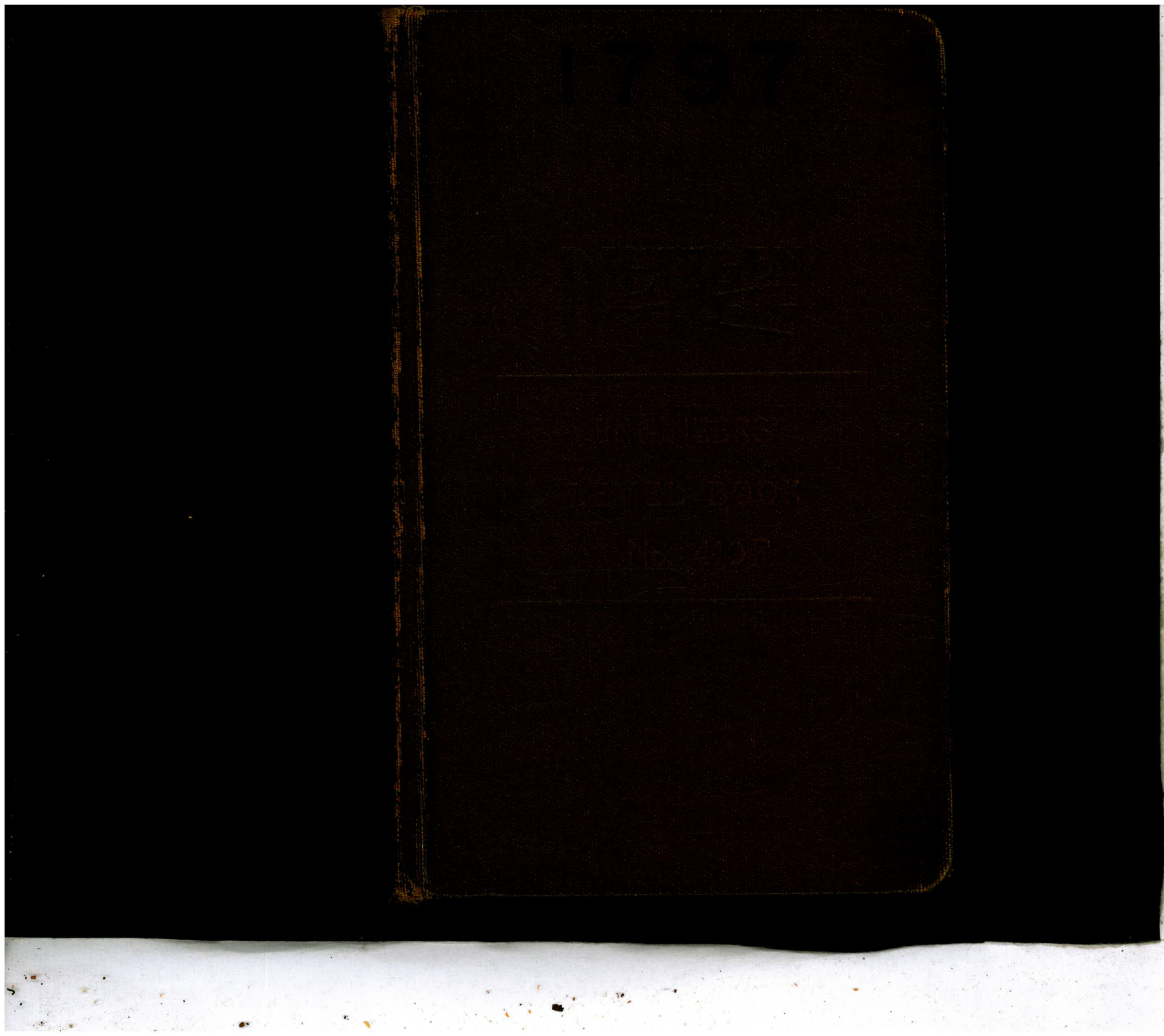


Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Page

Survey Soledad Rd.
Line change

Moore
8c99
Graeme
Roberts
9-2-47

W.O. 90058

Ref. F.B. 1672-27 ✓

" " 1324.46

" " 984

" " 1094

" " 1067

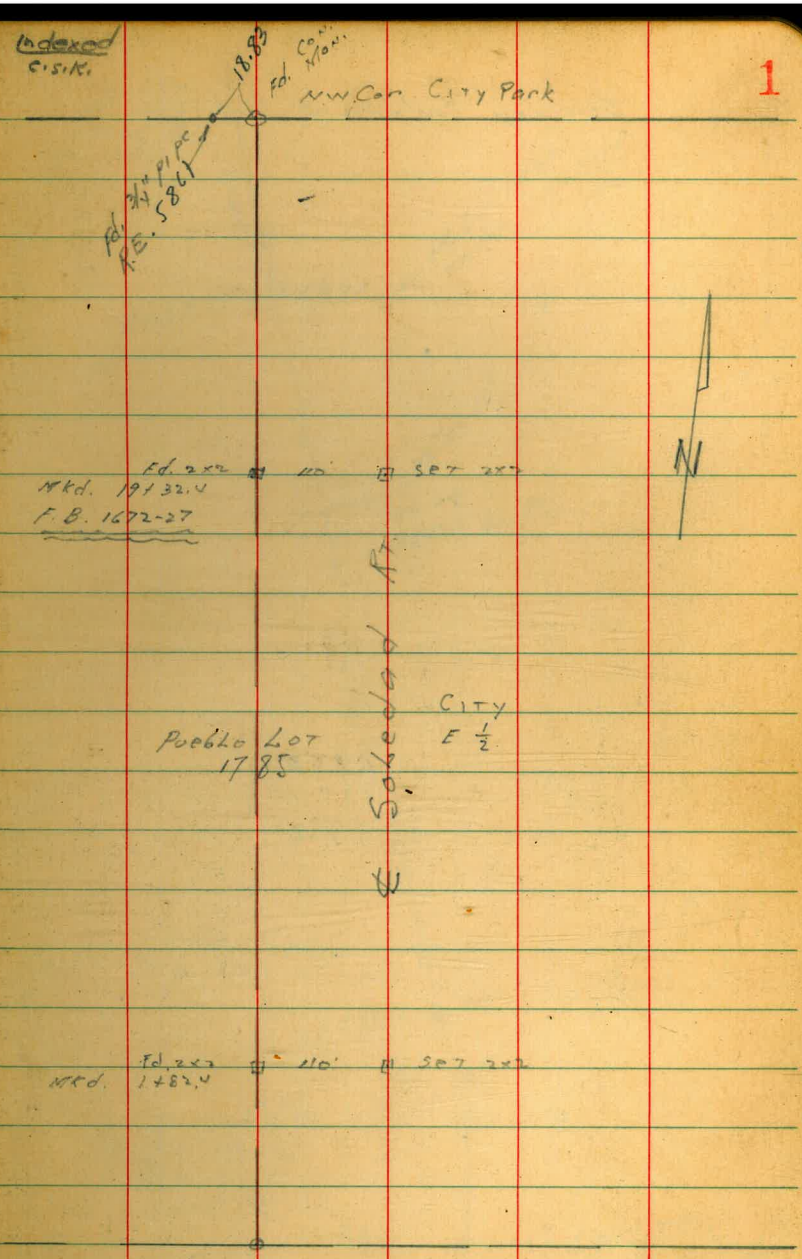
" " 1334

" " 1291

" " 1498

" " 1408-54

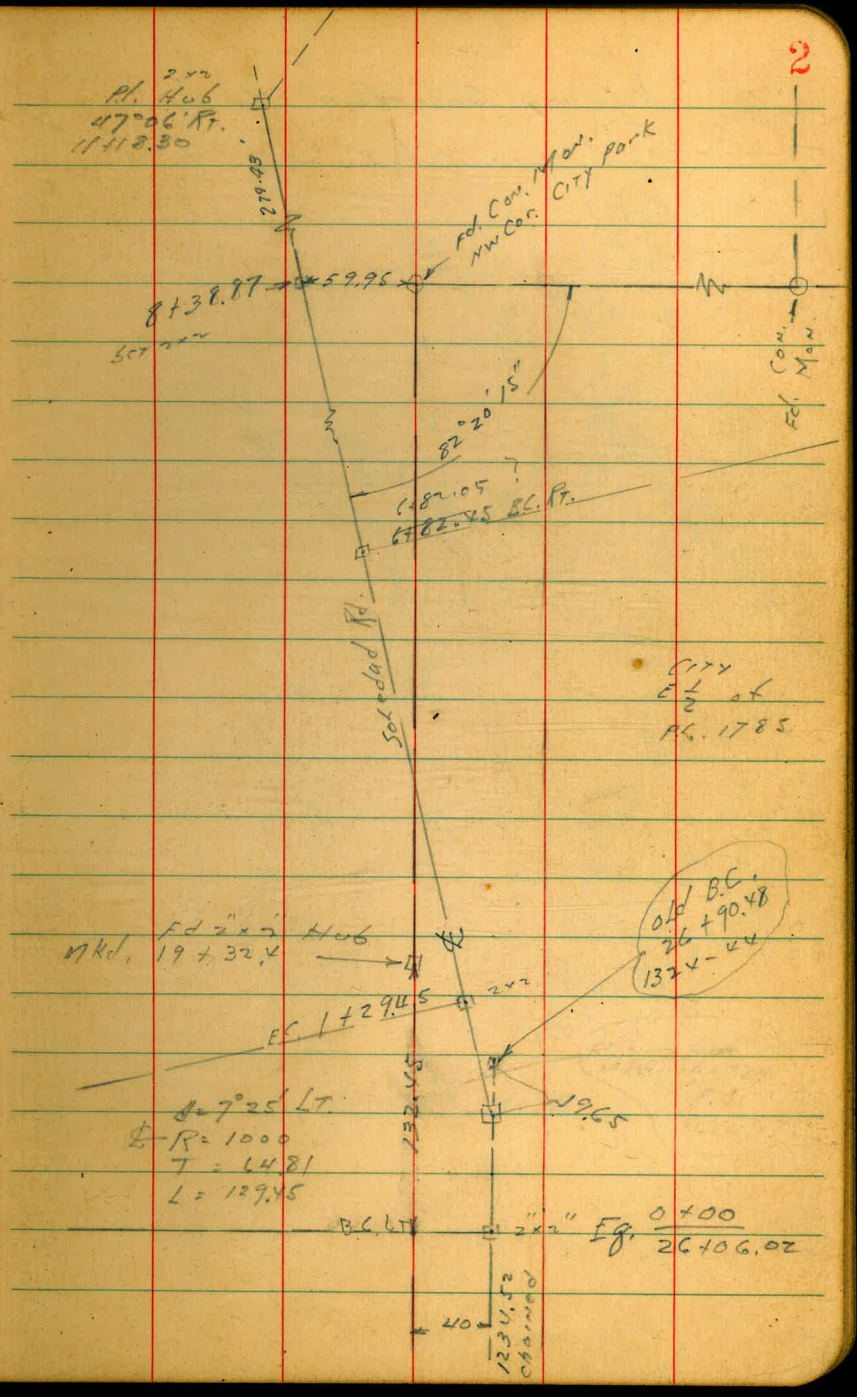
Indexed
C.S.M.



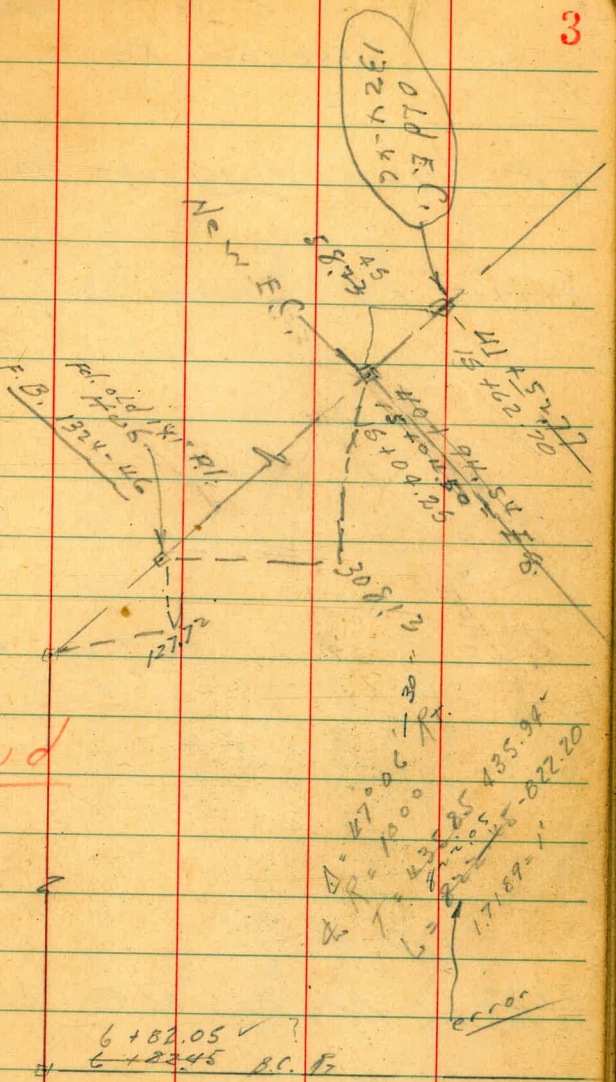
1

Survey Soledad Rd.

682.05
129.45
552.60



Survey Soledad Rd.
Line change.



6+82.45
8+20.5
150+.50

8+20.49
6+82.05
150+4.10

X sec Line Change
Soledad Rd.

T.P.	12.10	341.96	2.68	329.86	
1+29.45	E.C.	44' Lt 24" di. acasia tree			
1					
0+65	38' Lt Tel Pole	477715 H			
0+50					4.3 / 50
0+00 = 26+06.02	= Eq. = New BC. Lt.	Sketch p.r			
B.M. 3/4" Pipe 40' Lt. of old sta. 25+06	12.75	332.54		319.79 ?	
	1408-54				

Lt = West — ℄ — Rt

+1.4 / 50	+0.8 / 40 (33.3)	0.6 / 28 (31.9)	0.9 / 5 (31.6)	2.3 (30.2)	2.0 / 25 (30.5)	4.2 / 40 (28.3)	5.0 / 50 (27.5)	6.3 / 50	
0.9 / 50	1.8 / 40 (30.7)	2.3 / 7 (30.2)	3.3 (29.2)	3.4 / 24 (29.1)	5.2 / 40 (27.3)	5.8 / 50			
4.6 / 40 (27.9)	5.4 / 35 (27.1)	5.3 / 24 (27.2)	4.8 / 6 (27.7)	5.6 / 3 (26.9)	6.0 (26.5)	5.5 / 19 (27.0)	4.6 / 20 (27.9)	5.1 / 40 (27.4)	5.1 / 50
7.5 / 50	7.9 / 40 (24.6)	7.9 / 33 (24.6)	7.1 / 7 (25.4)	8.2 / 4 (24.3)	8.2 (24.3)	8.3 / 15 (24.2)	6.8 / 16 (25.7)	6.4 / 40 (26.1)	6.5 / 50

332.54

+69	3' Rt	Tel. P.	477717 H		
+50					
T.P.	12.70	354.41	0.25	341.71	
3					
+78	54 Lt	28" di. Eucal. tree			
+50					
2+00					
1+50					
1+43	72' Lt	20'x20' Bd. & Bar. house			
		341.96			

	Lt			℄			Rt		
	45.8	44.2	42.5	42.3	43.5	42.1	37.5	36.3	
8.3/50	8.6/40	10.2/20	11.9/18	12.1	10.9/2	12.3/7	16.9/40	18.1/50	
				354.41					
	40.9	40.4	39.3	38.6	38.7	39.2	35.6	33.9	
0.8/50	1.1/40	1.6/24	2.7/15	3.4	3.3/x	2.8/6	6.4/40	8.1/50	
	38.4	36.6	35.8	35.9	36.5	36.3	34.3	32.9	
3.4/50	3.6/40	5.4/16	6.2	6.1/11	5.5/13	5.7/23	7.7/40	9.1/50	
	36.0	35.4	33.8	33.3	33.0	33.7	34.2	31.7	30.1
6.3/50	6.0/40	6.6/22	8.2/3	8.7/2	9.0	8.3/22	7.8/24	10.3/40	11.9/50
	34.2	33.6	32.8	31.1	31.2	31.3	31.7	28.8	28.2
7.9/50	7.8/40	8.4/28	9.2/4	10.9/1	10.8	10.7/24	10.3/25	13.2/40	13.8/50
				341.96					

Station					Lt	℄	Rt
6					1.6/50; 2.0/40 (64.1); 2.5/36 (63.6); 2.1/32 (64.0); 2.4/19 (63.7); 3.5/16 (62.6); 3.9/5 (62.2); 6.9/1 (59.2)	7.1 (59.0)	7.5/18 (58.6); 12.0/40 (54.1); 16.2/50 (49.9); 20.3/60 (45.8)
+50					5.5/50; 6.2/40 (59.9); 7.4/11 (58.7); 10.7/7 (55.4)	10.6 (55.5)	10.7/11 (55.4); 10.1/12 (56.0); 16.0/31 (50.1); 21.3/40 (44.8); 29.1/50 (37.0) — Same Rate
5					9.3/50; 9.5/40 (56.6); 11.2/16 (54.9); 13.7/12 (52.4)	13.9 (52.2)	13.9/5 (52.2); 13.2/6 (52.9); 15.5/11 (50.6); 22.9/40 (43.2); 28.8/50 (37.3) — Same Rate slope for 70' Rt
T.P.	12.04	366.11	0.34	354.07		366.11	
+50					0.8/50; 1.4/40 (53.0); 1.5/31 (52.9); 2.9/24 (51.5); 2.1/19 (52.3); 4.5/16 (49.9)	4.9 (49.5)	4.9/1 (49.5); 3.4/4 (51.0); 11.7/32 (42.7); 19.0/40 (35.4); 21.9/50 (32.5) — Same Rate slope for 70 Rt
4+00					4.7/50; 5.0/40 (49.4); 6.1/22 (48.3); 8.1/19 (46.3)	8.2 (46.2)	6.4/2 (48.0); 12.6/40 (41.8); 16.0/50 (38.4); 19.3/60 (35.1)
		354.41				354.41	

Sta.						Lt — ℄ — Rt
8					5.4/50	5.9/40 (82.8); 6.1/31 (82.6); 7.0/23 (81.7); 9.9/20 (78.8); 7.7/17 (81.0); 7.6/2 (81.1); 8.1 ℄ (80.6); 10.9/3 (77.8); 10.1/26 (78.6); 9.6/27 (79.1); 12.9/35 (75.8); 14.1/40 (74.6); 15.3/50 (73.4)
T.P.	11.25	388.70	0.63	377.45		388.70
+50					+0.8/50; 0.0/40 (78.1); 0.3/32 (77.8)	2.8/23 (75.3); 1.7/20 (76.4); 1.2/5 (76.9); 1.8/3 (76.3); 2.7/1 (75.4); 2.8 ℄ (75.3); 2.8/3 (75.3); 5.6/6 (72.5); 3.4/8 (74.7); 5.6/10 (72.5); 4.4/30 (73.7); 3.6/33 (74.5); 5.5/40 (72.6); 8.1/50 (70.0)
7					4.0/50	4.4/40 (73.7); 6.1/17 (72.0); 8.5/14 (69.6); 6.4/12 (71.7); 6.2/8 (71.9); 8.3/5 (69.8); 7.5 ℄ (70.6); 7.3/5 (70.8); 9.7/7 (68.4); 9.5/29 (68.6); 8.3/30 (69.8); 10.5/40 (67.6); 12.7/50 (65.4)
6+82.45	B.C. Rt.				5.6/50	6.2/40 (71.9); 7.5/19 (70.6); 9.3/17 (68.8); 7.9/15 (70.2); 7.5/10 (70.6); 9.3/8 (68.8); 8.78/4.6 (69.30); 8.8/4 (69.3); 11.5/7 (66.6); 11.6/26 (66.5); 10.7/27 (67.4); 13.9/35 (64.2); 15.2/40 (62.9); 16.4/50 (61.7)
+71	41 Rt.	Tel. P.	47 7716	H		
6+50						8.5/50; 9.1/40 (69.0); 10.9/13 (67.2); 12.4/7 (65.7); 11.8/4 (66.3); 11.9 ℄ (66.2); 12.0/2 (66.1); 14.7/5 (63.4); 15.6/25 (62.5); 19.5/40 (58.6); 22.0/50 (56.1)
T.P.	12.02	378.08	0.05	366.06		378.08
		366.11				

							Lt	℄	Rt
+50							10.7/50 (02.9) 10.7/40 (01.6) 12.0/39 (00.4) 13.2/17 (01.8) 11.8/15	(01.6) 12.0	(400.0) 13.6/15 (01.1) 12.5/19 (00.8) 12.8/40 12.8/50
T.P.	12.73	413.64	0.52	400.91				413.64	
10					0.4/50	1.6/40 Fence 39	(99.5) 1.9/34 (97.8) 3.6/32 (97.8) 3.6/23 (97.2) 4.2/11 (98.5) 2.9/9	(97.9) 3.5	(97.3) 4.1/2 (97.1) 4.3/40 5.3/50
+69	37 Rt	Tel. P.	477718 H						
+50					4.4/50	(96.4) 5.0/40	(95.7) 5.7/30 (93.7) 7.7/28 (94.0) 7.4/17 (93.3) 8.1/7 (92.5) 8.9/6 (94.3) 7.1/3	(93.9) 7.5	(94.3) 9.1/40 8.8/50
9						9.8/50	(91.2) 10.2/40 Fence/32 (91.2) 10.2/23 (89.2) 12.2/19 (89.6) 11.8/9	(88.8) 12.6	(88.9) 12.5/5 (90.2) 11.2/6 (84.7) 16.7/40 (20.7) 20.7/50
T.P.	12.95	401.43	0.22	388.48				401.43	
8+50						1.4/40	(87.3) 1.4/40 (87.3) 1.4/30 (86.4) 2.3/29 (85.4) 3.3/8 (83.7) 5.0/5	(83.9) 4.8	(83.1) 5.6/15 (84.4) 4.3/18 (79.0) 9.7/40 (77.1) 11.6/50
8+39	31' Lt	Beg. wire stock Fence							
		388.70						388.70	

13					12.2/50 11.8/40	11.2/29
T.P.	12.47	437.73	0.11	425.26		
+50					4.3/50	4.0/48
+32	42 Lt. To L.P. 477719 H					
12					2.4/50	2.4/46
T.P.	11.90	425.37	0.17	413.47		
+50						
+40	69 Lt. Δ Fence Line					
11					7.6/50 7.6/48	8.8/45
		413.64				

Lt			℄			Rt
25.5	24.2 24.9		24.5	24.6 25.9	24.9	
Fence/32 12.2/22	13.5/19 12.8/12		13.2	13.1/5 11.8/6	12.8/40	12.6/50
		437.73				
21.0 19.8	19.9 19.2	20.8	21.0	20.7		
4.4/32 5.6/30	5.5/22 6.7/8	4.6/6	4.4	4.7/40	4.7/50	
32.5 Fence						
14.7	14.8 13.6	15.9	15.7	15.3		
Fence/46 10.7/40	10.6/35 11.8/22	9.5/12	9.7	10.1/40	10.2/50	
		425.37				
10.0	08.9	10.6	10.3	10.8		
3.6/50	3.6/40 4.7/29	3.0/27	3.3	2.8/40	3.8/50	
04.8	04.6	06.6	05.7	05.1 05.8	06.1	
Fence/57	8.8/40 9.0/22	8.0/20	7.9	8.5/8 7.8/32	7.5/40	7.8/50
		413.64				

B.M. Con. Mon, 40' Lt. of 41+52.77		4.68	443.94	443.82 / 0.12
41+52.77 = old E.C.				
40+94.54				
15+04.50 = E8 = New E.C.				
+50				
T.P.	10.97	448.62	0.08	437.65
14				
13+50				
	437.73			

Lt. ℄ Rt.

