

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

| H | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | H |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0 | 8.0 | 8.1 | 8.2 | 8.3 | 8.4 | 8.5 | 8.6 | 8.7 | 8.8 | 8.9 | 0 |
| 1 | 9.0 | 9.1 | 9.2 | 9.3 | 9.4 | 9.5 | 9.6 | 9.7 | 9.8 | 9.9 | 1 |
| 2 | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 2 |
| 3 | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 3 |
| 4 | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 4 |
| 5 | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 5 |
| 6 | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 6 |
| 7 | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 7 |
| 8 | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 8 |
| 9 | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 9 |
| 10 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 10 |
| 11 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 11 |
| 12 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 12 |
| 13 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 13 |
| 14 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 14 |
| 15 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 15 |
| 16 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 16 |
| 17 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 17 |
| 18 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 18 |
| 19 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 19 |
| 20 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 20 |
| 21 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 21 |
| 22 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 22 |
| 23 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 23 |
| 24 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 24 |
| 25 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 25 |
| 26 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 26 |
| 27 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 27 |
| 28 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 28 |
| 29 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 29 |
| 30 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 30 |
| 31 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 31 |
| 32 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 32 |
| 33 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 33 |
| 34 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 34 |
| 35 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 35 |
| 36 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 36 |
| 37 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 37 |
| 38 | 46.0 | 46.1 | 46.2 | 46.3 | 46.4 | 46.5 | 46.6 | 46.7 | 46.8 | 46.9 | 38 |
| 39 | 47.0 | 47.1 | 47.2 | 47.3 | 47.4 | 47.5 | 47.6 | 47.7 | 47.8 | 47.9 | 39 |
| 40 | 48.0 | 48.1 | 48.2 | 48.3 | 48.4 | 48.5 | 48.6 | 48.7 | 48.8 | 48.9 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.
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1807

INDEXED

Completely

(except page # 80)

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

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 " " Nashville " " "

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c.s.k.

1

X-Section Chalcedony - Gresham to

Lamont

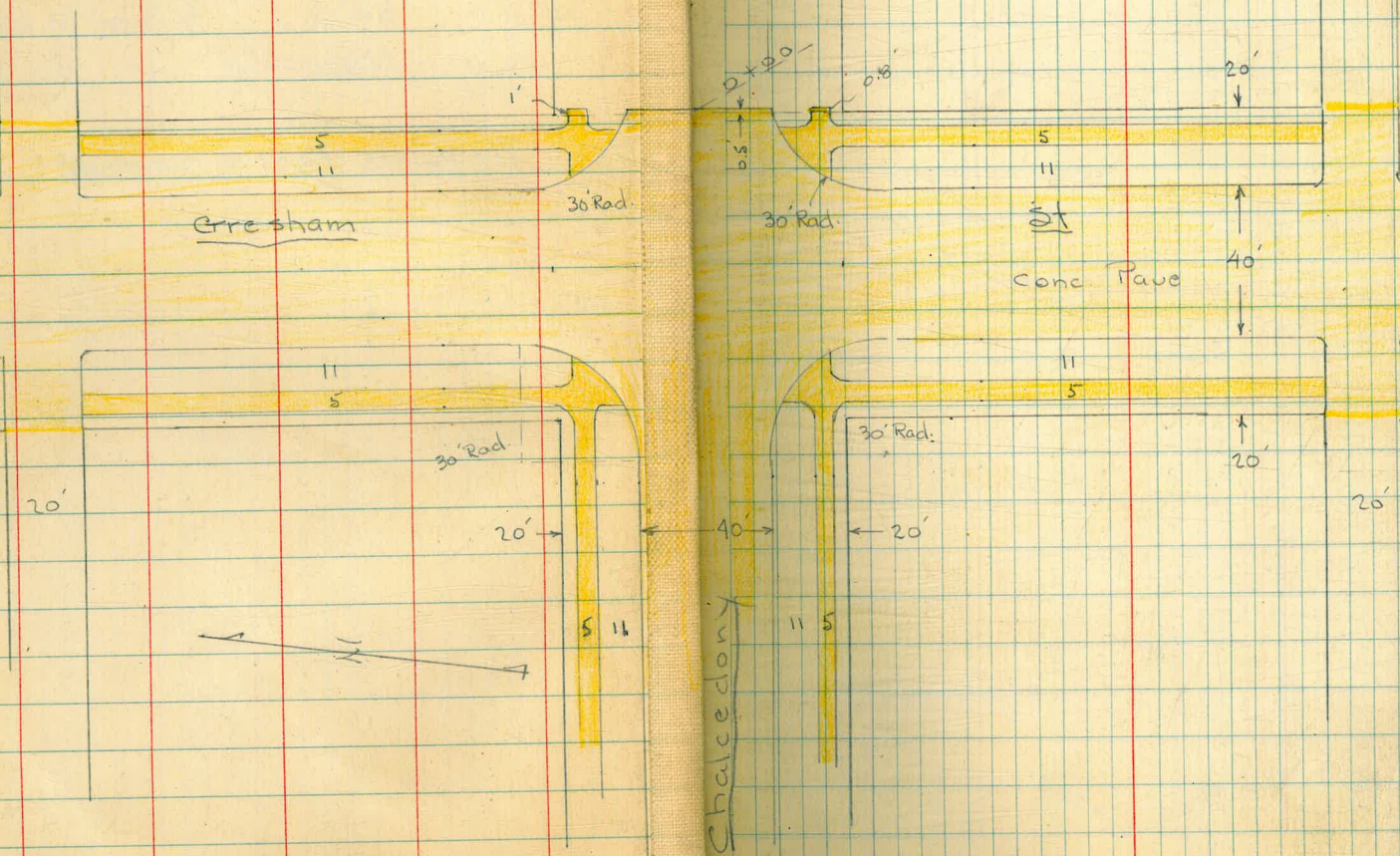
10-23-47

1846

Osborne
Hardin
Smith
Warrell

W.O. 31371

INDEXED



Haines

st

Ingraham

st

Mon.

~~4+99.94~~

7'
or

~~9+00~~

Grresham

st

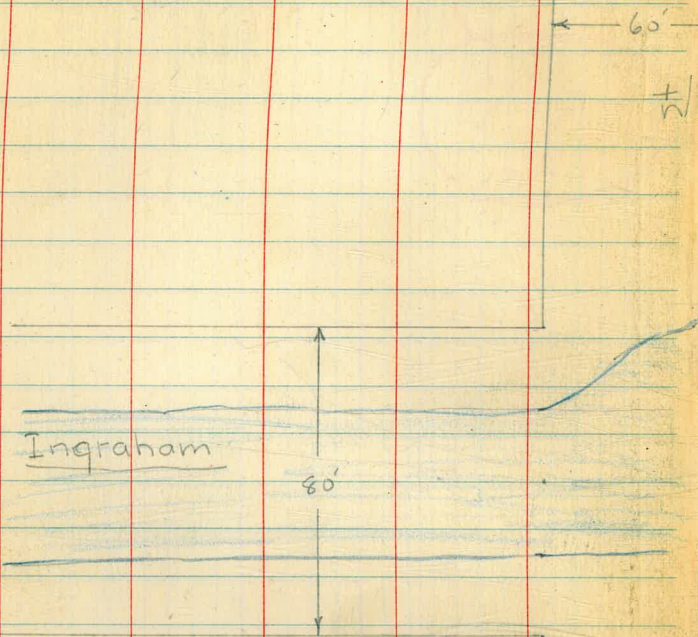
~~4+98.60~~



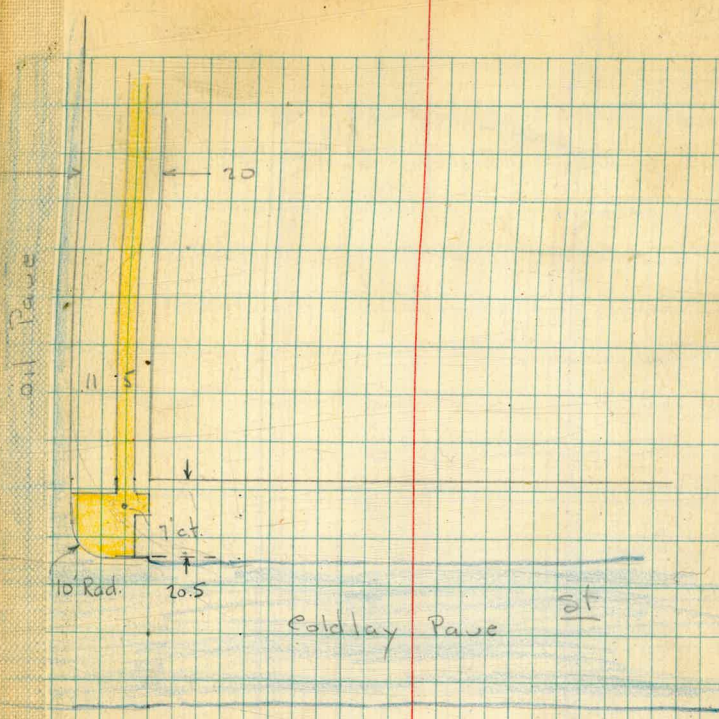
~~0+00~~

Haines

st

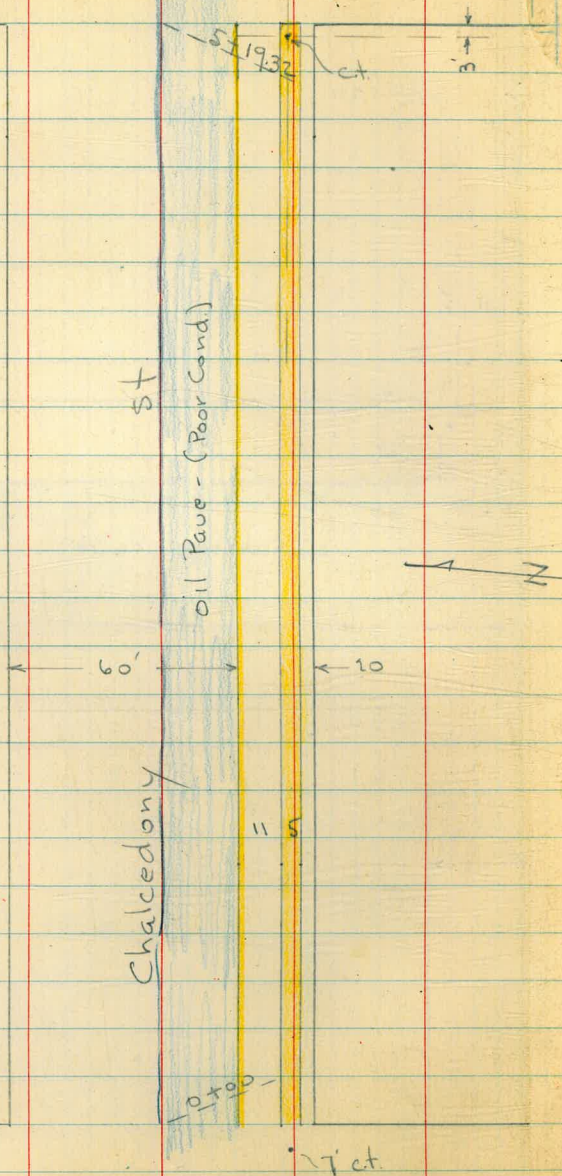


Chalcedony



Jewell

st



st

Oil Pipe - (Poor Cond.)

6'

10'

Chalcedony

5'

0700

7' ct



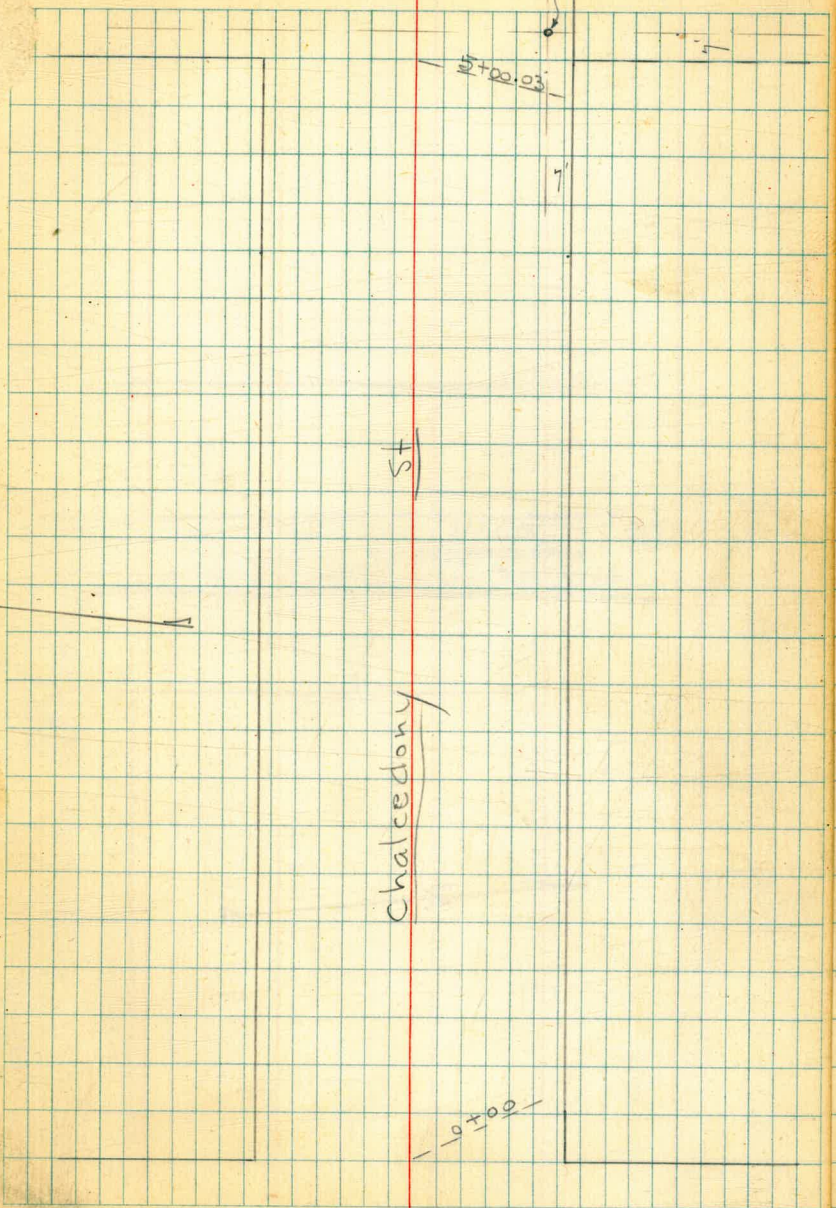
Ingraham

st

Kendall

st

4



st

Chalcedony

0700

Jewell

st

Jewell

st

st 100

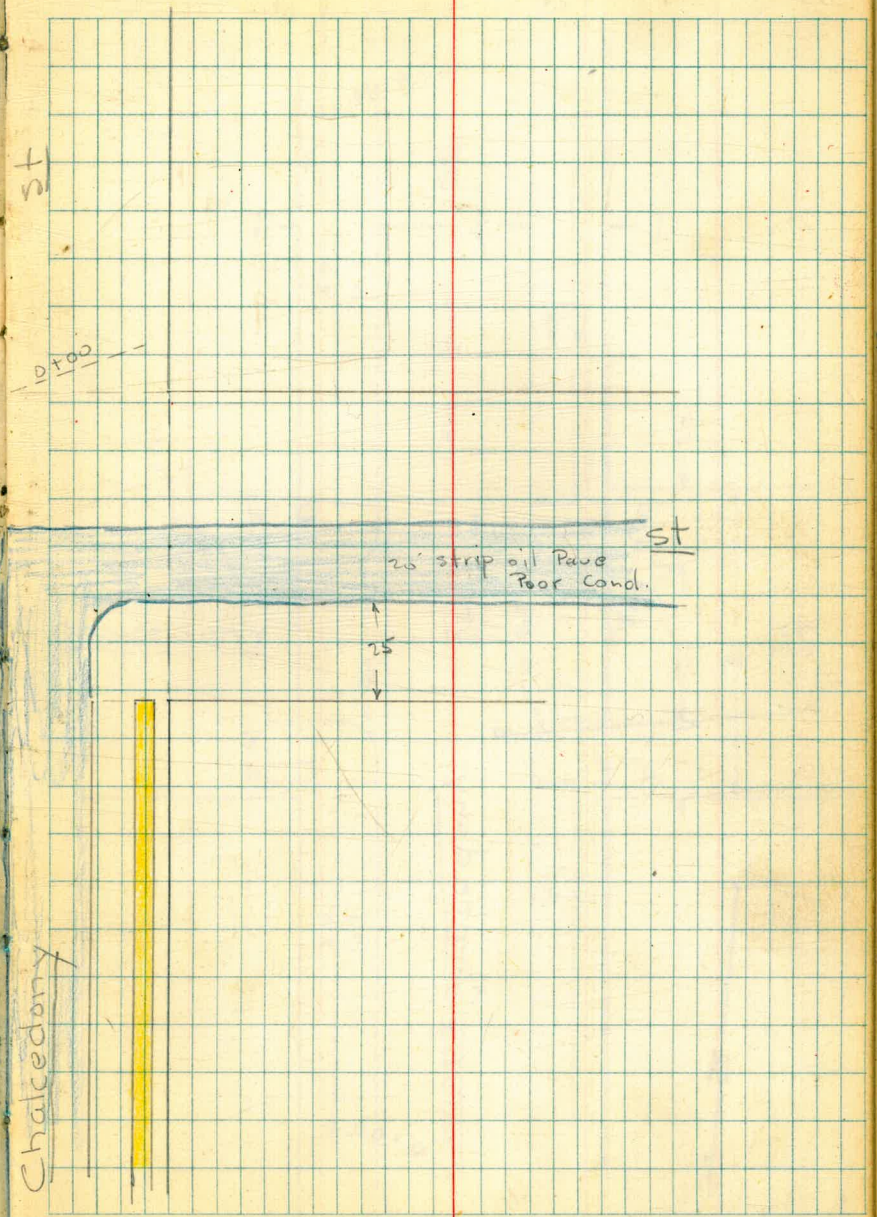
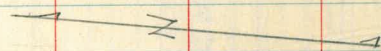
st 19.32

st

20' strip oil Pave
Poor Cond.

25

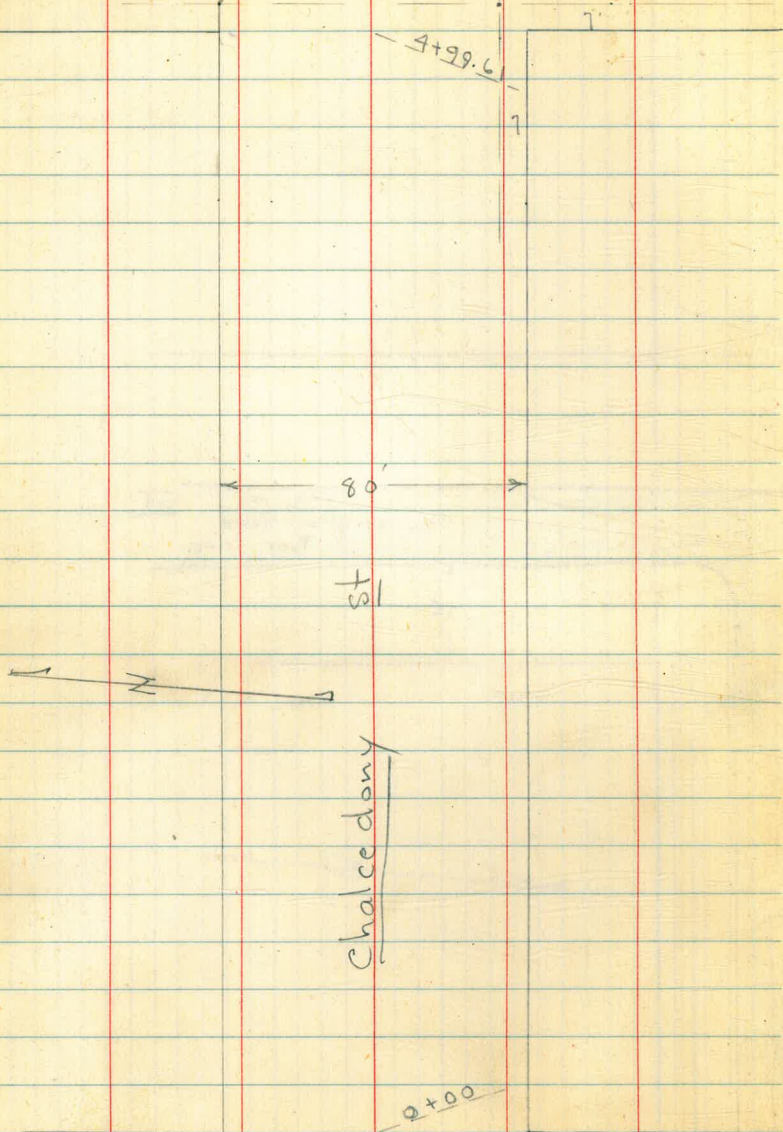
Chalcedony



Lamont

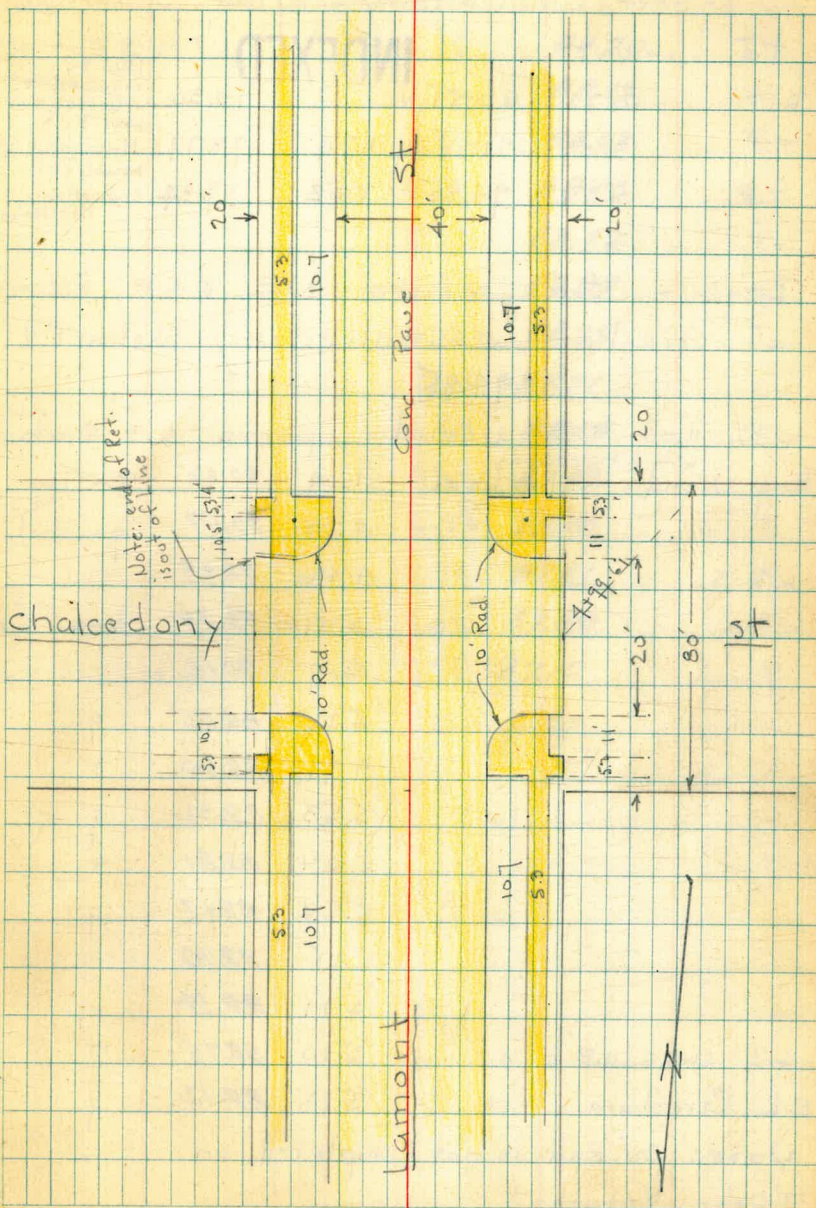
See Int. to opp. Page
ct.

st



Kendall

st



Lamont

X-Section Chalcedony - from Gresham

To Lamont

INDEXED

| | | | | |
|------|-------|-------|-------|----------------------------------|
| B.M. | 10.21 | 90.51 | 70.30 | NW 8-P Diamond + Gresham |
| T.P. | 13.09 | 91.86 | 174 | NW 7 ct. Missouri + Gresham |
| T.P. | 5.51 | 94.85 | 252 | NW 7 ct. Chalcedony + Gresham |

Begin - Rods around N.E. + S.E. Returns
of Gresham + Chalcedony - Sketch - P. 1

94.85

N.E. Ret. - 38' around - 6 parts - 6.3 Each.

| | | | |
|---------------------------------|------|-------|---------|
| Begin N. end = P.C. - 10' N. of | 4.19 | 90.66 | T = Top |
| | 4.78 | 90.07 | q = gut |
| 6.3 S. | 4.42 | 90.93 | T |
| | 5.01 | 89.84 | q |
| " | 4.67 | 90.18 | T |
| | 5.30 | 89.55 | q |
| " | 4.91 | 89.94 | T |
| | 5.53 | 89.32 | q |
| " | 5.04 | 89.81 | T |
| | 5.68 | 89.17 | q |
| " | 5.15 | 89.70 | T |
| | 5.71 | 89.14 | q |
| 6.3 = end = 10.8' E. of | 5.10 | 89.75 | T |
| E.L. Gresham | 5.73 | 89.12 | q |

Note: 30' Rad is not Completed on
These Returns

94.85

S.E. Ret. - 38' around - 6 - 6.3 each.

| | | | |
|---|------|-------|---|
| Begin - 0.8 E. of E.L. Gresham | 6.15 | 88.70 | T |
| | 6.72 | 88.13 | q |
| 6.3 W | 6.22 | 88.63 | T |
| | 6.79 | 88.06 | q |
| " | 6.33 | 88.52 | T |
| | 6.96 | 87.89 | q |
| " | 6.50 | 88.35 | T |
| | 7.14 | 87.71 | q |
| " | 6.68 | 88.17 | T |
| | 7.33 | 87.52 | q |
| " | 6.85 | 88.00 | T |
| | 7.54 | 87.31 | q |
| 6.3 = end = P.C. - 10' S. of S.L. Chalcedony | 7.05 | 87.80 | T |
| | 7.75 | 87.10 | q |

Begin X-Sections Chacedony - 80 st. 10' obs.
 ⊕ Gresham - Paved - Concr.

