

1800

WELDEN
J. WELDEN

ENGINEERS

FIELD BOOK

No. 404F

EUGENE DIETZGEN CO.

DRAWING MATERIALS MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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1800

120

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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

1-9 X-Sec. BIK 39 City Hgts

10-18 " Snowdrops Arbor Vitae

19 Location Bldg Merlin & Imperial
Lot 11 Block H West Hollywood

20-31 X Sect. Udal St. Plum to Voltaire

32-39 X Sect Drainage Ditch Keats &
Shatter to Harbor Drive

47-50 Storm Drain Thru. Lot #10 Mission Bay
Park Tract.

Cross Section Alley 32 City Hgts.

Oct. 8, 1947

INDEXED

Sennormeyer
W Moore
E Sherman

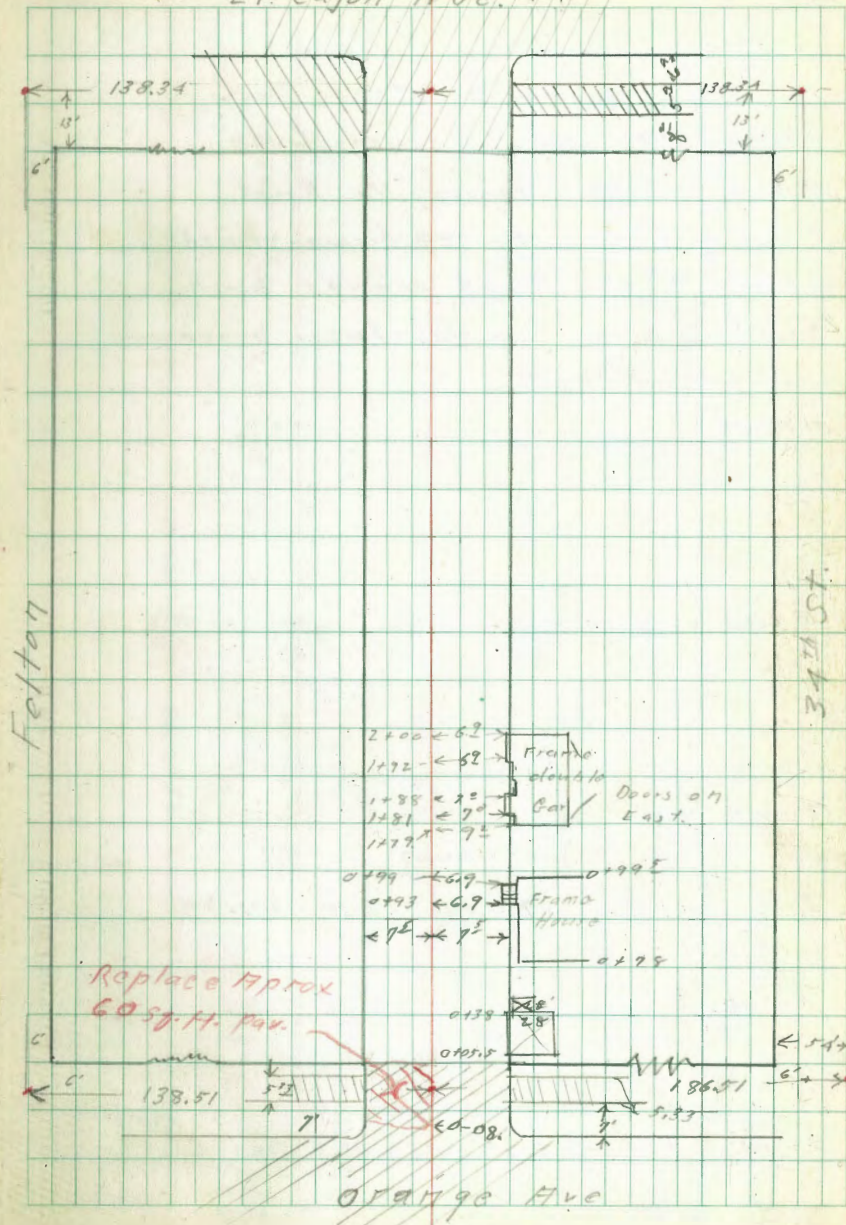
N.W. B.P.
Orange Ave.
+ 33rd

8.22 374.88 — 366.66

Indexed
c.s.k.

1

El. Cajon Ave.



1+22 7⁹ Lt. = End board fence

1+00

+99^E 9³ Rt. = N.W. Cor. Frame house

+99 6⁹ Rt. = End same

0+93 6⁹ Rt. = start porch & steps (Frame)

0+88^E 165 Lt. = Sing Bar. Conc. Floor
9³ Lt. = 8' wide Apron to Sing Bar

0+78 9³ Rt. = S.W. Cor. Frame House
(7.0 Lt. = P. pole # P.H. 4219

0+77 6.9 Rt. = End board fence

0+57 12² Rt. Ex Bar. New House. doors boarded up.
7^a Rt. = Sing. Bar. Apron.

0+50 7⁴ Rt. = start board fence

0+47 6⁹ Lt. = start board fence.

0+44 8⁰ Rt. = Sing. Bar. Conc. Floor. No Apron.

380.01

Lt.

Rt.

Rt.

3

375.8
4.1
7.5

375.8
4.1

375.8
3.8
6

375.8
3.8
7.5

375.8
4.19
7.3
Edge Apron

375.8
4.15
16.3
Bar

375.8
4.7
7.5

375.4
4.6
6

375.2
4.8
4

375.8
4.7

375.8
4.7
5

375.8
4.2
6

375.7
4.3
7.5

375.1
4.9
7.5

375.1
4.9

375.1
4.9
5

375.7
4.3
6

375.7
4.3
7.5

375.8
4.4
8

380.01

2+20

slat fence

2+18 7¹ Lt. = End board fence & start

2+14⁵ 7² Rt. = start lath fence.

2+01 9² Lt. = Φ 1 wide conc. gutter, turn E+W.

2+00 6² Rt. End same.

1+92 6¹ Rt. = start frame bar in alley

1+88 7⁰ Rt. End bar in alley

(7¹ Lt. Start board fence

1+84⁵ 7¹ Lt. = P. pole # P.H. 4235

1+81 7⁰ Rt. = start frame bar in alley
door on east end.

1+63 8⁰ Rt. = End same

1+51 7¹ Rt. = Start frame shed.

1+50

T.P.	5.83	<u>382.28</u>	3.56	376.45
		380.01		

Lt.

Rt.

Rt.

4

5.0
7.5

5.0
377.3

4.9
3
377.4

1.7
6
377.6

4.5
7.5
377.8

5.0
9.5
377.3

4.9
7.5
377.4

4.8
377.5

4.9
4
377.4

1.6
5
377.7

1.6
7.5
377.7

4.1
7.5
378.1

4.1
4
378.2

4.8
5
377.5

4.9
377.4

4.9
5
377.4

1.6
2
377.7

4.7
7.5
377.6

4.8
7.5
377.5

5.2
5
377.0

5.4
376.9

5.4
5
376.9

5.2
7.5
377.1

382.28

3+35

3+24 8th Lt. = End board fence

3+01 7th Rt. = Start wire fence

3+00 9th Rt. = End frame dwelling

2+90 7th Lt. = P. pole # P.F. 4251

2+75

2+70 9th Rt. = start frame dwelling

2+68 8th Rt. = End frame Bldg.

T.P. 5.22 382.94 4.56 377.72

2+52 { 9th Rt. = start frame Bldg

7th Lt. End lath fence
board fence.

2+50 8.2 Lt. = End slot fence & start

2+30

382.28

378.1
4.8
7.5

377.9
5.0
4

378.1
4.8

378.1
4.8
4

378.4
4.5
7.5

Bills
5.1
7.5

377.6
5.3
4

377.6
5.3

377.5
5.4
4

377.9
5.0
6

377.9
5.0
7.5

377.6
5.3
7.5

377.2
5.6
4

377.4
5.5

377.3
5.6
3

377.6
5.3
6

377.8
5.1
7.5

382.94

377.4
4.9
7.5

377.2
5.1
4

377.2
5.1

377.4
5.0
5

377.7
4.6
6

377.8
4.5
7.5

377.5
4.8
7.5

377.9
4.7
6

376.9
5.4
4

377.0
5.2
4

377.0
5.3
4

377.5
4.8
6

377.5
4.8
7.5

382.28

4+11 18^e Lt. = Φ Sing Bar. Conc. Floor.

4+08 12^l Lt. = Φ door of Sing Bar.
North Entrance. Conc. Floor.

T. R. 4.60 382.79 4.75 378.19

4+07 7^e Lt. = Pipe pole # P.A. 4267

4+00 8^o Rt. = End ^{chicken} wire fence - start ^{fence} board

3+93 7^e Rt. = End board stack

3+89 7^e Rt. = \angle in chicken wire fence

3+87^e 8^o Lt. = start frame shed.

3+87^e 8^o Lt. = End picket fence + ^{Slab.} conc.

3+82 7^o Rt. = start board stack.
conc. slab yard

3+75 8^o Lt. = start picket fence +

(7^o Rt. = start chicken wire fence)

3+50 7^o Rt. = End wire fence +

3+48 21^l Lt. = Φ 9^e wide conc. drive

382.94

Lt.

Φ

Rt

6

377.56
5.27
100
Car Floor.

377.87
4.92
12'
Car Floor

382.79

377.9
5.0
7.5

377.9
5.0
7.5

377.9
5.0
7.5

377.5
5.44
15
conc

377.53
5.41
8.4
conc

378.0
4.9
8.3
Rd.

377.54
5.00
7.5

377.55
5.39
8.7
conc.

377.9
5.0
8.5

377.9
5.0
7.5

377.9
5.0
7.5

377.9
5.0
7.5

382.94
5.27
21

382.94

7.5 Lt = Also = Face of wall.
 7.5 Lt = Start stucco store Bldg.
 7.5 Lt = End conc. wall
 7.2 Lt = End Footing for conc. wall
 6.8 Lt = P. pole # P.A. 4289
 9' Rt = Fence line

5+00

4+62.5

7.5 Lt = Face of wall.
 7.5 Lt = Footing for 9" wide conc. wall
 start

4+58

Picket fence on top of wall
 16.2 Lt = End 3 car Gar.
 6.2 Lt = End conc. Apron

4+51

8.7 No good wire & lath fence
 Rt = End board fence start

4+30.5

17.2 Lt = start 3 car Gar.
 7.3 Lt = start Apron to 3 car Gar.

4+27.5

14.3 Lt = 6" walk

4+20

18.6 Lt = 6" Sing Gar. dirt floor

382.79

378.01	377.8	377.0	377.0	377.9	378.0	
1.78	5.10	5.4	5.8	4.9	4.8	
7.5	7.5	7.5	7.2		7.5	
Top wall	Ord	top of footing	Bottom footing			
378.04	377.9	377.0	377.9			
4.75	5.4	5.8	4.9			
7.5	7.5	7.2	7.2			
top wall	top of footing	Bottom of footing	Ord			
377.58	377.39	377.37	377.8	377.9	377.8	378.1
5.21	5.40	5.42	5.0	4.9	5.0	4.7
16.9	7.5	6.9	6.8		6	7.5
Gar Floor		Apron	Ord			
377.56	377.33	377.33	377.7			
5.23	5.40	5.1				
17.3	7.3	7.2				
Gar Floor	Apron	Ord.				
377.55	377.8	378.0	377.9			
5.30	5.0	4.8	4.9			
14.3	7.5		7.5			
walk						
377.51	377.22					
5.22	18.6					
Gar Floor						

382.79

5+75

T.P. 4.92 383.05 4.66 378.13.

5+68^E 7^E Rt. = Φ 2' wide conc. walk

5+52 7^E Lt. = Ctr. Clean out. 4" drain

5+50 7^E Lt. = start lath fence
8^E Lt. = end wire fence

5+42 7^E Lt. = Ctr. Clean out - 4" drain

5+24^E 7^E Lt. = Φ 4' wide ^{into store.} doorway

5+12 7^E Lt. = Φ 4' wide ^{into store} doorway

382.79

5.1
377.8
7.5

5.1
378.0

5.0
378.1
7.5

383.05

5.0
378.26
7.6
walk

5.0
377.87
7.2
on cap

5.1
377.7
7.5

4.8
378.0

4.8
378.0
7.5

4.84
7.2
on cap

5.0
377.8
7.5
door sill

5.0
377.8
7.5
G+L.