2.4 ground 446?

7.8/50 — 7.0/40 (41.6) — Fence 2.1 — 5.2 (43.4) — 5.5/15 (43.1) — 7.1/18 (41.5) — 6.9/28 (41.7) — 6.9/29 (41.7) — 8.3/39 (40.3) — 6.9/40 (41.7) — 7.1/50

10.2/50 — 9.4/40 (39.2) — 8.8/19 (39.8) — 8.8/1 (39.8) — 9.3 (39.3) — 10.5/3 (38.1) — 10.5/7 (38.1) — 11.1/11 (37.5) — 10.7/19 (37.9) — 11.4/29 (37.2) — 10.7/32 (37.9) — 10.9/40 (37.7) — 11.0/50

448.62

2.8/50 — 2.5/40 (35.2) — Fence 7 — 1.7/2 (36.0) — 3.8 (33.9) — 3.6/12 (34.1) — 4.2/21 (33.5) — 3.1/24 (34.6) — 4.2/40 (33.5) — 4.5/50

7.0/50 — 7.0/40 (30.7) — 7.0/13 (30.7) — 8.8/9 (28.9) — 8.2 (29.5) — 8.8/13 (28.9) — 6.7/16 (31.0) — 8.0/20 (29.7) — 8.4/50

437.73

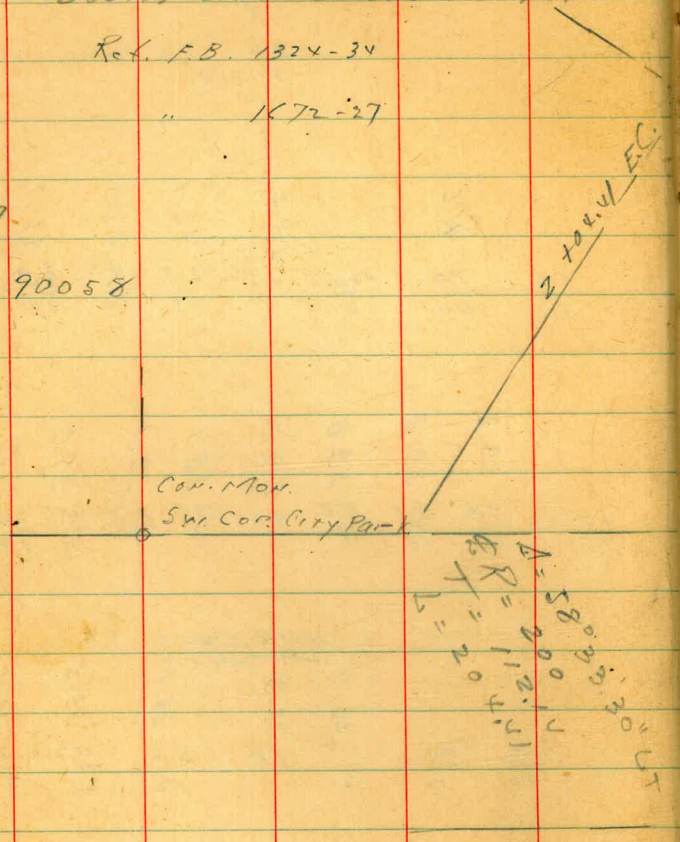
Proposed Line change
South end Soledad Rd.

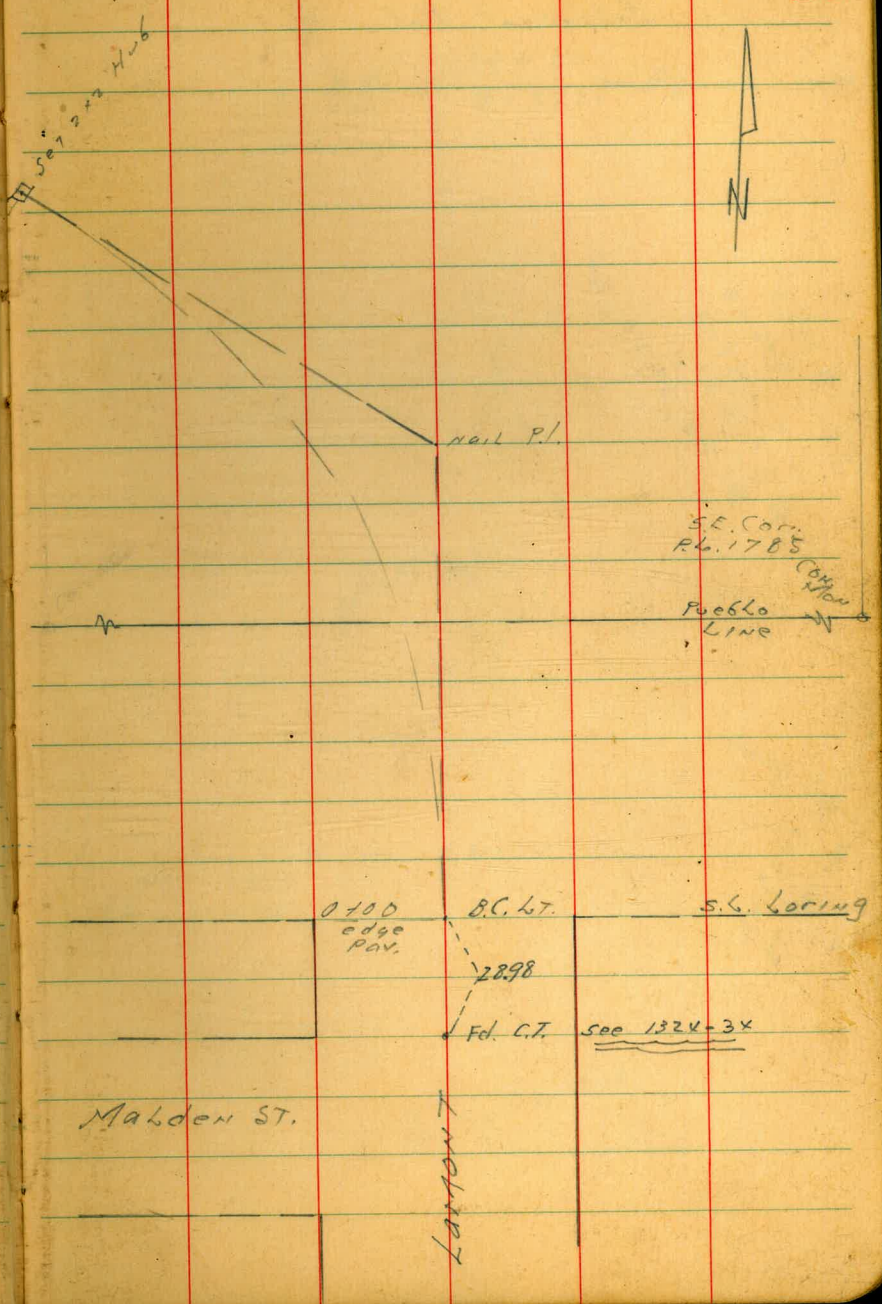
Ref. F.B. 1324-34

" 1472-27

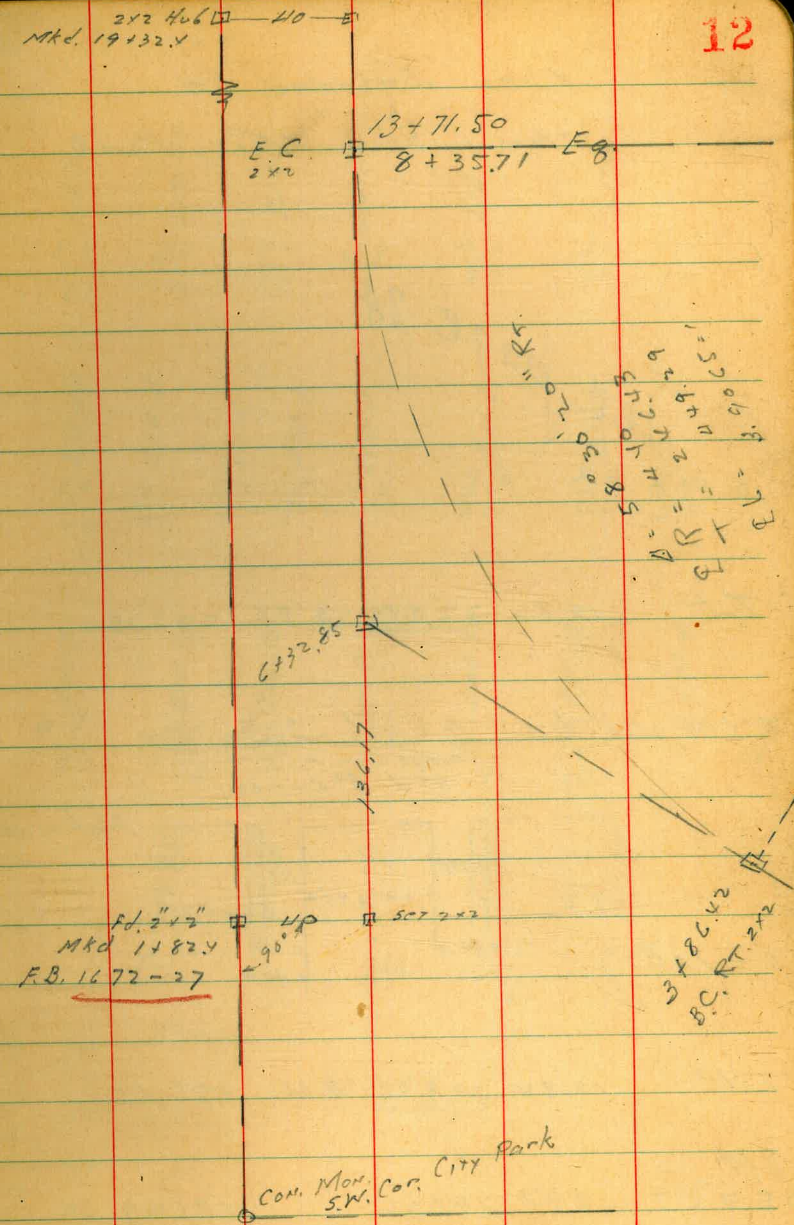
Moore
Begg
Green
Roberts
9-2-47

W.O. 90058





Soledad Rd.


2x2 Hub
40
Mkd. 19+32.4
E.C.
2x2
13+71.50
8+35.71
Δ = 58°03'20" Rt.
6+32.85
136.17
Fd. 2"x2"
Mkd 1+82.4
F.B. 1672-27
90°
up
set 2x2
3+86.42
B.C. Rt. 2x2
Con. Mon.
S.W. Cor. City Park

xsec Soledad Rd.
thru S. end City Park

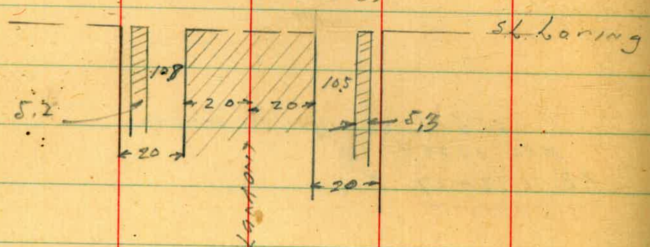
1

See page 2A

0+50

T.P.	12.80	220.55	0.84	207.75

0+100 B.C. Lt S.L. Loring St.
edge Con. pav.
end 8" curbs



0-100

T.P.	12.94	208.59	0.61	195.65
B.M. S.E. 7' C.T. Wilbur Lamont 1408-54 1324-47	9.97	196.26		186.29 ✓

indexed C.S.K.

Lt = West — ℄ — Rt

212.55 8.0/50	213.55 7.0/40	214.1 6.4/20	215.7 4.8	216.4 4.1/20	217.5 3.0/40	2.0/50		
210.4 10.1/50	210.65 9.9/40	210.4 10.1/20	211.3 9.2/4	210.7 9.8/3	210.7 9.8	211.2 9.3/20	211.7 8.8/40	8.4/50

Void Pav-31

220.55

0.7/50	207.9 0.7/40	207.15 1.44/20 c6	206.55 2.04/20 9T	206.97 1.62	206.57 2.02/20 9T	207.18 1.41/20 c6	207.4 1.2/40	1.2/50
199.75 8.84/20 c6	199.05 9.54/20 9T	199.53 9.06	199.14 9.45/20 9T	199.73 8.8c/20 c6				

208.59

					26.7
+50					16.7
					50
+37					
T.P.	12.48	243.36	1.35	230.88	
2+04.41 E.C.					
+75					
1+50					
T.P.	12.39	232.23	0.71	219.84	
		220.55			

L

228.4	232.9	235.5	238.2	238.5	238.0	238.4	238.4	
15.0	10.5	7.9	5.2	4.9	5.4	5.0	5.0	5.2 2.7
40	20	8	3		9	20	40	46 50
226.26	228.2	231.7	235.0		237.0	237.1	237.4	
17.1	15.2	11.7	8.4		5.6	6.3	6.0	5.8
50	40	20			5	20	40	50

243.36

+2.0/50

222.1	225.9	227.0	230.9		233.1	233.5	234.7	234.0
10.1	8.3	5.2	1.3		+0.9	+1.3	+2.5	+1.8
50	40	20			20	28	30	40
220.5	221.9	223.1	225.0		226.6	228.6		
11.7	10.3	9.1	7.2		5.6	3.6	5.1	2.4
50	40	20			20	40	45	50
							ditch	
217.1	217.9	220.2	221.3		222.9	224.6	223.4	
15.1	14.3	12.0	10.9		9.3	7.6	8.8	7.6
50	40	20			20	37	40	50

232.23

3+68				
3+59				
T.P.	12.08	266.47	1.63	254.39
3+15				
T.P.	13.16	256.02	0.50	242.86
3+08				
2+57				
		243.36		

Lt ℄ Rt

3+68: 53.1 13.4/40 (Top Bank) · 56.6 9.9/20 · 57.0 7.5 · 62.2 4.3/20 · 65.2 1.3/40 · +0.4/50

3+59: 45.1 21.4/50 · 44.7 21.8/40 · 52.7 13.8/31 · 55.3 11.2/20 · 57.6 8.9 · 60.2 6.3/20 · 63.4 3.1/40 · 1.5/50

266.47

3+15: 41.3 14.7/50 · 42.9 13.1/40 · 43.0 13.0/20 · 42.3 13.7/8 · 41.7 14.3/6 · 48.4 7.6 · 53.9 2.1/20 · 56.5 +0.5/40 · +2.5/50

256.02

3+08: 237.7 5.7/50 · 41.0 2.4/40 · 43.4 0.0/35 · 43.4 0.0/33 · 42.2 1.2/32 · 42.6 0.8/20 · 42.5 0.9/11 · 41.4 2.0 · 48.5 +5.1/5 · 52.2 +8.8/20 · 55.9 +12.5/40 · +13.6/50

2+57: 226.8 16.6/50 · 28.8 14.6/40 · 33.3 10.1/20 · 34.5 8.9/14 · 39.0 4.4/5 · 39.3 4.1 · 38.6 4.8/3 · 39.1 4.3/20 · 38.8 4.6/33 · 47.4 +4.0/40 · +6.6/50

243.36

5+00				
5+00				
T.P.	11.24	286.45	0.42	275.21
+50				
T.P.	12.11	275.63	2.95	263.52
4				
3+86.42 B.C. Rt.				
		266.47		

Lt		℄		Rt	
				84.0 (2.5 / 240)	78.0 (8.4 / 300)
74.8 (11.6 / 50)	74.9 (11.5 / 40)	76.0 (10.4 / 20)	77.7 (8.7)	79.5 (6.9 / 20)	81.5 (4.9 / 40)
84.1 (2.3 / 90)	86.4 (0.0 / 140)	86.7 (+0.3 / 190)			
		286.45			
	69.0 (6.6 / 40)	70.1 (5.5 / 20)	71.8 (3.8)	73.9 (1.7 / 20)	75.3 (0.3 / 40)
		275.63			
	60.5 (6.0 / 40)	62.7 (3.8 / 20)	64.4 (2.1)	66.5 (0.0 / 20)	68.1 (+1.6 / 40)
	56.7 (9.8 / 40)	59.3 (7.2 / 20)	62.3 (4.2)	64.3 (2.2 / 20)	67.3 (+0.8 / 40)
		266.47			

6+00				
6+00				
T.P.	5.76	291.53	0.68	285.77
5+50				
5+50				
5+25				
		286.45		

					86.9	87.0	81.9	78.2
					4.6	4.5	9.6	13.3
					150	190	250	300
74.6	74.7	76.0	76.6	78.2	78.8	86.3	86.5	
16.9	16.8	15.5	14.9	13.3	11.7	5.2	5.0	
50	40	20		20	40	85	100	
			291.53					
					87.8	85.4	82.4	77.5
					+1.4	1.0	4.0	8.9
					150	200	250	300
75.6	75.8	76.8	78.4	80.0	82.1	86.8		
10.8	10.6	9.6	8.0	6.4	4.3	+0.4		
50	40	20		20	40	100		
76.4	76.5	77.7	79.5	80.8	82.4	82.5		
10.0	9.9	8.7	6.9	5.9	4.0	3.9		
50	40	20		20	40	50		
			286.45					

					Lt		℄		Rt	
T.P.	5.04	283.74	8.05	278.70						
7+00								72.9 13.8/200	70.0 16.7/250	
7+00					79.0 7.8/50	78.6 8.1/40	77.6 9.1/20	77.5 9.2	77.6 9.1/20	78.4 8.3/40	78.4 7.4/42	80.9 5.8/100	78.5 8.2/150
6+50								85.0 1.7/150	82.7 4.0/200	77.2 9.5/250	73.7 13.0/300
6+50					73.8 12.9/50	74.0 12.8/40	75.1 11.6/20	76.1 10.6/4	77.2 9.5	78.3 8.4/20	78.9 7.8/40	83.8 2.9/100	84.8 1.9/120
T.P.	6.84	286.75	11.62	279.91			286.75			
		291.53								

Contd. 1324-51

1+28.5

13+71.5 / 8+35.71 E.C. Eq.

