

1796

MEMBER  
FIELD BOOK  
NO. 207



1796

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and

MICRO SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on 1 1/2 see inside of back cover.

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Walker  
Hendricks  
Becker  
Johnson

9-29-47

3107.96

8673  
8603

2182.96

8631  
8562

2157.96

8589  
8521

Bk 2132.96

8547  
8480

Bk 2107.96

8493  
8430

Bk 1182.96

8395  
8327

Bk 1157.96

8356  
8175

1132.96 Bk

8158  
8058

1100

04667

043333

0100

7555  
7808  
7303  
7230  
7485  
37740  
7991

1/4

Ave

INDEXED

WK

JAN 6 1949

Altadena

Ave

Trojan

8644  
8600  
8560  
8520  
8480  
8440  
8370  
8321  
8270  
8230  
8171  
8130  
8070  
7771  
7730  
7685  
7231  
7201  
7160  
7120  
7085  
7045  
6999

47046-7485

8125  
8100  
8040  
8005  
8125  
8172  
8125  
8084  
8037  
7883  
7843  
7803  
7513

ALTADENA ST. ROYING - Trojan to El Cajon 2

5182.96

8715  
38781  
38782  
38783

5157.96 Bk

8758  
38719  
38722  
38732

5132.96

8761  
8712

5107.96

8763  
8706

4182.96

8762  
8700

4157.96

8759  
8708

4132.96

8753  
8708

4107.96

8747  
8681

3182.96

8741  
8675

3157.96

8737  
8678

3132.96 Bk

38710  
8645

Ave

Altadena

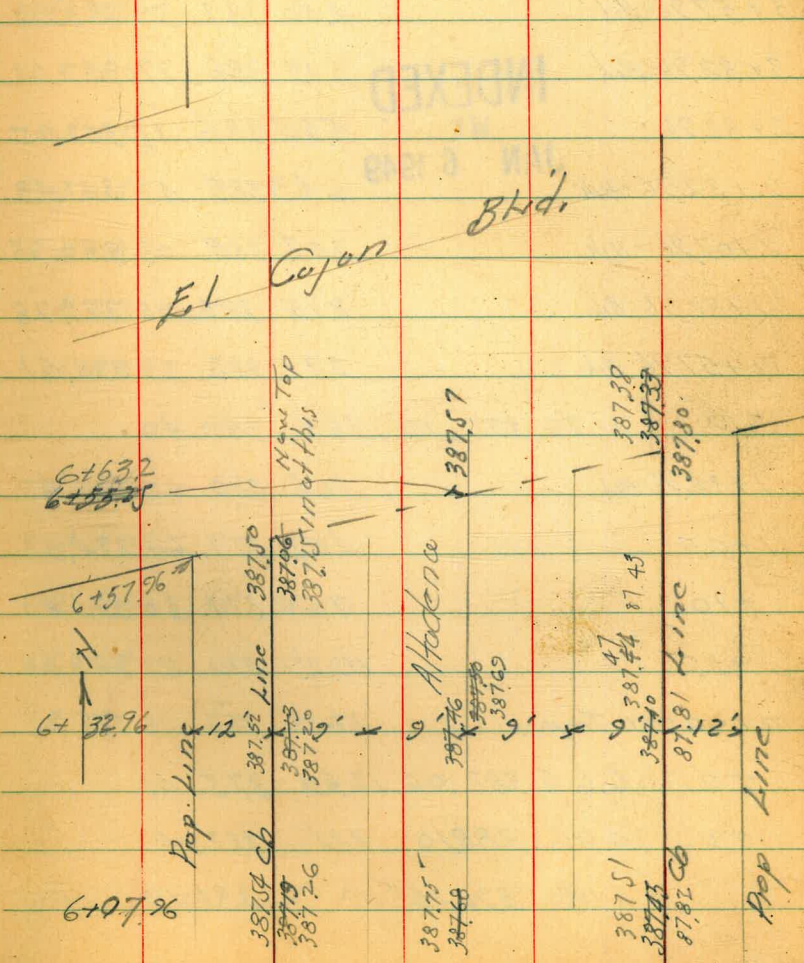
38781  
38782  
38783  
38780  
38783  
38786  
38789  
38792  
38795  
38798  
38801  
38804  
38807  
38810  
38813  
38816  
38819  
38822  
38825  
38828  
38831  
38834  
38837  
38840  
38843  
38846  
38849  
38852  
38855  
38858  
38861  
38864  
38867  
38870  
38873  
38876  
38879  
38882  
38885  
38888  
38891  
38894  
38897  
38900  
38903  
38906  
38909  
38912  
38915  
38918  
38921  
38924  
38927  
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38945  
38948  
38951  
38954  
38957  
38960  
38963  
38966  
38969  
38972  
38975  
38978  
38981  
38984  
38987  
38990  
38993  
38996  
38999

Bk

↖



Altadena St.  
Paving.





Walker  
Hendricks  
Becker  
Johnson  
9-29-47

Grades 6" Water Main  
on Alhambra St  
from Trojan Ave to El Cajon Blvd  
F.I.  
Bottom Trench

				Cuts	Offsets
4+24.63	449	387.61	383.69	3.92	6' 1/2
3+82.96-Bik	472	387.38	383.53	3.85	'
3+57.96-Bik	480	387.30	383.36	3.94	'
3+32.96-Bik	513	386.97	383.07	3.90	'
2+82.96	524	386.16	382.25	3.91	'
2+32.96-Bik	663	385.47	381.43	4.04	'
2+07.96-Bik	707	385.03	380.95	4.08	'
1+82.96 Bik	815	383.95	379.98	3.97	'
1+57.96 Bik	977	382.33	378.51	3.82	'
TR	1170	372.10	166 380.40		'
1+32.96-Bik	166	380.40	376.69	3.71	'
1+05	442	377.64	374.37	3.27	'
+70	768	374.38	371.45	2.93	'
+35	1019	371.87	368.53	3.34	'
0+00=HL Trojan	1288	367.18	365.61	3.57	'
TR	665	382.06	1269 375.41		
TR	006	38810	411 388.04		
	605	392.15	386.10		

BM Sta Top Hgt. El Cajon r. 50 1/2



El. Bottom  
of Trench

Cuts offsets

Chk Starting B.M.	5.45					
T.R.	3.95	391.56	4.49	387.61		
6+64.25			4.49	387.61	383.88	3.73 6.11
6+07.97 Bk			4.42	387.68	384.00	3.68 "
5+57.97 Bk			4.34	387.76	384.07	3.69 "
5+07.97=Bk			4.31	387.79	384.00	3.79 "
4+66.3			4.39	387.71	383.85	3.86 "

392.10  
K Cont. from D.4



Walker  
Heindricks  
Becker  
Johnson  
10-22-47

Altadena St. Grades - Sidewalks

	Rod	El. Stakes	Wk. Elev East edge Sidewalks
2+8296	4.78	386.36	386.35
2+5796	5.52	385.62	385.93
2+3296	5.74	385.40	385.51
2+0796	6.74	384.40	384.97
1+8296	7.17	383.97	383.99
1+5796	2.22	381.92	382.54
T.P. 2.86	391.14	0.17	381.28
1+3747	0.51	380.94	380.97
1+3296			380.62
1+10 <sup>06</sup>	2.79	378.66	378.88
1+0396			
1+00	3.67	377.78	378.12
0+86.06	4.40	377.05	377.05
0+70.6			
0+667	5.86	375.59	375.59
0+45.06	8.13	373.32	373.98
0+33.3	9.09	372.36	373.07
0+00 N.L.	10.92	370.53	370.55
T.P. 3.43	381.45	12.41	378.02
T.P. 2.85	390.43		
0+00	4.31	387.58	
5.79	391.89	386.10	

INDEXED

JAN<sup>W</sup> 6 1949<sup>K</sup>

Cuts & Fills	Rod	El. Stakes	East Line Elev. West edge	Cuts & Fills
+0.01 ✓	4.74	386.40	386.35	+0.05
-0.31 ✓	5.58	385.56	385.96	-0.40
-0.11 ✓	5.55	385.59	385.56	+0.03
-0.57 ✓	6.32	384.82	385.04	-0.22
-0.02 ✓	7.09	384.05	384.09	-0.04
-0.62 ✓	8.47	382.67	382.76	-0.09
	391.14			
-0.03 ✓				
	0.57	380.88	380.91	-0.03
-0.22 ✓				
	3.04	378.41	378.41	0.00
-0.34 ✓	3.38	378.07	378.07	0.00
0.00 ✓	6.10	375.35	375.46 <sup>50</sup>	-0.15
0.00	6.45	375.00	375.17	-0.17
-0.66 ✓				
-0.71 ✓	9.32	372.13	372.27	-0.14
-0.02 ✓	12.13	369.32	369.37	-0.05
	381.45			



	Rods	Stakes Elev.	West. Elev. E. edge Walk	Cuts & Fills	Rods	Stakes Elev.	E. Line Elev. W. edge Walk	Cuts & Fills
6+5796			387.54					
+3296	5.02	387.58	387.56	+0.02				
6+0796	5.05	387.55	387.58	-0.03				
+8296	5.04	387.56	387.60	-0.04				
+5796	5.58	387.02	387.62	-0.60				
5+3296	5.00	387.60	387.57	+0.03				
TP	5.05	372.60	3.59 387.55					
5+0796	3.60	387.54	387.67	-0.13				
4+8296	3.50	387.64	387.66	-0.02				
4+5796	3.52	387.58	387.63	-0.05				
4+3296	3.56	387.58	387.57	+0.01				
4+0796	3.66	387.48	387.51	-0.03			387.76	
3+8296	3.60	387.54	387.45	+0.09			387.65	
3+5796	4.17	386.97	387.36	-0.39			387.54	
3+3296	3.95	387.19	387.14	+0.05	3.98	387.16	387.14	+0.02
3+0796	4.42	386.72	386.77	-0.05	4.79	386.35	386.75	-0.40
	391.14				391.14			



Curb Levels - on 5th  
 from Adams to Dick St  
 and on Dick St. from 5th  
 to Winona to determine grade  
 for Concrete Gutters

Stations  
 are curb lines

2+00

**INDEXED**

WK  
**JAN 6 1949**

1+00

TP <sup>N<sup>o</sup> 2</sup> 7.22 396.22 6.81 389.00 <sup>NW cb  
Adams  
= 5th</sup>

0+00 = 16.8' N.W. Adams

P+C +21<sup>21</sup> on cb = N.W. Adams

PC +21<sup>21</sup>

PC cb Ref on Adams <sup>+51</sup>

Left BM on Adams BM  
 E.S. cb Ref N<sup>o</sup> 2 5.37 390.44

T.P. N<sup>o</sup> 1 6.49 395.81 5.68 389.32

B.M. 5.64 395.00 389.36 <sup>NE BR  
Adams  
& Winona</sup>

H. cb.

H. cb. 8

390.64

5.58

389.99

6.23

388.91

396.72

6.90

388.84

6.97

388.87

6.94

388.09

7/2  
Gutter

395.81



51st Cont.

Hcb.  
4

ECB  
RT.

9

7+00

5+60

5+80

6+33 = Approx S' N West cb Ret on 4.

5+95

=4+64

~~5+64~~ End Sisson's Work on RT

5+40 = PC. Ret

TR #3 4.63 327.04 3.81 322.41

5+00

4+00

3+00

32622

392.09

4.95

392.66

4.38

392.62

4.42

392.39

3.83

391.79

4.93

391.22

5.00

391.04

39222

5+60  
392.50

5+80  
392.39

392.39

391.89

5.15  
Ret.

4.65  
392.43  
4.61  
cb



10+90

10+45

Dep. Dick St

9+25 on Rt - BC. Lt.

9+25

T.P. NO 4 4.71 397.79 396 393.08

10+00 = PC. on Lt.

9+00

8+05 - E.C. cb Rt NW Collier

7+10 on R.

6+61 on Rt = Job Collier Produced = Low Point

7+24 BC. cb Ref.

397.04

397.53 04  
5.26

392.89  
4.15

392.47

4.67  
392.18

4.86

391.93  
5.11

397.79

397.04

H.C.

10

5.26  
-  
4.95  
4.71  
392.84  
393.08

393.08  
3.96

392.26  
4.78

392.04  
5.00



Dickist Curb Levels

16+00

15+80

T.P. <sup>195</sup> 5.80 398.72 4.87 392.92

15+00

14+80

14+20

13+61

13+28 = F.C. cb Ret. SW 50<sup>th</sup>

13+07 opp B.C. cb Ret on Sand

12+40 on RT

12+37 = B.C. cb Ret SW 50<sup>th</sup>

11+80 = F.C. on Lt

11+62 = F.C. on RT

397.79

16

392.97

575

545

392.58

398.72

526

372.37

372.37

542

392.10

392.10

569

392.09

392.09

570

392.24

392.24

553

397.79

16

11

393.27

393.27

545

392.22

392.22

392.22

4.87

392.59

392.59

520

392.39

392.39

540

392.50

392.79

500



Dick St. Curb Levels

<sup>201</sup>  
 Chk. Starting BM. 7.46 <sup>389.36</sup> 389.37  
 2.60 396.83  
 T.P. on fire Plug. 4.49 394.23  
 18+77 = End cb Ret on lt SE Winona & Dick St

18+62 = End of Curb

17+94 = E.C. cb Ret NE Winona & Dick

17+85 = RT

17+67 = B.C. cb Ret SE Winona

17+20

16+94 = B.C. RT

16+80 = B.C. RT

398.72

393.33  
539

393.48

544

393.18

554

INDEXED  
JAN 1918

391.31  
7.41  
393.52  
520  
393.60  
393.67  
525  
393.60  
5.12

398.72



Collier St. Curb Levels.