5.0
377.8
7.5
Door sill

5.0
377.8
7.5
G+L.

Milker - CROSS SECTION SNOWDROP
 Becker
 Withams from Poplar to Arbor Vitae
 3-15-48 Sketch p. 11

2 Stations

1700

INDEXED

0750

S.W.

0+00 = N.W. Lane Poplar St.

0-12

0-16 = Approx. Madge oil Patch Parking

0-40' = % Poplar St. Sec on Parking

7.15 296.29

289.14

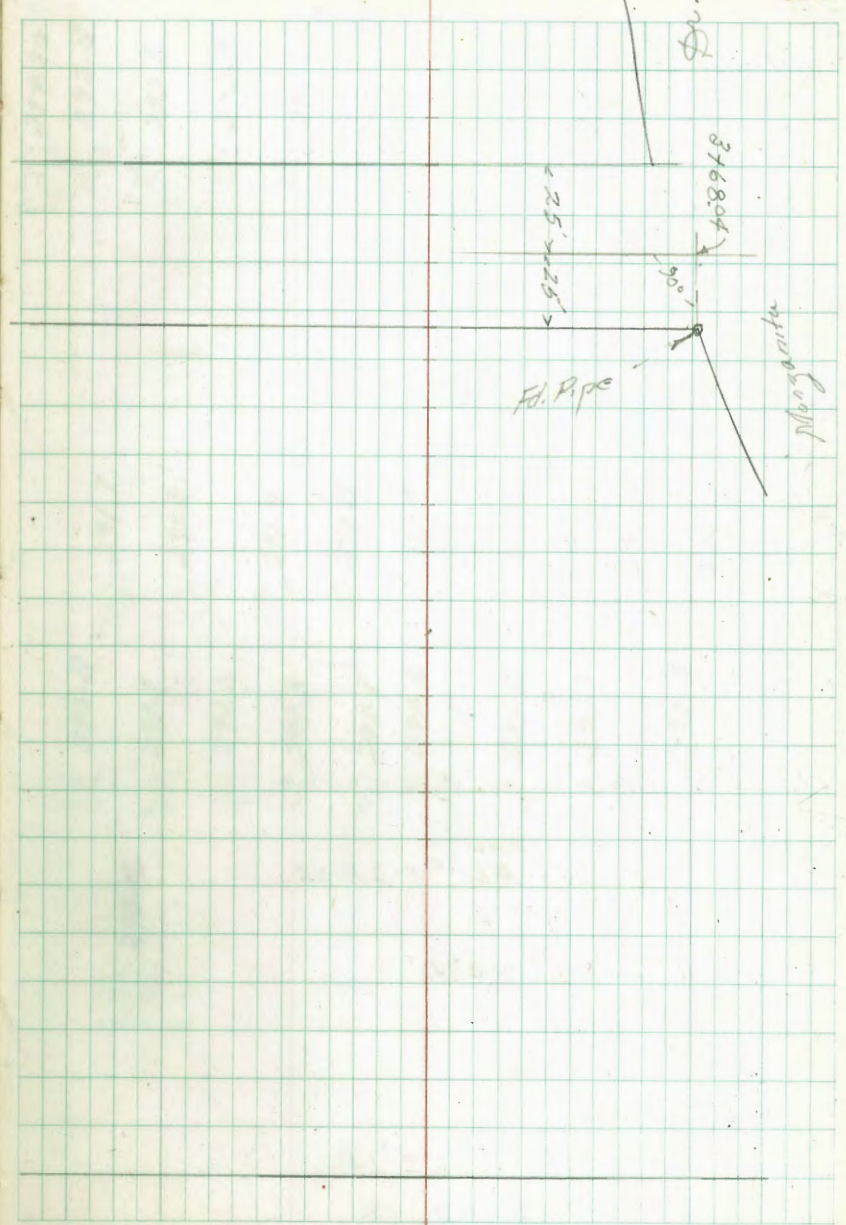
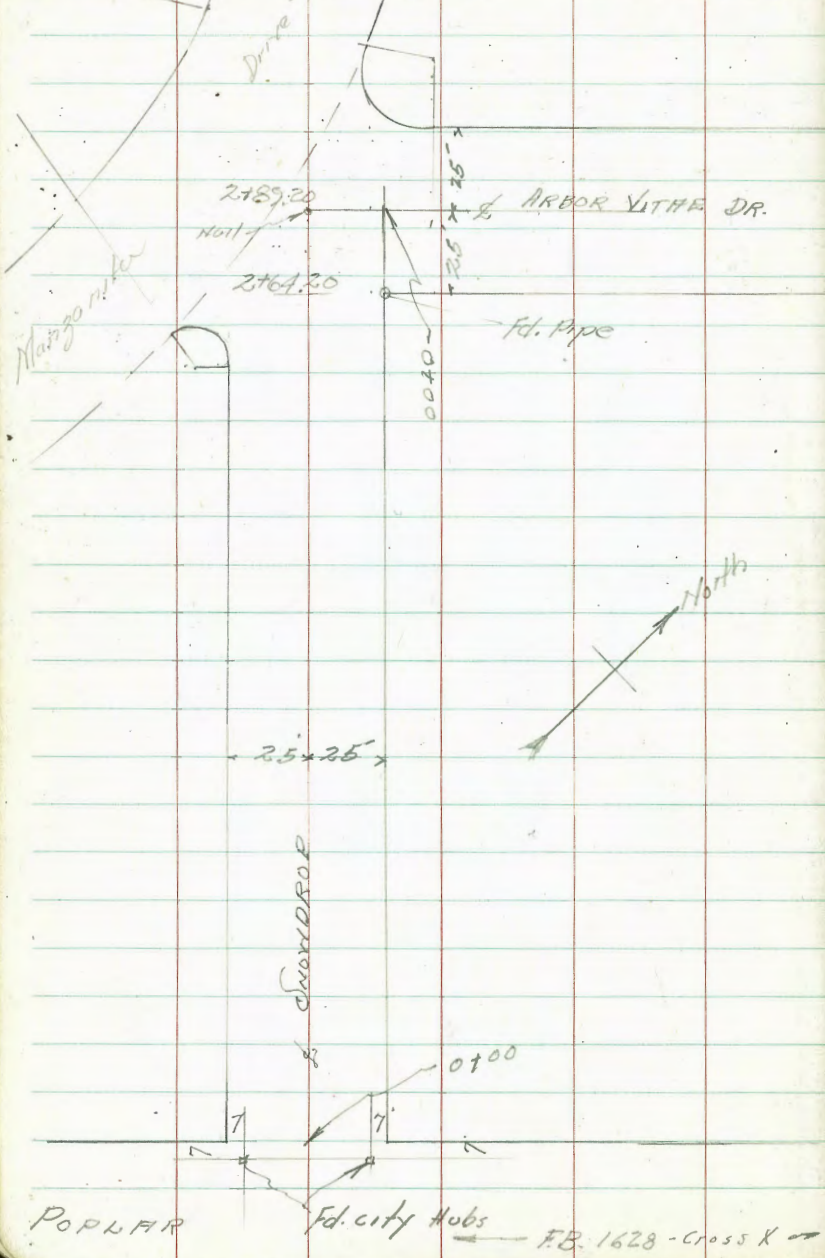
Note: Cross Sections
 on Poplar St. in FB 1628

Station	Index	Index	Index	Index	Index	Index	Index
290.8	289.9	290.4	290.3	290.6	291.0	290.7	291.4
55 35	55 25	55 13	57 12	58	56 11	52 12	50 25
290.8	290.4	290.3	289.6	291.0	289.7	291.1	291.3
55 35	53 25	60 19	67 12	68	66 10	62 16	49 25
289.1	289.16	289.1	288.4	288.7	288.4	289.7	290.1
72 35	71.8 25	72 14	79 12	76	79 12	66 15	62 25
	288.5	288.7	287.9	288.5	288.3	289.9	289.7
	7.8 35	7.6 25	8.4 15	7.8	8.0 14	6.4 25	5.4 35
	287.3	287.7	288.2	288.3	288.4	288.4	288.4
	9.0 30	8.6 25	8.1	8.0 25	7.9 30		
287.68	288.00	288.25	288.44	288.58	288.44	288.58	288.44
8.61	8.29 25	8.04	7.85 25	7.71 50			
		8.96 39					

B.M. 56 3/4" Iron Pipe Poplar to SNOWDROP

FB 1625
 27

CROSS SECTION - SNOWDROP ST.
from Poplar St to Arbor Vitae St.



ST.

SNOWDROP - Cross Sections

Cont from p-11

Stations

2+00

1+85

1+61.5 = ~~1~~ Conc. Patch on Pt

1+50

1+32.5 = ~~1~~ Alley

1+23 16.3 Lt = Pole ^{Elev} # P. 2H. 24

1+08 = ~~1~~ Conc. Patch 26.4' Lt.

1+04 = Pole Anchor 16.3' Lt.

296.29

H

A

H

12

294.20	292.5	292.5	292.3	291.9	291.7	292.2	292.0	292.8	293.0
200 37 Cm. Porch	38 25	38 25	40 23	44 15	46 12	41	43 13	35 25	33 25
								292.67	
								362 26.5 Broken Conc. Dr.	
									293.29
	291.7	291.8	291.4	291.3	291.8	291.6	292.3	292.3	292.3
	46 25	45 25	47 12	50 11	45	47 16	40 25	40 25	
	290.5	291.1	291.2	291.3	291.1	291.6	291.7	292.5	
	58 100	52 50	51 25	50 12	52 11	47	47 25	38 100	
	292.16								
	113 26.4 on Porch								
									296.29

300
29.0
on Porch

CROSS SECTION NO - ARBOR VITAE
Cont. from P 14

2700

1783 = 2.35' Conc. Walk 24' RT

1774 = Big Conc. Ribbon Drive on LT

1761 = 2.3' Conc. Walk 25.8' LT

1750

301.57
5

4

4

14

15

4.3 35	297.3	4.3 35	297.3	4.3 35	297.3	4.3 35	297.3	4.3 35	297.3
4.3 27	297.3	4.3 27	297.3	4.3 27	297.3	4.3 27	297.3	4.3 27	297.3
4.7 25	296.9	4.7 25	296.9	4.7 25	296.9	4.7 25	296.9	4.7 25	296.9
5.0 19	296.6	5.0 19	296.6	5.0 19	296.6	5.0 19	296.6	5.0 19	296.6
5.3 11	296.3	5.3 11	296.3	5.3 11	296.3	5.3 11	296.3	5.3 11	296.3
5.0	296.6	5.0	296.6	5.0	296.6	5.0	296.6	5.0	296.6
5.3 9	296.3	5.3 9	296.3	5.3 9	296.3	5.3 9	296.3	5.3 9	296.3
5.1 13	296.5	5.1 13	296.5	5.1 13	296.5	5.1 13	296.5	5.1 13	296.5
5.1 25	296.5	5.1 25	296.5	5.1 25	296.5	5.1 25	296.5	5.1 25	296.5
5.1 35	296.5	5.1 35	296.5	5.1 35	296.5	5.1 35	296.5	5.1 35	296.5
4.8 26	297.51	4.8 26	297.51	4.8 26	297.51	4.8 26	297.51	4.8 26	297.51
4.24 26	297.33	4.24 26	297.33	4.24 26	297.33	4.24 26	297.33	4.24 26	297.33
4.10 36	297.47	4.10 36	297.47	4.10 36	297.47	4.10 36	297.47	4.10 36	297.47
4.24 26	297.33	4.24 26	297.33	4.24 26	297.33	4.24 26	297.33	4.24 26	297.33
4.14 35.8	297.43	4.14 35.8	297.43	4.14 35.8	297.43	4.14 35.8	297.43	4.14 35.8	297.43
4.19 35.8	297.38	4.19 35.8	297.38	4.19 35.8	297.38	4.19 35.8	297.38	4.19 35.8	297.38
4.60 24	296.97	4.60 24	296.97	4.60 24	296.97	4.60 24	296.97	4.60 24	296.97
4.63 34	296.94	4.63 34	296.94	4.63 34	296.94	4.63 34	296.94	4.63 34	296.94

301.57

Arbor Vitae Dr.
Cross Sections

2 Stations

3+68.04

3+50

3+22 = 3' Conc Walk

3+15 = 7' Conc Drive 24.7 ft

3+00

2+83 = 9' Conc. Dr 24.4

301.57
m

14

15

ft.

