

1803

1803

120

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 - (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.

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Made in U. S. A.

Survey Lot H Blk 172 Mission Beach

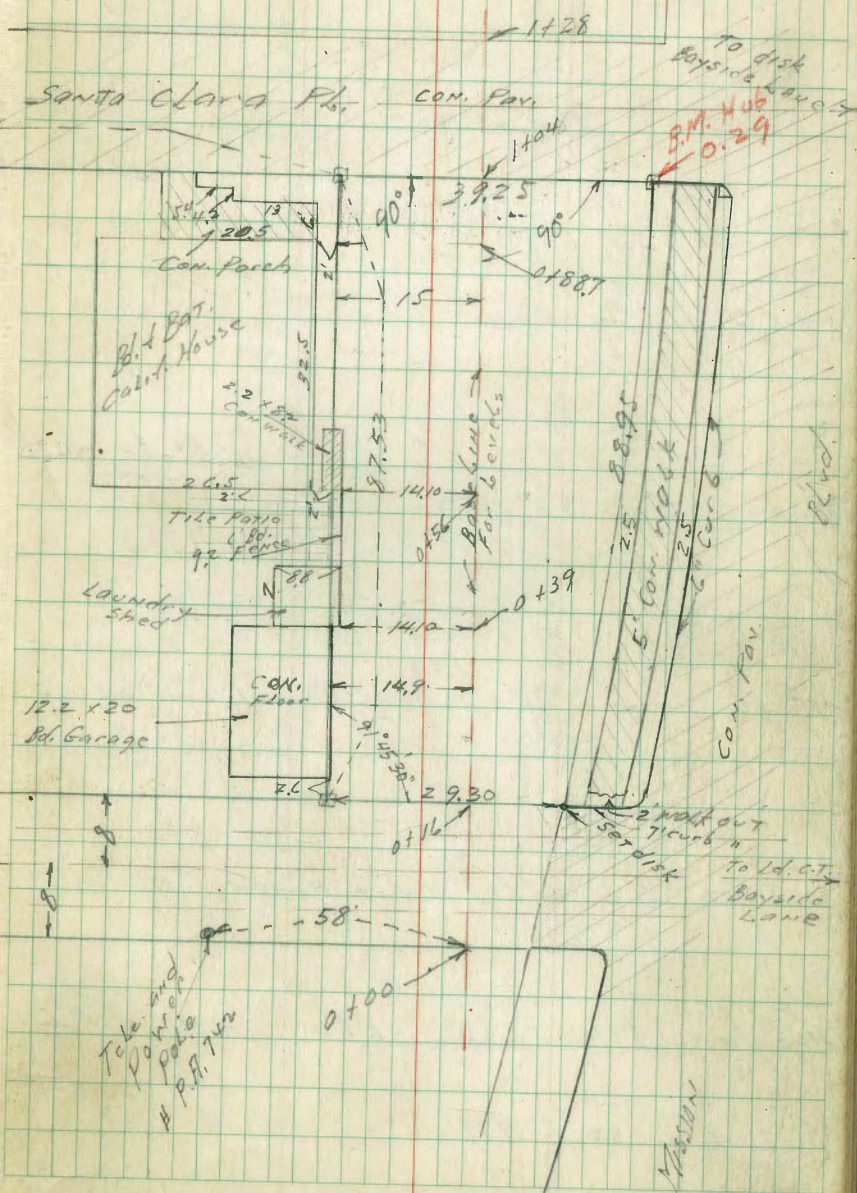
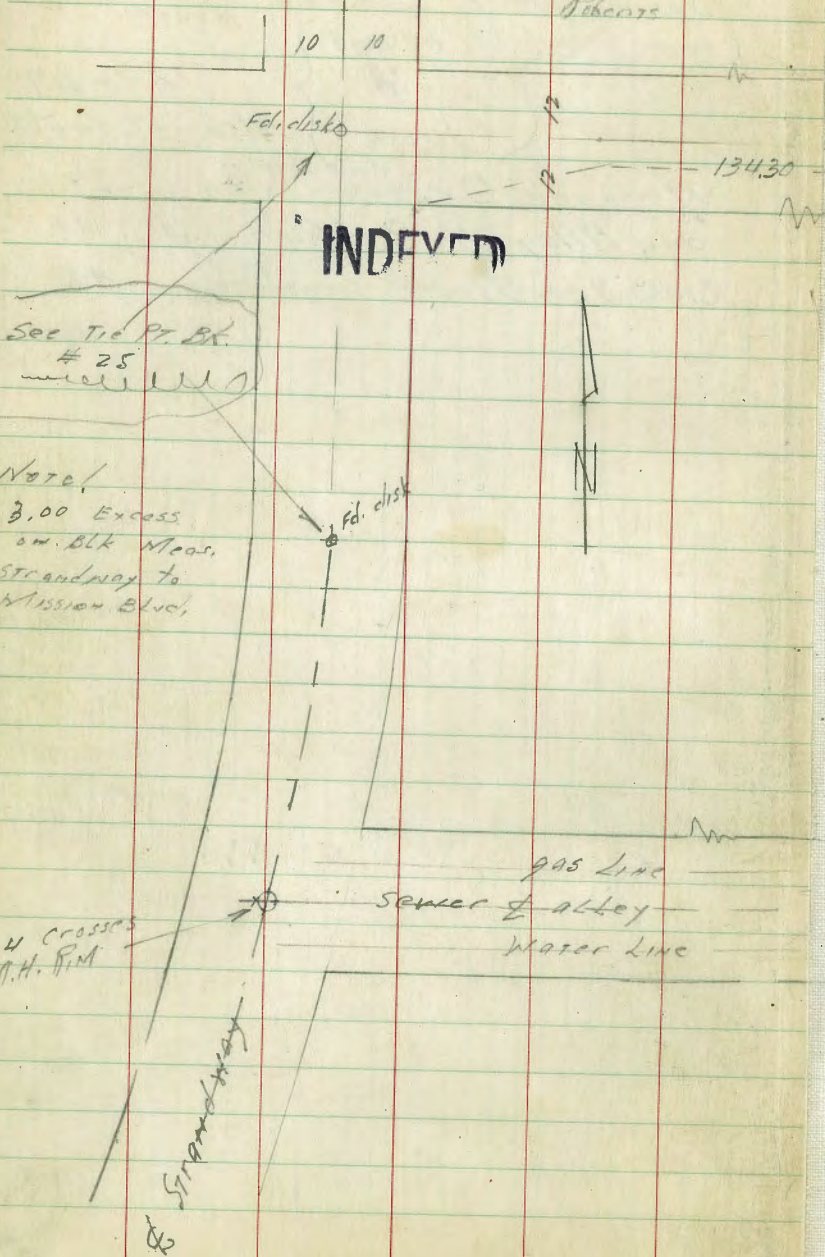
Cross Sec.	{ Oliphant }	
	{ Tustin }	4 to 27
	{ Clove }	Also 52 to 56
Warnera Dr.	{ Capistrano }	} 28 to
and Alley Blk B	{ Pt. Loma Hgts. }	
Cross Sec. Oliver	{ Faniel to Gresham }	41
		42-51

Indexed
C. SIKI

Moore
Begg 10-21-47
Green
Peters

Survey Lot A Blk 172
MISSION BEACH
2 1/2" Hubs & disks W.O. 90060

1



INDEXED

Indexed

Cross Sec. Oliphant
 " " Tustin Macaulay to Oliphant
 " " Clove " " "

W.O. 25001 Sommermeier
 11-7-47 W. Moore
 E. Sherman

■ = Fd. old Hub.

■ = Set 1/2 Hub + disk
 (Poor condition)

R ■ = Replaced old Hub with Hub + disk

● = 4 Crosses in M.H. Rim

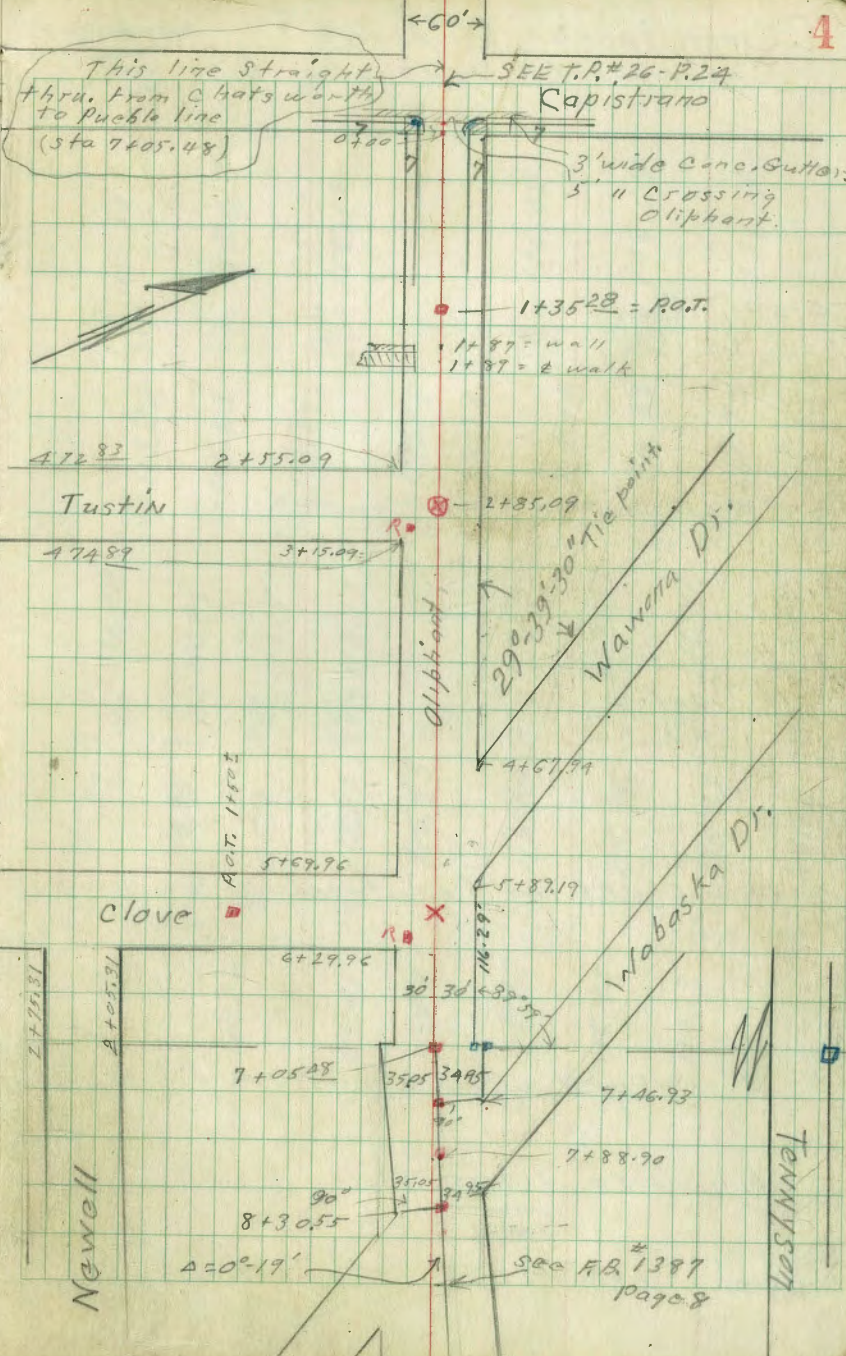
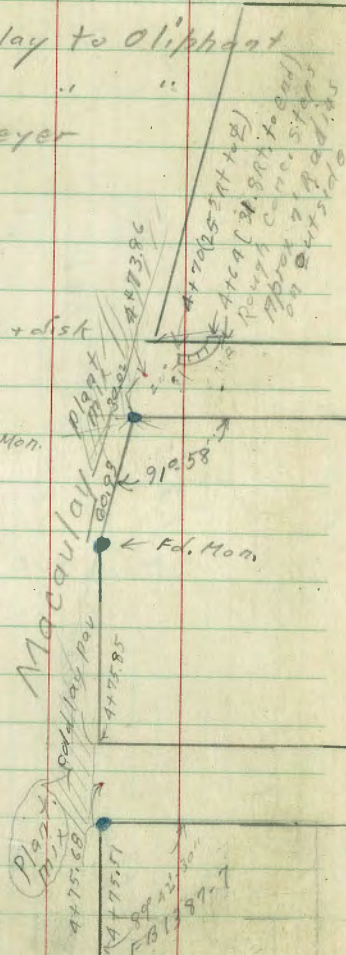
X = X N.W. Rim of M.H.