0+81 - 35.4 Rt = ⊕ 2.3 Brick walk

0+50

INDEXED

0+25

0+00 = E.L. Gresham - Note: edge of Concr.

Pave is 0.5 E. of E.L. will take rods on
 actual edge

0-20 = E. cb.

0-30

0-40 = ⊕ Gresham.

Lt. = N

⊕

Rt. = S 8

| | | | | | | | | | | | | |
|----------------------|------|------|------|------|------|------|------|------|----------------|---------|------|------|
| | | | | | | | 8896 | 8894 | | | | |
| | | | | | | | 5.89 | 5.91 | | | | |
| | | | | | | | 35.4 | 40 | | | | |
| | | | | | | | end | walk | | | | |
| 9025 | 9025 | 9005 | 9005 | 8985 | 8975 | 8955 | 8955 | 8955 | | | | |
| 4.1 | 4.1 | 4.8 | 4.8 | 5.0 | 5.1 | 5.3 | 5.0 | 5.3 | | | | |
| 40 | 22 | 20 | 10 | | 10 | 20 | 22 | 40 | | | | |
| 9115 | 9065 | 9015 | 8985 | 8975 | 8955 | 8935 | 8975 | 8955 | | | | |
| 3.7 | 4.2 | 4.7 | 5.0 | 5.1 | 5.3 | 5.5 | 5.1 | 5.3 | | | | |
| 40 | 22 | 20 | 10 | | 10 | 19 | 21 | 40 | | | | |
| 9025 | 9018 | 8975 | 8912 | 8912 | 8905 | 8864 | 8813 | 8770 | 8823 | 8877 | | |
| 4.61 | 4.67 | 5.10 | 5.73 | 5.68 | 5.80 | 6.21 | 6.72 | 6.15 | 6.12 | 6.08 | | |
| 36 | 31 | 21.5 | 21.5 | 10 | | 10 | 21.5 | 21.5 | 31 | 36 | | |
| walk | Top | Top | gut. | | | | gut. | Top | endwalk | endwalk | | |
| ends - 1' E. of E.L. | | | end | | | | | end. | 0.8 E. of E.L. | | | |
| 9208 | 9139 | 9066 | 9007 | 8961 | 8893 | 8861 | 8795 | 8741 | 8710 | 8780 | 8535 | 8598 |
| 2.81 | 3.46 | 4.19 | 4.78 | 5.24 | 5.92 | 6.24 | 6.90 | 7.44 | 7.75 | 7.05 | 9.50 | 8.87 |
| 100 | 100 | 50 | 50 | 40 | 20 | | 20 | 40 | 50 | 50 | 100 | 100 |
| Top | gut. | PC | gut. | | | | | | gut. | Top | gut. | Top |
| 9163 | 9018 | 8959 | 8910 | 8875 | 8808 | 8797 | 8725 | 8725 | 8552 | | | |
| 3.22 | 4.67 | 5.01 | 5.66 | 6.10 | 6.77 | 7.38 | 7.60 | 9.33 | | | | |
| 100 | 50 | 40 | 20 | | 20 | 40 | 50 | 100 | | | | |
| 9165 | 9002 | 8978 | 8922 | 8874 | 8810 | 8753 | 8727 | 8557 | | | | |
| 3.21 | 4.76 | 5.07 | 5.63 | 6.11 | 6.75 | 7.32 | 7.58 | 9.28 | | | | |
| 100 | 50 | 40 | 20 | | 20 | 40 | 50 | 100 | | | | |

94.85 - P. 7

2+79 - 40' Rt. = ± 3' Conc. walk

2+57 - 40' Rt. = ± 8' Conc. Dr.

2+50 - 23.6 Rt. = Uly. Picket Lot fence

2+20 - 34.5 Rt. = ± 3' Conc. walk

2+00

1+69 - 34.3 Rt. = ± 3' Conc. walk

1+50 - 39.5 Rt. = end fence

1+44 - 40' Lt. = ± 8' Conc. Dr.

1+34 - 40' Lt. = ± 3' Conc. walk

1+00 - 39.4 Rt. = Beg low bath fence

1+00

Lt.

±

Rt.

9

| | | | | | | | | | |
|-------|----------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | | | | | | | 40.18 | |
| | | | | | | | | 4.67 | 90.14 |
| | | | | | | | | 40 | 4.71 |
| | | | | | | | | walk | 40 |
| | | | | | | | | | Dr. |
| 90.25 | 91.25 | 91.55 | 91.35 | 91.15 | 90.25 | 90.95 | 90.65 | 89.95 | |
| 2.6 | 3.1 | 3.3 | 3.5 | 3.7 | 4.1 | 4.4 | 4.2 | 4.9 | |
| 40 | 20 | 17 | 10 | | 10 | 16 | 20 | 40 | |
| | | | | | | | | | |
| | | | | | | | | 89.95 | 89.94 |
| | | | | | | | | 4.90 | 4.91 |
| | | | | | | | | 34.5 | 40 |
| | | | | | | | | end | walk |
| 92.05 | 91.75 | 91.35 | 90.85 | 90.65 | 90.25 | 90.05 | 90.35 | 89.65 | 89.95 |
| 2.8 | 3.1 | 3.5 | 4.0 | 4.2 | 4.6 | 4.8 | 4.5 | 5.2 | 5.4 |
| 50 | 40 | 20 | 10 | | 10 | 18 | 21 | 40 | 50 |
| | | | | | | | | | |
| | | | | | | | | 89.72 | 89.71 |
| | | | | | | | | 5.13 | 5.14 |
| | | | | | | | | 34.3 | 40 |
| | | | | | | | | end | walk |
| 91.15 | 90.55 | | 90.95 | 90.35 | 89.95 | 89.75 | 89.35 | | |
| 3.7 | 4.3 | | 4.4 | 4.5 | 4.9 | 5.1 | 5.5 | | |
| 40 | 20 | | 10 | | 10 | 20 | 40 | | |
| | | | | | | | | | |
| | 91.20 | | | | | | | | |
| | 3.15 | | | | | | | | |
| | 40 = Dr. | | | | | | | | |
| 91.62 | | | | | | | | | |
| 3.22 | | | | | | | | | |
| 40 | | | | | | | | | |
| walk | | | | | | | | | |
| 91.59 | 91.19 | 90.34 | 90.22 | 90.04 | 89.64 | 89.24 | 89.04 | 88.54 | |
| 3.3 | 3.7 | 4.5 | 4.6 | 4.8 | 5.2 | 5.4 | 5.8 | 6.3 | |
| 50 | 40 | 20 | 10 | | 10 | 20 | 40 | 50 | |

94.85

0+50

0+41-40' Rt. = \pm 33 Conc. walk

0+32-40.6' Lt. = \pm 3' Conc. walk

0+04-40.2 = Rt. = \pm 2' Conc. walk

80' E = E.L. Haines = 0+00 ahead.

60' E = E. cb.

40' E = \pm

20' E = w. cb.

Set. B.M.

6.97 91.49

S.W. 7 Mon

4+99.94 = w.L. Haines - Extending sections along lines of Haines - To get profile

4+59-34.6 Lt. = \pm 6.5' Dr. - 2 - 15' Conc. strips

| Lt. | | \pm | | Rt. | | 11 | | | | |
|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| <u>99³⁶</u> | <u>93²⁶</u> | <u>93⁰⁶</u> | <u>92⁷⁶</u> | <u>92⁹⁶</u> | <u>92¹⁶</u> | <u>92⁵⁶</u> | <u>91⁴⁶</u> | | | |
| 4.1 | 5.2 | 5.4 | 5.7 | 6.0 | 6.3 | 5.9 | 7.0 | | | |
| 40 | 20 | 10 | 10 | 18 | | 20 | 40 | | | |
| | <u>94²¹</u> | | | | | <u>91⁵¹</u> | | | | |
| | 3.75 | | | | | 6.95 | | | | |
| | 40.6 | | | | | 40 | | | | |
| | walk | | | | | walk | <u>91³¹</u> | | | |
| | | | | | | | 7.15 | | | |
| | | | | | | | 40.2 | | | |
| | | | | | | | walk | | | |
| <u>96¹⁶</u> | <u>95⁰⁶</u> | <u>94⁰⁶</u> | <u>93¹⁶</u> | <u>92⁹⁶</u> | <u>92⁵⁶</u> | <u>92¹⁶</u> | <u>92³⁶</u> | <u>91³⁶</u> | <u>90⁴⁶</u> | <u>89⁴⁶</u> |
| 2.3 | 3.4 | 4.4 | 5.3 | 5.5 | 5.9 | 6.3 | 6.1 | 7.1 | 7.8 | 9.0 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 | 100 |
| <u>95⁸⁶</u> | <u>94⁸⁶</u> | <u>93⁹⁶</u> | <u>93²⁶</u> | <u>92⁸⁶</u> | <u>92⁵⁶</u> | <u>92¹⁶</u> | <u>91⁸⁶</u> | <u>91¹⁶</u> | <u>90²⁶</u> | <u>89¹⁶</u> |
| 2.6 | 3.6 | 4.5 | 5.2 | 5.6 | 5.9 | 6.3 | 6.6 | 7.3 | 8.2 | 9.3 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 | 100 |
| <u>95⁹⁶</u> | <u>94⁸⁶</u> | <u>93²⁶</u> | <u>93⁴⁶</u> | <u>92⁸⁶</u> | <u>92⁵⁶</u> | <u>92²⁶</u> | <u>92³⁶</u> | <u>91⁷⁶</u> | <u>90⁶⁶</u> | <u>89⁴⁶</u> |
| 2.5 | 3.6 | 4.2 | 5.0 | 5.6 | 5.9 | 6.2 | 6.1 | 6.7 | 7.8 | 8.8 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 | 100 |
| <u>95⁸⁶</u> | <u>94⁷⁶</u> | <u>93⁸⁶</u> | <u>93⁴⁶</u> | <u>92⁸⁶</u> | <u>92⁵⁶</u> | <u>92²⁶</u> | <u>92⁴⁶</u> | <u>91⁸⁶</u> | <u>90³⁶</u> | <u>89⁴⁶</u> |
| 2.6 | 3.7 | 4.6 | 5.0 | 5.6 | 5.9 | 6.2 | 5.8 | 6.6 | 8.1 | 9.0 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 | 100 |
| <u>95⁷⁶</u> | <u>94³⁶</u> | <u>93²⁶</u> | <u>93⁰⁶</u> | <u>92⁸⁶</u> | <u>92⁴⁶</u> | <u>92²⁶</u> | <u>92¹⁶</u> | <u>91⁷⁶</u> | <u>91⁰⁶</u> | <u>89⁷⁶</u> |
| 2.7 | 4.1 | 4.7 | 5.4 | 5.6 | 6.0 | 6.1 | 6.0 | 6.7 | 7.4 | 8.7 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 | 100 |
| | <u>93⁹⁹</u> | | <u>93⁸⁰</u> | | | | | | | |
| | 4.47 | | 4.56 | | | | | | | |
| | 40 | | 34.6 | | | | | | | |
| | Dr. | | | | | | | | | |

94.46

2+50

2+41- 39.9' Rt. = € 3.3' Conc. walk

1+03- 40' Rt. = € 2' Conc. walk

2+00

1+95- 40' Rt. = € 2' Conc. walk

1+58- 39.9' Rt. = € 3.3' Conc. walk

1+50

1+41- 39.9' Rt. = € 3.3' Conc. walk

1+03- 39.9' Rt. = € 2' Conc. walk

1+00

0+95- 39.9' Rt. = € 2' Conc. walk

0+58- 39.9' Rt. = € 3.3' Conc. walk

Lt.

€

Rt.

12

| | | | | | | | |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 94 ⁵⁶ | 93 ⁷⁶ | 93 ⁵⁶ | 93 ⁹⁶ | 93 ¹⁶ | 92 ⁸⁶ | 93 ¹⁶ | 92 ¹⁶ |
| 3.9 | 4.7 | 4.9 | 5.0 | 5.3 | 5.6 | 5.3 | 6.3 |
| 40 | 20 | 10 | | 10 | 18 | 20 | 40 |

| | |
|------------------|------------------|
| 92 ²¹ | |
| 6.25 | 92 ⁰⁷ |
| 39.9 | 6.39 |
| walk | 40 |
| | walk |

| | | | | | | | | | |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 94 ⁰⁶ | 94 ¹⁶ | 93 ⁵⁶ | 93 ³⁶ | 93 ²⁶ | 92 ⁸⁶ | 92 ⁰⁶ | 92 ⁸⁶ | 92 ⁰⁶ | 91 ⁹⁶ |
| 4.0 | 4.3 | 4.9 | 5.1 | 5.2 | 5.6 | 6.0 | 5.6 | 6.4 | 6.5 |
| 50 | 40 | 20 | 10 | | 10 | 18 | 20 | 40 | 50 |

| | |
|------------------|------------------|
| 92 ¹⁵ | |
| 6.31 | 92 ⁵¹ |
| 40 | 59.5 |
| walk | 39.9 |
| | walk |

| | | | | | | | |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 94 ⁰⁶ | 93 ²⁶ | 93 ³⁶ | 93 ¹⁶ | 92 ⁸⁶ | 92 ⁶⁶ | 92 ⁰⁶ | 92 ⁵⁶ |
| 4.4 | 4.7 | 5.1 | 5.3 | 5.6 | 5.8 | 5.5 | 5.9 |
| 40 | 20 | 10 | | 10 | 18 | 20 | 40 |

| | |
|------------------|------------------|
| 92 ⁰⁰ | |
| 6.00 | 91 ⁸³ |
| 39.9 | 6.63 |
| walk | 39.9 |
| | walk |

| | | | | | | | | | |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| 94 ⁹⁶ | 93 ⁸⁶ | 93 ²⁶ | 92 ¹⁶ | 92 ⁸⁶ | 92 ⁶⁶ | 92 ²⁶ | 92 ⁶⁶ | 91 ⁸⁶ | 91 ⁵⁶ |
| 4.0 | 4.6 | 5.1 | 5.3 | 5.6 | 5.8 | 6.2 | 5.8 | 6.6 | 6.9 |
| 50 | 40 | 20 | 10 | | 10 | 18 | 20 | 40 | 50 |

| | |
|------------------|------------------|
| 91 ⁸² | |
| 6.64 | 91 ⁴⁰ |
| 39.9 | 6.97 |
| walk | 39.9 |
| | walk |

98.46

Rods on Φ of Ret.

+59.5 E. = cb. line on Ret. on S.E. Cor

59 E. = E. side Pave strip - gutter. (Poor Cond.)

49 E.

40 E. = Φ

31 E.

21 E. = W. side Cold Lay Pave strip = gutter.

18 E. = Top of bank on edge of Rdwy.

17 E. 36.8' Rt. = Φ P. pole # 4798

5 E. = 23.2 Rt. = end fence

4+98.60 = W.L. Ingraham

Extending sections along lines of Ingraham to get profile

Lt.

#40

14050 Rt.

14

470

5.60

Top

gut.

| | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|--------------------|-------------------|-------------------|-------------------|
| | | | | | | 101 ²⁸ | 100 ³⁰ | 101 ²⁸ | 100 ⁰⁸ |
| | | | | | | 4.82 | 5.80 | 4.82 | 6.02 |
| | | | | | | 30 | 30 | 40 | 40 |
| | | | | | | Top-PC 10' Red. | gut. | Top end of cb. | gut. |
| 103 ²² | 102 ⁵¹ | 101 ⁹⁵ | 101 ⁴¹ | 100 ⁹¹ | 100 ⁰⁰ | 100 ⁰² | 99 ²⁸ | 97 ²⁸ | |
| 2.88 | 3.59 | 4.15 | 4.69 | 5.19 | 5.70 | 6.03 | 6.82 | 8.12 | |
| 100 | 65 | 40 | 20 | | 20 | 40 | 65 | 100 | |
| | | | | | | | | | |
| 103 ²⁹ | 102 ⁵⁵ | 101 ⁹² | 101 ⁵¹ | 101 ⁰⁷ | 100 ⁵⁹ | 100 ⁰² | 99 ²⁴ | 97 ⁹² | |
| 2.81 | 3.55 | 4.13 | 4.59 | 5.03 | 5.51 | 6.08 | 6.86 | 8.13 | |
| 100 | 65 | 40 | 20 | | 20 | 40 | 65 | 100 | |
| | | | | | | | | | |
| 103 ²⁸ | 102 ⁵¹ | 101 ⁹⁴ | 101 ⁵⁵ | 101 ⁰⁷ | 100 ⁵⁵ | 99 ⁹⁹ | 99 ¹¹ | 97 ⁸⁰ | |
| 2.82 | 3.59 | 4.14 | 4.55 | 5.03 | 5.55 | 6.11 | 6.99 | 8.30 | |
| 100 | 65 | 40 | 20 | | 20 | 40 | 65 | 100 | |
| | | | | | | | | | |
| 102 ⁹⁹ | 102 ¹⁴ | 101 ⁶⁰ | 101 ⁰⁹ | 100 ⁸⁹ | 100 ²⁰ | 100 ³² | 100 ⁰⁹ | 99 ⁵⁷ | 98 ²³ |
| 3.16 | 3.96 | 4.50 | 5.01 | 5.26 | 5.50 | 5.78 | 6.01 | 6.53 | 7.33 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 |
| | | | | | | | | | |
| 102 ⁵⁰ | 101 ⁵⁸ | 101 ⁰³ | 100 ⁹⁸ | 100 ²⁸ | 99 ⁹² | 99 ⁶⁷ | 99 ⁵³ | 99 ⁰⁹ | 98 ¹⁵ |
| 3.6 | 4.52 | 5.07 | 5.62 | 5.86 | 6.18 | 6.43 | 6.57 | 7.06 | 7.95 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 |
| | | | | | | | | | |
| 104 ²⁰ | 103 ²⁰ | 102 ²⁰ | 101 ⁵⁰ | 100 ⁵⁰ | 100 ¹⁰ | 99 ²⁰ | 99 ²⁰ | 100 ³⁰ | 99 ²⁰ |
| 1.4 | 2.4 | 3.3 | 4.6 | 5.6 | 6.0 | 6.2 | 6.2 | 5.8 | 6.3 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 17 | 23 | 40 |
| | | | | | | | | | |
| 103 ⁴⁰ | 102 ²⁰ | 101 ⁴⁰ | 101 ⁰⁰ | 100 ⁹⁰ | 99 ²⁰ | 99 ²⁰ | 100 ⁰⁰ | 99 ²⁰ | 99 ⁵⁰ |
| 2.7 | 3.9 | 4.7 | 5.1 | 5.7 | 6.2 | 6.3 | 6.1 | 6.8 | 7.6 |
| 100 | 65 | 40 | 20 | 10 | | 10 | 20 | 40 | 65 |

106.10

1+50

1+10 - 20' Rt. = ± Conc. Dr. 10'

1+00 - 36.4' Lt. = ± 8' Conc. Dr.

0+50

T.P. 8.19 110.87 3.42 152.68

0+25

Beq. cb. + walks on Rt. - See sketch
80' E. = E.L. Ingraham - 0+00 ahead.

70' E.

62 - 426 Lt. = ± Tel. pole " D 18481T
61' E. = Top bank along pave strip

| | 10262 | 10722 | 10592 | 10527 | 10437 | 10437 | 10442 | 10412 | 10322 | 10431 | 15 |
|--|-------|-------|-------|-------|-------|-------|------------------|-------|-------|-------|-------|
| | 2.2 | 3.8 | 4.9 | 5.0 | 6.3 | 6.3 | 6.4 | 6.7 | 7.1 | 6.58 | |
| | 50 | 40 | 36 | 23 | 18 | 10 | edge | 10 | 20 | 20 | |
| | | | | | | | | | gut | Top | |
| | | | | | | | | | | | 10302 |
| | | | | | | | | | | | 7.85 |
| | | | | | | | | | | | 20 |
| | | | | | | | | | | | Dr. |
| | | | | | | | | | | | 7.17 |
| | | | | | | | | | | | 51 |
| | | | | | | | | | | | walk |
| | 10210 | 10522 | 10495 | 10427 | 10337 | 10332 | 10322 | 10287 | 10332 | | |
| | 3.69 | 5.10 | 5.92 | 6.8 | 7.3 | 7.3 | 7.2 | 7.6 | 8.0 | 7.55 | |
| | 50 | 40 | 36.4 | 23 | 18 | 10 | 10 | 20 | 20 | | |
| | Dr. | Dr | end | | | | | gut. | Top | | |
| | 10622 | 10422 | 10327 | 10347 | 10232 | 10237 | 10227 | 10192 | 10242 | | |
| | 4.8 | 6.6 | 7.0 | 7.4 | 8.3 | 8.3 | 8.2 | 8.5 | 8.9 | 8.40 | |
| | 50 | 40 | 36 | 25 | 19 | 10 | 10 | 20 | 20 | | |
| | | | | | | | | gut. | Top | | |
| | 10620 | 10420 | 10320 | 10320 | 10230 | 10210 | 10220 | 10120 | 10140 | 10203 | |
| | 4.0 | 1.5 | 2.4 | 2.8 | 3.8 | 4.0 | 3.9 | 4.2 | 4.5 | 4.07 | |
| | 50 | 40 | 36 | 25 | 19 | 10 | 10 | 20 | 20 | 20 | |
| | | | | | | | | gut. | Top | Top | |
| | 10520 | 10520 | 10330 | 10220 | 10120 | 10120 | 10160 | 10140 | 10100 | 10155 | 10123 |
| | 10.9 | 0.4 | 2.8 | 3.4 | 4.2 | 4.4 | 4.5 | 4.7 | 5.1 | 4.55 | 4.37 |
| | 100 | 65 | 40 | 23 | 19 | 10 | edge of oil pave | 10 | 20 | 20 | 36 |
| | | | | | | | | | gut | Top | Back |
| | | | | | | | | | cb. | edge | walk |
| | 10420 | 10340 | 10300 | 10220 | 10180 | 10140 | 10140 | 10120 | 10080 | 10144 | 10150 |
| | 1.9 | 2.7 | 3.1 | 3.4 | 4.3 | 4.5 | 4.7 | 4.9 | 5.3 | 4.66 | 4.60 |
| | 100 | 65 | 40 | 25 | 22 | 10 | 10 | 10 | 20 | 20 | 36 |
| | | | | | | | | | gut | Top | edge |
| | | | | | | | | | | appbx | walk |
| | | | | | | | | | PC | | |
| | 10420 | 10320 | 10320 | 10300 | 10123 | 10122 | 10104 | 10080 | 10045 | 10140 | 10050 |
| | 1.9 | 2.9 | 2.9 | 3.1 | 4.67 | 4.88 | 5.06 | 5.30 | 5.65 | 4.7 | 6.1 |
| | 100 | 65 | 40 | 30 | 20 | 10 | 10 | 10 | 20 | 40 | 65 |
| | | | | | | | | | | | 100 |

106.10

Note ignore Ret. on this. Sect

3+59 = ± 9' Conc. Dr. on Rt.

3+50

3+28 - 22.2 Lt. = ± 3' Conc. walk

3+09 = ± 10' Conc. Dr. on Rt.

3+00

2+60 = ± 10' Conc. Dr. on Rt.

2+50

2+10 = ± 9.5' Conc. Dr. on Rt.

2+00

1+61 = ± 10' Conc. Dr. on Rt.

| LT | ± | RT. | 16 |
|--|--|--|--|
| 102 ²⁷ 0.6 50 | 109 ¹⁷ 1.7 40 | 108 ¹⁷ 2.1 20 | 107 ²⁷ 3.1 16 |
| 107 ⁶⁷ 3.2 10 | 107 ⁸⁷ 3.0 | 107 ⁶⁷ 3.2 10 | 107 ²⁷ 3.6 20 gut. |
| 109 ³¹ 1.56 40 walk | 108 ²² 18.8 366 Brk. | 108 ⁶⁴ 2.23 222 end | 107 ²⁷ 3.01 20 Top |
| 109 ²⁷ 1.1 50 | 108 ¹⁷ 2.7 40 | 107 ²⁷ 3.1 21 | 106 ²⁷ 4.1 17 |
| 106 ²⁷ 3.9 10 | 106 ²⁷ 3.9 edge | 106 ⁶⁷ 4.2 10 | 106 ²⁷ 4.6 20 gut. |
| 105 ²⁷ 5.1 10 | 105 ⁵⁷ 5.3 19.9 gut. | 106 ²⁷ 4.83 19.9 Top | 106 ⁹³ 3.94 20 Top |
| 104 ⁸¹ 6.06 19.8 Dr. | 105 ⁴¹ 5.41 31 walk | 104 ⁸¹ 6.06 19.8 Dr. | 105 ⁴¹ 5.41 31 walk |
| 108 ²⁷ 2.1 50 | 107 ³⁷ 3.3 40 | 107 ²⁷ 3.8 23 | 105 ⁸⁷ 5.0 18 |
| 106 ⁶⁷ 4.2 36 | 106 ¹⁷ 4.7 23 | 105 ¹² 5.7 18 | 105 ²⁷ 5.6 10 |
| 105 ²⁷ 5.6 edge | 105 ²⁷ 5.6 edge | 104 ⁹⁷ 5.9 10 | 104 ⁶⁷ 6.2 19.9 gut. |
| 103 ⁹⁴ 6.93 19.9 Dr. | 105 ¹³ 5.74 19.9 Top | 104 ⁶⁷ 6.2 19.9 Top | 104 ⁶³ 6.24 31 walk |

110.87

6.2 E. - 418 Rt. = Nly. of Φ Row of Euc. Trees
 2.5 Rt. = Φ Guy Pole
 5+19.32 = w.L. Jewell = end of cb. + walk on Rt.

5+09 = Φ 10' Conc. Dr. on Rt.

5+00

T.P. 7.60 117.70 0.77 110.10 Value-Meter

4+59 -- Φ 11' Conc. Dr. on Rt.

4+50

4+09 - Φ 10' Conc. Dr. on Rt.

4+00

3+84 - 40.2 Lt. = Φ 2.6' Stone + Conc. walk

Lt. Φ Rt. 17

112.50 111.40 111.20 111.00 110.70 110.50 110.89 111.07 111.24 111.30 110.30 109.80
 5.2 6.3 6.5 6.7 7.0 7.2 6.81 6.63 6.46 6.4 6.9 8.7
 40 20 40 10 199 199 21 36 40 25 100
 gut Top Walk end end

113.30 112.10 111.10 110.60 110.60 110.30 110.10 110.56 110.20 110.80
 4.4 5.6 6.6 7.1 7.1 7.4 7.6 7.14 7.44 6.80
 50 40 20 10 edge 10 199 199 199 31
 50 40 20 10 edge 10 199 199 199 31
 gut Top Top Dr. walk

117.70

110.37 110.87 110.07 109.37 109.67 109.47 109.07 108.69
 10.5 0.0 0.8 1.3 1.2 1.4 1.8 2.18
 50 40 20 10 10 20 20 20
 50 40 20 10 10 20 20 20
 gut Top Top Top Top Top Top
 1.48 0.91
 199 31
 Dr. walk

108.42 109.01
 2.45 1.86
 20 31
 Dr. walk

110.87 110.27 109.57 109.77 109.87 108.57 108.17 108.77
 0.0 0.6 1.3 2.1 2.0 2.3 2.7 2.10
 50 40 20 10 edge 10 20 20
 50 40 20 10 edge 10 20 20
 edge 10 gut Top

9.90
 40.2
 walk

110.87

0+20 - 39.8 Rt. = \pm 4' Conc. walk

BM. on F.H. Below 2.29 115.41

0+05 - 21.2 Rt. = \pm F.H.