17

294.0	294.8	293.6	294.73	293.05	293.0
5.6 25	6.8 25	8.0 25	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
297.08	294.2	293.6	294.73	293.05	293.0
4.49 35.5	7.4 25	8.0 25	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
296.70	293.9	293.3	294.73	293.05	293.0
4.87 2.55 Bk on Dr.	7.7 11	8.0 21	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
296.46	293.7	293.2	294.73	293.05	293.0
5.11 24 Toe Conc. Appl. 17	7.9	8.4	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
294.7	293.1	292.6	294.73	293.05	293.0
6.9 12	8.5 12	9.0 15	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
294.8	293.8	293.2	294.73	293.05	293.0
6.8 25	7.8 16	8.4 17	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
295.0	293.5	293.0	294.73	293.05	293.0
6.6 25	8.1 25	8.6 25	6.84 24.7 5.2 Conc. Dr.	8.52 25 on Pipe	8.6 25
301.57					

				<u>002</u>
				287.89 = FBK 28-25
chk BM Top Fire Hyd		3.82	287.91	Nail in Eloc Pile
TP	3.31	291.73	8.49	288.42
TP	3.86	296.91	8.52	293.05

3+93

301.57

W. Poplar + Hollywood Park
 W. Marlborough + Margarita

292.8	292.7	292.3	292.2	291.5	291.2
88 40	89 30	93 25	94	101 28	104 35

301.57

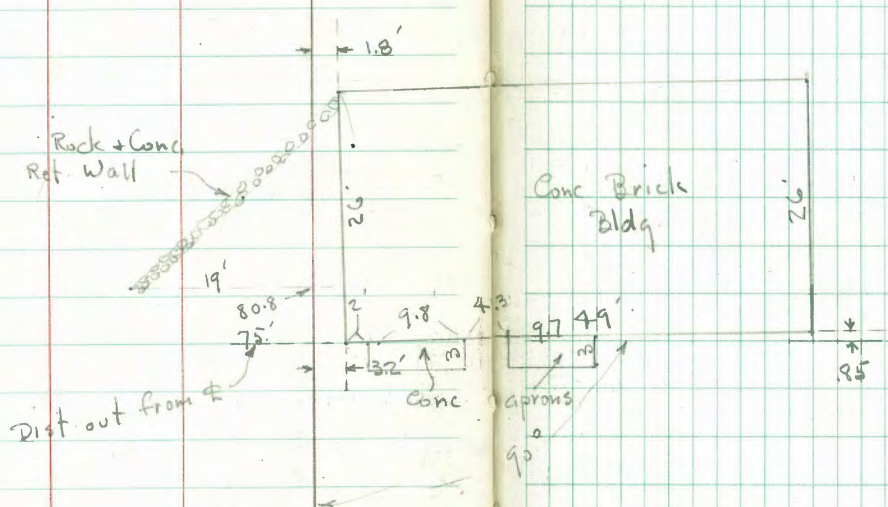
Lot 11 Block H
WEST HOLLYWOOD SUB

Location of Bldg.
Imperial + Merlin

1-3-49
7.0.

INDEXED
WK
JAN 4 1949

17+90 - Radial

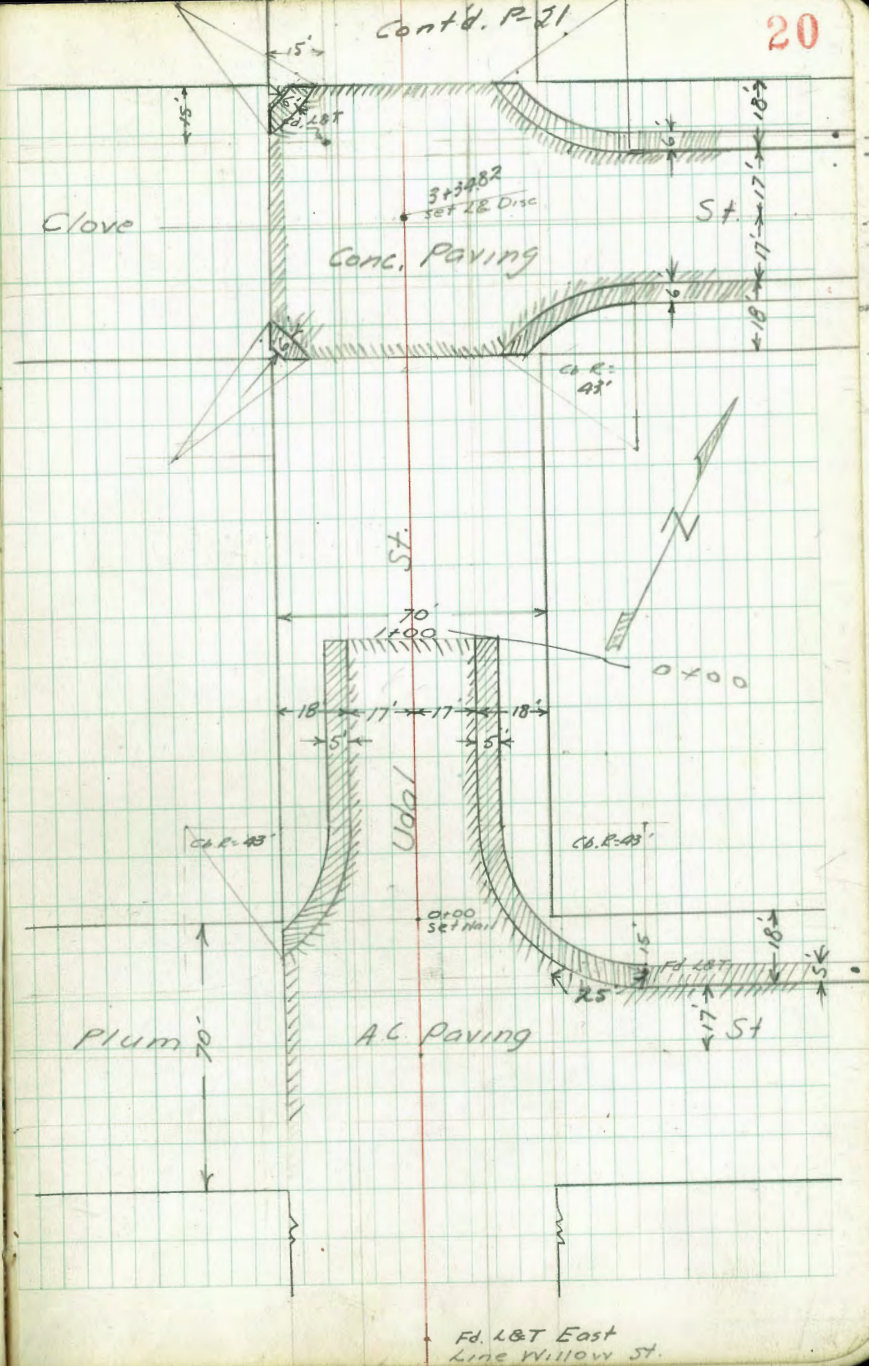


1-31-49
Hendricks
Bramby
Greer
Rorer
W.O.#31080

X Section Udal St.
Plum to Voltaire

Map #1863 (Reference)

INDEXED
WK
FEB 4 1949



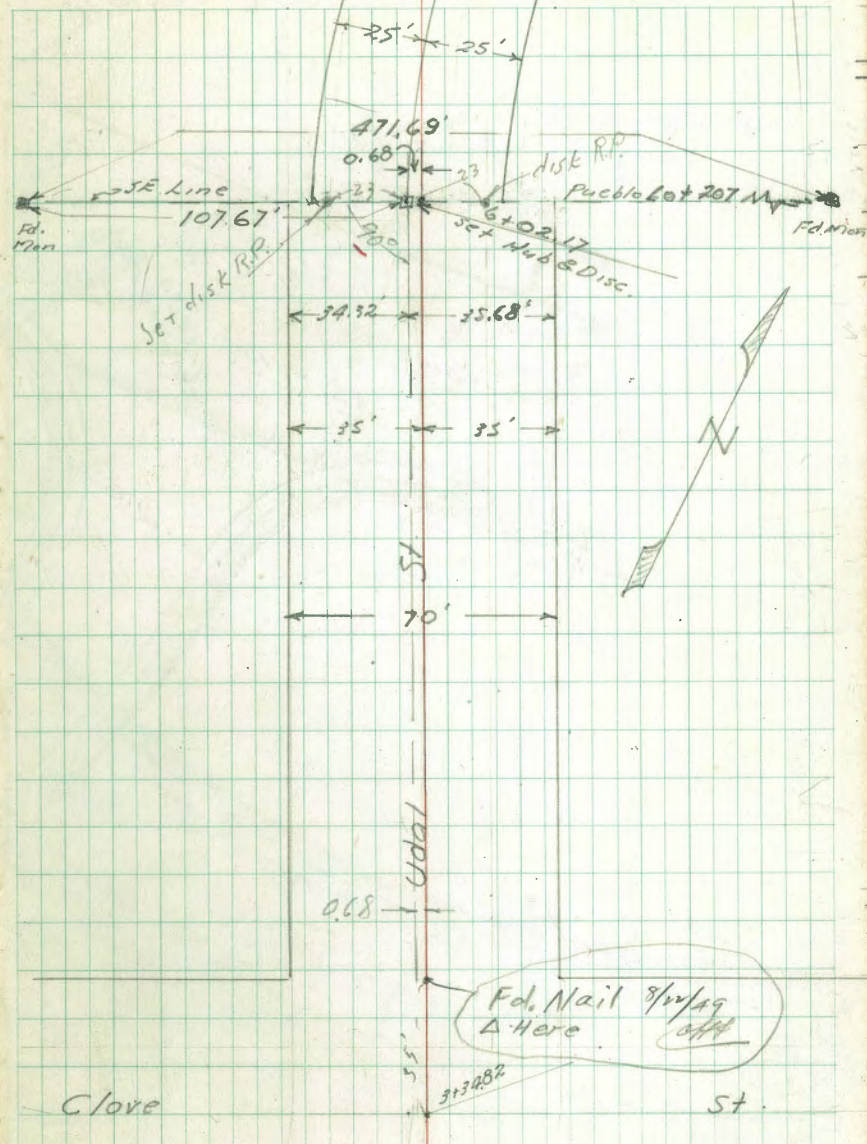
X Sect. Udal St
Plum to Voltaire Contd.

15.
0.68

14.32

Contd P. 22

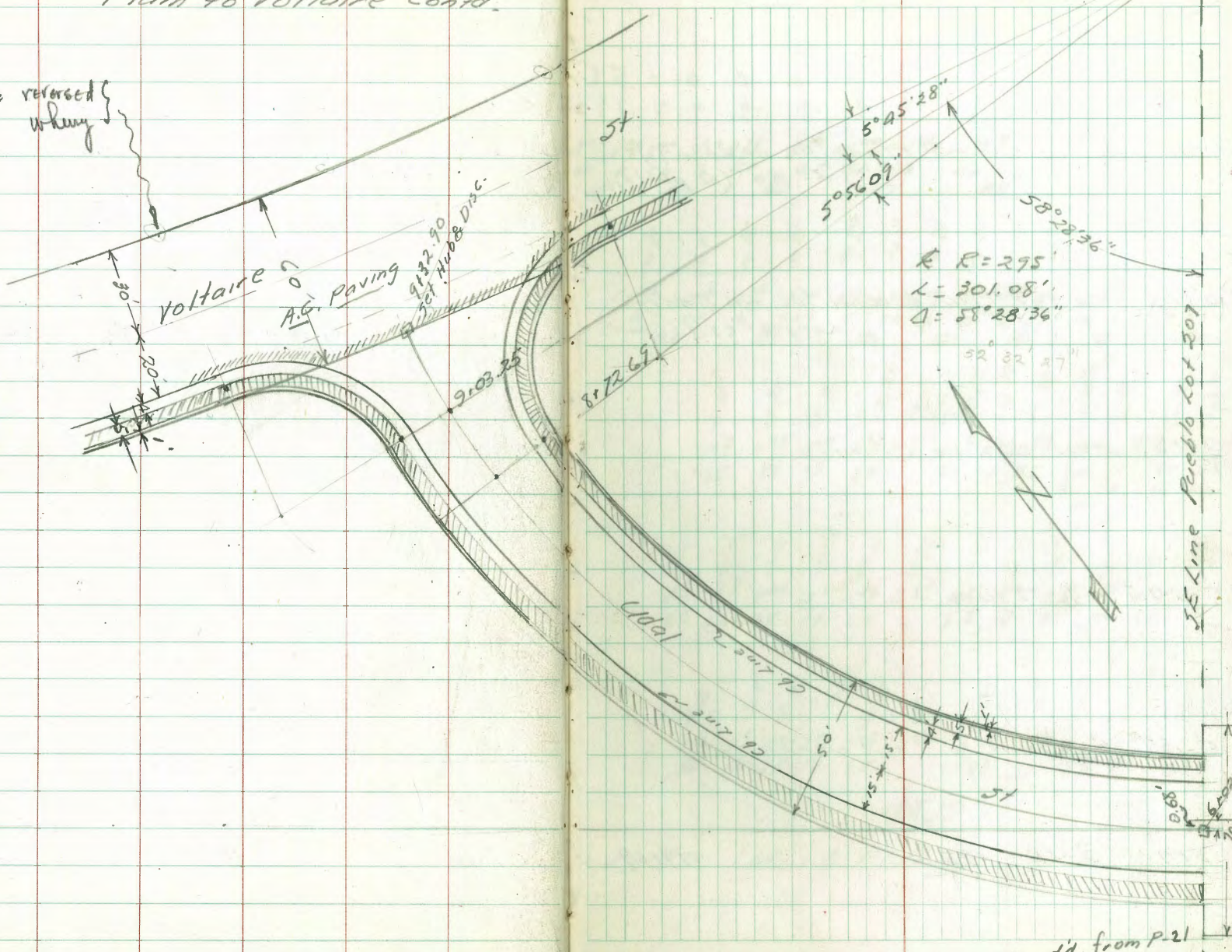
21



Contd. from P. 20

X Sect. Udal St.
Plum to Voltaire Contd.