INDEXED  
WIK  
JAN 6 1949

10 + 85 = BC. Ret SE. 50' h  
10 + 70 = BC. Ret NE. 50' h

7 + 64

chk 7 + 24 P-10

425 396.66

473 391.93

392.41

TR No 3  
P-9

4  
6

Ac. 13

390.39

627

390.62

604

391.83

483

391.97

469







Walker Curb Levels on Adams  
Becker from 51st to Altadena  
Johnson  
10-29-97 thence north on Altadena  
to 51st St. - To determine

Grades for Concrete Gutters

Curbline  
Stations

2+78 E.C. on Alt

2+53 P.R.C. on Alt.

2+18 = P.R.C. on Alt

Return  
2+08 = E.C. on Altadena NW Adams

1+98 = E.C.

1+48 = B.C. Ret. NE Altadena & Adams

1+00

1-

0+00 = E.C. cb Return NW 51st & Adams

4.53 394.97

T.P.N. 2  
390.44 Page 8

stcb

stcb 15

INDEXED  
WIK  
JAN 6 1949

390.64  
4.33

390.44  
4.53

390.24  
4.73  
NW Ret  
B.C. on Adams

390.85  
4.12

390.67  
4.30

390.57  
4.40

390.35  
4.62

389.87  
5.10

388.87  
6.10

394.97



Attadena Curb boards  
Cont. from P. 15

T.P. 443 397.10 509 392.67

8+40

INDEXED

WK  
JAN 6 1949

7+40

7+00 E.C. on RT

6+40

6+20

5+30

5+20

T.P. 6.00 397.76 3.21 391.76

4+50

4+20

4+00

3+50

3+00

394.97

HCB

HCB

16

392.72  
5.04

392.38  
5.38

392.03  
5.73

391.61  
6.15

397.76

391.32  
3.65

391.76  
3.21

391.57  
3.40

390.99  
3.98

391.30  
3.67

394.97



Altadena Curb Levels  
Cont. from P. 16

4cb

17

\* Cont P-18

T.P. 7.37 398.29 6.18 390.92

9+10 = 6+33 on 51st = E.C. Rt NW 51st

48' →  
Return

8+62 = E.C.

397.10

392.01  
5.09

392.28  
4.22

397.10  
1/4



Walker  
Becker  
Johnson  
10-29-47  
50th St. Curb Levels.  
from Collier to Dick St  
to determine Grade for  
Concrete Gutters NO 60215

Curb Line  
Stations Cont P-19

14+20 B.C. cb Return SE Cor Dick St.

14+00 = E.C.

13+80

13+10

12+80

12+50 P.C.

12+10 E.C.

12+00

11+30 P.P.C.

11+10

398.29  
x from P-17

14.6.

Rt. 18

392.03  
626

391.91  
638

391.86  
643

391.55  
674

391.47  
682

391.38  
691

391.38  
691

391.15  
714

391.18  
711

390.87  
742

390.85  
744

390.78  
751

398.29  
x



50th St.  
Cont. from p. 18

19

14 + 50 = 13 + 28 p. 11

~~0.01~~  
392.11  
392.10 p. 11

392.11  
5.73

JP 5.78 397.84 6.23 392.06  
398.29

397.84



Grades - Curc. Gutters

on 51st from Adams to Dick St  
 And on Dick St. from 51st  
 to Wizerza

Rt cb

Rt.

Curb line  
 Stations

**INDEXED**  
 WIK  
**JAN 6 1949**

Roots Elev. West cb  
 Elev. Gutter  
 at cb. line

Cuts

Sta.

Roots

Elev

Elev. Gutter  
 Grade  
 at cb line

Cuts.

2+80		5.51	391.12	390.56	0.56				
+60		5.61	391.02	390.44	0.58				
+40	17 Drive	6.15	390.48	390.32	0.16				
2+20	" "	6.28	390.35	390.20	0.15				
2+00		5.98	390.65	390.09	0.56				
1+80		6.09	390.54	389.97	0.57				
1+60.		6.24	390.39	389.85	0.54				
1+40		6.38	390.25	389.73	0.52				
1+20		6.44	390.19	389.61	0.58				
1+00 = Bk.		6.63	390.00	389.50	0.50				
0+80		6.79	389.84	389.28	0.56				
0+60		6.98	389.65	389.06	0.59				
0+40		7.15	389.48	388.84	0.64				
0+20		7.41	389.22	388.62	0.60				
0+00		7.71	388.92	388.40	0.52				
		4.22	396.63	392.91					

8M 17123  
 p-3



## 51st Gutter Grades

5+90		4.96	392.86	-	392.33
TP					
<del>+90</del>	5.12	397.82	3.93	392.70	
+80		3.80	392.83	-	392.29
+70		3.93	392.70	-	392.25
+60		4.08	392.55	-	392.20
+50		4.08	392.55	-	392.15
5+40 - R. Return		4.01	392.62	-	392.10
5+20		4.13	392.50	-	391.98
5+00		4.24	392.39	-	391.86
4+80 in Drive		4.75	391.88	-	391.74
+60		4.44	392.19	-	391.62
+40 in Dr.		4.69	391.94	-	391.50
4+20		4.69	391.94	-	391.38
4+00		4.84	391.79	-	391.27
3+80		4.98	391.65	-	391.15
+60		5.08	391.55	-	391.03
3+40 in Drive		5.55	391.08	-	390.91
+20		5.34	391.29	-	390.79
3+00		5.40	391.23	-	390.68

39663

Cuts.	St/b. Sto.	51st St. Rods	El.	Gutter Grade	Cuts. 21
0.53	5+40	5.21	392.61	392.00 391.94	0.61 0.67
	5+20	5.22	392.60	392.13 392.02	0.47 0.58
0.54	5+00	5.29	392.53	392.04 392.10	0.43
0.45	4+82.5	5.32	392.50	392.00 391.99	0.51
0.35	5+60/2	5.93	391.89	71.95 391.89	in Place Concrete Gutter
0.40			391.82		
0.52					
0.52					
0.53					
0.14					
0.57					
0.44					
0.56					
0.52					
0.50					
0.52					
0.17					
0.50					
0.55					



51st St

Station	Pods	Elev.	Gutter Grade	Cuts
7+98.1	5.66	392.16	391.53 <sup>63</sup>	
7+91.2	5.69	392.13	391.50 <sup>60</sup>	
7+84.3	5.74	392.08	391.47 <sup>57</sup>	
7+77.4	5.80	392.02	391.45 <sup>55</sup>	
7+70.5	5.79	392.03	391.42 <sup>52</sup>	
7+64 = NW Return	5.85	391.97	391.40 <sup>50</sup>	
BC on Collier				
7+64 = EC Return Collier	5.99	391.83	391.19	
7+54	5.95	391.87	391.25	
7+44	5.95	391.87	391.31	
7+34	5.96	391.86	391.37	
OK See check levels				
7+24 = BC Return	5.81	392.01	391.43	
7+15	5.81	392.01	391.50	
7+00	5.73	392.09	391.59	
+85	5.59	392.23	391.68	
+70	5.50	392.32	391.77	
+50	5.31	392.51	391.89	
NVI				
6+33 = EC Altadena	5.16	392.66	392.00	
SW				
6+00 = EC Altadena	4.95	392.87	392.38	

397.82

51st St

Station	Pods	Elev.	Gutter Grade	Cuts
edge Drive				
8+70	5.28	392.82	392.50	0.32
8+58	5.32	392.78	392.40	0.38
8+36	5.30	392.80	392.30	0.50
8+10	5.43	392.67	392.20	0.47
7+90	5.51	392.59	392.10	0.49
7+70	5.62	392.48	392.00	0.47
T.P. 398.10				
5.58				
edge Drive				
7+50	5.47	392.35	391.90	0.45
7+30	5.48	392.34	391.80	0.54
7+10	5.57	392.25	391.70	0.55
6+90	5.65	392.17	391.60	0.57
6+70	5.75	392.07	391.50	0.49
Low Point Valley Gutter to West				
6+61	5.78	392.04	391.44	0.49
6+55	5.78	392.04		0.51
6+40	5.75	392.07	391.52	0.50
6+25	5.63	392.19	391.59	0.55
6+10	5.52	392.30	391.66	0.55
5+95	5.43	392.39	391.72	0.62
5+80	5.38	392.44	391.78	0.66
5+60	5.21	392.61	391.86	0.49

397.82

22







Dick St.

Stations	Roads	Elev.	Elev. Gutter
13+80	6.37	392.25	391.75
13+60	6.42	392.20	391.68
TP 640	398.62	5.88	392.22 <del>391.68</del>
13+44	5.94	392.16	391.63
13+28	6.01	392.09	391.59
12+37	6.02	392.08	391.54
12+20	5.95	392.15	391.57
12+00	5.92	392.18	391.63
11+80	5.84	392.26	391.70
+70	5.79	392.31	391.73
+60	5.78	392.32	391.77
+50	5.80	392.30	391.80
11+40	5.80	392.30	391.84
11+30	6.02	392.08	391.88
11+20	5.72	392.38	391.91
+10	5.66	392.44	391.95
11+00	5.61	392.49	391.99
10+90	5.57	392.53	392.03

INDEXED

WK

JAN 6 1949

E.S. Ret on Dick

SE Dick + 8376

BC. Return

in Drive

39810

Plich. Dick St.

Cuts	Stations	Roads	Elev.	Elev. Gutter	Cuts
	13+60	6.07	392.55	392.02	0.53
0.50	+40	6.09	392.53	391.92	0.63
0.52	13+20	6.18	392.44	391.95	0.45 58
				391.85	0.68
				38	0.56
				391.78	0.66
			398.62		
0.53	13+07	5.65	392.45	391.74	0.71
0.50	13+00	5.68	392.42	391.76	0.66
	+80	5.72	392.38	391.81	0.47
0.57	+60	5.68	392.42	391.85	0.57
0.58	+40	5.71	392.39	392.00	0.39
0.55	+20	5.69	392.41	391.90	0.49
0.56	12+00	5.58	392.52	392.05	0.36
0.58	11+81	5.38	392.72	391.95	0.46
0.55	11+62	5.31	392.79	392.10	0.42
0.50	+55	5.31	392.79	392.10	0.52
0.46	+45	5.33	392.77	392.15	0.57
0.50	+35	5.31	392.79	392.18	0.67
0.47	+25	5.31	392.79	392.21	0.51
0.49	+15	5.29	392.81	392.23	0.61
0.50	11+05	5.27	392.83	392.26	0.48
0.50	10+95	5.28	392.82	392.28	0.58

24

Low Point in Gutter Grade = valley to South

39810



Dick St.			
H. cb.	Rods	Elev.	Elev. Gutter
Sections			
17+39	5.35	393.27	392.89
17+24	5.43	393.19	392.83
17+09	5.40	393.22	392.79
16+24	5.44	393.18	392.74
+80 in Drive	5.71	392.91	392.70
16+60 in Drive	5.82	392.80	392.64
+40	5.56	393.06	392.58
+20	5.62	393.00	392.51
16+00	5.65	392.97	392.45
15+80	5.73	392.89	392.39
+60 in Drive	6.05	392.57	392.32
+40 in Drive	6.08	392.54	392.26
+20	5.97	392.65	392.20
15+00	6.09	392.53	392.13
+80	6.14	392.48	392.07
+60	6.15	392.47	392.00
+40	6.19	392.43	391.94
+20	6.25	392.37	391.88
14+00 in Drive	6.61	392.01	391.81

398.62

H. cb.		Dick St.			Cuts	25
Station	Rods	Elev.	Elev. Gutter			
17+40	4.91	393.71	393.42 <sup>22</sup>	0.49		
Apex Grade			393.29	0.59		
17+25	4.94	393.68	393.19	0.39		
17+10	4.98	393.64	393.15 <sup>25</sup>	0.49		
16+95	5.04	393.58	393.10 <sup>20</sup>	0.38		
+80	5.03	393.59	393.05 <sup>15</sup>	0.44		
16+60	5.05	393.57	392.98 <sup>393.08</sup>	0.49		
16+40	5.11	393.51	392.91 <sup>393.01</sup>	0.50		
in Drive			392.94	0.37		
16+20	5.31	393.31	392.84	0.47		
16+00	5.31	393.31	392.87 <sup>392.87</sup>	0.44		
15+80	5.37	393.25	392.70 <sup>80</sup>	0.45		
+60	5.51	393.11	392.63 <sup>73</sup>	0.38		
+40	5.53	393.09	392.56 <sup>66</sup>	0.43		
15+20	5.61	393.01	392.49 <sup>59</sup>	0.42		
15+00	5.71	392.91	392.42 <sup>52</sup>	0.39		
+80	5.71	392.91	392.35 <sup>45</sup>	0.46		
+60	5.75	392.87	392.28 <sup>38</sup>	0.49		
14+40	5.82	392.80	392.21 <sup>31</sup>	0.49		
+20	5.78	392.84	392.14 <sup>24</sup>	0.60		
14+00	5.96	392.72	392.07 <sup>17</sup>	0.55		
13+80	5.96	392.66	391.99 <sup>392.09</sup>	0.57		

398.62







Gutter Grades  
Collier St.

from 51st to 50th

Lt. cb.	INDEXED WIK JAN 6 1949	Rods	Fl.	Elev Gutter
Stations				
10+20	in Drive	5.55	390.39	390.11
10+00		5.19	390.75	390.19
+80		5.10	390.84	390.28
+60		5.03	390.91	390.37
9+40		4.94	391.00	390.45
9+20		4.85	391.09	390.54
9+00		4.74	391.20	390.62
8+80	in Drive	4.83	391.11	390.70
+60		4.55	391.39	390.77
+40		4.43	391.51	390.87
8+20		4.23	391.71	390.96
8+00	in Drive	4.47	391.47	391.04
7+82		4.17	391.77	391.12
7+64-End Return		4.69	391.83	391.19

3.27 395.94

BM  
Elev. cb.  
7+64 NW

Cuts.	Rt. cb.	Station			
		10+40	5.23	390.71	390.40
0.28		+20	5.11	390.83	390.38
0.56		10+00	5.64	390.90	390.46
0.56		in Drive 9+80	5.09	390.85	390.54
0.54		9+60	4.85	391.09	390.52
0.55 0.45		9+40	4.77	391.17	390.70
0.55		9+20	4.70	391.24	390.78
0.58		in Drive 9+00	4.88	391.06	390.86
0.41		8+80	4.47	391.47	391.04
0.62		8+60	4.43	391.51	391.02
0.64		8+40	4.31	391.63	391.40
0.75		in Drive 8+20	4.51	391.43	391.48
0.43		8+00	4.18	391.76	391.26
0.65		7+82	4.08	391.86	391.33
0.64		7+64-End Return			