+9.7
47.8
edge of conc drive

8+00

8+00

+7.9
50.5
bes conc drive

+7.7
50

7+50

7+50

2 83.74

+

91.4 87.1 82.1 79.6 76.7 77.0 67.5

+10.7 Top / Base Brick Wall 40 | +7.7 40 | +3.4 20 | 1.64 Hub 6 | 4.1 13 | 7.0 20 | 6.7 40 | 16.2 100 S. Rim

75.1 68.6

E.C. 100 S. Rim Canon | 14.1 150 S. Rim

89.3 86.5 83.7 81.0 80.6 77.5 78.0 78.5

+8.6 41.2 Top of wall 40 | +5.6 40 | +2.8 20 | 0.0 | 2.7 20 | 3.1 28 | 6.7 36 | 5.7 40 | 5.2 50

79.2 77.5 74.1 71.4

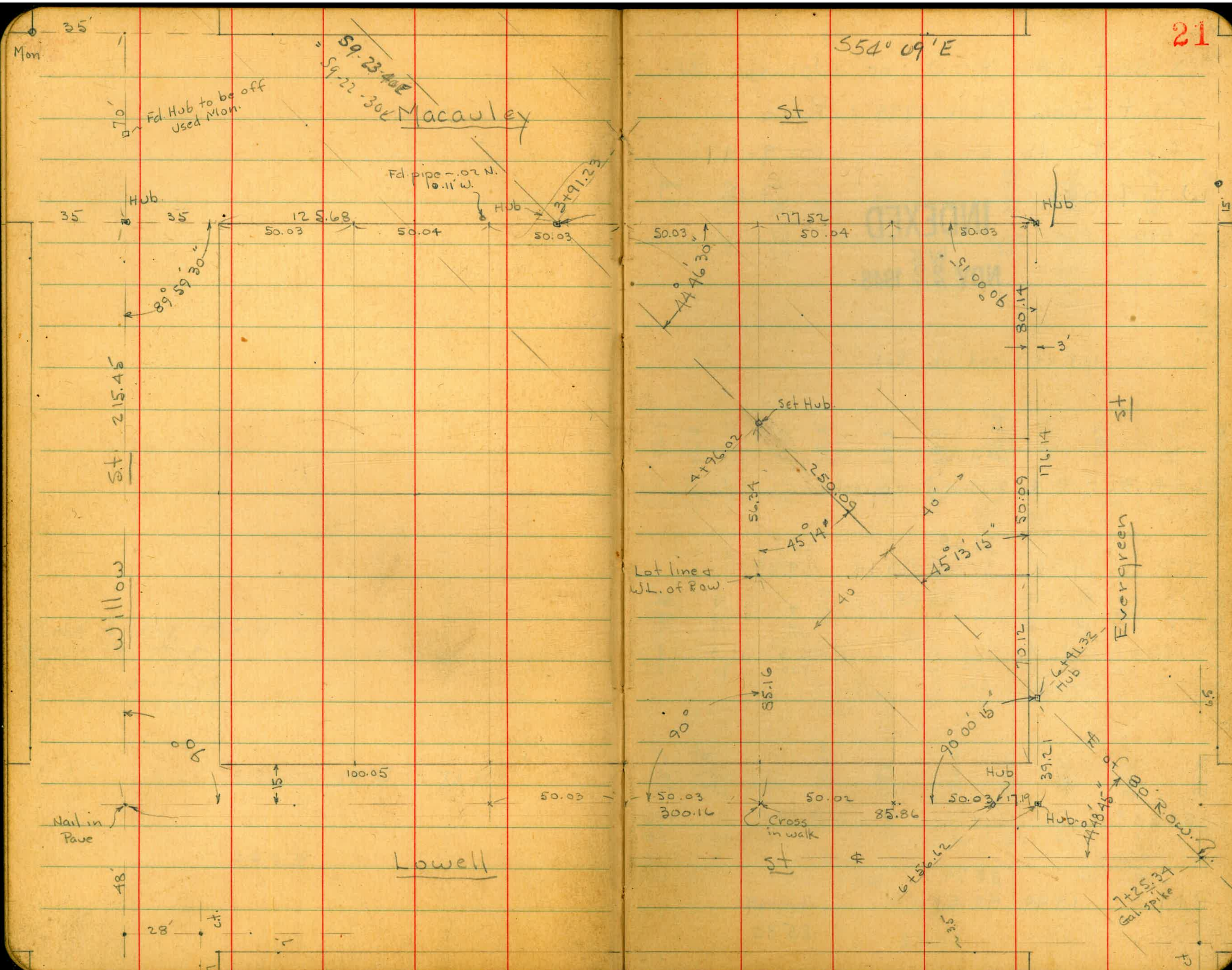
4.5 60 | 6.2 100 | 9.6 150 | 12.3 200

84.2 82.6 81.3 81.3 79.6 78.1 78.3

Top +3.4 Wall 40 | +0.9 | +0.5 40 | 1.1 20 | 2.4 | 2.4 20 | 4.1 30 | 5.6 33 | 5.4 40

2 83.74

Check to BM, Top of Lower Con. Stop. 105' Lt of old Sta. 8+54.88 F.B. 1291-51			10.40	265.62	265.51 (0.11)
T.P.	2.66	276.02	10.38	273.36	
		283.74			


Mon
35'
Fd. Hub to be off
Used Mon.
S9-23-40E
S9-22-30E
Macauley
St
S54° 09'E
Fd. pipe ~.02 N.
0.11' W.
Hub
3+91.23
35
125.68
177.52
50.03
50.04
50.03
50.03
50.04
50.03
89° 59' 30"
44° 46' 30"
90° 00' 15"
80.14
3'
Set Hub
4+96.02
250.09
56.34
176.14
45° 14'
45° 13' 15"
40'
40'
50.09
Lot line &
W.L. of Row
Willow
St. 215.46
St
Evergreen
70.12
6+41.32
Hub
85.16
90°
90°
90° 00' 15"
15
100.05
39.21
Hub
50.03
50.03
300.16
50.02
85.86
50.03
17.19
Nail in
Pave
Cross
in walk
Hub
44° 48' 45"
80' Row
Lowell
St
6+56.62
7+25.34
Gal. spike
48'
28'
15'

X-Sect. 80' R.O.W. of Wabaska Dr.
Cont. from Book 1794 - P. 20
for sta. to 5+00 10-9-47
W.O. 90051 7.0.

6+80

6+63 - 11.8 Rt. = end cb. Ret.

6+41.32 = ℄ + 3' Line Evergreen - on Hub.

T.P.	9.38	~~38.45~~ 34.68	13.44	~~29.07~~ 25.30
6+00				26.4 / 12.3 / 100 ; 26.4 / 12.3 / 70 ; 26.9 / 11.8 / 40
5+50				27.0 / 11.7 / 100 ; 27.1 / 11.6 / 70
B.M.	13.44	42.51 ~~38.74~~		~~29.07~~ 25.30

℄

Lt.

25.9 / 8.8 / 70
26.3 / 8.4 / 40
26.2 / 8.5 / 20
26.1 / 8.6
27.1 / 7.6 / 15
26.95 / 7.73 / 23 gut = edge of Pave
27.98 / 6.70 / 40
27.94 / 6.74 / 70 gut
28.63 / 6.05 / 70 Top cb
30.0 / 4.7 / 92
27.09 / 7.59 / 11.8 Top cb

26.1 / 8.6 / 100
26.4 / 8.3 / 70
26.5 / 8.2 / 40
27.1 / 7.6 / 20
28.5 / 6.2
29.3 / 5.4 / 20
29.7 / 5.0 / 40
30.34 / 4.34 / 60 Top cb
29.56 / 5.12 / 60 gut
31.47 / 3.21 / 84 ℄ on pave
32.07 / 2.61 / 107 gut
32.88 / 1.80 / 107 Top cb

~~38.45~~ 34.68

27.4 / 11.3 / 20
28.4 / 10.3
25.7
31.13 / 9.0 / 20
31.3 / 7.61 / 40 / 7.4 / 49 on Conc. Dr.
35.74 / 3.00 / 49 Ground floor
33.7 / 5.0 / 60
35.28 / 3.46 / 100 Top cb.
34.53 / 4.21 / 100 gut.

on Dirt floor Gar.

27.3 / 11.4 / 40 also Dirt floor Gar.
27.6 / 11.1 / 20
27.7 / 11.0 / 5
29.49 / 9.25
29.2 / 9.5 / 20
30.0 / 8.7 / 40
32.0 / 6.7 / 53
33.5 / 5.2 / 55
34.6 / 4.1 / 76 Ground along House
39.34 / +0.60 / 76 floor

on Conc. floor of Gar.

~~42.51~~ 38.74

Lt. ℄ Rt.

7+25.34 = ℄ + ℄ Lowell

7+04 = edge Pave

6+98 - 22.7 Lt. = end cb Ret.

25.4 25.4
9.3 9.3
80.3 40
along Bldg

25.7
9.0
59.3
along Bldg.

25.62 24.91 25.58 25.93 26.02 26.4 27.2 27.6 29.5
9.06 9.77 9.10 8.75 8.66 8.3 7.5 7.1 5.2
26.6 24 12 13 20 40 58 75
Top cb edge edge
+ground.

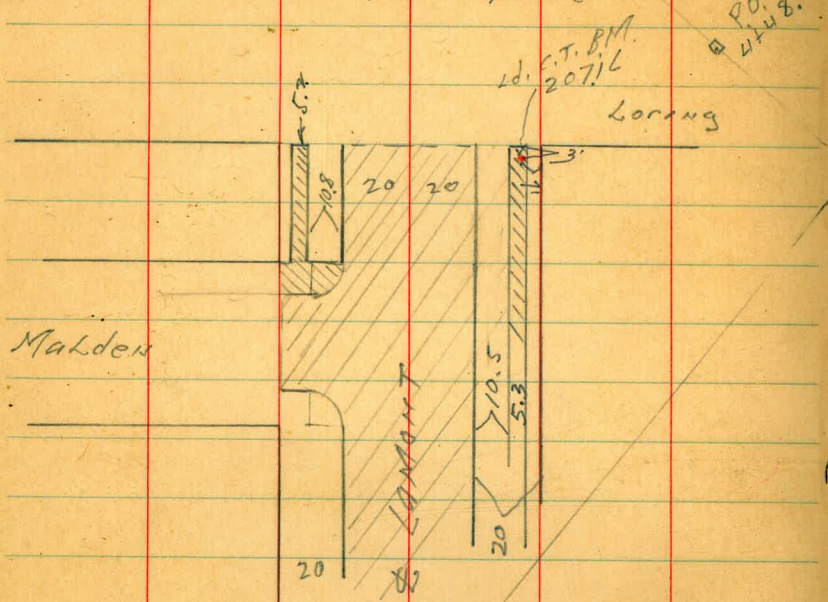
25.9 26.04 26.0 26.02 26.84 26.9 27.0 27.8 29.7
8.8 8.64 8.7 8.66 7.84 7.8 7.1 6.9 5.0
40 22.3 9 out = edge 22 40 47 50 75
Top cb
+ground.

26.01
8.67
22.7
Top cb.

34.68
~~38.75~~

Realignment Soledad Road

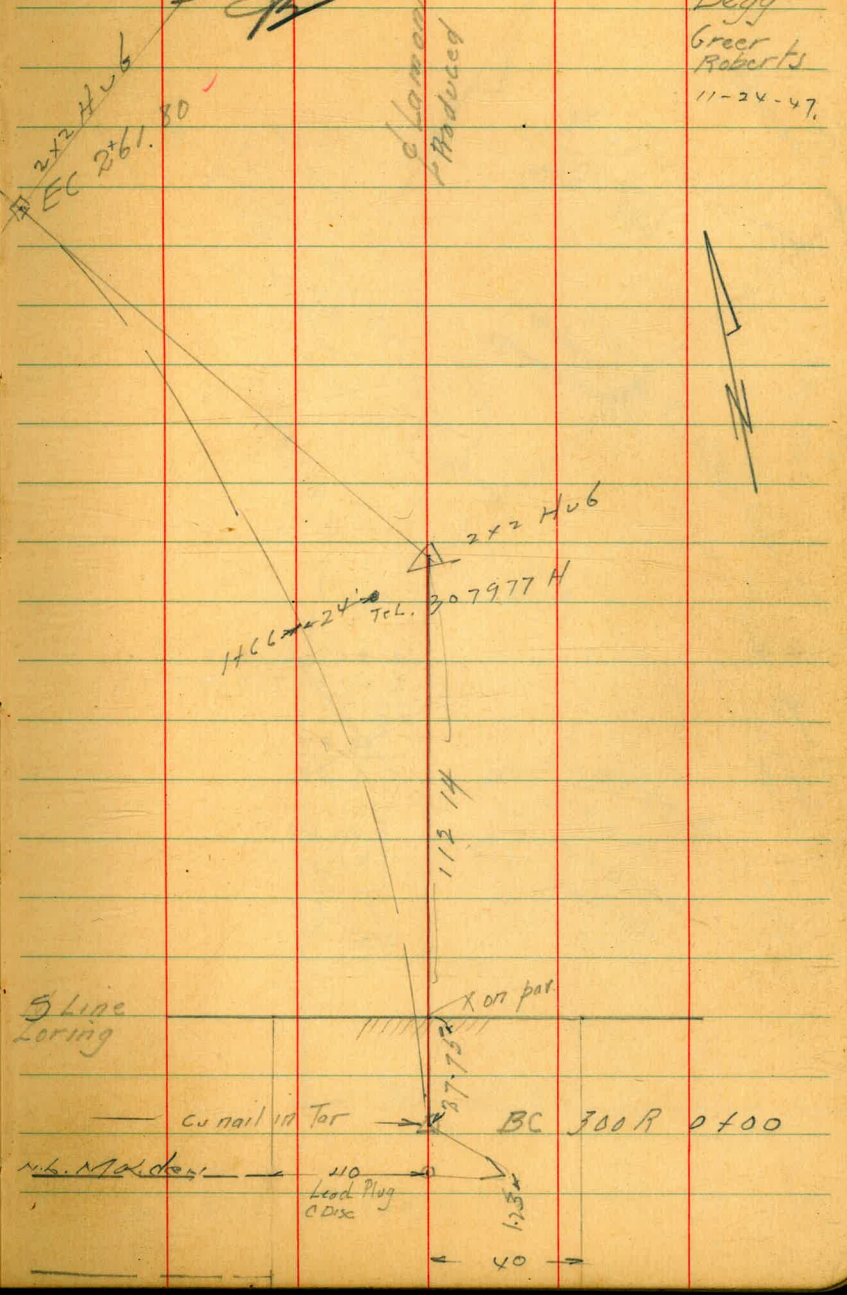
W.O. 90058



Δ R = 300
Δ = 50°
T = 139.89
L = 261.80
Rate 5°-29

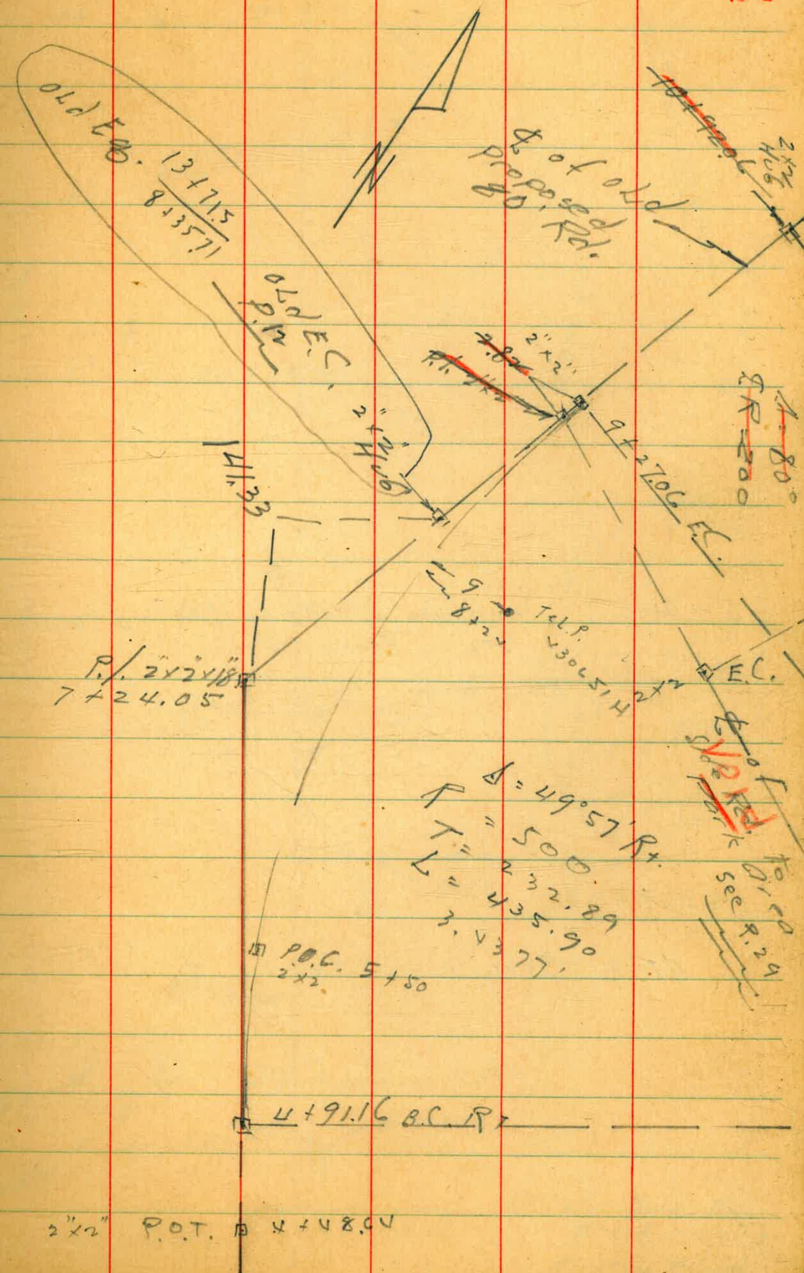
Indexed

Moore
Begg
Greer
Roberts
11-24-47.



10 97.06
9 27.96
167.80

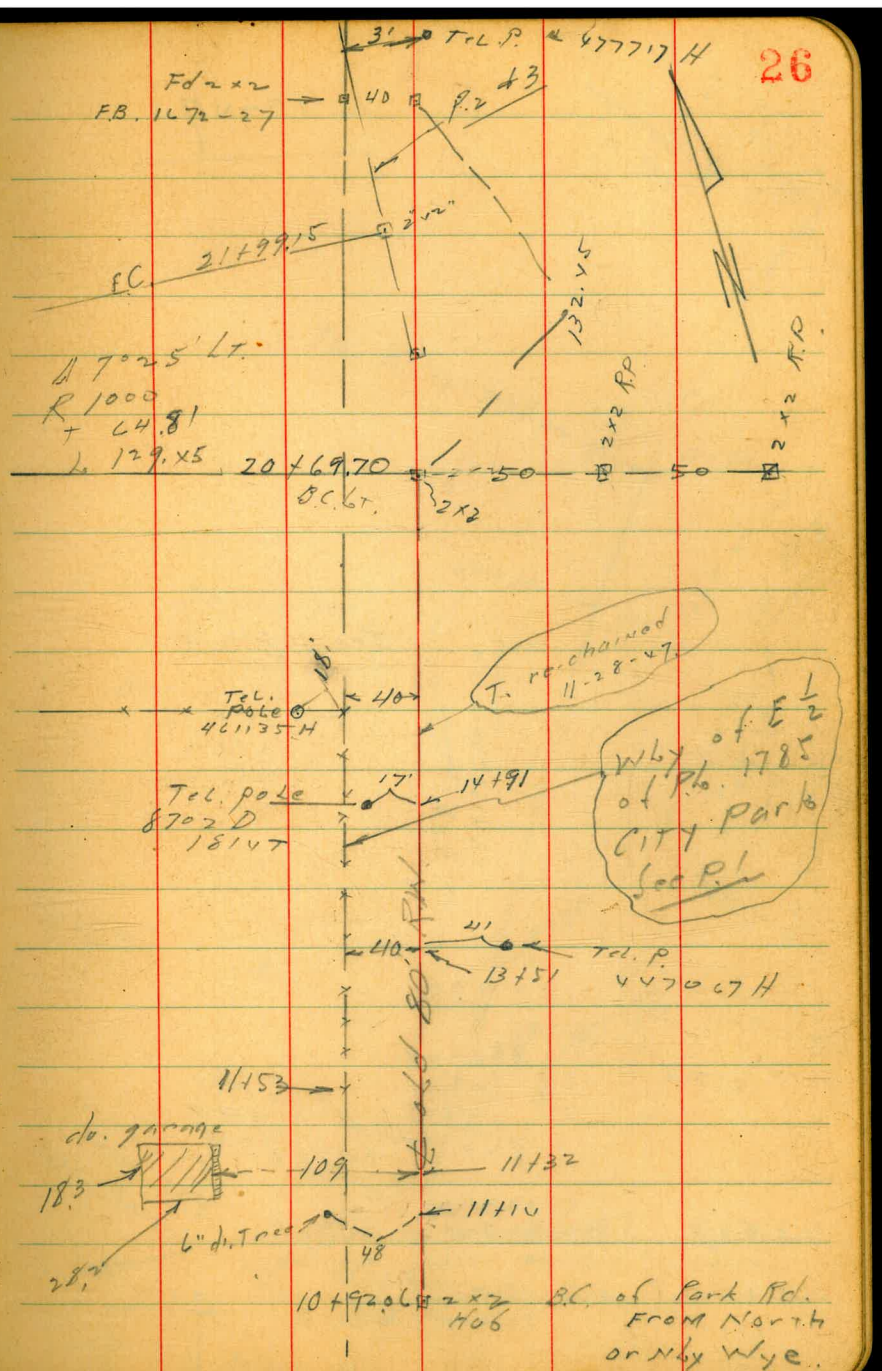
232.89
141.33
91.56



24 + 40 3' Rt Tel. Pole

18 + 91 end wire & Metal posts & Tel. P. Beg. " Fence wood "