80' E = E.L. Jewell, = 0+00 ahead

78' E - 23.4 Rt. = \pm Guy Pope #1701

60' E = F. cb.

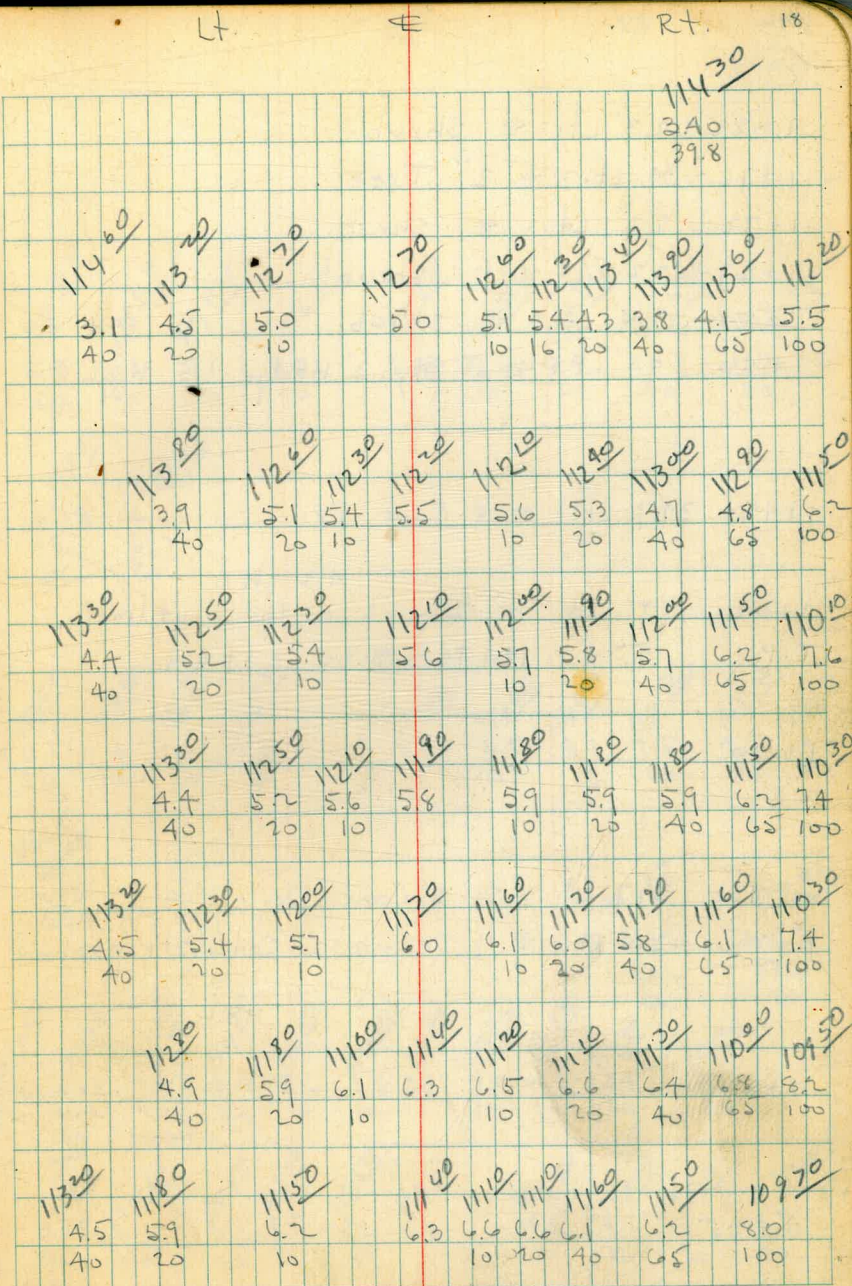
55' E = gut. - Dirt.

45' E = edge of Pave Strip

40' E = \pm

25' E = Edge of 20' oilpave strip - gutter
Poor Cond.

20' E = W. cb.



96
+1
58

1+85- 23' Lt. = \pm Shrub.

1+76- 39' Lt. = \pm 2" Tree.

1+72- 23' Lt. = \pm Shrub.

1+67- 22.5' Lt. = \pm Shrub.

1+54- 24' Lt. = \pm shrub.

1+50- 21' Lt. = \pm of Sly. 3' Hedge 5' High

1+42- 39.7' Lt. = \pm 8' Conc. Dr.

1+02- 22' Lt. = \pm Sly. 2' Hedge -lotline
4' High

T.P. 9.74 124.14 3.30 114.40

1+00

0+93- 39.7' Lt. = \pm 8' Conc. Dr.

0+85- 43.6' Rt. = \pm 7' Dr. - 2-2' Conc. strips

0+50

0+25

Lt.

\pm

Rt.

19

| | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 118.34 | 118.04 | 117.04 | 116.14 | 115.24 | 115.54 | 115.34 | 113.44 | 112.94 |
| 5.8 | 0.1 | 7.1 | 8.0 | 8.2 | 8.6 | 8.8 | 10.7 | 11.2 |
| 50 | 40 | 20 | 10 | | 10 | 20 | 40 | 50 |

| | |
|--------|--------|
| 118.36 | 118.03 |
| 5.78 | 6.11 |
| 49.7 | 39.7 |
| Dr. | Dr. |

| | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 117.60 | 117.30 | 116.30 | 115.30 | 124.14 | 115.00 | 114.60 | 114.60 | 115.20 | 115.00 | 113.70 |
| +0.1 | 0.4 | 14 | 24 | | 27 | 3.1 | 3.1 | 2.5 | 2.7 | 4.0 |
| 50 | 40 | 20 | 10 | | 10 | 16 | 20 | 40 | 50 | |

| |
|------------|
| 114.25 |
| +0.55 |
| 59.7 |
| floor Gar. |

| |
|--------|
| 117.29 |
| 0.71 |
| 39.7 |
| Dr. |

| |
|--------|
| 114.23 |
| 3.47 |
| 43.6 |
| Dr. |

| |
|--------|
| 113.71 |
| 3.99 |
| 53.6 |
| Dr. |

| | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 117.50 | 117.32 | 116.80 | 114.20 | 114.10 | 114.20 | 114.00 | 114.00 | 113.70 | 113.50 | 114.30 | 111.20 |
| 0.2 | 0.38 | 0.9 | 3.0 | 3.6 | 3.5 | 3.7 | 4.0 | 4.2 | 3.4 | 3.4 | 3.5 |
| 50 | 40.2 | 40 | 20 | 16 | 10 | 10 | 16 | 16 | 20 | 40 | 40 |

| | | | | | |
|----------|--------|----------------|--------|--------|--------|
| 117.15 | 115.60 | 114.00 | 113.30 | 113.50 | 113.50 |
| 0.55 | 2.1 | 3.7 | 4.4 | 4.2 | 4.2 |
| 40.2 | 40 | 20 | 16 | 10 | 10 |
| Top wall | | Base Rock wall | | | |

117.70

3+50 - 24.7' Lt. = Φ Sly. 2' Hedge - 5' High

3+43 - 39.7 Lt. = Φ 8' Conc. Dr.

3+37 - 21' Lt. = end Φ shrubs.

3+01 - 21' Lt. = Beg Φ of Row of shrubs

3+00 - 19.6 Lt. = Φ Sly. 2' Hedge - 5' High

2+97 - 19.1 Lt. = Φ Sly. 1' Hedge - 1' High

2+92 - 39.9 Lt. = Φ 8' Conc. Dr.

2+87 - 20' Lt. = Φ Sly. of 1' Hedge 1' High

2+84 - 41.2 Rt. = Φ 3' Conc. walk.

2+65 - 24.6 Lt. = Φ 18" Olive

2+63 - 90.6 Rt. = Φ Howse - Low

2+50 - 22' Lt. = Φ Sly. 1' Low Hedge

2+42 - 40.7 Lt. = Φ 8' Conc. Dr.

2+38 - 25.2 Lt. = Φ 18" Olive Tree

2+04 - 22.5 Lt. = Φ shrub.

2+00 - 19.5 Lt. = Φ Sly. 2.5' Hedge - 5' High

1+93 - 19.8 Lt. = Φ 11' Conc. Dr.

| | | | | | | | | | | | |
|-----------------------|-----------------------|-----------------------|--------------------|--------------------|--------------------|--------------------|---------------------|-------------------------------|--------------------|--------------------------------|--------------------|
| 12144 2.7 50 | 12104 3.1 40 | 12034 3.8 20 | 11924 4.9 17 | 11924 4.9 10 | 11904 5.1 13 | 11884 5.3 13 | 11934 4.8 20 | 11724 6.2 40 | 11754 6.6 50 | 20 | |
| 12122 2.37 59 | 12098 3.16 39.7 | 12024 4.0 40 | 11984 4.3 20 | 11854 5.6 17 | 11824 5.8 10 | 11814 6.0 13 | 11724 6.2 16 | 11854 5.6 20 | 11814 6.0 40 | 11704 7.1 40 | 11614 8.0 50 |
| 12044 3.7 50 | 12014 4.0 40 | 11984 4.3 20 | 11854 5.6 17 | 11824 5.8 10 | 11814 6.0 13 | 11724 6.2 16 | 11854 5.6 20 | 11814 6.0 40 | 11704 7.1 40 | 11614 8.0 50 | |
| 12046 3.68 49.9 | 11996 4.18 39.9 | | | | | | | | | | |
| | | | | | | | | 11634 7.80 41.2 walk | | | |
| | | | | | | | | | | 11594 8.20 70.6 floor | |
| 12014 4.0 50 | 11984 4.3 40 | 11914 5.0 22 | 11744 6.7 17 | 11724 6.9 10 | 11714 7.0 10 | 11624 7.1 10 | 11624 7.9 20 | 11524 8.9 40 | 11504 9.1 50 | | |
| 12069 3.45 58.7 | 11990 4.24 40.7 | | | | | | | | | | |
| 11934 4.6 50 | 11914 5.0 40 | 11794 6.2 20 | 11704 7.1 10 | 11654 7.6 10 | 11624 7.9 10 | 11544 8.7 20 | 11404 10.1 40 | 11374 10.4 50 | | | |
| 11914 5.00 40 | 11826 5.88 33.2 | 11758 6.56 19.8 | | | | | | | | | |
| Dr. | Brk | Dr. | | | | | | | | | |

124.14

26' E. - 35.5' Rt. = £ 5" Pepper

20' E. - w. cb. line - to N.

14' E. - 25.1 Lt. = £ 20" Pepper

7' E. - 30.2' Rt. = end wire fence

5+00.03 = w.L. Kendall - To N.

4+93- 25' Lt. = £ 18" Olive

4+83- 384 Lt. = £ 3' Conc. walk

T.P. 9.04 131.86 132 122.82 ^{sw 7 Mon.} Kendall

4+50 1.11 111.87 112 112.7

4+49- 20.5 Lt. = £ Sly. 2' Hedge - 5' High

4+41- 39.8 Lt. = £ 8' Conc. Dr.

4+36- 24' Lt. = End. £ flower planting.

4+27- 39' Lt. = £ 15" Olive

4+02- 24' Lt. = Beg. £ 8' wide flower planting

4+00- 21' Lt. = £ Sly. 2' Hedge - 5' High

1+89- 30' Rt. = Beg. old wire fence - poor

3+92- 39.8' Lt. = £ 8' Conc. Dr.

3+71- 23.4 and 36.5 Lt. = £ of shrubs

3+69- 25.5 Lt. = £ 2.5' Brick walk

3+67- 23.4 Lt. = £ shrub. also 36.5 Lt. = £ shrub.

| | | | | | | | | | | |
|--|-------------------------------------|--------------------------------------|-------------------------------------|-------------------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| | <u>125926</u> 5.9 40 | <u>12486</u> 7.0 20 | <u>12386</u> 8.0 10 | <u>12366</u> 8.2 10 | <u>12336</u> 8.5 10 | <u>12306</u> 8.8 17 | <u>12410</u> 7.7 20 | <u>12400</u> 7.8 40 | <u>12376</u> 8.1 50 | |
| | <u>12536</u> 6.3 40 | <u>12416</u> 7.7 20 | <u>12326</u> 8.6 10 | <u>12306</u> 8.8 | <u>12236</u> 9.5 15 | <u>12356</u> 8.3 20 | <u>12346</u> 8.4 40 | <u>12336</u> 8.5 50 | | |
| | <u>12404</u> +0.1 50 | <u>12374</u> 0.4 40 | <u>12294</u> 1.2 22 | <u>12164</u> 2.5 17 | <u>12154</u> 2.6 10 | <u>12124</u> 2.9 14 | <u>12194</u> 2.2 20 | <u>12154</u> 2.6 40 | <u>12134</u> 2.8 50 | |
| | <u>12409</u> 0.05 49.8 Dr. | <u>12360</u> 0.46 39.8 Dr. | | | | | | | | |
| | <u>12244</u> 17 50 | <u>12224</u> 19 40 | <u>12174</u> 24 22 | <u>12064</u> 35 18 | <u>12044</u> 37 10 | <u>12014</u> 40 | <u>11994</u> 42 13 | <u>12054</u> 3.6 20 | <u>11984</u> 4.3 40 | <u>11954</u> 4.6 50 |
| | <u>12172</u> 2.42 40 walk | <u>12115</u> 2.99 25.5 walk | <u>12245</u> 1.69 49.8 Dr. | <u>12218</u> 1.76 37.8 Dr. | | | | | | |

124.14

0+59 - 40' Lt. = ± 7' Dr. - 2-2' Conc. strips

0+57 - 40' Rt. = ± 12' Conc. Dr.

0+51 - 27 Rt. = ± Nly. 1' ledge - 1' High

0+50

0+25

0+11 - 39.9 Lt. = ± 3' Conc. walk

T.P. 12.19 135.01 9.04 122.82

0+08 - 39.9 Rt. = ± 8' Conc. Dr.

0+02 - 38.8 Rt. = ± 7" Pepper

21.2 Rt. = ± F.H.

80' E. = F.L. of Kendall to N. = 0+00 ahead.

60' E. = F. cb.

40' E. = ±

Lt. Rt. 22

130.02
4.99
5.0
Dr.

129.37
5.64
7.0
Dr.

129.41
5.6
5.0

129.01
6.0
4.0

128.41
6.6
2.0

127.21
8.0
1.0

127.41
7.6
1.0

127.41
7.6
1.0

127.61
7.4
2.0

127.41
7.6
4.0

127.41
7.6
5.0

127.66
7.35
4.0
Dr.

127.76
7.25
5.0
Dr.

129.01
6.0
5.0

128.51
6.5
4.0

127.21
7.3
2.0

126.21
8.8
1.0

126.51
8.5
1.0

126.51
8.5
1.0

126.71
8.3
2.0

127.01
8.0
4.0

127.01
8.0
5.0

129.08
5.93
4.99
walk

128.52
6.49
3.99
walk

135.01

127.66
4.2
4.0

126.46
5.4
2.0

126.16
5.7
1.4

125.46
6.4
1.0

125.66
6.2
1.0

125.66
6.2
1.0

126.16
5.7
2.0

126.56
5.3
4.0

126.60
5.26
3.99
Dr.

126.44
5.42
5.84
floor

122.66
5.6
5.0

126.96
4.9
4.0

125.96
5.9
2.0

124.76
7.1
1.0

124.86
7.0
1.0

124.86
7.0
1.0

124.86
7.0
1.0

124.86
7.0
1.0

125.56
6.3
4.0

125.26
6.6
5.0

126.36
5.5
4.0

125.06
6.8
2.0

124.46
7.4
1.0

124.26
7.6
1.0

124.06
7.8
1.0

123.86
7.9
1.0

124.86
7.0
2.0

124.26
7.1
4.0

124.26
7.6
5.0

131.86

2+37- 36.9 Rt. = end fence

2+00- 35.5 Rt. = £ Nly. 2 Hedge - 4' High

2+00 36.8 Rt. = Bsq. Picket fence

1+74- 26.2 Rt. = £ 2.5' Conc. Block walk +
8' Conc. Steps to House

1+60

1+40- 39.9 Lt. = £ 7' Dr. - 2-2' Conc. Strips

1+30

1+09- 39.8 Rt. = £ 8' Conc. Dr.

1+00

0+89- 26' Rt. = £ 3" Tree

0+80- 40' Lt. = £ 3' Conc. walk

0+71- 25.8 = £ 3" Tree

Lt.

£

Rt.

23

| | | | | | | | | | | | | | |
|-----------------------------------|-----------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|---------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|
| 132 ⁰¹ 3.0 50 | 131 ⁴¹ 3.6 40 | 130 ²¹ 4.8 20 | 130 ⁰¹ 5.0 10 | 129 ⁹¹ 5.1 | 129 ⁹¹ 5.1 10 | 130 ⁰¹ 5.0 20 | 129 ⁴¹ 5.6 40 | 129 ²¹ 5.8 50 | | | | | |
| 132 ⁰¹ 3.0 50 | 131 ⁵¹ 3.5 40 | 130 ⁸¹ 4.2 20 | 130 ⁴¹ 4.2 14 | 130 ⁴¹ 4.6 10 | 130 ⁴¹ 4.6 10 | 130 ³¹ 4.7 10 | 130 ¹¹ 4.9 20 | 129 ⁹¹ 5.4 40 | 129 ⁷⁶ 5.10 20 | 130 ⁹³ 4.08 40 | 129 ⁹¹ 5.10 20 | 129 ⁷⁶ 5.25 40 | 130 ⁹³ 4.08 40 |
| 131 ²¹ 3.30 49.9 | 130 ²⁶ 3.75 39.9 | 131 ⁴¹ 3.6 50 | 130 ⁶¹ 4.4 40 | 130 ⁵¹ 4.5 20 | 130 ⁴¹ 4.6 13 | 130 ⁰¹ 5.0 10 | 130 ¹¹ 4.9 | 130 ²¹ 4.8 10 | 130 ⁵¹ 4.5 20 | 129 ⁶¹ 5.4 40 | 129 ³¹ 5.7 50 | 129 ⁴⁵ 5.56 39.8 | 129 ⁰⁷ 5.94 39.8 |
| 130 ²¹ 4.8 30 | 129 ⁹¹ 5.1 40 | 129 ⁶¹ 5.4 20 | 129 ²¹ 5.3 13 | 129 ⁰¹ 6.0 10 | 129 ¹¹ 5.9 | 129 ³¹ 5.7 10 | 129 ⁶¹ 5.4 20 | 129 ¹¹ 5.9 40 | 128 ⁶¹ 6.4 50 | 129 ⁴⁵ 5.56 39.8 | 129 ⁰⁷ 5.94 39.8 | 129 ⁴⁵ 5.56 39.8 | 129 ⁰⁷ 5.94 39.8 |
| 130 ³³ 4.68 50 | 129 ⁹⁰ 5.11 40 | walk | | | | | | | | | | | |

135.01

Chalcedony

See sketch - P. 6

4+99.61 = w.l. Lamont. = edge of Conc. Pavc

4+98 - 36.8 Rt. = End. - \pm Hedge

4+98 - 25.8 Rt. = \pm 1" Palm

T.P. 4.89 130.89 9.01 126.00 sw. 7' ct. Lamont.

4+96 = Top of Bank

4+82 - 25.5 Rt. = \pm 1" Palm

4+75

4+67 - 25.8 Rt. = \pm 1" Palm

4+50 - 25.7 Rt. = \pm 1" Palm

4+42 - 25.8 Rt. = \pm Guy pole

4+35 - 26.3 Rt. = \pm Deadman

4+31 - 36.1 Rt. = Beg. \pm 1" Hedge - 2' High

4+31 - 26.2 Rt. = \pm 1" Palm

4+25

4+24 - 40' Rt. = \pm 14.5' Conc. Dr.

4+15 - 26.2 Rt. = \pm 1" Palm

Lt.

\pm

Rt

25

| | | | | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 127 ⁰⁹ | 127 ⁰⁷ | 127 ⁰³ | 126 ⁹⁷ | 126 ²⁹ | 126 ²⁷ | 126 ¹⁹ | 125 ⁸⁴ | 125 ⁸³ | 126 ⁰³ | 126 ⁰⁷ | 126 ⁰⁷ | 126 ¹⁹ |
| 3.8 | 3.82 | 3.86 | 3.92 | 4.0 | 4.42 | 4.70 | 5.05 | 5.51 | 4.86 | 4.82 | 4.82 | 4.7 |
| 40 | 36.2 | 31 | 20 | 20 | 10 | 10 | 10 | 20 | 20 | 31 | 36.3 | 40 |
| | end walk | | Top gut | Top gut | | | | gut. | Top end cb. | Top end walk | | |

| | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 131 ⁶¹ | 130 ⁷¹ | 128 ⁸¹ | 126 ⁸¹ | 126 ⁵¹ | 126 ¹¹ | 126 ⁹¹ | 126 ⁴¹ | 126 ³¹ |
| 3.4 | 4.3 | 6.2 | 8.2 | 8.5 | 8.9 | 8.6 | 8.6 | 8.7 |
| 50 | 40 | 20 | 9 | | 10 | 20 | 40 | 50 |

| | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 132 ⁰¹ | 131 ⁴¹ | 130 ³¹ | 129 ²¹ | 128 ²¹ | 127 ⁹¹ | 127 ⁵¹ | 127 ⁴¹ | 127 ¹¹ | 127 ⁰¹ |
| 3.0 | 3.6 | 4.7 | 5.8 | 6.8 | 7.1 | 7.5 | 7.6 | 7.9 | 8.0 |
| 50 | 40 | 20 | 11 | 9 | | 10 | 20 | 40 | 50 |

| | | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 132 ⁴¹ | 131 ⁵¹ | 130 ⁰¹ | 130 ²¹ | 129 ⁵¹ | 129 ³¹ | 128 ⁹¹ | 128 ⁶¹ | 128 ²¹ | 127 ²¹ | 127 ⁵¹ |
| 2.6 | 3.5 | 4.6 | 4.8 | 5.5 | 5.7 | 6.1 | 6.4 | 6.8 | 7.3 | 7.5 |
| 50 | 40 | 20 | 12 | 10 | | 10 | 15 | 20 | 40 | 50 |

| | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 133 ²¹ | 132 ¹¹ | 131 ¹¹ | 130 ¹¹ | 129 ⁷¹ | 129 ⁴¹ | 129 ¹¹ | 128 ²¹ | 128 ³⁰ | 127 ²² |
| 1.8 | 2.9 | 3.9 | 4.9 | 5.3 | 5.6 | 5.9 | 6.3 | 6.71 | 7.19 |
| 50 | 40 | 20 | 10 | | 10 | 15 | 20 | 40 | 50 |

| | |
|-------------------|-------------------|
| 128 ³² | 127 ⁸⁶ |
| 6.69 | 7.15 |
| 40 | 55.2 |
| Dr. | floor |
| | car |

135.01

40' E. = Φ Lamont = End.

20' E. (cont.)

20' E. = w. cb.

Rods on Mid points of 10' Rad. Returns

10' E. = opp. P.C. of 10' Rad. Returns.

| | | | | | | | | | | |
|--|--|---|---|---|--|--|--|---|---|--|
| 130 ¹³ 0.76 100 | 128 ⁰⁹ 2.80 65 | 127 ¹³ 3.76 40 | 126 ⁴⁹ 4.40 20 | 126 ⁰⁸ 4.81 | 125 ²³ 5.14 20 | 125 ⁴⁸ 5.41 40 | 124 ⁶⁴ 6.25 65 | 123 ⁵⁰ 7.39 100 | | |
| 130 ¹⁹ 0.70 100 Top | 129 ⁶⁹ 1.20 100 gut. | 128 ²⁵ 2.64 65 Top | 127 ⁶⁷ 3.22 65 gut. | 124 ³⁹ 6.50 65 gut. | 124 ²³ 5.96 65 Top | 123 ²⁵ 7.64 100 gut. | 123 ⁹¹ 7.08 100 Top | | | |
| 126 ⁹⁰ 3.99 40 Top | 126 ⁵⁴ 4.35 40 gut. | 126 ⁸⁶ 4.03 30 Top P.C. Ret. | 126 ²² 4.61 30 gut. | 126 ⁰⁸ 4.81 20 | 125 ⁷⁸ 5.11 | 125 ³³ 5.56 20 | 125 ¹⁸ 5.71 30 gut. | 125 ⁸⁰ 5.09 30 Top P.C. Ret. | 125 ¹¹ 5.78 40 gut. | 125 ⁷⁰ 5.19 40 Top |
| U.W. Ret. 126 ³⁵ 4.04 Top Φ Ret. | 126 ¹² 4.77 gut. | 125 ⁸⁶ 5.03 Top Φ Ret. | 125 ²⁸ 5.61 gut. | 126 ⁰⁰ 4.89 | 125 ²² 5.17 10 | 125 ³¹ 5.58 20 gut. | 125 ²⁸ 4.96 20 Top P.C. | | | |

Jewell St 80' See 1773-61 - for Jewell Sections

INDEXED

51892

X-Sections of
Beryl St. -
Ingraham to
Hamont

St

60'

20'

Beryl

New db

A

30' Rad.