Collier P. 22

395.94







50th St. Gutter Grades  
from Collier Street to Dick St

St. cb.	Rods	Elev.	Elev. Grade Gutter
Station			
12+20	7.26	391.22	390.72
12+10	7.32	391.16	390.68
12+00	7.37	391.11	390.64
11+90 in Dr	7.61	390.87	390.61
11+80 in Drive	7.63	390.85	390.57
+P	7.38	398.48	4.84 391.10
+70	4.24	391.00	390.53
+60	4.25	390.99	390.49
+50	4.25	390.99	390.45
+40	5.03	390.91	390.42
+30	5.12	390.82	390.38
+20	5.17	390.77	390.34
11+10 - Valley to South	5.14	390.80	390.30
11+00	5.19	390.75	390.30
10+90	5.14	390.80	390.31
10+80	5.18	390.76	390.32
NW 50th	5.19	390.75	390.33
10+70 = B.C. Return on Collier			

INDEXED

JAN<sup>WK</sup> 6 1949

395.94 x P. 28

St. cb.	Stations	Rods	Elev.	Elev. Gutter Grade	Cuts
	12+40	7.20	391.28	390.86 81 390.71	47 0.57
	12+30	7.26	391.22	390.82 77 390.67	45 0.55
	0.050 12+20	7.32	391.16	390.77 73 390.63	43 0.53
	0.48 12+10	7.33	391.15	390.74 70 390.60	45 0.55
	0.47		398.48		
	0.26 12+00	4.82	391.12	390.71 67 390.57	45 0.55
	0.28 11+90	4.87	391.07	390.67 63 390.53	44 0.54
	11+80	4.93	391.01	390.63 59 390.49	42 0.52
	0.47 11+70	4.99	390.95	390.60 56 390.46	39 0.49
	0.50 11+60	5.20	390.74	390.58 52 390.42	22 0.32
	0.54 +50	5.02	390.92	390.52 48 390.38	44 0.54
	0.49 11+40	5.05	390.89	390.49 45 390.35	44 0.54
	0.44 +30	5.14	390.80	390.45 41 390.31	39 0.49
	0.43 11+20	5.20	390.74	390.41 37 390.27	37 0.47
	0.50 11+10			P. 28 = 390.34 390.24	39.38 Const. at this Elev.
	0.45 11+00				
	0.49 10+90				
	0.44 10+80				
	0.42 10+70				
	10+60				

395.94



50th St.				50th				30		
Lt. cb. Stations	Rods	Elev.	Elev. Gutter	Cuts	Rt. cb. Stations	Rods	Elev.	Elev. Gutter	Grade	Cuts
+20	642	392.06	391.48	0.58	14+40	650	391.98	391.43	0.55	45
+10	643	392.05	391.48	0.61	14+30	647	391.01	391.49	0.52	52
14+00	655	391.93	391.42	0.53	+20	648	392.00	391.51	0.54	54
+90	663	391.85	391.36	0.49	14+10	657	391.91	391.42	0.49	49
+80	665	391.83	391.33	0.50	14+00	660	391.81	391.32	0.50	50
+70	668	391.80	391.29	0.51	+90	665	391.83	391.33	0.51	51
+60	676	391.72	391.25	0.47	13+80	683	391.65	391.18	0.47	47
+50	679	391.69	391.21	0.48	13+70	701	391.47	391.21	0.48	48
+40	680	391.68	391.18	0.50	+60	680	391.68	391.18	0.50	50
+30	680	391.68	391.14	0.54	+50	679	391.69	391.14	0.54	54
+20	682	391.66	391.10	0.56	+40	683	391.65	391.10	0.56	56
13+10	718	391.30	391.06	0.24	+30	691	391.57	391.06	0.51	51
13+00	720	391.28	391.02	0.26	+20	694	391.54	391.02	0.52	52
+90	704	391.44	390.98	0.46	+10	696	391.52	390.98	0.54	54
+80	705	391.43	390.94	0.49	13+00	731	391.17	390.94	0.23	23
+70	705	391.43	390.91	0.52	12+90	734	391.14	390.89	0.25	25
+60	734	391.14	390.87	0.27	12+80	734	391.14	390.87	0.27	27
12+50	713	391.35	390.83	0.52	12+70	708	391.40	390.82	0.58	58
+40	718	391.30	390.79	0.51	12+60	713	391.35	390.78	0.57	57
12+30	722	391.26	390.76	0.50	12+50	713	391.35	390.75	0.60	60

398.48  
4

398.48



Lt. cb. Stations	50th St. Rods	Elv.	Elv. Gutter
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Cuts	Rt. cb. Stations	50th Rods	Elv.	Elv. Gutter	Cuts
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31

= 13+28 on Dick St

14+50	639	392.09	✓ 391.59
140	643	392.05	✓ 391.55
14+30	643	392.05	✓ 391.52

39848

0.50	= 12+37 on Dick			391.60	
0.50	14+60	640	392.08	✓ 391.50	0.48
0.53	14+50	643	392.05	✓ 391.56	0.58
				391.46	0.59

39848



Gutter Grades

Stations Adams Ave 51st to Alhena

1+88	439	390.56	389.98
1+79.2 Int. Prop. N.W. Adams	492	390.53	389.95
1+68	444	390.51	389.89
1+58	455	390.40	389.84
1+48	461	390.34	389.79
1+40	470	390.25	389.71
1+20	474	390.01	389.51
1+00	508	389.87	389.33
0+80 Dr.	553	389.42	389.13
0+60	551	389.44	388.94
0+40 in Dr.	607	388.88	388.74
0+20	590	389.05	388.55
0+00 = E.C. on Adams	607	388.88	388.35
0-07.0'	610	388.85	388.32
0-14.4	609	388.86	388.30
0-21.2'	608	388.87	388.30
0-26 = N.W. Adams	611	388.84	388.30
0-35	609	388.86	388.35
0-43 = 0+00 on 51st	602	389.93	
4.51 394.95		390.44	

INDEXED  
WK  
JAN 6 1949

Rt. Cb

Cuts	Stations	Rods	Elev	E.L. Gutter	Cuts
0.58					
0.58					
0.62					
0.58					
0.56					
0.50					
0.55					
0.53					
0.54					
0.51					
0.50					
0.50					
0.54					
0.29					
0.29					
0.50					
0.50					
0.14					
0.14					
0.50					
0.50					
0.53					
0.52					
0.53					
0.54					
0.56					
0.54					
0.57					
0.50					
0.54					
0.51					
388.40	C 0.53				
1+98	438	390.57	390.01	0.56	
394.95					



Altadena St. Gutter Grades  
from Adams to 51st

Lt.  
#1. Co.  
Stations

Station	Elev.	Station	Elev.
3+96	384	391.11	390.58
3+70	390	391.05	390.51
3+50	396	390.99	390.44
3+30	406	390.89	390.36
3+10 in Drive	449	390.46	390.28
2+90 Drive	451	390.44	390.22
2+71	431	390.64	390.15
2+53	431	390.64	390.08
2+38	442	390.53	390.04
2+23 NW Adams	445	390.50	389.99
2+08 - E.C. Ret.	451	390.44	389.94
1+98	455	390.40	389.88
+88	457	390.38	389.83
1+82.7 - N.W. Ado 1778 - Beg. Gutter		390.28	389.80
+78	464	390.31	389.78
+68	458	390.37	389.72
+58	467	390.28	389.61
1+48 - E.C. Ret NW Altadena	471	390.24	389.57

394.95

Cond Post  
6100 P-37  
Per request

Stations	Rods	Elev.	Elev. Gutter	Cuts
0.53 ✓ 4+80	3.43	391.52	391.02	0.50
0.54 ✓ 4+60	3.49	391.46	390.95	0.51
0.55 ✓ 4+40	3.55	391.40	390.88	0.52
0.53 ✓ 4+20 in Drive	3.60	391.35	390.81	0.54
0.17 ✓ 4+00 in Dr.	4.03	390.92	390.74	0.18
0.22 ✓ 3+80	4.10	390.85	390.67	0.18
0.49 ✓ 3+60	3.80	391.15	390.60	0.55
0.56 ✓ 3+40	3.89	391.06	390.53	0.49
0.49 ✓ 3+20	3.99	390.96	390.46	0.50
0.51 ✓ 3+00 OK	4.03	390.92	390.39	0.53
0.50 ✓ 2+78 in Dr.	4.10	390.85	390.31	0.54
0.52 ✓ 2+68	4.50	390.45	390.27	0.18
0.55 ✓ 2+58	4.12	390.83	390.23	0.60
0.48 ✓ 2+48	4.16	390.79	390.19	0.60
+ 0.53 ✓ 2+38	4.20	390.75	390.15	0.60
0.62 ✓ 2+28	4.20	390.75	390.15	0.60
0.57 ✓ 2+18	4.24	390.71	390.11	0.60
0.54 ✓ 2+08	4.27	390.68	390.07	0.61
0.55 ✓ 2+08	4.38	390.57	390.01	0.56
1+98 = same as P-32				

394.95



Alhadena St. - Gutter Grades

H.S. Stations

6+40		5.30	392.00	391.51
6+30	in Drive	5.66	391.64	391.17
+20		5.47	391.83	391.44
6+10	in Drive	5.76	391.54	391.40
6+00		5.49	391.81	391.36
+90		5.53	391.77	391.32
+80		5.58	391.72	391.28
+70		5.61	391.69	391.25
+60		5.63	391.67	391.21
+50		5.66	391.64	391.17
+40	in Drive	5.66	391.64	391.14
+30	in Drive	6.11	391.19	391.10
5+10		5.80	391.50	391.02
4+90		5.85	391.45	390.95
T.P.	5.91	397.30	3.56	391.39
4+70		3.60	391.35	390.87
4+50		3.64	391.31	390.80
+30		3.73	391.22	390.73
4+10	Drive	4.17	390.78	390.56

394.95

Cuts	Stations	Rad.	Elev.	Elev. Gutter	Cuts
0.49	6+40	5.02	392.26	391.65	0.61
0.17	6+30	5.08	392.22	391.61	0.61
0.39	6+20	5.15	392.15	391.57	0.58
0.14	6+10	5.19	392.11	391.53	0.58
0.45	6+00	5.22	392.08	391.48	0.60
0.45	5+90	5.27	392.03	391.44	0.59
0.44	5+80	5.71	391.59	391.40	0.19
0.44	5+70	5.34	391.96	391.36	0.60
0.46	+60	5.78	391.52	391.32	0.20
0.47	+50	5.44	391.96	391.28	0.58
0.50	+40	5.48	391.82	391.24	0.58
0.09	5+30	5.51	391.79	391.20	0.59
0.48	5+20	5.56	391.74	391.16	0.58
0.50	* 5+00	5.73	391.57	391.09	0.48
			397.30		
0.48					
0.51					
0.49					
0.12					



Altadena St. - Gutter Grades

Elev.  
Gutter

Cuts	Rt. cb. Stations	Rods	Elev.	Elev. Gutter	Cuts
0.06 ✓					
0.44 ✓					
0.47 ✓	<sup>5190 51st St.</sup> 8+00	496	392.84	392.30	0.54 ✓
	7+90	4.95	392.85	392.26	0.59 ✓
0.46 ✓	7+80	4.98	392.82	392.22	0.60 ✓
0.51 ✓	7+70	5.05	392.75	392.18	0.57 ✓
0.19 ✓	7+60	5.14	392.66	392.14	0.52 ✓
0.28 ✓	7+50	5.21	392.59	392.10	0.49 ✓
0.56 ✓	7+40	5.26	392.54	392.06	0.48 ✓
0.49 ✓	7+30	5.29	392.51	392.02	0.49 ✓
0.46 ✓	<sup>in Drive</sup> 7+20	5.69	392.11	391.98	0.13 ✓
0.48 ✓	<sup>in Drive</sup> 7+10	5.74	392.06	391.94	0.12 ✓
0.51 ✓	<sup>T.P.</sup> 531	39780	4.81	392.49	T.P.
0.48 ✓	7+00	4.23	392.37	391.89	0.48 ✓
0.46 ✓	6+90	5.00	392.30	391.85	0.45 ✓
0.07 ✓	6+80	5.03	392.27	391.81	0.46 ✓
0.46 ✓	6+70	4.98	392.32	391.77	0.55 ✓
0.47 ✓	6+60	4.98	392.32	391.73	0.59 ✓
0.53 ✓	6+50	5.01	392.29	391.69	0.60 ✓

8+20	<sup>in Drive</sup>	5.56	392.24	392.18
8+10		5.22	392.58	392.14
8+00		5.22	392.58	392.11
T.P.	531 39780	4.81	392.49	T.P.
7+90		4.77	392.53	392.07
7+80		4.76	392.54	392.03
7+70	Drive	5.12	392.18	391.99
7+60	Drive	5.07	392.23	391.95
7+50		4.83	392.47	391.91
7+40		4.24	392.36	391.87
7+30		5.01	392.29	391.83
7+20		5.03	392.27	391.79
7+10		5.03	392.27	391.76
7+00		5.10	392.20	391.72
6+90		5.15	392.15	391.69
6+80	Drive	5.57	391.73	391.66
6+70		5.22	392.08	391.62
6+60		5.24	392.06	391.59
6+50		5.22	392.08	391.55

39730

39730



Gutter  
Elev.

