ²	9 ⁸	6 ¹¹
35	25	10	12.6	19	20	35

Hub

222.60
222.00
209.90

L&T 17' East of 7' Pl on SE Cor Harbor View Dr & Bangor St. FB 1565-14

Sta + HI - Elev BM

4100

TP 1308 23461 107 221.53

3+50

3+00

3+44³⁹ EC.

2+00

22260

218.61
 222.21
 223.11
 223.41
 222.61
 222.71
 229.31¹⁵

16° 12' 11" 11" 12° 11' 0"
 50 40 17⁵ 17⁵ 25 45

On Stake 25' 21' 50' 3+50
 219.4 221.2 221.6 221.8
 30 14 10 10 0
 45 35 22 17⁵ 17⁵ 25 45

219.20
 221.40
 220.60
 220.70
 220.60
 219.60
 220.00

34 13 20 19 20 30 26 17⁸
 50 30 28 17⁵ 17⁵ 25 45

218.80
 218.80
 219.70
 219.20
 218.50
 218.20

38 38 29 34 41 44
 50 37 17⁵ (355) 17⁵ 24 47
 (H40)

217.90
 217.70
 218.50
 218.20
 217.50
 217.10

42 49 41 44 52 55
 50 38 17⁵ 17⁵ 26 45 50
 167 177

Sta + H-1 - Elev

5+50

5+25

5+00

4+66.27 BC.

4+35

234.61

2 ⁵	0 ⁹	1 ¹	1 ⁵	3 ⁰	4 ¹	4 ⁴	+2 ⁶	+3 ¹
45	32	21	17 ⁵	17 ⁵	20	25	40	
228.51	228.91	231.11	230.51	229.41	228.71	228.41	234.61	
6 ¹	5 ¹	3 ⁵	4 ¹	5 ⁰	5 ⁹	6 ²	0 ⁰	+3 ⁵
50	40	24	17 ⁵	17 ⁵	22	30	50	
224.81	228.41	228.61	227.71	227.57	227.01	233.81		
9 ⁸	6 ²	6 ⁰	6 ⁹	7 ¹	7 ⁵	0 ⁸	+2 ⁵	
40	30	17 ⁵	17 ⁵	26	34	50		
220.61	224.01	225.81	226.31	225.31	225.11			
14 ⁰	10 ⁶	8 ⁰⁰	8 ⁰⁰	9 ⁰⁰	9 ⁵	+1 ⁰		
40	30	17 ⁵	8 ⁵⁰ Hab	17 ⁵	25	45		
217.21	221.41	223.21	224.91	225.91	223.91	223.91		
17 ⁴	13 ²	11 ⁴	9 ⁷	9 ⁶	10 ⁷	10 ⁷	+1 ⁰⁰	
50	40	30	17 ⁵	17 ⁵	25	45		

Sta + H.1 - Elev

6+75

6+50

6+25

6+00

TP. 1315 247.76 0⁰⁰ 234.61

5+75

234.61

246.86
246.06
244.06
243.26
245.86

+10° +8° 0° 11 31 4 19 +17 +07
50 40 23 17 16 18 26 45

244.26
241.96
240.56
243.76
247.76
246.86

+6° +4° 3° 5.8 7.2 4° 0° 0°
50 35 17 17 18 27 40

241.56
239.66
237.86
245.36
245.66

+16° +11° 6° 8° 9° 2° 2°
50 24 17 17 17 27 40

242.76
242.06
238.76
237.16
235.76
241.36
241.36

50 52 9° 10° 12° 64 64
40 26 17 17 17 25 40

235.71
234.41
233.21

+18° +21° +11° 0° 14 14.5 +5°
50 35 17 17 25 40

Sta + H-1 - Eley

£

BM 2.91 26043 26038

9+45.60 £ Golden Gate & Bangor

263.24

£ Hub Sta 5105 2 Bangor St. See P7 this Book

17	261.64	37	259.94	37	259.74	37	259.54	37	259.04
35		175		175		175		35	

X-Section of Prop. 80' Row of Wabaska
 Dr. - Sections taken by Plus or Minus
 Rods from \pm elev.

Sections are on Radial Lines on Curve

Rods on 8" Water pipe - exposed - on 2 - conc.
 Piers - see sketch Pro for Loc.

INDEXED

48.8
 +9.7
 101

1+25

1+00

0+50

0+00 = P.C.

54.5 48.53 2.31 43.08

9.68 45.39 0.05 35.71

B.M. 6.69 35.76 29.07

25.30

cur. - 3.77

S.W. B.P.
 Lowell
 Evergreen

H = F

#

Rt = W

33.94

10.82

Top pipe at Nly.
 Pier

34.38

10.38

Top of pipe at Sly.
 Pier

34.0	34.8	32.1	29.4	38.8	39.6	38.8	39.6	39.1	38.8	50.3	54.9	63.1	74.4
-0.1	-4.3	-7.0	-9.7	-0.3	+0.5	-0.3	0.1	+0.0	-0.3	+1.7	+15.8	+24.0	+35.3
70	50	46	37	20	10	6	57	16	26	40	62	100	

52.5	38.1	31.8	30.6	30.6	39.2	39.9	39.1	39.48	39.5	39.2	51.1	53.9	64.5	76.3
+13.0	-1.4	-7.7	-8.9	-8.9	-0.3	+0.4	+0.4	5.7	+0.0	-0.3	+11.6	+14.4	+25.0	+35.8
105	4	60	43	34	22	10	15	57	16	30	38	51	102	

52.5	37.7	33.7	31.0	40.4	40.3	40.53	40.6	40.1	48.0	52.3	67.7	76.0
+12.0	-2.8	-6.8	-9.5	-0.1	-0.2	1.4	+0.1	-0.4	+1.0	+1.8	+2.2	+3.5
104	50	43	29	17	4	17.4	7	17	28.5	40	73	100

53.9	44.9	37.8	33.7	32.0	41.6	41.4	41.51	41.5	41.1	51.3	56.7	71.0	74.0
+12.4	+3.4	-3.7	-7.8	-9.5	+0.1	-0.1	3.5	+0.0	-0.4	+9.8	+15.2	+29.5	+31.5
101	75	40	32	21	10	4	35	7	17	28.5	40	73	100

Old Lay

48.53

44.76

-3.77

T.P. 3.50 44.55 748 41.05 ^{on Hub} at # E.C.

3+33 -47.5 Rt. = ± P. pole # P 3287 26.0 34.2 332
 3+29.67 = E.C. 36.9 337
 -0.4 -3.6 -11.3 -3.1 -4.1
 118 79 60 50 47
 edge

3+00 -0.7 37.7 32.0 29.3 27.2 28.9 36.1
 106 67 62 57 50 40

2+89 -24.6 Rt. = ± Guy Pole # 89760 H
 2+50 433 369 333 284 292
 +7.7 +1.3 -2.3 -1.2 -6.4
 105 90 71 66 50

1+25 -20.3 Rt. = ± P. pole # 301400 H
 2+00 44.1 34.6 30.7 29.0
 +6.7 -2.8 -6.7 -8.4
 105 67 60 40

1+50 46.5 37.6 34.8 29.6 34.5
 +8.0 -0.9 -3.7 -8.9 -4.0
 102 69 53 47 34
 Top of
 8" Water pipe
 on Rad. Line

Lt. # Rt.
 40.78
 44.55

33.9 33.9 31.7 34.3 37.28 42.1 47.5 54.1 58.8
 34 -24 -5.6 -3.0 7.48 +1.8 +10.2 +16.8 +21.5
 36 25 16 11 17 40 78 116
 edge

34.5 34.7 34.4 34.4 38.4 44.7 49.3 60.0
 -3.9 -3.7 -4.0 -4.0 6.4 +6.3 +10.9 +21.6
 37 26 16 13 64 22 42 100
 edge

36.2 36.8 35.5 35.9 35.7 35.6 42.7 52.4 63.2 63.0
 +0.6 +1.2 -0.1 +0.3 +0.1 9 40 76 100
 40 25 23 13 3
 edge

36.9 37.8 36.7 37.42 37.2 37.4 50.0 55.4 66.1 75.0
 -0.8 +0.4 -0.7 1.3 -0.2 0.0 +12.6 +18.0 +28.7 +37.6
 36 20 14 13 6 10 23 40 78 108
 edge

30.5 38.5 38.8 38.1 38.4 38.6 51.3 56.3 67.5 73.5
 -8.0 0.0 +0.3 -0.4 6.2 8 -0.1 +0.1 +12.8 +17.8 +29.0 +35.0
 32 25 10 8 14 17 27 41 75 104
 edge
 44.76
 48.53

check Starting B.M. 6.62 29.08 29.07

T.P. -0.03 35.70 8.82 35.73

5+00 28.0
-0.9
100

4+50 30.8
+0.9 30.9
100 83
edge

4+00 31.6 27.2 24.7 32.4 31.4 32.1
-0.8 -5.2 -7.7 0.0 -1.0 -0.3
110 100 90 80 77 65
edge +

3+50 34.1 33.8 27.9 25.7 33.5 32.5
-1.6 -1.9 -7.8 -10.0 -2.2 -3.2
100 90 82 69 59 55
edge

3+49.5 - 6.13 Lt. = outlet of 18" Culvert

3+42.5 - 1.2 Lt. = Sewer 5.57 on rim

3+38.4 - 12.7 Lt. = inlet of 18" Corr. Iron Culvert

Lt.

#

Rt.

28.1 27.9 28.1 28.9 30.3 33.4 35.5 37.0
-0.8 -1.0 -0.8 1.9 +1.4 +4.5 +5.6 +8.1
67.8 40 20 119 20 40 56 104

along House
29.7 29.8 29.2 29.9 32.8 36.2 41.7 49.8
-0.7 -0.1 -0.7 0.9 +2.9 +6.3 +11.8 +19.9
75 40 20 102 20 40 84 102

32.4 31.6 31.3 31.3 32.4 37.0 41.0 45.4 49.6
0.0 -0.8 -1.1 -1.1 8.4 +4.6 +8.6 +13.0 +17.2
52 46 40 20 20 40 61 103
edge

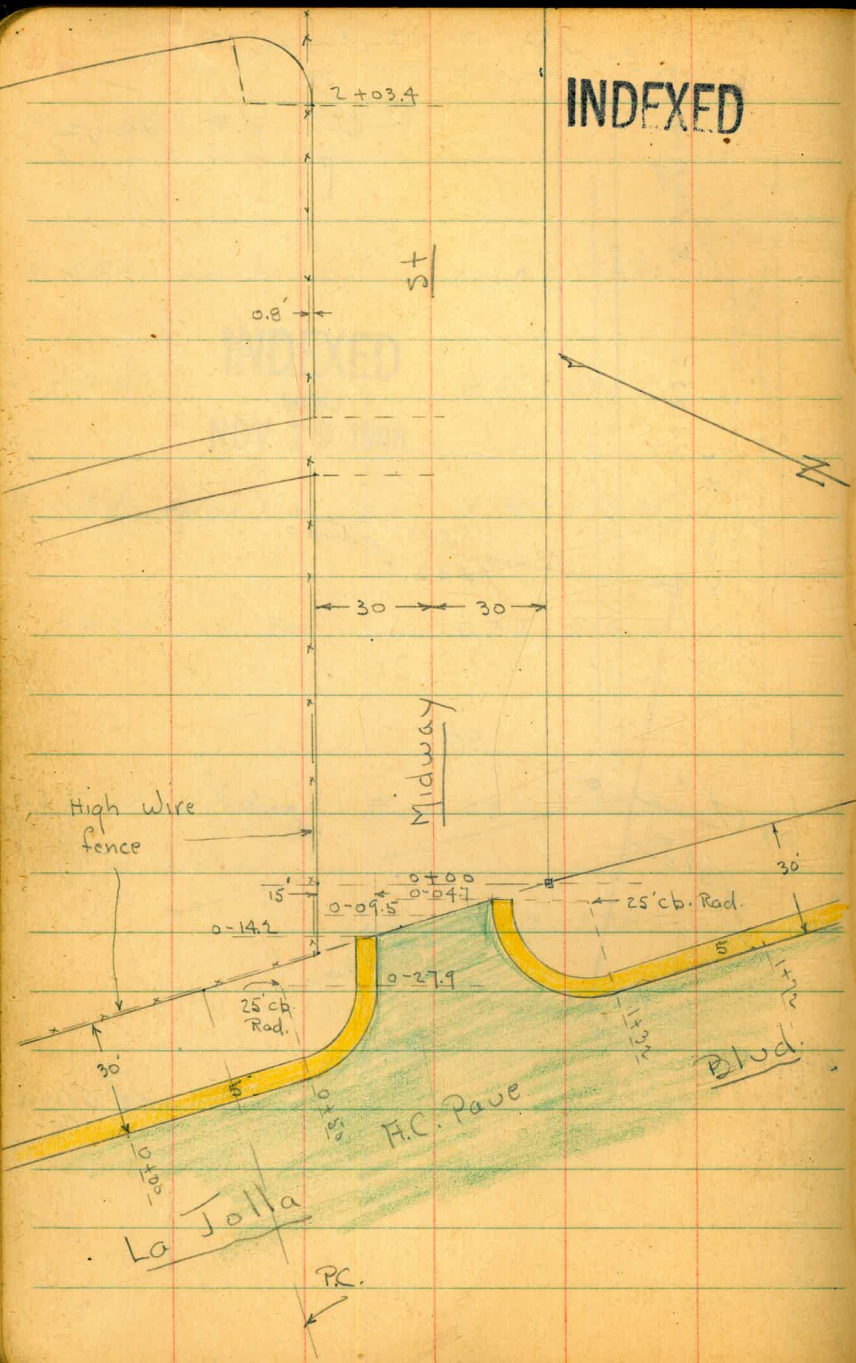
33.5 33.6 33.1 34.2 35.7 42.5 46.4 51.1 55.0
-2.2 -2.1 -2.6 -1.5 0.1 +5.8 +10.7 +15.4 +19.3
43 31 25 13 5 24 41 70 99
edge

11.29/12
11.66
61.3
flowline
outlet.