12'

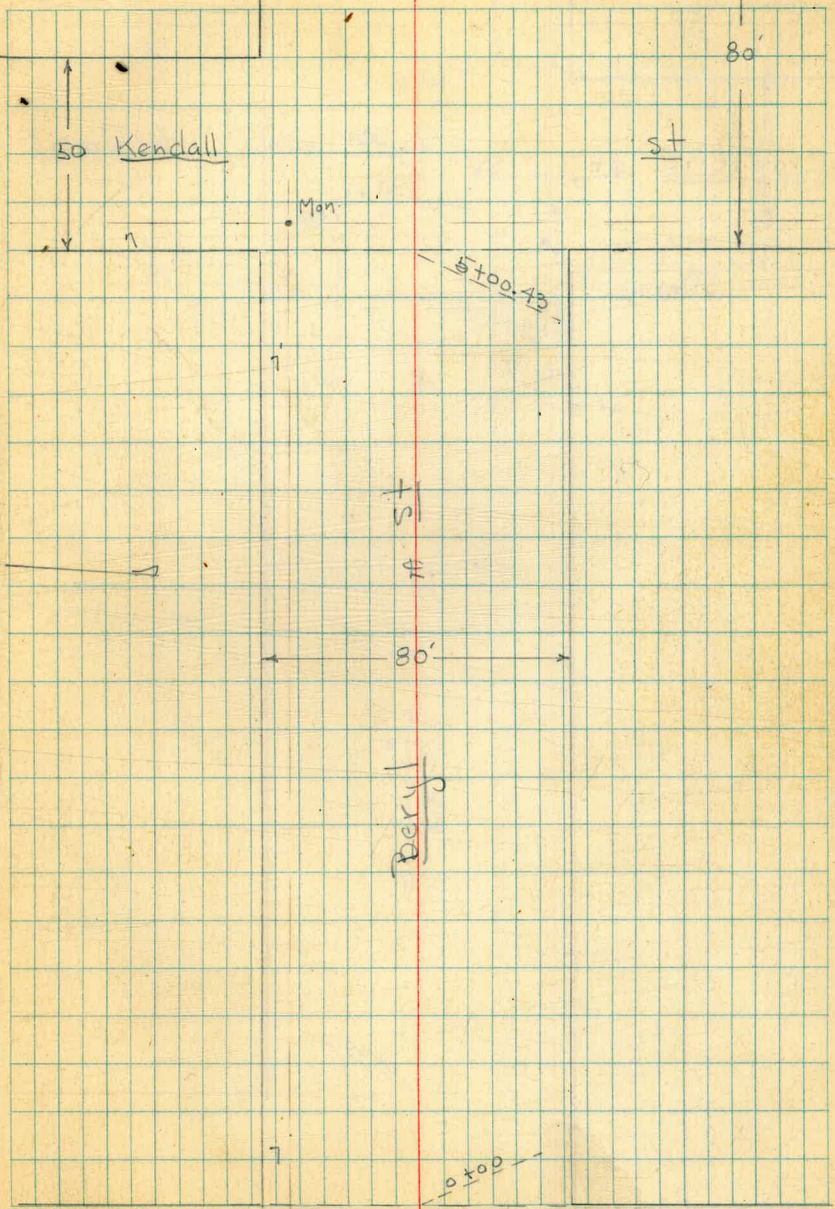
0 to 0

Disk

See 1773-55 for Int.

Ingraham

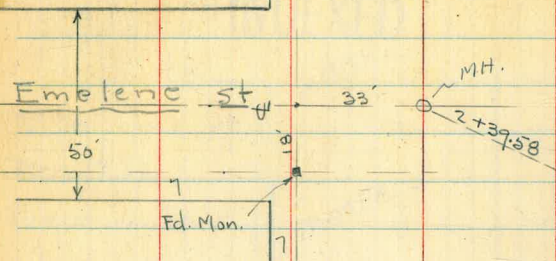
St



Jewell

Man.

St



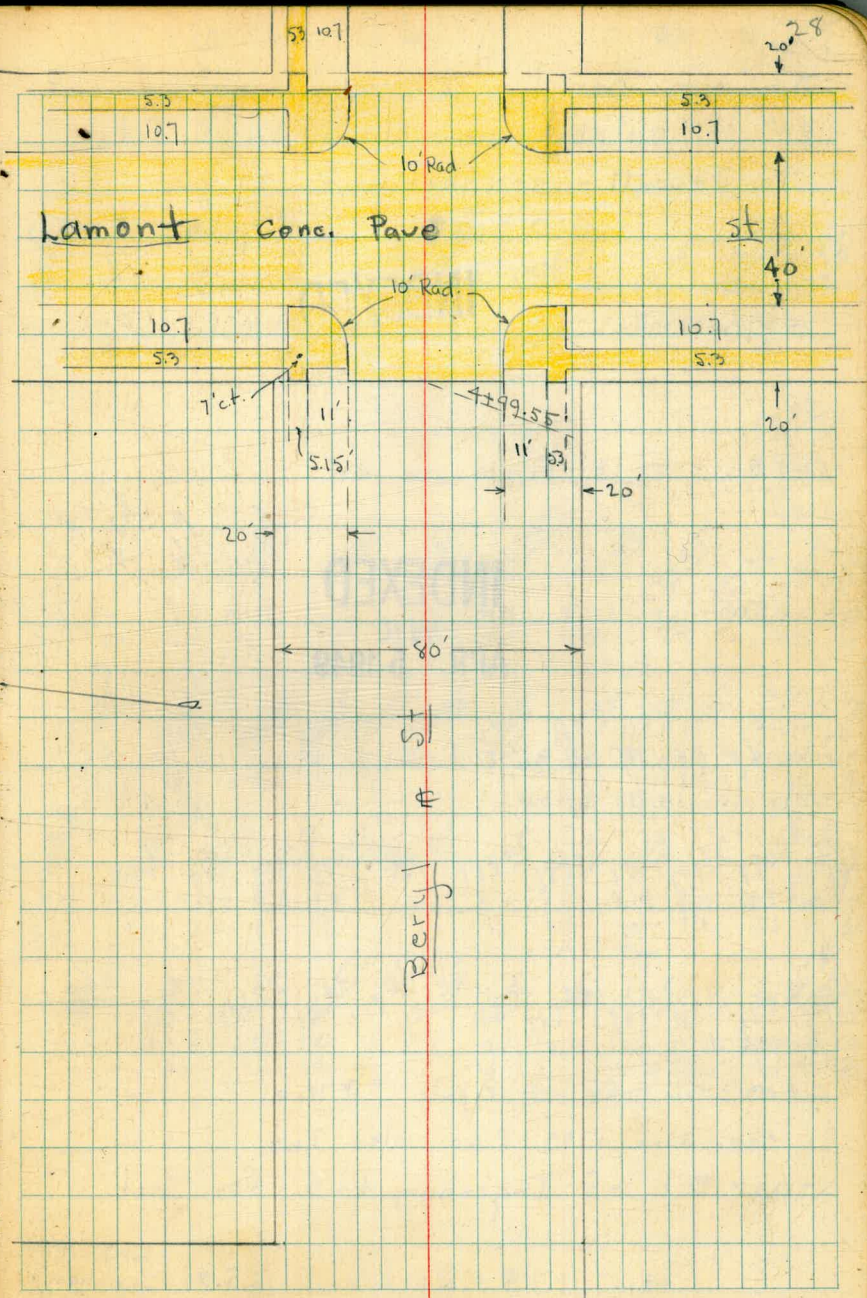
Beryl St

Beryl St

0+00

Kendall

St



Emelene St

X-Sect. Beryl - Ingraham to Lamont
 80' st. 20' cbs. - new cbs. in on S. side
 To Jewell - see sketch P. 27

W.O. 31371 11-7-47 - 70.

INDEXED

0+70

0+56 - ± 18' Drive on Rt.

INDEXED

0+50

WIC
 APR 5 1949

0+18 = opp. P.C. of 30' Rad. Ret on Rt.

Note: should be below.

0+25

0+10 - 23 Rt. = ± F.H.

0+06

0+03 = 26.1 Rt. = ± P. pole # P 1601

See Book 1773 - P. 60 - also Int.

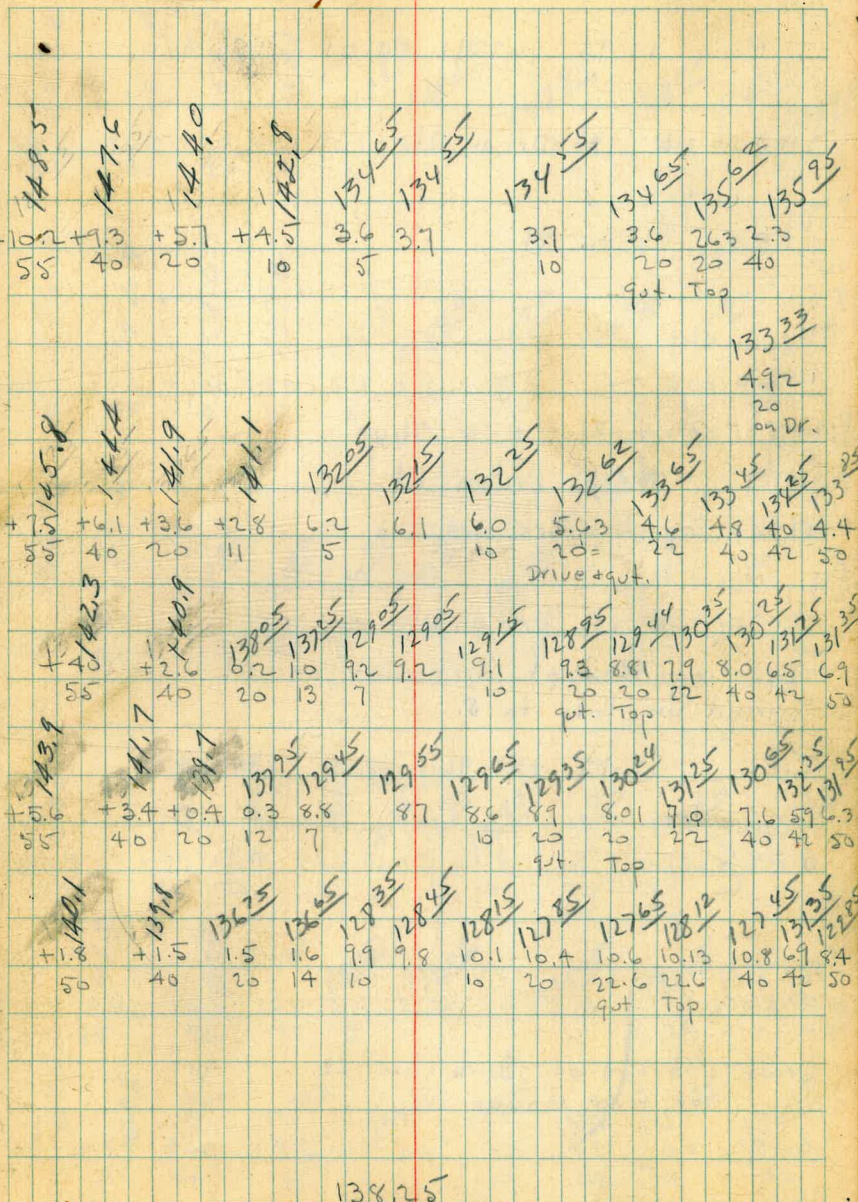
0+00 = F.L. of Ingraham to S. for Sect.

13.17 138.25

sw 1' ct.
 125.08 Ingraham &
 Beryl

Lt = N.

Rt. = S 29



T.P. 11.96 162.91 0.01 150.95

2+00 = ± 18' Dr. on Rt.

1+80 = cb. on Rt.

1+60

1+58 = 26.6' Rt. ± 6" Olive

1+49 = ± 18' Dr. on Rt.

1+40 = Top cb. = Brk. on U.C.

1+20 = ± 18' Dr. on Rt.

Ignoring Row of dirt piles on S.L. - will spread on Lots to S.

T.P. 12.89 150.96 0.18 138.07

0+86

0+83

Drive cut out of Bank on Lt.
for Prop. House

0+72

Lt.

±

Rt.

30

| | | | | | | | | | |
|-------|-------|--------|--------|--------|--------|--------|-----------|-----------|--------|
| 159.2 | 157.4 | 154.7 | 154.1 | 148.86 | 148.80 | 148.86 | 148.80 | 149.46 | 149.96 |
| +5.2 | +6.4 | +3.7 | +3.1 | 2.1 | 2.1 | 2.1 | 2.1 | 2.10 | 1.5 |
| 5 | 40 | 20 | 10 | 5 | 5 | 10 | 10 | 20 | 22 |
| | | | | | | | | Dr. + gut | 40 |
| 156.3 | 154.3 | 152.0 | 151.4 | 145.15 | 145.00 | 145.26 | 144.96 | 145.92 | 146.46 |
| +5.3 | +3.3 | +1.0 | +0.4 | 5.8 | 5.9 | 5.7 | 6.0 | 5.04 | 4.5 |
| 5 | 40 | 20 | 10 | 5 | 5 | 10 | 20 | 20 | 40 |
| | | | | | | | gut | Top | |
| 152.9 | 151.4 | 148.96 | 147.86 | 140.26 | 140.36 | 140.46 | 143.83 | 141.86 | 141.27 |
| +1.9 | +0.4 | 2.0 | 3.1 | 10.2 | 10.6 | 10.5 | 7.13 | 9.98 | 9.3 |
| 55 | 40 | 20 | 10 | 5 | 5 | 10 | 20 = Top | 20 | 22 |
| | | | | | | | Dr. + gut | 40 | 40 |
| 150.6 | 148.0 | 145.7 | 144.1 | 150.96 | 136.55 | 136.95 | 136.25 | 137.53 | 137.85 |
| +12.3 | +9.9 | +7.4 | +5.5 | 12.6 | 11.7 | 11.8 | 1.5 | 0.72 | 0.4 |
| 5 | 40 | 20 | 10 | 5 | 5 | 10 | 20 | 20 | 40 |
| | | | | | | | gut | Top | |
| 148.3 | 143.8 | 137.65 | 136.15 | 136.05 | 136.05 | 136.05 | 136.25 | 136.35 | 137.16 |
| +0.0 | +5.5 | +0.6 | 2.1 | 2.2 | 2.2 | 2.2 | 1.9 | 1.99 | 0.8 |
| 5 | 40 | 20 | 5 | 5 | 5 | 10 | 20 | 20 | 40 |
| | | | | | | | gut | Top | |
| 148.2 | 143.8 | 139.2 | 135.03 | 134.85 | 134.25 | 134.25 | 134.25 | 135.12 | 136.25 |
| +9.7 | +5.5 | +0.9 | 3.2 | 3.4 | 3.5 | 3.5 | 3.3 | 2.38 | 2.0 |
| 5 | 40 | 20 | 5 | 5 | 10 | 10 | 20 | 20 | 40 |
| | | | | | | | gut | Top | |
| | | | 138.25 | | | | | | |

4+26 = ± 18' Dr. on Rt.

4+12 = 26.7 Rt. = ± 10' Olive

4+00

3+66 = 26.8 Rt. = ± 7" Olive

3+50 = 1' E. of ± 18' Dr. on Rt.

3+42 = 25.5 Rt. = ± 7" Olive

3+20 = Seems like end of U.C. on cb.

2+18 = 25.5 Rt. = ± 8" Olive

2+00 = 1' E. of ± 18' Dr. on Rt.

2+80

2+69 = ± 18' Dr. on Rt.

2+60

2+58.7 = ± Sewer M.H. 10.74 on Rim

2+50 = 26 Rt. = ± 8" Olive

2+40

2+31 = 26 Rt. = ± 8" Olive

2+20 = cb. on Rt.

2+07 = 26 Rt. = ± 7" Olive

Lt.

±

Rt.

156.39 31

| | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|------------|--------|--------|--------|
| 164.0 | 162.61 | 159.31 | 157.41 | 156.01 | 156.01 | 155.71 | 155.81 | 156.51 | 156.21 | 156.71 |
| + 1.1 | 0.3 | 3.6 | 5.5 | 6.9 | 6.9 | 7.0 | 7.1 | 6.40 | 6.7 | 6.2 |
| 55 | 40 | 20 | 10 | 7 | 6.9 | 10 | 20 | 20 | 22 | 40 |
| 163.8 | 162.01 | 158.01 | 157.21 | 155.61 | 155.41 | 155.31 | 155.00 | 155.61 | 156.01 | |
| + 0.9 | 0.9 | 4.9 | 5.7 | 7.3 | 7.5 | 7.6 | 7.85 | 7.3 | 6.9 | |
| 55 | 40 | 20 | 10 | 6 | 7.5 | 10 | 20 | 22 | 40 | |
| | | | | | | | Dr. + gut. | | | 155.18 |
| | | | | | | | | | | 7.73 |
| | | | | | | | | | | 20 |
| | | | | | | | | | | Top |
| 163.2 | 161.31 | 158.61 | 157.21 | 154.61 | 154.41 | 154.31 | 154.12 | 154.81 | 154.81 | 154.81 |
| + 0.3 | 1.6 | 4.3 | 5.7 | 8.3 | 8.5 | 8.6 | 8.79 | 8.1 | 8.1 | 8.1 |
| 55 | 40 | 20 | 10 | 5 | 8.5 | 10 | 20 | 22 | 40 | 40 |
| | | | | | | | Dr. + gut. | | | |
| 162.81 | 160.71 | 158.11 | 157.41 | 153.91 | 153.21 | 153.81 | 153.71 | 154.09 | 154.31 | |
| 0.1 | 2.0 | 4.8 | 5.3 | 9.0 | 9.0 | 9.1 | 9.2 | 8.82 | 8.6 | |
| 55 | 40 | 20 | 10 | 5 | 9.0 | 10 | 20 | 20 | 40 | |
| | | | | | | | gut. | Top | | |
| | | | | | | | | | | 153.10 |
| | | | | | | | | | | 9.81 |
| | | | | | | | | | | 2.0 |
| | | | | | | | | | | Dr. |
| 162.11 | 160.21 | 157.21 | 156.21 | 153.91 | 153.21 | 153.01 | 152.81 | 153.18 | 153.61 | |
| 0.8 | 2.7 | 5.2 | 6.2 | 9.5 | 9.7 | 9.9 | 10.1 | 9.73 | 9.3 | |
| 55 | 40 | 20 | 10 | 5 | 9.7 | 10 | 20 | 20 | 40 | |
| | | | | | | | gut. | Top | | |
| 161.4 | 159.21 | 156.81 | 156.21 | 152.4 | 151.91 | 151.81 | 151.71 | 152.12 | 152.71 | |
| 1.8 | 3.7 | 6.1 | 6.7 | 10.8 | 11.0 | 11.1 | 11.2 | 10.74 | 10.2 | |
| 55 | 40 | 20 | 10 | 5 | 11.0 | 10 | 20 | 20 | 40 | |
| | | | | | | | gut. | Top | | |
| | | | | | | | | | | 150.25 |
| | | | | | | | | | | 11.96 |
| | | | | | | | | | | 2.0 |
| | | | | | | | | | | Top |

162.91

40' E = E = Sewer M.H.

25' E

20' E = w. cb.

18' E. - 10' Lt = end planting + 40' Lt = end Hedge

check B.M. 0.10 Higher than other line
See P. 54 + 68 166.44 2.89 166.54 U.E. 7 Mon. Beryl + Jewell

5 + 18.92 = w.l. Jewell st.

T.P. 11.26 169.43 4.74 158.17

5 + 08.92 = opp. P.C. of 30' Rad. Ret. on Rt.

4 + 75

4 + 69 - 40' Lt. = 2' Hedge - 7' High

4 + 67 - 9' Lt. = Beg Cactus + ice plant - planting

4 + 53 = 18' Dri. on Rt.

4 + 50

4 + 36 - 26.5 Rt. = 10" Olive

Lt. Rt. 32

| | | | | | | | |
|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------------|---------------------------------|---|---|
| 165 ⁶³ 3.8 40 | 164 ⁴³ 5.0 30 | 162 ⁵³ 6.9 20 | 160 ³³ 9.1 10 | 159 ⁰¹ 10.42 on Rim | 158 ⁶³ 10.8 10 | 157 ⁵³ 11.9 20 | 155 ⁸³ 13.4 40 |
| Cor. pave | | | | | | | |
| 165 ⁶³ 3.8 40 | 162 ⁴³ 7.0 20 | 160 ¹³ 9.3 10 | | 158 ²³ 10.5 | 158 ²³ 11.2 10 | 157 ⁴³ 12.0 20 | 155 ⁹³ 13.5 40 |
| Cor. oil | | | | | | | |
| Pave | | | | | | | |
| 166 ³³ 3.1 40 | 163 ²³ 6.2 20 | 161 ⁶³ 7.8 10 | 159 ¹³ 10.3 5 | 158 ²³ 10.7 | 158 ¹³ 11.3 10 | 157 ⁵³ 11.9 20 | 156 ⁰³ 13.4 40 |
| | | | | | | | |
| 166 ⁰³ 3.4 40 | 163 ²³ 6.2 20 | 160 ⁹³ 8.5 9 | 158 ³³ 11.1 5 | 158 ⁰³ 11.4 | 157 ²³ 11.7 10 | 157 ²³ 12.2 21.6 gut. | 156 ²⁴ 11.19 21.6 Top |
| | | | | | | | |
| 166.9 +4.0 55 | 166.9 +3.4 46 | 162 ⁶¹ 0.3 20 | 160 ³¹ 2.6 8 | 158 ¹¹ 4.8 5 | 157 ¹¹ 5.2 | 157 ⁶¹ 5.3 10 | 157 ³¹ 5.6 20 gut |
| | | | | | | | |
| 164.6 +2.3 55 | 163.6 +0.7 40 | 160 ⁴¹ 2.5 20 | 159 ²¹ 3.9 10 | 157 ²¹ 5.7 6 | 157 ¹¹ 5.8 | 156 ⁹¹ 6.0 10 | 156 ⁷¹ 6.2 20 gut. |
| | | | | | | | |
| 164.5 +1.6 55 | 163.3 +0.4 40 | 159 ²¹ 3.0 20 | 158 ²¹ 4.7 9 | 156 ²¹ 6.0 7 | 156 ²¹ 6.2 | 156 ²¹ 6.5 10 | 156 ³¹ 6.6 20 gut. |
| | | | | | | | |
| | | | | | | | 156 ⁸¹ 5.62 20 Top |
| | | | | | | | 157 ⁹¹ 5.0 40 |
| | | | | | | | 157 ⁸¹ 5.1 40 |
| | | | | | | | 6.10 20 Dr. |

162.91

1+04 - 40' Rt. = Beg. 1' Rock + Conc wall

0+85

0+75

0+50 - 36.6 Lt. - end wall

0+30

0+10

0+09 - 24' Rt. = ϕ F.H.

80' E. = E.L. Jewell = 0+00 ahead.

78' E. - 36.3 Lt. = Beg. 1' Rock + Conc. wall

60' E. = E. cb.

Lt

Rt

Rt.

33

14.12

8.14

Top wall

| | | | | | | | | | | | |
|--|--------------------------------|-----------------------------------|----------------------------------|--------------------------------|--------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|
| | 168 ⁵³ 0.8 50 | 167 ⁹³ 2.0 40 | 166 ⁸³ 2.6 25 | 166 ⁰³ 1.7 15 | 167 ¹³ 5.0 6 | 164 ⁰³ 54 | 163 ⁴³ 6.0 15 | 161 ⁹³ 7.5 20 | 160 ⁰³ 9.4 38 | 157 ¹³ 11.7 40 | 156 ⁹³ 13.0 50 |
| | 168 ²³ 1.2 50 | 166 ⁹³ 2.5 40 | 166 ¹³ 3.3 25 | 164 ⁵³ 4.9 10 | 163 ⁵³ 59 | 162 ⁹³ 6.5 15 | 160 ⁸³ 8.6 23 | 159 ³³ 10.1 38 | 157 ⁶³ 11.8 40 | 155 ⁹³ 13.5 50 | |
| | 168 ⁵³ 0.9 40 | 168 ⁶⁴ 0.77 36.6 | 166 ²³ 3.2 36.6 | 165 ⁵³ 3.9 24 | 164 ³³ 5.1 15 | 162 ⁸³ 6.6 5 | 162 ⁵³ 6.9 | 161 ²³ 7.7 15 | 159 ⁰³ 10.4 23 | 157 ¹³ 12.3 40 | 154 ⁹³ 14.5 50 |
| | 168 ⁶³ 0.8 40 | 168 ⁶⁴ 0.79 36.4 | 165 ⁹³ 3.5 36.4 | 165 ⁶³ 3.8 24 | 166 ²³ 3.2 15 | 162 ³³ 7.1 5 | 161 ²³ 7.7 | 160 ⁶³ 8.8 15 | 159 ²³ 10.2 20 | 156 ⁵³ 12.9 40 | 154 ⁶³ 14.8 50 |
| | 168 ³³ 0.9 40 | 168 ⁷⁸ 0.65 36.4 | 166 ⁰³ 3.4 36.4 | 165 ¹³ 4.3 24 | 163 ⁸³ 5.6 15 | 161 ⁴³ 8.0 5 | 161 ⁰³ 8.4 | 160 ²³ 9.2 10 | 159 ⁴³ 10.0 20 | 158 ⁹³ 11.0 25 | 155 ⁴³ 14.0 40 |
| | 167 ¹³ 1.7 40 | 168 ⁶⁸ 0.75 36.3 | 166 ¹³ 3.3 36.3 | 165 ²³ 4.2 20 | 162 ⁸³ 6.6 10 | 160 ²³ 8.5 5 | 160 ⁰³ 8.8 | 159 ⁸³ 9.6 10 | 158 ²³ 10.7 20 | 155 ¹³ 14.3 40 | |
| | 167 ¹³ 2.3 40 | 166 ⁴³ 3.0 30 | 164 ⁷³ 4.7 20 | 162 ²³ 6.7 10 | 159 ⁸³ 9.6 | 159 ³³ 10.1 10 | 158 ²³ 11.2 20 | 156 ²³ 13.2 40 | | | |

169.43

2+45 - 39.71t = Φ 8' Conc. Dr.