Cuts

		<sup>002</sup>	
= 6133 57st. St. Lt. Side		392.66	
9+08.6	5.16	392.64	392.00
9+00	5.12	392.68	392.05
8+90	5.15	392.65	392.11
8+80	5.10	392.70	392.18
8+70	4.99	392.81	392.25
8+60 = Bik	4.99	392.81	392.36
8+50	5.14	392.66	392.29
8+40	5.13	392.67	392.24
8+30 in Drive	5.58	392.22	392.21

397.80

0.64  
P22 This Book

0.63

0.54

0.52

0.56 ✓

0.45 ✓

0.50 ✓

0.37 ✓

0.39 ✓

0.43 ✓

0.01 ✓

This is per Construction 6-7-48 = G.R.W.

This change made in order to fit Exist.  
Conc. Gut at 8+70



Walker  
Hendricks  
Bocher  
Johnson  
10-31-47

Adams Ave. Gutter Grades

on North Side Street

from 58th to End existing Cb

N.C.B. Line  
Stations

1+05 - End Cb	5.89	389.30	388.80 ✓
1+00	5.86	389.33	388.84 ✓
0+80	5.63	389.56	389.01 ✓ 388.29
0+60	5.84	389.35	389.14 <sup>18</sup> ✓
0+40	5.26	389.93	389.29 <sup>34</sup> ✓
0+20	5.11	390.08	389.44 <sup>51</sup> ✓
= 0+00			389.59 <sup>68</sup> ✓
1+18 P-33	4.96	390.23	389.59 ✓

4.75 395.19 390.44 BM P-32

Cond P-33

Cuts

- 0.50
- 0.49 ✓
- 0.55
- 0.57 ✓
- 0.17
- 0.24 ✓
- 0.59
- 0.64 ✓
- 0.57
- 0.64 ✓
- 0.55
- 0.64 ✓



Adams Ave - Gutter Grades  
on North



Collier St. Gutter Grades

Ech Station	from 50th to Winona	thence
2+80	5.50	392.43 - 391.90
2+70	5.54	392.39 - 391.85
2+60	5.54	392.39 - 391.79
2+50	5.63	392.30 - 391.73
2+40	5.75	392.18 - 391.67
2+20	5.87	392.06 - 391.56
2+00	6.00	391.93 - 391.45
1+80	6.15	391.78 - 391.33
1+60	6.32	391.61 - 391.20
1+40	6.44	391.49 - 391.09
1+20	6.54	391.39 - 390.98
1+00	6.62	391.24 - 390.87
0+80	6.72	391.14 - 390.75
0+60	6.90	391.03 - 390.64
0+40	7.12	390.79 - 390.52
0+20	7.11	390.82 - 390.41
= 0+00		
10+70 P29	7.20	390.73 - 390.30
T.P.	3.73	397.93
	1.69	394.20
	6.53	395.89
0-24.6		390.16

39

Station	West of	North on Winona to Dick St.
0.53	4750	465 393.28 393.04 0.24
0.54	+40	444 393.49 393.00 0.49
0.60	Drive 4+30	465 393.28 392.96 0.32
0.57	+20	449 393.44 392.92 0.52
0.51	+10	452 393.41 392.88 0.53
0.50	81k 4+00	459 393.34 392.84 0.50
0.48	+90	466 393.27 392.77 0.50
0.45	+80	472 393.21 392.70 0.51
0.41	DRIVE 3+70	563 392.90 392.63 0.27
0.40	+60	486 393.07 392.57 0.50
0.41	+50	497 392.96 392.50 0.46
0.37	+40	508 392.85 392.43 0.42
0.39	+30	517 392.76 392.36 0.40
0.39	DRIVE 3+20	543 392.50 392.29 0.21
0.27	+10	524 392.69 392.22 0.47
0.41	3+00	534 392.59 392.15 0.44
0.43	2+90	539 392.54 392.08 0.46
	+79	547 392.46 392.01 0.45
	+67	555 392.38 391.93 0.45
2+55	5.58	392.35 391.85 0.50
2+56		391.70
2+17		391.54
	397.93	

Fire Hydrant  
N. NE BR  
Adams Winona















Grades - Subsurface Ditch  
South Side Collier  
from East of 51st to 50th

Station	Cont. on P-44	Elev.	Flow Rate
+80		390.84 388.88	1.96
+60		390.91 388.85	2.06
+40		391.00 388.82	2.18
+20		391.09 388.79	2.30
9+00		391.20 388.76	2.44
8+80		391.11 388.73	2.38
+60		391.39 388.70	2.69
8+40		391.51 388.67	2.84
8+20		391.71 388.64	3.07
8+00		391.97 388.61	2.86
7+82		391.77 388.58	3.19
7+64		391.83 388.55	3.28
7+01.7		5.04 392.03 <del>388.46</del>	3.57
6+90.8	E side of 51st East edge Side Walk	4.23 392.14 388.44	3.70
6+50		5.29 391.78 388.38	3.40
6+01.59	Bk	6.62 390.38 388.31	2.07
5+75.9	Born Canyon	8.54 388.53 <del>386.53</del>	2.00
5.24	397.07	391.83	

BM on cb 7+64 S. of Collier & 51st P-22



Grades - Subsurface Ditch

South Side Collier

Cont from P. 43

Cb Line  
Stations

El.  
Flow line

11+65.7 = Int cbs NW 1/4 50th Wub 50th Collier	390.16	389.16	1.00
11+80.7 = 1/2 Collier 6.99	390.08	389.14	0.94
11+32.7 = Int. wub 50th S.E. Cor 50th 6.93	390.14	389.11	1.03
10+88 = B.C. cb Return	390.36	389.04	1.32
+80	390.38	389.03	1.35
+60	390.48	389.00	1.48
+40	390.57	388.97	1.60
+20	390.79	388.94	1.85
10+00	390.75	388.91	1.84

397.07  
K from P. 43



Walker  
Hendricks  
Becker  
11-13-47

Grades Subsurface Ditch.  
North Side Adams

45

INDEXED

wk

JAN 6 1949

El.  
Flow Line  
Ditch.

2+12.7	5.02	390.17	388.77	1.40
1+95.1	4.95	390.24	388.74	1.50
1+77.5	5.02	390.17	388.71	1.46
1+48 - B.C. Ret. NE Pitodena	4.84	390.35	388.66	1.69
1+20 P-32		→ 390.01	388.51	1.50

4.75 395.19

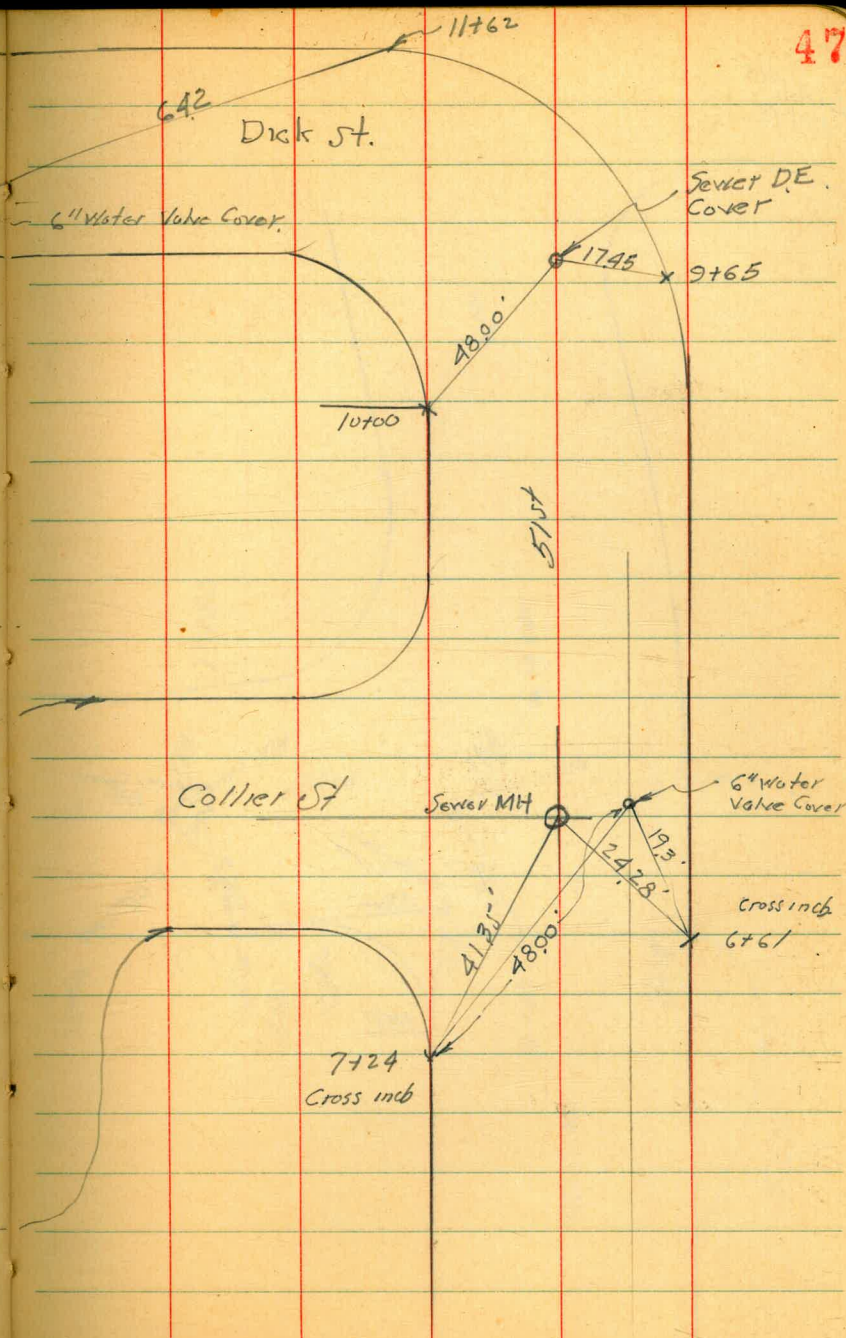
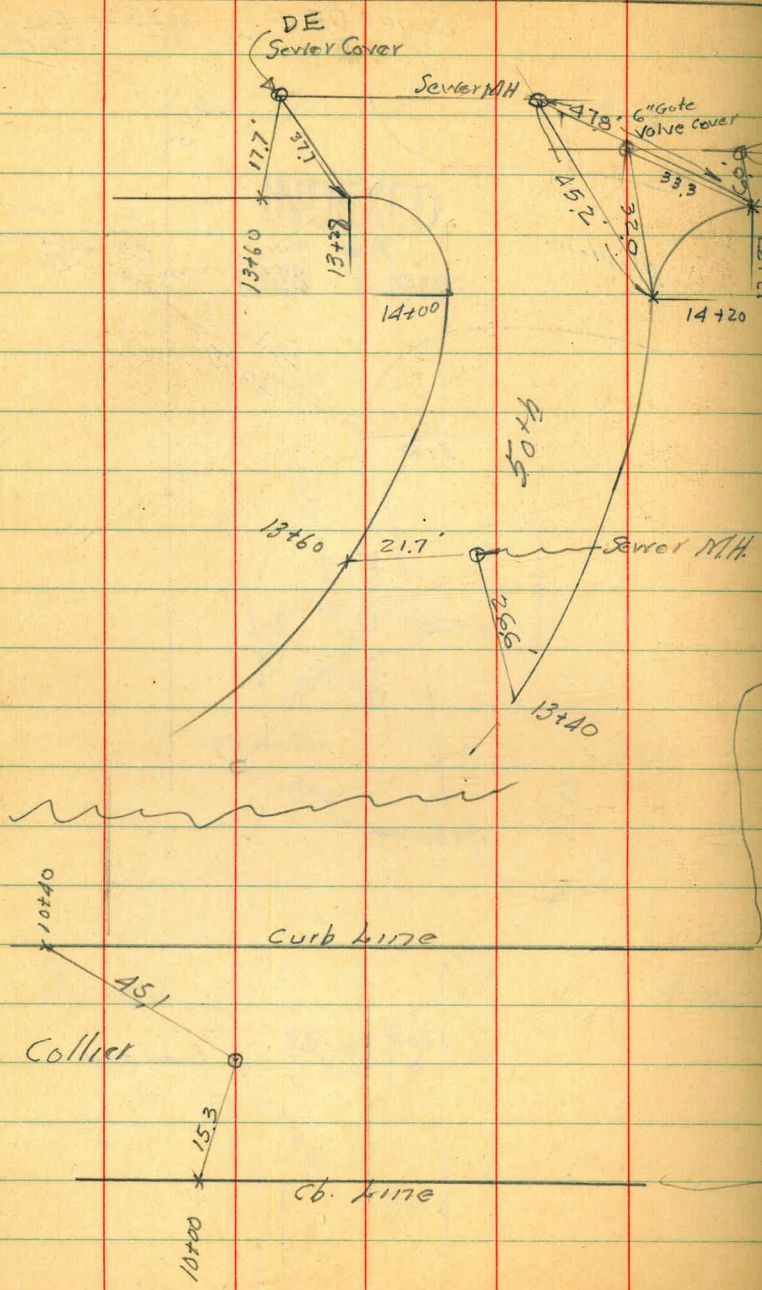
390.44

JMI No. 2 on ch P-7







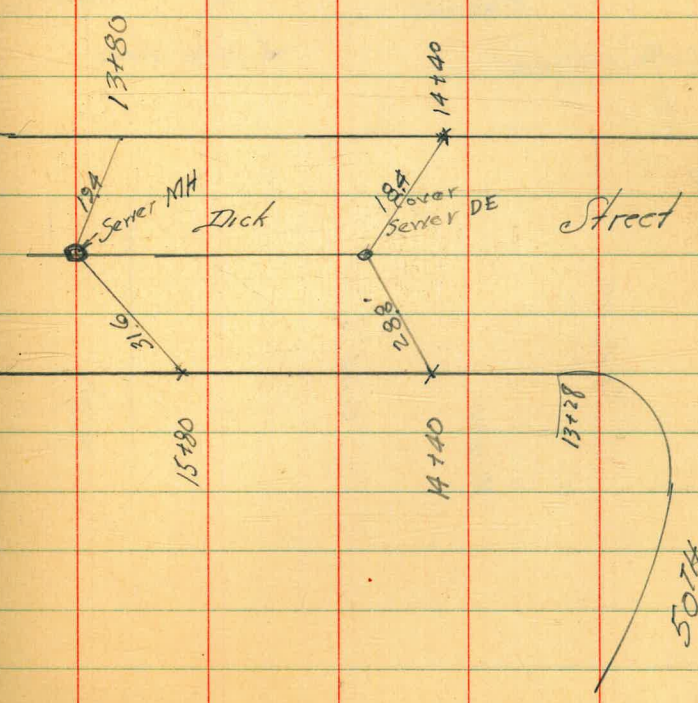
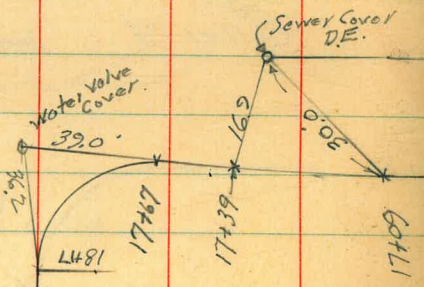