• = Set Nail

NOTE

A ~ = additional note
 on Page 52 -

Also 2038
 67



Cross Section Olyphant
Capistrano to Vapaska Dr.

4-10-47

Indexed

5

0-08 Cont.

0-08 Ely. Edge Conc. gutter.

0-10 Cont.

0-10 = Ely. Cb. line Capistrano

0-13 = Wly. Edge Conc. gutter

T.P. 0.50 119.03 13.16 118.53

N.W. 3' Tie
Back, 44 ft

1.82 131.69 — 129.87

Macaulay
+
Capistrano

	115.90	115.63	115.12	116.02	116.63	116.90
	3.13 24.2 Top. Oc.	3.4 24.2 Dirt	3.71 24.2 Conc.	3.91 23.6 Conc.	2.4 23.6 Dirt	2.13 23.6 Top. Oc.
	115.63	115.22	115.53	115.39	115.58	115.73
	3.4 20 Dirt	3.81 20 Conc.	3.5 20 Dirt	3.64 20 Conc.	3.45 20 Butt & Dirt	3.3 20 Dirt
	115.82	110.83	113.17	112.17	116.27	117.27
	7.21 80 Oc.	8.10 109 Butt	5.86 86 Oc.	6.86 86 Butt	2.76 80 Butt	1.76 80 Oc.
	115.94	114.94	115.10	115.27	115.43	115.60
	3.09 20 Oc.	4.09 20 Butt	3.93 20	3.76 20	3.60 20	3.43 20
	115.04	115.23	115.41	115.57	115.77	115.93
	3.77 20	3.80 20	3.62 20	3.46 20	3.26 20	3.10 20
	116.13	115.93	116.96	117.58	116.56	117.58
	3.10 20	3.10 20	2.97 20 Butt	1.45 150 Oc.	2.47 150 Butt	1.45 150 Oc.
	119.03					

0+73 29² Lt. = start lath house

0+71 29² Lt. = End shed - out

0+60 A ~ ~ ~ ↙ out

0+61 29² Lt. = End lath house start shed

0+50 29² Lt. = start lath house - out

0+50 A ~

0+40 A ~

0+30 30' Lt. = 2' Diam. Eucalyptus

0+26 A ~

0+195 A ~

0+0.5

T.P. 10.31 127.74 1.60 117.43

0+00 Cont.

0+00 = Ely. line Capistrano

119.03

115.96	6.7 30	121.04	5.7 30	122.04	5.5 30	122.29
116.93	8.2 28	119.54	7.0 12	120.74	6.1 12	121.64
116.53	8.0 14	119.74	7.7 7	119.84	6.5 0	121.24
116.33	10.7 10	117.04	7.9	119.84	6.2	121.54
116.23	11.0	116.74	7.7 6	120.04	5.7 0	121.84
116.63	127.74	117.29	5.8 8	121.94	4.7 16	122.84
117.93	10.9 6	116.84	4.8 18	122.94	4.0 17	123.74
117.73	8.0 9	119.74	4.1 27	123.64	3.4 26	124.34
116.93	6.2 30	121.54	3.6 30	125.14	2.7 30	125.04
			4.6 30	125.14	2.7 30	125.04

Back edge solid
Return (Also around)

Also back edge
solid return.

3.07
2.0
Top. sh.

2.6
2.0
Erd

2.5
1.6

2.7
9

2.8

2.4
4

1.1
8

1.3
195
Erd.

2.10
19.5
Burb
Erd.

119.03

Oliphant

T.P. 212 P.O.T.
1+35.28 3.80 124.80 6.74 121.00 B.M.# 2

1+07

1+05 29⁸ Lt. = start 6" wide Conc. wall.

1+03

1+00

0+98 A ~
0+88 A ~
0+85 A ~

0+80

127.74

#

7

122.14	120.94	120.74	121.84	121.94	122.74	123.34	125.14	125.44
5.6 30	6.8 40	6.3 23	5.9 29.5	5.6 22	5.0 16	5.0 7	5.4 10	2.3 30
122.19	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
5.7 40	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
122.34	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
5.4 29	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
122.54	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
5.7 30	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
122.74	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
5.5 6	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
122.54	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
5.2 7	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
123.04	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
4.7 7	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
124.04	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
3.7 11	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30
125.54	120.84	120.64	122.25	122.64	122.74	123.84	125.04	125.64
2.2 30	6.9 30	7.1 29.8 Bottom Footings	5.49 29.8 Top wall	5.1 15	5.3 7	4.8 7	2.7 20	2.1 30

127.74

1+27

1+22

1+20

1+18 29th Lt. = End conc wall + lath house

1+17 Cont

1+17 20th Rt = Ctr. P. pole #

124.80

119.60	120.80	121.70	120.20	121.10	121.40	122.06	122.80	123.50
$\frac{5.2}{35}$	$\frac{4.0}{30}$	$\frac{3.1}{26}$	$\frac{4.6}{21}$	$\frac{3.7}{18}$	$\frac{3.4}{7}$	2.8	$\frac{2.0}{15}$	$\frac{1.3}{30}$
119.90	120.00	120.9	120.2	120.6	121.1	121.80	122.7	123.4
$\frac{6.2}{30}$	$\frac{5.4}{30}$	$\frac{4.3}{19}$	$\frac{3.3}{8}$	$\frac{2.5}{8}$	$\frac{2.1}{15}$	3.0	$\frac{1.7}{30}$	
118.60	119.90	120.50	121.50	121.50	121.50	121.50	122.50	123.30
121.60	120.30	121.20	121.80	121.60	121.70	122.20	123.20	125.20
$\frac{3.3}{24}$	$\frac{1.5}{21}$	$\frac{3.6}{19}$	$\frac{3.0}{14}$	$\frac{3.2}{7}$	2.6	$\frac{1.6}{16}$	$\frac{+0.4}{20}$	$\frac{+0.6}{30}$
121.90	120.70	121.70	121.50	121.50	121.50	121.50	122.50	123.30
2.9	4.1	3.3	2.9	2.9	2.9	2.9	2.9	2.9
Top wall	Bottom footing	Bottom footing	Bottom footing	Bottom footing	Bottom footing	Bottom footing	Bottom footing	Bottom footing

124.80

Oliphant

1+875

1+87 20' Rt. = £ 6" conc. wall

1+86

1+73 23' Rt. = Ctr. 15" pepper tree

1+55

1+53 30' Rt. = End lath fence & start wire fence

1+40

1+35 30' Rt. = start lath fence.

124.80

118.46	119.90	119.20	116.40	116.90	117.20	117.10	118.52	117.20	117.60
0.9 30	4.9 30	5.6 30	8.4 30	8.2 30	8.1 15	7.7 15	6.28 2014 top wall	7.6 2014 Base. Footing	7.2 30
119.40	120.20	119.60	116.60	116.96	117.40	117.10	118.90	119.20	117.50
5.1 30	4.6 25	5.2 20	8.4 30	7.7 15	7.4	7.7 15	5.7 20	5.6 30	7.2 30
120.00	120.70	119.60							
4.8 19	4.1 10	5.2 10							
120.90	120.50	119.20							
3.9 9	4.7 6	5.6 6							
121.10	120.80	119.50							
3.7 9	4.0	5.3							
121.70	121.30	120.90							
3.1 6	3.5 7	3.9 12							
123.00	122.30	121.90							
1.8 18	2.5 11	2.9 20							
123.60	123.40	122.60							
1.2 30	1.9 30	2.2 30							

124.80

118.58
6.22
30
off wall

Set. B.M. Oliphant
 X in Wly.
 side M.H.
 Right & Tustin
 + Oliphant

55

10.10

102.25

Sat.
 B.M.
 #3

10

2+70

101.65
 $\frac{10.7}{80}$

102.95
 $\frac{9.4}{30}$

103.55
 $\frac{8.8}{15}$

104.35
 8.0

107.95
 $\frac{7.4}{15}$

105.45
 $\frac{6.9}{20}$

105.45
 $\frac{6.9}{30}$

2+55⁰⁹ = Wly. line Tustin

105.45
 $\frac{6.9}{30}$

106.25
 $\frac{6.1}{15}$

107.15
 5.2

107.35
 $\frac{5.0}{15}$

108.25
 $\frac{9.1}{30}$

2+53 22² Rt. = @ P. pole # 3501

T.P. 0.38 112.35 12.83 111.97

112.35

2+30 A 21⁵ Rt. = 8" Diam. pepper tree.

109.30

110.60

111.70

112.90

114.10

115.10

2+20 A

155

142

131

11.9

10.7

9.7

2+14 27⁸ Rt. = Ctr. 6" Diam. tree.

112.30

113.60

113.90

114.90

115.70

116.30

117.00

2+10 A

2+03 A

2+00

12.5

112

10.9

9.9

7.1

8.5

7.8

1+89 20² Rt. = @ 3' wide Conc. walk

7.20
 20.4
 @ walk

7.19
 30
 walk

124.80

124.80

Oliphant

4+00

3+50

3+15⁰⁹ = Ely line Tustin

Sly. 7' Hubs
T.P.

0.57 100.83 12.09 100.26

Oliphant &
Tustin

2+98

2+95

185⁰⁹ Cont.

2+85⁰⁹ E. Tustin

112.35

140
50
86.83

13.6
30
87.23

13.7
20
87.53

10.7
90.13

10.1
6
90.73

7.1
25
93.73

5.0
30
95.83

3.6
50
97.23

9.5
30
95.33

5.3
15
95.53

1.8
96.03

7.1
15
96.63

3.8
25
97.03

2.8
30
98.03

2.6
40
98.23

3.4
30
97.43

2.5
15
98.33

1.8
99.03

1.9
15
99.73

1.1
30
99.73

97.65

14.7
50
99.55

14.5
30
100.25

13.5
15
100.25

100.83
11.7
101.25

11.2
15
101.55

11.0
30
101.85

99.55

100.25

100.25

101.25

101.55

101.85

12.8
50

12.1
30

12.1
15

11.1

10.8
15

10.5
30

10.9
30
101.45

10.5
15
101.85

9.8
102.25

9.3
15
103.05

9.2
30
103.15

10.10
on. M.H.
R/07

112.35

oliphant

5+69⁹⁶ = Wly. line Clove

5+30⁵⁶

5+00

4+67^{9A} = Int. Wly. line Wawona + N. line oliphant

T.P. 5.53 93.28 13.08 87.75

4+50 { 17^L Lt = Guy. pole 30^L Lt. = Dead man
21^R Rt. = Ctr. P. pole # P3475

4+35

100.83

12

13.2	11.2	9.0	7.0	5.7	4.5	2.9
<u>50</u>	<u>30</u>	<u>15</u>		<u>12</u>	<u>15</u>	<u>30</u>
80.08	82.08	84.28	86.28	87.58	88.78	90.88
81.78	84.38	86.88	88.68	89.28	90.88	92.98
11.5	8.9	7.4	4.6	4.0	2.1	0.3
<u>50</u>	<u>30</u>	<u>18</u>		<u>9</u>	<u>12</u>	<u>30</u>
81.28	84.28	86.28	88.08	88.18	90.08	92.98
12.0	9.2	7.8	5.2	5.1	3.2	0.3
<u>50</u>	<u>50</u>	<u>15</u>		<u>7</u>	<u>12</u>	<u>30</u>
78.18	81.88	84.78	87.48	88.18	89.98	92.78
15.1	11.4	8.5	5.8	5.1	3.3	0.5
<u>50</u>	<u>30</u>	<u>15</u>		<u>7</u>	<u>14</u>	<u>30</u>

93.28

80.43	82.33	86.73	88.63	90.13	92.43
20.4	18.5	14.1	12.2	10.7	8.4
<u>50</u>	<u>30</u>	<u>15</u>		<u>15</u>	<u>30</u>

100.83

Oliphant

7+46.93 at 90° to B.L. See sketch page 4

7+23 Cont.