2+40

2+35 - 41 Lt. = end wall

2+00

1+99 - 41 Lt. = Beg. 18" Rock + Conc. wall - Rod on 2+00

1+70

1+59 - 12' Lt. = Φ 12" Cactus

1+50 - 40' Rt. = end wall

1+40

1+15

1+12 - 40' Rt. = Φ 4' Conc. walk

Note: House on Rt. Has Basement

| | Lt | | | | | | | | | | Rt | | | | | 34 |
|--|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-----|----|--|----|
| | 16649 | | | | | 16555 | | | | | | | | | | |
| | 2.94 | | | | | 3.84 | | | | | | | | | | |
| | 49.7 | | | | | 39.7 | | | | | | | | | | |
| | Dr. | | | | | Dr. | | | | | | | | | | |
| | 16613 | 16543 | 16393 | 16213 | 16073 | 16053 | 16013 | 15813 | 15653 | 15453 | 15303 | | | | | |
| | 3.3 | 4.0 | 5.5 | 7.3 | 8.7 | 8.9 | 9.3 | 11.3 | 12.9 | 14.9 | 14.4 | | | | | |
| | 50 | 40 | 20 | 10 | 7 | | 12 | 20 | 38 | 40 | 55 | | | | | |
| | 1.07 | | | | | | | | | | | | | | | |
| | 41 | | | | | | | | | | | | | | | |
| | Topwall | | | | | | | | | | | | | | | |
| | 16913 | 16821 | 16723 | 16583 | 16403 | 16253 | 16223 | 16163 | 16093 | 15883 | 15623 | 15492 | | | | |
| | 0.3 | 0.62 | 2.4 | 3.6 | 5.4 | 6.9 | 7.2 | 7.8 | 8.5 | 10.4 | 13.2 | 14.5 | | | | |
| | 50 | 41 | 40 | 20 | 7 | 5 | | 15 | 20 | 40 | 42 | 55 | | | | |
| | Topwall | | | | | | | | | | | | | | | |
| | 16913 | | | | | | | | | | | | | | | |
| | 16713 | | | | | | | | | | | | | | | |
| | 16513 | | | | | | | | | | | | | | | |
| | 16393 | | | | | | | | | | | | | | | |
| | 16333 | | | | | | | | | | | | | | | |
| | 16183 | | | | | | | | | | | | | | | |
| | 16013 | | | | | | | | | | | | | | | |
| | 15803 | | | | | | | | | | | | | | | |
| | 15673 | | | | | | | | | | | | | | | |
| | 10.4 | 0.3 | 2.3 | 4.3 | 5.5 | 6.1 | 7.6 | 9.3 | 11.4 | 12.7 | 15.6 | 16033 | | | | |
| | 50 | 40 | 20 | 10 | | 15 | 20 | 40 | 42 | 55 | | 9.1 | 40 | | | |
| | 16943 | | | | | | | | | | | | | | | |
| | 16792 | | | | | | | | | | | | | | | |
| | 16613 | | | | | | | | | | | | | | | |
| | 16503 | | | | | | | | | | | | | | | |
| | 16423 | | | | | | | | | | | | | | | |
| | 16383 | | | | | | | | | | | | | | | |
| | 16223 | | | | | | | | | | | | | | | |
| | 16103 | | | | | | | | | | | | | | | |
| | 16013 | | | | | | | | | | | | | | | |
| | 16003 | | | | | | | | | | | | | | | |
| | 16023 | | | | | | | | | | | | | | | |
| | 9.3 | 0.0 | 1.5 | 3.3 | 4.4 | 4.6 | 5.6 | 7.2 | 8.4 | 9.3 | 9.4 | 9.4 | 9.4 | 50 | | |
| | 50 | 40 | 20 | 10 | 7 | | 15 | 20 | 30 | 40 | 41 | 50 | | | | |
| | Top | | | | | | | | | | | | | | | |
| | 16913 | | | | | | | | | | | | | | | |
| | 16903 | | | | | | | | | | | | | | | |
| | 16723 | | | | | | | | | | | | | | | |
| | 16753 | | | | | | | | | | | | | | | |
| | 16503 | | | | | | | | | | | | | | | |
| | 16483 | | | | | | | | | | | | | | | |
| | 16413 | | | | | | | | | | | | | | | |
| | 16223 | | | | | | | | | | | | | | | |
| | 16113 | | | | | | | | | | | | | | | |
| | 16033 | | | | | | | | | | | | | | | |
| | 16013 | | | | | | | | | | | | | | | |
| | 15923 | | | | | | | | | | | | | | | |
| | 0.2 | 0.4 | 1.5 | 1.9 | 4.4 | 4.6 | 5.3 | 6.7 | 8.3 | 8.9 | 9.3 | 9.5 | | | | |
| | 50 | 40 | 25 | 15 | 6 | | 15 | 20 | 30 | 40 | 41 | 50 | | | | |
| | Top | | | | | | | | | | | | | | | |
| | 16022 | | | | | | | | | | | | | | | |
| | 16023 | | | | | | | | | | | | | | | |
| | 16022 | | | | | | | | | | | | | | | |
| | 16022 | | | | | | | | | | | | | | | |
| | 8.45 | | | | | | | | | | | | | | | |
| | 40 | | | | | | | | | | | | | | | |
| | Top wall | | | | | | | | | | | | | | | |
| | 9.20 | | | | | | | | | | | | | | | |
| | 40 | | | | | | | | | | | | | | | |
| | Top walk | | | | | | | | | | | | | | | |
| | 9.36 | | | | | | | | | | | | | | | |
| | 60.2 | | | | | | | | | | | | | | | |
| | Top porch | | | | | | | | | | | | | | | |
| | 8.44 | | | | | | | | | | | | | | | |
| | 62.2 | | | | | | | | | | | | | | | |
| | Top floor | | | | | | | | | | | | | | | |
| | 16022 | | | | | | | | | | | | | | | |
| | House (upper) | | | | | | | | | | | | | | | |
| | 169.43 | | | | | | | | | | | | | | | |

4+41 - 26' Rt. = ± 17" Olive

4+40

4+28 = 60' Rt. = ± House

4+22 - 26' Rt. = ± 12" Olive

4+05

4+03 - 26.5' Rt. = ± 12" Olive

3+90

3+87 - 26' Rt. = ± 12" Olive

3+64 - 26' Rt. = ± 8" Olive

3+60

3+49 - 27' Rt. = ± 10" Olive

3+31 - 27' Rt. = ± 10" Olive

3+30

3+11 - 26.5' Rt. = ± 12" Olive

T.P. 12.98 178.12 429 165.14

Note: Prop. owners wish Olive trees Removed.

3+00

2+95 - 28' Rt. = ± 11" Olive

2+70

Lt.

±

Rt.

35

| | | | | | | | | | | | | |
|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|
| $\frac{176.52}{1.6}$ | $\frac{175.22}{2.9}$ | $\frac{171.22}{6.9}$ | $\frac{169.92}{8.2}$ | $\frac{168.82}{9.3}$ | $\frac{167.82}{10.3}$ | $\frac{167.62}{10.5}$ | $\frac{167.92}{10.2}$ | $\frac{166.22}{11.9}$ | $\frac{165.92}{14.3}$ | $\frac{162.02}{16.1}$ | | |
| 50 | 40 | 30 | 20 | 10 | | 7 | 12 | 20 | 40 | 55 | | |
| | | | | | | | | | $\frac{163.92}{16.3}$ | $\frac{163.94}{14.88}$ | | |
| | | | | | | | | | 60 | 60 | | |
| | | | | | | | | | ground | Floor | | |
| $\frac{175.52}{2.6}$ | $\frac{174.12}{4.0}$ | $\frac{172.82}{5.3}$ | $\frac{169.22}{8.7}$ | $\frac{168.12}{10.0}$ | $\frac{167.12}{11.0}$ | $\frac{166.32}{11.9}$ | $\frac{165.82}{12.3}$ | $\frac{166.42}{11.6}$ | $\frac{164.12}{13.7}$ | $\frac{163.92}{14.2}$ | $\frac{162.22}{15.9}$ | $\frac{161.32}{16.8}$ |
| 50 | 43 | 40 | 30 | 20 | 10 | 11.9 | 8 | 12 | 20 | 30 | 40 | 55 |
| $\frac{170.22}{7.2}$ | $\frac{170.22}{7.8}$ | $\frac{168.42}{9.7}$ | $\frac{158.32}{10.8}$ | $\frac{166.42}{11.7}$ | $\frac{165.62}{12.5}$ | $\frac{165.22}{12.9}$ | $\frac{165.22}{12.4}$ | $\frac{164.22}{13.9}$ | $\frac{161.52}{14.6}$ | $\frac{159.82}{18.3}$ | | |
| 50 | 40 | 30 | 20 | 10 | | 8 | 12 | 20 | 40 | 55 | | |
| $\frac{170.22}{7.4}$ | $\frac{169.22}{8.4}$ | $\frac{167.22}{11.1}$ | $\frac{166.42}{11.7}$ | $\frac{165.42}{12.7}$ | $\frac{164.42}{13.7}$ | $\frac{164.22}{13.9}$ | $\frac{164.52}{13.6}$ | $\frac{162.62}{15.5}$ | $\frac{160.62}{17.5}$ | $\frac{157.82}{20.3}$ | | |
| 50 | 40 | 30 | 20 | 10 | | 8 | 15 | 20 | 40 | 55 | | |
| $\frac{167.22}{10.4}$ | $\frac{166.22}{11.2}$ | $\frac{165.42}{12.7}$ | $\frac{165.42}{12.5}$ | $\frac{165.92}{12.2}$ | $\frac{164.12}{14.0}$ | $\frac{163.22}{14.9}$ | $\frac{162.42}{15.7}$ | $\frac{162.22}{15.9}$ | $\frac{161.12}{17.0}$ | $\frac{159.42}{18.7}$ | $\frac{157.22}{20.9}$ | |
| 50 | 40 | 30 | 20 | 15 | 12 | | 8 | 15 | 20 | 40 | 55 | |
| $\frac{168.22}{3.7}$ | $\frac{165.02}{4.4}$ | $\frac{164.12}{5.3}$ | $\frac{163.42}{6.0}$ | $\frac{162.12}{7.3}$ | $\frac{178.12}{7.6}$ | $\frac{161.22}{8.2}$ | $\frac{159.82}{9.5}$ | $\frac{157.82}{11.8}$ | $\frac{155.22}{13.7}$ | | | |
| 50 | 40 | 20 | 12 | 10 | | 10 | 20 | 40 | 55 | | | |
| $\frac{165.52}{3.9}$ | $\frac{163.92}{5.8}$ | $\frac{163.22}{6.2}$ | $\frac{161.22}{7.6}$ | $\frac{160.52}{8.9}$ | $\frac{160.32}{8.9}$ | $\frac{160.32}{9.1}$ | $\frac{159.12}{10.3}$ | $\frac{156.32}{12.9}$ | $\frac{154.52}{14.9}$ | | | |
| 50 | 40 | 20 | 10 | 8 | 8 | 12 | 20 | 40 | 55 | | | |

169.43

61-E - 26' Rt. = ± 8" Olive

60'E - cb. to S.

50'E = E.L. of Kendall to N.

41-E 26' Rt. = ± 8" Olive

40'E = ± To S. + E. cb. to N.

34-E - 22.8' Lt. = ± 36" Euc. Tree

25'E = ± To N.

22'E = 23' Lt. = ± 18" Euc. Tree

20'E = W. cb. to S. - 27' Rt. = ± 12" Olive

10'E = W. cb. to N.

B.M. - N.W. Prop. pipe 1.69 176.43

26.5' Rt. = ± 6" Olive

5 + 00.43 = W.L. Kendall

4+70

4+61 - 26' Rt. = ± 10" Olive

| | | | | | | | | | | |
|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|
| 176 ¹² 2.0 50 | 175 ⁵² 2.5 40 | 173 ¹² 5.0 30 | 173 ¹² 5.0 20 | 172 ⁵² 5.6 10 | 172 ¹² 6.0 | 172 ²² 5.9 10 | 171 ⁵² 6.6 20 | 167 ³² 10.8 40 | | |
| 174 ⁰² 4.1 40 | 173 ⁹² 4.2 25 | 173 ⁵² 4.6 20 | 172 ²² 5.4 10 | 172 ⁴² 5.7 | 172 ⁴² 5.7 10 | 171 ⁵² 6.6 20 | 167 ³² 10.8 40 | | | |
| 174 ⁵² 3.6 40 | 174 ²⁴ 3.4 25 | 173 ²² 4.4 18 | 172 ⁹² 5.2 10 | 172 ⁵² 5.6 | 172 ²³ 5.4 12 | 172 ¹² 6.0 20 | 167 ⁰² 10.5 40 | | | |
| 174 ⁹² 3.2 40 | 175 ⁴² 2.7 25 | 173 ⁸² 4.3 18 | 172 ¹² 5.2 10 | 172 ⁵² 5.6 | 172 ²² 5.4 12 | 171 ⁹² 6.2 20 | 168 ⁰² 10.1 40 | | | |
| 174 ⁵² 3.6 40 | 174 ⁰² 4.1 20 | 172 ⁸² 5.3 10 | 172 ⁴² 5.7 | 172 ²² 5.9 | 172 ⁵² 5.3 12 | 172 ⁰² 6.1 20 | 168 ⁸² 9.3 40 | | | |
| 173 ⁹² 4.2 40 | 173 ³² 4.8 20 | 172 ⁶² 5.5 10 | 172 ¹² 6.0 | 172 ⁰² 6.1 7 | 172 ²² 5.4 12 | 172 ⁴² 5.7 20 | 168 ⁸² 9.3 40 | | | |
| 176 ⁴² 1.7 40 | 172 ⁹² 5.3 27 | 172 ⁶² 5.5 20 | 172 ²² 5.9 10 | 171 ²² 6.4 | 171 ²² 6.4 7 | 172 ⁸² 5.3 12 | 171 ⁸² 6.3 20 | 167 ⁸² 10.3 40 | | |
| 177 ⁰² 0.5 50 | 176 ¹³ 2.0 40 | 173 ⁰² 5.1 30 | 171 ³² 6.8 20 | 170 ⁴² 7.7 10 | 169 ²² 8.4 | 169 ⁴² 8.5 7 | 170 ⁴² 7.7 12 | 169 ⁸² 10.3 20 | 165 ⁸² 12.3 40 | 163 ⁰² 14.5 55 |

178.12

1+68- 20.1 Rt. = 2 Brick walk - 39.9 Rt. = 3 Conc. walk

1+40

1+31- 40.4 Lt. = 1' Conc. Block walk

1+28- 40' Rt. = 3' Conc. walk to E House

1+08- 40' Rt. = 7 Dr. - 2-2 Conc. strips

1+04- 37.1 Lt. = 36" Cypress

1+00

0+71- 37.6 Lt. = 4" Tree

0+56- 60' Rt. = (Being Built) Gar. in House - Conc. floor.

0+50

0+25

0+09- 21.1 Rt. = F.H.

T.P. 58.5 177.62 6.35 171.77 = Top F.H. above

80' E = E.L. Kendall to S. = 0+00 ahead.

Lt.

Rt.

| | | | | | | | | | | | | | | |
|-----------------------------------|-----------------------------------|--------------------------------|--------------------------------|---------------------------------|--------------------------------|----------------------------------|------------------------------------|------------------------------------|----------------------------------|----------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|
| 174 ⁴² 3.2 50 | 173 ¹² 4.5 40 | 170 ²² 7.4 25 | 168 ³² 9.3 20 | 167 ¹² 10.5 10 | 166 ⁴² 11.2 | 166 ³² 11.3 10 | 165 ³² 12.1 20 | 163 ⁶² 14.0 40 | 162 ⁰⁷ 14.8 55 | 163 ¹¹ 14.57 | 163 ⁰⁶ 14.56 | 162 ⁰⁷ 15.55 | 163 ⁰⁷ 15.55 | 163 ¹¹ 14.57 |
| 174 ²⁵ 2.87 53.5 | 173 ²² 4.40 40.4 | | | | | 163 ⁹⁵ 13.67 40 | 162 ³⁵ 14.77 57.7 | 163 ⁰⁴ 13.68 59.7 | 164 ⁴⁸ 13.4 40 | 163 ⁸² 13.80 50 | | | | |
| 174 ⁸² 2.8 50 | 173 ⁹² 3.7 40 | 171 ⁴² 6.2 23 | 170 ¹² 7.5 20 | 169 ¹² 8.5 10 | 168 ³² 9.4 | 167 ⁵² 9.1 10 | 167 ²² 10.4 20 | 165 ⁰² 12.9 40 | 163 ³² 14.3 55 | | | | | |
| | | | | | | | | | | | | | | |
| 175 ⁹² 1.7 50 | 174 ²² 2.9 40 | 171 ⁷² 5.9 20 | 170 ²² 6.8 10 | 170 ³² 7.3 | 169 ⁹² 7.7 10 | 168 ⁵² 9.1 20 | 167 ²² 10.4 30 | 164 ⁷² 12.9 40 | 162 ²¹ 15.41 60 | | | | | |
| | | | | | | | | | | | | | | |
| 176 ⁵² 1.1 50 | 175 ¹² 2.5 40 | 172 ⁰² 5.6 20 | 171 ⁴² 6.2 10 | 171 ³² 6.3 | 170 ⁷² 6.9 10 | 169 ⁰² 8.6 20 | 168 ²² 9.4 30 | 165 ³² 12.3 40 | 163 ¹² 14.5 55 | | | | | |
| | | | | | | | | | | | | | | |
| 176 ⁴² 1.7 50 | 175 ¹² 3.0 40 | 173 ⁴² 4.7 35 | 172 ⁵² 5.6 20 | 172 ¹² 6.0 10 | 171 ²² 6.4 | 170 ⁷² 7.4 10 | 169 ⁵² 8.6 20 | 167 ²² 10.9 40 | | | | | | |

178.12

4+50

4+33 - 38.7 Lt. = ± 2.5' Conc. Steps

4+27 - 24.8' Rt. = ± 20" Euc.

4+20

3+90

3+89 - 24.5' Rt. = ± 36" Euc.

3+84 65' Lt. = ± Double Gar. - Conc. floor.

3+72 - 39' Rt. = ± 3' Conc. Walk to + House

3+67 - 24.6' Rt. = ± 20" Euc.

3+60

3+30

3+15 - 26' Lt. = ± P. pole # P.I. 866

3+09 - 24' Rt. = ± 18" Euc.

3+00

| | Lt. | | | | Rt. | | | | 39 |
|-------------------|-----------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | 166 ²⁹ | 164 ⁸⁹ | 164 ⁴⁹ | 164 ³⁹ | 164 ³⁹ | 165 ⁰⁹ | 164 ⁵⁹ | 162 ⁸⁹ | 162 ³⁹ |
| + 1.2 | 2.5 | 1.5 | 4.9 | 5.0 | 5.0 | 4.3 | 4.8 | 6.5 | 7.0 |
| 50 | 40 | 20 | 10 | 6 | 8 | 20 | 40 | 50 | |
| | + 0.169 ⁵⁷ | | | | | | | | |
| | 46.3 | 18.5 | | | | | | | |
| | Top step | 38.7 | | | | | | | |
| | | | 167 ⁵⁴ | | | | | | |
| 169 ⁸⁹ | 167 ⁴⁹ | 165 ¹⁹ | 164 ⁷⁹ | 164 ⁵⁹ | 164 ⁶⁹ | 164 ³⁹ | 162 ⁹⁹ | 162 ⁷⁹ | |
| 0.5 | 1.9 | 4.2 | 4.6 | 4.8 | 4.7 | 5.0 | 4.4 | 6.6 | |
| 50 | 40 | 20 | 10 | 10 | 10 | 20 | 40 | 50 | |
| | 169 ²⁹ | 168 ¹⁹ | 166 ⁷⁹ | 164 ³⁹ | 169 ⁰⁹ | 163 ⁷⁹ | 164 ⁰⁹ | 163 ⁸⁹ | 162 ⁴⁹ |
| 0.1 | 1.2 | 2.6 | 5.0 | 5.3 | 5.6 | 5.3 | 5.5 | 6.9 | 7.1 |
| 50 | 40 | 25 | 20 | 10 | 10 | 20 | 40 | 50 | |
| | + 1.2 | | | | | | | | |
| | 6.5 | | | | | | | | |
| | floor | | | | | | | | |
| | | | | | | | 162 ⁰¹ | 161 ³⁴ | 162 ³⁴ |
| | | | | | | | 7.38 | 7.55 | 7.05 |
| | | | | | | | 39 | 59.3 | 63 |
| | | | | | | | walk | walk at porch | floor house |
| 169 ⁰⁹ | 165 ⁹⁹ | 164 ⁴⁹ | 163 ¹⁹ | 163 ⁰⁹ | 162 ⁸⁹ | 162 ⁹⁹ | 162 ⁵⁹ | 161 ⁸⁹ | 141 ⁸⁹ |
| 0.3 | 3.4 | 4.9 | 6.2 | 6.3 | 6.5 | 6.4 | 6.8 | 7.5 | 7.5 |
| 50 | 40 | 20 | 19 | 10 | 5 | 10 | 20 | 40 | 50 |
| | 167 ⁹⁹ | 165 ³⁹ | 163 ⁸⁹ | 162 ⁴⁹ | 162 ²⁹ | 162 ⁰⁹ | 161 ¹⁹ | 160 ⁴⁹ | 160 ¹⁹ |
| 1.4 | 4.0 | 5.4 | 6.9 | 7.1 | 7.1 | 7.3 | 8.2 | 8.9 | 9.2 |
| 50 | 40 | 22 | 20 | 10 | 10 | 10 | 20 | 40 | 50 |
| | 167 ³⁹ | 164 ⁰⁹ | 163 ²⁹ | 162 ³⁹ | 162 ²⁹ | 162 ¹⁹ | 160 ⁹⁹ | 160 ¹⁹ | 159 ⁷⁹ |
| 2.0 | 5.3 | 6.1 | 6.8 | 7.0 | 7.1 | 7.2 | 8.4 | 9.2 | 9.6 |
| 50 | 40 | 21 | 20 | 10 | 10 | 10 | 20 | 40 | 50 |

169 39

20' E. Cont.

20' E. = w. cb.

Rods on Midpoints of 10' Rad. Ret.

10' E. = opp. PC. of 10' Rad. Ret.

4+99.55 = w.l. Lamont = edge Conc. Pav

I.P. 5.42 167.56 7.25 162.14

4+94

4+70

4+64 - 24' Rt. = ± 8' Olive

4+54 - 23' Lt. = ± Guy Pole " P 1886

| | | | | | | | | | | | | | |
|---|---|---|---|---|--|---|---|---|---|--|---|-----------------------------------|--------------------------------|
| 167 ²⁸ 0.18 100 Top | 166 ⁷⁹ 0.82 100 gut. | Lt 164 ⁴² 3.34 65 Top | 163 ⁶⁴ 3.92 65 gut. | 158 ⁵⁶ 9.00 65 gut. | 159 ⁴⁶ Rt. 8.40 65 Top | 156 ²³ 11.33 100 gut. | 40 156 ⁸² 100 Top | | | | | | |
| 161 ⁹² 5.59 40 Top | 161 ⁵⁰ 6.06 40 gut. | 161 ⁹¹ 5.65 30 Top PC. | 161 ²³ 6.34 30 gut. | 161 ⁰³ 4.53 20 | 160 ⁸² 6.74 20 | 160 ⁵² 7.04 20 | 160 ³⁷ 7.19 30 gut. | 161 ⁰³ 6.51 30 Top PC. | 160 ⁰⁵ 7.51 40 gut. | 40 160 ⁹⁶ 40 Top | | | |
| N.W. Ret. | 161 ⁸⁷ 5.69 Top | 161 ²² 6.34 gut. | | | | 160 ⁴⁵ 7.11 gut. | | 161 ¹³ 6.43 Top | S.W. Ret. | | | | |
| | 161 ⁹⁰ 5.66 20 Top PC. | 161 ²⁰ 6.36 20 gut. | 161 ²² 6.34 10 | 161 ¹² 6.44 | 160 ²⁹ 6.67 10 | 160 ²⁶ 7.00 20 gut. | 161 ¹⁴ 6.42 20 Top PC. | | | | | | |
| | 162 ⁴³ 5.13 40 | 162 ²⁷ 5.29 36.5 walk | 162 ²² 5.34 31 | 161 ⁹³ 5.63 20 Top | 161 ²⁷ 6.29 20 gut. | 161 ³⁴ 6.22 10 | 161 ³² 6.24 | 160 ⁹⁵ 6.61 10 | 160 ⁵⁸ 6.98 20 gut. | 161 ²⁰ 6.36 20 Top | 161 ²³ 6.33 31 walk | 161 ²⁵ 6.31 36.3 | 161 ⁷⁶ 5.8 40 |
| | + 170.6 | 170.6 1.2 50 | 164 ⁴⁹ 4.9 40 | 162 ⁰⁹ 7.3 20 | 161 ⁰² 7.4 10 | 161 ⁵⁹ 7.8 | 167 ⁵⁶ 7.8 | 161 ⁵⁹ 7.8 8 | 164 ⁰⁹ 5.3 11 | 163 ⁴⁹ 5.9 20 | 162 ⁶⁹ 6.7 40 | 161 ⁶⁹ 7.7 50 | |
| | + 170.6 | 164 ⁴⁹ 2.9 40 | 163 ⁹⁹ 5.4 20 | 163 ³⁹ 5.8 10 | 163 ³⁹ 6.0 | 163 ⁴⁹ 5.9 7 | 164 ⁵⁹ 4.8 9 | 164 ⁵⁹ 4.8 20 | 162 ⁶⁹ 6.7 40 | 161 ⁸⁹ 7.5 50 | | | |

169.39

Beryl

Lt.

£

Rt.

41

should be .10 High



P.25

| | | | | |
|-----------------------|-----------|--------|--------|----------------------|
| Check BM - S.W. 7' ct | Chacodony | 6.24 | 126.11 | 126.00 |
| 1.61 | 132.35 | 12.89 | 130.74 | |
| 1.08 | 143.63 | 12.58 | 142.58 | sw. 7' low + lamont. |
| T.P. | 0.39 | 155.13 | 12.82 | 154.74 |

40' E. = £ - end.

$\begin{array}{r} 167.18 \\ 0.38 \\ \hline 100 \end{array}$

$\begin{array}{r} 164.07 \\ 3.49 \\ \hline 65 \end{array}$

$\begin{array}{r} 162.09 \\ 5.47 \\ \hline 40 \end{array}$

$\begin{array}{r} 161.31 \\ 6.25 \\ \hline 20 \end{array}$

$\begin{array}{r} 160.93 \\ 6.63 \\ \hline 20 \end{array}$

on M.H.