Lucille Drive

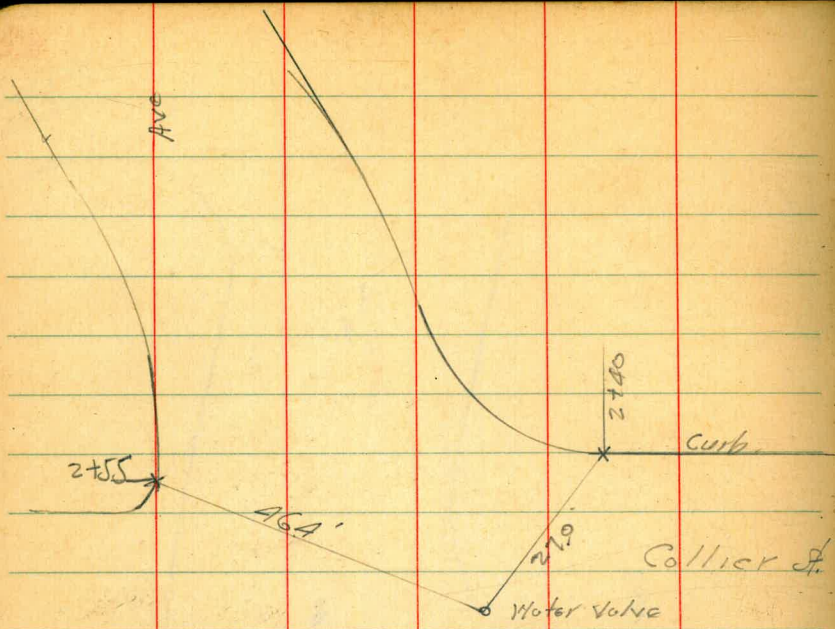
Ave

Whitona



Street

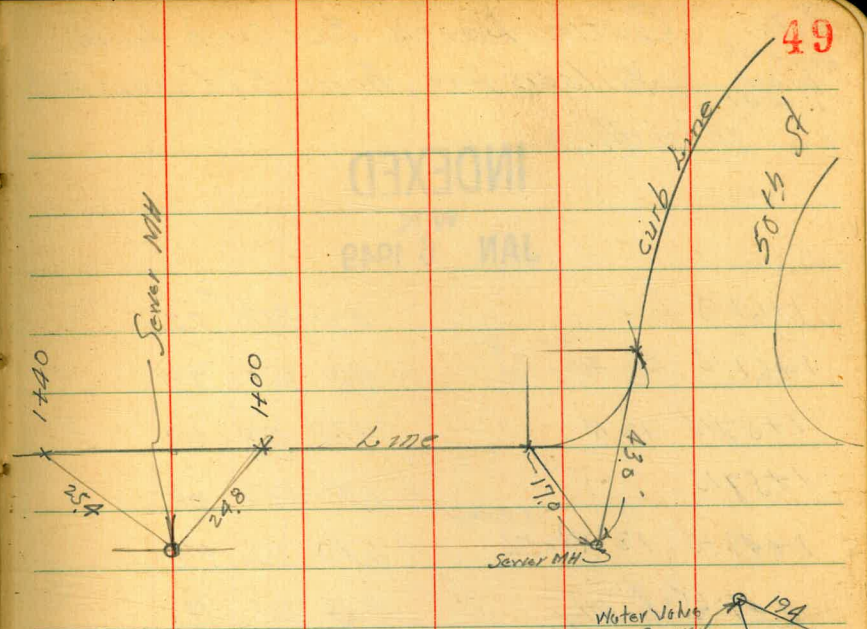




sb line

Witroza

Curb Line



Alley

Water Valve Cover

49

5011 ft



Walker  
Hendricks  
Pickett  
11-14-47

Gutter Levels East Curb Line  
Wilson Ave From E. I. Canyon Blvd  
North.

50

# INDEXED

WIK  
JAN 6 1949

1+61'5 Gut	5.21	382.22
1+61'5 - EC. Alley Ref <sup>on cb</sup>	4.80	382.93
1+57'5 12'R	4.76	382.67
1+57'5	5.37	382.06
1+49'5 12' RT = EL. <sup>Alley</sup>	5.10	382.33
+49'5 = 1/2 Alley <sup>12' RT</sup>	5.45	381.98
1+42'5 Gut	4.84	382.59
	5.37	382.06
1+37'5 Gut	5.36	382.07
1+37'5 = PC. Alley Ref <sup>on cb</sup>	4.50	382.93
Gut.	5.32	382.11
1+00 cb	4.86	382.57
Gut.	6.25	381.18
0+50 cb	5.67	381.76
Gut.	6.88	380.55
0+00 = NW. E. I. Canyon cb	6.40	381.03

7.35 387.43 380.08

B.M. SW. B.P. E. I. Canyon + Wilson.



3+50 Gut.	474	384.38
3+50 cb.	450	384.62
3+25 Gut.	503	384.09
3+25 cb	477	384.35
3+00 Gut.	519	383.93
3+00 cb	499	384.13
2+75 Gut	539	383.73
2+75 cb	519	383.93
2+50 Gut.	552	383.50
2+50 cb.	542	383.70
2+25 Gut.	583	383.29
JP		
<del>2+25 Gut</del> 5.71	389.12	402
		383.41
2+25 cb	391	383.52
2+00 Gut.	437	383.06
2+00 cb	417	383.26
1+72 Gut.	468	382.75
1+72 cb	443	383.00
1+67.5 Gut	523	382.20
1+67.5 Gut.cb	448	382.95

387.43



Wilson Ave Cont.

from 10-51

(1+5715)	25' RT	551	382.72
(1+5715)	21' RT	554	382.69
(1+4965)	25' RT	547	382.76
(1+4965)	21' RT	550	382.73
(1+4215)	25' RT	535	382.88
(1+4215)	21' RT	539	382.84
816	388.23		380.07

001

chk Starting B.M.		6.91	380.07
T.P.	395	386.51	6.56
4+17	in <sup>g</sup> Drive	4.04	385.08
4+00	cut	4.20	384.92
4+00	ch	3.90	385.22
3+75	cut	4.47	384.65
3+75	cb.	4.20	384.92
(3+61)	11' RT on walk N side loco cola	3.91	385.21
3+61	2' Drive	4.59	384.53

389.12

52

80' RT	E.L. Alley	4.90	383.33
80' RT	Ramp	4.48	383.75
80' RT	E Alley	5.05	383.18
(1+5715)	12' RT on ch	5.39	382.84
(1+4215)	12' RT. on ch	5.23	383.00
(1+5715)		5.19	383.04
	E Alley	5.27	382.96
	Ramp	4.55	383.68
			388.23







Wilson Ave Cont.

from P. 53

54

4+00	3.60	384.93	-
3+75	3.82	384.71	384.71
3+61 <sup>2</sup>	3.96	384.57	384. <sup>57</sup> <del>59</del>
3+50	4.03	384.49	384.49
3+25	4.26	384.27	384.27
3+00	4.48	384.05	384.05
2+75	4.70	383.83	383.83
2+50	4.92	383.61	383.61
2+25	5.14	383.39	383.39
2+00	5.36	383.17	383.17
1+72 - 8d	5.61	382.92	382.92
1+61.15	5.76	382.77	382.77

388.53

5

Meet  
Existing Gutter at this point.



## 6" Subsurface Drain

0+46	6.15	390.16	388.42	1.74
0+95	4.68	391.58	389.42	2.16

0+100 = East edge Gutter

## Levels Drain

19+29.8	5.60	390.66	390.60	+0.06
19+08 = Bk	5.27	390.99	390.93	+0.06
18+90	5.18	391.08	391.09	-0.01
18+75	5.06	391.20	391.13	+0.07
18+62 = End cb	4.98			

this set run 11-25-97

4.98 396.26 391.28

B.M. Top cb 18+62 P-26



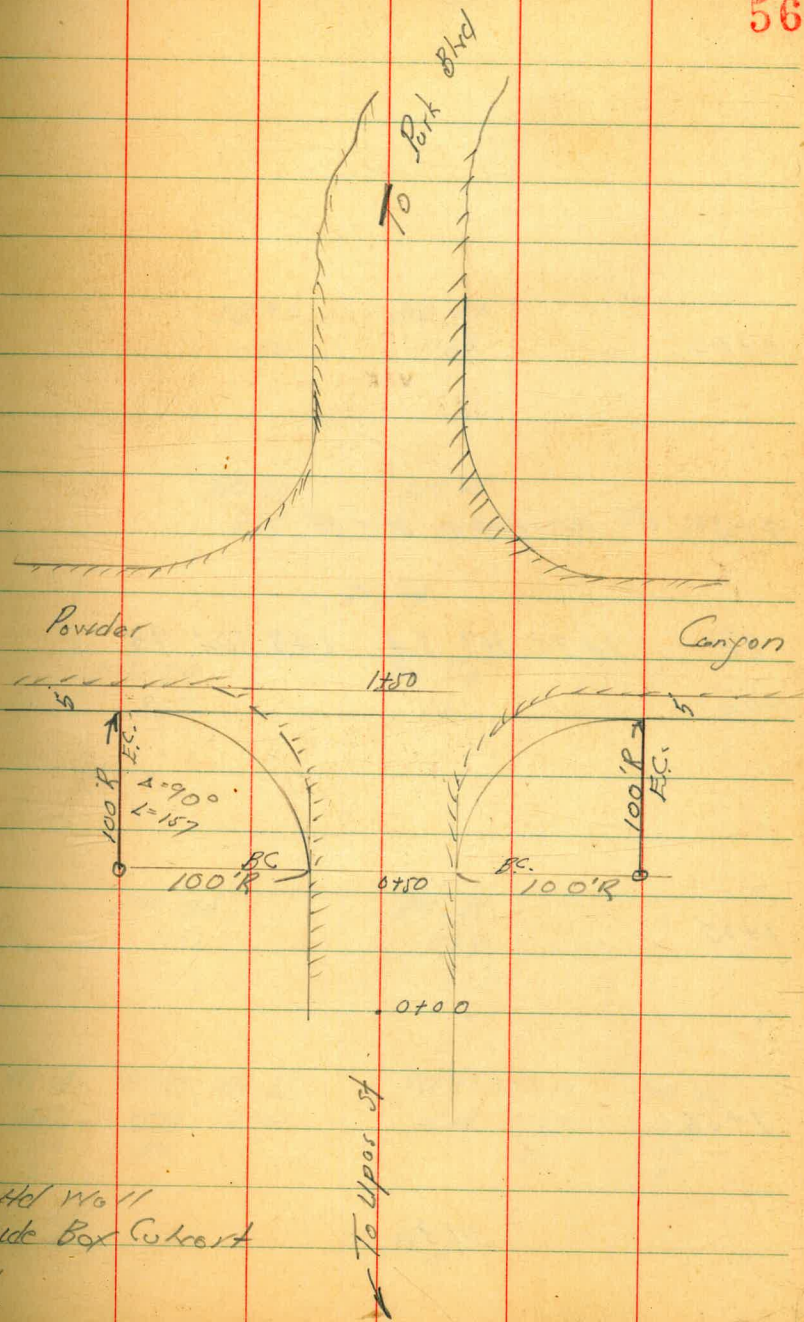
Walker  
Hendricks  
Becher  
Johnson  
11-26-47

Grades - Upper & Powder Canyon  
Road S of Up  
for Daylighting NE. & SE. Cors.

56

B.M. = Assumed Elevation  
Cut Slopes =  $1:1\frac{1}{2}$  see P-58

INDEXED  
WK  
JAN 6 1949



11.36 311.36

South end Hd Wall  
300.0 on East Side Box Culvert  
Elev. Assumed



0+00

318.92

318.17

0.32

1.07

0+50 = 80. 100 Radius H & Ft.