11 + 53 Beg. wire fence & Metal Posts



12-10-47

See p. 3

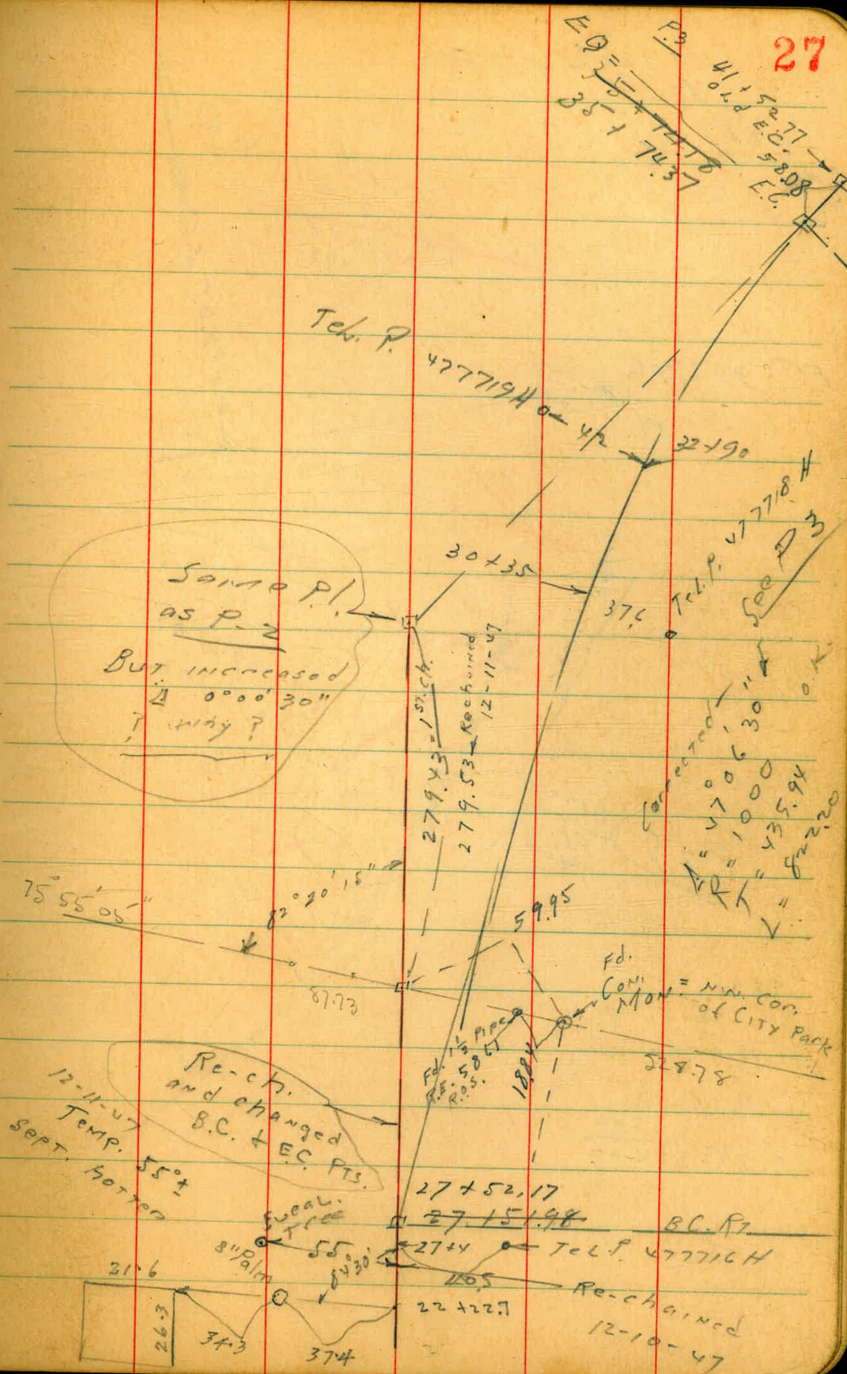
435.94

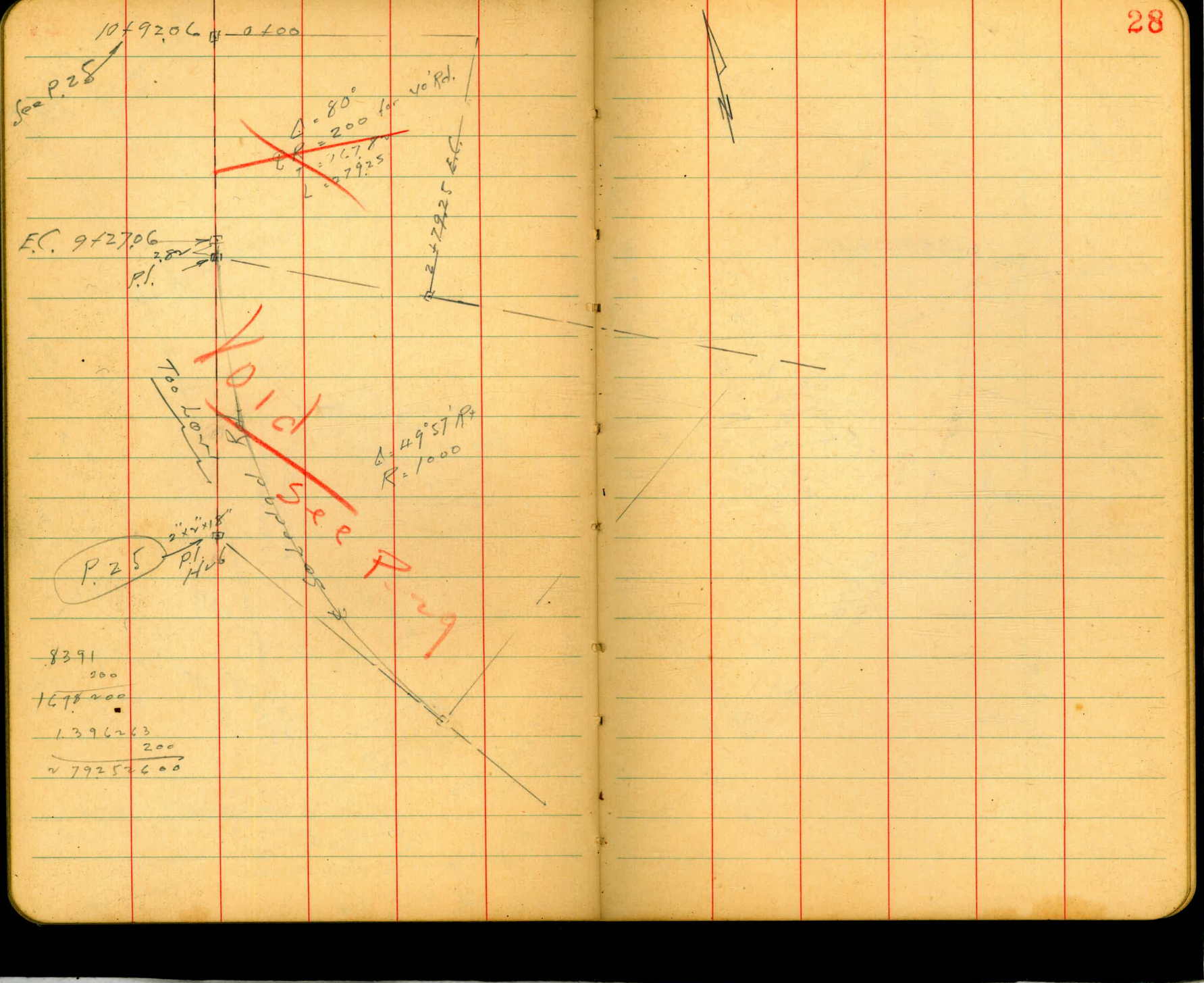
82°20'30"
17 45
1 45
82 21.94

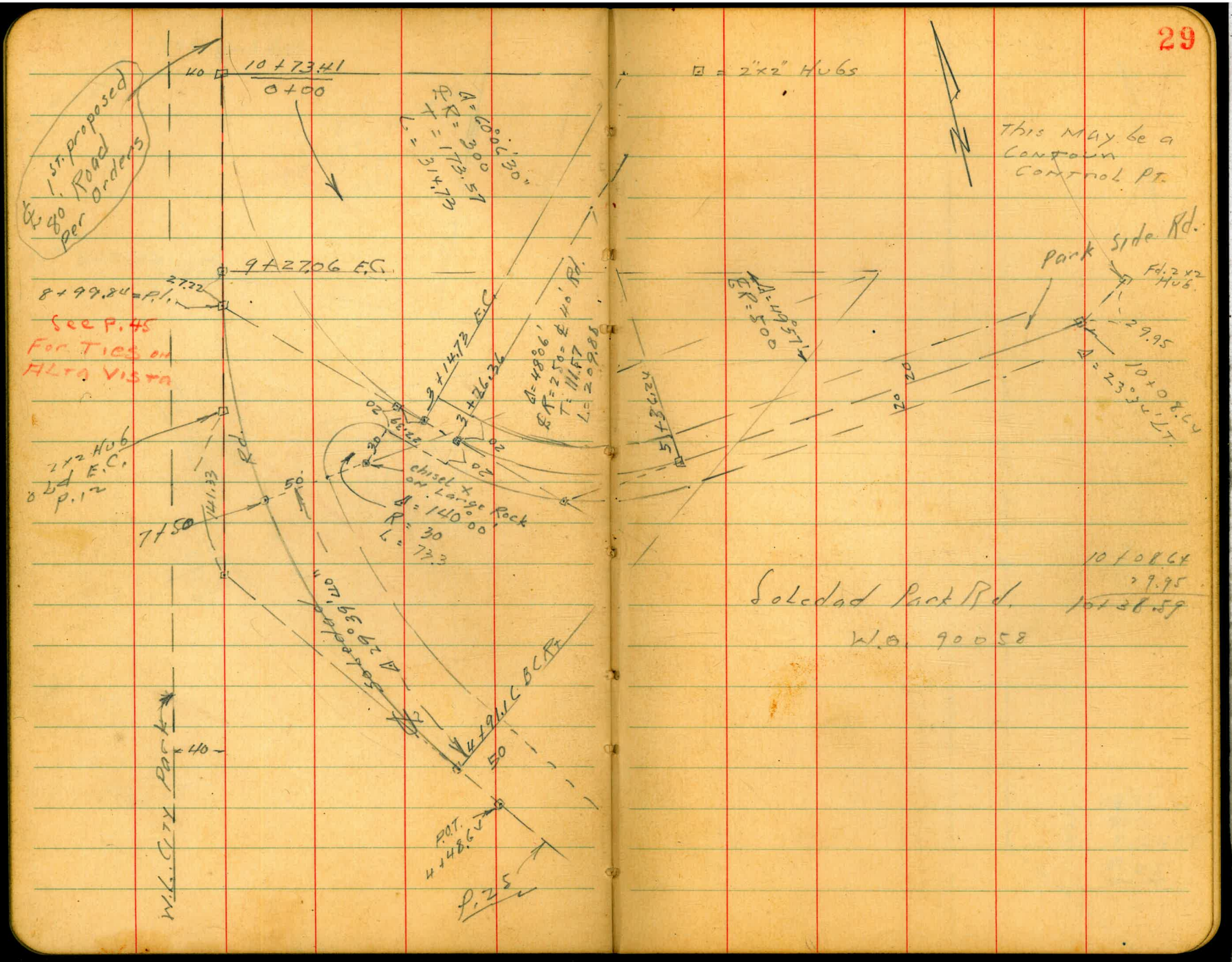
27 51.98
8 22.20
35 74.18

23+47 55 Lt 24" di Eucal.

~~22+22.7 H.L. Small Dwelling~~
Board & Batten


E.C. 35+74.37
P3
Old E.C. 41+52.77
Tel. P. 477719H
32+90
30+35
Same P.I. as P. 2
But increased Δ 0°00'30"
? why ?
Tel. P. 477718 H
See P 3
376
Corrected
Δ = 47°06'30"
R = 1000'
T = 435.94
L = 822.20
O.K.
279.43
279.53
Rechained 12-11-47
75°55'05"
82°20'15"
59.95
67.73
Fd. Conc. Mon. = N.W. Cor. of City Park
328.78
Fd. 1½" Pipe R.E. 5861 R.O.S.
188
Re-ch. and changed B.C. & E.C. Pts.
12-11-47
Temp. 55°±
Sept. hotter
27+52.17
27+51.98
B.C. Rt
Eucal. Tree
8" palm
55
27+4
Tel. P. 477716 H
Re-chained 12-10-47
22+22.7
21.6
26.3
34.3
37.4

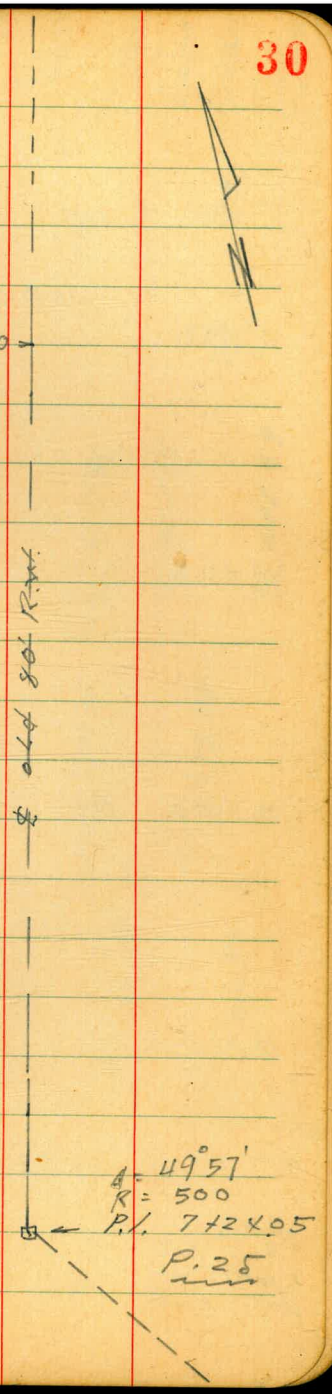

10+92.06 = 0+00
See P. 28
Δ = 80° for 40' Rd.
R = 200
T = 167.77
L = 279.25
E.C. 9+27.06
P.I.
2+79.29
VOID
See P. 29
Too Long
Δ = 49°51' Rt
R = 1000
2"x4"x18"
P.I. Hub
P. 25
8391
200
1678200
1396263
200
279252600



□ = 2"x2" Hubs

This May be a Contoun Control Pt.

Soledad Rd.



Re-Xsec Soledad Rd.
Sketch P24

Sta.	+		-		
1+00					
T.P.	11.95	219.11	4.53	207.16	10' C.T. Tie Back S.E. Cor Loring and Lamont
	20' × 10' × 1"				
0+50					
0+20					
0+00	B.C. Lt.				
0-60					
T.P.	12.98	211.69	0.09	198.71	
B.M. S.E. 7' C.T. Lamont Wilbur	12.51	198.80		186.29	

Lt

1+00: 209.21 9.9/100 · 211.01 8.1/50 · 213.91 5.2 · 213.31 5.8/12 · 214.91 4.2/50 · 214.91 4.2/63 · 213.11 6.0/66 · 216.01 3.1/70 · 218.71 0.4/100

0+50: 207.29 4.4/100 · 208.69 3.0/50 · 209.19 2.5/15 · 219.11 208.39 3.3 · 208.29 3.4/29 · 210.19 1.5/37 · 210.19 1.5/50 · 210.89 0.8/100

0+20: 206.49 5.2/100 · 207.59 4.1/50 · 206.89 4.80/18.7 c6 · 206.32 5.37/18.7 · 206.84 4.85 · 206.59 5.10/21.3 · 207.20 4.49/21.3 c6 end · 208.79 2.9/50 · 208.59 3.1/100

0+00: 204.99 6.7/100 · 205.29 6.4/50 · 205.14 6.55/20 c6 · 204.64 7.05/20 · 204.94 6.75 · 204.53 7.16/20 · 205.11 6.58/20 c6 · 205.89 5.8/40 Lawn

0-60: 202.09 9.6/40 Lawn · 200.66 11.03/20 c6 · 200.04 11.65/20 · 200.45 11.24 · 200.03 11.66/20 · 200.65 11.04/20 c6 · 200.99 10.7/40 dirt against cobble wall

211.69

3+01				
2+61.80 E.C.				
2+45				
T.P.	11.09	242.20	0.35	231.11
2				
1+50				
T.P.	12.68 ~~12.67~~	231.46 ~~231.47~~ 219.11	0.33	218.78

225.00	232.60	235.10	240.20	239.60	248.00	254.60	263.70	
17.2	9.6	7.1	2.0	2.6	+5.8	+12.4	+21.5	
100	54	50	40		7	50	100	
220.60	230.20	237.10	237.50	236.30	237.40	245.50	252.70	
21.6	12.0	5.1	4.7	5.9	4.8	+3.3	+10.5	
100	50	15	4		34	10	100	
219.60	228.1	235.80	234.90	236.20	242.40	247.10		
22.6	14.1	6.4	7.3	2.0	+0.2	+4.9		
100	50		15	50	64	100		
215.26	221.96	242.20 ✓	227.56	225.46	229.46	227.76	230.96	227.46	232.66	×235.56
16.2	9.5	6.2	3.9	6.0	2.0	3.7	0.5	4.0	+1.2	+4.1
100	50		33	38	46	50	77	82	87	100
211.76	214.96	217.96	220.46	223.36	221.46	225.86	226.76			
19.7	16.5	13.6	11.0	8.1	10.0	5.6	4.7			
100	50		50	85	81	96	100			

231.46 ✓
~~231.47~~

NOSEY P.O.

20' cut bet. 4+00 & 6+00

4+48.64				
P.O. + Hub T.P. 4+48.64	12.70	285.59	2.04	272.89 ✓
4+00				
T.P.	12.59	274.93	1.98	262.34
T.P.	12.75	264.32	2.84	251.57
+64				
3+53				
3+08				
T.P.	12.30	254.41 242.20	0.09	242.11

L	21.0/100 264.59	17.6/50 267.99	12.7 272.89	7.7/50 277.89	2.6/100 282.99 R	
			285.59 ✓			
	18.8/100 256.13	14.9/50 260.03	9.8 265.13	3.8/50 271.13	+0.7/100 275.63	
			274.93 ✓			
10.0/100 244.41	10.7/60 243.71	3.7/50 250.71	+0.5/25 254.91	+3.3 257.71	+12.0/50 266.41	+19.1/100 273.51
15.1/100 239.31	11.1/90 243.31	11.4/50 243.01	1.0/25 253.41	+2.1 256.51	+10.1/50 264.51	+16.8/100 271.21
28.4/100 226.01	22.1/70 232.31	13.6/50 240.81	14.2/8 240.21	6.6 247.81	+1.0/50 255.41	+7.8/100 262.21
			254.41 ✓			

Station					Lt		℄			Rt
+50					14.9/100 274.35	12.7/50 276.55	10.2 275.39	6.1/50 283.15	5.1/100 284.15	
6					15.0/100 274.25	13.2/50 276.05	8.6 280.65	3.2/40 286.05	3.0/50 286.25	2.7/100 286.55
T.P. Rock	6.92	289.25	3.26	282.33 ✓			289.25			
5+50					9.6/100 276.19	6.6/50 278.99	2.3 283.29	+0.6/50 286.19	+2.0/87 287.59	+2.0/100 287.59
5+25					11.0/100 274.59	7.8/50 277.79	3.3 282.29	0.8/50 284.79	+1.0/100 286.59	
4+91.16 B.C. Rt					14.8/100 270.79	11.4/50 274.19	7.7 277.89	3.7/50 282.39	0.0/100 285.59	
		285.59					285.59 ✓			

Cont'd P 37

Lt — Rt

Station									
+33		+ 6.3 / 50 (290.85) Wall	0.0 / 15 (284.55)	3.5 (281.05)	7.8 / 10 (276.75)	7.5 / 34 (277.05)	11.1 / 50 (273.45)	14.8 / 70 (269.75)	
8	+3.4 / 59 (287.95) Wall	+2.8 / 50 (287.35)	0.0 / 20 (284.55)	2.5 (282.05)	4.1 / 13 (280.45)	6.9 / 20 (277.65)	6.2 / 41 (278.35)	8.4 / 50 (276.15)	12.4 / 75 (272.15)
+50		2.0 / 75 (282.55) Wall	2.5 / 50 (282.05)	4.3 (280.25)	6.4 / 10 (278.15)	6.0 / 40 (278.55)	6.4 / 50 (278.15)		
+30	3.8 / 86 (280.75)	5.1 / 50 (279.45)	5.5 / 12 (279.05)	5.0 / 7 (279.55)	6.1 (278.45)	5.3 / 50 (279.25)	9.3 / 100 (275.25)		
7+00	7.4 / 100 (277.15)	7.7 / 50 (276.85)	6.6 / 30 (277.95)	7.7 / 25 (276.85)	6.6 (277.95)	4.9 / 20 (279.65)	4.4 / 50 (280.15)	5.3 / 100 (279.25)	

Ground at Base of Con. Blk Wall 3' to 4' high (at +30, 3.8 / 86)

T.P.	4.19	284.55	10.89	278.36
		289.75		

284.55 ✓

Levels on Curve to Rt.
Δ = 140° Curve in 4 parts

#4 = E.C. Sketch p 29

#3

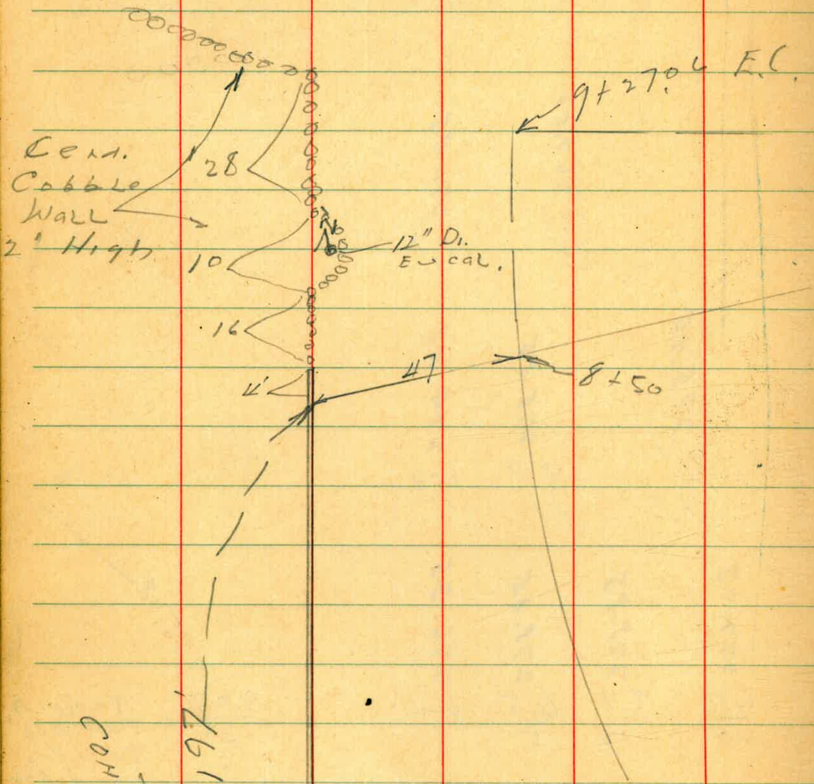
#2

#1

P.R.C. = 50 Rt. of 7+50

Lt	Prop. Line	Rt
	270.85	
	B.7	
	271.85	
267.55	12.7	
17.0 / 25		
275.45	274.25	
9.1 / 45	10.3	
	275.85	
	8.7 / 32	
277.75	276.35	275.48
6.8 / 40	8.2	9.07 / 30 = Radius Pt. Top Big Boulder good For B.M.
278.85	278.15	Chiseled Cross for Point IS 0.03 ft Lower
5.7 / 17	6.4	
278.05		
6.5 / 15		

284.55 ✓



T.P. 3.93 279.48 9.00 275.55

8+50

284.55

IN Road

L				℄		R		
293.55	290.95	284.55	279.75	277.95	276.65	276.35	271.75	270.25
+9.0 / 57	+6.4 / 47	0.0 / 22	4.8 / 5	6.6	7.9	8.2 / 30	12.8 / 50	14.3 / 70

Wall

2 84.5 5

IN Garden

Lt — ℄ = 40' Lt. to W.L. Bank — Rt

9+74

Rod	1.4	4.5	6.1	6.3	8.2	7.7	9.7
Dist.	100	50	32	10	Wash	50	100
Elev.	278.08	274.98	273.38	273.18	271.28	271.78	269.78

9+43

Rod	+6.3	+4.1	+2.4	+1.0	1.9	3.1	6.2	17.0	9.9	10.1	13.5
Dist.	100	80 Wall	78	67	66	50		20	40	50	100
Elev.	285.78	283.58	281.88	280.48	277.58	276.38	273.28	262.48	269.58	269.38	265.98

9+27.0 E.C.