$\begin{array}{r} 160.73 \\ 6.83 \\ \hline 20 \end{array}$

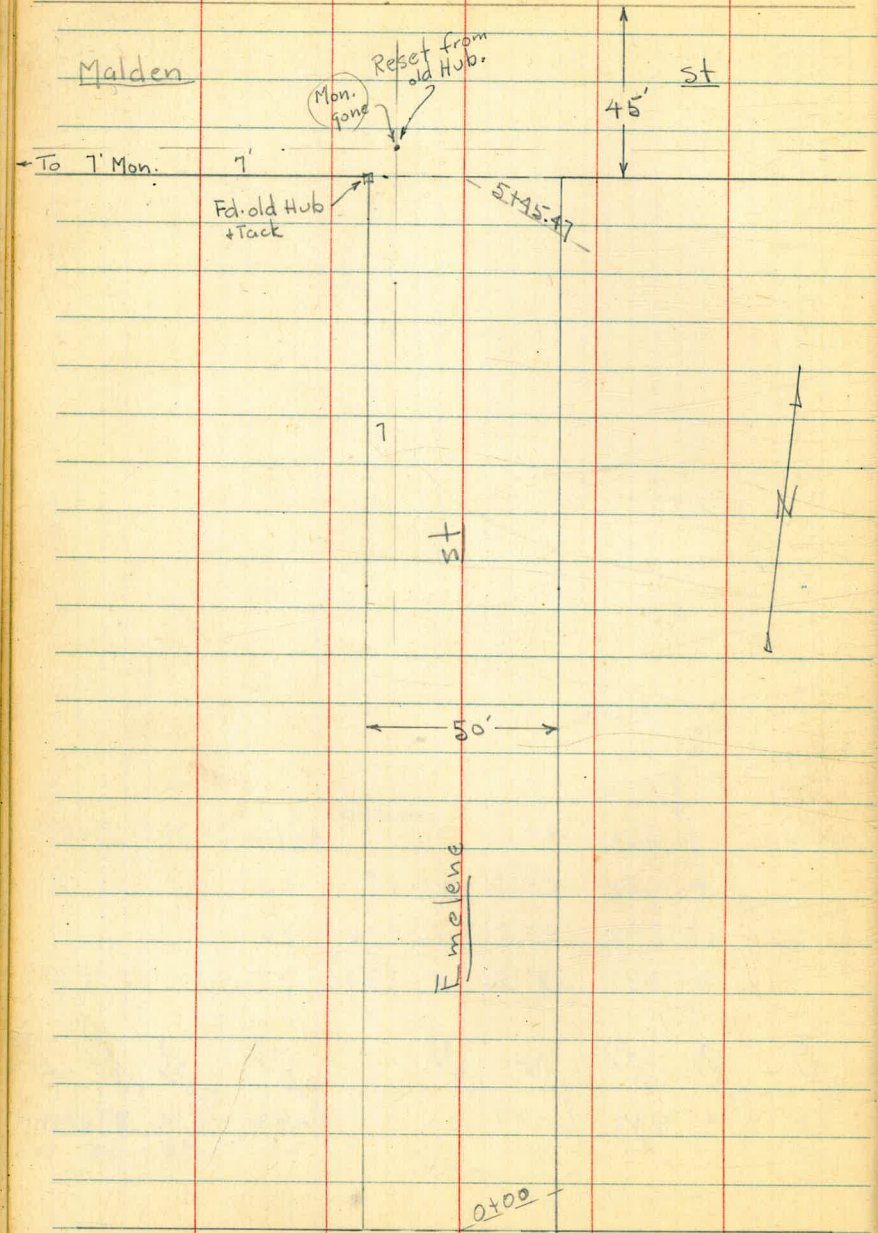
$\begin{array}{r} 160.24 \\ 7.32 \\ \hline 40 \end{array}$

$\begin{array}{r} 158.80 \\ 8.76 \\ \hline 65 \end{array}$

$\begin{array}{r} 156.42 \\ 11.14 \\ \hline 100 \end{array}$

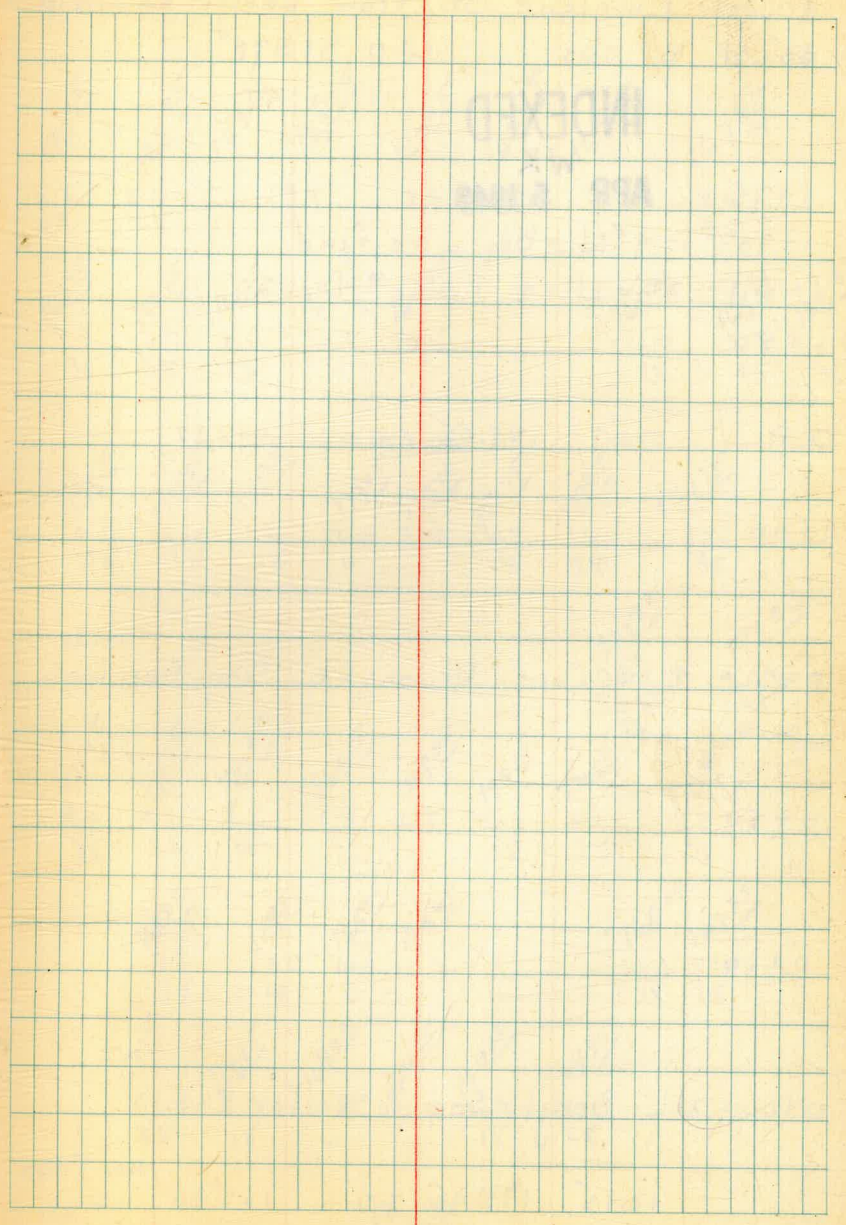
167.56

Malden



Beryl

st



X-Sect. Emelene St. from Beryl to Malden
 50' st. 10' cbs. - W.O. 31371

INDEXED

11-10-47
 7.0.

WK
 APR 5 1949

1+75
 1+70- 12.9 Lt. = Beg. wire fence
 1+69- 22.6 Lt. = ± P pole # None
 1+50

T.P. 12.67 188.05 0.07 175.38

1+00

0+72 = ± 8' Conc. Dr. on Rt. - Sing. Gar. Conc. floor

0+50

0+10

0+00 = N.L. Beryl - See P. 38 for Int.

10.15 175.45 165.30

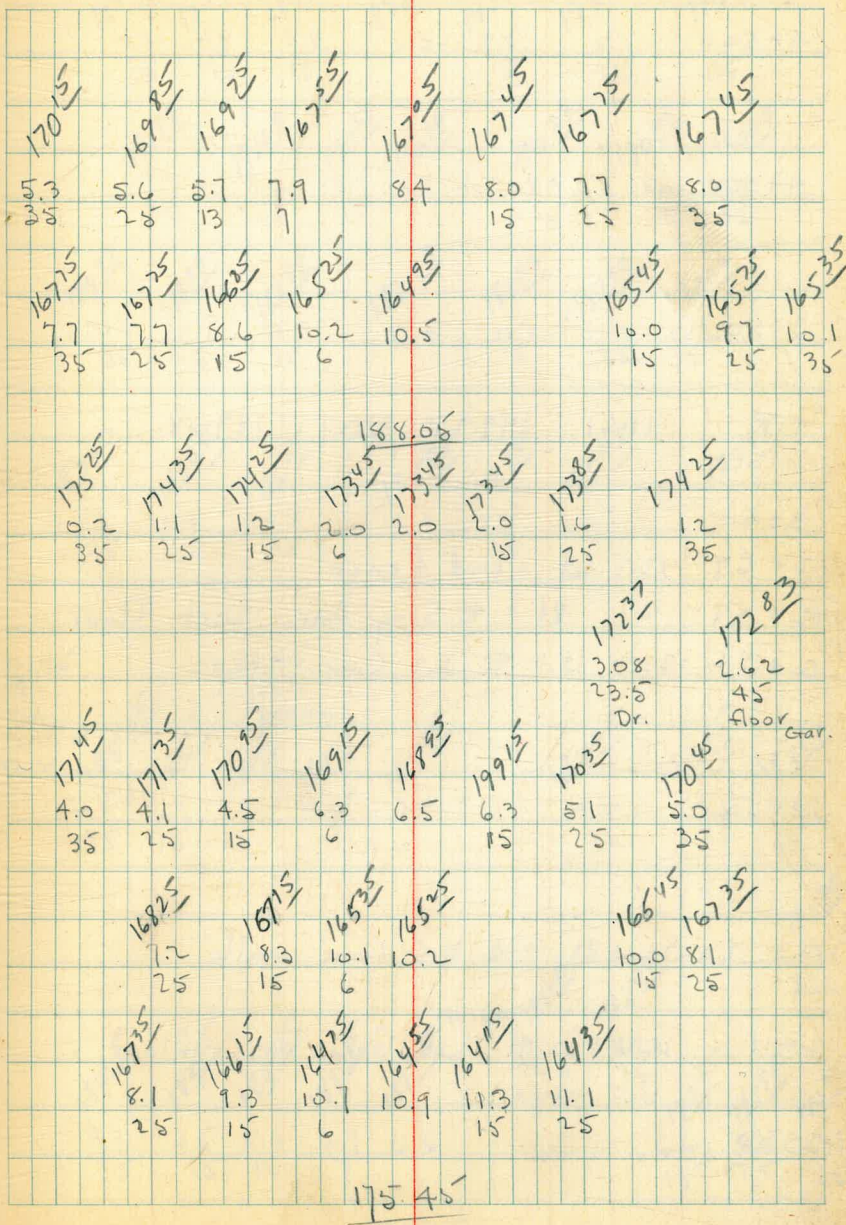
N.W. 7' Mon
 P. 38

Lt.

±

Rt.

43



4+50

4+00

3+50

T.P. 11.61 199.29 0.37 187.68

3+00

2+69 - 13.3 Lt = end fence

2+58 - 27 Rt. = Sing Gar. - Dirt floor

2+52 - 32.3 Lt. = 5.2 Conc. steps

2+50

2+ 20-26.6 Rt. = 3.5' Conc walk

2+11 26.6 Rt. = apron Dub. Gar. - Conc. floor

2+00

| | | | | | | | | |
|---|---------------------|---------------------|---------------------|------------------------|---------------------|-----------------------------|-----------------------------|-------------------------------|
| | 19499 4.3 35 | 19439 4.9 25 | 19349 5.8 15 | 19299 6.3 | 19349 5.8 15 | 19359 5.7 25 | 19329 6.0 35 | |
| | 19199 7.3 35 | 19169 7.6 25 | 19059 8.7 15 | 19039 8.9 | 19089 8.7 15 | 19069 8.6 25 | 19049 8.8 35 | |
| | 18949 10.8 35 | 18839 10.9 25 | 18789 11.4 15 | 18789 11.4 | 18809 11.2 15 | 18799 11.3 25 | 18809 11.2 35 | |
| | 18760 11 35 | 18665 14 25 | 18625 1.8 15 | 199.29 18595 2.1 | 18615 1.9 15 | 18595 2.1 25 | 18555 2.5 35 | |
| 0.45 41 Top Porch at House | 18555 2.5 35 | 18515 2.9 25 | 18445 3.2 15 | 18405 4.0 7 | 18415 3.9 | 18405 4.0 15 | 18395 4.1 25 | 18365 4.4 35 |
| | 18325 4.3 35 | 18355 4.5 25 | 18305 5.0 12 | 18135 6.7 7 | 18145 6.6 | 18120 6.1 15 apron | 18206 5.9 29 floor | 18145 6.6 15 |
| | | | | | | | | 18120 6.15 26.6 walk |
| | | | | | | | | 18155 6.5 25 |
| | | | | | | | | 18125 6.8 35 |

188.05

| | | | |
|---------------------|--------|--------|--------|
| check Starting B.M. | 12.68 | 165.31 | 165.30 |
| 0.18 | 177.99 | 13.14 | 177.81 |
| 0.31 | 190.95 | 12.76 | 190.64 |
| T.P. | 7.35 | 203.40 | 11.27 |
| | | | 196.05 |

5 + 45.47 = S.L. Malden = end.

| | | | | |
|------|------|--------|------|--------|
| T.P. | 9.77 | 207.32 | 1.74 | 197.55 |
|------|------|--------|------|--------|

5 + 00

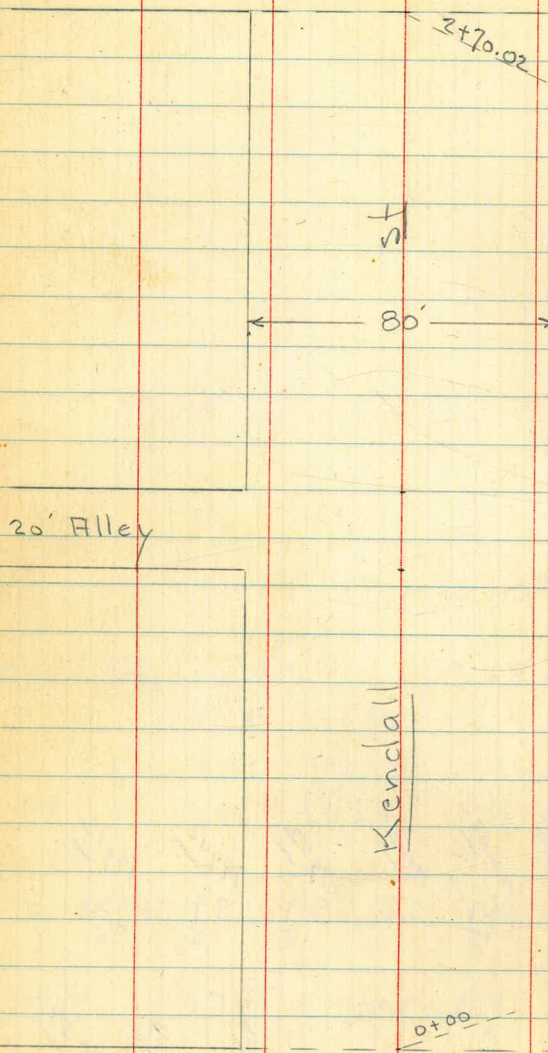
| | | | | | | |
|-------|-------|-------|--------|-------|-------|-------|
| 20312 | 20212 | 20082 | 19962 | 19942 | 19902 | 19912 |
| 7.2 | 5.2 | 6.7 | 7.7 | 7.9 | 7.9 | 8.2 |
| 35 | 25 | 15 | | 15 | 25 | 35 |
| 19849 | 19799 | 19659 | 207.32 | 19629 | 19609 | 19589 |
| 0.8 | 1.3 | 2.7 | 3.0 | 2.7 | 3.4 | 3.4 |
| 35 | 25 | 15 | | 15 | 25 | 35 |

199.29

Law

See B. 1775 - P 10?
for Int.

St



Chalcedony

See P. 21 + 22 for Int.

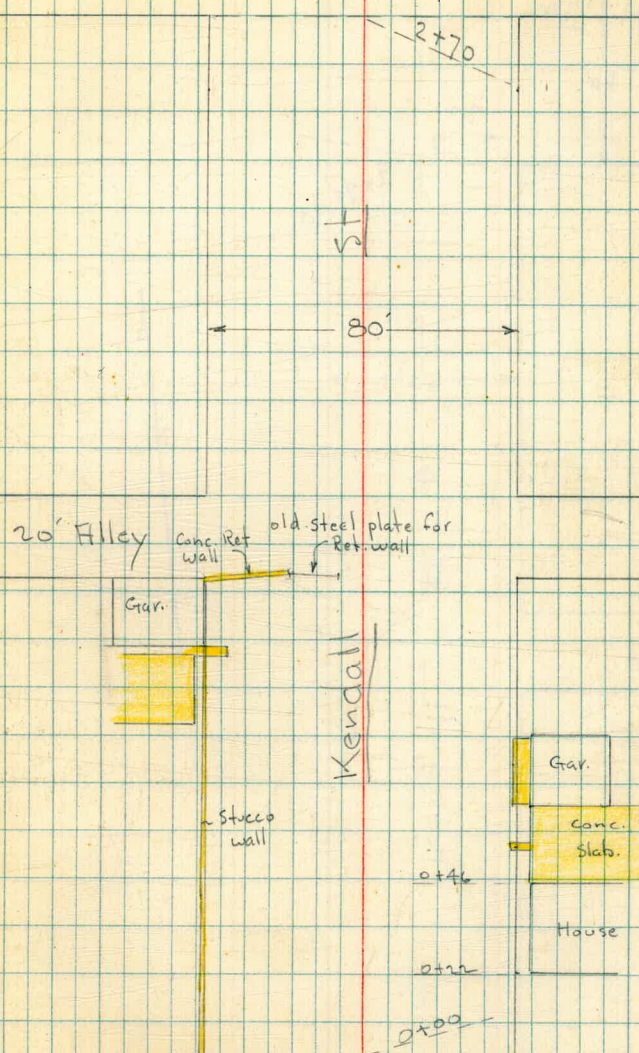
St

Beryl

See P. 36 for Int.

St

46



Law

St

Collingwood Dr.

60'

Mon.

7'

2799.03

2'
50'

A

st

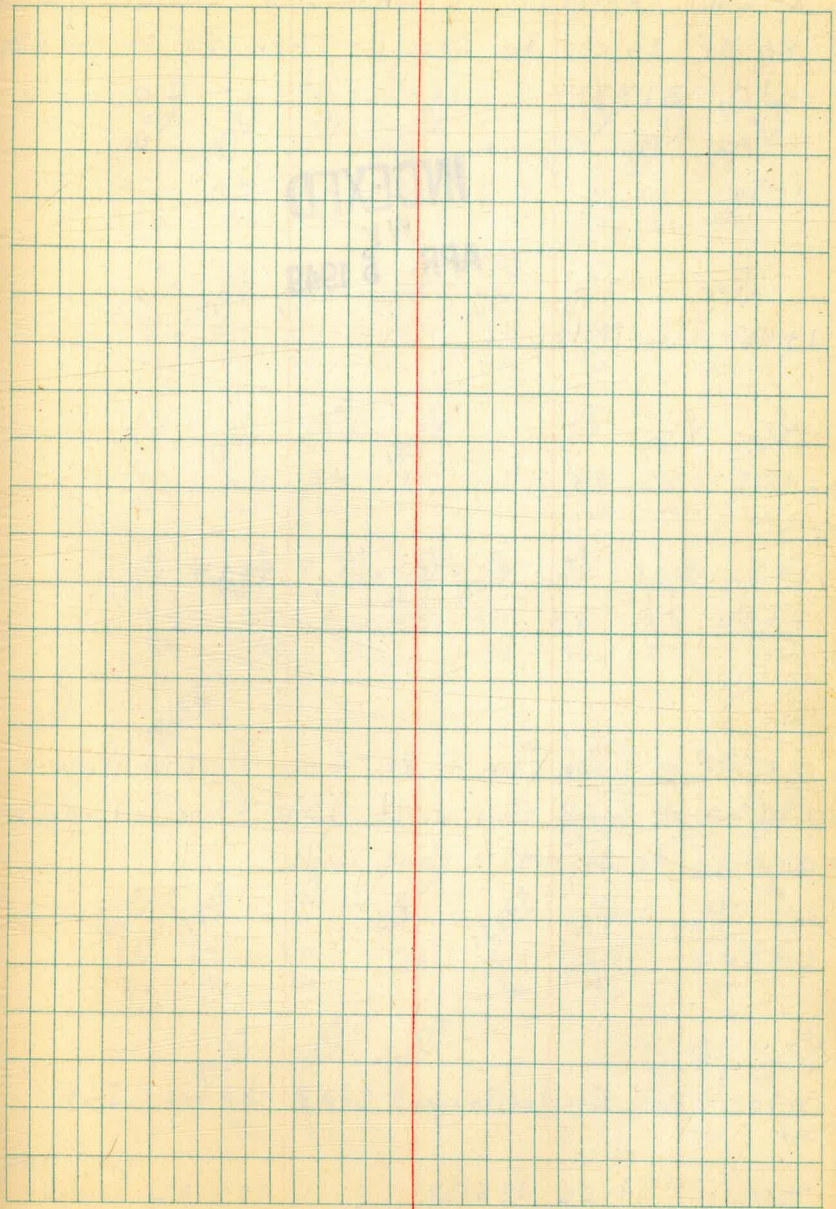
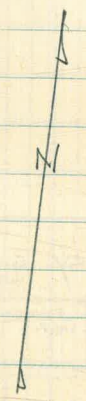
20' Alley

Kendall

04.00

Beryl

st



X- Sect. Kendall - Chalcedony to Collingwood
 80' st. - 20' cbs. to Beryl - Then 50' st. + 10' cbs.
 W.O. 31371 11-12-47 - 70.

1+90

INDEXED
 WK
 APR 5 1949

1+45 = N.L. Alley

1+25 = S.L. 20' Alley

1+22-31.1 Lt. = \pm P. pole # P 4824

1+00

0+70 = \pm Doub. Gar. on Rt. - Conc. floor + Apron

0+56 = \pm Sing. Gar. on Lt. - Conc. floor + Apron

0+54 = 40' Rt. = \pm 2' Conc. walk

0+50

0+00 = N.L. Chalcedony - See P. 21 for Int.

B.M. 12.55 135.37

122.82
 SW 7' Mon
 Kendall +
 Chalcedony
 P. 21

Lt. = W. \pm

Rt. = E 48

| | | | | | | |
|--|--|--------------------------------|--------------------------|--------------------------------|--|--|
| 130 ⁶⁷ 4.7 50 | 130 ⁹⁷ 4.4 40 | 131 ⁹⁷ 3.4 20 | 132 ³⁷ 3.0 | 133 ⁵⁷ 1.8 20 | 134 ²⁷ 1.1 40 | 134 ³⁷ 1.0 50 |
| 129 ⁷⁷ 5.6 50 | 129 ⁹⁷ 5.4 40 | 130 ⁵⁷ 4.7 20 | 131 ⁰⁷ 4.3 | 132 ³⁷ 3.0 20 | 132 ⁹⁷ 2.4 40 | 133 ⁵⁷ 2.0 50 |
| 129 ⁷⁷ 6.6 50 | 129 ⁹⁷ 6.2 40 | 129 ⁹⁷ 5.4 20 | 130 ⁴⁷ 4.9 | 131 ⁵⁷ 3.8 20 | 132 ⁰⁷ 3.3 40 | 132 ⁰⁷ 3.3 50 |
| 128 ⁰⁷ 7.3 50 | 128 ⁶⁷ 6.7 40 | 129 ¹⁷ 6.2 20 | 129 ³⁷ 5.5 | 130 ⁴⁷ 4.9 20 | 130 ⁸⁷ 4.5 40 | 131 ⁰⁷ 4.3 50 |
| 130 ⁸⁵ 4.52 45 floor | 130 ⁵² 4.55 40 apron | | | | 127 ¹¹ 8.26 38.7 apron | 127 ²⁷ 8.10 44.7 floor |
| 126 ⁷⁷ 8.6 50 | 127 ⁰⁷ 8.3 40 | 127 ³⁷ 8.0 20 | 128 ²⁷ 7.1 | 128 ⁶⁷ 6.7 20 | 129 ⁹⁷ 5.4 40 | 130 ³⁷ 5.0 50 |
| | 125 ⁵⁷ 9.8 40 | 125 ⁹⁷ 9.4 20 | 126 ³⁷ 9.0 | | | 126 ⁸⁷ 8.5 20 |
| | | | | | | 127 ⁵⁷ 7.8 40 |

135.37

1+28-31.1 Lt = ± P. pole # P. 4874
 1+27- 18.5" Lt = E end 10" Ret. wall - ground to top
 top of wall

10" Conc. Retaining wall - ground on N. side to
 1+25 = S.L. 20' Alley - + N. end Gar. + w. end of

1+07 = S. end Doub. Gar. on Lt. - Conc. floor

1+05 = 34' Lt. = ± 3.5" Conc. walk

1+03 = 40' Lt. = end wall

1+00

T.P. 13.21 159.96 0.44 146.75

0+83 = N. edge Gar. Apron

0+74 = ± Doub. Gar. on Rt. - Conc. floor + Apron

0+64 = 32.3 Lt. = ± 12" - Abasynian Kumquat Tree

0+59 = 32.8 Lt. = ± Guy Pole

Lt.

±

Rt. 50

| | | | | | | | | | |
|---|--------------------------------|--------------------------|-------------------------|--------------|--------------|-----------------------|------------------------|-----------------------|--------------|
| <u>14986</u> | <u>15026</u> | <u>15137</u> | <u>15096</u> | <u>14956</u> | <u>14966</u> | <u>15016</u> | <u>15166</u> | <u>15216</u> | <u>15226</u> |
| 10.1 .50 | 9.7 40 | 8.59 18.5 Top wall | 9.0 7 | 10.4 | 10.3 10 | 9.8 20 | 8.3 30 | 7.8 40 | 7.7 50 |
| <u>15080</u> | <u>14931</u> | <u>14916</u> | <u>14896</u> | <u>14976</u> | <u>14936</u> | <u>15006</u> | <u>15136</u> | <u>15106</u> | <u>15116</u> |
| 9.36 40.2 Top wall | 12.65 40.2 floor Gar. | 11.8 20 | 11.0 10 | 10.7 | 10.6 10 | 9.9 20 | 8.6 30 | 8.9 40 | 8.8 50 |
| | | | <u>14728</u> | | | | | | |
| | | | 12.68 40.2 floor. | | | | | | |
| <u>14766</u> | <u>14675</u> | | | | | | | | |
| 13.30 42 walk | 13.21 34' | | | | | | | | |
| <u>14612</u> | <u>14606</u> | <u>14666</u> | | | | | | | |
| 13.84 50 on Conc. Stab. Behind wall | 13.9 40 along wall | 13.3 20 | 13.3 | 13.1 20 | 11.3 30 | 10.7 40 | 10.7 50 | | |
| | | | <u>159.96</u> | | | | | | |
| <u>14449</u> | <u>14449</u> | <u>14569</u> | <u>14539</u> | <u>14509</u> | <u>14529</u> | <u>14639</u> | <u>14641</u> | <u>14624</u> | |
| 2.7 50 | 2.7 40 | 1.5 20 | 1.8 | 2.1 10 | 1.9 20 | 0.8 30 | 0.78 39.2 apron | 0.45 43.2 floor | |
| | | | | | | <u>14639</u> | <u>14624</u> | | |
| | | | | | | 0.80 39.2 apron | 0.45 43.2 floor. | | |

147.19

0+10

0+00 - N.L. Beryl
See P. 36 for Int.

T.P. 12.15 183.83 0.40 171.68

2+70.00 = S.L. Beryl

2+70 - 21.8 Lt = ϕ P. pole # H 4898

2+30 - New House under Const. on Rt. - Conc. floor
Kendall - Beryl lower line
check B.M. Top F.H. S.E. 0.40 171.68 171.77
P.37

T.P. 12.70 172.08 0.58 159.38

1+90 -

1+45 - N.L. Alley

Gas Co. M.H.