310.59

310.05

8.65

2.19

TP 14.31 319.24 643 304.93

319.24

1+00

302.74

302.54

8.62

8.82

1+25

300.04

300.18

11.32

11.18

1+55

297.04

297.83

298.35

298.92 299.99

300.96

14.32

13.53

12.01

12.44

11.37

10.4

100

50

EC

50

100

EC

311.36

311.36



Powder Canyon

Cont. from P-57

Cut slopes 1 1/2 : 1

Sketch P-56

58

EC # 11	c 69 10.4	297.00
EC # 10	c 47 71	297.25
# 9	c 40 60	297.50
# 8	c 40 00	297.80
# 7	c 61 93	298.10
# 6	c 61 92	298.75
# 5	c 75 113	300.15
# 4	c 72 108	302.85
# 3	c 63 95	305.35
# 2	c 58 88	307.85
# 1	c 57 85	310.60

BC. on Upper Extension

S. East Return 100' Radius

EC # 11

301.00

c 33  
49

# 10

300.65

c 0.6  
09

# 9

300.35

c 0.6  
09

# 8

300.35

c 1.6  
24

# 7

300.52

c 1.6  
24

# 6

301.05

c 6.3  
95

# 5

302.00

c 6.8  
104

# 4

303.20

c 7.6  
114

# 3

305.20

c 7.2  
108

# 2

307.40

c 7.6  
114

BC # 1

310.05

c 8.4  
122

N. East Return

12.68 312.68

BM  
300.00 P-56

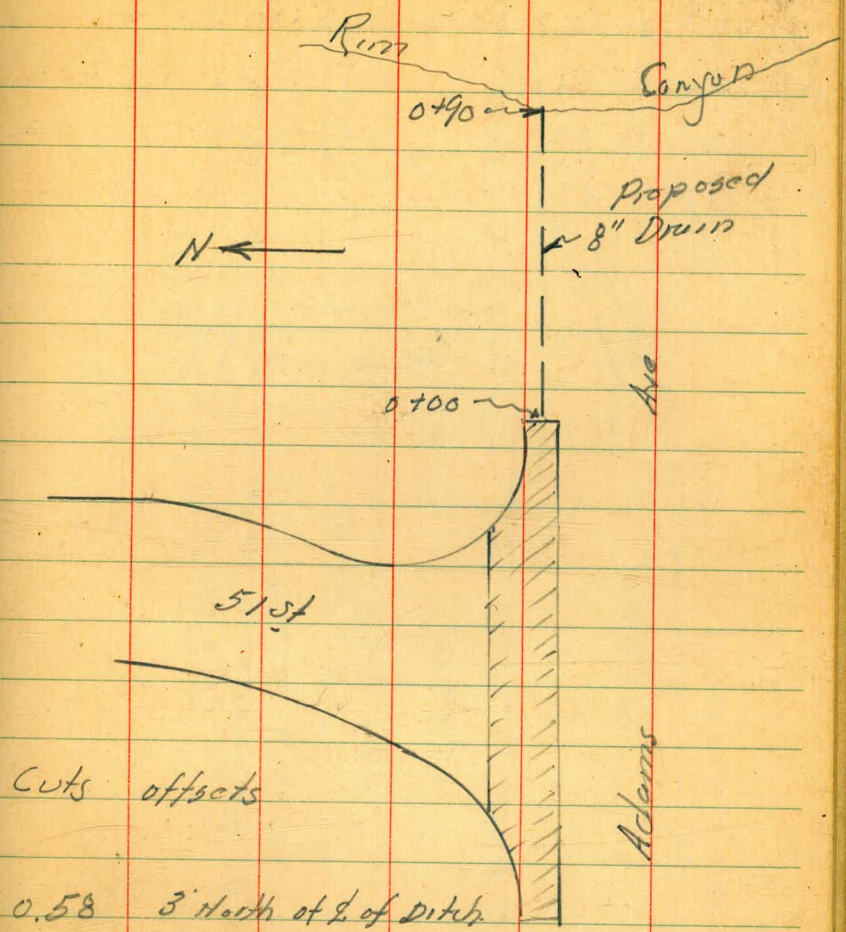


Mulker Grader 8" drain tile  
 Hendricks on North Side Adams Ave  
 Baker  
 Johnson  
 12-20-47 from End of Return NE 51st  
 to Canyon

INDEXED  
 WK  
 JAN 6 1949

El.  
 Flow 6.1170

0+90	7.25	386.00	385.42
0+75	6.29	386.96	385.50
0+50	5.84	387.41	385.63
0+25	5.93	387.32	385.76
0+00	6.20	387.05	385.88
	2.81	393.25	390.44



Cuts offsets

0.58	3' North of E. of Ditch
1.46	"
1.78	"
1.56	"
1.17	→ from <sup>Cone.</sup> Gutter.

814 NE 2 P. 8

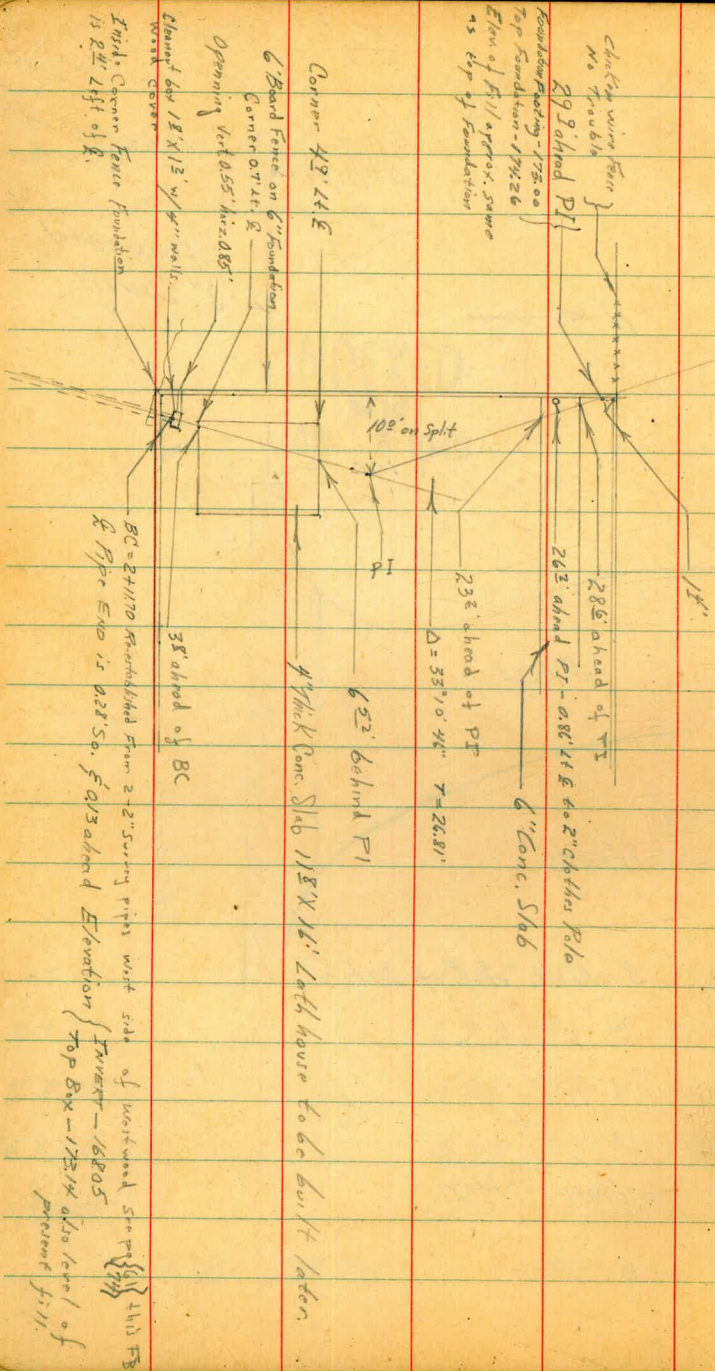


Location of Improvements in 60  
Storm Drain Easement Lot 8

BLK 16 Paradise Hills (See next Page)

Roberts  
Cota  
Moore  
Fuller  
5-17-51  
H.O. 20530

ahead is a chicken wire fence about 15' Lt. &  
fence in bad shape & hung on 4x4 posts.  
Should cause no trouble





Walker  
Hendricks  
Secher  
Williams

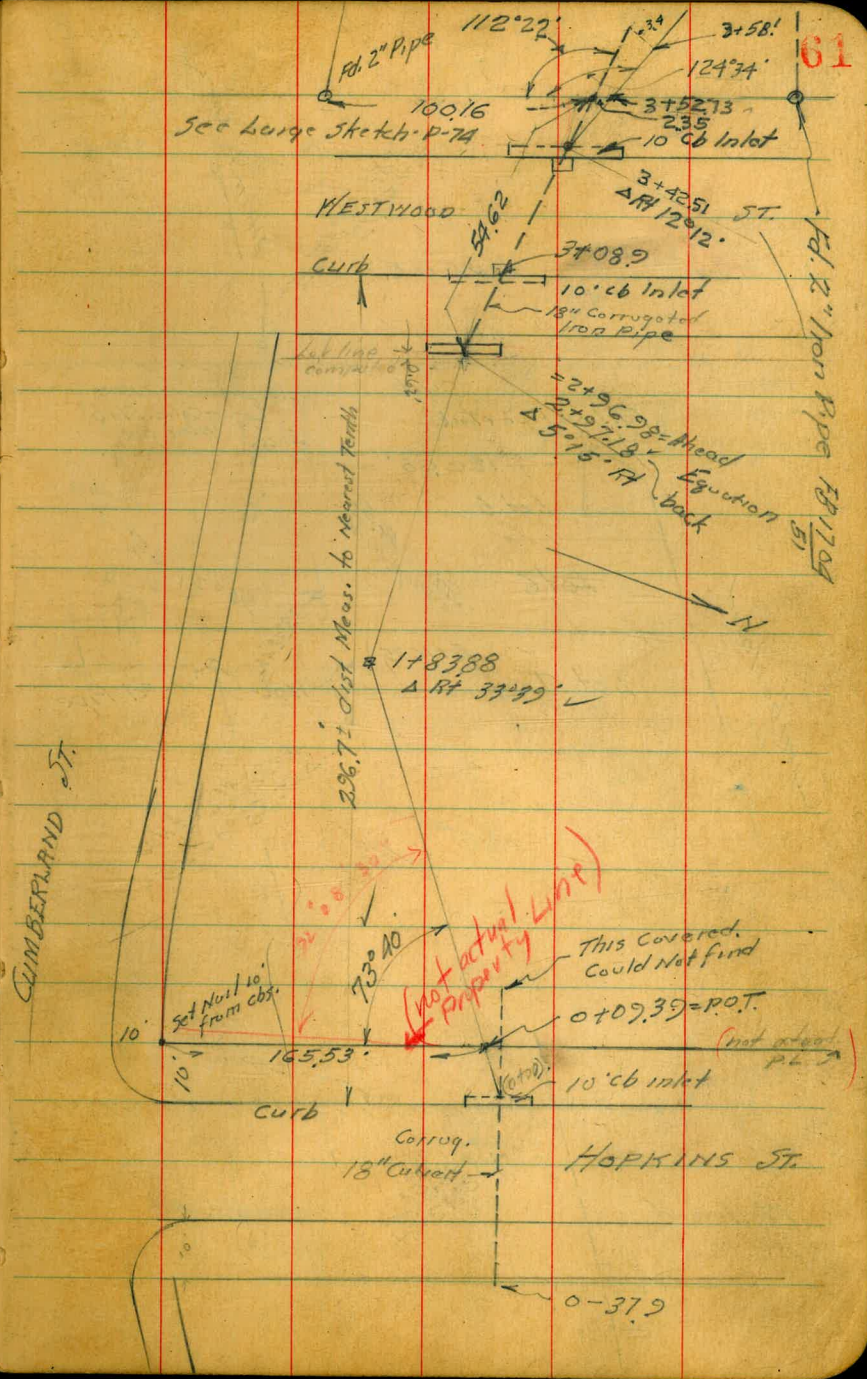
PARADISE HILLS

SURVEY PROPOSED DRAIN

17 Blocks 15, 16 NO 800 <sup>98</sup><sub>99</sub>

~~Indexed~~

For re-alignment Proposed Drain  
See 7234-L ~~ADD~~





646779  
49921  
17048

RACHEL

Fd. Iron Pipe & Tack

curb line

Cone. Slab Inlet Box

120.68'

Lot 5

Lot 6

Lot 7

Prop. Line

5+16.25

96° 27'

45°

Fd Pipe

1806  
+ 9921 Set Hub  
Δ Lt. 28° 06' 40"

curb

Westwood

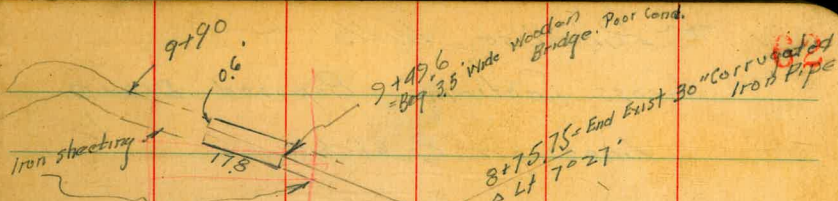
3+42.51  
Δ Lt. 12° 12' 14"

St.

8+05.8

8+3035-45"  
Δ Lt. 69° 15"

Alignment Line



Lot 3  
Lot 2

line of Re-subdivision  
lots 1-12 Inc. of Blk 15 Paradise Hills

FB 1704  
51

N

Prop line

708'

Curb line  
Not Parallel  
to prop. line

FB 1704  
52

~~Hopkins~~  
Westwood



Paradise Hills

Cross Sections Proposed Drain

Location P. 61-62

0+23

0+10

0-01 - WLY cb.

0-16 - Westwood Hopkins

0-31 - ELY cb line Hopkins Westwood

0-37.9 - Beg 18" corr Pipe

114 192.78

191.64

4

4

4

63

Reduced 4-21-48

(C/S)

182 <sup>3</sup>	181 <sup>4</sup>	180 <sup>8</sup>	181 <sup>4</sup>	184 <sup>3</sup>	184 <sup>6</sup>
10.5	11.4	12.0	11.4	8.5	8.2
15	6		4	14	20

185 <sup>4</sup>	184 <sup>8</sup>	185 <sup>11</sup>
7.6	8.0	7.7
		10

185 <sup>24</sup>	184 <sup>23</sup>	180 <sup>10</sup>
7.54	8.53	12.68
cb	Grating	Flow Line Inlet Box

185 <sup>08</sup>
7.70
on Pav.

186 <sup>05</sup>	185 <sup>36</sup>
6.73	7.42
cb	cut.