Rod	+13.0	+5.1	+5.0	+2.7	+1.4	2.5	2.6	5.6	5.4	18.0	16.6	14.3	21.4
Dist.	100	70	63 Wall	62	55	52	50	12		27	37	50	100
Elev.	292.48	284.58	284.48	282.18	280.88	276.98	276.88	273.88	274.08	261.48	262.88	265.18	258.08

9+14

Rod	+13.0	+12.6	+5.1	+4.9	+2.0	+0.6	2.8	4.7	4.6	16.8	19.7	17.5	18.0	23.0	24.0
Dist.	100	80	62	52 Top Cobble Wall	51	41	39	10		26	35	45	50	80 Wash	100
Elev.	292.48	292.08	284.58	284.38	281.48	280.08	276.68	274.78	274.88	262.68	259.78	261.98	261.48	256.48	255.48

9+00

Rod	+13.2	+13.0	+4.1	+3.9	+1.0	2.9	3.9	4.8	17.3	20.7	21.0	22.0
Dist.	50 ?	72	50	41	40	28		5	37	42	50	100
Elev.	292.68	292.48	283.58	283.38	280.48	276.58	275.58	274.68	262.18	258.78	258.48	257.48

279.48

279.48

	+	HI	−	EI
11+50				
11+32				
11+00				
10+73.4	See Sketch			
T.P. 2"x7" Hub RT. Park Rd. 10+73.4	11.40	286.43	4.45	275.03
10+00				
		279.48		

Baseline

Lt							Rt
	279.03	280.73	283.73	283.03	281.83	281.63	282.93
	7.4 / 100	5.7 / 50	2.7	3.4 / 4	4.4 / 10	4.8 / 50	3.5 / 100
	278.71	278.54					
	7.72 / 113.5	7.89 / 109					
	Gar FL.	Corr apron					
	276.03	278.13	277.73		277.73	279.03	
	10.2 / 100	8.3 / 50	8.7		8.7 / 50	7.4 / 100	
	274.43	276.13	275.03		275.93	276.63	
	12.0 / 100	10.3 / 50	11.4		10.5 / 50	9.8 / 100	
	277.98	276.58	273.48	273.28	272.78	272.68	272.68
	1.5 / 100	2.9 / 68	6.0 / 50	6.2 / 4	6.7	6.8 / 50	6.8 / 100
				279.48			

14				
+50				
T.P.	11.80	307.32	0.00	295.52
13				
+50				
12				
~~T.P.~~	11.48	295.96	1.95	284.48
		2643		

Lt

291.12	295.22	295.72	296.92	297.12	297.22	296.12	296.32	297.62	298.32	300.42
16.2	12.1	11.6	10.4	10.2	10.1	18.2	11.0	9.7	9.0	6.9
100	50	35	12		2	6	30	32	50	100

B.L.

Rt

292.12	292.32	293.0	293.32	294.02	294.52	293.62	293.62	295.22	295.32	297.22
18.7	15.0	14.3	14.0	13	12.8	13.7	13.7	12.1	12.0	10.1
100	50	40	14		5	10	31	33	50	100

286.26	289.56	289.06	290.16	291.46	291.76	292.16	290.46	290.46	291.86	292.36	295.36
9.7	6.4	6.1	5.8	4.5	4.2	3.8	5.5	5.5	4.1	3.6	0.6
100	50	32	17	12		8	12	27	24	50	100

307.3

283.86	286.56	287.86	287.46	287.66	288.96	290.06	294.16		
12.1	9.4	8.1	8.5	8.3	7.0	5.9	1.8		
100	50		11	35	36	15	100		

280.96	283.36	284.46	285.36	285.46	286.26	287.16	287.66	289.76	
15.0	12.6	11.5	10.6	10.5	9.7	8.8	8.3	6.7	
100	50	9	8		35	36	50	100	

295.96

Sta.				
+50				
16				
+50				
T.P.	11.71	313.63	5.40	301.92
15				
14+50				

307.32

Lt | CL | Rt

Sta.														
+50	11.7/100 301.93	10.1/50 303.53	8.1 305.53	9.4/5 304.23	8.4/22 305.23	7.4/27 306.23	5.8/50 307.83	6.0/100 307.63						
16	13.6/100 300.03	11.6/50 302.03	9.7 303.93	10.4/6 303.23	9.8/27 303.83	8.8/28 304.83	7.5/50 306.13	6.4/100 307.23						
+50	16.2/100 297.43	13.5/50 300.13	12.3/40 301.33	12.5/20 301.13	11.8/18 301.83	11.0 302.63	11.8/6 301.83	11.0/27 302.63	10.2/28 303.43	9.1/35 304.53	8.8/50 304.83	6.2/100 307.43		
15	12.0/100 295.32	8.1/50 299.22	7.5/37 299.82	7.3/19 300.02	6.2/18 301.12	5.4 301.92 (313.63)	7.8/4 299.52	6.3/6 301.02	5.9/28 301.42	5.4/29 301.92	4.2/50 303.12	1.5/100 305.82		
14+50	14.3/100 293.02	10.0/50 297.32	9.4/40 297.92	9.6/32 297.72	8.9/15 298.42	8.5/14 298.82	7.5 299.82	7.5/2 299.82	9.8/5 297.52	8.4/7 298.92	8.4/28 298.92	7.0/30 300.32	6.6/50 300.72	3.5/100 303.82

307.32

						Lt	316.73	317.18	BL			Rt
19+10 Brickwalk							5.60 / 50	5.15 / 40				

19

Offset (rod / dist.)	Elevation
5.9 / 50	316.43
4.7 / 6	317.63
6.1	316.73
5.5 / 20	316.83
4.3 / 21	318.03
4.6 / 50	317.73
7.9 / 100	314.43

+50

Offset (rod / dist.)	Elevation
9.6 / 100	312.73
8.0 / 50	314.33
8.2 / 28	314.13
7.0 / 19	315.33
6.9 / 6	315.43
8.0	314.33
7.7 / 19	314.63
6.6 / 20	315.73
6.9 / 50	315.43
9.2 / 100	313.13

18

Offset (rod / dist.)	Elevation
14.3 / 130	308.03
11.2 / 50	311.13
10.8 / 40	311.53
11.8 / 39	310.53
10.8 / 25	311.53
9.7 / 16	312.63
9.3 / 6	313.03
10.6	311.73
10.4 / 20	311.93
9.1 / 21	313.23
8.9 / 50	313.43
11.1 / 100	311.23

T.P. 12.09 322.33 3.39 310.24

322.33

+50

Offset (rod / dist.)	Elevation
7.0 / 100	306.63
5.2 / 50	308.43
5.0 / 38	308.63
5.7 / 36	308.93
5.2 / 25	308.43
3.8 / 18	309.83
3.5 / 5	310.13
4.2	309.43
4.4 / 22	309.23
2.8 / 23	310.83
2.4 / 40	311.23
2.4 / 50	311.23
5.0 / 100	308.63

17

Offset (rod / dist.)	Elevation
9.4 / 100	304.23
7.6 / 50	306.03
8.1 / 27	305.53
6.5 / 16	307.13
6.1 / 2	307.53
7.0	306.63
7.1 / 24	306.53
5.7 / 25	307.93
4.0 / 45	309.63
3.8 / 50	309.83
5.3 / 100	308.33

313.63

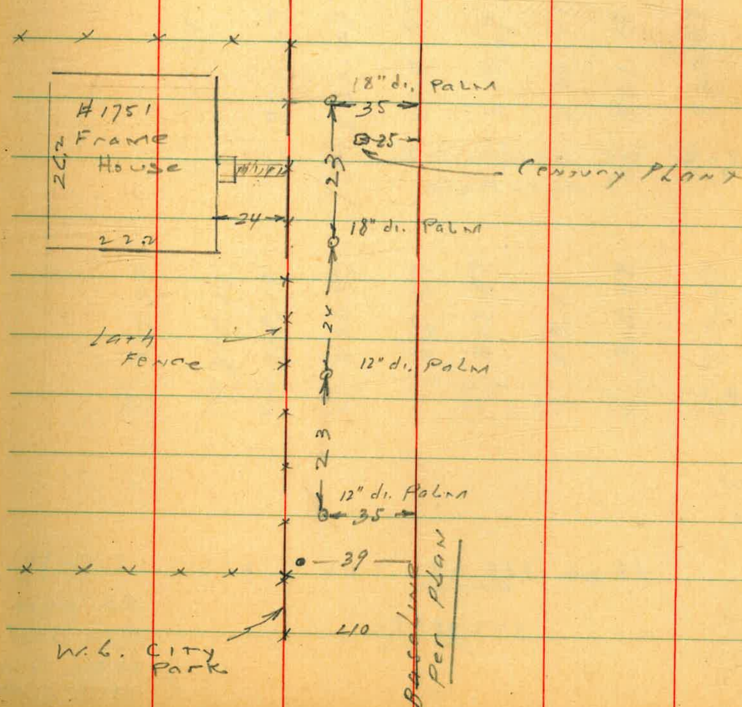
313.63

19 + 39.12

19+10 ℄ 4' Brick Walk Shrubs inside Fence

18 + 97.7 S.L. House

18+53 Beg. Row of Palms
+41 Tel. P. 477713 H
18 + 40 end wire + Beg. Lath fence



Note: 5195 AL has equation here instead of at Sta 35+74
H. Hom 11/22/57

20+69.70 BC ℄

20+50

20+00

19+79.12 M.L. opening at Yazoo

19+39.12

T.P. B.M. 3/4" Pipe 40' Lt. of Sta. P.V

13.00 333.07 2.26 320.07 319.79

322.33

P.O. says pipe had been pulled up and redriven?

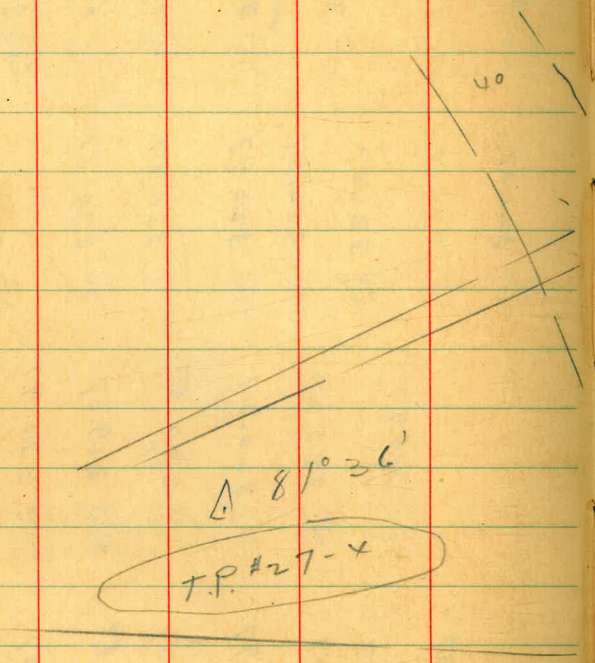
0.28 error

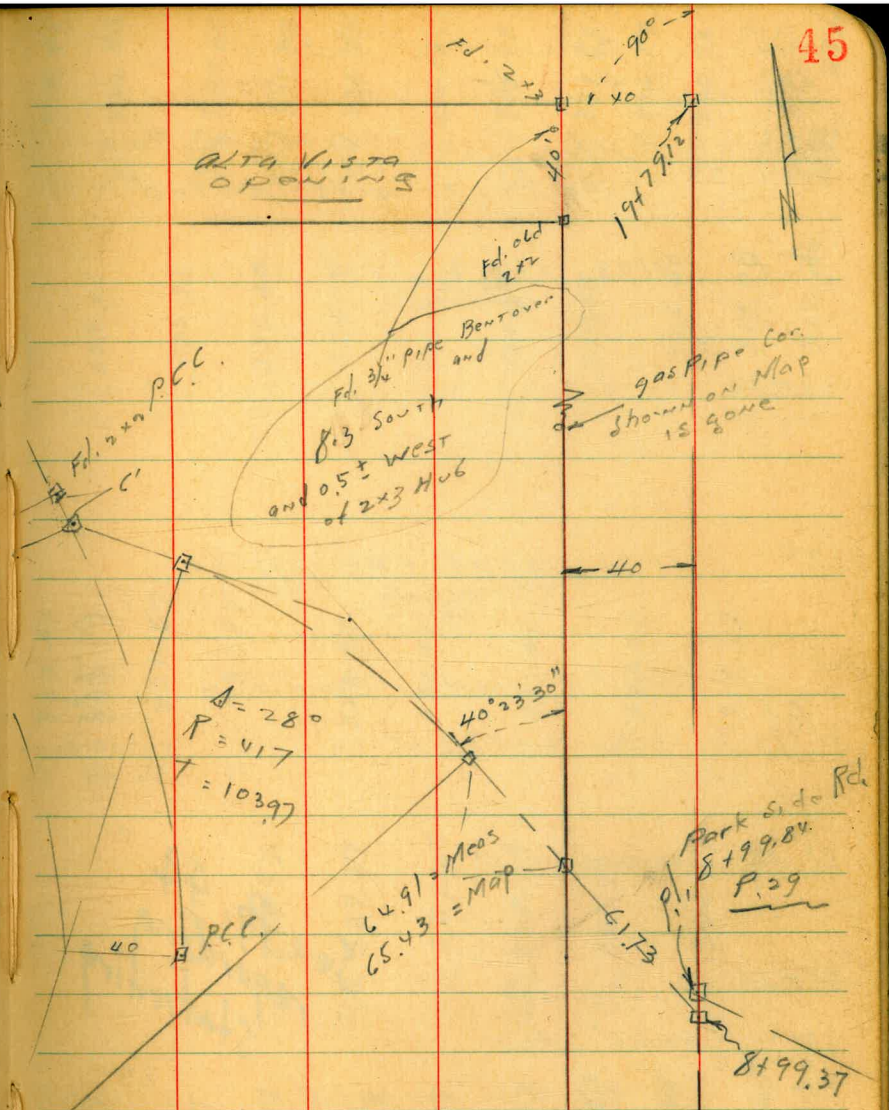
333.07

324.57	325.37	324.87	325.67	324.47	324.77	324.57	326.07	326.37	325.47
8.5/100	7.7/50	8.2/25	7.4/1	8.6/4	8.3	8.5/16	7.0/17	6.7/50	7.6/100
323.47	324.37	324.97	323.47	323.67	323.47	324.57	325.77	324.87	
9.6/100	8.7/50	8.1/9	9.6/5	9.4	9.6/17	8.5/18	7.3/50	8.2/100	
321.07	321.17	321.07	322.37	320.97	321.37	320.77	322.17	322.17	321.77
12.0/100	11.9/50	12.0/24	10.7/9	12.1/7	11.7	12.3/17	10.9/18	10.9/50	11.3/100
	319.97	320.27	320.27	320.47	319.67	320.97	321.17	320.47	
	13.1/100	12.8/50	12.8/40	12.6	13.4/16	12.1/17	11.9/50	12.6/100	
317.37	318.17	318.17	320.97	318.07	317.87	319.37	318.57	317.47	
15.7/100	14.9/50	14.7/40	12.1/11	15	15.2/17	13.7/17	14.5/50	15.6/100	

Ties to Soledad Ter.

⊡ = 2×2 Hub





Soledad X Sections

	+	HI	–	TP	
23	Note! cuts more than 100' Rt. only estimated				
T.P.	11.23	342.83	11.36	331.60	
22+50					
T.P	11.36	342.96	1.47	331.60	
	See P 27 location Board House				
E.C. 21+99.15	18" acacia 43.5 Lt				332.77 / –0.3 / 50
21+52	acacia 4" 45 Lt				
21+50					
21+41	acacia 2" 46 Lt				
21+38	Tel Pole 38 Lt 477/15 Rt				
21+15	acacia 3" 48 Lt				
21+00					
		333.07			

See Pg. 44 regarding stationing

46

Station 23: 334.43 8.4/100 · 336.43 6.4/80 · L · 337.03 5.8/50 · 337.43 5.4/35 · 336.23 6.6/17 · ℄ 335.13 7.7 · 335.43 7.4/30 · 331.63 11.2/50 · 326.83 16.0/70 · 320.73 22.1/87 · 315.03 27.8/100 · Bot. Wash 307.83 34.0/130

Station 22+50: 333.56 9.4/100 · 335.36 7.6/77 · 335.46 7.5/50 · 334.16 8.8/5 · 342.83 / 332.66 10.3 · 333.36 9.6/28 · 330.56 12.4/50 · 326.46 16.5/70 · 319.96 23/84 · 312.76 30.2/100

342.96

Station 21+99.15: 333.47 +0.4/50 · 334.87 +1.0/47 · 332.57 0.5/28 · 331.87 1.2/4 · 330.47 2.6/1 · 330.47 2.6 · 330.47 2.6/27 · 327.67 5.4/50 · 315.37 17.7/100

Station 21+50: 328.87 4.2/100 · 329.97 3.1/50 · 329.57 3.5/35 · 327.27 5.8 · 328.77 4.3/23 · 327.17 5.9/50 · 320.37 12.7/100

Station 21+00: 326.17 6.9/100 · 327.17 5.9/50 · 326.37 6.7/35 · 326.67 6.4/4 · 326.17 6.9 · 326.27 6.8/17 · 327.57 5.5/18 · 327.47 5.6/50 · 324.67 8.4/100

333.07

Station				
25+50				
Nail SE Cor Lath house T.P	6.70	365.97	365	359.27 ✓
scrambled to Otra Trabajo.				
T.P.	8.90	362.92	0.22	354.02
25				
+50				
T.P.	11.81	354.24	0.40	342.43
24				
23+50				
		342.83		

See Pg 44 For note on Stationing

Station											
25+50	355.97 10.0/100	355.67 10.3/50 Lt	355.77 10.2/33	352.17 13.8/15	351.77 14.2/13	351.47 14.5	351.37 14.6/2	345.77 20.2/22	332.37 33.6/50	322.47 43.5/78	312.87 53.1/100 wash
					365.97						
25	352.14 2.1/100	352.34 1.9/50	351.94 2.3/30	350.94 3.3/19	349.34 4.9/17	348.74 5.5/5	350.14 4.1/4	342.44 11.8/40	337.44 16.8/50	328.74 25.5/67	312.74 41.5/100
											310.24 44.0/110 Wash
+50	347.74 6.5/100	348.64 5.6/50	347.14 7.1/21	345.04 9.2/20	344.04 10.2/1	345.34 8.9	346.24 8.0/1	341.04 13.2/42	338.84 15.4/50	336.04 18.2/58	321.74 32.5/100
											308.24 46.0/115 wash
					354.24						
24	342.43 0.4/100	+ 343.33 0.5/50	342.63 0.2/20	341.33 1.5/17	341.43 1.4	336.73 6.1/41	334.93 7.9/50	329.53 13.3/70	314.63 28.2/100	312.83 30.0/125 Bot. wash	
23+50	337.43 5.4/100	340.23 2.6/25	340.33 2.5/50	338.93 3.9/19	337.33 5.5	337.13 5.7/6	338.53 4.3/7	334.33 8.5/50	331.63 11.2/65	317.13 25.7/100	310.83 32.0/125 Bot wash
					342.83						

T.P.	12.43	390.00	0.11	377.57
28				
27+52.17	8C Rt.			
T.P.	11.94	377.68	0.23	365.74
27				
+50				
26		365.97		

See Pg 44
For note
on stationing

Lt ℄ Rt

		0.1/100 377.58	1.2/50 376.48	2.7/4 374.98	4.1 373.58	6.4/12 371.28	4.9/36 372.78	8.6/50 369.08	14.1/75 363.58	18.8/100 358.88		
		3.8/100 373.88	5.3/50 372.38	8.1 369.58	8.0/4 369.68	11.0/8 366.68	11.0/29 366.68	14.5/50 363.18	27.5/100 350.18	40.4/140 337.28 Wash		
377.68		+2.1/100 368.07	+1.5/50 367.47	0.9/2 365.07	2.4 363.57	4.4/4 361.57	4.9/23 361.07	10.7/45 355.27	13.0/50 352.97	26.3/87 339.67	36.0/100 329.97	44.0/123 321.97
	1.8/100 364.17	2.4/50 363.57	5.1/5 360.87	8.1/3 357.87	8.2 357.77	8.5/18 357.47	15.9/46 350.07	17.4/50 348.57	27.1/75 338.87	39.0/100 326.97	48.5/120 317.47 Wash	
5.3/100 360.67	5.4/95 360.57	6.4/50 359.57	8.1/14 357.87	11.6/9 354.37	11.3 354.67	11.4/13 354.57	16.3/30 349.67	20.7/41 345.27	25.6/50 340.37	50.0/96 315.97	50.3/100 315.67 Wash	

365.97

E edge & ℄ of Wo'Lash house

31 — +2.0/100 404.32 — 0.0/50 402.32 — 401.72 0.6/38 — 400.42 1.9/37 — 399.42 2.9/15 — 400.82 1.5/12 — 400.32 2.0 — 398.62 3.7/10 — 400.42 1.9/50 — 400.22 2.1/100

+50 — 400.02 2.3/100 — 399.12 3.2/50 — 397.82 4.5/33 — 396.02 6.3/32 — 396.12 6.2/10 — 396.82 5.5 — 396.22 6.1/37 — 397.02 5.3/50 — 397.02 5.3/70 — 395.32 7.0/100

See pg. 44 for note on stationing

30 — 396.92 5.4/100 — 394.72 7.6/50 — 394.12 8.2/28 — 392.52 9.8/24 — 392.12 10.2/5 — 392.92 9.4 — 393.22 9.1/5 — 390.42 11.9/21 — 391.02 11.3/50 — 391.72 10.6/75 — 390.62 11.7/100

T.P. 12.66 402.32 0.3x 389.66 — 402.32

+50 — 392.60 +2.6/100 — 390.30 +0.3/50 — 388.80 1.2/18 — 387.20 2.8/15 — 387.50 2.5 — 387.00 3.0/10 — 388.60 1.4/12 — 382.40 7.6/47 — 380.50 9.5/50 — 378.70 11.3/55 wash — 379.90 10.1/63 — 380.30 9.7

See P.8 for location of 4 wire stock fence on Lt.