7+23
T.P. 0.21 74.02 13.24 73.81

Note. From here on base line is 0.05
North of ϕ Oliphant, see sketch
page 4.

7+05⁴⁸ Cont.

7+05⁴⁸ Intersect. Pub. line

87.05

B.L.

14

52.32	52.12	51.92	52.82	59.32	61.6	61.72	60.52	64.32	69.42	73.22
21.7 92 Pav.	21.9 35 Pav.	22.1 28 Pav.	21.2 25	14.7 15	12.86 0.17 Hib	12.3 1	13.5 0	7.7 12	4.6 35	0.8 50
		52.52		52.22		73.22		79.02		
		21.5 69 Pav.		21.8 46 oil pav.		0.8 30		4.50 50		
53.22	57.82	62.32	64.32	65.62	66.42	65.92	68.22	70.82		
20.8 14	16.2 35	14.7 15	7.7 8	8.4	7.6 4	8.1 8	5.8 10	3.2 20		
			74.02							
52.85	52.55	54.15	54.65	79.95	83.15	85.55	86.55			
34.2 80 ditch rd.	34.5 65 oil rd.	32.7 60	32.9 56	7.1 30	3.9 35.05	1.5 40	0.5 50			
60.05	61.75	63.55	68.15	69.35	70.05	68.85	72.55	75.85		
27.0 47	25.3 34.75	23.5 30	18.9 8	17.7	17.0 4	18.2 7	14.5 12	11.2 24		

87.05

Olipiant

Nly. B.P.
Poc + Capistrano

3.82 ^{+ 0.02} 71.72 71.70

T.P. 10.15 75.54 4.58 65.39

T.P. 5.23 69.97 9.28 64.74

8+30.55 90° to B.L.

7+88.9 Cont.

7+88.90 90° to B.L.

4+84 90° to B.L.

74.02

B.L.

15

23.8	23.8	22.4	18.0
35	36.5	37	48
PAV	PAV		
50.22	50.22	51.62	56.02
61.22	65.62		
12.8	8.4		
35	30		
51.22	51.12	53.92	57.32
22.8	22.7	20.1	16.7
PAV	PAV	6	12
51.22	51.12	53.92	57.32
51.62	53.52	56.42	63.62
22.4	22.9	20.6	10.9
23	1	20.5	17.6
PAV	PAV	9	6
51.62	51.12	53.42	63.62
51.62	51.12	53.52	63.62
56.42	56.42	56.42	63.62
67.92	67.92	67.92	67.92
67.92	67.92	67.92	67.92

74.02

Tustin

A ~ = Additional notes
on page 5A-56
7/19/50

B ~ = Additional notes p. 57-71-140 1951

T.P. 11.90 122.94 0.35 111.04

0+74 B ~

0+74

0+73

0+54 B ~

0+41 B ~

0+35 22^E Rt. = 12" Diam. Tree.

0+32

0+31 22^E Rt. = Dtr. 12" Diam tree.

0+15 B ~

0+00 = Sly. line Oliphant (online oliphant)

Sly. 7' Hubs.
Tustin +
Oliphant
page 11

11.13 111.89 — 100.26

Also P-54 + 56 + 57
 June '51
 July 1950

99.69	98.89	100.69	100.89	100.89	102.89	105.89	107.89	107.89	108.19	110.29	110.89	112.59
11.7 30	12.5 30	10.7 50	10.5 50	8.5 50	7.1 30	5.5 17	3.4 6	3.2	1.1 16	0.5 18	+1.2 30	
101.39	99.29	100.99	100.99	102.69	105.59	107.89	107.89	107.99	110.19	110.69	112.49	
12.1 40	12.1 40	8.7 30	8.7 30	5.8 17	5.8 17	3.5 6	3.4	1.2 16	0.7 18	+1.1 30		
101.89	100.39	101.59	100.69	101.59	103.29	104.99	104.99	106.29	107.29	109.89		
2.5 10	14.8 30	9.8 30	10.7 50	9.8 30	8.1 15	6.4	5.1 15	4.1 18	1.5 30			
103.09	109.29	109.99	98.89	99.29	103.29	104.99	106.19	107.19	107.89			
6.4	5.2 15	4.2 18	1.5 30									
105.39	107.89	107.89	107.89	107.89	107.89	107.89	107.89	107.89	107.89	107.89	107.89	107.89
6.0 15	9.5 30											
111.39												

Tustin

T.P. 12.26 147.01 0.09 134.75

2+63 A ~

2+50

2+35 A ~

2+20 A ~

2+90 A ~

1+75 A ~

T.P. 12.44 134.84 0.54 122.40

1+55 A ~

1+53

1+52

1+35 A ~

1+12

1+11

0+96 B ~

122.94

17

118.34	126.44	8.4	50
121.24	128.54	6.3	30
123.04	130.64	4.2	15
125.24	131.74	3.1	4
124.64	130.84	4.0	2
129.74	130.84	4.0	
125.94	131.34	3.5	14
127.14	132.24	2.6	22
127.84	132.54	2.3	30
	134.74	0.1	50
118.34	111.34	16.5	50
114.34	114.34	13.6	30
116.04	116.04	11.8	15
118.54	118.54	9.6	3
118.54	134.84	10.2	2
119.24		10.1	
120.14		8.9	17
121.34		7.7	19
122.94		7.0	30
108.34	111.34	11.6	50
112.44	114.34	8.6	30
115.84	116.04	6.9	17
118.44	118.54	4.9	8
119.04	119.24	3.7	
120.34	120.14	2.5	17
121.14	121.34	1.6	19
122.74	122.94	0.0	30
107.44	108.34	14.6	50
109.54	112.44	10.5	30
111.34	115.84	7.1	19
113.64	118.44	4.8	8
113.94	119.04	5.7	
115.44	120.34	2.6	17
116.24	121.14	1.8	19
117.54	122.74	0.2	30
104.24	107.44	15.5	50
107.34	109.54	13.4	30
111.24	111.34	11.6	16
113.44	113.64	7.3	7
113.84	113.94	7.0	
115.24	115.44	7.5	17
116.34	116.24	6.7	19
117.44	117.54	5.9	30
104.24	104.24	18.7	50
107.34	107.34	15.6	30
111.24	111.24	11.7	16
113.44	113.44	7.5	7
113.84	113.84	7.1	
115.24	115.24	7.7	17
116.34	116.34	6.6	19
117.44	117.44	5.5	30

122.94

3+23 ^{Cont.} / 30³ Rt. = 6" wide Fly + Wly Conc. wall.

3+23

3+16 A ~

2+95 A ~

2+93 Cont.

2 steps to street

2+93 31⁸ Rt. = 4" wide Conc. walk with

2+78

2+76 A ~

2+73

147.01

16.5 30	14.8 15	13.3 4	13.7 2	13.6	12.7 15	10.8 30	8.9 35	138.11	136.21	136.91	138.61	139.01	138.61	137.51	136.61	135.01	134.01	134.01	133.81	133.31	133.01	132.21	132.91	131.31	131.31	142.31	141.01	141.11	140.78	142.21	143.41	143.41	145.26	
7.0 16	5.6 18	4.8 28	3.6 30.2 Ord.	7.6	7.0	5.6	4.3 30.2 Base of footing	3.6 30.3 top of wall	7.0	7.5	8.7	8.0	9.7	10.4	11.2	11.3	14.0	12.7	14.2	14.2	11.3	11.2	10.4	9.5	9.7	8.0	7.98	7.98	7.98	7.98	7.98	7.98	7.98	7.98
136.61	138.11	139.61	139.11	139.41	140.01	141.41	142.21	143.41	143.41	142.21	143.41	143.41	142.21	141.41	140.01	139.41	139.11	138.61	138.11	137.51	136.61	136.21	135.71	135.81	135.01	134.01	134.01	133.81	133.31	132.91	132.81	132.81	132.81	132.81
35.6 Top of top step	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6	35.6
6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23	6.23

147.01

TUSTIN

4+45 = 31' At. = End 5' wide Cactus Clump.
4+40

4+29 31' At. = Start of 5' wide Cactus clump.
4+25

4+20 A ~
4+05 B ~
4+00

3+73 36" At. = 8" wide E+W. conc. wall.

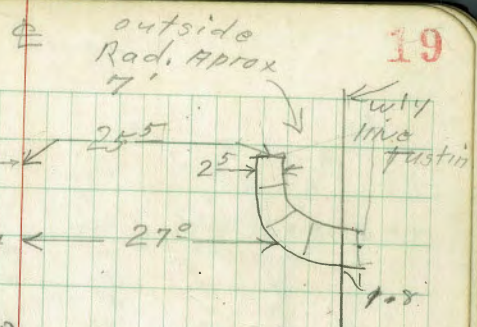
3+55 A ~

T.R. 7.94 154.50 0.45 146.56

3+41 A ~

3+26

147.01



Detail Rough
Conc. steps

148.20	149.30	150.20	149.60	149.50	150.00	151.50	152.90
<u>6.3</u> 30	<u>5.2</u> 15	<u>4.5</u> 7	<u>4.9</u> 5	5.0	<u>4.5</u> 13	<u>3.0</u> 17	<u>1.6</u> 30
147.60	148.20	149.40	149.00	149.10	149.70	150.80	
<u>6.3</u> 30	<u>6.3</u> 7	<u>5.1</u> 4	<u>5.5</u> 4	5.4	<u>4.8</u> 15	<u>3.7</u> 30	
145.70	146.50	147.70	147.40	147.60	148.2	148.70	150.00
<u>8.8</u> 30	<u>8.0</u> 15	<u>6.8</u> 8	<u>7.1</u> 0	6.9	<u>6.3</u> 15	<u>5.8</u> 17	<u>5.3</u> 27
143.20	143.60	145.30	144.90	145.20	146.60	147.20	147.00
<u>11.3</u> 30	<u>10.9</u> 18	<u>9.2</u> 7	<u>9.6</u> 3	9.3	<u>7.9</u> 15	<u>7.3</u> 30	<u>7.5</u> 30.2
145.71	145.41	144.21	143.41	140.51	139.61	140.21	138.71
<u>14.3</u> 35	<u>1.6</u> 31	<u>2.8</u> 30	<u>3.6</u> 18	<u>6.5</u> 15	7.2	<u>7.4</u> 2	<u>6.8</u> 4
				147.01			

A+73.86 Cont.

Taken on Nly line Macaulay

A+73.86 Intersect. Nly line Macaulay.

A+70 Cont.

A+70

A+64 Cont.

From 2³ to 2⁴ wide.

A+64 31⁸ Rt. ⁴ - 17⁴ of conc. steps.