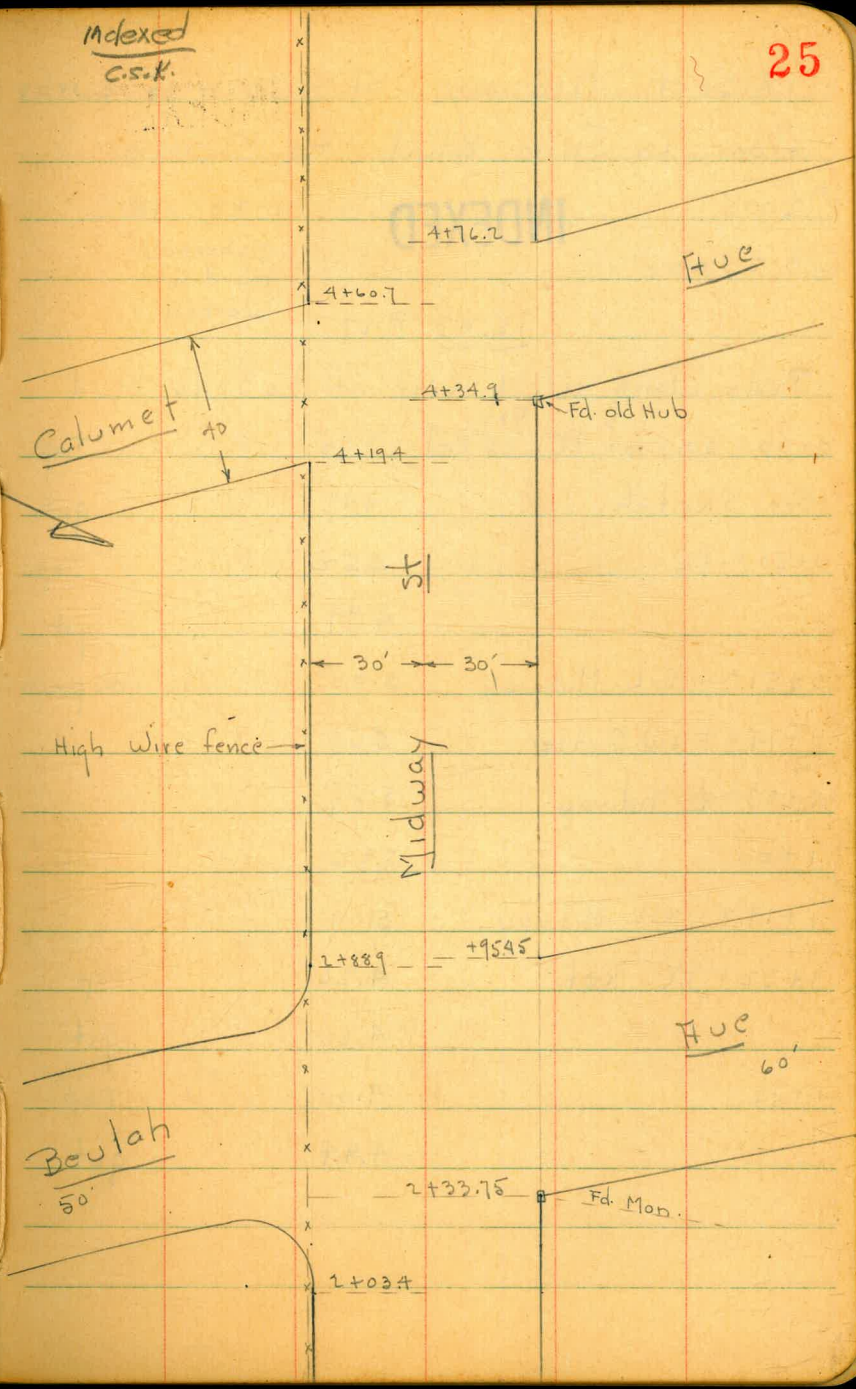
30.46
10.32
22.7
Flow line inlet.

44.55 / 40.18

INDEXED



Indexed
C.S.K.



X-Sept. Midway St. - 60' - 15' curbs
from La Jolla Blvd. to Ocean.

2005

INDEXED

1-23-48

W.O. 25001

Osborne
Hardin
Worrell

75.43 P. 27

Rods along w. cb. line of La Jolla Blvd.

0+00 = 50' S. of P.C. Ret. 25' Rad	3.95		Top
See Sketch.	4.49		gut.
0+50 = P.C.	4.52		Top
	4.99		gut.
0+51.3 = S.L. Midway	5.05		on pave
0+74 = E & W Gutter.	5.69		
0+83 = ϕ Midway	5.59		
1+00	5.26		
1+14.8 = N.L. Midway	5.09		
1+32 = P.C. Ret	4.26		Top
	4.66		gut
1+72	4.00		Top
	4.44		gut.

X-Sect Midway

INDEXED

Rods around Returns - 25 Rad.

N.W. Ret - 44' ground - 5 Parts - 88' Each

Req. - N. end = P.C.	75.43	4.26	T = Top
		4.66	q = gut
6.8.5		4.60	T
		5.05	q
"		5.10	T
		5.52	q
"		5.61	T
		6.07	q
"		6.21	T
		6.61	q
8.8 = end = w.L. LaTolla Blvd		6.83	T
		7.35	q

B.M. 3.63 75.43

71.80

S.E. B.P.
Midway +
LaTolla Blvd.

5 parts

S.W. Ret. - 44.6' ground - 89' Each

Req. N. end = w.L. LaTolla Blvd	7.15	T
	7.65	q
8.9.5	6.35	T
	6.92	q
"	5.67	T
	6.27	q
"	5.10	T
	5.65	q
"	4.77	T
	5.33	q
8.9 = P.C. - 25 Rad.	4.52	T
	4.99	q

Reg. Midway Sections -

INDEXED

0+50
 0+25
 0+00 = N.W. Prop Cor.
 0-04 = 16.8 Lt. = \pm Guy Pole
 0-04.7 = end of cb on Rt.
 0-09.5 = Edge of Pave on \pm
 0-14.2 = End of cb on Lt.
 0-18.2 = S.W. Prop Cor. 7.4
 0-18.2 = 30.7 Lt. Beg Wire fence
 0-27.9 = opp. P.C. 25' Ret on Lt.

Station	63.1	63.2	63.7	64.3	64.1	58.9	58.2	63.8	64.3	65.3
12.3	12.2	11.7	11.1	11.3	11.5	17.2	11.6	11.1	10.1	
40	30	15	3	5	15	18	30	40		
65.0	65.4	65.1	65.6	61.7	59.7	61.4	65.9	66.5	67.1	
10.4	10.0	10.3	9.8	13.7	15.7	14.0	9.5	8.9	8.3	
40	30	15	10	8	15.7	14	15	30	40	
66.4	66.9	66.0	67.6			64.1	68.5	68.5	68.9	
9.0	9.5	7.4	7.8			11.3	6.9	6.9	6.5	
40	30	15	7.8			11	15	30	40	
66.5	66.9	68.3	68.2	68.08		68.60	68.82	69.0	69.5	
8.9	8.5	7.1	7.2	7.35	7.35	6.83	6.61	6.4	6.9	
40	30	15	7.2	15	15	15	20	30	40	
				9.4	9.4	Top of cb	For walk			
67.0	67.4	67.6	67.79	68.44		68.46	68.85	69.7		
8.4	8.0	6.8	7.64	6.99		6.97	6.48	5.7		
40	30	15	edge Pave	15		16.2	16.2	30		
67.8	68.31	68.28	67.78	68.18		68.88	69.30	70.2		
7.6	7.12	7.15	7.65	7.25		6.55	6.13	5.2		
30	20	15	15	15		17.8	17.8	20		
	Back for. Walk	Top end of cb.	9.4			9.4	Top			
69.9	69.89	68.89	69.18			69.67	70.08			
5.5	5.95	6.54	6.25			5.76	5.35			
30	15	15	6.25			15	30 = N.L. on Pave			
	Top P.C. Ret	9.4								
			75.43							

It = S

Rt = N

28
28

2+889 = P.C. Prop- Beulah to S.

1+50

2+33.75 = N.E. Cor. Beulah St

2+03.4 = opp. P.C. Prop on Lt.

1+80

1+50

1+00

T.P. 0.88 63.38 12.93 62.50

48.7
40 14.7
48.6
30 14.8
48.6
20 14.8
43.5
18 19.9
43.9
9 19.5
49.2
8 14.2
49.5
13.9
51.6
15 11.8

50.6
12.4
40 40
50.5
12.9
30 30
45.8
17.6
25 25
45.8
17.6
15 15
50.9
12.5
13 13
51.1
12.3

51.8
11.6
40 40
51.7
11.7
30 30
49.3
14.1
25 25
48.0
15.4
15 15
51.4
12.0
14 14
51.9
11.5
51
53.4
10.0
15 15

53.2
10.2
40 40
53.1
10.3
30 30
49.0
14.4
25 25
50.3
13.1
15 15
53.0
10.4
14 14
53.4
10.0
53.6
8.8
15 15

54.8
8.6
40 40
54.6
8.8
30 30
54.1
9.3
22 22
51.1
12.3
20 20
51.2
12.2
15 15
50.3
13.1
7 7
54.6
8.8
6 6
54.7
8.7

57.0
6.4
40 40
56.8
6.6
30 30
56.6
6.8
25 25
54.3
9.1
23 23
52.1
11.3
15 15
54.7
11.7
15 15
56.6
6.8
14 14
56.8
6.6

60.0
3.4
40 40
59.9
3.5
30 30
60.1
3.3
15 15
56.6
6.8
12 12
54.0
9.4
54.3
9.1
4 4
60.4
3.0
5 5
60.9
2.5
15 15

52.4
11.0
30 30
53.9
9.5
30 30
53.6
9.8
30 30
53.9
9.5
30 30
53.6
9.3
40 40
55.1
3.5
80 80

53.0
10.4
15 15
53.6
9.8
30 30
55.1
4.3
40 40

53.9
9.5
30 30
53.4
10.0
15 15
53.9
9.5
30 30
55.1
9.3
40 40
59.9
3.5
80 80

54.7
8.7
30 30
55.4
8.0
40 40
54.7
8.7
30 30
55.4
8.0
40 40

55.5
7.9
15 15
56.1
7.3
30 30
57.0
6.4
40 40

57.8
5.6
15 15
58.8
4.6
30 30
57.8
5.6
15 15
58.8
4.6
30 30

61.3
2.1
30 30
61.3
2.1
40 40

63.38
75.43

4+60.7 = SW. Cor.

T.P. 0.53 41.94 13.00 41.41

4+34.9 = N.E. Cor.

4+194 = S.E. Cor. Calumet.

4+00 - 30.8 Lt. = Wire fence

3+50

2+98.45 = N.W. Cor. Beulah

T.P. 0.43 54.41 9.40 53.98

on Hub.
N.E. Cor
Calumet

Man - N.E. Cor
Beulah
High Cor.

2.0	2.0	1.9	1.9	4.2		2.0	2.0	2.4	2.4
10	30	15	19	7		5	5	30	40
39.0	39.0	40.0	40.0	33.7		39.9	39.9	39.5	39.5
									30

41.2	41.2	41.2	38.8	33.0	41.94	41.3	41.3	41.6	
13.2	13.2	13.2	15.6	21.4	12.8	13.1	13.1	12.8	
40	30	15	13		5	15	30	40	

42.2	42.3	42.1	42.1	39.2	33.8	42.4	42.4	42.1	40.4	42.2	42.6	46.2
12.2	12.1	12.3	12.3	15.2	26.4	12.0	12.9	12.3	14.0	12.2	11.9	8.2
40	30	15	12	11		4	15	20	15	30	40	60

42.3	43.3	43.3	36.2	37.8	43.3	43.4	41.4	43.3	43.7			
11.1	11.1	11.1	18.2	16.6	11.1	11.0	13.0	11.1	10.7			
40	30	5	13	1		15	22	30	40			

45.7	45.7	45.6	39.9	39.8	41.7	46.0	45.9	45.5	47.0	48.9		
8.7	8.7	8.8	14.5	14.6	12.7	8.4	8.5	8.9	7.4	5.5		
40	30	24	22	15	10	9		5	30	40		

48.5	48.5	48.5	43.2	43.2	43.9	49.0	49.4	51.5	52.2	53.9	57.8	
5.9	5.9	5.9	11.2	11.2	10.5	5.4	5.0	2.9	2.2	0.5	+3.4	
40	30	20	17	15	10	9	5.0	16	20	40	60	

54.41

63.38

Bangor St, X-Sec.
Jennings to Harbor View Dr.