29. — 386.90 3.1/100 — 386.50 3.5/50 — 384.30 5.7/16 — 381.70 8.3 — 381.00 9.0/25 — 375.50 14.5/50 — 371.80 18.2/73 — 364.00 26.0/96 — 364.70 25.3/100 — side wash

28+50 — 381.50 8.5/100 — 380.80 9.2/50 — 379.70 10.3/3 — 378.70 11.3 — 378.50 11.5/2 — 375.90 14.1/4 — 376.60 13.4/32 — 372.40 17.6/50 — 364.00 26.0/100

340.00

390.00

+50				
33				
+50				
T.P.	11.75	423.95	1.09	412.20
32				
31+50				
T.P.	12.47	413.29	1.50	400.82
		402.32		

See pg. 44 for note on stationing

422.35 (1.6 / 100) 423.95 (0.0 / 50) 424.35 (+0.4 / 30) 423.95 (0.0 / 26) 422.55 (1.4 / 23) 423.05 (0.9) 424.35 (+0.4 / 4) 423.35 (0.6 / 50) 421.95 (2.0 / 75) 419.65 (4.3 / 100)

418.55 (5.4 / 100) 419.65 (4.3 / 50) 419.55 (4.4 / 38) 417.85 (6.1 / 35) 417.75 (6.2 / 14) 419.35 (4.6 / 11) 419.45 (4.5) 418.85 (5.1 / 50) 414.65 (9.3 / 100)

414.05 (9.9 / 100) 414.25 (9.7 / 50) 412.75 (11.2 / 48) 412.35 (11.6 / 24) 413.55 (10.4 / 21) 413.75 (10.2) 413.95 (10.0 / 50) 413.65 (10.3 / 75) 412.45 (11.5 / 100)

423.95

410.29 (3.0 / 100) 408.69 (4.6 / 53) 407.89 (5.4 / 52) 407.89 (5.4 / 50) 407.29 (6.0 / 30) 408.89 (4.4 / 24) 408.49 (4.8) 409.59 (3.7 / 50) 408.69 (4.6 / 100)

406.89 (6.4 / 100) 405.29 (8.0 / 50) 405.09 (8.2 / 45) 403.79 (9.5 / 43) 403.09 (10.2 / 21) 404.59 (8.7 / 20) 404.49 (8.8) 405.49 (7.8 / 50) 405.09 (8.2 / 100)

413.29

Sta.	B.S.	H.I.	F.S.	Elev.	
Check to Con. Mon. 40' Lt. of 41+52.77			3.35	443.28	443.82 / 0.46 error
35+77.37 = E.C. = Eq. P. 27					
+50					
35					
T.P.	12.15	447.63	0.34	435.48	
+50					
34					
T.P.	12.72	435.82 / 423.95	0.85	423.10	

Dwg No 519SAL has equation at Sta. 20+70.07 instead of here

Lt					℄					Rt
	14.8/100 432.83	6.9/50 440.73			3.8 443.83	4.5/15 443.13	5.7/17 441.93	6.6/40 441.03	5.2/42 442.43 · 5.8/50 441.83 · 7.7/76 439.93	10.7/100 436.93
	16.5/100 431.13	8.2/50 439.43			5.4 442.23	5.9/12 441.73	7.3/15 440.33	8.0/36 439.63	6.9/38 440.73 · 7.5/50 440.13	12.5/100 435.13
	16.8/100 430.83	10.1/50 437.53	9.0/6 438.63		9.8 437.83	11.2/6 436.43	11.2/28 436.43	10.9/35 436.73	11.4/50 436.23	16.3/100 431.33
					447.63					
6.1/100 429.72	4.9/94 430.92	1.8/50 434.82	1.1/6 434.72	3.5/6 432.32	3.3 432.52	3.4/18 432.42	2.1/21 433.72	3.6/50 432.22	8.2/100 427.62	
	9.5/100 426.32	6.9/50 428.92	6.6/18 429.22	8.4/13 427.42	7.7 428.12	8.6/10 427.22	6.4/12 429.42	7.5/50 428.32	11.8/100 424.02	
					435.82					

Check Levels
Soledad Rd.

12-15-47

P. 36 BM. Rock	7.48	282.96		275.48	
T.P.	4.62	276.35	11.23	271.73	
Check to N. Cor. BM Lower Step			10.70	265.65	265.51 / 0.14 error

checked Level and Fd. it to be out 0.005 by peg method

By Limey Method out .00125

12-16-47.

Re-adj. of Level by Peg method and is now O.K.

P. 53 check Levels Wilbur + Lamont to BM. Lower step of House

High Pt. on Large Rock 30' R Δ = 140°

Rods on Rex.
5.35
9.55
dif. 4.20

Rod at 200' dis.
8.59
-4.20
4.39 - should
4.385
0.005 error

Far nail - dif. 2.265
Near " 2.2525
0.0125 dif.

Top of hill

12-16-47

check Levels

B.M.	11.49	197.78		186.29	
T.P.	12.86	210.60	0.04	197.74	
T.P.	12.66	222.99	0.27	210.33	
T.P.	12.26	234.84	0.41	222.58	
T.P.	11.27	245.65	0.46	234.38	
T.P.	9.95	255.52	0.08	245.57	
T.P.	11.39	266.78	0.13	255.39	
T.P.	6.26	272.98	7.33	265.65	265.51
		2.		2.	0.14
					See P. 52

1408-54

SE 7'ld C.T. Lamont & Wilbur

Old City = 186.06
FB. 1324-47

Los Altos Rd.
N. Cor. Lowon Cov. Step of house #1751

265.28 = FB 1324-50 Feb. 9-34

" 1408.

265.51 Field B. Book

X sec. of 40' Park Rd. Sketch p.29

1+25 Soledad Park

W.O. 90058

1+00 W = Wash

0+90

0+50

0+00 B.C. Lt. From 10+73.41 Sta. Soledad Rd

B.M. 3.05 278.53 278.48 High PT. Big Rock 30' R. PT. Δ 140°

P.3C

	271.03	270.93	270.53	265.13	263.03	270.33	274.13
	7.5 / 40	7.6 / 20	8.0 / 11	13.4	15.5 / 9	8.2 / 20	4.4 / 30
	272.53	272.53	271.23	271.23	269.33	272.53	273.03
	6.0 / 30	6.0 / 20	7.3 / 8	7.3	9.2 / 11	6.0 / 20	5.5 / 30
					Begin Wash		
	273.13	273.13	271.73	271.33	272.83	273.03	
	5.5 / 30	5.4 / 20	6.8 / 10	7.2	5.7 / 20	5.5 / 30	
	273.23		273.63	274.03	273.53		
	5.3 / 20		5.9 / 2	4.5	5.0 / 20		
	275.53	275.73	274.83	275.23	276.38		
	3.0 / 20	2.8 / 16	3.7 / 15	3.3	2.2 / 20		

278.53

	Lt			℄		Rt
N 150	259.63	264.13		268.03	269.13	270.83	275.03
	18.9 / 40	14.4 / 20		10.5	9.4 / 15	7.7 / 20	3.5 / 40
	256.43	261.13	264.63	269.23	270.53	272.53	
	22.1 / 50	17.4 / 35	13.9 / 20	8.8	8.0 / 20	6.0 / 30	
2	262.53	255.13	261.13	265.33	269.93	272.93	
	16.0 / 70	23.4 / 45 W	17.4 / 20	13.2	8.6 / 20	5.6 / 30	
	Rim Canon						
	260.23	258.43	257.73	257.93	257.13	261.93	266.93	275.63
1+80	18.3 / 40	20.1 / 30	20.8 / 20	20.6 / 12	21.4 / 4	16.6 / 1X	11.6 / 20	2.9 / 47
	253.33							
	25.2 / 67							
	Bot. Wash							
	264.13							
	14.4 / 55							
	N. Rim of draw or canon							
	W = Wash							
1+50	267.83	267.83	267.63	267.83	260.83	265.23	270.23	275.73
	10.7 / 40	10.7 / 20	10.9 / 10	15.7	17.7 / 11 W	13.3 / 20	8.3 / 30	2.8 / 45
								Rim
	278.53			278.53				

From here on use your Contour map for Canon

+25

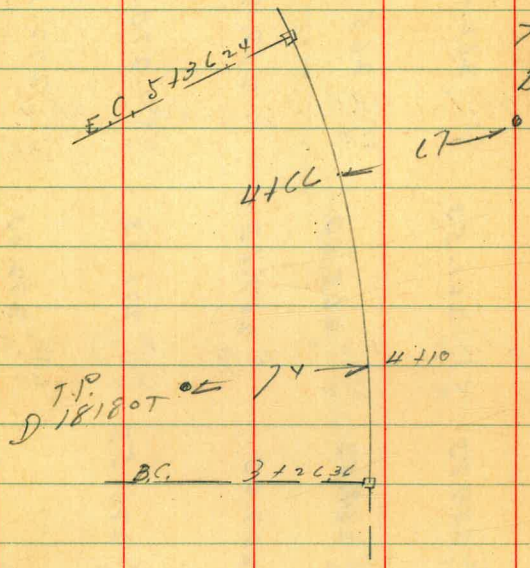
278.53

	Lt		Q	Rt
3+50	266.63	266.93	269.03	271.83
	11.9 / 40	11.6 / 20	9.5	6.7 / 20 — 4.6 / 30
3+26.36 B.C. Lt.	262.43	265.43	267.93	270.43 — 272.13
	16.1 / 40	13.1 / 20	10.6	8.1 / 20 — 6.4 / 30
3+14.73 E.C.	261.53	265.63	267.63	270.33 — 272.03
	17.0 / 40	12.9 / 20	10.9	8.2 / 20 — 6.5 / 30
3+00	259.83	264.53	267.03	270.53 — 271.63
	18.7 / 40	14.0 / 20	11.5	8.0 / 20 — 6.9 / 30
2+75	258.93	264.33	267.23	270.23 — 272.53
	19.6 / 40	14.2 / 20	11.3	8.3 / 20 — 6.0 / 30

278.53

278.53

5+36.24 E.C.



T.P.	9.93	286.79	1.67	276.80
4+00				
		279.53		

18.9	16.8	12.8	10.0	7.8
40	20		20	30
267.89	269.99	273.99	276.79	278.99
15.8	15.6	12.8	9.6	8.2
40	20		20	30
270.99	271.19	273.99	276.99	278.59
18.6	16.5	14.0	11.2	8.5
40	20		20	30
268.19	270.29	272.79	275.59	278.29
18.1	17.0	11.5	10.4	9.8
40	20		20	30
268.69	269.79	275.29	276.39	277.39
12.7	9.3	6.0	3.5	0.3
40	20		20	30
266.33	269.23	272.53	275.03	278.23

286.79

279.53

7+50							
	12.9	297.23	1.75	285.04			
7							
6+50							
6							
5+50							
		-286.79					

	272.93	282.13	283.23	286.73	287.93	288.93	291.63
	24.3	15.1	14.0	10.5	9.3	8.3	5.6
	50	26	20		20	30	80
							Ridge
	267.49	270.19	281.09	282.49	284.69	286.29	
	19.3	8.6	5.7	4.3	2.1	0.5	
	45	20	11		20	30	
	261.89		270.79	277.79	281.89	282.99	286.79
	24.9		16.0	9.0	4.9	3.8	0.0
	45		20		20	30	85
							Ridge
	264.49		269.59	274.99	279.59	280.69	
	22.3		17.2	11.8	7.2	6.1	
	50		20		20	30	
	267.99		270.59	274.89	276.79	279.09	
	18.8		16.2	11.9	10.0	7.7	
	40		20		20	30	
			-286.79				

Soledad Park Rd.

Turn Back

to T.P. ~~…~~	309.03	π
~~…~~	13.03	
~~P.33~~	296.00	T.P.
	1.01	
10+38.59 old 2x2 Hub, P.34 Rock T.P. 282.33	297.01	π
	13.30	
	283.71	
	5.28	
	288.99	π
	6.69	
	282.30	

10+08.64 23°34' Lt.

+50

9

+50

T.P. 1303. 309.03 1.23 296.00

8

297.23

Lt ℄ Rt

59

Lt		℄		Rt	
		3.88 / 305.15			
7.5/40 301.53	5.3/20 303.73	3.4 305.63	2.5/20 306.53	2.7/30 306.33	
10/40 298.63	8.7/20 300.33	6.2 302.83	4.6/20 304.43	4.1/30 304.93	
15.0/40 294.83	11.4/20 297.63	9.1 299.93	7.5/20 301.53	6.9/30 302.13	
18.7/40 290.33	14.7/20 294.33	12.5 296.53	11.1/20 297.93	10.3/30 298.73	9.2/55 Ridge 299.83
11.7/40 285.53	8.0/20 289.23	5.6 291.63	4.3/20 292.93	3.5/30 293.73	
		309.03			

297.23

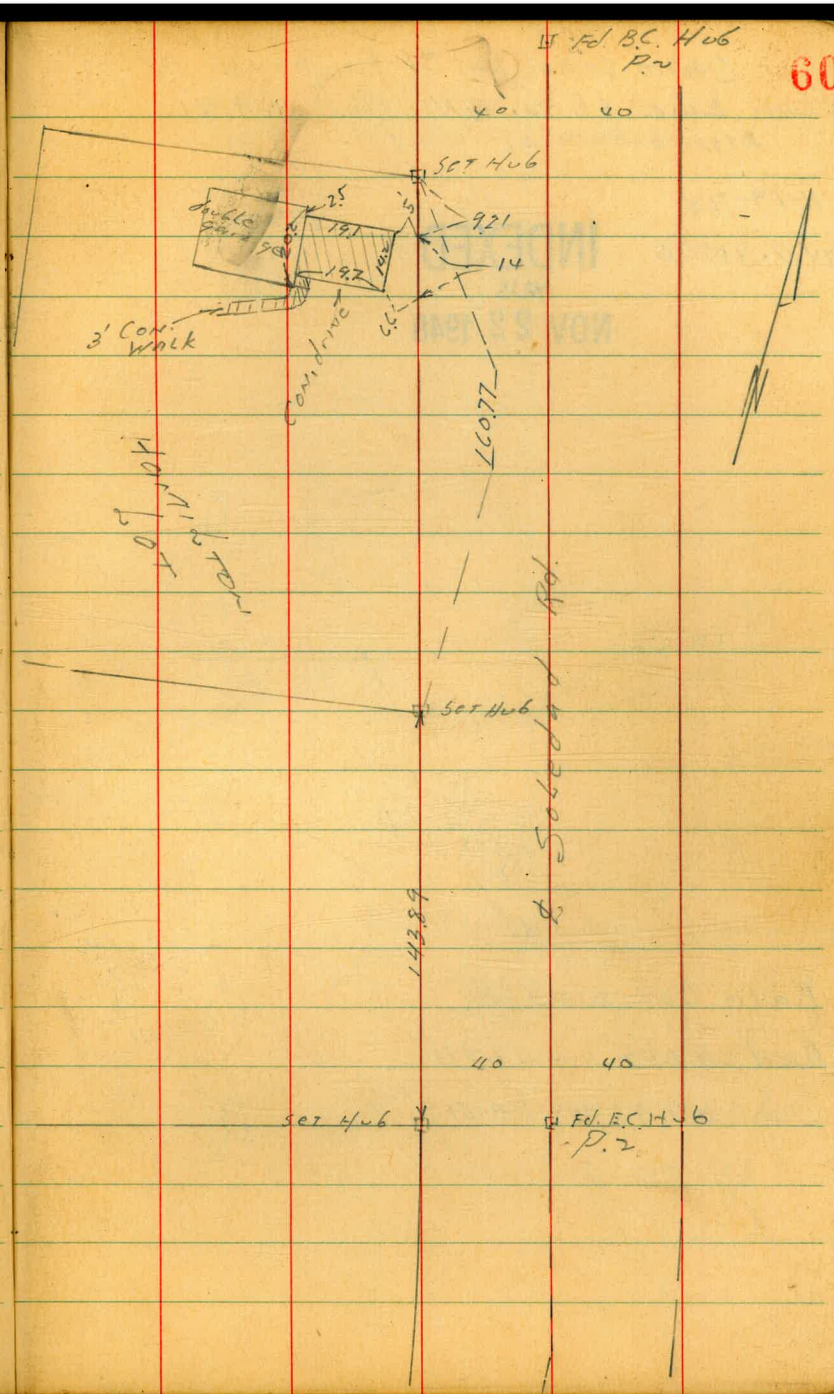
Location of Double Garage and Con. Drive on Soledad Rd. Hamilton Lot

Moore
BC99
Sherman
Bunch
9-17-48

W.O. 90058

Set 6 & 10 setback stakes

S.E. Cor drive		8.21		
S.W. Cor drive		7.30		
N.W. Cor drive		7.30		
N.E. Cor. Con. drive		7.55		
T.P.	1.40	358.92	12.12	357.52
BC Hub 7+82.45 P.7	0.34	369.64		369.30

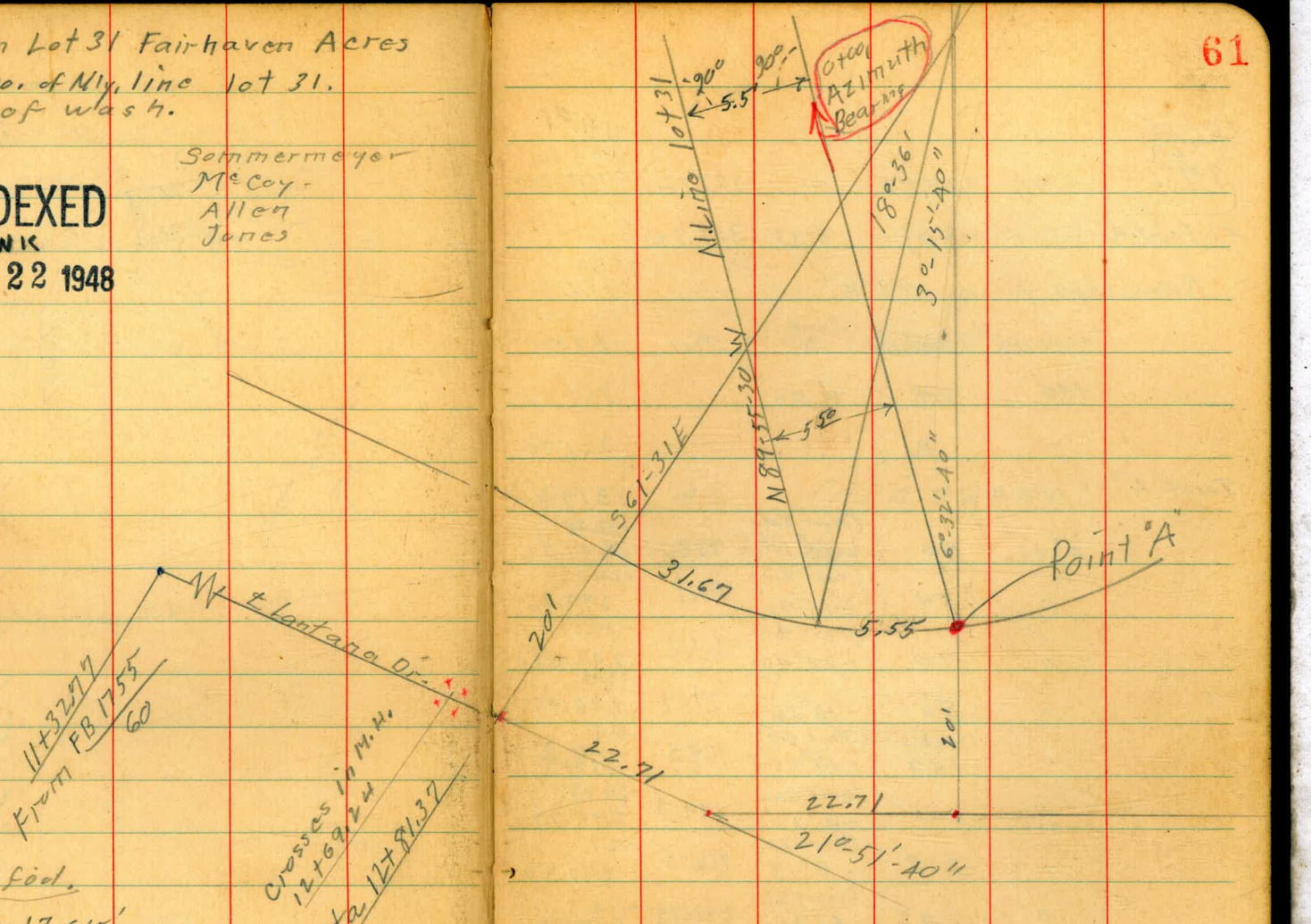


Storm Drain Lot 31 Fairhaven Acres
on Line 5± So. of Nly. line lot 31.
Also bottom of wash.

11-19-48
W.O. 3150G

INDEXED
WK
NOV 22 1948

Sommermeyer
McCoy-
Allen
Jones



Rate Def. per foot.

Rad = 97.58' = 17.61°

" = 117.58' = 14.61°

Curve figures to establish point "A" (5± So. of Nly. line lot 31) are on page 63.