154.50

145.50	146.10	147.50	147.60	146.60	146.50	146.90	147.60	149.20	149.90
9.0 35	8.4 30	7.0 15	6.9 8	7.9 6	8.0	7.6 8	6.9 13	5.3 15	4.6 29
						150.70	150.70	151.70	151.70
						3.8 25.5 # stop	2.8 27 end	2.8 29	2.8 30
148.40	149.50	149.70	147.20	147.10	147.20	148.10	149.70	150.50	
6.1 30	5.0 20	4.8 10	4.3 5	7.4	7.3 8	6.4 13	4.8 15	4.0 24	
					153.50				
149.46	150.00	149.70	147.90	147.90	148.80	151.00	151.70	151.90	
5.1 30	4.5 25	4.8 8	6.6 5	6.6	5.7 13	3.5 15	2.8 20	2.6 27 end conc	
					1.0 31.8	END of steps			

154.50

Tustin

Set, B.M.
Fly. Prop. Mem.
Macaulay + Tustin

8.94 145.56

Edge cold lay paving.
line of Macaulay. Also =

A+88 Along Existing Nly gutter

taken Along Macaulay

A+84 Sections from here on

154.50

137.50	142.10	143.10	139.80	146.00	146.90	147.70	147.80	147.30	145.70
17.0 100	12.4 50	11.4 35	9.7 15	8.5	7.6 15	6.8 35	6.7 50	7.2 70	8.8 100
145.10	146.20	146.40	145.30	145.90	146.80	147.50	149.00	148.30	
9.4 35	8.3 10	8.1 12	9.2 9	8.6	7.7 13	7.0 20	5.5 25	5.2 35	

154.50

Cross Sec. Clove - Oliphant to Macaulay

1+00

T.P. 12.06 110.27 0.15 98.21

0+65 27' Rt. = 12" Diam. Tree

0+61 23.3 Rt. = 14" Sundial set in 10"x10" - 3' High
Corr. Post.

0+60.

0+55 27' Rt. = 16" Diam Tree

4" off sheet trunks

0+45 26' Rt. = old olive tree 1' diam trunk with

0+35

0+20

0+00 = Sly. line Oliphant

x wly. r. in M.H.

& oliphant + 12.34

98.36

86.02

Clove
page 13

	98.57	99.07	100.27	100.37	100.97	101.57	
	$\frac{117}{50}$	$\frac{112}{30}$	$\frac{10}{17}$	9.9	$\frac{9.9}{11}$	$\frac{8.7}{50}$	
	97.96	97.76	97.26	97.06	96.66	96.96	97.36
	$\frac{0.4}{50}$	$\frac{0.6}{30}$	$\frac{1.1}{9}$	1.9	$\frac{1.7}{3}$	$\frac{1.7}{11}$	$\frac{1.0}{14}$
	94.96	96.76	95.86	95.26	94.86	94.66	95.26
	$\frac{3.9}{50}$	$\frac{1.6}{30}$	$\frac{2.5}{12}$	$\frac{3.1}{8}$	3.5	$\frac{3.7}{13}$	$\frac{3.2}{17}$
	93.56	93.06	92.96	93.36	92.96	93.66	94.66
	$\frac{4.8}{30}$	$\frac{5.3}{17}$	$\frac{5.1}{11}$	5.0	$\frac{5.4}{12}$	$\frac{4.7}{20}$	$\frac{3.7}{50}$
	89.36		90.86	90.66	90.66	91.06	
	$\frac{9.0}{30}$		7.5	$\frac{7.7}{11}$	$\frac{7.3}{30}$		
			78.36				

Clove

T.P. 10.00 119.85 0.42 109.85

2+28 21² RT. = Cr. 2A" Diam. Palm

2+05²¹ Nly. line Newell sec. at. 90°

1+75

1+53

1+51

1+30

1+05

110.27

23

102.37	106.27	106.27	107.57	108.67
$\frac{2.9}{50}$	$\frac{4.0}{50}$	$\frac{4.0}{50}$	$\frac{2.7}{50}$	$\frac{1.6}{50}$
102.07	105.37	105.57	107.57	108.57
$\frac{8.2}{30}$	$\frac{4.9}{50}$	$\frac{4.7}{30}$	$\frac{3.7}{10}$	$\frac{1.2}{10}$
101.87	105.47	105.57	106.57	108.57
$\frac{8.4}{18}$	$\frac{2.8}{9}$	$\frac{4.7}{9}$	$\frac{3.7}{10}$	$\frac{1.2}{10}$
101.37	104.07	104.27	105.77	107.47
$\frac{8.7}{8}$	$\frac{6.2}{5}$	$\frac{6.0}{5}$	$\frac{2.5}{7}$	$\frac{2.8}{7}$
100.67	104.07	104.17	105.77	107.67
$\frac{9.6}{5}$	$\frac{6.2}{5}$	$\frac{6.1}{5}$	$\frac{4.5}{7}$	$\frac{2.6}{7}$
100.87	104.07	104.17	105.77	107.67
$\frac{9.4}{5}$	$\frac{6.2}{5}$	$\frac{6.1}{5}$	$\frac{4.5}{7}$	$\frac{2.6}{7}$
101.17	103.07	104.37	105.67	107.57
$\frac{9.1}{15}$	$\frac{7.2}{12}$	$\frac{5.9}{9}$	$\frac{4.6}{15}$	$\frac{2.7}{10}$
101.67	102.67	103.97	105.27	108.17
$\frac{8.6}{30}$	$\frac{7.6}{21}$	$\frac{6.8}{20}$	$\frac{5.0}{18}$	$\frac{2.1}{21}$
101.27	102.77	104.17	105.97	108.67
$\frac{9.0}{50}$	$\frac{7.5}{30}$	$\frac{6.1}{30}$	$\frac{4.3}{25}$	$\frac{1.6}{30}$
		104.97	106.37	
		$\frac{5.3}{30}$	$\frac{3.7}{30}$	
		105.37		
		$\frac{4.7}{30}$		

110.27

3+56 Cont.

3+56 29⁷ Rt. = Start 6" wide Conc. wall

3+25

2+85

2+75³¹ = Sly. line Newell. Taken at 90°

2+40³¹ = Newell. taken at 90°

119.85

118 100	9.5 30	110.35	108.65	110.95	8.9 50
9.5 30	9.5 30	110.35	110.35	113.15	6.7 30
9.3 11	9.3 30	110.55	111.55	112.75	6.5 29
10.6 9	9.3 11	110.75	112.75	113.55	5.7 50
9.9	10.6 9	111.55	114.95	113.15	6.0 30
10.0 14	9.9	111.65	112.05	113.35	5.8
8.7 20	10.0 14	111.75	112.35	113.85	5.4 18
8.7 20	8.7 20	113.15	113.75	114.75	5.1 23
8.7 30	8.7 20	114.05	114.25	115.15	4.7 29E
	8.7 30	114.05	114.85	115.55	4.3 29.7
					Bottom of wall.
					Top of wall

119.85

4+91.5

4+88

(E.P. = edge of paving)

4+78 = start Cold lay paving

E.P. T.P. Property 9.31 124.26 4.90 114.95 Macaulay + Clove Cor. Men.

on taken along line of Macaulay.
4+75.68 brick topped Cono. wall. Sections From here = Nly. line Macaulay. 30.7 RT. = End

4+69 27² RT. = End row of 12" Diam Patms

4+54 30.4 RT. = start brick topped 4" wide ^{Cono. wall}

4+52 30.4 RT. = ^(5 steps) 4' wide cono. steps, to walk.

119.85

9.0 50	9.5 14 E.P.	9.6 13 E.P.	8.0 70	6.7	5.2 15	4.2 30	4.0 35 E.P.	115.26	116.76	116.66	116.26	117.56	119.06	119.96	120.26
	8.8 30	7.1 12	7.5 5 E.P.	6.5	5.1 15	4.1 30	3.7 32 E.P.	115.76	117.76	116.76	117.75	119.16	120.16	120.56	
	8.5 30	6.5 9 E.P.	7.4 6 E.P.	6.9	5.8 11	5.1 29 E.P.	4.7 30 E.P.	114.25	115.75	112.65	116.95	117.45	118.45	119.35	119.45
					124.26			118.25	118.15	118.15	117.95	118.05	118.79	119.35	120.35
5.6 50	4.1 30	2.2 8	2.9 5	2.4	1.4 12	0.5 30	0.4 30.6 Ord Bottom of wall	0.9 30.7 Top of wall	1.6 30.4 Ord	1.7 30.4 Bottom of wall	1.9 30.4 Bottom of wall	0.5 30.5 Top of wall	1.06 30.5 Top of wall	1.4 35 Top of walk	1.4 35 Top of walk
								118.25	118.15	118.15	117.95	118.05	118.79	119.35	120.35
								119.85							

Check Ely Prop. Mon.
Tustin & Macaulay
Page 21

3.11 145.56 OK

T.P. 12.59 148.67 0.19 136.08

T.P. 12.75 136.27 0.74 123.52

street proper. (starts on paving)

A+96 Nly. Edge paving along Macaulay

124.26

112.16	114.16	115.56	117.56	119.06	120.26	121.86
$\frac{12.1}{50}$	$\frac{10.1}{30}$	$\frac{8.7}{18}$	6.9	$\frac{5.2}{15}$	$\frac{4.0}{30}$	$\frac{1.9}{50}$

124.26

Wawona Drive

12-1-77

28

Capistrano to Wabaska
Sketch on Page 31

0+00 = S. Ely. Line Capistrano

INDEXED

0-11³⁸ = End curb on East

0-17.08 = 90° to Ely. Prop. Cor

Back up to ↗

Here on at 90° to Wawona.

Cross section sections from

0-11⁵ Cont. ← This section to
show curb grades
on Capistrano only.

taken along curb line Δ 60°-21'

0-11⁵ = Ely. Curb line Capistrano

10.83 94.11 0.38 83.28

11.76 83.66 — 71.70

N.Y. B.P.
Poc +
Capistrano

Indexed
J

84.31	86.91	86.91	85.41	86.01	85.91	85.41	85.71
9.8 50	7.2 34	7.2 30	8.7 24	8.1 15	8.2	8.7 10	8.4 30
85.91	86.41	83.93	84.51	84.51	84.51	84.91	85.81
8.2 30	7.7 24	10.18 20 End of.	9.6 20	9.6 11	7.6	9.2 15	8.3 30
84.17	83.94	83.91	84.31	84.21	84.91	85.81	
9.94 30 Back Cor. of Rd.	10.15 20 top of E.C.	10.2 20 Dtd	9.8 15	9.9	9.2 15	8.3 30	
77.22	76.26	80.64	79.66		88.71	89.62	92.43
16.89 75 top of	17.85 75 Curb	13.47 53 top of.	14.45 53 Curb		5.40 65 Curb	4.49 65 top of.	1.68 90 Curb
83.99	82.95	83.31	84.41	86.21	85.0	85.95	
10.12 28.2 E.C. top of.	11.16 28.2 Curb at Curb E.C.	10.8 28	2.7 and. 94.11.	1.7 40.3 Curb	9.11 40.3 Curb at at of E.C.	8.46 40.3 top of. E.C.	

Wawona Drive

0+65

0+30

T.A. on
Meter 607

8.21 99.52 2.80 91.31

0+24

0+17²⁸ = Prop. Cor. on Rt.

0+11³⁹ Cont

0+11³⁹ = End Ch. on Rt.