7-2-48 INDEXED
W.O.# 31568

Sommermayor
M^e Coy
Melton
Duncan

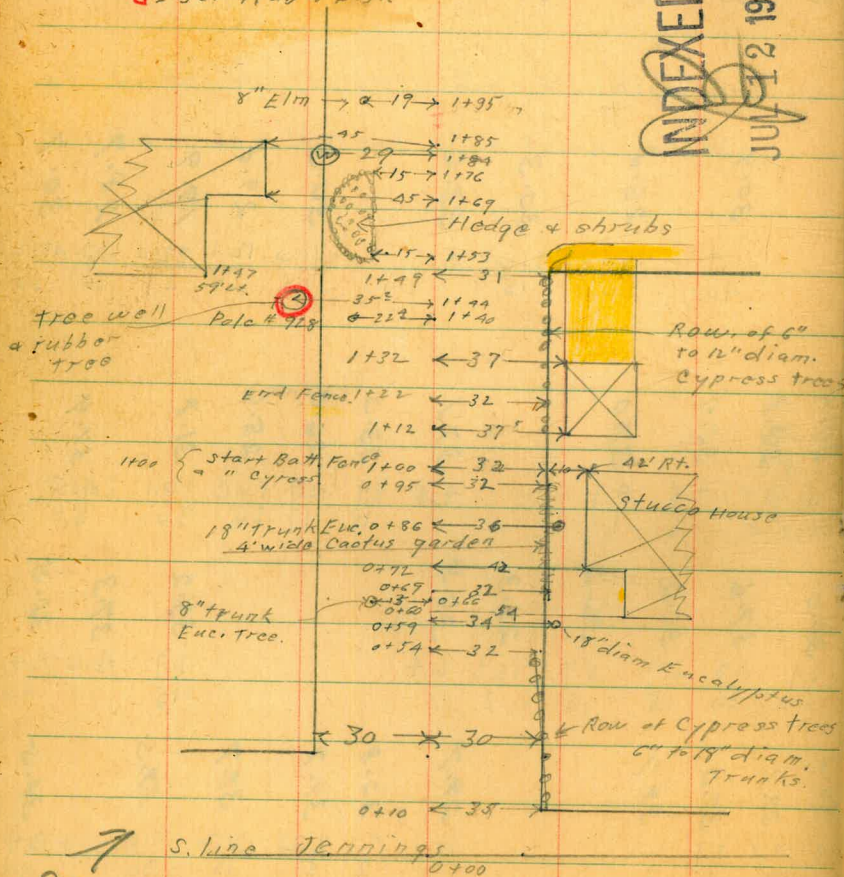
□ = Fd Hub & Tack.

• = Fd. L & T.

⊙ = Water meter box

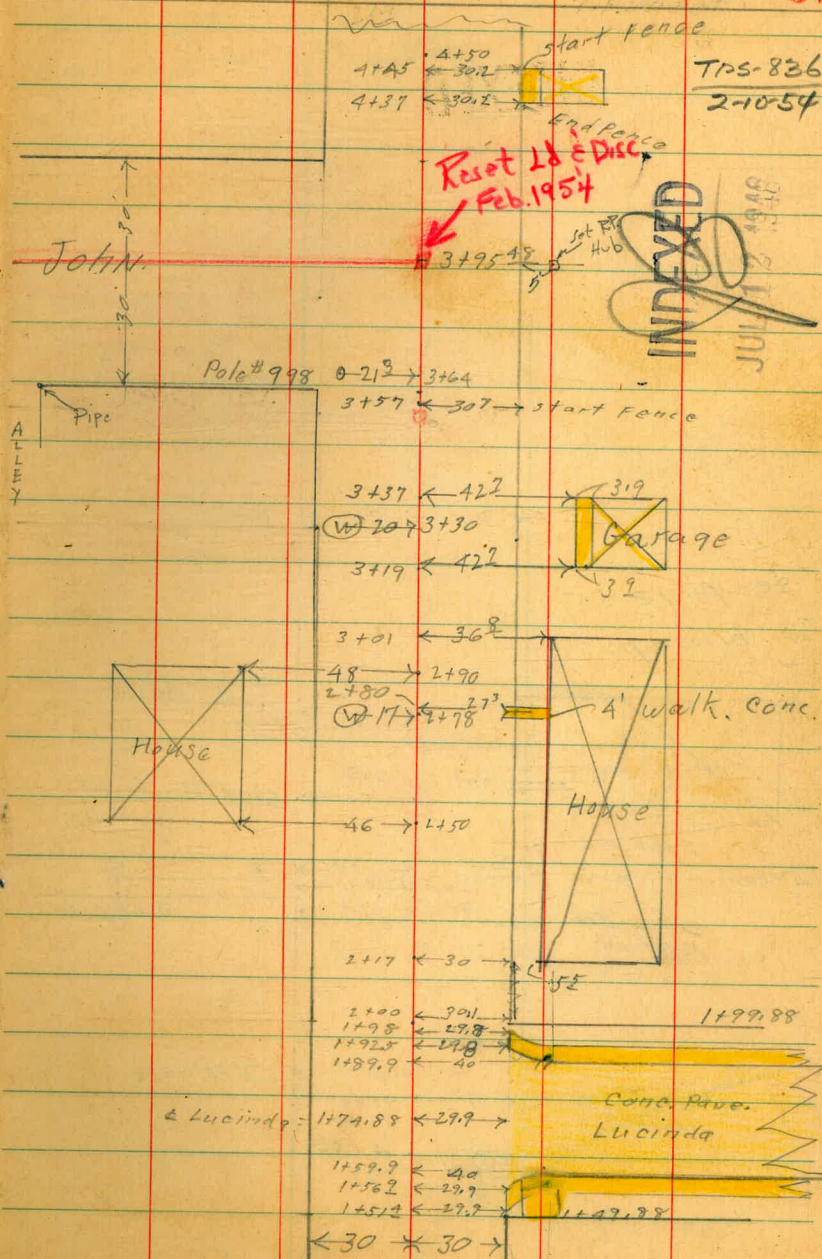
⊠ = Set Hub & Disk

INDEXED
JUL 12 1948



See page 77
6/11/53

Also John St. Bangor to 300' west ³²



Rim of Canyon \nearrow

\square - 3+12 Post 1/2 Dist

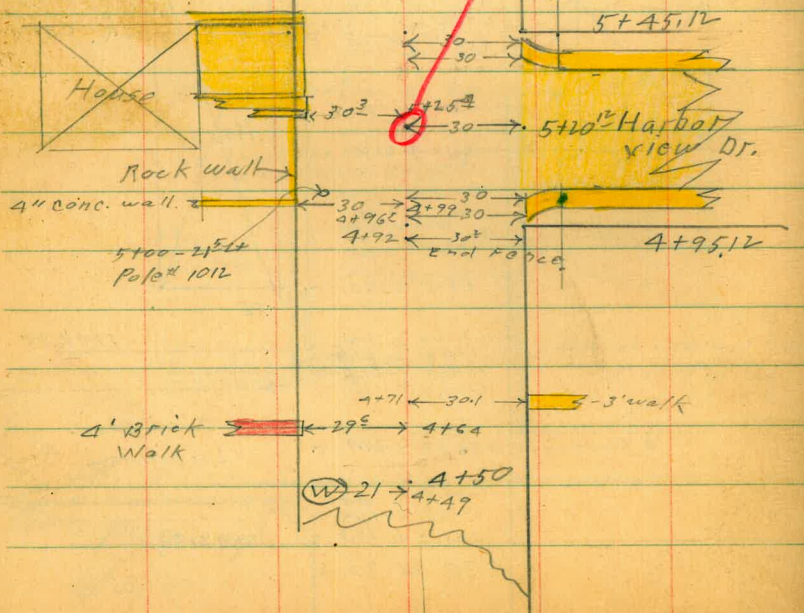
4 chisel crosses on MH & both sts.

Levels Page 45

Banqor

$\leftarrow 30 \times 30 \rightarrow$

see page 35 for blow up.



John St.

$\leftarrow 30 \times 30 \rightarrow$ 1+24 Post 1/2 Dist

0+80 $\leftarrow 29^5 \rightarrow$
0+74 $\leftarrow 29^5 \rightarrow$

30
 \uparrow
 \downarrow

0+00
Rock w/ Disc
 Φ Banqor

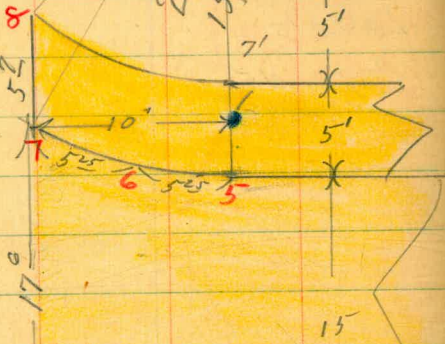
S.E. + N.E. Returns
Lucinda + Bangor

INDEXED

5.74	5.18	5.82
7	7	8
Cl.	G	walk

5.39	5.85	5.58	5.75
5	5	6	6
Cl	G	Cl	G

274.80
↑



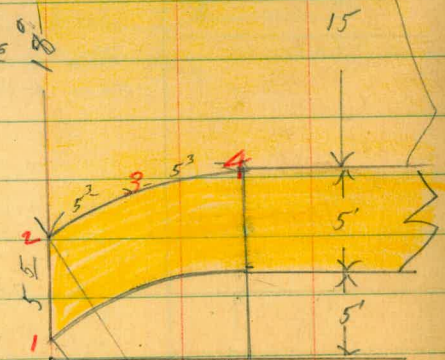
Conc. Pave

Σ = 174.88

Lucinda

5.24	5.68	5.20	5.66
3	3	4	4
Cl	G	Cl	G

5.24	5.34	5.83
1	2	2
walk	Cl.	G.



Σ 274.80
From P. 37
RCD

S.E. + N.E. Returns
Harbor View Dr
+ Bangor

INDEXED
JUL 19 1948

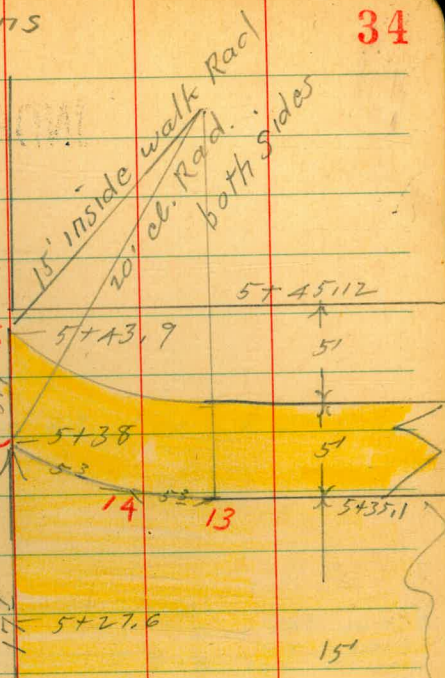
12.56	13.00	12.43
15	15	16
Cl	G	walk

12.83	13.38	12.69	13.11
13	13	14	14
Cl	G	Cl	G

11.62	12.24	11.85	12.32
11	11	12	12
Cl	G	Cl	G

11.19	11.38	11.88
9	10	10
walk	Cl	G

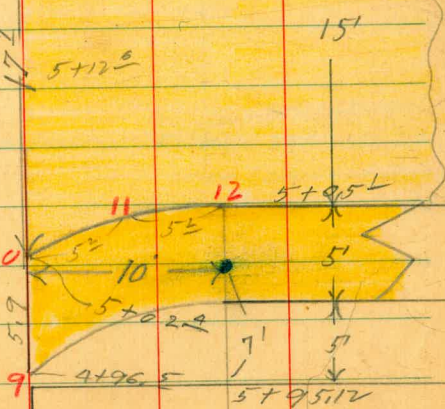
Σ = 266.53
From
page. A1



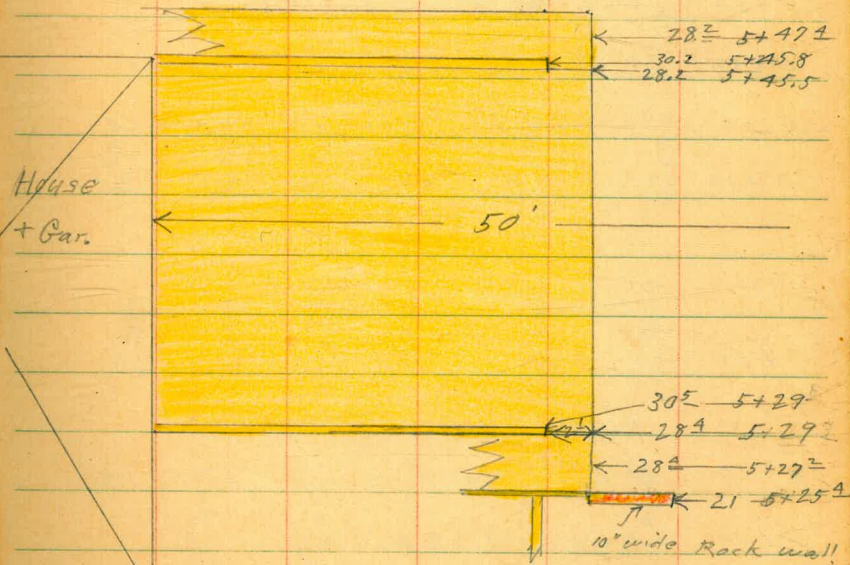
Conc. Pave.

Σ = 5+20.12

Harbor View Dr.



See page 33 for location



Bangor Street Levels
Sketch pages 32 to 35

1+32 37' Rt. = N.W. Cor. Gar. - North Front
1+22 32' Rt. = End Fence
1+12 37' Rt. = S.W. Cor. Gar. - North Front

INDEXED

1+00 42' Rt. = Cor. House.
31' Rt. = start row of 30' High Cypress
32' Rt. = start lattice fence

0+95 32' Rt. = End cactus bed

0+86 36' Rt. = 18" diam Eucalyptus
54' Rt. = Δ in house

0+72 42' Rt. = Cor. House

0+69 32' Rt. = ⊥ - start 4' wide cactus bed
50' Rt. = conc. steps to house

0+66 13' Lt. = 8" diam. Eucalyptus

0+59 34' Rt. = 18" diam. Eucalyptus

0+54 32' Rt. = End row of cypress

0+50

0+20

Diam. Cypress trees

0+10 35' Rt. = start row of 6" to 18"

0+00 = s. line Jennings.