1+41.5 - 10.5 Lt = ϕ 2' x 2' 8.30 on Rim

1+35 = ϕ Sewer M.H. 9.25 on Rim

Lt.

ϕ

Rt.

51

177⁵³
6.3
25

174⁸³
9.0
13

175⁰³
8.8

174⁸³
9.0
15

176⁶³
7.2
25

176³³
7.5
25

173⁶³
10.2
15

174⁸³
9.0

174⁴³
9.4
15

174⁰³
9.8
25

167⁵⁸
4.5
40

168²⁸
3.3
20

183.83
167⁵⁸
4.5

167¹⁸
4.9
20

166⁸⁸
5.2
40

161³⁸
10.7
50

161⁸⁸
10.2
40

162⁰⁸
10.0
20

162³⁸
9.7

162²⁸
9.8
10

162⁴⁸
9.6
20

163¹⁸
8.9
40

162¹⁰
9.98

59.8
conc floor
House

156⁴⁶
3.3
50

156²⁶
3.2
40

157³⁶
2.6
20

172.08
157⁵⁶
2.4

157⁴⁶
2.5
10

158²⁶
1.7
20

158⁵⁶
1.4
40

158¹⁶
1.1
50

150⁹⁶
9.5
50

150²⁶
9.2
40

151⁹⁶
8.5
20

152⁰⁶
7.9
10

151⁹⁶
8.0

152⁴⁶
7.5
10

153⁰⁶
6.9
20

153⁹⁶
6.0
40

154³⁶
5.6
50

159.96

1+70
 1+65 - 23.4 Lt. = \pm 30" Cypress
 1+61 - 23.6 Lt. = \pm 18" Cypress Tree
 1+45 = N.L. Alley - 24.5 Lt. = Beg. board fence
 C. M.H.
 1+38 - 9.5 Lt. = \pm 2'x2' Gas 10.33
 1+35 = \pm Sewer M.H. 10.49 on Rim
 1+25 = S.L. 20' Alley on Lt.
 1+24 - 45.4 Rt. = \pm Doub. Gar. - Conc. floor.
 1+24 - 16.7 Lt. = \pm P. pole # P 4924
 T.P.
 1+06 - 11.36 195.09 0.10 183.73
 1+00 19' Rt. = end wly. Hedge
 0+86.5 = N. end apron
 0+80
 Gar. - Conc floor
 0+69.5 - 15.9 Lt. = S. end Conc. apron to Doub.
 0+40
 0+25 - 21' Rt. = wly. Large tree Hedge

| | | | | | | | | |
|---------------------------------------|-------------------------------|---------------------|---------------------|-----------------------|--------------------|------------------------|---------------------|-------------------------------|
| 18969 5.4 35 | 18992 Lt. 5.1 25 | 18909 6.0 15 | 18809 7.0 10 | 18839 6.7 15 | 18819 6.9 15 | 18939 Rt. 5.7 15 | 18989 5.2 25 | 19039 4.7 35 |
| 18509 9.6 35 | 18589 9.2 25 | 18529 9.3 15 | 18539 9.7 10 | 18559 9.5 15 | 18569 9.4 10 | 18619 8.9 15 | 18649 8.6 25 | 18699 8.6 35 |
| 17539 10.7 35 | 17559 10.5 25 | 17529 10.8 15 | 18329 11.8 10 | 18359 11.5 15 | | 18409 11.0 15 | 18459 10.5 25 | 18519 9.9 35 |
| | | | | | | | | 18514 9.5 45.4 floor |
| 18293 0.9 35 | 18253 1.3 25 | 18193 1.9 15 | 18113 2.7 10 | 19509 18193 2.4 | 18123 2.1 15 | 18263 1.2 25 | 18243 1.2 35 | |
| 18077 3.06 27.7 = floor. | 18027 3.56 15.9 = apron | | | | | | | |
| 18059 3.24 40 on Conc. | 18015 3.68 15.9 edge | 17923 4.1 10 | 18003 3.8 | 18023 3.8 15 | 18083 3.0 25 | 19083 3.0 35 | | |
| 18022 3.11 27.7 = floor Gar. | 17986 3.97 15.9 = apron | | | | | | | |
| 17903 4.8 35 | 17903 4.8 25 | 17813 5.7 15 | 17623 7.1 10 | 17703 6.8 | 17713 6.7 15 | 17833 5.5 25 | 17823 5.6 35 | |
| 183.83 | | | | | | | | |

+2 Sewer M.H.
30' N. = \pm Collingwood 3.36 on Rim

2+99.03 = S.L. Collingwood - 24' Lt. = end fence

2+93 - 16.2 Lt. = \pm P. pole # P 4948

2+85 - 24' Lt. = \pm 26" Cypress

2+60 = \pm 9' Conc. Dr. on Rt.

2+48 - 22.4 Lt. = \pm 5' Conc. walk

T.P. 6.35 200.89 0.55 194.54

2+45.5 - 23.8 Lt. = end of board + beg picket fence
2+30

2+24 - 27' Rt. = \pm 5' Conc. walk

2+00

| Lt. | | ± | | Rt. | | 53 | | |
|--|---|--------------------------------|--------------------------------|--------------------------------|--|--------------------------------|--|-----------------------------------|
| 1988 ⁹ 2.0 35 | 1985 ⁹ 2.3 25 | 1979 ⁹ 2.9 15 | 1976 ⁹ 3.2 | 1976 ⁹ 3.2 15 | 1969 ⁹ 3.9 25 | 1963 ⁹ 4.5 35 | | |
| 1975 ⁹ 3.3 35 | 1974 ⁹ 3.4 25 | 1970 ⁹ 3.8 15 | 1962 ⁹ 4.6 10 | 1960 ⁹ 4.8 10 | 1960 ⁹ 4.8 10 | 1961 ⁹ 4.7 15 | 1952 ⁹ 5.1 25 | 1951 ⁹ 5.7 35 |
| 1954 ⁹ 5.4 35 | 1945 ⁹ 6.3 25 | 1945 ⁹ 6.3 15 | 1944 ⁹ 6.4 10 | 1942 ⁹ 6.1 | 1946 ⁹ 6.2 10 | 1942 ⁹ 6.1 15 | 1944 ⁵ 6.44 25.7 Dr. | 1944 ⁰ 6.49 35.7 |
| 1945 ³ 6.36 27.9 at step | 1940 ² 6.82 22.4 walk | 200.89 | | | | | | |
| 1936 ⁹ 1.4 35 | 1934 ⁹ 1.6 25 | 1932 ⁹ 1.5 15 | 1922 ⁹ 2.1 10 | 1932 ⁹ 1.7 | 1932 ⁹ 1.8 10 | 1934 ⁹ 1.6 15 | 1941 ⁹ 0.9 25 | 1941 ⁹ 0.9 35 |
| 1915 ⁹ 3.5 35 | 1916 ⁹ 3.4 25 | 1912 ⁹ 3.7 15 | 1902 ⁹ 4.1 10 | 1912 ⁹ 3.7 | 1912 ⁹ 3.7 13 | 1922 ⁹ 3.0 15 | 1925 ⁹ 2.5 25 | 1922 ⁹ 2.2 35 |
| | | | | | 1939 ⁸ 1.1 27 walk | | 1940 ⁸ 1.01 37 at step | |
| 195.09 | | | | | | | | |

check F.H. S.E. Beryl 6.39 171.68 171.68

2.78 178.07 13.21 175.29

T.P. 0.12 188.50 12.51 188.38

Set B.M. on S.W. 7 Mon. 3.67 197.22 197.32

(Put High in
Book)

60' N. = N.L. Collingwood

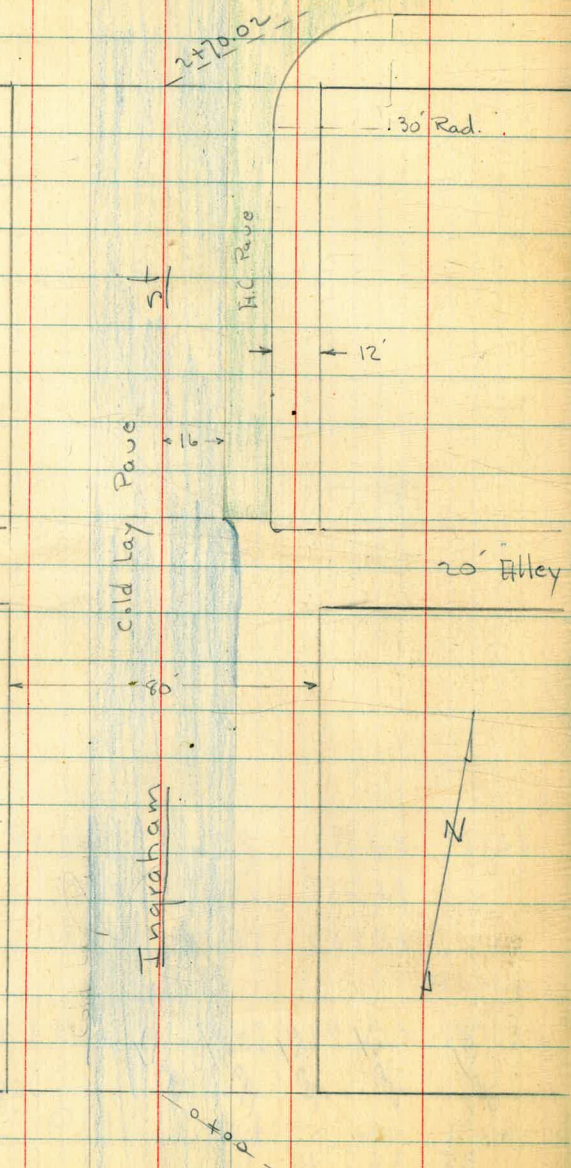
| | | | | | | | |
|--|---|---|---|--|---|---|---|
| $\begin{array}{r} 200.19 \\ +0.7 \\ \hline 35 \end{array}$ | $\begin{array}{r} 200.29 \\ 0.6 \\ \hline 25 \end{array}$ | $\begin{array}{r} 200.19 \\ 0.7 \\ \hline 15 \end{array}$ | $\begin{array}{r} 199.39 \\ 1.5 \\ \hline 10 \end{array}$ | $\begin{array}{r} 199.19 \\ 1.1 \\ \hline \end{array}$ | $\begin{array}{r} 199.59 \\ 1.3 \\ \hline 15 \end{array}$ | $\begin{array}{r} 199.19 \\ 1.7 \\ \hline 25 \end{array}$ | $\begin{array}{r} 199.19 \\ 1.7 \\ \hline 35 \end{array}$ |
|--|---|---|---|--|---|---|---|

200.89

Law

INDEXED

st



chalcedony

st

Indexed

55

X-Sect. Ingraham - from ^BN.L.
Chalcedony to SL Law.

1913

W.O. 31371

11-25-47

Osborne
Hardin
Smith
Worrell

X-Sect. Ingraham - 80' st. - 12' cbs.
from N.L. Chalcedony to S.L. Law.

1+47 = Beg. AC Pavc on Rt. (11' Rt.)

INDEXED

NK
APR 5 1949

1+45 = N.L. Hilley - Beg. curb on Rt.

1+25 = S.L. 20' Hilley -

1+23 - 22.6 ft. = ± P. pole # P 4824

0+85

0+50

0+00 = N.L. Chalcedony - See P. 14 - for Int.

B.M.

1.58 110.26

108.68

SE. 7' c. in cb.

Law + Ingraham

Charley - Note: These elevs are .10 lower than
levels originating at Beryl + Ingraham.

Lt. = W

±

Rt. = E

56

| | | | | | | | | | | | |
|--|--|--|---|---|---|---|---|--|--|--|--|
| 104 ⁴⁶ / ₄₀ 5.6 | 104 ⁵⁸ / ₂₈ 5.7 | 105 ²² / ₂₂ 4.5 | 104 ⁰⁶ / _{18.6} 6.20 edge | 104 ⁵⁹ / ₁₀ 5.67 | 105 ⁰² / ₁₀ 5.24 | 105 ⁰⁸ / ₁₀ 5.18 | 105 ⁰² / ₁₆ 5.24 edge AC + edge C.L. | 105 ²⁴ / ₂₀ 5.02 | 105 ¹⁴ / ₂₈ 5.12 | 105 ⁸⁵ / ₂₈ 4.41 gut. Top | 106 ⁴⁶ / ₄₀ 3.8 |
| 104 ⁴⁶ / ₄₀ 5.8 | 104 ⁴⁶ / ₂₈ 5.8 | 104 ⁸⁶ / ₂₂ 5.4 | 104 ⁰⁰ / _{18.6} 6.26 edge | 104 ⁵⁴ / ₁₀ 5.72 | 104 ⁹⁸ / ₁₀ 5.28 | 105 ⁰² / ₁₀ 5.24 | 104 ⁹¹ / _{18.2} 5.35 edge | 105 ¹⁶ / ₂₈ 5.1 gut. | 105 ⁸⁵ / ₂₈ 4.41 Top 2 Rad. Ret. | 106 ¹³ / ₄₀ 4.13 Top gut end Ret. | |
| 104 ¹⁶ / ₄₀ 6.1 | 104 ⁴⁶ / ₂₈ 5.8 | 104 ⁸⁶ / ₂₃ 5.4 | 103 ⁶³ / ₁₉ 6.4 edge | 104 ²⁰ / ₁₀ 6.06 | 104 ⁵⁸ / ₁₀ 5.68 | 104 ⁶¹ / ₁₀ 5.65 | 104 ⁴¹ / _{18.5} 5.85 edge | 105 ⁴⁶ / ₂₈ 4.8 | 106 ⁵⁶ / ₄₀ 3.7 | | |
| 103 ²⁶ / ₄₀ 7.0 | 104 ³⁸ / ₂₈ 5.9 | 104 ⁴⁶ / ₂₂ 5.8 | 102 ⁹⁹ / _{18.3} 7.27 edge | 103 ³⁶ / ₁₀ 6.90 | 103 ³³ / ₁₀ 6.53 | 103 ⁷⁹ / ₁₀ 6.47 | 103 ⁸⁰ / _{18.7} 6.46 edge | 104 ⁶⁶ / ₂₂ 5.6 | 104 ⁹⁶ / ₂₈ 5.3 | 105 ⁴⁶ / ₄₀ 4.8 | |
| 103 ¹⁶ / ₄₀ 7.1 | 104 ⁰⁶ / ₂₈ 6.2 | 104 ⁵⁶ / ₂₃ 5.7 | 102 ²³ / ₁₉ 8.04 edge | 102 ⁶⁴ / ₁₀ 7.62 | 103 ⁰⁰ / ₁₀ 7.26 | 103 ⁰² / ₁₀ 7.24 | 103 ⁰⁰ / _{16.5} 7.26 edge | 104 ⁰⁶ / ₂₁ 6.2 | 103 ⁹⁶ / ₂₈ 6.3 | 104 ⁹⁶ / ₄₀ 5.3 | |
| 101 ⁴⁶ / ₄₀ 8.9 | 102 ¹⁶ / ₂₈ 8.1 | 102 ²⁶ / ₂₃ 7.5 | 101 ⁰² / ₁₉ 9.24 edge Pavc | 101 ⁴⁶ / ₁₀ 8.80 | 101 ⁹⁴ / ₁₀ 8.32 | 101 ⁹⁷ / ₁₀ 8.29 | 101 ⁹⁶ / ₁₉ 8.30 edge Pavc | 103 ¹⁶ / ₂₈ 7.1 | 103 ²⁶ / ₄₀ 7.0 | | |
| | | | | CL. rolls up side | | 110 26 | | | | | |

2+70.02 = S.L. Law. = end - See Law Sect. for Int.

2+68 - 22 Lt. ← Pole # 4848

2+60 = opp. PC. 30' Rad. Return on Rt.

2+25

1+85

1+69 - 29.8 Rt. ← Tel. pole # 430665 H

| | | | | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 107 ³⁶ | 107 ³⁶ | 107 ²⁵ | 106 ⁷³ | 107 ²⁰ | 107 ⁵⁰ | 107 ⁶² | 107 ⁶¹ | 107 ⁸⁰ | 107 ⁷¹ | 107 ⁶⁸ | 108 ¹² | 107 ²⁰ |
| 2.9 | 2.9 | 2.2 | 3.53 | 3.06 | 2.76 | 2.64 | 2.65 | 2.46 | 2.55 | 2.58 | 1.84 | 0.9 |
| 40 | 28 | 21 | 18.6 | 10 | 10 | 10 | 16 | 20 | 28 | 29.7 | 29.7 | 40 |
| | | | edge | | | | edge | | | gut | Top | cb. |

| | | | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 107 ¹⁶ | 107 ⁰⁶ | 107 ⁵⁶ | 106 ⁴⁶ | 106 ⁹³ | 107 ²⁴ | 107 ³⁷ | 107 ³⁹ | 107 ⁴⁷ | 107 ⁴⁷ | 108 ¹⁷ | 108 ⁷⁶ |
| 3.1 | 3.2 | 2.7 | 3.80 | 3.33 | 3.02 | 2.89 | 2.87 | 2.79 | 2.79 | 1.09 | 1.5 |
| 40 | 24 | 21 | 18.6 | 10 | | 10 | 16 | 20 | 28 | 28 | 40 |
| | | | edge | | | | edge | | gut | Top | pk. |

| | | | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 106 ³⁶ | 106 ⁴⁶ | 107 ⁰⁶ | 105 ⁶⁸ | 106 ¹³ | 106 ⁴⁶ | 106 ⁶² | 106 ⁶³ | 106 ⁸⁶ | 106 ⁷⁹ | 107 ⁴⁸ | 107 ⁸⁶ |
| 3.9 | 3.8 | 3.2 | 4.58 | 4.13 | 3.80 | 3.64 | 3.63 | 3.40 | 3.47 | 2.78 | 2.4 |
| 40 | 28 | 21 | 18.6 | 10 | 10 | 10 | 16 | 20 | 28 | 28 | 40 |
| | | | edge | | | | edge | | gut | Top | |

| | | | | | | | | | | | |
|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 105 ⁴⁶ | 105 ⁸⁶ | 106 ⁴⁶ | 104 ⁸⁶ | 105 ³² | 105 ⁷² | 105 ⁸⁵ | 105 ⁸⁴ | 106 ⁰⁴ | 105 ⁹² | 106 ⁶⁴ | 107 ¹⁶ |
| 4.6 | 4.4 | 3.8 | 5.40 | 4.94 | 4.54 | 4.41 | 4.42 | 4.22 | 4.29 | 3.62 | 3.1 |
| 40 | 28 | 22 | 18.6 | 10 | 10 | 10 | 16 | 20 | 28 | 28 | 40 |
| | | | edge | | | | edge | | gut | Top | |

110.26

Walker
Hendricks
Becker
Millharris
3-17-48

CROSS SECTION ALLEY
in Highland Gardens
from Doyton St. to Gilbert Dr.
North of El Cajon Blvd.
see BK.G 263 P-15 W.O. 25001

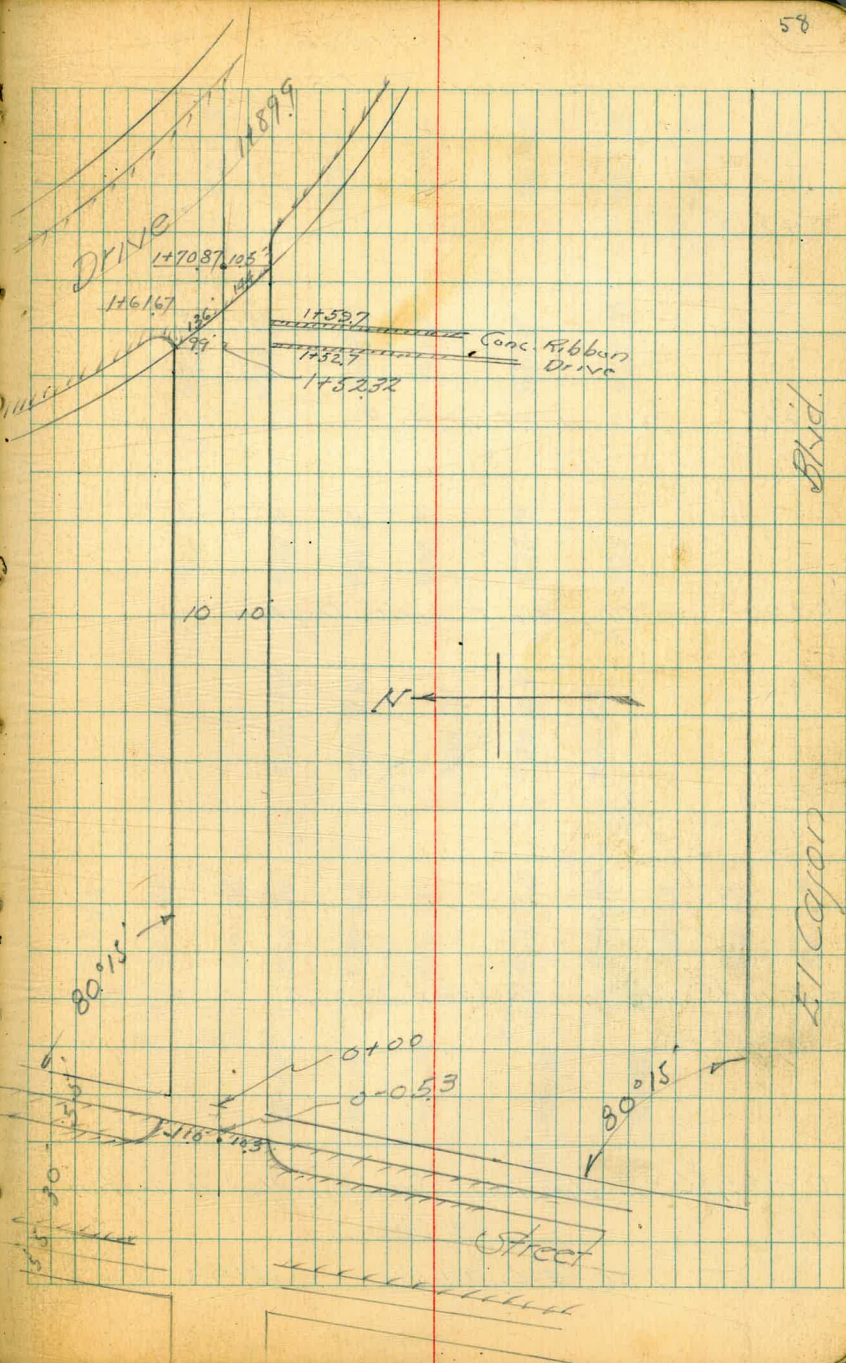
INDEXED
MAR 19 1948

1+70.07
59
61

Gilbert

Doyton

Street



Cross Section Alley Block 'E'
Point Loma Hts

Roberts
W. Moore
T. Clark
7-1-49
W.O. 25001

Map 1523, TP 720, 721, 731

T.P. 26

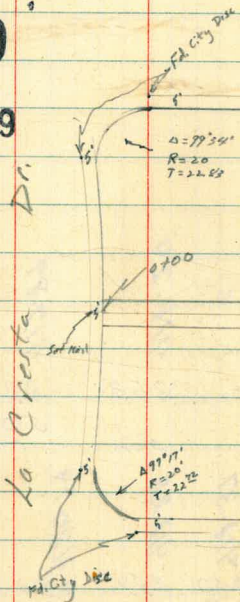
INDEXED

WK

APR 5 1949

Note: -

La Cresta is
blacktop paved.
10' Parking
4' Ch. Fee & walk
5' wide walk.



Centra Loma

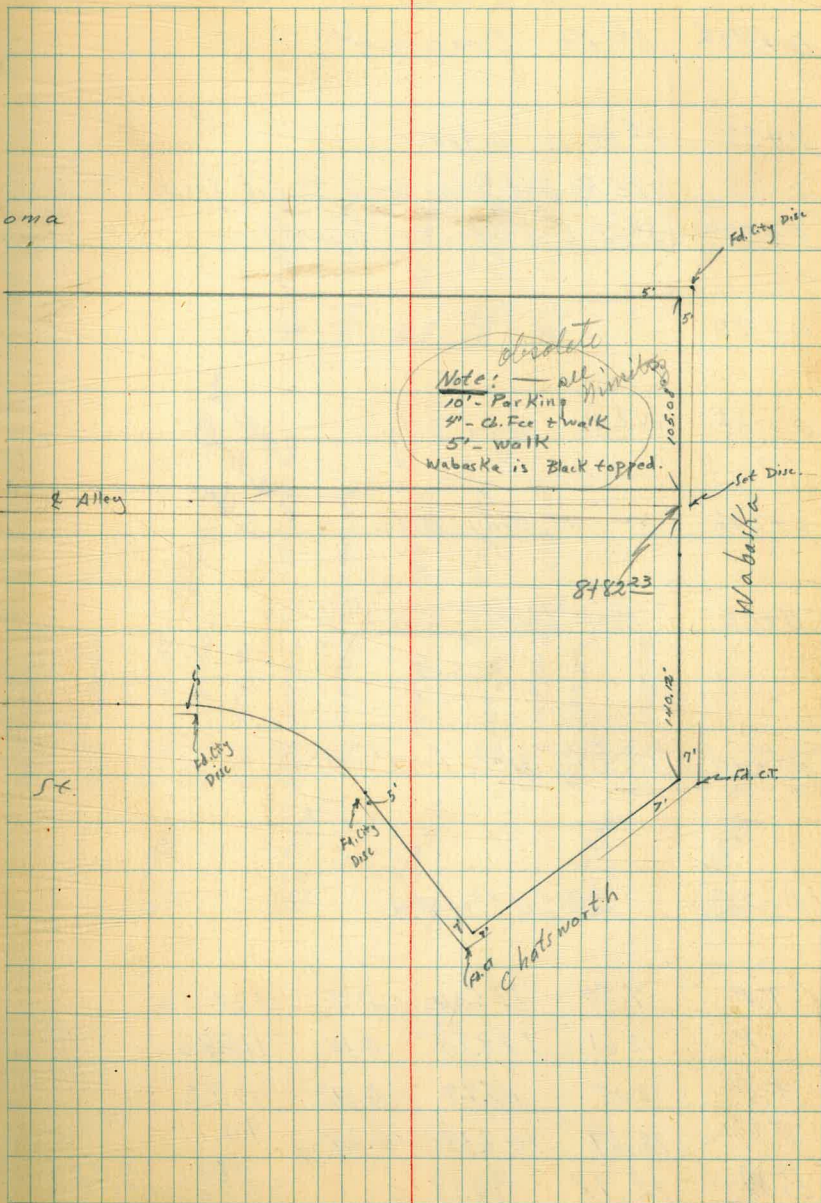
Poc

For & Alley: -

A = 25° 52'

R = 730

To further check & alley Prop. lines on
Poc & Centraloma were extended into Cresta
and split.