Curve reversed
whenever



R = 295
L = 301.08'
Δ = 58°28'36"

52°32'27"

SE Line Pueblo Lot 207

Contd. from P. 21

Cont'd. From P. 26

5+00

4+60

4+18

3+85

SW CB Ret Udal & Clove #1 on Udal
Length = 144
(2 parts)

NW CB Ret Udal & Clove #1 on Udal
Length = 109
(5 parts)

171.89

27

147	147	157	157	158	159	159	160	160	160	161	161
14	14	14	13	13	12	12	11	11	11	10	10
50	35	35	35	35	20	20	28	28	25	25	20
157	157	157	157	159	160	160	161	161	162	162	162
12	12	12	12	12	11	11	10	10	9	9	9
50	35	20	13	13	16	16	27	25	25	50	50
161	161	161	161	162	162	162	163	164	165	165	165
10	10	10	9	9	9	8	7	7	6	6	6
50	30	15	19	19	19	27	35	35	50	50	50
163	163	163	163	164	165	165	166	166	166	166	166
8	8	8	8	7	8	7	6	6	5	5	5
50	35	23	16	19	19	28	27	27	50	50	50
164	163	164	163	164	165	165	166	166	166	166	166
7	7	7	7	7	8	8	8	8	8	8	8
727	727	763	808	725	815						
CB	G	CB	G	CB	G						
(3)		(1)		(1)							
144	144	144	144	145	146	146	146	146	146	146	146
727	741	725	679	670	624	608	562	544	493		
G	CB	G	CB	G	CB	G	CB	G	CB		
(4)		(2)		(3)		(3)		(3)	(1)		

171.89

6+77.44

6+52.35

6+27.26

bet. 6+02.17 & 9+03.25 Curve divided into 12 equal parts of 25.09' each

6+02.17 B.C. (Section taken using hub as ϵ which is 0.65 so. of ϵ Uda 5+ coming from the East.)

5+55

5+15

T.P. 3.24 $\frac{162.15}{\wedge}$ 1298 15891

$\frac{171.89}{\wedge}$

85	80	80	74	75	76	709
15	15	11	3	15	15	15
G	Dirt			G	CG	
Drive						
154	154	154	154	154	154	154
704.8	704.8	704.8	704.8	704.8	704.8	704.8
1515.2	1515.2	1515.2	1515.2	1515.2	1515.2	1515.2
CGG	CGG	CGG	CGG	CGG	CGG	CGG
Drive	Drive	Drive	Drive	Drive	Drive	Drive
154	154	154	154	154	154	154
730	72	70	65	66	632	
15	15	11	9	15	15	15
CG	Dirt			G	CG	
156	156	156	156	156	156	156
672	678	676	57	60	500	55
24	19	14.8	15	12	9	574
SW	SW	CG	Dirt		Hub	9
156	156	156	156	156	156	156
55	57	57	49	43	49	37
50	35	29	18	14	13	13
157	157	157	157	157	157	157
46	45	47	40	34	39	35
50	35	29	10	15	13	27
162.15	20	35	50			
ON NW Cor. Drive	35	41	47.5			

$\frac{171.89}{\wedge}$

8127.98

T.P. 7 15 160.77 853 153 62

8102.89

7177.80

7152.71

7127.62

7102.53

162.15
A

153 24	153 27	153 30	153 33	153 36	153 39	153 42	153 45	153 48	153 51	153 54	153 57	153 60	153 63	153 66	153 69	153 72	153 75	153 78	153 81	153 84	153 87	153 90	153 93	153 96	153 99	154 02	154 05	154 08	154 11	154 14	154 17	154 20	154 23	154 26	154 29	154 32	154 35	154 38	154 41	154 44	154 47	154 50	154 53	154 56	154 59	155 02	155 05	155 08	155 11	155 14	155 17	155 20	155 23	155 26	155 29	155 32	155 35	155 38	155 41	155 44	155 47	155 50	155 53	155 56	155 59	156 02	156 05	156 08	156 11	156 14	156 17	156 20	156 23	156 26	156 29	156 32	156 35	156 38	156 41	156 44	156 47	156 50	156 53	156 56	156 59	157 02	157 05	157 08	157 11	157 14	157 17	157 20	157 23	157 26	157 29	157 32	157 35	157 38	157 41	157 44	157 47	157 50	157 53	157 56	157 59	158 02	158 05	158 08	158 11	158 14	158 17	158 20	158 23	158 26	158 29	158 32	158 35	158 38	158 41	158 44	158 47	158 50	158 53	158 56	158 59	159 02	159 05	159 08	159 11	159 14	159 17	159 20	159 23	159 26	159 29	159 32	159 35	159 38	159 41	159 44	159 47	159 50	159 53	159 56	159 59	160 02	160 05	160 08	160 11	160 14	160 17	160 20	160 23	160 26	160 29	160 32	160 35	160 38	160 41	160 44	160 47	160 50	160 53	160 56	160 59	161 02	161 05	161 08	161 11	161 14	161 17	161 20	161 23	161 26	161 29	161 32	161 35	161 38	161 41	161 44	161 47	161 50	161 53	161 56	161 59	162 02	162 05	162 08	162 11	162 14	162 17	162 20	162 23	162 26	162 29	162 32	162 35	162 38	162 41	162 44	162 47	162 50	162 53	162 56	162 59	163 02	163 05	163 08	163 11	163 14	163 17	163 20	163 23	163 26	163 29	163 32	163 35	163 38	163 41	163 44	163 47	163 50	163 53	163 56	163 59	164 02	164 05	164 08	164 11	164 14	164 17	164 20	164 23	164 26	164 29	164 32	164 35	164 38	164 41	164 44	164 47	164 50	164 53	164 56	164 59	165 02	165 05	165 08	165 11	165 14	165 17	165 20	165 23	165 26	165 29	165 32	165 35	165 38	165 41	165 44	165 47	165 50	165 53	165 56	165 59	166 02	166 05	166 08	166 11	166 14	166 17	166 20	166 23	166 26	166 29	166 32	166 35	166 38	166 41	166 44	166 47	166 50	166 53	166 56	166 59	167 02	167 05	167 08	167 11	167 14	167 17	167 20	167 23	167 26	167 29	167 32	167 35	167 38	167 41	167 44	167 47	167 50	167 53	167 56	167 59	168 02	168 05	168 08	168 11	168 14	168 17	168 20	168 23	168 26	168 29	168 32	168 35	168 38	168 41	168 44	168 47	168 50	168 53	168 56	168 59	169 02	169 05	169 08	169 11	169 14	169 17	169 20	169 23	169 26	169 29	169 32	169 35	169 38	169 41	169 44	169 47	169 50	169 53	169 56	169 59	170 02	170 05	170 08	170 11	170 14	170 17	170 20	170 23	170 26	170 29	170 32	170 35	170 38	170 41	170 44	170 47	170 50	170 53	170 56	170 59	171 02	171 05	171 08	171 11	171 14	171 17	171 20	171 23	171 26	171 29	171 32	171 35	171 38	171 41	171 44	171 47	171 50	171 53	171 56	171 59	172 02	172 05	172 08	172 11	172 14	172 17	172 20	172 23	172 26	172 29	172 32	172 35	172 38	172 41	172 44	172 47	172 50	172 53	172 56	172 59	173 02	173 05	173 08	173 11	173 14	173 17	173 20	173 23	173 26	173 29	173 32	173 35	173 38	173 41	173 44	173 47	173 50	173 53	173 56	173 59	174 02	174 05	174 08	174 11	174 14	174 17	174 20	174 23	174 26	174 29	174 32	174 35	174 38	174 41	174 44	174 47	174 50	174 53	174 56	174 59	175 02	175 05	175 08	175 11	175 14	175 17	175 20	175 23	175 26	175 29	175 32	175 35	175 38	175 41	175 44	175 47	175 50	175 53	175 56	175 59	176 02	176 05	176 08	176 11	176 14	176 17	176 20	176 23	176 26	176 29	176 32	176 35	176 38	176 41	176 44	176 47	176 50	176 53	176 56	176 59	177 02	177 05	177 08	177 11	177 14	177 17	177 20	177 23	177 26	177 29	177 32	177 35	177 38	177 41	177 44	177 47	177 50	177 53	177 56	177 59	178 02	178 05	178 08	178 11	178 14	178 17	178 20	178 23	178 26	178 29	178 32	178 35	178 38	178 41	178 44	178 47	178 50	178 53	178 56	178 59	179 02	179 05	179 08	179 11	179 14	179 17	179 20	179 23	179 26	179 29	179 32	179 35	179 38	179 41	179 44	179 47	179 50	179 53	179 56	179 59	180 02	180 05	180 08	180 11	180 14	180 17	180 20	180 23	180 26	180 29	180 32	180 35	180 38	180 41	180 44	180 47	180 50	180 53	180 56	180 59	181 02	181 05	181 08	181 11	181 14	181 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26	188 29	188 32	188 35	188 38	188 41	188 44	188 47	188 50	188 53	188 56	188 59	189 02	189 05	189 08	189 11	189 14	189 17	189 20	189 23	189 26	189 29	189 32	189 35	189 38	189 41	189 44	189 47	189 50	189 53	189 56	189 59	190 02	190 05	190 08	190 11	190 14	190 17	190 20	190 23	190 26	190 29	190 32	190 35	190 38	190 41	190 44	190 47	190 50	190 53	190 56	190 59	191 02	191 05	191 08	191 11	191 14	191 17	191 20	191 23	191 26	191 29	191 32	191 35	191 38	191 41	191 44	191 47	191 50	191 53	191 56	191 59	192 02	192 05	192 08	192 11	192 14	192 17	192 20	192 23	192 26	192 29	192 32	192 35	192 38	192 41	192 44	192 47	192 50	192 53	192 56	192 59	193 02	193 05	193 08	193 11	193 14	193 17	193 20	193 23	193 26	193 29	193 32	193 35	193 38	193 41	193 44	193 47	193 50	193 53	193 56	193 59	194 02	194 05	194 08	194 11	194 14	194 17	194 20	194 23	194 26	194 29	194 32	194 35	194 38	194 41	194 44	194 47	194 50	194 53	194 56	194 59	195 02	195 05	195 08	195 11	195 14	195 17	195 20	195 23	195 26	195 29	195 32	195 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8 9142.9± 50. Cb line Voltairc
(section taken along Cb. line)

84	147	147	148	148	150	151	151	152	152	153	153	154	154	155	155	156	156	157
1273	1275	1125	979	817	673	595	541	519	470	409	427	369						
60.7	60.7	50	33	17		15	36	50	75	75	100	100						
4C																		

8 9132.90 50. Line Voltairc Edge Asph. Paving

151	151	151	151	151	151	151	151	151	151	151	151	151	151	151	151	151	151	151
923	909	723	608	595	554	554	558	512										
31.0	31.0	13	6.77	13	30	44.0	44.0											
Cb	G		1446			G	Cb											

7 9103.25 BC. Cb Ret. on Lt.