N.E. 10' dia'
Backen v. 7' dia'
Lucinda +
Bangor
G. 230
P. 19

5.73 275.21 — 269.48

270.0
 $\frac{5.2}{30}$

270.2
 $\frac{5.0}{15}$

270.2
5.0

270.0
 $\frac{5.2}{20}$

270.9
 $\frac{4.3}{30}$

271.6
 $\frac{3.6}{42}$
At House

271.46
 $\frac{3.75}{50}$
Bottom of steps

273.1
 $\frac{2.1}{54}$
doorway floor level

$\frac{3.2714}{30}$

$\frac{3.2714}{20}$

$\frac{4.1}{10}$

271.0
4.2

270.5
 $\frac{4.7}{24}$

271.2
 $\frac{1.0}{30}$

$\frac{3.2717}{30}$

$\frac{3.2718}{20}$

$\frac{3.2718}{4}$

271.6
3.6

270.6
 $\frac{4.6}{24}$

272.0
 $\frac{3.2}{30}$

272.2
 $\frac{3.0}{30}$

272.1
 $\frac{3.1}{10}$

271.0
4.2

270.3
 $\frac{4.7}{21}$

271.9
 $\frac{3.3}{30}$

275.21

INDEXED

1+69 59' Lt. = Δ in house
45' Lt. = Cor. of house

1+59⁹ Cont.

1+59² Sly. cl. line Lucinda

see page 34

For detail of ob. returns

T.P. 4.57 274.10 4.98 270.23

1+53 15' Lt. = start semi circle hedge

1+49⁸⁸ = S. line Lucinda

1+49 31 Rt. = End 30' high Cypress hedge

1+47. 59' Lt. = S.E. Cor. House

brick tree well.

1+44 35² Lt. = ctr. 10' diam. Round.

1+40 22^A Lt. = Pole # 928

275.21

INDEXED
271.3
3.5
45
Floor 1
level

270.7
4.1
45
10rd

268.94	268.84	268.28	267.59	266.87
57.86	5.96	6.57	7.41	7.73
65	80	90	100	100
Q	66	Q	66	Q

269.06	269.60	269.14	269.38
5.74	5.20	5.66	5.42
293	70	70	65
Edge.	66.	Q.	66
par.	50.		

274.80

270.1	270.0	269.8	269.9	269.4	270.5
5.1	5.2	5.4	5.3	5.8	4.7
50	30	15		24	30

275.21

3+65⁴⁸ = S. Line John to west.3+64 21³Lt. = Pole # 9983+57 30⁷Rt. = start fence (Picket)

T.P. 1/2					B.M. #1
£ Bangor +	2.44	<u>266.53</u>	7.26	264.09	5 ⁷² 3+95.08
£ John					

3+47⁴ £ = £ Alley to east3+37 42²Rt. = End Conc. Apron to double Gar.3+19 42²Rt. = Start Conc. Apron to double Gar.3+16 30⁵Rt. = End lattice fence

3+00

covered lattice fence.

2+82 30 Rt. = Start 8' high, wire

271.35

265.5	265.6	265.6	266.0	266.1
1.0	0.9	0.9	0.5	0.4
30	15		15	30

266.53

266.3	266.4	266.6	266.9	266.8	266.6	265.1
5.1	5.0	4.8	4.5	4.6	4.8	6.3
30	10		24	30	50	90

266.4	266.8	267.3	267.4	267.2	267.4	268.05	268.24
5.0	4.6	4.1	4.0	4.2	4.0	3.30	3.11
30	15		15	26	30	Apron	Gar Floor

3.21
42.7
Apron3.07
16.6
Gar. Floor

267.4	267.4	268.6	268.8	268.9	268.4	268.7
4.0	4.0	2.8	2.6	2.5	3.0	2.7
45	30	12		15	26	30

271.35

Bangor INDEXED

4+92 30² Rt. = End picket fence.

4+71 30¹ Rt. = £ 3' wide Conc. walk

4+64 29⁶ Lt. = £ 4' wide brick walk

4+49 21' Lt. = (W)

Also = start picket fence.
4+45 30² Rt. = End Conc. Apron to Sing. Bar.

Also = start Conc. Apron to Sing. Bar.
4+37 30² Rt. = End picket fence

4+25⁴⁸ = N. line John.

3+95⁴⁸ = £ John

266.53

261.39	261.55	261.3	260.2	260.3	260.1	260.62	260.81
5.14	5.18	5.2	6.3	6.2	6.4	5.91	5.72
40	29 ⁶	29 ²	18		12	30 ¹	40
871 walk	walk					£ walk	on walk
262.31	262.38						
4.22	4.15						
30 ²	34.2						
Apron	Bar. Floor						
262.33	262.45						
4.20	4.10						
30 ²	34.2						
Apron	Bar. Floor						
262.5	262.5						
4.0	4.0						
30	15						
262.44	264.5						
2.1	2.0						
30	15						
264.4	264.4						
2.1	2.1						
30	15						
264.3	264.3						
2.2	3.2						
15	30						
264.8	264.8						
1.7	1.7						
30	30						
<u>266.53</u>	<u>266.53</u>						

Bangor

INDEXED

T.P. 1.50 259.03 9.00 257.53

4+99² 30' Lt. = start 8" wide rock & Conc. wall

4+99 Cont.

4+99 30' Lt. = 5" wide E.+W. Conc. wall
Have same elevation
top of wall + ground to south

For curb returns see Page 34

4+96³ 30' Rt. = S.W. conc. walk.4+95^{1/2} = S. Lima. H.V. Drive

4+93

266.53

258.1	258.2	258.1	259.0	257.8	257.9	258.9	256.5	255.2
7.4	7.3	8.1	7.5	8.7	8.6	9.6	10.0	11.3
40	30	30	30	15		15	28	30
Grd	top wall	Base wall	Grd.					

258.9	260.0
6.6	6.5
40	31
top wall + Grd	top wall + Grd.

259.86	259.0	259.5	257.8	257.9	256.9	256.5	255.2
6.5	7.5	7.0	8.7	8.6	9.6	10.0	11.3
30	30	30	15		15	28	30
top wall	Base wall						

260.6	261.0	258.0	258.2	257.9	257.6	256.5	255.1
5.9	6.5	8.5	8.3	8.6	8.9	10.0	11.4
40	30	15		10	26	30	40

260.6	260.2	258.5	258.5	258.1	258.1	259.5	259.6
5.9	6.3	8.0	8.0	8.4	8.4	7.0	6.9
40	30	15	266.53	10	22	30	40

41

Bangor

INDEXED

S.E. Lt.
10' tieback on
S. 7' lineFB 1565
14

4.31 254.72 (254.71)

6+50

6+00

6+57

5+48^E 29' Lt. = 3' wide E. & W. hedge5+47^E 28^E Lt. = 2^E wide Conc. walk,

double car.

5+45^E 28^E Lt. = End Conc. ramp to

259.03

44

	244.1		248.4		242.8
	14.9		15.6		16.2
	30				30

	246.8		247.3		246.7		245.6		245.3
	12.2		12.2		11.7		12.3		13.4
	60		30		20		30		60

	251.1		252.3		253.2		253.0		253.3		253.0		251.5
	7.9		6.7		5.8		6.0		5.7		6.0		7.5
	60		30		25		25		25		30		60

	253.8		254.1		253.8		253.8		253.5		252.8
	5.2		4.9		5.1		5.2		5.5		6.2
	50		30				25		30		50

	254.05		254.32		254.30
	4.78		4.71		4.73
	50		30		28.2
					Rods on walk

	251.33		254.44		254.38
	7.70		4.59		4.65
	50		30.2		28.2
					Ramp

259.03

019 B.M. #1
P. 39445

INDEXED

3.52 264.09 ✓

T.P. 12.63 267.61 0.73 254.98

3700

2765

2720

T.P. 0.73 255.71 12.46 254.98

1770

29th Mt. = End board fence
1725[±] = 2 1/2 P.O.T.

1708

267.44

12.6
05 243.1

10.6
56 245.1

12.6
30 243.1

15.2 240.5

14.1
30 241.6

21.8
60 233.9

with
Hornel
level

8.1
60 247.6

9.6
30 246.1

11.7 244.0

13.2
30 242.5

14.6
60 241.1

6.1
60 249.6

6.3
30 249.4

6.7 249.0

8.4
30 247.3

8.4
60 247.3

255.71

13.5
3 253.9

13.7 253.7

13.9
30 253.5

6.5
60 240.9

7.2
30 240.2

8.0 259.4

9.3
30 258.1

10.0
60 257.4

5.6
30 261.8

6.7 260.7

7.7
15 259.7

8.4
22 259.0

8.4
30 259.0

267.44

11-18-48
Hendricks
Bramby
Greer
Korer
#0-31605

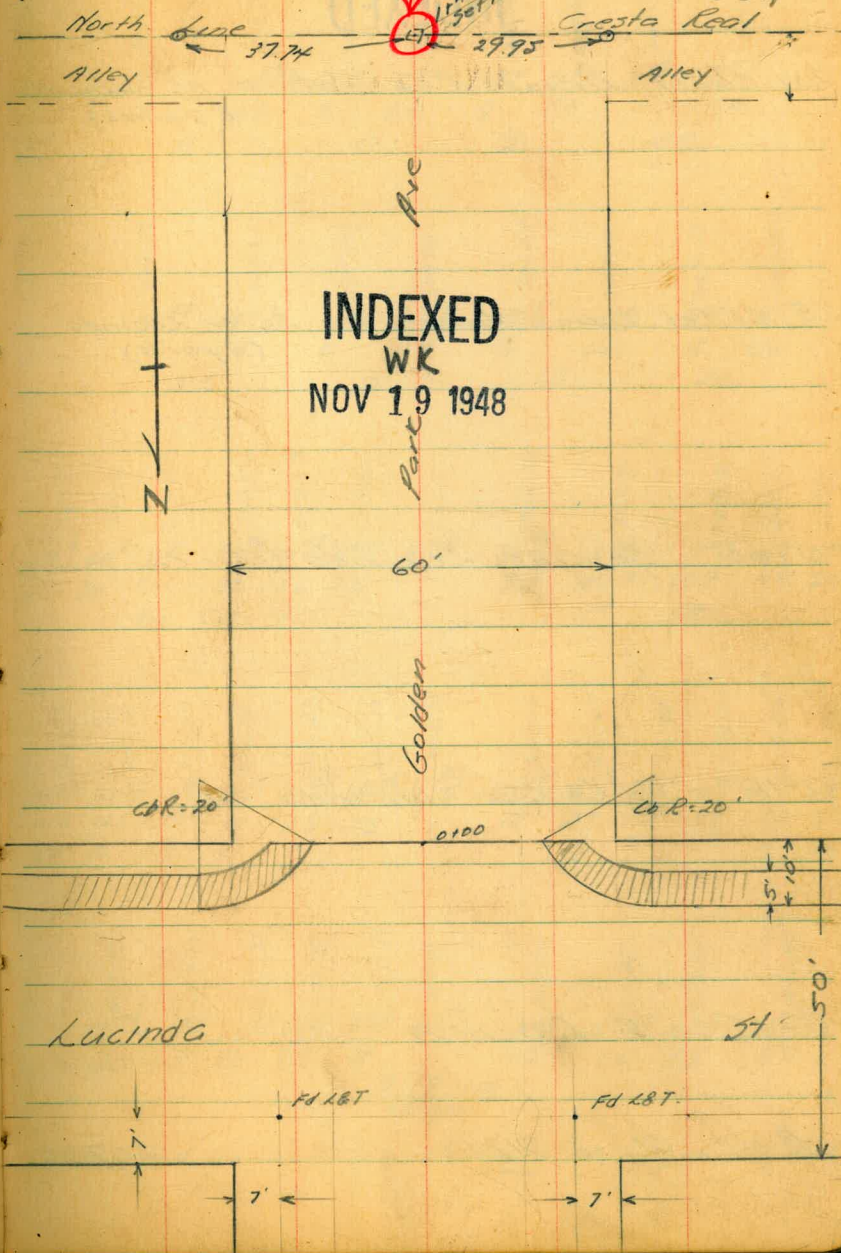
X Sect. Golden Park Ave
Soline Lucinda to
North line Cresta Real Sub.

INDEXED

Reset 2d E Disc
Feb 1954

47

IPS 835
2-10-54



Levels Golden Park Ave.
Lucinda to No. Line Cresta Real

INDEXED

SW Cb Ret Lucinda & Golden Park BC on Lucinda
(3 parts)

SE Cb Ret Lucinda & Golden Park BC on Lucinda
(3 parts)

0+00 30 Line Lucinda (Edge Conc Paving)

0-10 30 Cb Line Lucinda St.

0-25 E Lucinda

B.M. 714 217.10

209.96

211.84	212.21	210.36	210.85	209.36	209.80	208.71	209.12
5-26	4-89	6-74	6-25	7-74	7-30	8-39	7-8
G	Cb.	G	Cb.	G	Cb.	G	Cb.
BC		①		②		BC.	

203.18	203.63	205.87	206.31	206.65	207.10	207.03	207.52
13-22	13-7	11-23	10-79	10-15	10-00	10-7	9-28
G	Cb.	G	Cb.	G	Cb.	G	Cb.
BC		①		②		LC.	

203.8	206.6	207.29	207.52	207.03	207.66	208.07	208.36	208.71	209.12	212.7	215.7
13-3	10-5	9-21	9-28	10-7	9-44	9-02	8-14	8-39	7-28	4-4	1-4
50	30	24	178	178	75		7.5	16.9	16.9	35	50
		SW	Cb.	G				G	Cb.		