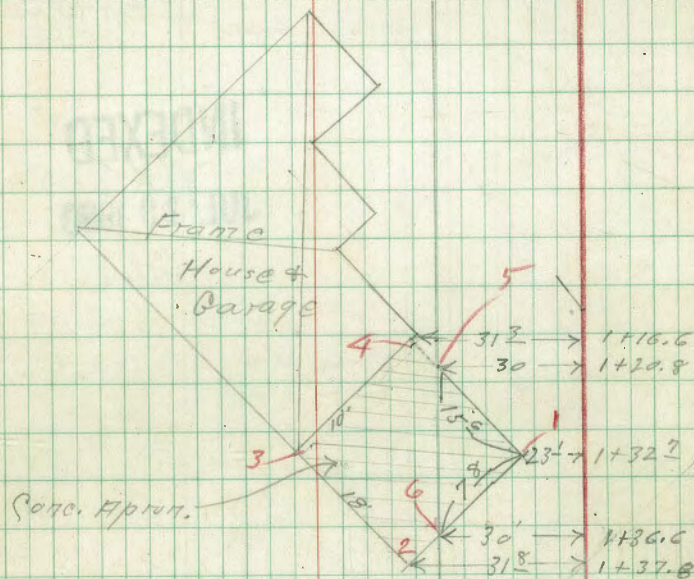
94.11

85.61	87.02	85.82	91.32	93.02	93.52	94.72	100.52
$\frac{86}{30}$	$\frac{17.5}{50}$	$\frac{13.7}{50}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	6.0	$\frac{9.8}{2}$	$\frac{7.0}{30}$
89.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.2}{34}$	$\frac{9.3}{30}$	$\frac{9.3}{30}$	8.7	$\frac{6.5}{12}$	99.52	$\frac{2.2}{4}$	$\frac{2.2}{4}$
88.11	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{6.0}{30}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
88.21	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{5.7}{24}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
89.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.9}{19}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
89.91	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.2}{2}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
90.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{9.3}{2}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
94.51	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{10.4}{24}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
91.71	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{2.4}{30}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
85.51	87.02	85.82	91.32	93.02	93.52	94.72	100.52
$\frac{8.5}{30}$	$\frac{17.5}{50}$	$\frac{13.7}{50}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	6.0	$\frac{9.8}{2}$	$\frac{7.0}{30}$
89.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.3}{33}$	$\frac{9.3}{30}$	$\frac{9.3}{30}$	8.7	$\frac{6.5}{12}$	99.52	$\frac{2.2}{4}$	$\frac{2.2}{4}$
88.21	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.9}{30}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
88.11	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{6.0}{22}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
88.91	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{5.2}{16}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
88.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{5.3}{2}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
90.51	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{3.6}{2}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
93.11	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{1.0}{20}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
89.21	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.9}{30}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
86.31	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{1.8}{30}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
86.11	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{9.0}{50}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
89.11	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{5.0}{34}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
88.11	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{6.0}{30}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
87.41	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{6.9}{33}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
87.91	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{6.2}{2}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
90.41	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{3.7}{2}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
89.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{4.3}{11}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
91.41	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{1.7}{14}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
88.81	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{5.3}{20}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
85.95	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{8.1}{20}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
86.31	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{8.1}{20}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$
85.95	85.82	90.22	91.32	93.02	93.52	94.72	100.52
$\frac{8.1}{20}$	$\frac{13.7}{50}$	$\frac{9.3}{30}$	$\frac{8.2}{30}$	$\frac{6.5}{15}$	8.7	$\frac{6.5}{12}$	$\frac{2.2}{4}$

94.11

End Cl.

Wawona
⊕



Sketch is upside down.

Elev. is 0.2 lower than conc. slab
shots by number. ground

102.46	102.85	102.73	102.56	102.55	102.77
$\frac{1.55}{1}$	$\frac{1.16}{2}$	$\frac{1.28}{3}$	$\frac{1.45}{4}$	$\frac{1.46}{5}$	$\frac{1.29}{6}$
74.62	85.62	92.22	94.12	95.92	96.42
$\frac{24.9}{100}$	$\frac{13.7}{60}$	$\frac{1.3}{30}$	$\frac{5.4}{18}$	$\frac{3.6}{13}$	$\frac{3.1}{3}$
104.91	97.82	101.42	101.92	102.02	
	$\frac{1.7}{3}$	$\frac{+0.9}{22}$	$\frac{+2.4}{30}$	$\frac{+2.5}{40}$	

T.P. 2x2
1146.67

Continued on p. 33
6.97 104.01 2148 97.04

11.00 10' Rte side of house

99.52

99.52

Alley BIK 8
Pt. Loma Hgts.

elephant 12-1-47

193.67 = Ely.
line elephant

N.O. 2500.1

Sommermejer
W. Meier
E. Sherman

INDEXED
MK
JUL 19 1950

notes checked
6-21-51
Dob



6+60.68

Wawona Dr.

31

Screw 1 1/2
Foot Tree

0+00.27
Nail
in power pole 12-1-47

Set #46
Disk
on 6-20-51

6+07.99

See Detail
Page 32

1002 x 5118

5125.29

see FB 2179
46

30

← 30 → 30 →

INDEXED

JUN 27 1951

1+46.69 = ex P.O.T.
on E. Alley produced.

1+72.40

1+55.14

out
9/16/54

17.26

138.06

160.11

0+17.08 = Ely. Cor

Ret. #1
page 32

0-17.08 = Ely Cor

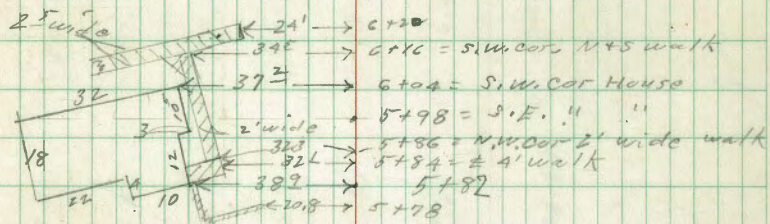
39

34.52

Return
#2
page 32

Ely line Capistrano

Capistrano



83.99	82.95	84.09	83.96	83.99
10.12	11.16	10.08	10.15	10.18
#1	#1	#2	#3	#4
Top of	Gutter	Top of	Top of	Top of
		Cl.	E.C.	End of Cl.

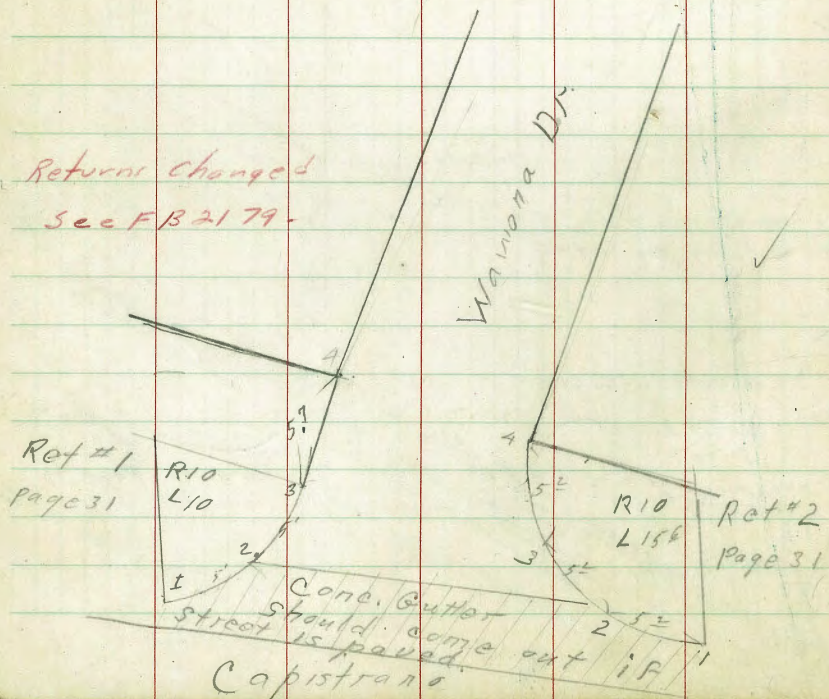
Ret. #1

85.95	85.00	85.95	85.91	85.95
8.16	9.11	8.16	8.12	8.16
#1	#1	#2	#3	#4
Top of	Gutter	Top of	Top of	Top of
		Cl.	Cl.	End of Cl.

Return #2

9A.11

Returns changed
See FB 2179.



2+00

1+72¹⁰ East line alley on Rt. at 90° ✓

28' Rt. = ctr. Pole 3584 ✓

1+55¹⁴ 90° to Alley (west line) on Rt. at 90°

1+50 start of bench

1+44

17 Lt. = Deadman

1+33 11.9 Lt. = ctr. Guy pole

1+16.6 3 1/2 Rt. = Cor. Main house ✓

104.01 Conti. from Page 30.

82.81	83.01	84.51	91.61	95.21	95.81	96.81	102.01
21.2 75	20.0 30	14.0 30	10.4 15	8.8 11	8.2	7.2 2	2.0 30
83.31	84.71	91.71	94.91	96.51	97.11	99.01	101.61
20.7 75	19.3 41	12.3 30	9.1 17	7.5 12	6.9	5.0 2	2.4 17
83.61	84.81	91.61	93.91	96.61	97.11	98.61	102.01
20.4 75	19.2 41	12.4 30	10.1 20	7.4 11	6.9	5.4 3	2.0 20
81.31	89.71	91.71	94.21	96.61	97.21	98.21	102.01
22.7 75	14.3 41	12.3 30	7.8 20	7.4 11	6.8	5.8 3	2.0 19
92.91	94.81	96.31	96.71	97.81	100.31	102.21	102.21
11.1 30	7.2 17	7.7 11	7.3	6.2 3	3.7 20	1.8 30	1.8 30
							87.11 house

104.01

3+37

14.2	92	9.3	7.1	4.7	4.1	3.2	1.8	+ 2.0
60	39	38	30	70		13	15	30
80.63	85.63	85.53	87.73	90.13	90.73	91.63	93.03	96.83

3+36

14.2	13.6	9.3	7.1	4.6	4.1	3.2	1.8	+ 2.0
60	39	38	30	70		13	15	30
80.63	81.23	85.53	87.73	90.23	90.73	91.63	93.03	96.83

3+26

14.3	14.3	10.0	7.5	4.7	4.2	3.3	2.0	+ 2.0
58	40	39	30	7		10	12	30
80.53	80.53	94.83	87.33	90.53	90.63	91.53	92.83	96.83

3+25

14.3	14.3	10.8	7.4	4.3	4.1	3.4	2.1	+ 2.0
58	39	29	28	9		9	12	30
80.53	80.53	84.03	87.43	90.53	90.73	91.43	92.73	96.83

3+20²

57² Lt. = S. Ely Cor. House
 31² Lt. = S. Wly Cor. House ✓

14.4	13.4	10.3	11.0
58	40	Floor	31
80.63	81.43	84.53	83.83

3+05

58¹ Lt. = N. Ely Cor. Frame house
 31² Lt. = N. Wly Cor. Frame house ✓

14.7	10.9
58	31.3
At N. Ely	At House
Cor. House	Cor.
80.13	83.93

9483

5+25

$\frac{21.8}{50}$	$\frac{19.2}{30}$	13.3	$\frac{9.1}{17}$	$\frac{7.9}{30}$
67.17	69.27	75.17	79.37	80.57

5+10

$\frac{16.4}{30}$	$\frac{14.1}{17}$	10.7	$\frac{7.5}{18}$	$\frac{3.3}{30}$
92.07	74.37	77.77	86.97	85.17

4+90

$\frac{13.8}{50}$	$\frac{12.0}{30}$	8.7	$\frac{4.5}{30}$	
74.67	76.47	79.77	83.97	
		88.47		

T.P. 6.52 88.47 12.88 81.95

4+40

$\frac{12.5}{30}$	8.8	$\frac{5.7}{30}$		
82.33	86.03	89.13		

3+90

$\frac{13.7}{50}$	$\frac{7.8}{30}$	$\frac{7.1}{20}$	5.2	$\frac{4.3}{8}$	$\frac{0.0}{25}$	$\frac{10.4}{30}$
81.13	85.03	87.73	89.63	90.53	94.83	95.23

3+50

$\frac{8.1}{30}$	$\frac{5.3}{12}$	4.5	$\frac{3.0}{8}$	$\frac{1.7}{20}$	$\frac{1.0}{30}$
86.73	89.53	90.33	91.83	93.13	95.83

94.83

94.83

5+86 = 32.3 Lt. N.W. Cor. 2' wide N.W. Sly. Conc. Walk

5+84 = 4' Conc. Walk 32' Lt.