192 <sup>26</sup>	181 <sup>33</sup>
10.52	7.45
Flow Line	Howell
192.78	

B.M. SHIPP Cumberland & Hopkins FB 1692  
31



Revised 4-21-48

(CUB)

1+83.88 Δ Rt 33°39' sec. on split

174 <sup>4</sup>	172 <sup>43</sup>	173 <sup>8</sup>	175 <sup>00</sup>	179 <sup>0</sup>
72	914	78	66	26
20	on H. 6	8	14	21

1+54

174 <sup>3</sup>	173 <sup>6</sup>	174 <sup>1</sup>	174 <sup>8</sup>	175 <sup>4</sup>	174 <sup>4</sup>	174 <sup>8</sup>
73	80	75	68	62	22	18
21	19	15		7	11	20

1+48

174 <sup>5</sup>	174 <sup>0</sup>	174 <sup>3</sup>	175 <sup>3</sup>	176 <sup>3</sup>	178 <sup>2</sup>
71	76	73	63	53	34
20	18	14		8	30

1+25

175 <sup>9</sup>	175 <sup>7</sup>	175 <sup>1</sup>	176 <sup>0</sup>	177 <sup>2</sup>	178 <sup>6</sup>
57	59	65	56	44	30
20	8	5		8	20

1+00

178 <sup>2</sup>	177 <sup>2</sup>	176 <sup>6</sup>	178 <sup>0</sup>	178 <sup>6</sup>
34	34	50	36	30
20	7		18	19

TR 113 181.57 12.34 180.44

181.57

0+50

180 <sup>6</sup>	179 <sup>6</sup>	179 <sup>4</sup>	180 <sup>4</sup>	183 <sup>5</sup>
122	132	134	124	93
20	10		10	20

192.78

192.78



~ Paradise Hills ~ Blk. 15, 16  
 Drain Cross Sections

TP 0.52 168.96 1313 168.44

Δ Rt 5015'

2+97.18 = Face of Hd. Wall sec. Parallel to Hd. Wall

2+76

2+50

2+30

2+24

2+00

181.57

Reduced 4-21-58

(C.S.)

170 <sup>4</sup>	169 <sup>7</sup>	169 <sup>2</sup>	168 <sup>40</sup>	165 <sup>44</sup>	169 <sup>2</sup>
11.2 20	11.2 13	12.4 8	13.7 on Hd. Wall	14.3 0	12.4 17
				Flowline	

171 <sup>4</sup>	170 <sup>7</sup>	168 <sup>1</sup>	168 <sup>1</sup>	169 <sup>4</sup>	173 <sup>1</sup>	173 <sup>6</sup>
10.2 20	10.2 11	13.5 8	12.5 9	12.2	8.5 10	8.0 20

172 <sup>3</sup>	171 <sup>6</sup>	169 <sup>9</sup>	170 <sup>9</sup>	170 <sup>8</sup>	171 <sup>5</sup>	176 <sup>1</sup>	176 <sup>5</sup>
9.3 20	10.0 13	11.7 6 Ditch	10.7 3	10.8	10.1 3	5.5 13	5.1 20

172 <sup>8</sup>	171 <sup>7</sup>	171 <sup>2</sup>	172 <sup>6</sup>	173 <sup>0</sup>	178 <sup>0</sup>	178 <sup>6</sup>
8.8 20	9.9 9	10.4 1 Ditch	9.0	8.6 3	3.6 19	3.0 25

173 <sup>0</sup>	172 <sup>3</sup>	171 <sup>2</sup>	172 <sup>8</sup>	174 <sup>0</sup>	178 <sup>3</sup>
8.6 20	9.3 8	10.4 Ditch	8.8 2	7.6 8	3.3 20

173 <sup>6</sup>	172 <sup>8</sup>	172 <sup>3</sup>	172 <sup>3</sup>	174 <sup>0</sup>	175 <sup>3</sup>	178 <sup>8</sup>	178 <sup>9</sup>
8.0 20	8.8 5	9.3	9.3 4	7.6 6	6.3 12	2.8 19	3.7 25

181.57



4+00

3+65

3+58.1 opp end East 18" Pipe

3+53 Sec Parallel to cb

3+42.5 = Δ RH

3+41.5 = WLY cb

3+25.5 = L Paving

3+08.9

3+07.2

3+07 = ELY cb

#

Revised 4-21-48 *(initials)*

165 <sup>6</sup>	160 <sup>8</sup>	159 <sup>6</sup>	160 <sup>9</sup>	162 <sup>1</sup>	163 <sup>1</sup>
3.4	8.2	9.4	8.1	6.9	5.9
20	3	2		6	20

161 <sup>0</sup>	162 <sup>0</sup>	162 <sup>2</sup>	163 <sup>0</sup>	165 <sup>1</sup>
2.0	7.0	6.8	6.0	3.9
20	7	2		19

164 <sup>8</sup>	166 <sup>3</sup>	162 <sup>8</sup>	163 <sup>7</sup>	163 <sup>5</sup>	167 <sup>6</sup>
10.8	2.7	6.2	5.7	5.5	1.4
23	15	5	3.4		10

168 <sup>0</sup>	167 <sup>6</sup>	167 <sup>6</sup>
1.0	1.4	1.8
20		20

167 <sup>66</sup>	160 <sup>63</sup>	164 <sup>22</sup>
1.30	2.33	4.74
on cb	0	0
	Grading	Flow inlet Box

167<sup>66</sup>  
1.00  
Paving

167 <sup>94</sup>	164 <sup>75</sup>	167 <sup>43</sup>
1.92	4.21	1.53
cb	0	0
	Flow	inlet Box

168<sup>96</sup>



Paradise Hills - Drains

5+05

5+04

TP 127 157.61 1262 156.34

4+99.31 =  $\Delta$  17 28°06'45" Sec on split

4+89

4+86

4+70

4+50

67

153<sup>8</sup>

38

Reduc 4-21-48

~~CHP~~

156<sup>0</sup>

16

157.61

157 <sup>7</sup>	155 <sup>8</sup>	154 <sup>2</sup>	155 <sup>9</sup>	156 <sup>34</sup>	158 <sup>4</sup>
93	132	12.8	131	1262	10.6
25	6	4 ditch	3	on Hub	20

156<sup>8</sup>

122

155<sup>7</sup>

133

ditch

162 <sup>7</sup>	158 <sup>2</sup>	157 <sup>5</sup>	156 <sup>6</sup>	158 <sup>2</sup>	159 <sup>3</sup>
63	10.8	11.5	12.9	10.9	9.7
25		2	3	5	20

163<sup>3</sup>

5.7

18

162<sup>0</sup>

7.0

8

159<sup>8</sup>

92

168.26

159<sup>1</sup>

9.9

3

157<sup>9</sup>

11.1

ditch

159<sup>2</sup>

9.8

6

160<sup>6</sup>

8.4

20



Paradise Hills - Drain Blocks  
15.16  
Cross Sections

6+54.84 = Conc Slab Inlet 4" Curbing

T.P. 1.84 146.88 12.57 145.04

6+47

6+38

6+00

5+68

5+25

157.61

4

4

FF

68

Reduced 4.21.48 (2413)

47	74	
143	144	144 <sup>26</sup>
3.41	2.14	2.62
Flow	0	0
	cb	on slab
	inlet	

146.88

148 <sup>5</sup>	148 <sup>5</sup>	147 <sup>1</sup>	145 <sup>1</sup>	147 <sup>0</sup>	147 <sup>3</sup>
91	81	105	125	10.6	10.3
20	10	2			20

157	150 <sup>7</sup>	149 <sup>7</sup>	148 <sup>4</sup>	149 <sup>6</sup>	149 <sup>7</sup>
59	6.9	7.9	9.2	8.0	7.9
20	13	8	6		20

154 <sup>5</sup>	151 <sup>4</sup>	150 <sup>1</sup>	150 <sup>8</sup>	151 <sup>2</sup>	151 <sup>6</sup>
3.1	6.2	7.5	6.8	6.4	6.1
20	6	4		4	20

156 <sup>0</sup>	152 <sup>9</sup>	151 <sup>5</sup>	151 <sup>9</sup>	153 <sup>1</sup>	153 <sup>1</sup>
16	4.7	6.1	5.7	4.5	4.5
20	5	3		6	

158 <sup>9</sup>	157 <sup>9</sup>	154 <sup>2</sup>	152 <sup>7</sup>	152 <sup>7</sup>	154 <sup>9</sup>	153 <sup>8</sup>
+1.3	+0.3	3.4	4.9	4.9	2.7	1.8
26	18	2		3	4	20

157.61



Paradise Hills - Blocks 15, 16  
 Drain Cross Sections

8+00

7+50

7+16

7+00

6+69.79 = Δ RT 87°35'45"

6+68.79

6+64.8 - FLY cb line Rachel

146.88

4

6

RT

69

Revised 4-21-48

140 <sup>0</sup>	139 <sup>8</sup>	139 <sup>70</sup>	139 <sup>53</sup>	140 <sup>29</sup>
69	71	71.8	7.25	6.59
10		1.5	5	5
		Lip.	Gut	cb.

140 <sup>8</sup>	140 <sup>5</sup>	140 <sup>21</sup>	139 <sup>98</sup>	140 <sup>68</sup>
61	64	6.57	6.20	6.20
10		1.5	5	5
		Conc.	Gut	cb.

141 <sup>8</sup>	141 <sup>2</sup>	141 <sup>66</sup>	140 <sup>67</sup>	141 <sup>37</sup>
51	57	5.82	6.26	5.51
10		1.5	5	5
		on Conc.	Gut	cb
		Lip.		

142 <sup>5</sup>	141 <sup>9</sup>	141 <sup>69</sup>	141 <sup>32</sup>	142 <sup>03</sup>
4.4	50	5.19	5.56	4.85
10		1.5	5	5
			Gut	cb

143<sup>53</sup>  
 3.35  
 on Hub

143<sup>55</sup>  
 3.33

143 <sup>22</sup>	144 <sup>42</sup>	144 <sup>00</sup>	143 <sup>28</sup>	143 <sup>60</sup>	142 <sup>89</sup>
3.16	3.4.6	2.88	3.60	3.2.8	3.99
5	5	5	5	5	5
Gut Flow	cb	cb	Flow	cb	Flow

146.88



Paradise Hills - Drain

9+67.4 = End Bridge

9+49.6 = Lt

= NLY end Bridge

9+35

8+75.75 = Lt 7°27'

= End 30" Pipe

8+60

on Hd Wall of "A"

8+41.41 = Lt 129°06'30"

146.88

4 2 Reduced 4-21-48 70

139 <sup>9</sup>	139 <sup>9</sup>	135 <sup>0</sup>	135 <sup>0</sup>	135 <sup>0</sup>	139 <sup>9</sup>	139 <sup>9</sup>
7.0	7.0	11.9	11.9	11.9	7.0	7.0
10	3	2.9		0.6	0.7	10

140 <sup>2</sup>	139 <sup>9</sup>	135 <sup>2</sup>	135 <sup>4</sup>	135 <sup>2</sup>	139 <sup>9</sup>	140 <sup>2</sup>
6.7	7.0	11.7	11.5	11.7	7.0	6.7
10	3	2		2	3	10

Bridge Floor

136 <sup>8</sup>	138 <sup>0</sup>	136 <sup>2</sup>	136 <sup>2</sup>	136 <sup>2</sup>	138 <sup>0</sup>	138 <sup>5</sup>
10.1	8.9	10.7	10.7	10.7	8.9	8.4
10	2	1.3		1.3	2	10

139 <sup>5</sup>	136 <sup>3</sup>	134.65	138 <sup>1</sup>	139 <sup>0</sup>
7.4	10.6	12.3	8.8	7.9
10	0	Flow	2	10

Ditch Partly Filled 30" Pipe

139 <sup>7</sup>	139 <sup>6</sup>	139 <sup>7</sup>
7.2	7.3	7.2
10		10

139 <sup>90</sup>	135 <sup>40</sup>
6.98	11.48

on Hd Wall "A" Flowline 30" Pipe

139 <sup>48</sup>	139 <sup>22</sup>	140 <sup>04</sup>	139 <sup>00</sup>	135 <sup>08</sup>
7.40	7.66	6.84	7.88	11.80

Lip 6' 6" Grating box

146.88



Paradise Hills - Drain

H

←

RT

71

Reduced 4-21-48

(CWP)

9+90

146.88

135.3

136.9

134.9

134.9

138.4

140.9

11.6

10.0

12.0

12.0

8.5

6.0

18

3

2.3

Flow

1

10

Ditch

Ditch

Wedge

146.88

E edge

146.88

146.88



## Paradise Hills

Levels - Alternate line sketch P.62

from 6+6979 to 8+058

4

2

177

72

Redund 4-21-58

(CND)

8+03

$$\begin{array}{r} 3 \\ 135 \\ 146 \\ 10 \end{array}$$

$$\begin{array}{r} 4 \\ 135 \\ 115 \end{array}$$

$$\begin{array}{r} 2 \\ 135 \\ 117 \\ 10 \end{array}$$

7+62

$$\begin{array}{r} 6 \\ 136 \\ 109 \\ 10 \end{array}$$

$$\begin{array}{r} 5 \\ 135 \\ 114 \end{array}$$

$$\begin{array}{r} 5 \\ 135 \\ 114 \end{array}$$

7+50

$$\begin{array}{r} 4 \\ 139 \\ 75 \\ 10 \end{array}$$

$$\begin{array}{r} 4 \\ 139 \\ 75 \end{array}$$

$$\begin{array}{r} 2 \\ 139 \\ 77 \\ 10 \end{array}$$

7+20

$$\begin{array}{r} 9 \\ 138 \\ 80 \\ 20 \end{array}$$

$$\begin{array}{r} 0 \\ 139 \\ 79 \end{array}$$

$$\begin{array}{r} 1 \\ 139 \\ 78 \\ 10 \end{array}$$

7+17

$$\begin{array}{r} 1 \\ 141 \\ 4.8 \\ 10 \end{array}$$

$$\begin{array}{r} 3 \\ 142 \\ 4.6 \end{array}$$

$$\begin{array}{r} 5 \\ 141 \\ 3.9 \\ 10 \end{array}$$

6+90

$$\begin{array}{r} 0 \\ 149 \\ 2.9 \\ 10 \end{array}$$

$$\begin{array}{r} 4 \\ 143 \\ 3.5 \end{array}$$

$$\begin{array}{r} 9 \\ 142 \\ 4.0 \\ 10 \end{array}$$

6+69.79 = P.O.T. this line

146.88

146.88



Paradise Hills - Drain  
Cross Sections

Cont. from P-71

Rachel & Cumberland

chk. S.E. RP	1.97	152.31	181692
		152.32	30
T.P.	2.25	154.29	1.84
			145.04

8 + 0.8

146.88  
5

73

Reduced 4-21-48

~~(C.C.B.)~~

134 <sup>3</sup>	134 <sup>2</sup>	134 <sup>3</sup>
12.6	12.7	12.6
10 in ditch	10 in ditch	10 ditch
	146.88	
	5	





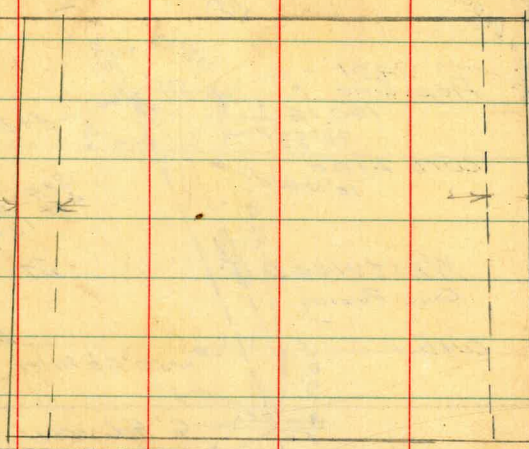


5-10-48

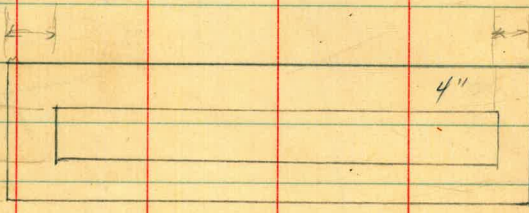
(CGO)



curb  
line  
Rachae  
St.