208.63	203.18	205.29	204.84	206.53	207.17	208.18	209.16	210.27	211.84	212.21	214.84	215.35
12-7	13-22	11-21	12-25	10-57	9-72	8-92	7-24	6-23	5-26	4-89	2-26	1-25
45	45	35	35	23	15		15	27	35	35	50	50
Cb.	G	Cb.	G					G	Cb.	G	Cb.	

205.96	205.55	206.26	206.73	207.72	208.87	209.97	211.69	212.64	215.85
12-14	11-53	10-24	10-27	9-38	8-23	7-13	5-41	4-16	1-25
45	35	20	26	15		15	30	35	50

217.10

1

on Hub 0+00 E Golden Park Ave P.M. this Book

1+30

13 ⁴	11 ⁶	9 ³	6 ⁶	7 ²	7 ⁰	7 ⁰	4 ⁴	3 ¹	2 ¹²	1 ¹²	1 ⁰	1 ⁰
203.7	205.5	207.8	210.5	209.9	210.1	210.1	212.6	214.0	214.9	217.5	218.0	
50	30	18	13	11	7	8	12	18	27	34	44	

1+21 Power Pole # D33512T 22.3 Lt

1+00

13 ⁴	10 ⁷	10 ⁰	8 ⁷	7 ¹	7 ²	7 ⁵	7 ²	8 ⁹	3 ¹⁸	3 ¹¹	3 ⁰	1 ⁰	1 ¹²
203.7	206.4	207.1	208.2	210.0	209.4	209.6	209.9	211.3	213.8	214.1	217.2	218.3	
50	30	23	17	13	11	6	6	9	13	22	35	43	

0+65

12 ⁷	10 ⁹	10 ⁷	8 ⁰	8 ⁴	8 ⁴	8 ¹	6 ¹	6 ¹⁵	3 ¹	1 ¹²	1 ⁴	
204.4	206.2	206.4	209.1	208.7	208.7	208.7	210.6	213.7	215.9	219.5		
50	30	27	16	11	6	6	6	13	30	50		

0+53.5 Power Pole # P925 21.5 Lt

0+25

11 ⁹	10 ⁴	9 ⁹	8 ⁵	8 ²	8 ¹⁰	8 ⁹	8 ⁴	5 ⁵	4 ⁴	3 ⁰	1 ²	1 ⁰	1 ⁰
205.2	206.7	207.2	208.6	208.9	208.3	208.2	208.7	211.6	212.7	214.1	215.9	219.1	
50	30	26	22	17	15	2	6	6	12	15	30	50	

0+04

10 ¹⁰	10 ⁵	8 ⁷	9 ⁵	9 ⁰	7 ⁹	6 ¹²	2 ¹	0 ⁷	1 ²⁰		
204.3	204.5	208.4	207.6	208.1	209.2	210.9	214.4	216.4	219.1		
50	30	18	16	9	5	9	15	30	50		

217.10217.10
1

CK Starting B.M. 7.14 209.96 209.96

1+48.95 No Line Crests. Real

217.10

199.5	204.2	205.3	208.6	211.0	211.3	210.6	210.6	210.9	212.4	215.4	215.7	218.5
17	12	11	8	6	5	6	14	6	4	17	14	14
50	30	27	20	15	11	8	17	18	26	30	30	50

217.10

11.19.48
Hendricks

Location of water valves
Jennings & Bangor.

INDEXED
WK
NOV 19 1948

51

Bangor

Fd. Conc. Mon.
S.E. Cor. Roseville Mts.
S.W. Cor. Golden Park

Jennings St.

130.85

Fd. Conc. Mon.
N.W. Cor. P.L. 179
N.E. Cor. P.L. 180

90° 505
8" gate

90° 93
8" gate

St.

Location of E.C. of Con. Wall
 S. end Bangor St, Skerret P.I.

W.O. 25001

1-17-49
 Moore Sperrin
 Boffa Binch

52

T.P. NAIL
 P.P. 3301 3.15 275.69 1.79 272.54
 T.P. 10.59 274.33 5.80 263.74

1+70.6

1+26

S. 2nd
 B.M. Con. 11.12 269.54 258.42
 Mon.
 Con. P.I.
 179 P.I.

266.8
 2.7
 42.1
 Base
 wall
 ON DICT
 249.20
 2.08
 34.3
 Top
 wall

269.04
 0.50
 42.1
 Top Wall
 B.C.
 249.20
 0.34
 38.4
 Top
 wall

269.50

LOT A BLOCK 2

Survey of Existing Septic Tank

Foot of Camino de La Costa

Blk "A" La Jolla Herrerosa

Moore
Bc99

Sherman
Bunch

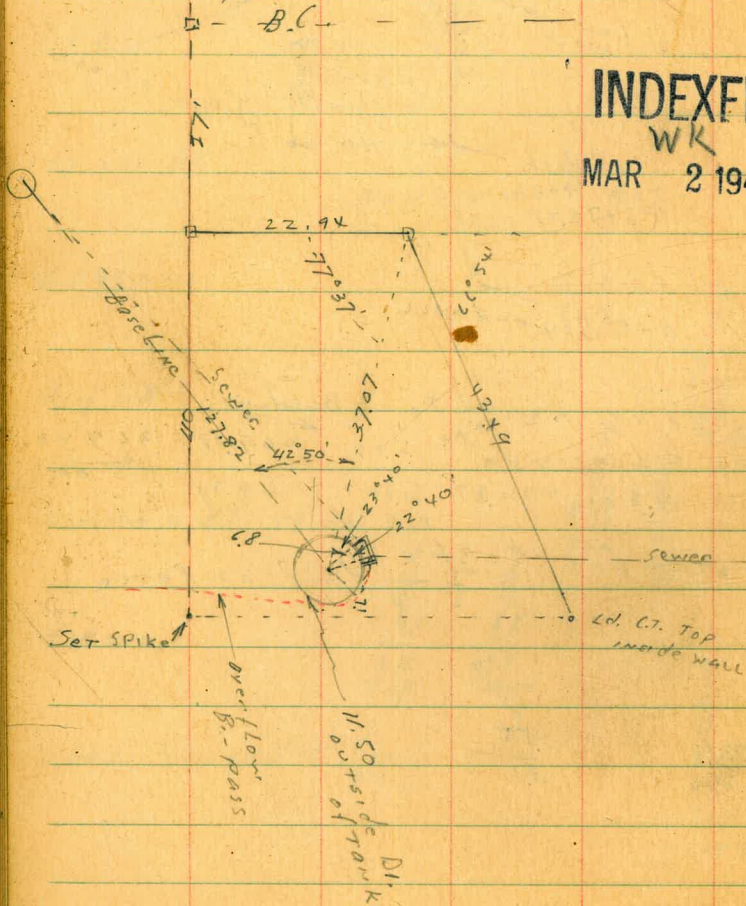
3-1-49

□ = Set 2"x2" R.M. Hubs

INDEXED

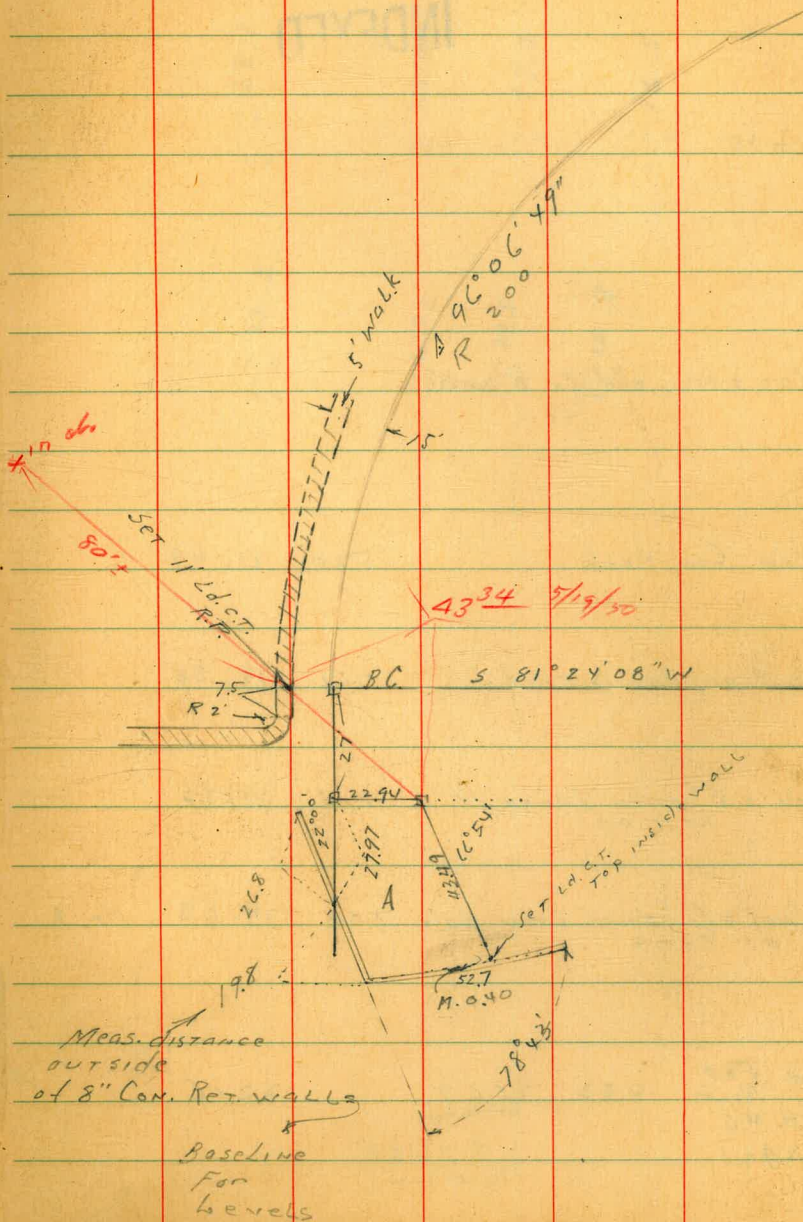
WK

MAR 2 1949



W.O. 60058

54



INDEXED

0 + 15

0/100 = Nly end Ex 8" Wall

Top Con Tank 5.20 21.49

Inv. Pipe, Box to Tank 7.14 19.55

Inv of Sewer from N M.H. #7 7.13 19.56

Inv. of Sewer from East of Tank 7.06 19.63 PT. A

B.M. Top Rim M.H. #C 1429-1 4.53 26.69 22.16

Lr

Top Wall

Rr

23.1

41.0
3.0
20

23.3

3.0
21.4
20

22.42

41.7

22.92
3.97

17.3

9.4

15.2

10

16.5

10.2

10.520.8

10

26.69

0771

0764

0750

0748

0746.6 Con Wall 78° 23' LT

0735

0726.8

26.69

3.3	3.7	4.5	6.4
40	20	10	1
			dirt

TOP 22.44 9.4 R7 56

Wall	17.3	19.0	22.0	24.1	26.4
	4.25	1	1.7	1.0	2.0
			dirt	sand	Rock
Base					
Wall					

22.39 6.9

x30	19.8	21.0	23.1	25.8	27.2
	1	1.3	2.5	1.0	2.0
			dirt	sand	Rock
Base					
Wall					

22.27 6.2

x2	20.5	21.0	22.4	25.6	25.7
	1	1.2	2	1.0	2.0
			dirt	sand	
Base					
Wall					

22.20 6.6

x4.9	20.1	23.0	25.6	25.9
	1	4	1.0	2.0
			dirt	sand
Base				
Wall				

22.21 6.1 1.5

6.9	4x8	18.8	19.2	22.8	24.5
1		1	1.2	1.0	2.0
dirt		Base			
		Wall			

22.19 6.5 7.4

x5.0	11.0	17.2	19.3	21.2
	1	2	1.0	2.0
			dirt	

23.4	23.1	22.1	21.9	22.9	21.2	21.7
3.3	3.6	4.6	4.8	4.40	12.5	14.0
45	25	10	1		1	10
			dirt			
					dirt	

26.69

0199.3 end Wall

0191

0181

Lt

Top
Wall

Rt

57

$\frac{3.0}{20}$

$\frac{3.3}{8}$

$\frac{8.5}{1}$
dirt

22.17

$\frac{8.9}{1}$
dirt

17.8

$\frac{13.0}{18}$

$\frac{3.7}{25}$

$\frac{4.3}{10}$

$\frac{7.1}{1}$
dirt

22.29

$\frac{10.5}{1}$
dirt

16.2

$\frac{12.8}{6}$

$\frac{13.4}{18}$

$\frac{3.3}{25}$

$\frac{4.3}{10}$

$\frac{7.1}{1}$
dirt

22.32

$\frac{13.8}{1}$
Base
Wall

12.9

$\frac{14.2}{1.2}$

$\frac{15.5}{3}$

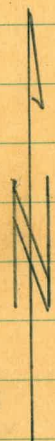
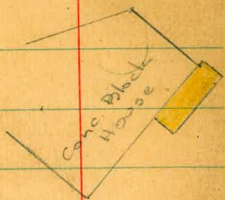
$\frac{20.0}{8}$ $\frac{25.7}{15}$

26.69

4+24.25
2+79.20
1 45.00

INDEXED

NOV 14 1950



8" Conc. Wall

Conc. Block House

Prop. Dr.

Fd. Hub.

1+14.11
Ang. 4054 Lt.

6' open Conc. Drain

Restford Way

Fd. 7' ct.

UPAS St.