FB 1755
69

BM #1					BM #1 Nails in Pole PA798
BM #1	0.43	328.15	—	327.72	
El. Point "A" - (see sketch)			8.35	319.80	

Readings From Pt. "A"

El. = 319.80

	Azimuth	Stadia Dist	Vert Δ	Dist	Elev.
	180°	24	0° 00'		321.20
	"	2	"		321.70
Point "A"					319.80
	0° 00'	40	(Boot 8.0) -23° 11'	33.8	-22.48 297.32
	"	54	(Boot 8.0) -15° 40'	50.1	-22.04 297.76
	"	70	(Boot 4.0) -20° 45'	61.2	-27.19 292.61
	"	86	-16° 26'	79.12	-23.33 296.47
	"	(108.5) 120	(Boot 6.0) -18° 05'	108.5	-41.4 278.4
	"	201	(Boot 6.0) -5° 10'	199.3	-24.03 295.77
	"	218	(Boot 7.0) -5° 18'	216.15	-27 292.80
	"	248	(Boot 6.0) -6° 35'	244.75	-34.3 285.5
	6° 00' Rt	71	(Boot 12.0) -15° 55'	65.65	-30.72 289.1
	11° 03' Rt	100	(Boot 12.0 -14° 15'	93.94	-35.9 283.9
	13° 30' Rt	128	(Boot 12.0 -12° 47'	121.74	-39.61 280.2
	16° 35' Rt	190	(Boot 12.0) -11° 45'	182.15	-49.59 269.9

0° 00' 00" Azimuth ∠ = S 89° 55' 30" E

HI Rod 4.6 (HI = 324.40)

Bottom of Wash

Bottom of Wash

" " "

" " "

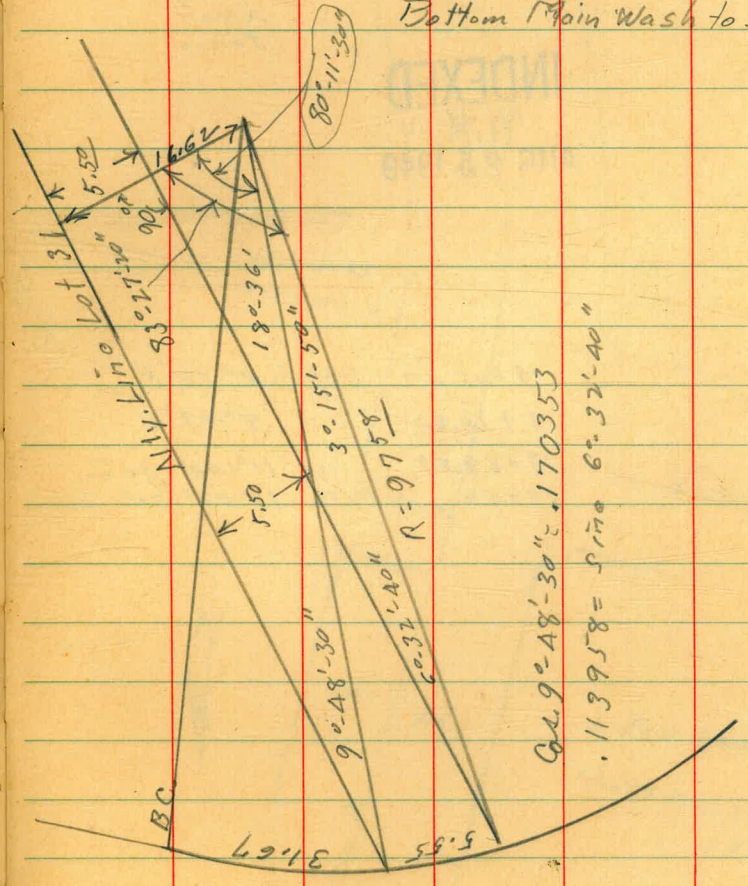
" " "

	Azmuth	Stad. Dist	Vert. Δ	Dist.	Elev.
Pt "A"		328.15'			319.80
Pt "A"			(Boot 14.0)		-64.5
	17°20'Rt	300	-9°47'	291.3	255.3
			(Boot 17.0)		-80.7
	14°25'Rt	385	-9°40'	374.1	239.1
			(Boot 8.0)		-78.9
	17°23'Rt	402	-10°20'	389.1	240.9

(H.T. Rod 4.6) Bottom of Wash

Junction of No-South Wash with Main wash

Bottom Main Wash to South



Additional Notes

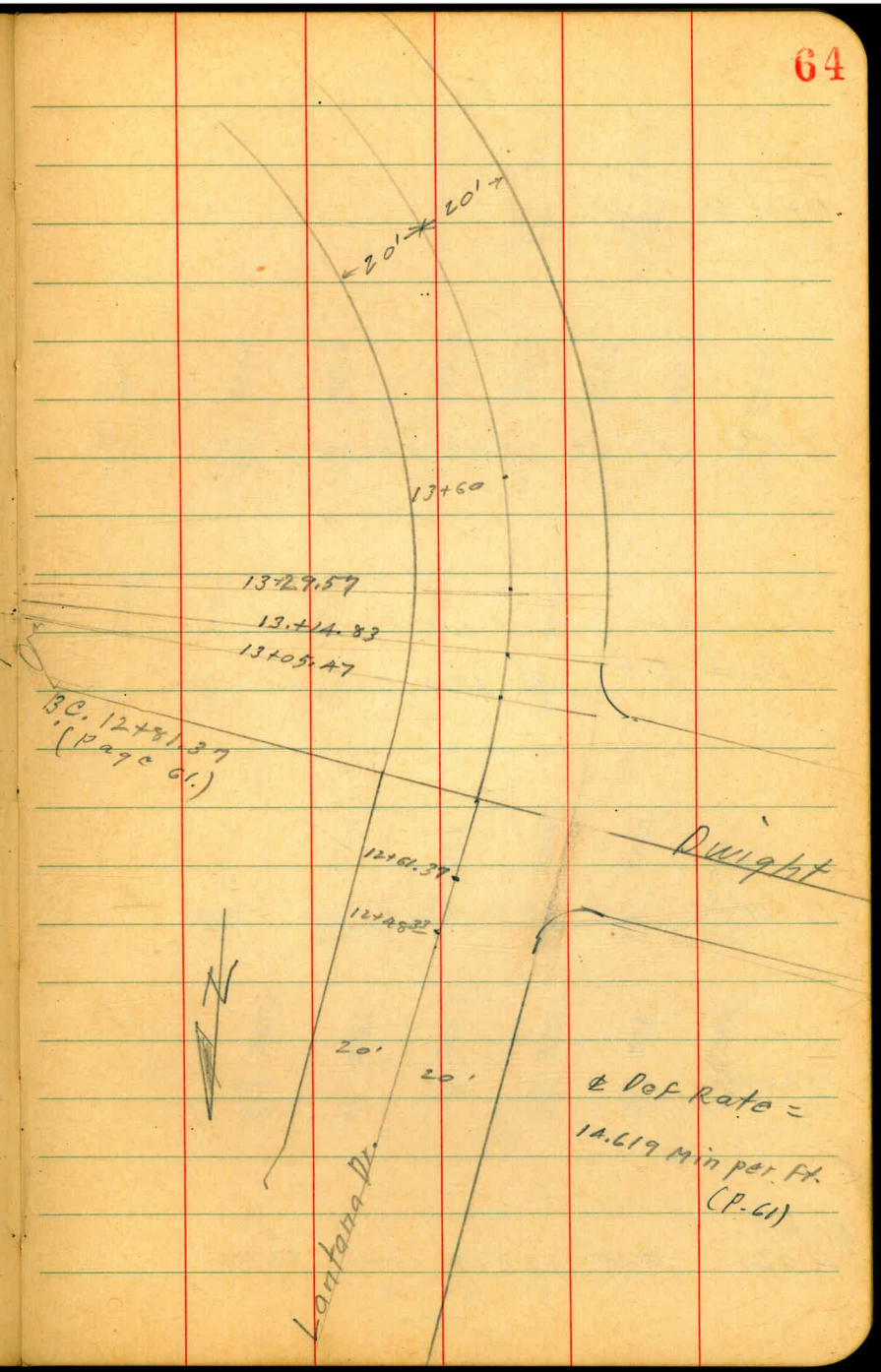
Lantana & Dwight

11-30-48
W.P. 3150G

orig 1755/59 & 1797/61

Sommermeyer
McCoy
Allen
Jones

13+05.47	Def =	5°-52'+
13+14.83	" =	8°-09'+
13+29.57	"	11°-44'-40"—
13+60	"	19°-09'-30"



Lantana Dr.

℄

13+05 47	Cont.								
13+05 47	17' Lt. = Canyon rim								
12+81 37 = B.C.	15' Lt. = canyon rim								
12+61 37	20' Lt. = Canyon rim								
12+48 37									
BM#1 P. 62	0.45	328.17	—	327.72					

13+05 47 Cont.					326.0 2.2/30	328.2 0.0/40		
13+05 47	318.3 7.9/25	320.5 7.7/20	321.8 6.4/17	322.0 6.2	322.1 6.1/9	323.2 5.0/12	324.4 3.8/17	324.4 3.8/20
12+81 37	317.9 10.3/25	319.6 8.6/20	322.1 6.1/15	323.2 5.0	324.9 3.3/20			
12+61 37		320.4 7.8/25	322.9 5.3/20	324.3 3.9	324.8 3.4/20	327.2 1.0/30	328.2 0.0/38	
12+48 37		323.3 4.9/20	324.6 3.6/10	325.2 3.0	325.3 2.9/13	328.1 0.1/15	328.4 +0.2/20	

328.17

Lantana Dr.

13+60 12' Lt. = Canyon rim

13+29.57 15' Lt. = Canyon rim

13+14.83 17' Lt. = Canyon rim

℄

314.8	316.6	320.7	320.7	321.0	323.2	323.9	326.4
13.4/25	11.6/20	7.5/12	7.5	7.2/10	5.0/11	4.3/20	1.8/30
316.4	318.9	321.0	321.2	321.4	324.3	324.3	327.0
11.8/25	9.3/20	7.2/15	7.0	6.8/10	3.9/16	3.9/20	1.2/30
317.8	320.1	321.6	321.6	321.9	325.7	325.7	327.4
10.4/25	8.1/20	6.6/17	6.6	6.3/10	2.5/16	2.5/20	0.8/30

328.17

Beech St.

X-Sec. for grade Est'mt.

8-24-49

W.O. 25020 (Blue° 3904)

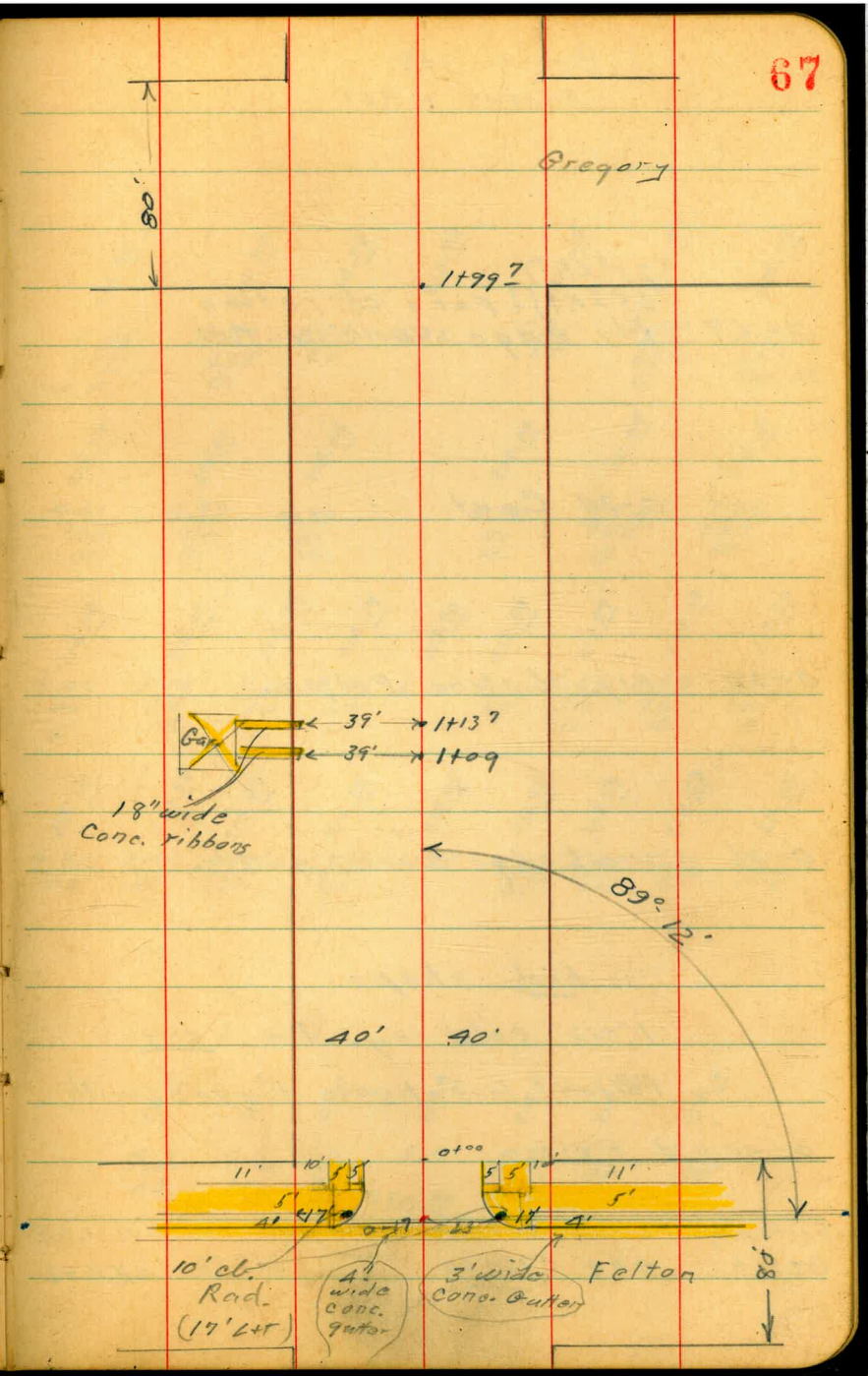
Sommermeyer
McCoy
Allen
Rorer.

● = Fd. L+T. (T.P. sheet °192)

• = Set nail

F.B. 949
21

Notes Reduced & Plotted
Profile 3619
McClaren
9-7-49



Beech St.
Sketch = P. 67

25^{5} Lt. }
25^{3} Rt. } = Face cl. return
0-19 Ely edge conc. gutter.

0-20 Cont.

0-20 = Ely. cl. line Felton

0-23 = west edge conc. gutter.

Felton has been topped with
1" to 2" cold lay. in very
bad shape.

0-40 = ℄ Felton

Felton & Beech	4.04	220.00	—	215.96 N.W.B.P. = B.M. #1

214.95 / 5.05 / 25^{5} / Top. cl.	214.30 / 5.70 / 25^{5} / G.	214.28 / 5.72 / 20	213.98 / 6.02	213.65 / 6.35 / 20	213.47 / 6.53 / 25^{7} / G	214.02 / 5.98 / 25^{7} / Top. cl.		
215.59 / 4.41 / 100 / cl.	215.01 / 4.99 / 100 / G.	215.04 / 4.96 / 40 / cl.		214.00 / 6.00 / 40 / cl.	211.46 / 8.54 / 100 / G	212.15 / 7.85 / 100 / cl.		
214.54 / 5.46 / 40 / G.	215.00 / 5.00 / 30 / cl.	214.34 / 5.66 / 30 / G	214.19 / 5.81 / 20 / G.	213.90 / 6.10	213.59 / 6.41 / 20	213.37 / 6.63 / 30 / G	214.03 / 5.97 / 30 / cl	213.33 / 6.67 / 40 / G
215.18 / 4.82 / 100	214.58 / 5.42 / 40	214.49 / 5.51 / 30	214.32 / 5.68 / 20	214.05 / 5.95	213.73 / 6.27 / 20	213.59 / 6.41 / 30	213.53 / 6.47 / 40	211.65 / 8.35 / 100

215.3 / 4.7 / 40	215.2 / 4.8 / 30	215.0 / 5.0 / 20	214.9 / 5.1	214.5 / 5.5 / 20	214.2 / 5.8 / 30	214.0 / 6.0 / 40

220.00

Beech

same drive

1+13.7 — 39°Lt. = ℄ Ely. ribbon (18" wide)

ribbon drive

1+09 — 39°Lt. = ℄ wly ribbon (18" wide) of

T.P	5.27	218.45	6.82	213.18

1+00

0+50

0+00 Cont.

0+00 — 20' Rt. / 20' Lt. } = End cl. — end of walk: 30' Lt. / 30' Rt. } = Back edge

0-10 — 20' Rt. / 20' Lt. } = cl. E.C.

220.00

℄

216.89 / 1.56 / 68 Gar. floor

216.82 / 1.63 / 48.5

214.98 / 3.47 / 40

214.76 / 3.69 / 39

216.90 / 1.55 / 68 Gar. floor

216.85 / 1.60 / 48.5

215.00 / 3.45 / 40

214.78 / 3.67 / 39

218.45

215.9 / 4.1 / 60

214.7 / 5.3 / 40

213.5 / 6.5 / 20

213.2 / 6.8

212.2 / 7.8 / 25

210.2 / 9.8 / 40

207.7 / 12.3 / 60

215.5 / 4.5 / 40

214.4 / 5.6 / 20

213.7 / 6.3

213.2 / 6.8 / 19

210.4 / 9.6 / 40

217.3 / 2.7 / 60

216.3 / 3.7 / 40

216.0 / 4.0 / 30 End

214.0 / 6.0 / 30 End.

212.9 / 7.1 / 40

212.1 / 7.9 / 60

215.23 / 4.77 / 30 walk

214.98 / 5.02 / 20 cl.

214.7 / 5.3 / 20

214.2 / 5.8

214.0 / 6.0 / 20

214.05 / 5.95 / 20 cl.

214.20 / 5.80 / 30 walk

214.93 / 5.07 / 20 cl.

214.1 / 5.9 / 20

214.1 / 5.9

213.7 / 6.3 / 20

214.01 / 5.99 / 20 cl.

220.00

Beech.

B.M. #1 - P. 68			2.73	215.97	215.96
T.P.	5.09	218.70	8.84	213.61	
3+50					
2+79 ± : Ely line Gregory					
2+39 ± = ℄ Gregory					
1+99 ± Wly. Gregory					
T.P.	5.89	222.45	1.89	216.56	
1+50					
		218.45			

℄

207.2

15.3

211.4	213.8	215.0	215.7	215.5	215.3	212.1
11.1 / 75	8.7 / 40	7.5 / 20	6.8	7.0 / 20	7.2 / 40	10.4 / 75
213.0	217.1	218.0	218.7	218.4	217.4	210.4
9.5 / 100	5.4 / 40	4.5 / 20	3.8	4.1 / 20	5.1 / 40	12.1 / 100
217.3	217.0	216.8	216.6	216.4	215.2	213.5
5.2 / 75	5.5 / 40	5.7 / 20	5.9	6.1 / 20	7.3 / 40	9.0 / 75

222.45

215.1	214.1	213.5	212.3	211.5	208.4
3.4 / 40	4.4 / 20	5.0	6.2 / 14	7.0 / 40	10.1 / 70

218.45

Xenophon & Locust

Check S. Ely. walk.