152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152
786	822	76	70	66	623													
15	15	8		216	216													
Cb	G			G	Cb													

7 8178.16

152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152
726	81	74	69	60														
15	15		15	15														
Cb	G		G	Cb														

7 8172.69 BC Cb Ret. on Rt.

152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152
796	72	71	65															
15		15	15															
G		G	Cb															
Drive																		

7 8153.07

152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152	152
724	72	70	65															
15	15	15	15															
Cb	G	G	Cb															

16077
T

16077

B.M.		11.58	116.91	116.79
T.P.	3.68	128.49	10.18	124.81
T.P.	0.17	134.99	13.13	134.82
T.P.	0.41	147.95	13.23	147.54

S.W.B.P. Voltaire & Chatsworth

1278	1348	1124	1202	1044	1028	957	987	881	93	836	808	801	84	786	53
Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G
80	⑥	⑤	④	③	②	①									
1278	911	675	586	544	473	440	328								
G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb
80	①	②	③	④	⑤	⑥	⑦								
1315	957	730	627	555	478	426	324								
G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb	G	Cb
61	35	15		15	44	78	100								

So. Westerly Cb Cb Ret. Udal & Voltaire BC on Udal
 (Length = 714 parts)

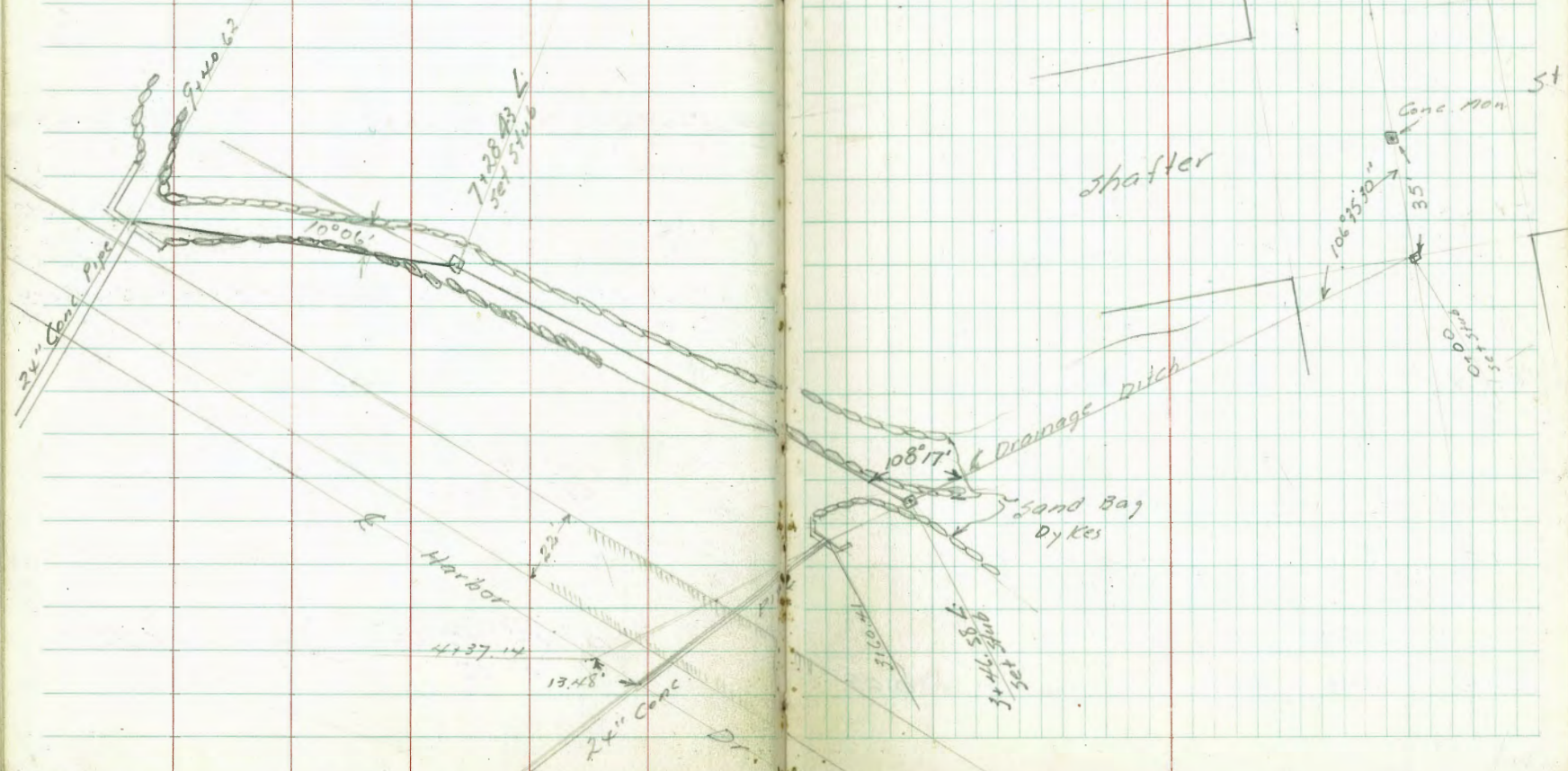
So. Easterly Cb Ret. Udal & Voltaire BC on Udal
 (Length = 7428 parts)

9162.9 ± & Voltaire

9152.9 So 1/4 Voltaire

3-11-49 Levels for Drainage Ditch
 Hendricks from Keats & Shafter to
 Greer Harbor Drive
 Rover
 W O # 22004

INDEXED
 WK
 MAR 15 1949



Levels for Drainage Ditch

1+50

1+00

0+47

0+22

0+11

0+00 & Keats & Se Line Shafter

B17 8.00 869 0.69

3.9 3.1 1.3 2.3 10.8 3.6 3.7
 5.3 5.3 10.0 11.0 9.5 5.1 5.0
 36 20 6 7 19 33

3.9 3.6 1.4 1.9 2.1 0.7 1.2 1.1
 4.8 5.1 10.1 10.5 10.8 9.4 4.5 4.5
 36 21 5 1 7 20 32

1.0 3.9 0.5 1.9 1.2 3.4 3.8
 4.7 4.8 9.2 10.5 9.9 5.3 4.8
 36 20 7 6 17 30

1.1 1.5 1.0 1.9 2.2 1.1 0.6 2.1 2.8
 4.3 4.2 9.7 10.5 10.8 10.4 9.3 6.3 5.9
 37 23 6 3 6 9 17 27

1.3 1.1 0.3 1.7 2.2 1.5 1.0 1.2 1.7
 4.4 4.3 8.4 10.4 10.8 10.3 9.7 7.5 7.9
 50 28 12 5 9 16 20 28

1.1 3.9 2.0 0.2 1.4 1.9 1.1 0.1 2.3
 4.6 4.8 6.7 8.7 10.1 10.5 9.8 8.3 6.4
 57 44 27 7 8.69 24 36 44 50

& Hub Lowell & Shafter FB 1777 P. 14

3121

0.9 0.7 1 2.1 2.1 0.1 2.1
 64 61 41 41 68 92 101 92 34 39
 40 35 33 12 5 22 9 24 40

3100

3.2 3.3 2.1 1.8 3.0 2.4 3.4 2.9
 35 35 41 85 98 98 34 39
 36 19 15 4 6 23 40

2+92 6" Iron Pipe across Ditch

1.0 54
 733
 Top of Pipe

2+50

2 0 1 1 3 5 0.9 0.9 A
 31 21 0.1 1.1 2.3 2.5 0.9 2.9 3.1
 35 37 75 85 91 92 77 29 34
 32 17 9 2 1 6 22 36

2+09 2" Iron pipe across Ditch

1.16
 503
 Top of Pipe

T.P. 395 6.79 5.88 2.84

(Top of Iron Pipe)
 20' at 2+00

2+00

6.79
 3.3 3.1 2 1.5 2.6 1.1 3.9 3.1
 54 55 102 112 101 48 53
 34 18 5 5 20 35

869
 1

869
 1

CKFL 24" Pipe 7.81 -1.02 -1.07

FB 1773 P 78

-1.02
7.81

3+60.41 Fl. 24" Conc. Pipe

3+54

1.5	1.4	1.0	0.6	0.8	0.2	2.4	2.1	2.1	1.8	5
53	54	78	74	50	70	93	95	93	50	43
24	12	3		1	18	20	25	29	31	48

3+50

1.7	0.8	0.7	0.9	0.6	1.9	0.3	2.4	3.0	2.1	1.9	1
53	60	75	77	78	49	65	93	98	93	49	41
50	18	10	4	2		14	15	20	27	30	47

3+33

0.6	0.2	2.4	5	0.1	1.8	2.4	3.0	2.6	0.8	1.8	2.6
74	65	44	53	69	85	92	98	93	60	59	42
30	16	15	8		2	3	7	13	16	23	39

3+30

0.5	0.1	2.4	1.5	0.2	1.9	3.0	2.4	0.2	1.5	3.1	2.9
73	67	44	53	65	82	95	93	70	53	37	33
33	18	16	10	1		6	11	12	21	26	41

6.79

6.79
1

3-14-49
Hendricks

Continuation of 4 Sections
Drainage Ditch from Leats &
Shatter to Harbor Drive
(see P. 32)

4+50

4+00

3+71

3+66

3+46.58 L

BM 3.98 6.82

2.84

36

1.3	0.7	2.1	2.3	2.2	1.2	1.4	2.4	2.6
5.5	6.5	8.9	9.1	9.0	8.0	5.4	4.4	4.3
23	11	3		2	5	6	13	20

1.5	0.8	2.2	2.3	1.8	2.4	2.6
5.3	6.0	9.0	9.1	8.5	4.4	4.3
23	11	3		4	7	17

1.3	0.2	2.0	2.6	2.4	1.6	2.3
5.5	7.0	8.8	9.4	9.2	5.3	4.5
16	2		5	9	11	20

1.8	1.2	0.3	2.6	2.8	2.6	2.3	1.7	1.5
5.0	5.5	7.5	9.4	9.5	9.4	9.1	5.4	4.3
25	9		2	6	8	9	11	20

1.5
5.3

6.82

Top of 1" I.P. left 2100
P. 34 this Book

7+28.43 ← Lt. (Sec. Taken Rt. to do)
Back Line

TP. 7.99 6.02 879 -1.97

7100

6150

6100

5150

5100

652

0.3	0.2	0.1	0.0	0.4	0.9	0.9
57	67	81	80	74	51	51
22	4	3		3	x	20

R. Sub 7+28.43 6.02

0.1	0.9	0.0	0.0	1.2	1.7	1.7
67	77	88	88	89	51	51
19	5	4		3	5	15

1.0	0.4	0.4	0.9	1.0	1.9	2.6
58	72	82	82	78	49	43
27	11	7		3	4	22

1.1	0.5	1.1	1.9	1.3	2.1	2.7
52	73	85	87	81	42	41
24	7	5		4	6	22

0.6	0.4	0.9	1.9	1.0	1.1	1.1
59	73	82	87	78	51	41
23	8	x		5	6	21

1.0	0.5	1.0	2.1	1.2	1.2	2.5
58	65	78	89	80	55	43
23	9	6		4	5	21

682

9100

0.7	10.9	2.3	2.6	2.0	0.1	0.4
5 ³	6 ⁹	8 ³	8 ⁵	8 ⁰	6 ¹	5 ⁵
17	1		6	7	8	12

8155

1.1	0.8	2.3	2.6	2.0	0.3	1.0
4 ⁹	6 ⁸	8 ³	8 ⁵	8 ⁰	5 ⁷	5 ⁰
17		1	7	8	8	18

8450

1.0	0.9	1.0	1.5	2.3	1.9	0.0	0.4
5 ⁰	6 ⁹	7 ⁰	8 ⁵	8 ³	7 ⁹	6 ⁰	5 ⁵
20		2	2	8	10	10	17

8100

0.9	0.9	1.1	2.3	2.3	1.6	0.5	0.4
5 ¹	6 ⁹	7 ¹	8 ³	8 ³	7 ⁵	5 ⁵	5 ⁵
19		2	2	6	9	9	20

7474

0.9	0.8	2.1	2.2	1.1	0.5	0.4
5 ¹	6 ⁸	8 ¹	8 ³	7 ⁷	5 ⁵	5 ⁵
22		1	4	6	7	20

7466

0.5	0.4	2.1	1.9	1.0	0.9
5 ⁵	6 ⁴	8 ¹	7 ⁹	5 ⁰	5 ¹
19	1		6	7	27

$$\frac{6.02}{1}$$

$$\frac{6.02}{1}$$

5-10-49 Location & Elevs of Drains & Structures on MISSION Blvd
 Hendricks Creek (Ostend Court to Pismo Court)
 Korer
 WOT