23.74
Cross
0-0822

Fd. 13' Ld. + ct.
B. - G 128-P. 29

appears to be 17' off Nly line of Curlew } J.C. 9-21-56
ct is not 17' 5/8" of Nly Line UPAS

3/4 Pipe

3+65.71 = Stub.

95.55

92° 08'

13' ct.

24" RC. Culvert outlet

2+79.20 = Hub.

20.9

1/2 pipe - By Day.

26° 27' 15"

146.02

17' Curlew St.

12.35

Fd. 13' ct.

Fd. Hub

INDEXED

NOV 14 1950

6+36.61 = Hub
 Ang. 32° 52' Lt.

Prop. Drain

4+24.20 = Hub.
 Ang. 4° 36' Rt.

Dist out from E

12 15 15

42

26.5
 22.85

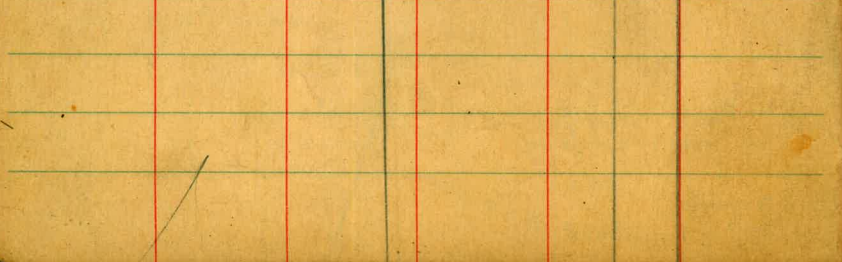
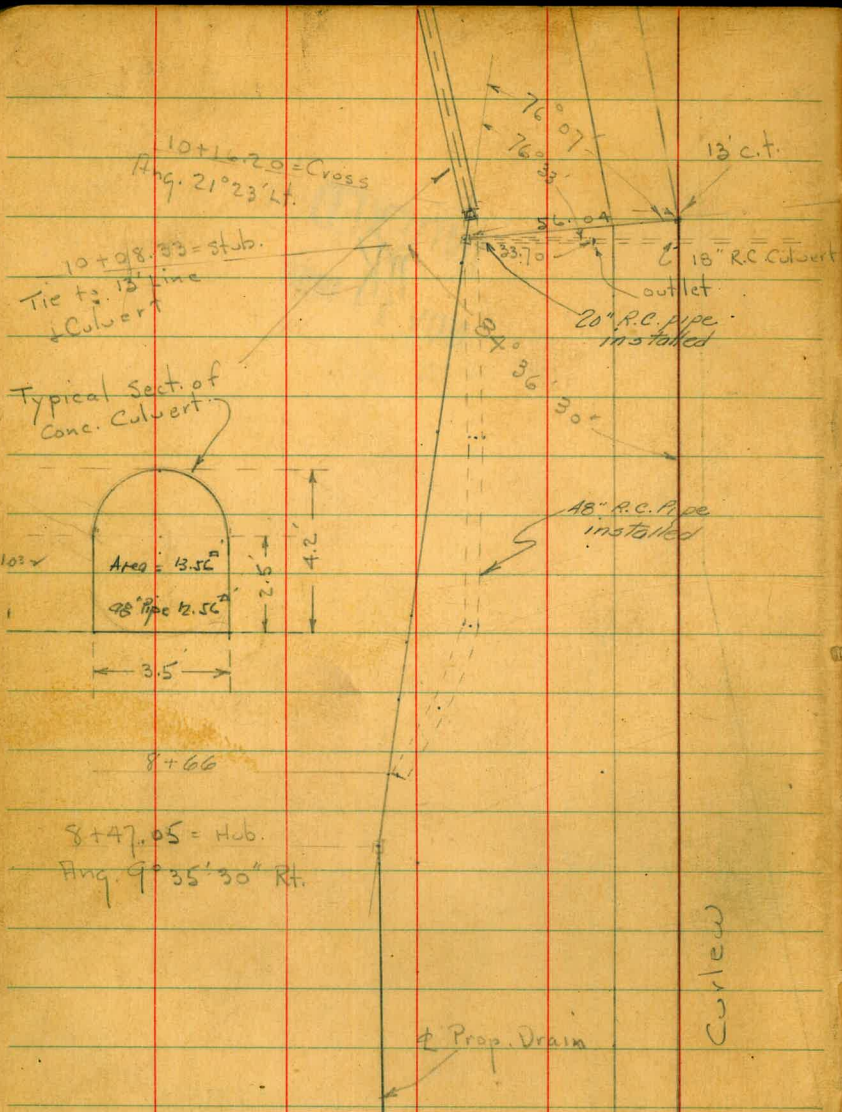
3+83.5 = ±

Ave. 18"

along Lot line

± of Row of Cypress trees

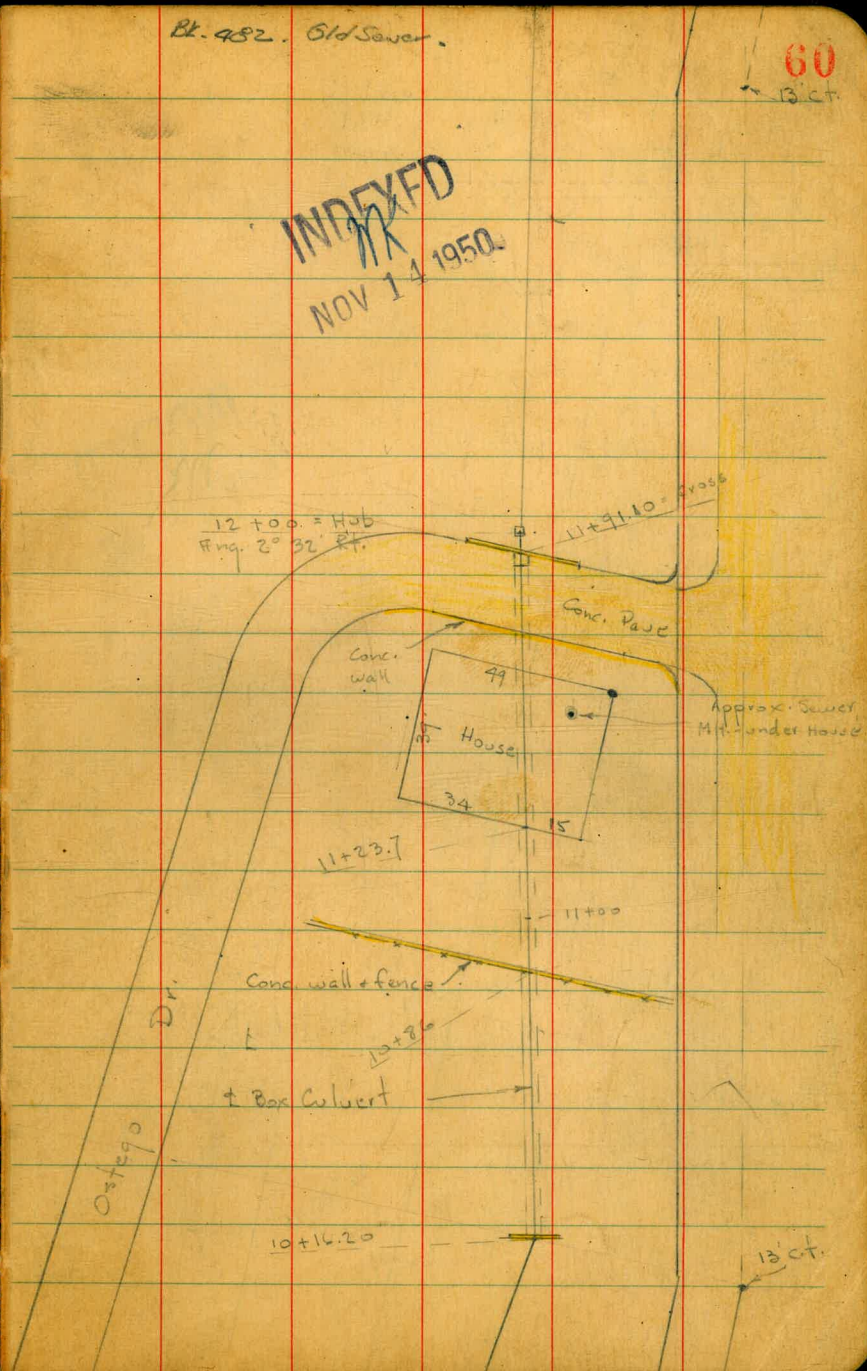
Curlew st



Rt. 482. Old Sewer.

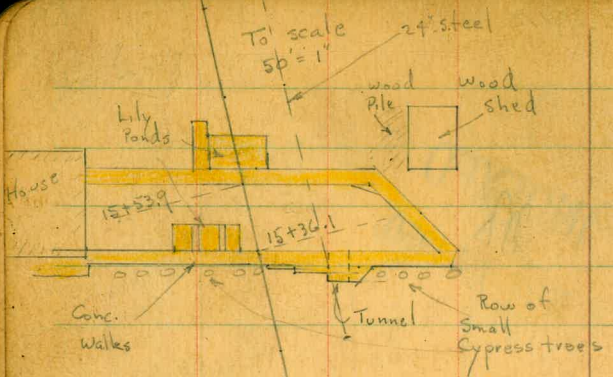
60
13 c.t.

INDEXED
NOV 14 1950



10+16.20

13 c.t.



To scale
5b = 1"

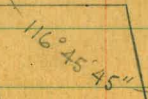
INDEXED
NOV 14 1950

Curlew St

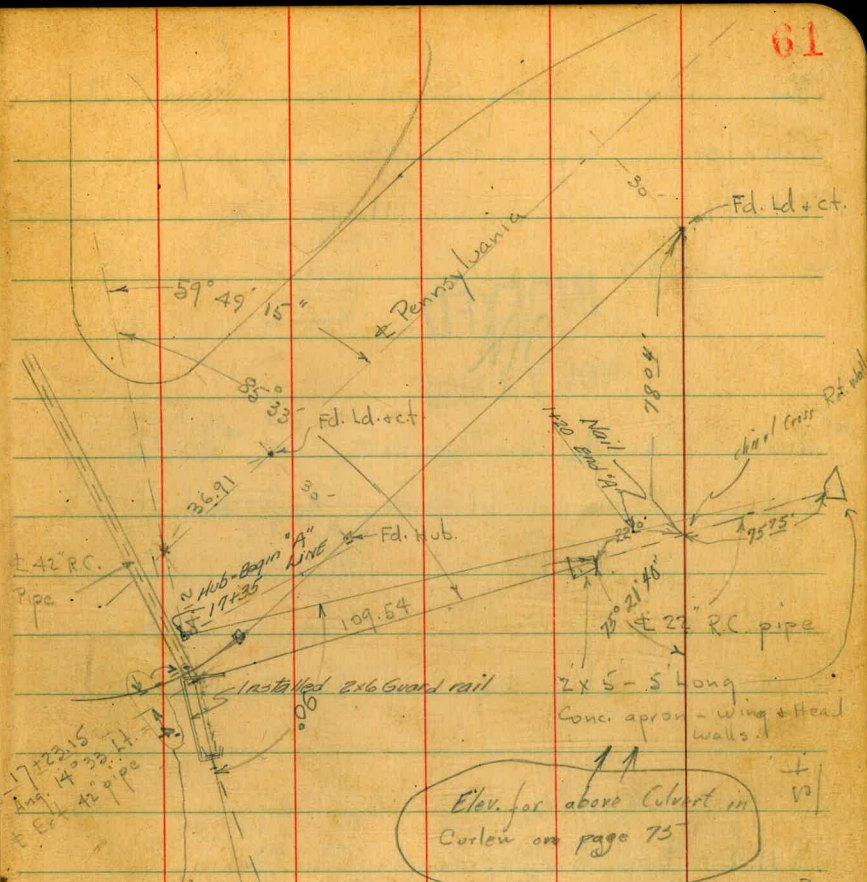


13+43.39 = Hub.
Ang. 01° 21' 30" Rt.

Torrence St.



2 Lt.
Reynold
6-9-54



Elev. for above Culvert in
Curlew on page 75

Note
tie in survey to
here
P.B.

± 24" Steel Culvert

Curlew

vertical by Reg. from Curlew

Beq. Levels along \pm of Prop. Drain - w. of
Curlew - Upas to Pennsylvania.

4699

11-10-50

Osborne
Hardin
Hatch
Rimmer

w.o. 20740

INDEXED

NOV 14 1950

open Drain - Rough Conc. Walls.



0+21 - 3' Rt. + 3' Lt. = Beq. Reg. Sect. of Conc

0+15 = 5.5' Lt. = Beq. Rough Conc. Wall of Drain

0+11.2 = Beq. Conc. apron to Conc. Drain

0+00 = N. gut. Line - outs along gut. line

0-23 = \pm st.

B.M. 12.85 126.57

113.72 B.P. in w.

cb. Reynardway + curlew
B. 1621 - P. 267

Lt

R

Rt

62

Lt	R	Rt
119.7 6.9 20	121.0 5.60 3.1 Top	119.6 7.00 3.1 Bot
120.60 5.97 5.5 Top end wall	119.37 7.20 5.5 Conc. Bot.	119.63 6.94 3 Bot
	118.98 7.59 22 Top end Ret	118.35 8.22 22 9+ Ret
116.42 10.15 50 gut	115.57 8.90 30 Top Cor. ch.	117.67 9.77 30 9+ Ret
	116.80 8.78 15	117.79 7.75
	116.53 8.04	119.79 6.66 14 9+ Ret
	126.57 ✓	120.14 5.69 8 Top end Ret. + Beq. Conc wall
		120.88 5.83 14 Top cb. on Ret.