6' walk - 2' gutter on ct. face

Red & yellow = New curb & walk

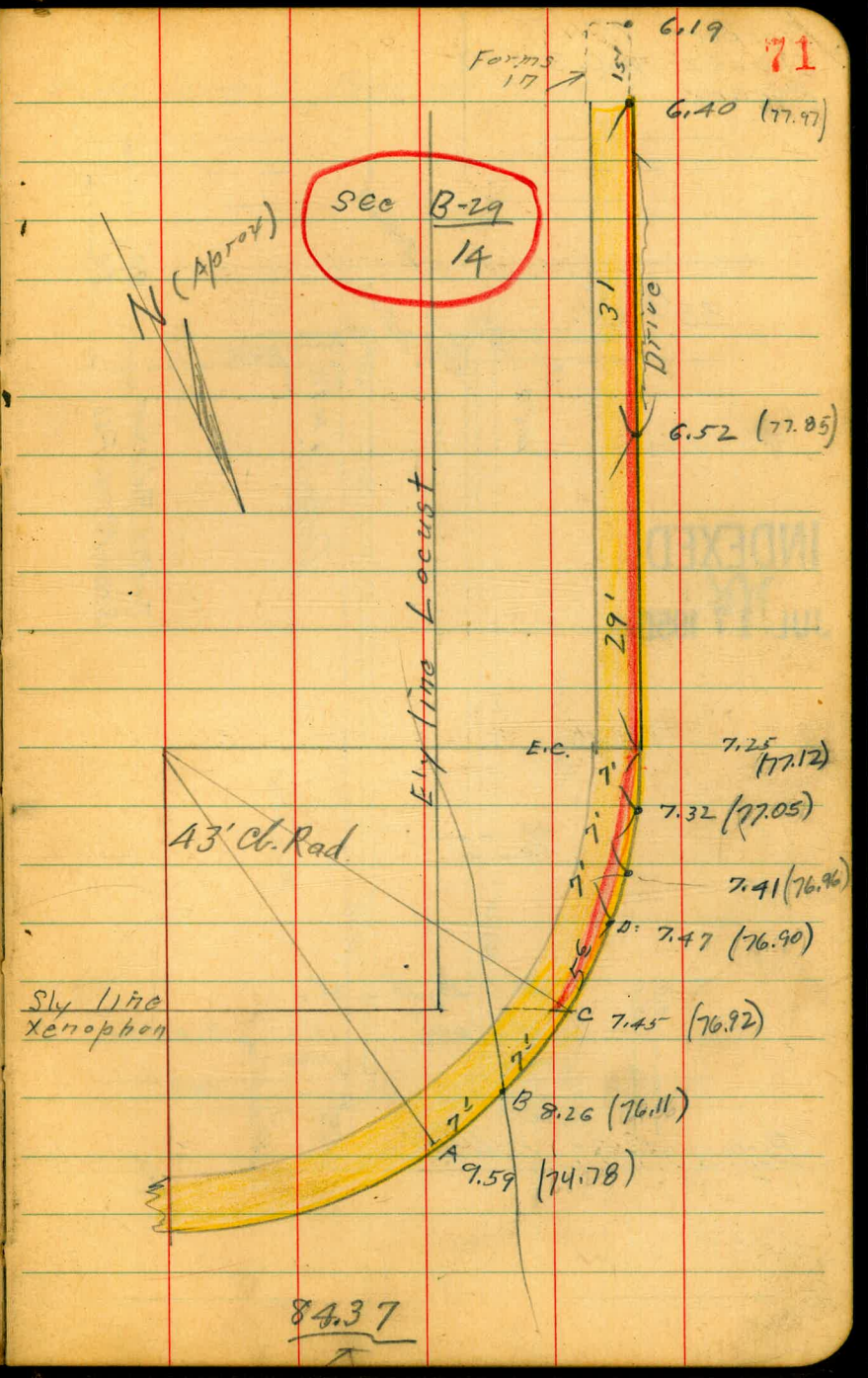
yellow alone = old curb & walk.

replaced but was not removed.
Curb. A to B (14½') was to have been

B.C. & 0+ stake: F 2.24 - Rod: 7.47

6.55 84.37 77.82

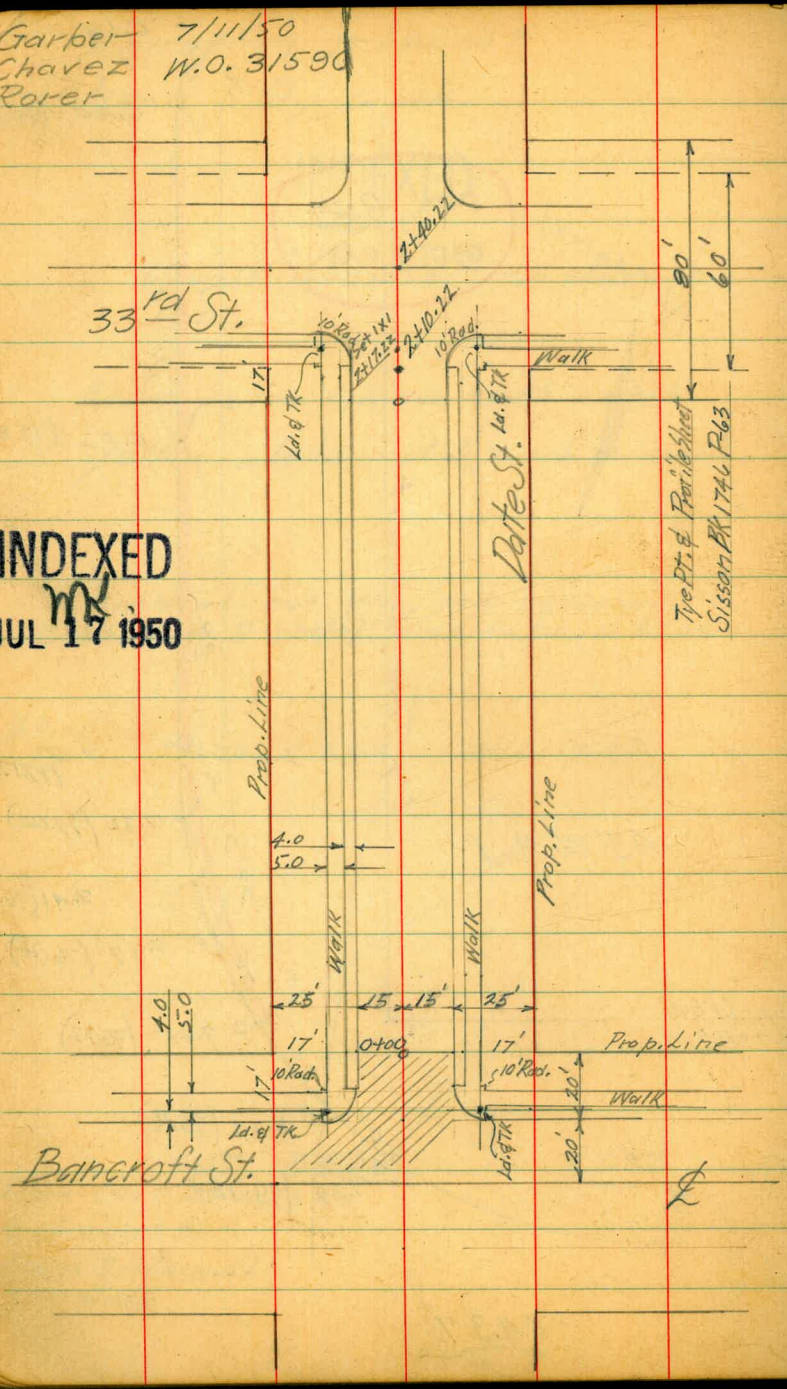
L4 Disk So. of Xenophon & Locust. (From Sidewalk book)



Garber 7/11/50
Chavez W.O. 31590
Rorer

X-Sec. Dorte St., Bancroft to 33rd

72



+54 ℄ 9.0 Conc. Dr.

+50

+24 30" Palm 17.0 Lt.

0+00

-10 E.C. curb return

Center of curb return

-20

0-40

6.63	233.69	6.01	227.06	NE Lot & TK Bancroft 1 & Date
6.51	233.07		226.56	NE 1'Ld. & TK 32nd & Date

℄

4.8 40 | 4.53 24 WIK | 4.61 19 WIK | 5.31 15

228.6 228.18 228.36 228.8 229.0 229.85 229.96 229.6

5.1 40 | 4.71 19 WIK. | 5.33 15 Conc. Dr | 4.9 | 4.7 15 GUT | 3.84 15 Cb | 3.73 19 WIK | 4.1 40

227.3 227.38 227.29 226.7 227.21 227.4 228.28 228.41 229.0

6.4 40 | 6.31 19 WIK | 6.42 15 Cb | 7.0 15 GUT | 6.48 | 6.3 15 GUT | 5.41 15 Cb | 5.28 19 WIK | 4.7 40

226.75 227.00 226.49 227.11 227.31 227.98 228.7

6.94 40 | 6.69 15 Cb | 7.20 15 GUT | 6.58 | 6.38 15 GUT | 5.71 15 Cb | 5.10 40

224.93 226.30 227.24 228.93

6.76 Cb | 7.39 GUT | 6.45 GUT | 5.76 Cb

224.97 227.24 226.15 225.85 226.89 226.27 226.49 226.94 227.19 227.39 228.02 227.75 229.62 230.25

8.77 100 Cb | 4.07 100 GUT | 3.44 100 Cb

9.45 100 GUT | 7.14 40 Cb | 7.84 40 GUT | 6.80 25 Cb. | 7.42 25 GUT | 7.20 15 | 6.75 | 6.50 15 | 6.30 25 GUT | 5.67 25 Cb | 5.94 40 GUT | 5.20 40 Cb.

225.19 226.91 227.49 227.66 228.04 229.82 232.79

8.50 100 | 6.78 40 | 6.20 15 | 6.03 | 5.65 15 | 4.87 40 | 2.90 100

233.69

+53 ℄ Conc. Dr. 8° Wide (Ribbons from walk to Garage)

+41 ℄ 11.0 Conc. Dr. (From wilk 2-1.5 Ribbons 6° Over-all)

TP 8.25 239.58 2.36 231.33

+18 End Conc. Dr.

+07 ℄ 7.0 Conc. Dr. 2 Ribbons 1° Wide, 6° outside meas. from wlk to garage

+02 Begin Conc. Dr. also Power Pole # P3271 16.7 Rt.

1+00

1+89 ℄ 2.5 Conc. Walk

1+76.5 ℄ 4.0 Conc. Walk

232.7 | 232.13 | 232.10 | 231.4 | 232.2 | 232.48 | 233.21 | 233.34 | 233.34

6.9 / 10 | 7.35 / 19 / Wlk | 7.48 / 15 / Cb | 8.2 / 15 / Gut | 7.4 | 7.10 / 15 | 6.37 / 19 | 6.24 / 24 | 6.24 / 40

232.08 | 232.85 | 232.93 | 232.82

7.50 / 15 | 6.73 / 19 | 6.65 / 24 | 6.76 / 40

231.01 | 231.29 | 231.12 | 230.45 | 239.58

2.68 / 40 | 2.40 / 24 | 2.57 / 19 | 3.24 / 15

231.06 | 231.75 | 231.81 | 231.81

2.63 / 15 | 1.94 / 19 | 1.88 / 24 | 1.88 / 40

230.80 | 230.75 | 230.65 | 229.96

2.89 / 40 | 2.94 / 24 | 3.04 / 19 | 3.73 / 15

230.29 | 230.57 | 230.15 | 229.7 | 230.6

3.40 / 40 | 3.12 / 19 / Wlk | 3.24 / 15 / Cb | 4.0 / 15 / Gut | 3.1

230.5 | 231.45 | 231.53 | 231.9

3.2 / 15 / Gut | 2.24 / 15 / Cb | 2.14 / 19 / Wlk | 1.8 / 40

231.04 | 231.29 | 231.82

2.65 / 15 / Cb | 2.40 / 24 / Wlk | 1.83 / 37 / Wlk

229.52 | 229.92 | 229.66

4.16 / 40 / Wlk | 3.77 / 24 / Wlk | 4.03 / 15 / Cb

233.69

Con. Mon. S/E
Cor. 33rd Date
Rec. 238.56

+40.22 ℄ 33rd St.

+20.22

Centers of curb returns

+10.22

+9.5 Power Pole #3299 16.5' Rt.

2+00

+83 ℄ 3.6 Conc. Wlk

1.03 238.55

235.0 235.9 235.3 234.3 234.0 234.4 234.8 234.8 234.8

4.6 3.7 4.3 5.3 5.6 5.2 4.8 4.8 4.8
100 72 50 40 15 15 50 100

234.1 235.4 233.45 233.4 233.9 233.7 233.6 234.2 234.0 234.1 234.2 234.74

5.5 4.2 6.13 6.2 5.70 6.3 6.0 5.4 5.6 5.6 4.72 5.5 4.76 5.4 4.84
100 45 40 Clb 40 Gut 25 Clb 25 Gut 15 15 25 Gut 25 Clb 40 Gut 40 Clb 100 Gut 100 Clb

234.10 234.81

6.5 Gut 5.70 Clb 5.6 Gut 4.77 Clb

233.92 233.3 234.1 234.83

5.66 6.3 5.5 5.9 4.75
15 Clb 15 Gut 15 Gut 15 Clb

235.5 234.3 233.78 233.72 233.64 233.0 233.8 233.6 234.55 234.65 235.2

4.1 4.3 5.80 5.86 5.94 6.6 5.8 6.0 5.03 4.93 4.4
40 33 27 Wlk 19 Wlk 15 Clb 15 Gut 15 Clb 19 Wlk 40

234.02 234.15 234.77

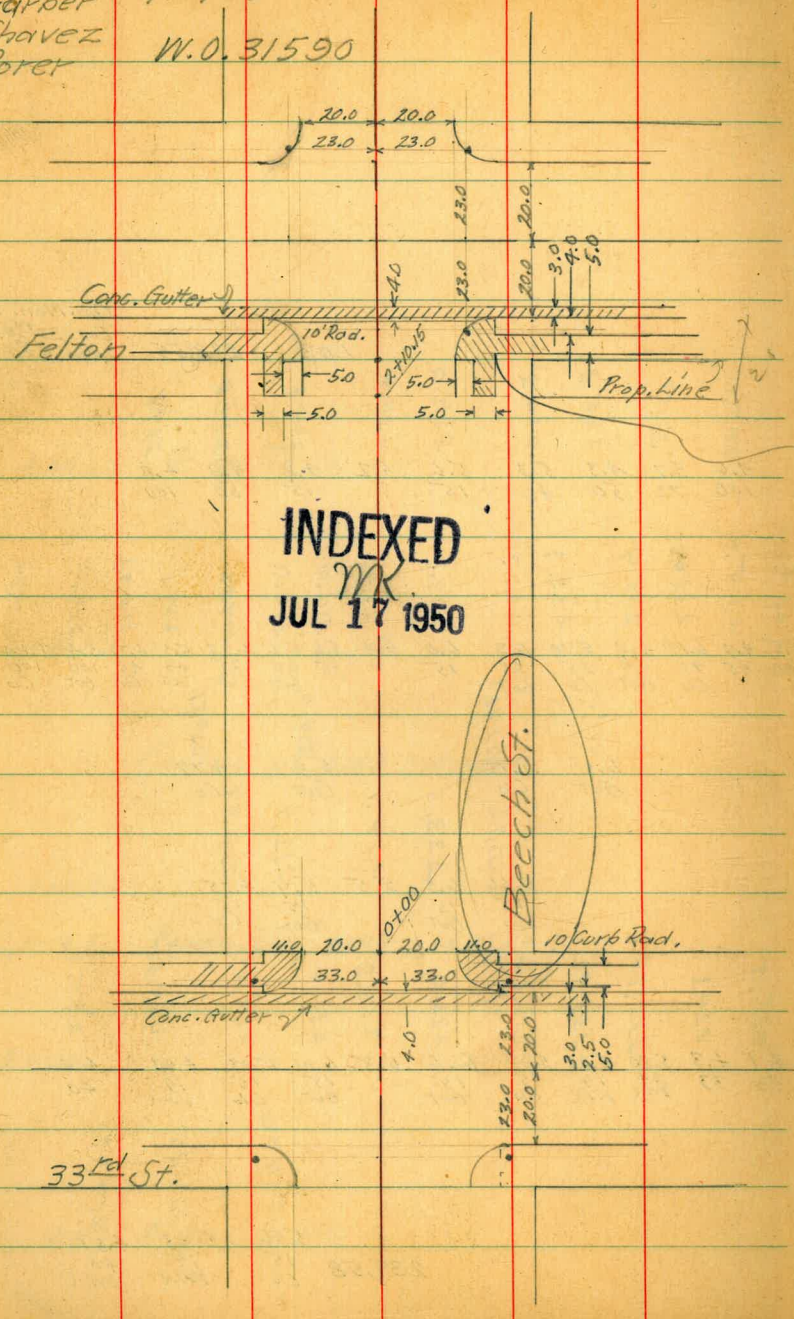
5.56 5.43 4.81
15 Clb 19 Wlk 40 Wlk

239.58

Garber
Chavez
Rorer

7/14/50

W.O. 31590



INDEXED
MR
JUL 17 1950

X-Sec. Beech St. 33rd to Felton

76

NW & SW Returns

→ New Curbs 20'R Set in Sidewalk

Book B-27
Page 74

+03 ℄ Conc. Steps 1st of 4 3° Wide = 37.5 Lt.

0+00

Center of curb returns

-09 Conc. Gutter

-10 Conc. Gutter

-13 Conc. Gutter

0-30 ℄ 33 Rd

6.42 226.01 219.57 Con. Mon. S.E. 33 Rd & Beach

3.46 100 Cb 4.20 100 Gut

220.4 224.91 221.8 221.51 220.4 217.1 217.0 219.4

5.6 3.10 41 Top. Conc Wall 5.2 40 4.50 37.5 5.4 20 6.5 7.0 20 6.6 40

220.33 220.18 220.08 220.4 219.4 219.8 219.00 219.11 219.28

5.68 31 Wlk 5.83 24 Wlk 5.93 20 Cb 5.6 20 Gut 6.6 7.2 20 Gut 7.01 20 Cb 6.90 24 Wlk 6.73 31 Wlk

219.96 219.7 219.51 219.41

6.05 Cb 6.3 Gut 7.5 Gut 6.90 Cb

219.99 219.82 218.81 219.40 219.09

6.02 26 Cb 6.79 26 Gut 7.20 7.61 Gut 26 6.92 Cb 26

220.06 219.29 220.06 219.33 219.18 219.10 218.77 218.50 218.39 218.32 219.10 218.06

5.95 40 Cb. 6.72 40 Gut 5.95 30 Cb. 6.78 30 Gut 6.83 26 6.91 20 7.24 7.51 20 7.62 26 7.68 30 Gut 6.91 30 Cb 7.95 40 Gut

219.27 218.84 219.61 219.08 212.1

6.74 26 7.13 7.40 26 6.92 40 Cb 13.60 100 Gut 12.78 100 Cb

222.2 220 219.8 219.7 219.5 219.1 216.7 216.2 212.6

3.8 100 6.0 40 6.2 30 6.3 20 6.5 6.9 20 7.3 30 7.8 40 13.4 100

226.01

+75 End of 5° Conc. Blk. Wall 37.3 Lt.

+68 Center of 8° Conc. Dr. 37.0 Rt

+60 Angle Pt. in fence 36.0 Rt. (End of fence)

+50

+40

+30 Begin Conc. Block Wall 5.0 High 39.0 Lt.

+21.5 & 15.0 Conc. Drive 39.8 Lt.

+09 Begin solid wood 4° fence 38.5 Rt.

+08 Power & Phone Pole # P3315 35.0 Rt

1+00

+97 & 15' Conc. Drive 48.8 Lt

5.88 228.15 3.74 222.27

+50

0+10 226.01

225.9 225.4 224.7 224.4 225.1 224.8 219.9 219.5 219.9 219.98

1.5 2.0 2.7 3.0 2.3 2.6 7.5 7.9 7.5 7.45

40 37 37 33 20 14 20 40 40 Edge Wlk

Wall Ft. (Hedge

Pt 7.12 227.43 H.I. 7.84 220.31 220.30

7.81 7.85

37.0 43

227.3 226.8 226.2 223.0 222.1 221.3 221.1 220.6

0.9 1.4 2.0 5.2 6.1 6.8 7.1 7.6

50 38 14 20 36 40 50

227.5 227.0 226.8 224.8 223.5 222.1.6 224.6 220.8

0.7 1.2 1.4 3.4 4.7 5.6 6.6 6.6 7.4

50 38.5 227.0 23 10 20 36 40 50

1.4 1.2 227.34

39 39

Bot. Foot. 228.08

0.07 0.81

52 39.8

227.2 225.2 223.5 222.5 222.7 221.5

1.0 3.0 4.7 5.9 5.5 6.7

40 20 20 21 40

229.45 228.05

+1.30 0.10

66.3 48.8

226.8 226.5 224.11 222.2 228.15 H.I. 221.4 221.7 220.6 220.4

+0.8 +0.5 1.9 3.8 4.0 4.6 4.3 5.4 5.6

50 40 16 5 22 19 20 40 50

225.2 224.6 224.5 224.3 222.0 220.1 219.2 220.0 219.1 217.0

0.8 1.4 1.50 1.7 4.0 5.9 6.8 6.0 6.5 7.0

50 40 36.5 28 20 226.01 19 20 40 50

Pt 1.5 Wlk H.I.

should be (O.T.J.)

+50.15

+40.15 ℄ Felton

(X) +33.15 Ely edge gutter

+30.15 Curb Line

+29.15 Wly edge gutter

Center of returns

+20.15 B.C. Cb. return & End Rock Wall Lt.

+10.15 Prop. Line

2+00

BB NW Beech & Felton 215.96

5.90 215.96

215.97 215.46 214.18 214.95 214.58 213.87 212.44

5.89 100 | 6.40 50 | 6.68 20 | 6.91 | 7.28 20 | 7.99 50 | 9.42 100

215.35 214.19 214.87 214.52 214.48 214.26 215.05 214.20

6.61 26 | 6.67 20 | 6.99 | 7.34 20 | 7.38 26 | 7.60 30 Gut | 6.81 30 Cb | 7.66 40 Gut

222.17 221.3 215.93 215.19 215.96 215.14 215.10 215.07 214.74 214.39 214.34 214.96

5.26 100 Cb | 6.06 100 Gut | 5.93 40 Cb | 6.67 40 Gut | 5.90 30 Cb | 6.72 30 Gut | 6.76 26 Gut | 6.79 20 | 7.12 | 7.47 20 | 7.52 26 | 6.90 40 Cb. | 9.90 10' Gut | 9.16 10' Cb

215.96 215.17 215.16 214.82 214.50 214.61 215.07

5.90 26 Cb | 6.69 26 Gut | 6.70 20 | 7.04 | 7.36 20 | 7.47 26 | 6.79 26 Cb

216.97 214.3 214.5 215.18

5.89 Cb | 7.6 Gut | 7.4 Gut | 6.78 Cb

218.71 216.26 216.08 215.89 215.8 215.3 214.9 215.00 215.18

3.15 31 Top Wall | 5.60 31 Wlk | 5.78 25 Wlk | 5.97 20 Cb. | 6.1 20 | 6.6 | 7.0 20 | 6.86 20 Cb | 6.68 25 Wlk

& Base Rock Wall

221.4 217.8 216.29 216.10 215.87 216.7 215.8 215.6 215.00 215.21 216.2

0.5 40 | 3.1 31 Top Wall | 5.57 31 Wlk | 5.76 25 Wlk | 5.99 20 Cb. | 5.2 20 | 6.1 | 6.3 20 | 6.86 20 Cb | 6.65 25 Wlk | 5.7 40

Base Rock Wall

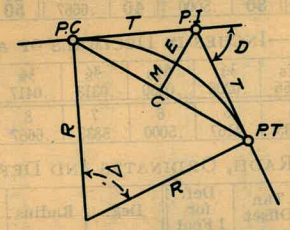
FF 5.95 221.86 H.I. 11.52 215.91

222.9 221.4 220.3 218.8 218.31 216.7 216.2 216.9 217.20 217.23

4.5 40 | 6.0 34 | 7.1 31 | 8.6 20 | 9.1 8 | 10.7 | 11.2 26 | 10.5 30 | 10.23 39 Edge Wlk | 10.20 40.5 Wlk

End Hedge 227.43 H.I.

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\sin. D/2}$(1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=Rtan$\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=Rvers $\frac{\Delta}{2}$ (6)

External=E=Ttan$\frac{\Delta}{4}$-(7)=R÷cos.$\frac{\Delta}{2}$—R(8)=Rexsec$\frac{\Delta}{2}$(9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50 \div 100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

6.19 707 114 523

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.