Drain #4 (Btm Conc. Jump) 8.50
 Drain #4 (FL 8" Conc. Pipe) 8.46
 From Drain #5
 Drain #4 (FL 12" Vit. Pipe) 7.89
 *to Drain #3
 Drain #4 Grate 6.10

Drain #3 FL 12" Vit. From 9.03
 Cleanout #6
 Drain #3 (FL 12" Vit. Pipe from) 8.97
 Drain #4
 Drain #3 FL 8" Lateral 9.01
 from Drain #1
 Drain #3 Btm Conc. Jump 9.94
 Drain #3 Grate 6.33

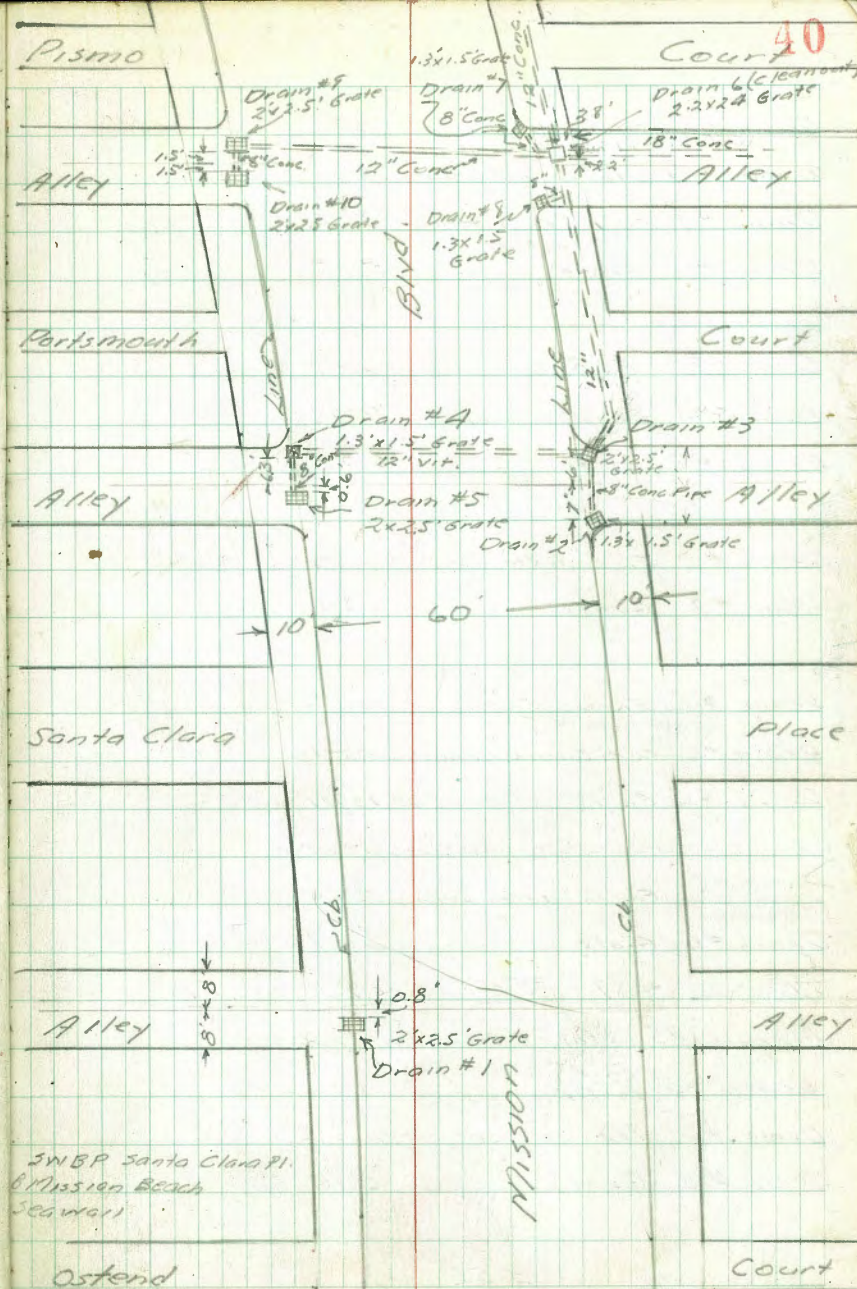
Drain #2 Btm 12" Conc. Sumpt 9.29
 Pipe
 Drain #2 FL 8" Conc. Lateral 8.50
 to Drain #3
 Drain #2 Grate 6.39

Drain #1 Btm 24" pipe 9.18
 Drain #1 Top 24" Pipe 6.85 into Ground -
 Drain #1 Grate 6.07

Note (At Drain #1 24" CRP goes down Vertical)

TP	5.54	5.56	9.67	0.02
BM	250	9.69	7.19	

INDEXED
 WK
 MAY 11 1949



Drain #11 (Fl. 8" Conc. to...)
Drain #10 7.29

Drain #9 Btm Conc. Sump 8.74

Drain #9 Fl. 12" Conc. to... 8.12
Cleanout #6

Drain #9 Grate 5.95

Drain #8 Fl. 8" Conc. Pipe 8.41

Drain #8 Fl. Btm Sump 9.16

Drain #8 Grate 6.34

Drain #7 Fl. 8" & Btm Sump 7.93

Drain #7 Grate 6.30

Drain #6 Fl. 12" From (visi) 10.25
(to Drain #9)

Drain #6 Btm Sump (conc) 10.21

Drain #6 Fl. 18" From East 10.41

Drain #6 Fl. 12" From North 10.10

Drain #6 Fl. 12" From South 10.20

(Cleanout)

Drain #6 Grate 6.27

TP 4.89 5.48 4.97 0.59

Drain #5 Btm 24" vert. CMP. 9.2

Drain #5 (Fl. 8" Conc. Pipe
to Drain #4) 8.36

Drain #5 Top 24" vert. CMP. 6.82

Drain #5 Grate 6.16

556
X

B.M.			4.21	7.17	7.19
T.P.	11.38	11.38	5.48	0.00	

Drain #10 Btm 24" Vert CMP 9.9

Drain #10 Top 24" Vert CMP 6.78

Drain #10 FL 8" From Drain #9 7.42

Drain #10 Grate 6.03

5.48
↑

SUBP Santa Clara Pl
& Mission Beach Sea Wall

D. Smith Re Check X sec Blk "B" Riviera

W. Moore

J. Clark

E. Acuna

Note: Added Notes to
FB 1806 21-27

TP ↙ 1192 7² Lt Top End of wall 28333 ✓
1142 283³³

INDEXED

W.K.

JUL 28 1949

5710 7² Lt E single garage con floor + apron

3+16 E SMH

2775 13⁵ Rt E double garage con floor + apron

TP 85° 294⁷⁴ 264 286²⁴

BM ↙ 705 288⁸⁸ 281⁸³ SW cor Apron

1160 18⁹ Lt start con apron to double garage

Lt

E

Rt

43

292.56

292.37

218
132
Floor

237
72
Apron

290.06

468
on rim

288.25

288.54

640
135
Apron

620
185
Floor

29474

0+17.5 Beg Conc Slab for Highway

0+01.3 End Cb Inlet

0-08.7 R Cb Inlet & 24" Conc. Pipe

0-18.7 Beg Cb Inlet

0-40

T.P.	3.88	24.51	8.20	20.63
B.M.	0.51	<u>28.83</u>		28.32

20.63	20.22	20.11	20.02	19.09
3.88	4.29	4.30	4.19	5.12
0.7	0.7		5	5
Wall	Wall		Cb	6

19.5	19.61	19.61	19.61	18.59
5.10	4.90	4.90	5.93	
	5	5	5	
	Cb	Cb	6	

19.3	19.62	18.34	12.84
5.13	4.89	6.14	10.87
	5	5	5
	Cb	Grate	Pl.

19.5	19.64	19.66
5.10	4.87	5.15
	5	5
	Cb	Cb

19.3	19.81	18.52
5.13	5.00	5.15
	5	5
	Cb	6

24.51
NEBP Gravitia & Vista Del Mar

CC 217

5.03 1948 1948

0+60

0+42.5 End conc. slab for Stairway

0+30 & Stairway

0+21.9

24.51

Wly Edge septic Tank center sq. with

FR 126

P 19

19.9
20.10
19.16

20.41
20.35
20.35
20.37
19.31

380
0.7
16.11
18.40
286
Blm
Tread

2/6
0.6
Top

20.34
20.34
20.23
19.28

5
5
5
5

5
5
5
5

20.28
20.16
19.21

5
5
5

24.51

Storm Drain through Lot #10

Mission Bay Park Tract

Sommermeier
McCoy
Allen
Burch

3-6-50
W.O. ~~20006~~
20651

INDEXED

Y.K.
MAR 7 1950

= Fd. Conc. Mon.

■ = set. 1/2 disk

x = Cut chisel cross

Map 1120

Tie P.t. shoot #1516

" " " 1610

Def. rate for 1933.7 Rad = .889' per foot.

" " " 1993.7 " = .862' " "

1+40

Δ 1°-29' Lt

stub. in fill over pipe

47

0+62.3

Δ 4°-30' Lt.

= start 24" conc. pipe

0+15 (See p. 48 Left.)
for Prop. Tie.

0+00

Δ 5°-45' Rt.

90°-09' off Tang.

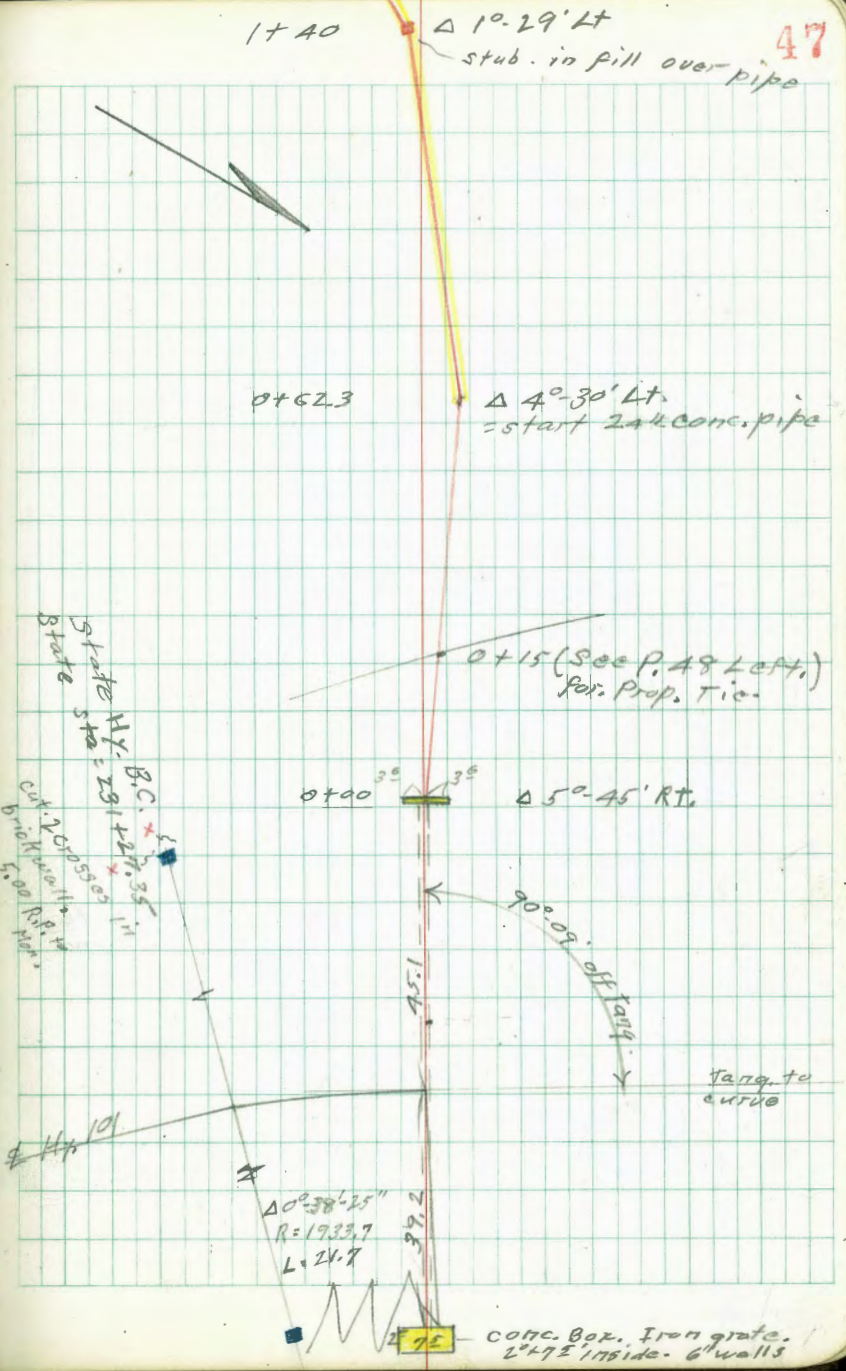
Tang. to curve

State
Highway
Sta = 291 + 27.35
BC. x
Cut 2 crosses
brick walls
500 R.R. W.
Mar.