9 = Top
cb. along
N.L.

3+00

2+50

2+00

1+55

T.P. 6.53 128.99 4.11 122.46

to Back Tang.

1+14.11 = Ang. 4° 54' Lt = end Conc. Drain - Sect. 90°

0+91 = 55' Lt. - Sewer M.H.

0+65

0+43 = 18' Rt. = end cb. along N.L.

Lt

Rt

Rt

63

127.0
2.0
38
Toe

124.6
4.4
15

123.9
5.1
25

124.6
4.4
38

124.8
4.2
40
D.

125.1
3.7
42

124.9
4.1
50

126.1
2.9
35
Toe

125.3
3.7
20

123.8
5.2
25

124.4
4.6
30
± 2' ditch

122.9
6.1
35

124.6
4.4
35

124.1
4.9
60 = Toe

124.8
4.2
33

123.1
5.9
28

123.4
5.6
15

123.4
5.6
19
± 2' ditch

121.8
7.2
25

123.7
5.3
25

123.0
6.0
50

123.2
5.8
25

122.8
6.2
7

122.7
6.3
11
± 3' ditch

119.6
9.4
15

123.8
5.2
15

123.1
5.9
45 = Toe

128.99 ✓

122.7
3.9
30

122.45
4.12
3

120.2
6.35
3 on cross

123.5
6.22
3

120.36
6.21
3 Top end wall

122.49
4.09
3

123.5
3.1
20

125.2
1.4
40

5.74 = Rim

121.1
5.5
30
Top

121.87
4.70
3

120.07
6.50
3

120.04
6.53
3

120.11
6.46
3

122.34
4.23
3
Top

123.11
3.46
29.7 = edge walk

126.57 ✓

122.50
4.07
18 = End cb.

Hill to Lt.

4+39 - Cross 4" C.I. Sewer Lat. - from House at Top of

4+38.5 = Sly. of 4' wood foot bridge

4+37.5 - 15.5 Lt. = Φ 30" Cypress

4+24.20 = Ang. 4° 36' Rt. - Sect. on split

4+24 - 29.8' Rt. = Φ 16" Pine

4+14.5 - 13' Lt. = Φ 14" Pine

4+00

3+95.5 - 7' Lt. = Φ 12" Pvc.

3+89.5 - 25' Lt. = Near Cor. Stecco House

3+65.71 = Ang. Tie to Culvert. on Rt. outs along Tie Line

3+60

T.P. 3.81 131.67 1.13 127.86

3+59.5 - 7.2 Rt. = N. cor.

3+40 - 0.5 Rt. = Cor. shed - 9.5 wide

3+32 - 28' Rt. = Φ Sewer M.H. ^{25 99} 464 on Rim
24 35

Lt. 129.51 Φ 127.44 Rt. 64

2.16 4.23 = Top Pipe

8" Top Pipe

3.74 127.93

3 w. end - Top

5.9 125.18 127.75

3.92 Top Bridge

4.67

17 = end - Top.

133.7

+2.0 20

2.3 129.14

3

4.55 127.12

on Hub.

5.5 126.2

10 Φ wash

5.3 126.4

40

0.8 130.9

10

2.7 129.0

5.8 125.9

14 Φ wash

5.6 126.1

35

4.4 127.3

60 = Toe

+1.9 133.6

25 ground.

4.84 126.83

on sub

5.4 125.3

25

4.4 127.3

50

+1.3 133.0

90

1.48 130.19

95.55 = I.E. Pipe

131.6

0.1 25

5.1 126.6

20

5.5 126.2

32

6.1 125.6

34 Φ 2 D.

6.8 124.9

37

5.6 126.1

50

4.4 127.3

50

2.5 124.2

75

131.67 ✓

128.99 ✓✓

6+00

end Bamboo on Rt.

5+65.5 - 27.5 Rt. = ± 30" Cypress

5+60

5+55.5 = 12.5' Rt. = N.E. Cor. - Toilet

5+49.5 = 4.5' Rt. = N.W. Cor. of 5' Wood-daub Toilet

5+46 - 11' Lt. = ± 30" Cypress

5+42 - 14.5' Lt. = ± 8" Cypress

5+38 - 3' Lt. = ± 30" Pepper

5+28.5 - 12' Lt. = ± 24" Cypress

5+25 - 12' Lt. = ± 24" Cypress

5+21.5 - 16' Lt. = ± 16" Cypress

5+17 - 18.5' Lt. = ± of 14" Cypress

T.P. 12.75 140.95 3.47 128.20

5+00 - Beg. Bamboo Jungle on Rt. (Cut down)

4+97' - 14.8' Lt. = end-Cor. Conc. Slab.

4+54 - 15.8' Lt. = Cor. 18' Conc. Slab. - Level

Lt.	±	Rt.	
137.0		129.0	
4.0	8.2	12.0	14.2
40	15	35	40
			± 30.
			128.4
			48 = 70

133.6	130.0	128.2	128.4	126.8	134.6
7.3	11.0	12.8	12.5	14.1	6.3
30	20	30	35	50	
			± wash		
				12.17	128.78
				± 5	floor Toilet

140.95 ✓

133.2	130.5	127.6	127.5	125.6	127.4	128.2	130.1
+1.5	1.2	4.1	4.2	6.1	4.3	3.8	1.6
16	10		4	8	12	30	50
				± 40.			

+1.54
14.8
Cor.
conc.

133.44	129.6	126.7	127.0	125.9	127.0	126.8	129.0
+1.75	2.1	5.0	4.7	5.8	4.7	4.9	2.7
15.8	8		8	12	17	40	65
Cor. conc.				± 4 Ditch			
		131.67 ✓					

Planting - flowers + Trees - from House to wash.

7+86.5 - 15.6 Rt. = Sw. Cor. House

E. side Dirt floor 16 E. + W
17' N. + S.

7+70 - 11.5 Lt. = \pm Doo. Grav. opened shed.
(Gar. removed)

7+65

7+55

7+41 - 2' Lt. = Fly. at 19' Long. Rabbit Hutches

T.P. 12.67 148.99 4.63 136.32

7+25

7+00

6+70 = \pm 4' Ditch

6+50

6+37.5 - 19' Rt. = \pm Sewer M.H. 10.22

6+36.41 - Flng. 32° 52' Lt.

Lt.

\pm

Rt.

66

135.9

13.1
11.5
floor

136.3

12.7

136.2

12.8
8

140.0

9.1
35

137.0
12.0
15.6
ground at Cor.

141.0

8.0

60

135.9

13.1

50

Toe

134.6

14.4

40

\pm 4' D.

132.5

16.5

35

\pm 4' D.

133.9

15.1

32

20

125.7

13.3

20

136.5

12.5

6

136.9

12.1

6

142.4

6.6

15

143.0

6.0

40

Fill

148.99 ✓

135.0

5.9

40

Toe

133.6

7.4

28

\pm 4' D.

132.0

8.9

23

\pm 4' D.

134.0

6.9

20

5

133.6

7.3

5

136.4

4.8

7

142.0

+1.1

7

142.6

+1.6

40

- fill

136.4

4.8

35

Toe

134.0

6.9

15

\pm 3' D.

133.0

7.9

11

7

133.8

7.1

7

133.6

7.3

25

133.4

7.5

25

140.0

0.9

40

131.0
10.0 = Bottom

139.7

1.7

50

134.8

6.2

25

132.6

8.3

6

132.6

8.3

15

131.4

9.6

20

131.6

9.3

20

140.0

0.9

35

\pm wash

131.85

9.10

on Hub

140.95 ✓

9+40

9+00

8+60

8+55 - 13' Lt. = ± 3" Peck

8+55 = ± 5' Ditch - end of Planting

8+47.05 = Ang. 9° 35' 30" Rt.

8+40

8+25

8+12.5 - 16' Rt. = N.W. Cor. House - Conc. floor in Basement

8+00

67

Lt.

±

Rt.

1.0	7.8	7.6	8.7	11.6	10.0	9.0	1.9
40	20		10	15	20	35	45

1.7	6.1	8.4	10.8	12.3	3.2	
40	20		33	37	48	

9.3	11.3	13.0	13.8	12.7	11.8	5.5
35	4		4	8	16	28

14.3

11.23
on Hub.

8.0	13.3	14.1	11.9	10.0	6.7	5.5
40	30	23	15	30	8	30

7.8	14.5	12.6	12.0	10.7	7.2	6.1
50	35	30		20	23	40

11.6	12.60
16	16
ground	Conc. floor

7.1	15.8	13.4	12.8	12.3	11.9
60	50	45	20		16

148.99
at House ✓

12+20

12+00 = Ang. 2° 32' Rt. - Sect. 90' to forward Tang.

5-15' R.R. rails set on slope for grate - 2 part

15.5' Rt. of ϕ = E end - 14' Lt. - w end.

11+91.10 = ϕ at end of Box Culvert - 10" Conc. Headwall

At Osteo - B. 1621 - P. 27

check B.P. in E.ch. 6.71 153.67 153.57 ✓

T.P. 11.80 160.38 0.41 148.58 ✓

10' Long - 10" Conc. Headwall

10+16.20 = outlet of Box Culvert + Ang. 21° 23' Lt.

Shots along Line

10+08.33-33.70 Rt on Ang. Shown = 18" R.C. Culvert.
Conc. apron 45' Long. - 2' wide at pipe - 6' wide at end.
6" Conc. wing walls at side

Back Tang.

10+08.33 = Tie to Culvert on Rt. - Sect. at 90° to

9+75

Lt.	157.7	156.1	152.3	149.2	148.8	Rt.	149.1	154.4	153.9
	4.7	4.3	8.1	11.2	11.6		11.3	6.0	4.5
	25	6		5	8		11	15	40

153.0	154.9	148.1	147.2	148.0	153.9	154.5
7.4	5.5	12.3	13.2	12.4	6.5	5.9
30	12	5		4	12	35

edge
Road

152.45	147.12	153.45
7.90	13.26	6.93
Top 1/4"	I.E. culvert	Top
Gas pipe	- Cross =	Head
along wall	ground ahead.	wall

160.38 ✓
139.7
9.3
ground
142.03
6.56
I.E. =
Cross
1.34
Top
wall
147.65

138.93	139.2	141.9	142.1	143.39	145.99	143.77
10.06	9.8	4.1	6.9	5.60	3.00	5.22
	7	15	25	29.2	33.70	33.70
				edge	Top	I.E.
				Apron	Head	Pipe
					wall	

144.5	144.3	139.93	139.2	142.4	146.3
4.5	4.7	10.06	9.8	6.6	2.7
20	5	on stub.	7	25	30
			edge		
			wash		

147.6	142.7	140.9	139.4	139.6	147.2
1.4	6.3	8.1	9.6	9.4	1.8
40	28		6	12	20
			twash		
		148.99			

13+50.5 - 17' Rt. = ± of Top of 3-24" = inlet

13+40 = Top of Dirt fill - Dike

13+20

Poor Cond. outlet.



13+19 - 18' Rt. = ± of Top of 3-24" Steel pipes

13+00

12+70 - ± is on Ely of shell yard.

check 13' ct. Torrence 6.65 161.23 161.47

T.P. 7.83 167.88 ✓ 0.33 160.05 / Bin cb.

12+55

Lt.

±

Rt.

89

				152.08		153.88
				15.80		14.00
				I.E. of 2 Bottom pipes		I.E. Top pipe
167.1	165.8	164.7	164.3	158.4	155.4	163.8
0.8	2.1	3.2	3.6	9.5	12.5	4.1
35	20		8	11	19	25
						47 wly. walk

	157.54	157.0	156.4	155.4	151.7	151.1	161.9
	10.34	10.9	11.5	12.5	16.2	12.8	6.0
	28.1	20		12	18	22	36
N. Cor. Conc. slab.		Nly. of shell yard			Dirt. under pipes		

	150.96	152.79
	16.92	15.09
	I.E. Bottom 2-pipes	I.E. of Top one

	158.35	157.95	159.4	158.7	150.8	151.4	159.1	160.2
	9.53	9.93	8.5	9.2	17.1	16.5	8.8	7.26
	42.7	24.5		10	20	27	35	43
Conc. floor Gar + shop		edge Conc. along House			Ditch			wly. walk

	9.1	9.3	9.2	17.4	17.5	14.0	9.3	8.7
	49.5	20		13	19	20	30	40
Bench Book				Ditch				
Shell House								

167.88 ✓

	158.4	157.4	156.3	149.1	153.9	158.0
	2.0	3.0	5.1	11.3	6.5	2.4
	25	5		10	13	40
in Shell yard.				± + D.		

160.38 ✓

T.P. 1.93 168.47 2.03 166.54

15+00

14+54 - 16.5' Rt = £ 8" Pop

14+50

14+42 - 17' Rt. = £ 8" Pop.

14+36 - 16.5' Rt. = £ 8" Pop.

14+32 - 17' Rt. = £ 6" Pop.

Poor Cond. 26' Lt. = end.

14+29 - Cross wire fence - 18' Rt. = Cor. - goes N.

14+28 = 11.5' Rt. = £ 2-4" pop.

14+27 - 18' Rt. = £ 10" pop.

14+25 - 10' Rt. = £ 8" pop.

14+21.5 - 14.5' Rt. = 12" Pop.

14+16 - 10.5' Rt. = £ 6" Poplar Tree

Nail in Guy Pole alt.

T.P. 2.03 168.57 1.24 166.54

14+00

13+88.5 - 10' Rt. = £ 18" Euc.

13+60

Lt

£

Rt.