5+82 38' Lt. = N.W. Cor House - See Page 32

5+81 22' Lt. = Ctr. P. pole # P 3460
sketch page 32

5+78 20' Lt. = 6" Conc. wall (running E-W)

5+70

5+55.29 See page 31

5+35

88.47

80.67	80.68	80.67	82.57	86.17
$\frac{71.8}{39}$	$\frac{71.9}{30}$	$\frac{71.8}{30}$	5.9	$\frac{2.3}{30}$
N.W. Cor Walk				
80.17	80.17	80.57	82.57	85.87
$\frac{71.8}{39}$	$\frac{81.31}{32.1}$	$\frac{71.9}{30}$	5.9	$\frac{2.6}{30}$
Floor Elv	2' Walk			
79.67	80.17	79.57		
$\frac{8.8}{30}$	$\frac{10.00}{30}$	$\frac{8.3}{30}$	$\frac{3.9}{20.8}$	
Top wall	Ord Wall	Top wall	Ord Wall	
30	Bottom wall	Bottom of wall		
	74.57	77.77	81.87	84.67
	$\frac{13.67}{30}$	$\frac{10.7}{30}$	6.0	$\frac{3.8}{30}$
		74.97	78.97	81.77
		$\frac{13.5}{30}$	9.5	$\frac{6.7}{30}$
				Prop. Cor.
	68.27	70.47	74.67	79.77
	$\frac{20.2}{30}$	$\frac{18.0}{30}$	13.8	$\frac{8.7}{30}$

88.47

Wawona Dr.

B.M. on M.H.
Oliphant + Clove Page 22

247

86.00

86.02

G+60⁸² 30' Lt. = Prop. Cor (Page 31)

G+40

244

G+20 = E-End 2^E wide conc. walk

G+19 30' Lt. = on E 2^E wide walk

G+16 34^E Lt. = S.W. Cor 2^E wide walk.

G+07⁹⁹ = Int. N.Ely line Oliphant.

88.47

81.77

$\frac{6.7}{30}$
prop. Cor.

77.77

$\frac{10.7}{50}$

80.87

$\frac{7.6}{30}$

83.07

$\frac{5.4}{12}$

84.87

3.6

87.07

$\frac{1.4}{12}$

88.47

$\frac{0.0}{24}$

91.47

$\frac{+3.0}{30}$

80.82

$\frac{7.65}{30}$

81.42

$\frac{7.05}{24}$

80.16

$\frac{8.31}{34.5}$

80.77

$\frac{7.7}{30}$

82.67

$\frac{5.8}{14}$

85.47

3.0

87.17

$\frac{1.3}{13}$

88.57

$\frac{+0.1}{30}$

80.87

$\frac{7.6}{30}$

82.37

$\frac{6.1}{13}$

84.57

3.9

87.67

$\frac{1.9}{18}$

88.27

$\frac{0.2}{30}$

Alley BIK 8, Pt. Loma Hgts

Sketch - Page 31

conc. floor - No apron

0+50^E 10² Rt. = start door double garage

T.P. 10.57 120.62 0.01 110.05

0+28^A 11³ Rt. = End same



floor no apron.

0+13[±] 11³ Rt. = start double garage doors conc.

0+04²⁷ = Wly line Wawona on Lt.

0+00 = Wly line Wawona

0-04²⁷ = Wly line Wawona on Rt.

2x1 T.R. Page 30

13.02 110.06 — 97.04

104.42	109.12	109.87	110.62	110.82	111.37
16.2 50	11.5 7.5	10.8 120.62	10.0 7.5	9.8 10.8	9.25 10.9 Base Floor
102.86	104.16	106.76	107.06	107.56	107.90
7.2 25	5.9 25	3.3 7.5	3.0	2.5 7.5	2.5 7.5
104.86	106.06	105.76	105.86	107.06	107.16
5.2 12	4.0 11	4.3 7.5	4.2	3.0 7.5	2.9 7.5 Ord
104.86	104.66	104.96	105.86	105.36	106.26
5.2 12	3.4 7.5	5.1	4.2 7.5	4.7 7.5	3.3 7.5
103.36	103.56				
6.7 7.5	6.5 7.5				
		110.06			

2.16
7.5
Flat
Gar.
floor.

1+1A³ 7² Rt. = End 4" wide Conc. wall

6.3
7.5

114.32

0+92 7² Rt. = start 4" wide Conc. Wall.

7.2
7.5

113.22

0+90 { 10³ Rt. = ± 4' wide Conc. walk
7² Rt. = ± 4' wide grant slab

7.6
7.5

113.02

0+86¹ 10⁷ Rt. = End Sing Gar. floor
Conc. floor No Apron

7.8
7.5

112.82

0+78¹ 10⁷ Rt. = start Sing Gar. door
Conc. floor - No Apron

8.3
7.5

112.32

0+72⁵ 7² Rt. = Back edge pole # PA. 1915
Conc. floor - No Apron

10.1
7.5

110.52

0+65⁵ 10² Rt. = End door double gar. door.

10.1
7.5

110.52

6.4

114.22

112.92

112.82

112.72

112.72

111.12

111.12

9.0
7.5

114.62

113.12

112.92

112.72

112.42

111.32

111.32

6.3
7.9

114.32

112.72

112.62

112.72

112.52

111.22

111.22

5.2
7.9

115.42

114.12

112.74

112.73

112.72

111.38

111.38

120.62

Base wall

Base d wall

± 2 Grant

10.6

10.6

10.8

Top of wall

Top of wall

± walk

Gar. Floor

Gar. Floor

Gar. Floor

Gar. Floor

Oliver St.

{Faruel to
Cresham

Cross Section

W.O. 31472

12-24-47

Sommermeier
W. Moore
E Sherman

INDEXED

Set. NW.B.P.
Faruel &
Oliver

4.74 21.02

B.M. #1

T.P. 6.77 25.76 2.33 18.77

T.P. 2.49 21.12 6.37 18.63

Doc. Beach Dr.
& Cresham

3.81 25.00

21.19

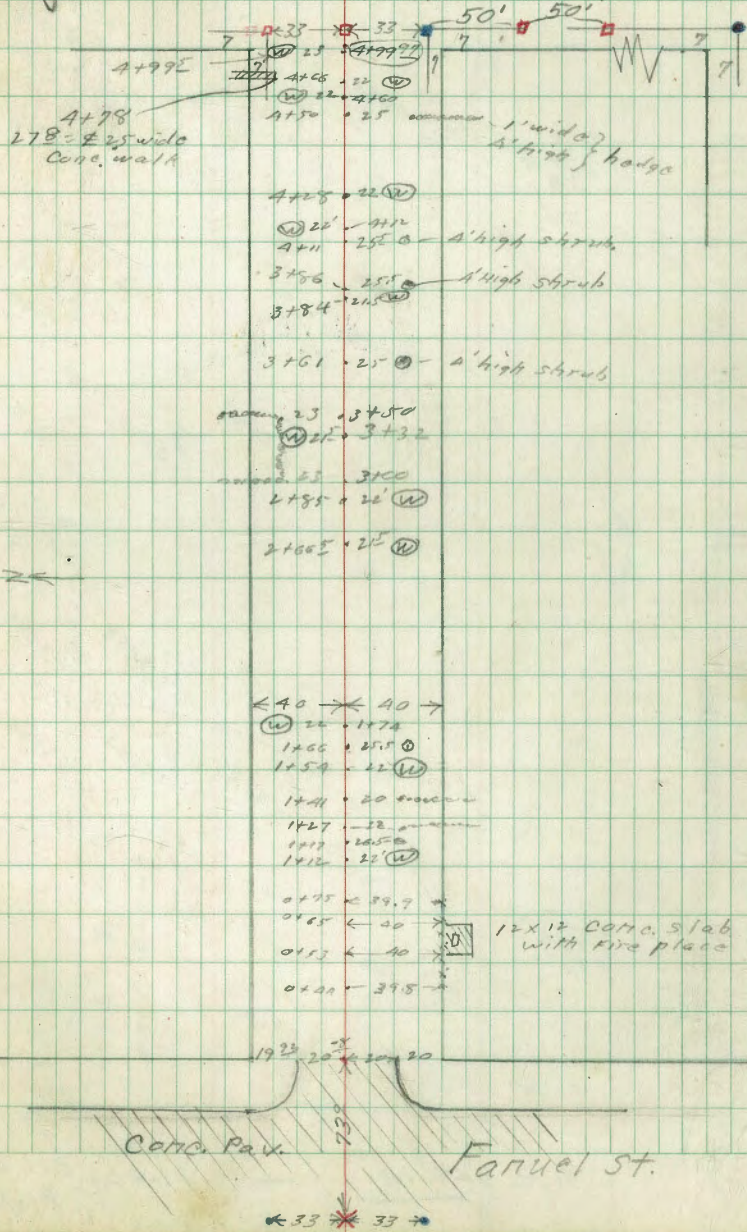
N.W.B.P.

Indexed

42

1/2 Set. 7/20/49

Cresham St.



Oliver Street Cross Sec.

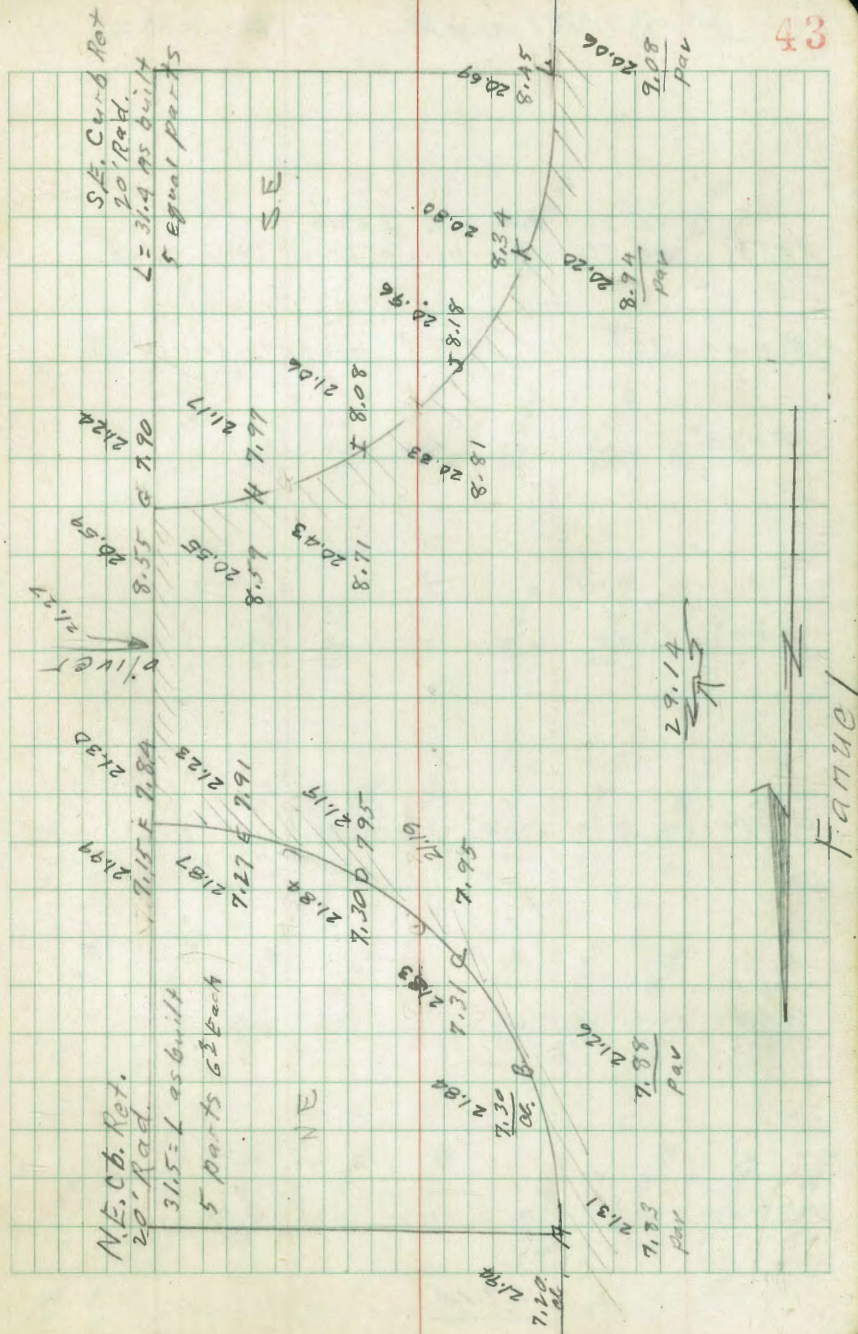
Fanuel to Gresham

8.12

29.14

— 21.02

B.M. #1
P-42



Oliver

0+53 50' Rt. = S.W. Cor. same
40" Rt. = N.W. Cor. 4" Thick Conc. Slab

0+44 39' Rt. = start picket fence.