Property  
Line





Location of House<sup>And</sup> Garage  
 on N<sup>1</sup>/<sub>2</sub> Lot 8, and Lot 7  
 Block 16 - Paradise Hills.

Walker  
 Johnson  
 Allen  
 Gregory (Frank)  
 6-30-48

No. 80098

Cumberland St.



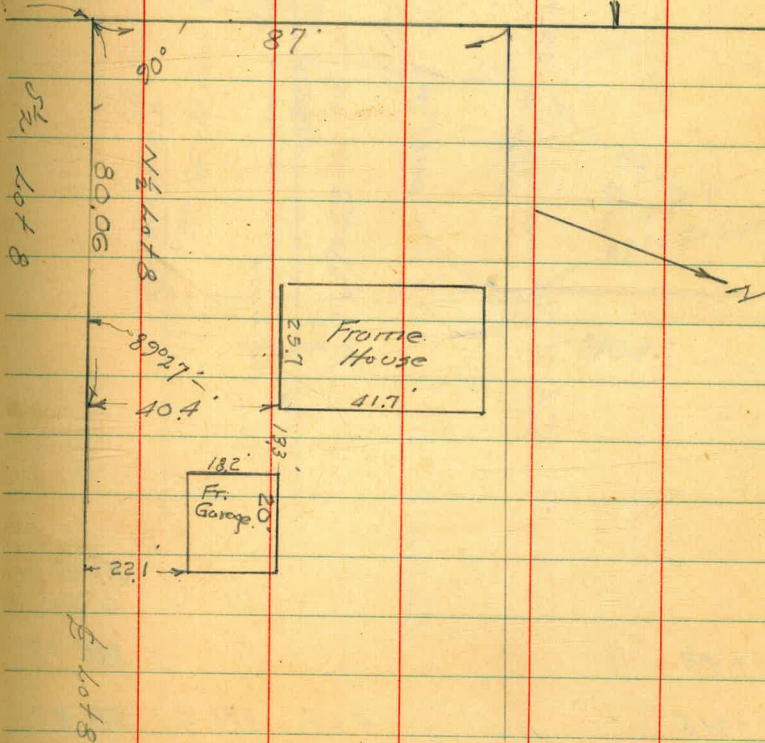
INDEXED  
 W K  
 JAN 6 1949

76

Lot 13  
 2" Pipe

Westwood

50 St.

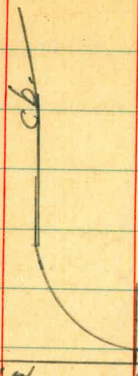








Winona St.



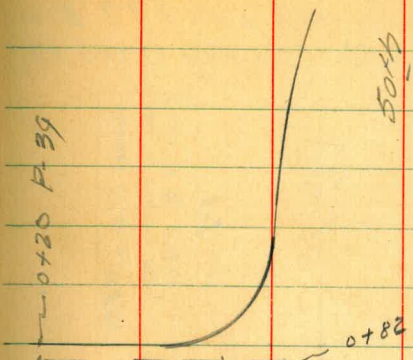
Grades Drain Tile  
Collier 50+6

Flux 6 Drain 12.5 below Gutter

Collier

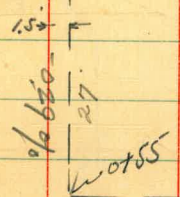
cb.

1+205		390.41	389.16
1+00.5	4.81	390.30	389.10
0+82	4.69	390.42	389.05
0+55	4.93	390.18	388.97
0+27.5	5.04	390.07	388.89
0+00	6.30	389.81	388.81
4.75	395.11	390.36	B.M.



Walker  
Johnson  
Gregory  
Stamps  
6-9-48

6" Drain 0.29%



Collier St.

6" Drain

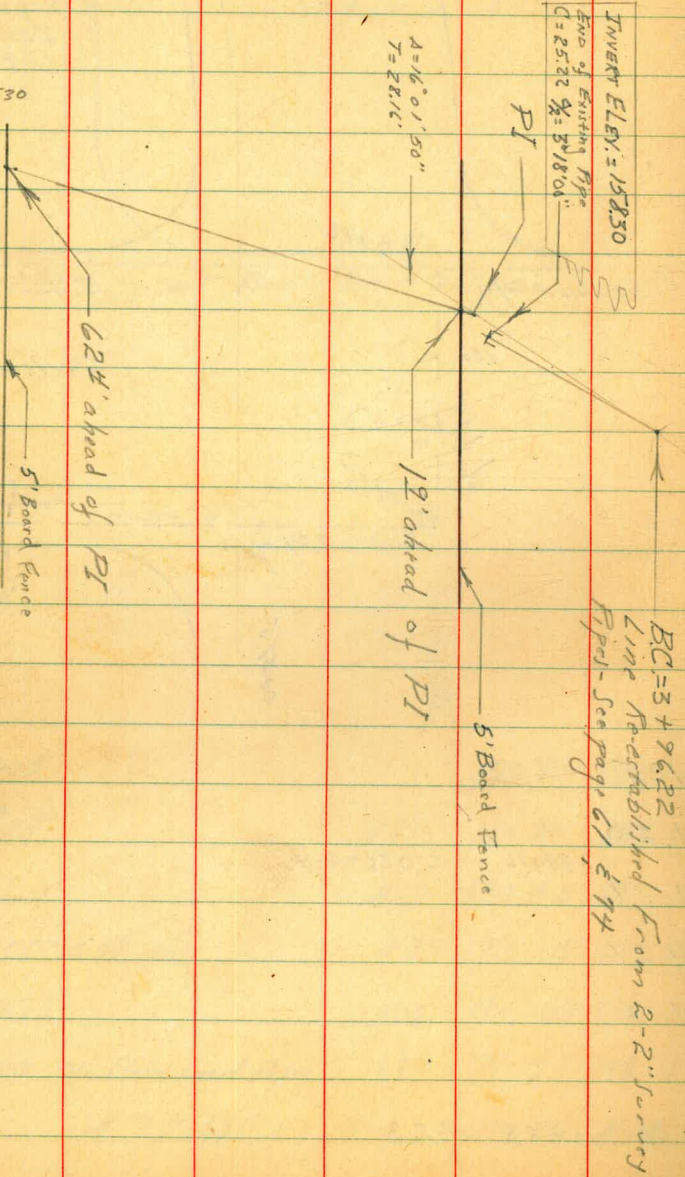
C 1.25	
C 1.20	390.16 - C 0.26 = Gut.
C 1.87	
C 1.21	
C 1.18	
on cb	10+88 P. 2.8

Existing  
End. 6" Drain Tile  
0+00



Location of Improvements in  
Storm Drain Easements Lots 8 & 9 Block  
15 Paradise Hills (See page 61 this FB.)

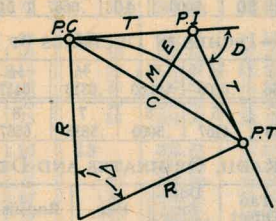
Roberts  
Cata  
Moore  
Pulley  
5-17-51  
W.O. 20530





# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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### CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve= $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)
- Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)
- Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)
- External= $E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)
- Long Chord= $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

### EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I. —  $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance =  $158 - \text{Sta. P. C.} = 54.50$ , hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$  and from Table V correction = .10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .



TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II.—INCHES IN DECIMALS OF A FOOT.

1/16	3/32	1/8	3/16	1/4	5/16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Deg.	Radius	Mid. Ord.	Tan Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan Offset	Def. for 1 Foot
0° 10'	34377.5	.036	.145	0.05'	7°	819.02	1.528	6.105	2.10'
20	17188.8	.073	.291	0.10	20	781.84	1.600	6.395	2.20
30	11459.2	.109	.436	0.15	30	764.49	1.637	6.540	2.25
40	8594.42	.145	.582	0.20	40	747.89	1.673	6.685	2.30
50	6875.55	.182	.727	0.25					
1 10	5729.65	.218	.873	0.30	8 20	716.78	1.746	6.976	2.40
20	4911.15	.255	1.018	0.35	30	688.16	1.819	7.266	2.50
30	4297.28	.291	1.164	0.40	40	674.69	1.855	7.411	2.55
40	3819.83	.327	1.309	0.45					
50	3437.87	.364	1.454	0.50	9 20	637.28	1.965	7.846	2.70
	3125.36	.400	1.600	0.55	30	614.56	2.037	8.136	2.80
2 10	2864.93	.436	1.745	0.60	40	603.80	2.074	8.281	2.85
20	2644.58	.473	1.891	0.65		593.42	2.110	8.426	2.90
30	2455.70	.509	2.036	0.70	10 30	573.69	2.183	8.716	3.00
40	2292.01	.545	2.181	0.75		546.44	2.292	9.150	3.15
50	2148.79	.582	2.327	0.80	11 30	521.67	2.402	9.585	3.30
	2022.41	.618	2.472	0.85	40	499.06	2.511	10.02	3.45
3 10	1910.08	.655	2.618	0.90	12 30	478.34	2.620	10.45	3.60
20	1809.57	.691	2.763	0.95		459.28	2.730	10.89	3.75
30	1719.12	.727	2.908	1.00	13 30	441.68	2.839	11.32	3.90
40	1637.28	.764	3.054	1.05		425.40	2.949	11.75	4.05
50	1562.88	.800	3.199	1.10	14 30	410.28	3.058	12.18	4.20
	1494.95	.836	3.345	1.15		396.20	3.168	12.62	4.35
4 10	1432.69	.873	3.490	1.20	15 30	383.07	3.277	13.05	4.50
20	1375.40	.909	3.635	1.25		370.78	3.387	13.49	4.65
30	1322.53	.945	3.718	1.30	16 30	359.27	3.496	13.92	4.80
40	1273.57	.982	3.926	1.35		348.45	3.606	14.35	4.95
50	1228.11	1.018	4.071	1.40	17 30	338.27	3.716	14.78	5.10
	1185.78	1.055	4.217	1.45	18 30	319.62	3.935	15.64	5.40
5 10	1146.28	1.091	4.362	1.50	19 30	302.94	4.155	16.51	5.70
20	1109.33	1.127	4.507	1.55	20 20	287.94	4.374	17.37	6.00
30	1074.68	1.164	4.653	1.60	21 20	274.37	4.594	18.22	6.30
40	1042.14	1.200	4.798	1.65	22 20	262.04	4.814	19.08	6.60
50	1011.51	1.237	4.943	1.70	23 20	250.79	5.035	19.94	6.90
	982.64	1.273	5.088	1.75	24 20	240.49	5.255	20.79	7.20
6 10	955.37	1.309	5.234	1.80	25 20	231.01	5.476	21.64	7.50
20	929.57	1.346	5.379	1.85	26 20	222.27	5.697	22.50	7.80
30	905.13	1.382	5.524	1.90	27 20	214.18	5.918	23.35	8.10
40	881.95	1.418	5.669	1.95	28 20	206.68	6.139	24.19	8.40
50	859.92	1.455	5.814	2.00	29 20	199.70	6.360	25.04	8.70
					30 20	193.18	6.583	25.88	9.00

NOTE. Chord Deflection=2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1° 10'	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
20	58.34	.30	10'	560.11	27.31	10'	1070.2	99.16
30	66.67	.39	20	568.53	28.14	20	1079.2	100.75
40	75.01	.49	30	576.95	28.97	30	1087.8	102.35
50	83.34	.61	40	585.36	29.82	40	1096.4	103.97
	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2 10	100.01	.87	12	602.21	31.56	22	1113.7	107.24
20	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
30	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
40	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
50	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3 10	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
20	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
30	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
40	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
50	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4 10	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
20	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
30	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
40	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
50	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5 10	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
20	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
30	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
40	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
50	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6 10	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
20	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
30	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
40	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
50	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7 10	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
20	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
30	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
40	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
50	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8 10	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
20	409.03	14.58	10	916.05	72.76	10	1437.4	177.55
30	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
40	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
50	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9 10	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
20	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
30	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
40	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
50	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10 10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
20	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
30	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
40	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
50	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86



1470  
0490



392.06  
562  
397.68

509  
392.59

18407  
518  
392.50  
525  
392.43

388

352.73  
146.18  
499.31

1448 388.66

1477.5 71

126  
149.51 70

2112.7 388.77

1231  
511.62

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) \* 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.