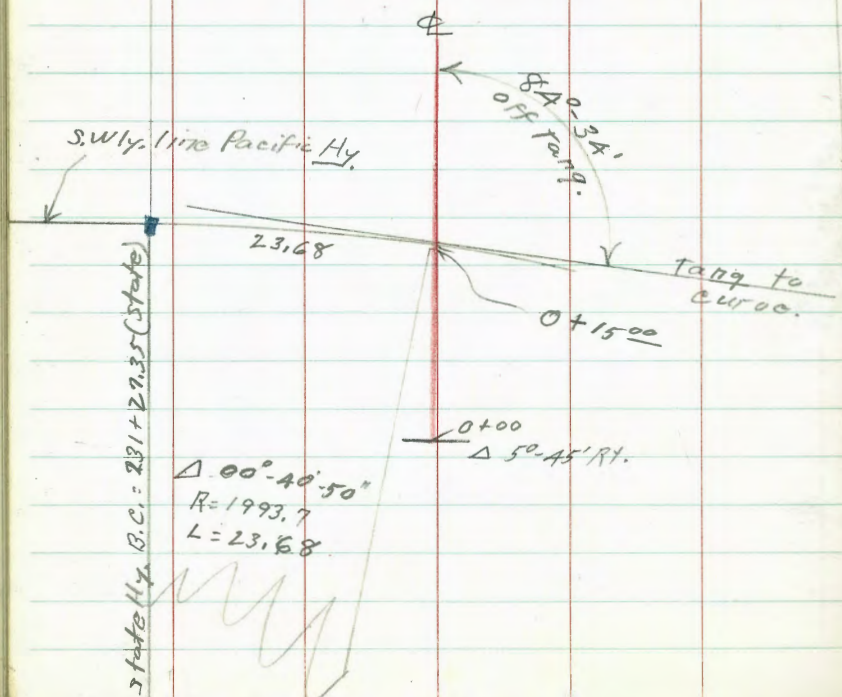
Δ 0°-38'-25"
R = 1933.7
L = 24.7

39.2
75

conc. Box, Iron grate.
2' x 7' inside 6" walls



Lot 10
Mission Bay Park Tract.



3+00 • End of ditch

2+07.2 • End of pipe

1+40 • $\Delta 1^{\circ} 29' 44''$

Levels Culvert
Lot 10 Mission Bay Park Tract.

$\Delta 4^{\circ}30''$ Ht.
0+62³ = start existing 24" Conc. culvert.

= $\Delta 5^{\circ}45'$ Rt. Culvert.
0+00 Invert. end of existing 24" Conc.

0-00⁴ Top of Head wall

0-84 on Head wall of box

0-84³ = intake existing culvert under Hy. 101.

Ely. B.C. Man
State Hy. 101 231+27.35

5.69	15.70 ✓	7.06	10.01 ✓
------	---------	------	---------

T.P.	2.51	17.07 ✓	7.46	14.56 ✓
	1.00	22.02 ✓	—	21.02 ✓

B.P. in Service station pump Island
N.Y. Co. Balboa + Pacific

4.75
10.95
I.F.
7.90
7.80

8.88 6.82 3.6	8.90 6.80	8.90 6.80 3.5
10.54 5.16 4.25	10.51 5.19	10.48 5.22 4.25
13.15(?) 2.55 Grate	7.52 8.18 7.5	(INVERT ELEV.)
	15.70 ✓	

REDUCED -
REKUNA

DATA FROM STATE X-SECTS.:

E EL. = 11.31 INCREASED TO 11.50

INV. EL. N. END = 7.54

" " S. " = 5.9, HDWL = 6.9

S. CREST = 034'5 EL = 11.8

N. " = 0-33 EL = 11.0

STATION = 231450

Mon. Ely. Cor. Bunker Hill 6.19 9.51 ✓
+ Pacific (Hy. 101)

ditch thru filled ground
3+00 = ground shot at end of

2+07¹ = End of pipe.

1+40 = Δ 10 29' Lt.

2.5

13.2

3.32

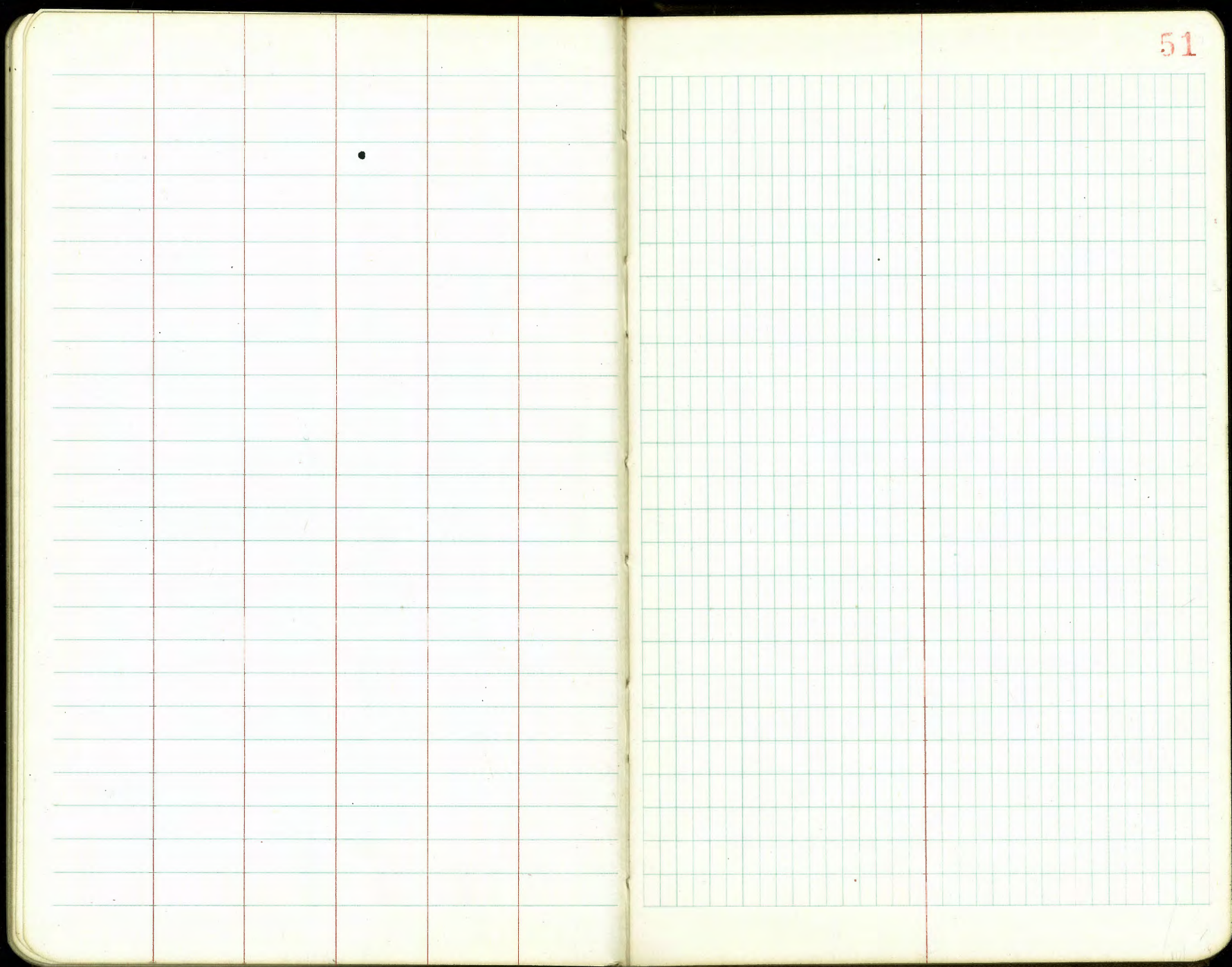
12.38

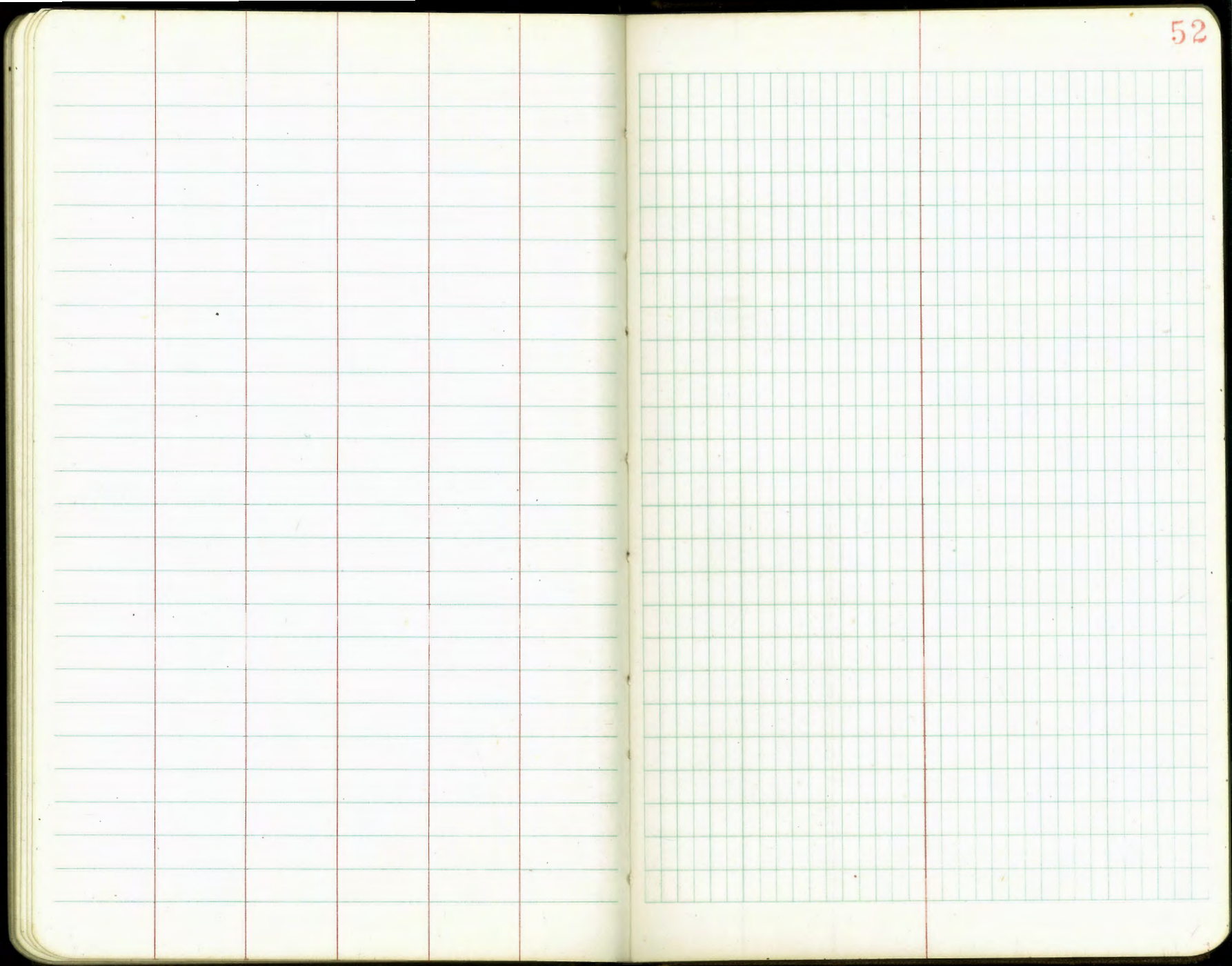
4.09

11.61

I.E.