0+30

0+03

0+00 = Ely line Fannell

0+20 Cont.

0-20 = Ely. Curb line Fannell

29.1A

Lt = North

±

Rt. = South

44

$$\begin{array}{r} 6.11 \\ 40 \\ \hline 23.03 \end{array}$$

$$\begin{array}{r} 6.16 \\ 52 \\ \hline 22.98 \end{array}$$

$$\begin{array}{r} 5.20 \\ 40 \\ \hline 24.1 \end{array}$$

$$\begin{array}{r} 7.23 \\ 19 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 6.7 \\ 15 \\ \hline 22.4 \end{array}$$

$$6.6$$

$$\begin{array}{r} 22.1 \\ 16 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 6.7 \\ 40 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 5.9 \\ 10 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 6.5 \\ 22 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 7.6 \\ 18 \\ \hline 21.5 \end{array}$$

$$7.6$$

$$\begin{array}{r} 20.9 \\ 18 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 7.7 \\ 20 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 22.5 \\ 6.6 \\ 40 \\ \hline \text{Dirt} \end{array}$$

$$\begin{array}{r} 21.99 \\ 7.5 \\ 20.08 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 21.30 \\ 7.84 \\ 20.09 \\ \hline \text{Pav.} \end{array}$$

$$\begin{array}{r} 21.36 \\ 7.78 \\ 10 \\ \hline \text{Pav.} \end{array}$$

$$21.27$$

$$\begin{array}{r} 21.06 \\ 8.58 \\ 10 \\ \hline \text{Pav.} \end{array}$$

$$\begin{array}{r} 20.59 \\ 8.55 \\ 20 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 21.24 \\ 7.90 \\ 20 \\ \hline \text{Dirt} \end{array}$$

$$21.0$$

$$\begin{array}{r} 22.84 \\ 6.30 \\ 100 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 22.26 \\ 6.88 \\ 100 \\ \hline \text{Pav.} \end{array}$$

$$\begin{array}{r} 22.08 \\ 7.00 \\ 100 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 21.46 \\ 7.68 \\ 50 \\ \hline \text{Pav.} \end{array}$$

$$19.88$$

$$\begin{array}{r} 20.49 \\ 9.26 \\ 50 \\ \hline \text{Pav.} \end{array}$$

$$\begin{array}{r} 18.59 \\ 10.25 \\ 100 \\ \hline \text{Pav.} \end{array}$$

$$\begin{array}{r} 9.58 \\ 7.56 \\ 100 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 21.31 \\ 7.83 \\ 40 \\ \hline \text{Pav.} \end{array}$$

$$\begin{array}{r} 21.94 \\ 7.20 \\ 40 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 21.14 \\ 8.00 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 20.99 \\ 8.15 \\ 10 \\ \hline \end{array}$$

$$20.75$$

$$\begin{array}{r} 20.61 \\ 8.53 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 20.42 \\ 8.72 \\ 20 \\ \hline \end{array}$$

$$\begin{array}{r} 20.69 \\ 8.45 \\ 40 \\ \hline \text{Cl.} \end{array}$$

$$\begin{array}{r} 20.06 \\ 9.28 \\ 40 \\ \hline \text{Pav.} \end{array}$$

Cl. F.C. Cl. F.C.

oliver

- 1+27 22' Rt. = E N+S 1' High hedge
- 1+17 26⁵ Rt. = Ctr. 2" Diam Tree.
- 1+12 22' Rt. = E Water Meter Box.

1+00

0+89⁵ 40² Rt. = E East ribbon to Sing. Car Gar.

Sing. car. garage.

0+84⁵ 40.9 Rt. = E 2' wide west ribbon to

0+75 39⁸ Rt. = End picket fence.

54' Rt. = S.E. cor. same
 0+65 40' Rt. = N.E. cor. 4" thick conc. slab

29.14

45

$\frac{24.7}{4.4}$	$\frac{24.4}{4.7}$	$\frac{23.4}{5.7}$	$\frac{23.6}{5.5}$	$\frac{23.0}{6.1}$	$\frac{22.5}{5.6}$	$\frac{23.4}{5.7}$
$\frac{4.4}{40}$	$\frac{4.7}{20}$	$\frac{5.7}{18}$		$\frac{6.1}{18}$	$\frac{5.6}{21}$	$\frac{5.7}{40}$

$\frac{23.38}{5.76}$	$\frac{23.07}{6.07}$
$\frac{40.9}{57.4}$	$\frac{65}{65}$
End of Ribbon	on ribbon

$\frac{23.34}{5.80}$	$\frac{22.56}{6.18}$
$\frac{40.9}{57.4}$	$\frac{65}{65}$
End Ribbon	on ribbon

$\frac{24.7}{4.4}$	$\frac{24.2}{4.9}$	$\frac{23.0}{6.1}$	$\frac{23.2}{5.9}$	$\frac{22.5}{6.9}$	$\frac{23.0}{6.1}$	$\frac{23.1}{5.6}$
$\frac{4.4}{40}$	$\frac{4.9}{21}$	$\frac{6.1}{15}$	$\frac{5.9}{15}$	$\frac{6.9}{15}$	$\frac{6.1}{21}$	$\frac{5.6}{40}$

$\frac{22.98}{6.16}$	$\frac{22.95}{6.19}$
$\frac{40}{40}$	$\frac{52}{52}$

29.14

1+88^E = 40' Lt. = ^{Conc.} West Ribbon to Sing Garage

26.11
3.03
55
Ribbon

25.94
3.24
48
Ribbon

1+85

25.7
3.4
40

25.6
3.5
23

25.2
3.9
15

25.7
3.4

25.1
4.0
17

25.7
3.4
18

25.1
4.0
40

1+75

25.6
3.5
40

25.6
3.5
23

24.9
4.2
15

25.4
3.7

24.9
4.2
15

25.1
4.0
20

24.9
4.2
40

1+74 22' Lt. = Ctr. water meter box.

1+66 25^E Rt. = Ctr. 4" Diam tree

1+54 22' Rt. = Ctr. Water Meter box

1+50

25.8
3.8
40

24.9
4.2
24

24.5
4.6
20

24.8
4.3

24.2
4.9
16

24.5
4.6
20

24.5
4.6
40

1+41 20' Rt. = ± 1' High N.+S. Hedge.

Ribbon to Sing Gar.

1+36 = 40^E Rt. = ± Comb 3' wide conc. walk + East

24.21
4.93
55
Start Ribbon

24.18
4.96
55
Ribbon

1+30^E 40^E Rt. = ^{2' wide} West Ribbon to Sing Gar

24.08
5.06
40.8
Start Ribbon

24.12
5.02
55
Ribbon

Oliver

T.P. 4.99 31.86 2.27 26.87

± 1' High N.E.S. Hedge.

3+00 23' Lt. = start 1' High hedge also =

2+85 22' Rt. = ctr. water meter box

2+75

2+65 21' Rt. = ctr. water meter box

2+34 40' Rt. = End conc. drive

2+27 40' Rt. = start conc. drive

2+25

1+93 40' Lt. = East conc. ribbon to Sing Apr

29.14

4

47

$\frac{1.2}{40} \begin{matrix} 27.9 \\ - \end{matrix}$

$\frac{1.3}{20} \begin{matrix} 27.8 \\ - \end{matrix}$

$\frac{1.9}{16} \begin{matrix} 27.2 \\ - \end{matrix}$

$\frac{1.9}{15} \begin{matrix} 26.9 \\ - \end{matrix}$

$\frac{2.2}{20} \begin{matrix} 27.1 \\ - \end{matrix}$

$\frac{2.2}{40} \begin{matrix} 26.9 \\ - \end{matrix}$

$\frac{1.5}{40} \begin{matrix} 27.6 \\ - \end{matrix}$

$\frac{1.6}{20} \begin{matrix} 27.5 \\ - \end{matrix}$

$\frac{2.2}{16} \begin{matrix} 26.9 \\ - \end{matrix}$

$\frac{1.8}{14} \begin{matrix} 26.6 \\ - \end{matrix}$

$\frac{2.2}{20} \begin{matrix} 26.9 \\ - \end{matrix}$

$\frac{2.2}{40} \begin{matrix} 26.7 \\ - \end{matrix}$

$\frac{3.00}{40.7} \begin{matrix} 26.14 \\ - \end{matrix}$

$\frac{3.15}{70} \begin{matrix} 25.99 \\ - \end{matrix}$
on drive

$\frac{3.02}{40.7} \begin{matrix} 26.12 \\ - \end{matrix}$

$\frac{3.24}{70} \begin{matrix} 25.99 \\ - \end{matrix}$
on drive

$\frac{2.1}{50} \begin{matrix} 26.0 \\ - \end{matrix}$

$\frac{2.4}{40} \begin{matrix} 26.7 \\ - \end{matrix}$

$\frac{2.2}{20} \begin{matrix} 26.9 \\ - \end{matrix}$

$\frac{3.1}{17} \begin{matrix} 26.0 \\ - \end{matrix}$

$\frac{2.5}{14} \begin{matrix} 26.6 \\ - \end{matrix}$

$\frac{3.1}{14} \begin{matrix} 26.0 \\ - \end{matrix}$

$\frac{2.9}{20} \begin{matrix} 26.2 \\ - \end{matrix}$

$\frac{3.4}{40} \begin{matrix} 25.7 \\ - \end{matrix}$

$\frac{3.06}{55} \begin{matrix} 26.08 \\ - \end{matrix}$
on ribbon

$\frac{3.17}{40} \begin{matrix} 25.95 \\ - \end{matrix}$
Ribbon

29.14

Oliver.

3+45 40¹ Rt = End 15' wide conc. drive

3+32 21⁵ Lt = Ctr. Water-Meter box

3+30 40¹ Rt = start 15' wide conc. drive

3+28 40¹ Lt = 3' wide conc. walk.

(on ribbon) single Gar.

3+12 = 4 East. 2' wide conc. ribbon to

shots on ribbon walk 4

3+09 40² Rt = 4' wide conc. walk.

shots on ribbon

west

3+07 40¹ Lt = 12' wide conc. ribbon to Sing. Gar.

31.86

Lt.

Rt.

Rt.

48

21.09
4.77
40.1

26.70
5.16
60

21.06
4.80
40.1

26.66
5.20
60

28.78
3.09
50

28.46
3.40
40

28.43
3.43
50

28.30
3.56
40

26.85
5.01
40.2

28.74
5.12
50

28.33
3.53
50

28.26
3.60
40

31.86

Oliver St.

to single Bar.

4+43 40' Rt. = Φ East, 2' wide conc. ribbon

single Bar

4+38 40' Rt. = Φ West 2' wide conc. ribbon to

4+28 20' Rt. = Ctr. water meter box

4+27 40' Lt. = Φ 2' wide Conc walk.