70

166.9
1.7
50

160.0
8.6
35
Toe

159.1
9.5
12

158.1
10.5
12

155.7
12.9
17
£

157.4
11.2
20
fence

160.0
8.6
35

164.7
3.9
50

155.4
3.2
25
on fill
slope

159.1
9.5
15
Toe
fill

157.6
11.0
8

157.3
11.3
8

154.5
14.1
13
£ wash

158.0
10.6
16

166.1
2.5
30

171.1
3.5
40

171.1
2.5
60

168.57 ✓

161.7
6.7
20
8' High
Toe
fill

158.8
9.1
4

158.8
9.1
4

154.4
13.5
12
£ wash

161.6
6.3
25

167.1
0.8
35

168.3
+0.4
35

162.9
4.0
14

157.4
8.5
10

158.2
9.7
10

152.2
15.7
14
Ditch

153.6
14.3
19

164.1
3.8
35

165.0
2.9
50

167.88 ✓

15+58.1 = Nly. walk at Lilly ponds. - 7.8' wide

15+57 - 15.5 Lt. = € 3" Cypress

15+54 - 25.2 Rt. = € 4" Olive

15+53.9 = € at Sly. of 4' Conc. walk - outs are along walk

outs are along walk - Normal to hot lines P 61
wider + Makes top to Rough Conc. Tunnel - See Sketch

15+36.1 € at Nly. of 3.6 Conc. Walk - to W. S. edge jags

15+29 = Nly. Chicken Coop

15+25

15+23 - 29.8 Rt. = € outlet of 12" pipe = water Heater tanks
welded Together

15+18 = Sly. chicken Coop - Poor Cond. 6.5 Lt. = W. Cor. 9' Rt. = E. cor.

15+18 - 24.3 Rt. = € Sewer M.H. 8.96 on Rim.

15+11 - 7' Rt. = € outlet 24" steel pipe - fair Cond.

15+09 - 17.3 Rt. = € outlet of 24" Steel pipe - poor Cond.

15+05 - 6 Lt. = € 8' Diam. Conc. fish pond.
1' Deep.

	Lt.	€	Rt.	
	163.72			71
	163.36			
4.75	5.11	5.48	4.79	5.64
Top Pond.	8' Cor. walk Pond.	walk	Top Pond. Conc.	7.2 = Cor. Pond. Top Pond
	165.00	162.96	163.00	164.3
3.47	5.51	5.45	4.2	
40.5 walk at House	walk	33' ang. Pt. walk	50' Toe fill	
	164.75	163.82	164.26	161.47
3.47	3.72	4.60	4.21	7.00
44.5 walk at House	4.1 Top of 1st Lilly pond.	4.1 walk	23' Top walk at € 4.5' Conc. Tunnel	26 Bottom Tunnel
	163.87	163.82	164.26	161.47
	164.75			165.63
	3.47	4.60	4.21	2.84
	44.5 walk at House	4.1 Top of 1st Lilly pond.	23' Top walk at € 4.5' Conc. Tunnel	51 Ely. end walk
	161.3	160.1	160.0	
7.2	8.4	8.4	8.5	4.7
40	15	15	15	35
Toe				
				158.13
				9.94
				20.9
				I.E. Pipe
				157.63
			165.37	10.84
			13.10	17
			17.3 = I.E. Pipe	I.E. Pipe
	169.42			
9.05				
6				
Top of Rim.		168.47 ✓		

at E. edge of pipe
 17+23.5 = \pm out let of 42" RC. Pipe - Rip Rap fence ends
 17+23 - 7.4 Rt. = NW. Cor. Grav.
 17+22 - 4 Rt. = \pm 24" Cypress
 17+22 - 5' Lt. = \pm 48" Euc.
 17+18 - 11' Lt. = \pm 36" Euc.
 17+16 - 6.5' Lt. = \pm 14" Cypress
 17+14.5 - 18' Lt. = \pm 24" Euc.
 17+16 - 4.5' Rt. = SW. Cor. of 16x16 Gar. dirt floor
 Posts - 3
 17+16 - 2.5' Rt. = Beq. Wire fence - Rip Rap - Steel Rail

17+10.5

Rock + Conc. wing walls

17+102.9 = \pm of 4' Conc. Headwall + \pm inlet 24" pipe

16+80.5 - 5.5' Lt. = \pm 4x6 Clothes post.

16+80

16+78 - 9.3 Lt. = end Rock wall

16+77.5 - 21' Rt. = \pm 4"x6" Clothes Line Post.

72.39
 9.50
 82

16.29
 9.50 =
 I.E. pipe

165.4 7.0 10
 16.35 8.04 2 Top wing
 16.20 10.4 2
 16.20 10.4 2
 16.20 8.15 2 Top wing
 16.24 7.4 8 along Grav.

166.5 3.9 30
 165.4 7.0 10 Top Head wall
 16.49 7.90 10 I.E. Pipe
 16.50 7.4 10
 16.3 4.1 57
 16.1 6.3 61
 16.7 3.7 75
 \pm 3" ditch

165.71
 6.68
 9.3
 Top wall

166.3 6.1 20
 16.3 8.1
 16.54 7.0 30
 16.6 6.4 50
 16.46 7.8 57
 16.70 5.4 63
 \pm 3" ditch = water way from Curlew culvert to inlet shown at 16+51

72.39 ✓

Notes Reduced 11-17-50

		1.95	194.83	195.00
T.P.	13.19	196.78	0.12	183.59
check B.P. in s. cb. - Penns.	13.01	170.70		170.61
T.P.	12.07	183.71	0.75	171.64

= sw. ct. Pennsylvania + Curlew.

= B 1621 - P. 27

outs along $\frac{1}{2}$ of Tie.

= Tie to outlet of 22" RC culvert - 109.54 Rt.

17 + 23.15 = Ang. $85^{\circ} 33'$ Rt. from Tang. produced

12.58	16.1	16.4	19.8	171.89	11.64	114.52
9.50	7.3	5.0	2.6	0.90	0.75	+ 217
I.E.	4	40	75	104.5	109.64	Top
42" pipe				edge	outlet	Head
				conc apron	= I.E.	wall
					22"	
					pipe	

172.39 ✓

Roberts
4-13-51

see page 61

75

Check

			1.70	195.00	= 195.00
I.P.	12.10	196.76	2.46	184.60	

Starting BM

Culvert Outlet West Side Curlew 22° W. of R.L. Intersection

I.P.	5.02	187.06	13.04	182.04
------	------	--------	-------	--------

Culvert Inlet East Side Curlew 75° E. of R.L. Intersect.

10' Curb Inlet Easterly Cb Line Curlew 51° E. of R.L. Intersect

10' Curb Inlet Westerly Cb Line Curlew 10° E. of R.L. Intersection

BM	0.08	195.08	195.00	SW.C.T. Curlew & Penn.	195.08
----	------	--------	--------	------------------------	--------

171.86
1.7
171.69
15.20
INVERT

187.06

178.89
1.7
178.72
16.19
INVERT

187.77
1.1
187.60
7.31
Bottom
Box

190.28
1.9
190.11
4.80
Gutter
Grate

NOTE: Elevations 0.17 High
See Page 74
Reduced CRN
4-25-51

191.28
1.1
191.11
3.80
Curb

186.56
1.7
186.39
8.52
Bottom
Box

189.21
1.7
189.14
5.77
Gutter
Grate

190.31
1.1
190.14
4.77
Curb

Ties

Linda Vista Rd. + Ulrich

11-20-52

C.H.S.

■ denotes cross in square (⊠)

x " cross

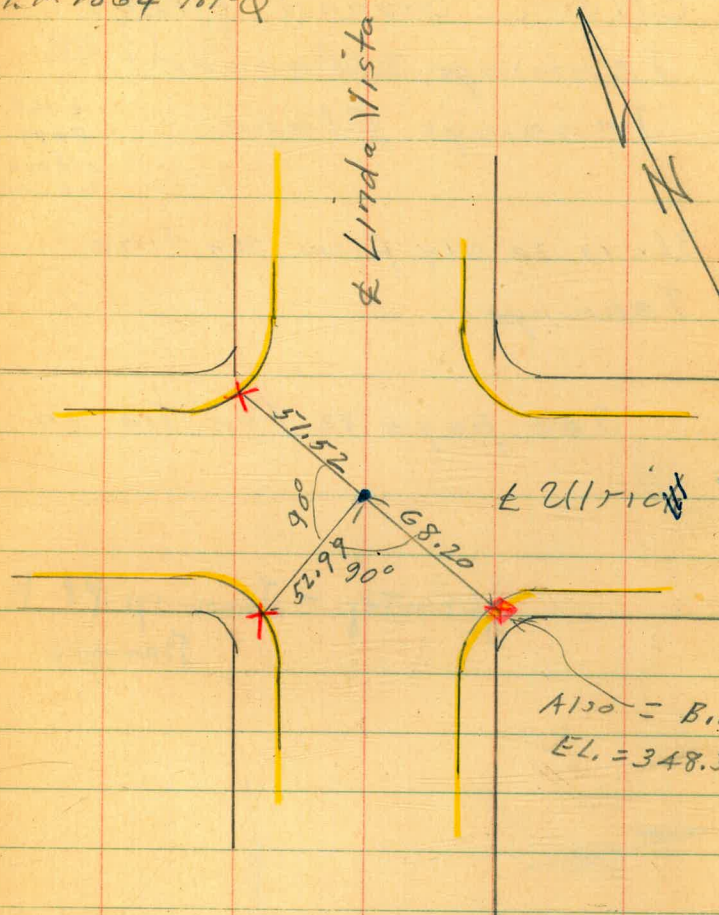
yellow denotes existing curb.

• Denotes Fd. L+T.

Posted - 11-21-52
T.P. 1064 M^oQ

↳ Linda Vista Rd.

↳ Ulrich



Also = B.M.
EL. = 348.39

INDEXED
NOV 21 1952

INDEXED
Law
JUN 11 1953

B.L.

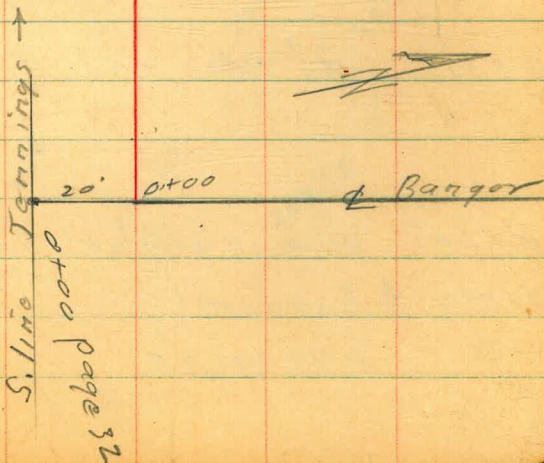
Check Ground Elevs.
Jennings + Bangor
+ Jennings Place.

C.H.S.
Bogg
Altman
Schallin

B.L. is 20' Nly. from sly line
Jennings

See page 32 for tie in

Jennings - Jennings Pl to
Bangor



T.P. 7.90 275.73 8.42 267.83

0+93 - 19² = end drive

0+77 19² H. = start Conc. Drive

0+37 14² = end pave. + ch.

0+34 = end conc. pave

0+31^E 15² H. = end pave + ch.

0+20^t wly gutter line

0+00 = Bangor

6.77 276.25

269.48

B. M.
From
page
3C

271.59
4.66 1.84
30 drive 19²

271.61 271.51 271.4 271.2 270.8 270.6
4.64 4.74 4.8 5.1 5.4 5.6
30 drive 19² 19 5.1 12 20

269.90 269.48
6.35 6.77
14² 14²
ch. ch.

269.81
6.44

269.74 270.18
6.51 6.07
13² 13²
ch. ch.
269.50 269.55
6.75 6.70
269.38
6.87 15

276.25

1+30

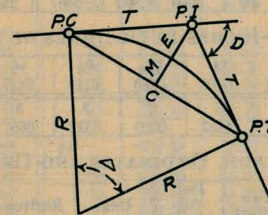
271.7	271.4	271.1	268.3
4.0	4.3	4.6	7.1
200	160	120	100

268.8	267.7	267.9	268.6	268.7
6.9	8.0	7.8	7.1	7.0
50	35	20		20

2751.73

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

Radius= $R = \frac{50}{\sin. \frac{D}{2}}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) Δ = Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 - Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

2+44.39
2+21.88
4+66.27

50
171312
36 88

14
2'

306
1313

.8036838
275

40184190
56257866
6073676
22.1013045.8

2750

9+38.45
715

712495
615809
6689

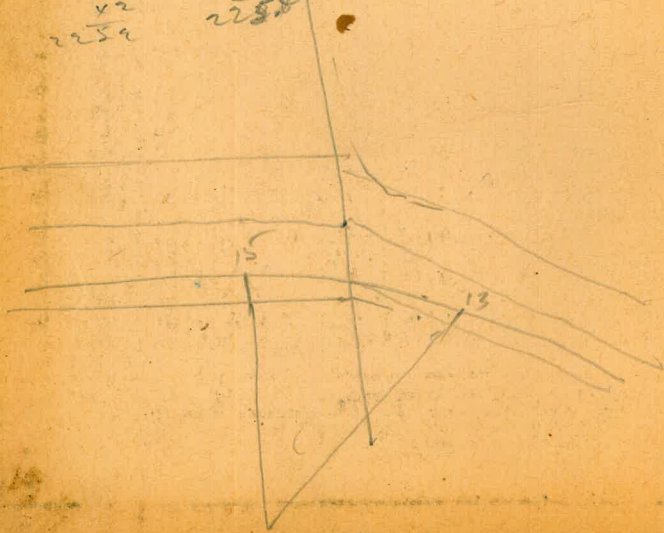
21.19
4125
6244

297

29.7

229.4
v2
2252

229.6
v2
2252



DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20-16)+2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.