15.70



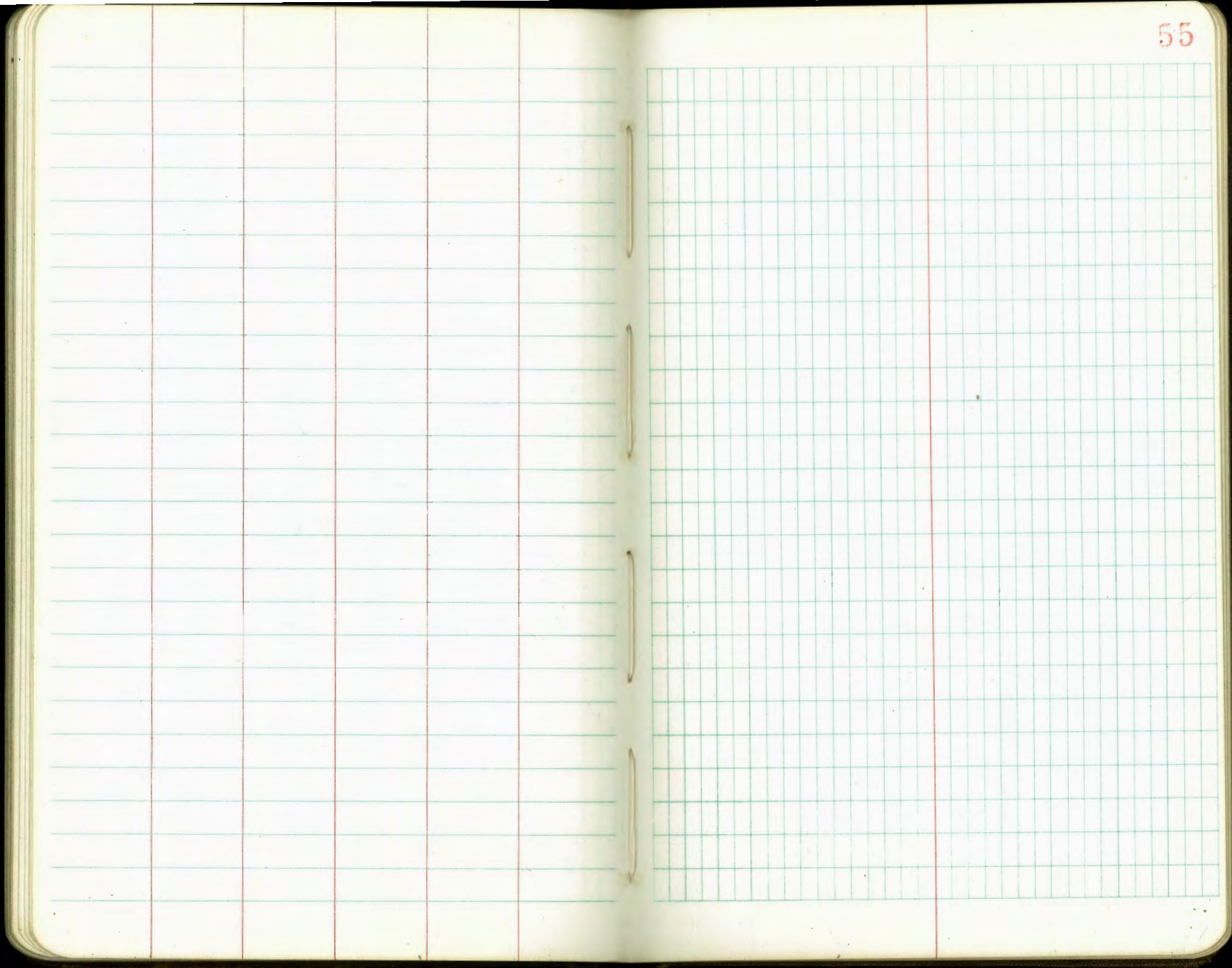


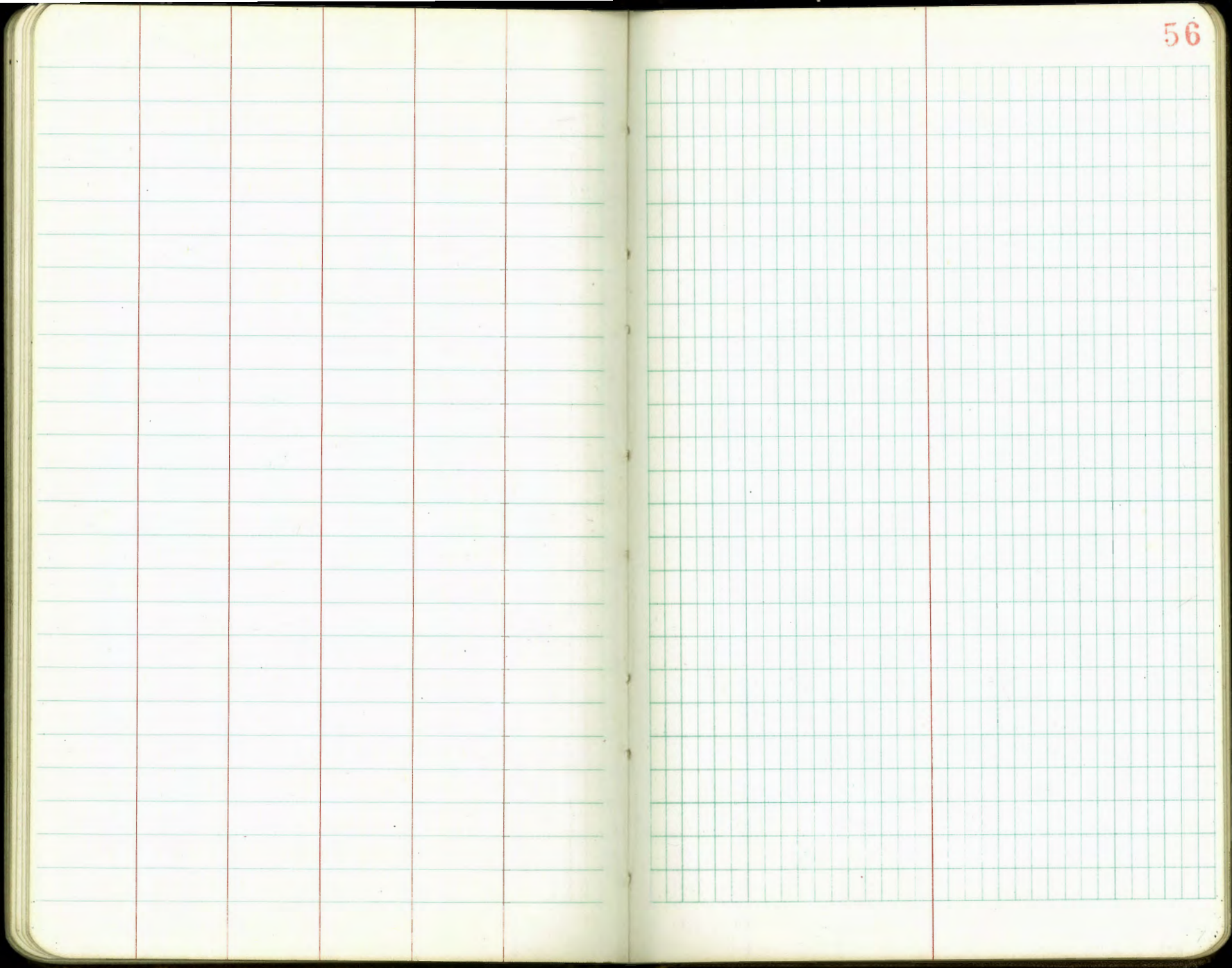
A table with 6 columns and 20 rows. The columns are defined by vertical red lines, and the rows are defined by horizontal blue lines. The table is currently empty.

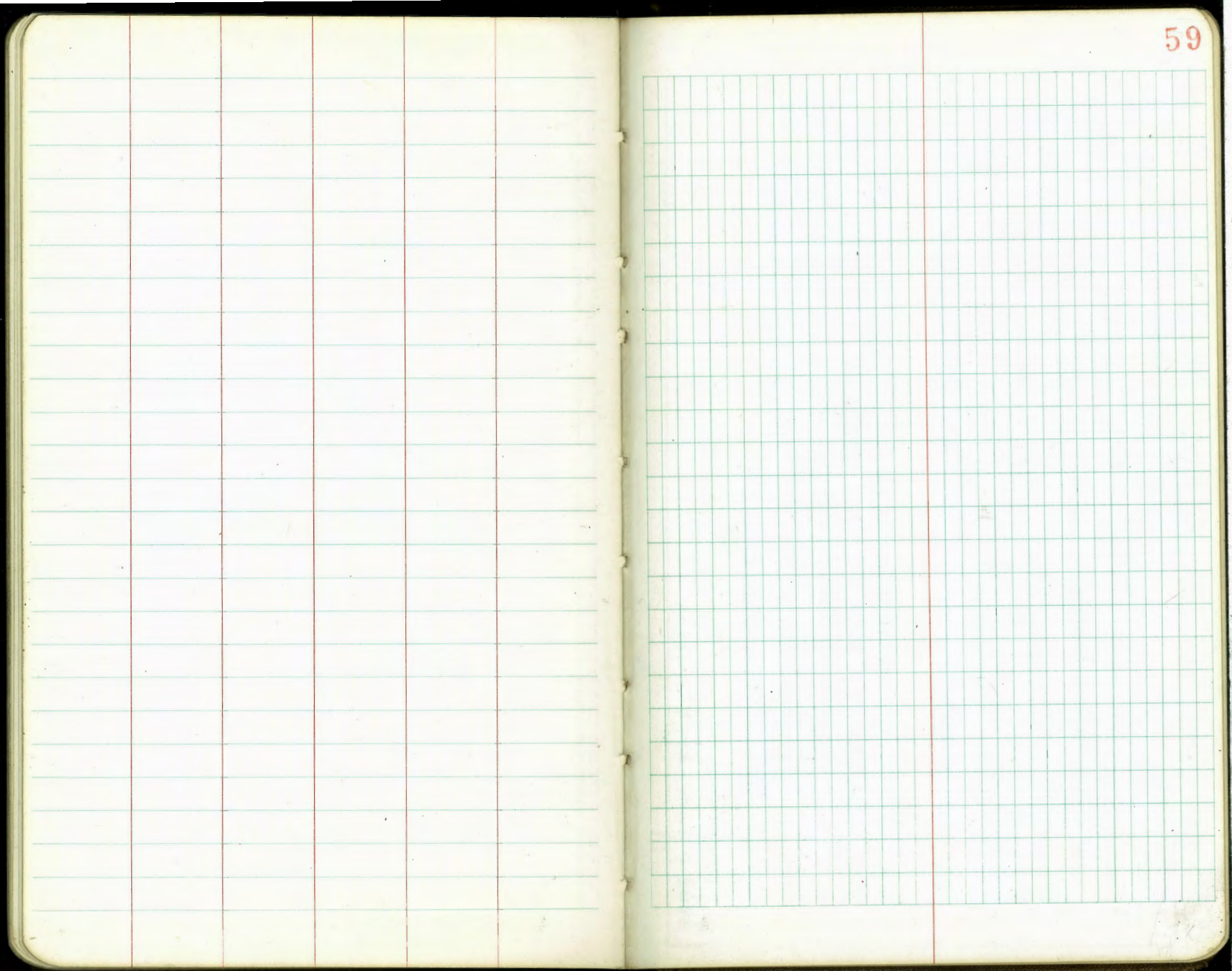
A table with 1 column and 20 rows. The rows are defined by horizontal blue lines. The table is currently empty.

A table with 6 columns and 20 rows. The columns are defined by vertical red lines, and the rows are defined by horizontal blue lines. The table is currently empty.

A table with 1 column and 20 rows. The rows are defined by horizontal blue lines. The table is currently empty.

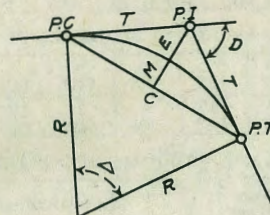






DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ = Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. $- T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. $+ L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158—Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

675
67

942

1122 Arbor Vitae

Mrs. Nelson

366.66

7.61

374.27

1.15

373.12

7.80

380.9

9103 25

6102.17

30108

1175
8/94

8509

6102.17

62726

8

14

8

60

5

189-59-60

7324 30

10635 30

376041

7679

23712

582
22
362

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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