4+21 40' Rt. = Φ 3' wide Conc. walk

4+12 Lt. = water meter box.

4+11 25' Rt. = 3' High Hibiscus

4+00

3+86 25' Rt. = Ctr. 5' high shrub

3+84 21' Rt. = Ctr. Meter box

3+72 40' Rt. = Φ 3' wide Conc. walk.

3+61 25' Rt. = 4' High shrub

= Φ 1' high N.t.S. hedge

3+50 23' Lt. = End 1' High hedge also

3186

Lt.

Φ

Rt.

49

26.24
5.82
40.7

26.42
5.44
55

26.38
5.48
40.7

26.46
5.40
55

28.36
3.50
50

28.01
3.85
70

26.75
5.11
40.6

26.84
5.02
50

28.1
3.8
40

27.8
4.1
21

27.0
4.9
18

27.5
4.4

26.7
5.2
16

27.1
4.8
20

26.7
5.2
40

27.04
4.82
40

26.76
5.10
55

28.6
3.3
40

28.0
3.9
70

27.4
4.5
16

27.7
4.2

27.0
4.9
16

27.2
4.7
21

26.9
5.0
40

Oliver

5+19²² W. ch line Gresham

4+99²² (Chained meas.) = W.L. Gresham

4+99²² = 22⁹ Rt. = £ N+S picket fence

4+99²² 23 Lt = Ctr. water meter box

4+99 24² Lt = £ N+S. picket fence

4+79 40² Rt. = £ 3 wide Conc. walk.

4+78 27² Lt. = £ 2² wide Conc. walk

4+66 22 Rt. = Ctr. water meter box

4+60 22 Lt. = Ctr. water meter box

4+50 25 Rt. = £ 1' wide N+S Hedge

31.86

Lt.

£

Rt.

00

$\frac{27.2}{40}$	$\frac{26.9}{23}$	$\frac{26.2}{18}$	5.8	$\frac{25.5}{17}$	$\frac{25.9}{25}$	$\frac{24.0}{40}$
-------------------	-------------------	-------------------	-----	-------------------	-------------------	-------------------

$\frac{27.6}{40}$	$\frac{27.3}{25}$	$\frac{26.5}{18}$	5.4	$\frac{26.0}{16}$	$\frac{26.4}{19}$	$\frac{26.3}{40}$
-------------------	-------------------	-------------------	-----	-------------------	-------------------	-------------------

$\frac{26.27}{40.6}$	$\frac{26.22}{50}$
----------------------	--------------------

$\frac{28.14}{50}$	$\frac{27.85}{40}$	$\frac{27.62}{27.8}$
--------------------	--------------------	----------------------

$\frac{28.0}{40}$	$\frac{27.8}{23}$	$\frac{26.6}{17}$	4.9	$\frac{26.4}{17}$	$\frac{26.7}{21}$	$\frac{26.3}{40}$
-------------------	-------------------	-------------------	-----	-------------------	-------------------	-------------------

31.86

Oliver

£ 277. Road
+ Ingraham

7.69 44.20

shown as
(44.15)

T.P. 6.23 53.87 6.53 46.96

T.P. 9.39 53.47 0.38 44.10

T.P. 12.23 44.48 0.31 ~~0.7~~
32.25

T.P. 5.75 32.56 2.13 26.81

N.W.B.P.
Graham &
Pat. B. Drive

7.74 28.94 7.74 21.20

orig. B.M.
2119

T.P. 2.13 28.94 5.05 26.81

Graham

5+43 = £ Road as traveled 07

5+31 = Gutter as graded on Graham

5+28

31.86

61

$$\begin{array}{r} 27.4 \\ 4.5 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 26.5 \\ 5.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 25.8 \\ 6.1 \\ \hline \end{array}$$

$$\begin{array}{r} 25.0 \\ 6.9 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 24.5 \\ 7.4 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 27.2 \\ 4.7 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 26.3 \\ 5.6 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 25.6 \\ 6.3 \\ \hline \end{array}$$

$$\begin{array}{r} 24.8 \\ 7.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 24.2 \\ 7.7 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 27.0 \\ 4.9 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 26.8 \\ 5.1 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 25.7 \\ 6.2 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 25.5 \\ 6.4 \\ \hline \end{array}$$

$$\begin{array}{r} 25.3 \\ 6.6 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 25.2 \\ 6.7 \\ \hline 40 \end{array}$$

31.86

Oliphant { Capistrano }
 To Tustin }

Additional notes to show new Const.
 Sommermeier 7-1A-50
 Begg
 Shepard. N.O. 25020

Ground contour has not been changed enough to affect grade.
Original notes (P-6) are o.k.
 These notes show additional construction on property on Oliphant. Capistrano to Tustin

0+50 37⁴ Lt. = end house, under Const.

0+40 37⁴ Lt. = start house under const.
 35² Lt. = end Conc slab porch

B.F. = base of footing

0+26 34¹ Rt. = start house + Conc. Porch.

0+19⁵ 35² Lt. = start Conc. slab porch

6.48 127.48 - 121.00 BM #2
 Page 9

Lt.

±

Rt.

52

INDEXED
 JUL 19 1950

122.03	121.8
5.45	5.7
35 ²	35
Porch	

124.9	125.5	126.15
2.6	2.0	1.33
34	34 ¹	34 ¹
Orl.	B.F.	porch

121.99	121.7
5.49	5.8
35 ²	35
Porch	Orl

127.48

Oliphant

To house

2+30 40' Rt. = \pm 3' wide Conc. steps

2+20 34² Rt. = End Conc. porch

34² Rt. = start Conc. porch

2+10 30² Rt. = end conc wall

2+03 30² Rt. = start 6" wide Conc. wall

T.P. 0.94 6.48 121.00
Floor level
Conc floor - No apron

0+98 34² Rt. = \pm 20' wide double Gar.

0+88 34² Rt. = \pm 6' wide Conc walk

0+85 34² Rt. = end house + Conc. Porch

Conc. Floor level - No apron

0+60 44' Lt. = \pm 20' wide double Gar.

Lt.

\pm

Rt.

53

112.9	113.42			
9.5	8.52			
40 Grd	40 Top of bottom step			
114.1	113.7	117.85		
7.8	8.2	4.39		
34 Grd	34 ² B.F	34 ² Porch		
116.3	116.1	117.72	115.94	117.57
5.6	5.8	4.22	6.0	4.37
30 Grd	30 ² B.F	30 ² Top	34 ² B.F	34 ² Porch
116.3	116.4	117.79		
5.1	5.5	4.15		
30 Grd	30 B.F	30 ² Top		
<u>121.94</u>				
			126.57	
			0.91	
			34 ²	
			Gar. Floor	
125.8	126.13			
1.7	1.35			
34 Grd	34 ² walk			
125.8	125.4	126.19		
1.7	2.1	1.29		
34 Grd.	34 ² B.F.	34 ² porch		
127.1				
5.4				
44				
Approx Gar. floor under Const. shot on form				
			127.48	

TUSTIN SEE PAGE - 16

Oliphant to Macaulay St.
Additional notes to show
improvements in property since
previous X-sec. in 1947.

Original notes start on
page 16 - sketch on page 4

No change in ground
contour large enough to affect
grade. Orig. notes o.k.

These notes show elevations
& locations of construction since
1947. 0+00 = Sly line Oliphant.

1+75 4' Lt. = \pm 4' wide Conc. steps to porch

1+55 31' Lt. \pm 6" wide Ext. W. Conc. Ret. wall

T.P. 12.67 ~~125.07~~ 0.64 112.40

1+35 59' Lt. = \pm house

BM#3 10.79 113.04 — 102.25
Page #10

54

Reduced
H.T. Lane

120.1	118.4	117.8
5.0	6.7	7.3
45	42	42
on porch	1st step	0+00

116.2	112.1	114.9
8.9	13.0	10.7
31	31	31
Top	End	End to
Wall	to North	South
	of wall	of wall

125.07

107.7	107.7
5.3	5.3
59	59
Approx	End

113.04

Tustin

2+76 30' Lt. = ϕ 6" wide Conc. Ret. wall

130.25	131.2	131.6
<u>5.3</u>	<u>2.8</u>	<u>3.5</u>
30.5	30.5	30.5
End on North	End on South	Top of wall

2+63 30' Lt. = ϕ 2' wide Conc. walk

128.5	130.0
<u>7.2</u>	<u>6.10</u>
49	30
At house	walk

2+35 30' Lt. = ϕ 6" wide Conc. Ret. wall

126.4	128.0	128.2
<u>9.7</u>	<u>8.0</u>	<u>7.9</u>
30	30	30
End on North	End on South	Top

2+20 29' = ϕ 3' wide Conc. walk

125.0	124.4	124.6
<u>11.0</u>	<u>11.83</u>	<u>11.45</u>
49	49	29
Approx Floor level	at house	walk

T.P. 12.06 136.05 1.08 123.99

136.05

1+96 29' Lt. = ϕ 8" Conc. Ret. wall

122.6	120.1	124.9
<u>2.5</u>	<u>4.5</u>	<u>1.1</u>
30	30	29.6
End to South of wall	End to North of wall	Top wall

125.07

Reduced
B. & C.
6/28/51

55

(P. 21)
 Tustin + Macarita
 check Ely. Prop. Mon. 8.79 145.58 145.56

4+20 29' Rt. = 2' wide Conc. walk

T.P. 7.86 154.37 1.36 146.51

3+55 29' Rt. = 4' wide Conc. walk

22' Lt. = 1' wide Conc. walk

8" high curb on sly side
 of walk

3+41 23' Lt. = 3' wide Conc. walk

3+16 30' Lt. = 8" wide Conc. Ret. wall

T.P. 11.97 147.87 0.15 135.90

2+95 30' Lt. = 3' wide Conc. walk.

151.5
 2.90
 45
 on walk

151.21
 3.16
 30
 walk

151.2
 3.18
 29
 walk

154.37

139.3
 8.53
 46
 End of
 walk

140.4
 7.26
 30
 walk

141.0
 6.82
 22.5
 walk

146.85
 1.02
 29.9
 walk

142.6
 0.31
 48
 at house

139.0
 8.88
 46
 at house

139.7
 8.20
 30
 walk

140.0
 7.91
 23.2
 walk

137.1
 10.8
 30
 Ord. on
 south

137.6
 12.3
 30
 Ord. on
 north

137.21
 10.6
 30
 top

124.12
 1.93
 42
 At house

134.50
 1.55
 30
 walk

147.87

136.05

Additional Notes 11-June '51

N.O. 25020

Tustin-Oliphant to Macaulay

Sommermayor
Bagg
Shepard
Htman

orig. notes - p-16.

with direct elevation rod

Plotted
by RIDEMASS
6-14-51

floor no apron

0+05 45' Lt. = \pm double Gar. Conc.

0+96 25' Lt. = \pm 3' wide E+W. Conc. walk

0+78 24' Lt. = \pm 6" E+W. Conc. wall

0+58 26' Lt. = \pm 3' wide E+W. Conc. walk

0+41 26' Lt. = \pm 8" E+W. Conc. wall.

0+15 44' Lt. = bottom of ^{to porch} Conc. steps

B.M. = M.H. Ring
2+85⁰⁹ P.11

102.25

INDEXED

JUN 21 1951

145.93
45
Conc. floor

108.49 108.79 108.92
45 30 25'

107.9 104.3 107.9 104.3
30 30 24' 24'
Base Top Base

104.75 104.85 104.88
45 30 26'

105.2 101.0 105.2 101.0
30 30 26 26
top base top Base

103.20 101.8
on porch 44'
bottom of steps

L47. 779. + Road. = 44.15

A+05-45 Lt. - Car

27
31
58

72
27
45



DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on-1 see inside of front cover.

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