Cont'd From Page 62

0+42^E 6⁶' R4 Deadman

0+37 7¹' R4 Δ in fence

0+33^E $\left\{ \begin{array}{l} 9²' R4 \text{ End Bldg. Begin Picket fence} \\ 8⁸' Lt. \text{ End Bldg. Begin wire fence} \end{array} \right.$

0+20

0+13^E 8¹' R4 Begin Bldg.

Reduced
4-11-49
G.J.H.

0+09^E 8²' Lt. Begin Bldg.

0+00 Prop. Line

0-10 cb. Line LaCresta

0-25 Δ LaCresta

| | | | | | |
|------|-------|--------|------|--------|--------|
| T.P. | 7.54 | 135.86 | 0.12 | 128.32 | |
| T.P. | 12.61 | 128.74 | 0.14 | 115.83 | |
| T.P. | 13.05 | 115.97 | 0.46 | 102.92 | |
| T.P. | 12.67 | 103.38 | 0.28 | 90.71 | |
| BM | 12.78 | 90.99 | | 78.21 | SE.B.P |

Lt.

Δ

R4

63

| | | | | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|------|-------|------|
| 132.12 | 131.43 | 131.53 | 130.68 | 130.54 | 129.93 | 130.88 | 130.50 | 130.15 | 130.31 | 130.98 | 128.25 | | | | |
| 3.74 | 4.43 | 4.53 | 5.18 | 5.32 | 5.79 | 5.74 | 5.71 | 6.05 | 6.16 | 6.23 | 5.87 | 8.11 | 6.47 | 7.80 | 7.17 |
| cb. | Gutt. | cb. | Gutt. | cb. | Gutt. | Gutt. | Gutt. | cb. | Gutt. | cb. | Gutt. | Gutt. | cb. | Gutt. | cb. |
| | | 132.18 | | 131.79 | | 130.96 | | | | 129.98 | | 129.35 | | | |
| | | 3.38 | | 7.07 | | 4.90 | | | | 5.91 | | 6.57 | | | |
| | | 90.5 | | 50 | | | | | | 50 | | 90 | | | |
| | | | | | | | | 135.86 | | | | | | | |

Poa Δ Chotworth

Cont'd From Page 63

1+28 8³' Lt Begin Conc. Block Wall

1+26³ 10⁶' Lt ← 3' Walk

1+24⁸ 13⁸' Lt End Patio

1+18³ 9²' Rt W. Edge Conc. Apron. to Double Garage

1+16 8⁵' Rt End Picket Fence

1+08⁶ 13⁶' Lt Begin Patio

T.P. 0.82 123.71 12.97 122.89

1+02 9⁴' Lt End wire Fence

0+60

0+57 7' Rt to Center P. Pole # PA 3880

135.86

126.51

lt.

120.91
2.8
8³
TOP

127.41

43.7
8³
Dirt

119.57

8³
Floor

Rt

64

121.50

2.21
10⁶
Walk

121.95

17⁶
13⁸
Patio

121.92

3.39
9²
Apron

121.20

2.51
22.7
Floor

121.92

1.79
13⁶
Patio

121.91

4⁸
13⁶
Dirt

123.01

0.7
7²

122.91

0.8

123.21

0.5
7²

122.71

1.0
1⁶

123.71

125.65

10.2
7²

124.16

11.7
8

123.76

2.1
7²

123.86

12.0
7²

128.66

12.0
2⁵

128.16

12.7
7²

128.56

7.3
7²

135.86

Cont'd From Page 64

2+20^E 9' Lt End Board Fence

2+00

1+97^E 6' Rt End Picket Fence

1+69 8' Lt Begin Board Fence

1+67 8' Lt End Conc Block Wall

T.P. 6.63 $\frac{117.76}{5}$ 12.59 11 1.13 P. Pole

1+51 7' Rt Begin Picket Fence

1+50

1+37 6' Rt to Center P. Pole #JPA 3876 #305822H

1+34 10' Rt E. Edge Apron of Double Garage

$\frac{123.71}{5}$

lt.

2

11

65

114.76.
 $\frac{3.0}{16}$

114.06.
 $\frac{3.7}{25}$

113.66.
4.1

113.76.
 $\frac{4.0}{25}$

113.46.
 $\frac{4.3}{16}$

125.76.
 $\frac{4.0}{25}$
Tip

116.76.
 $\frac{4.0}{25}$
Dirt

115.96.
 $\frac{1.8}{25}$
Foot

117.76

118.21.
 $\frac{5.5}{72}$

117.81.
5.9

117.81.
 $\frac{5.5}{72}$

118.61.
 $\frac{5.7}{72}$

117.51.
 $\frac{6.2}{72}$

117.31.
 $\frac{6.4}{11}$

118.41.
 $\frac{5.3}{72}$

117.91.
5.8

117.91.
 $\frac{5.8}{3}$

118.61.
 $\frac{5.7}{7}$

118.21.
 $\frac{5.5}{11}$

120.52.

$\frac{3.19}{102}$
Apron

121.22.
 $\frac{2.49}{222}$
Apron

$\frac{123.71}{5}$

Cont'd From Page 66

5+50

5+42 85' Lt Begin Lathe House

5+23 72' Lt End Cypress Hedge

5+00

4+99 74' Rt Hedge Cypress Trees Begins

4+96.5 62' Rt to Center P. Pole # PA 3110

4+94.1 81' Lt End Garage Tto $\frac{1}{2}$

T.P. 1.66 97.55 8.88 95.89

4+76.2 82' Lt End Board Fence {Begin Tto Garage}

4+50

4+38.1 78' Rt Begin Board Fence

104.77

Lt.

Rt

67

93.75.
 $\frac{3.8}{75}$

93.75.
41

93.75.
 $\frac{2.1}{5}$

93.95.
 $\frac{3.6}{75}$

95.95.

95.75

95.35

95.45.

95.65.

95.65.

$\frac{1.6}{15}$

$\frac{1.8}{75}$

2.2

$\frac{2.1}{5}$

$\frac{1.7}{75}$

$\frac{1.9}{15}$

96.14.

96.14.

$\frac{1.41}{293}$
Floor

$\frac{1.41}{102}$
Floor

97.55

97.57.

97.27.

96.97.

97.17.

96.97.

$\frac{7.2}{15}$

$\frac{7.5}{75}$

7.8

$\frac{7.6}{75}$

$\frac{7.8}{15}$

104.77

Cont'd from Page 67

7+43 { 75' Lt to Garage opens on Centroloma
72' Lt End Picket Fence

7+37.5 73' Rt to Center P. Pole # 7A3750

7+02 { 75' Lt Begin Picket Fence
76' Rt End Conc. Block Wall & Begin Lathr Fence

T.P. 0.76 85.92 12.39 85.16

6+37.3 72' Rt Begin Conc. Block Wall

6+21 ^{28.5'} 213' Rt X Double Garage Begin floor

6+16.2 62' Rt to Center P. Pole # PA3790

6+00 Sewer M.H.

5+62 91' Lt End Lathr Fence

5+57 96' Rt End Board Fence

97.55

Lt

Rt

Rt

68

| | | | | | |
|------------------|------------------|--------|------------------|--------------------------|--------------------------|
| 83.72. | 82.72. | 82.72. | 82.92. | 82.52. | 88.82. |
| $\frac{2.5}{75}$ | $\frac{3.2}{72}$ | 3.2 | $\frac{3.0}{73}$ | $\frac{3.4}{76}$ Foot | $\frac{42.4}{76}$ Top |

| | | | | | | |
|------------------|------------------|-------|------------------|------------------|---------------------------|--------------------------|
| 89.45 | 88.25 | 87.25 | 87.45 | 87.75 | 86.65 | 92.10. |
| $\frac{8.1}{93}$ | $\frac{9.3}{72}$ | 10.3 | $\frac{10.1}{3}$ | $\frac{9.8}{72}$ | $\frac{10.9}{72}$ Foot | $\frac{5.45}{72}$ Top |

88.38.
 $\frac{8.17}{213}$
Floor

| | | | | |
|------------------|------------------|-------------------|------------------|------------------|
| 91.75. | 91.95. | 91.95. | 91.95. | 92.25. |
| $\frac{5.8}{75}$ | $\frac{5.6}{72}$ | 5.60 Rim MH | $\frac{5.6}{75}$ | $\frac{5.3}{75}$ |

97.55

Cont'd From Page 68

8751⁵ 75' to Center of 4' Wide Hedge

8750

8749¹ 72' RT End Tile Wall

8746² 70' RT to Center P. Pole PA 3710

8718 78' RT End Lattice Fence Begin Tile Wall

8715 82' RT & 2' Conc. Walk

8700

7782 72' RT End Lath Fence Begin Lattice Fence

7761 75' LT End Garage

7750

85.92

LT

R

RT

69

80.22.
 $\frac{5.7}{75}$

80.12.
 $\frac{5.8}{75}$

80.32.
 $\frac{5.6}{75}$

80.32.
 $\frac{5.6}{72}$ Part
79.92.
 $\frac{6.5}{72}$ Foot
83.69.
 $\frac{2.13}{72}$ Top

80.22.
 $\frac{5.7}{72}$ Part

78.92.
 $\frac{7.0}{72}$ Foot

83.40.
 $\frac{2.52}{72}$ Top

80.92.
 $\frac{5.0}{75}$

80.52.
 $\frac{5.4}{75}$

80.62.
 $\frac{5.3}{75}$

80.52.
 $\frac{5.4}{75}$ Walk
79.96.
 $\frac{6.16}{75}$

80.02.
 $\frac{5.9}{70}$

80.02.
 $\frac{5.9}{70}$

81.72.
 $\frac{4.2}{75}$

81.92.
 $\frac{4.5}{75}$

81.52.
 $\frac{4.4}{75}$

80.52.
 $\frac{5.4}{75}$

85.92

Cont'd From Page 69

check 6.51 78.23 = 78.21

8787²³ Cb. Line WabasKa

T.P. 5.23 84.74 6.41 79.51

8782²³ P.L. on WabasKa

8781²³ Par. Edge

85.92

Lt.

£

Rt.

70

Start, BM

| | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 80.97. | 80.29. | 80.30. | 79.57. | 79.51. | 79.36. | 79.26. | 79.22. | 79.93. | 78.45. | 79.22. |
| 2.77 | 2.45 | 4.44 | 5.10 | 5.23 | 5.38 | 5.44 | 5.52 | 4.81 | 6.29 | 5.52 |
| cb. | cut | cb. | cut | cb. | cut | cb. | cut | cb. | cut | cb. |

84.74

| | | | | |
|--------|--------|--------|--------|--------|
| 80.92. | 80.02. | 79.54. | 79.53. | 80.03. |
| 5.50 | 5.90 | 6.38 | 6.29 | 5.49 |
| cb. | cut | cut | cut | cb. |

85.92

Paul St + Nashville St.

Morena to Tonopah

Grade Est.

N.O. 25020

1-8-50

Sommermeier

McCoy

Allen

Bunch

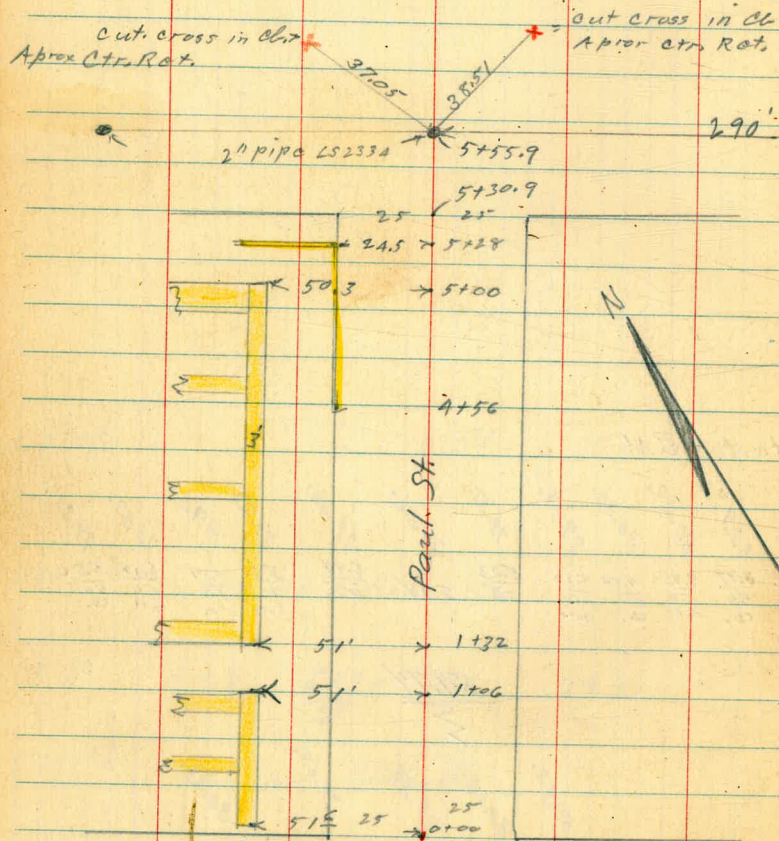
INDEXED

M.K.
FEB 10 1950

FB1791-42

Map # 1571

± Paul as shown = Willy. line Corolla Tract.



Pave. $\frac{0-27}{0-375}$
 Morena Fd $\frac{1791}{42}$ $\frac{25}{2}$ Blvd.

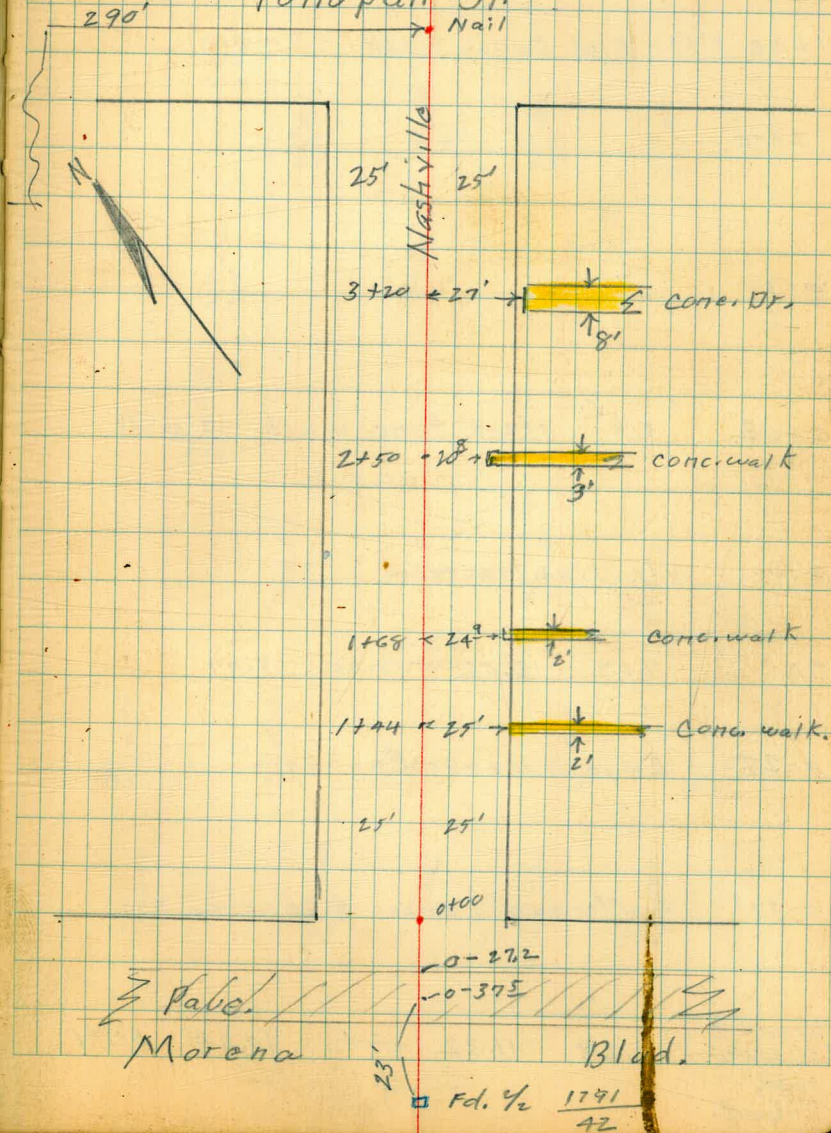
37.5
23
60.5

±

71

Tonopah St.

Nail



Pave. $\frac{0-272}{0-375}$
 Morena Fd. $\frac{1791}{42}$ $\frac{25}{2}$ Blvd.

1+32 51' Lt = start Conc. walk (3' wide)

1+06.51 Lt = End Conc. walk (3' wide)

1+00

0+50

0+02 51' Lt = start Conc. walk - 3' wide

0+00 Nly. line Morena

T.P. 7.19 12.66 5.85 5.47

0-27 = Edge Morena Paving

0-37^E = ± Morena (approx ± Paving)

Morena +
Tacolote
Creek
Culvert. 1.28 11.32 — 10.04 BM#1

$$\begin{array}{r} 6.75 \\ 5.93 \\ \hline 51 \\ \text{walk} \end{array}$$

$$\begin{array}{r} 6.58 \\ 5.08 \\ \hline 1 \\ \text{walk} \end{array}$$

$$\begin{array}{r} 7.57 \\ 7.19 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.49 \\ 7.18 \\ \hline \end{array}$$

$$\begin{array}{r} 5.50 \\ 7.17 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.50 \\ 7.17 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 5.58 \\ 6.97 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.52 \\ 7.15 \\ \hline \end{array}$$

$$\begin{array}{r} 7.49 \\ 7.18 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.75 \\ 6.93 \\ \hline 576 \end{array}$$

$$\begin{array}{r} 5.74 \\ 7.23 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 4.8 \\ 7.19 \\ \hline \end{array}$$

$$\begin{array}{r} 5.50 \\ 7.17 \\ \hline 25 \end{array}$$

$$\underline{12.66}$$

$$\begin{array}{r} 4.58 \\ 6.74 \\ \hline 125 \end{array}$$

$$\begin{array}{r} 5.28 \\ 6.24 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.17 \\ 6.15 \\ \hline \end{array}$$

$$\begin{array}{r} 5.24 \\ 6.08 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.65 \\ 5.67 \\ \hline 125 \end{array}$$

$$\begin{array}{r} 5.44 \\ 6.38 \\ \hline 125 \end{array}$$

$$\begin{array}{r} 5.54 \\ 5.98 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.87 \\ 5.95 \\ \hline \end{array}$$

$$\begin{array}{r} 5.44 \\ 5.88 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.75 \\ 5.37 \\ \hline 125 \end{array}$$

$$\underline{11.32}$$

4+50

4+00

3+50

3+29 20' Rt. = End House

T.P. 12.93 24.75 0.84 11.82

This house is to be moved by owner.

3+07 21⁵ Rt. = S.W. Cor. House.

3+00

2+50

2+00

1+50

±

$$\begin{array}{r} 16.4 \\ 8.4 \\ \hline 25 \end{array} \quad \begin{array}{r} 17.2 \\ 7.6 \\ \hline \end{array} \quad \begin{array}{r} 15.7 \\ 7.1 \\ \hline 25 \end{array} \quad \begin{array}{r} 11.9 \\ 12.9 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 14.4 \\ 10.4 \\ \hline 25 \end{array} \quad \begin{array}{r} 15.0 \\ 7.8 \\ \hline \end{array} \quad \begin{array}{r} 12.5 \\ 12.3 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 12.5 \\ 12.3 \\ \hline 25 \end{array} \quad \begin{array}{r} 12.75 \\ 12.00 \\ \hline \end{array} \quad \begin{array}{r} 10.2 \\ 14.6 \\ \hline 25 \end{array} \quad \begin{array}{r} 8.0 \\ 16.8 \\ \hline 75 \end{array}$$

24.75

$$\begin{array}{r} 11.2 \\ 1.5 \\ \hline 35 \end{array} \quad \begin{array}{r} 11.2 \\ 1.5 \\ \hline 25 \end{array} \quad \begin{array}{r} 10.0 \\ 2.7 \\ \hline 20 \end{array} \quad \begin{array}{r} 10.2 \\ 2.5 \\ \hline \end{array} \quad \begin{array}{r} 8.5 \\ 4.2 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.5 \\ 3.2 \\ \hline 25 \end{array} \quad \begin{array}{r} 8.0 \\ 4.7 \\ \hline 18 \end{array} \quad \begin{array}{r} 7.4 \\ 5.3 \\ \hline \end{array} \quad \begin{array}{r} 6.1 \\ 6.6 \\ \hline 25 \end{array} \quad \begin{array}{r} 5.3 \\ 7.4 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} 8.1 \\ 4.6 \\ \hline 35 \end{array} \quad \begin{array}{r} 8.1 \\ 4.6 \\ \hline 25 \end{array} \quad \begin{array}{r} 6.3 \\ 6.4 \\ \hline 18 \end{array} \quad \begin{array}{r} 6.0 \\ 6.7 \\ \hline \end{array} \quad \begin{array}{r} 5.0 \\ 7.7 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.1 \\ 5.6 \\ \hline 35 \end{array} \quad \begin{array}{r} 7.1 \\ 5.6 \\ \hline 25 \end{array} \quad \begin{array}{r} 5.5 \\ 7.2 \\ \hline 19 \end{array} \quad \begin{array}{r} 7.51 \\ 7.6 \\ \hline \end{array} \quad \begin{array}{r} 5.1 \\ 7.6 \\ \hline 25 \end{array}$$

12.66

Temp B.M. 13.03 11.72 stub.

5455² = ϕ Tonopah5430² = Sly line Tonopah5428 24² Lt. = End 6" wide Conc. wall
also = ϕ E+W. Conc. wall5400 50² Lt. = End 3' wide Conc. walk
24² Lt. = wall

A+77 25' Lt. = wall

A+74 = 25' Lt. = wall

A+56 25' Lt. = Start 6" Retaining wall

$$\begin{array}{r} 31.8 \\ + 7.0 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 28.2 \\ + 3.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 26.3 \\ + 1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 24.8 \\ 0.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 20.8 \\ 4.0 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 19.7 \\ 5.1 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 23.0 \\ 1.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 24.6 \\ 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 23.9 \\ 0.9 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 21.4 \\ 3.4 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 11.0 \\ 6.8 \\ 2.6 \\ \hline \text{Ord.} \\ \text{inside of} \\ \text{wall} \end{array}$$

$$\begin{array}{r} 22.5 \\ 2.3 \\ 2.25 \\ \hline \text{wall} \\ \text{Ord.} \end{array}$$

$$\begin{array}{r} 22.2 \\ 2.6 \\ 2.45 \\ \hline \text{Ord.} \end{array}$$

$$\begin{array}{r} 17.8 \\ 7.0 \\ 50.3 \\ \hline \text{walk} \end{array}$$

$$\begin{array}{r} 7.4 \\ 7.4 \\ 25 \\ \hline \text{Ord.} \end{array}$$

$$\begin{array}{r} 20.46 \\ 1.29 \\ 24.5 \\ \hline \text{Top wall} \\ \text{Ord.} \end{array}$$

$$\begin{array}{r} 20.3 \\ 4.5 \\ 24.5 \\ \hline \text{Ord.} \end{array}$$

$$\begin{array}{r} 21.4 \\ 3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 21.4 \\ 3.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 19.7 \\ 5.1 \\ \hline 25 \\ \text{top of wall} \end{array}$$

$$\begin{array}{r} 18.5 \\ 6.3 \\ \hline 25 \\ \text{top of wall} \end{array}$$

$$\begin{array}{r} 16.4 \\ 8.4 \\ 25 \\ \hline \text{inside} \\ \text{of wall} \\ \text{or Ord.} \end{array}$$

$$\begin{array}{r} 7.5 \\ 7.3 \\ 25 \\ \hline \text{top} \\ \text{wall} \end{array}$$

$$\begin{array}{r} 16.9 \\ 7.9 \\ 25 \\ \hline \text{wall} \end{array}$$

Levels Nashville st.

±

T.P. 4.88 11.22 5.52 6.34

1+50

$$\begin{array}{r} 5.6.1 \\ 5.8 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 5.6.2 \\ 5.7 \end{array}$$

$$\begin{array}{r} 5.6.2 \\ 5.7 \\ \hline 25 \end{array}$$

35

1+44 25' At. = ± 2' wide Conc. walk

$$\begin{array}{r} 5.6.28 \\ 5.58 \\ \hline 25 \\ \text{walk} \end{array}$$

$$\begin{array}{r} 5.6.32 \\ 5.54 \\ \hline 35 \end{array}$$

1+00

$$\begin{array}{r} 5.5.8 \\ 6.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 5.5.9 \\ 6.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6.3 \\ 5.6 \end{array}$$

$$\begin{array}{r} 5.6.2 \\ 5.7 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6.2 \\ 5.7 \\ \hline 50 \end{array}$$

0+50

$$\begin{array}{r} 5.5.9 \\ 6.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6.3 \\ 5.6 \end{array}$$

$$\begin{array}{r} 5.6.0 \\ 5.9 \\ \hline 25 \end{array}$$

0+00 = Nly line Morena

$$\begin{array}{r} 5.5.8 \\ 6.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 5.5.7 \\ 6.2 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6.2 \\ 5.7 \end{array}$$

$$\begin{array}{r} 5.5.9 \\ 6.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.5.9 \\ 6.0 \\ \hline 50 \end{array}$$

0-27[±] = Nly edge Morena Pauc

$$\begin{array}{r} 5.5.6 \\ 6.00 \\ \hline 125 \end{array}$$

$$\begin{array}{r} 5.6.5 \\ 5.21 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6.97 \\ 4.89 \end{array}$$

$$\begin{array}{r} 5.26 \\ 4.60 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.8.99 \\ 3.37 \\ \hline 125 \end{array}$$

0-37[±] = ± Morena

$$\begin{array}{r} 5.6.12 \\ 5.74 \\ \hline 125 \end{array}$$

$$\begin{array}{r} 5.6.98 \\ 4.88 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.7.29 \\ 4.57 \end{array}$$

$$\begin{array}{r} 5.7.57 \\ 4.29 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.8.79 \\ 3.12 \\ \hline 125 \end{array}$$

BM#1P72 1.82 11.86 — 10.04

11.86

Nashville St.

Temp. B.M. P 74

2.88

11.75

11.72

5+55² = ϵ Tomopaki (on new fill)

5+30² = 9/y. line Tomopaki

5+00

ϵ

77

$$\begin{array}{r} 12.2 \\ 2.4 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 10.3 \\ 4.3 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.92 \\ 5.4 \end{array}$$

$$\begin{array}{r} 9.8 \\ 4.8 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 9.7 \\ 4.9 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 9.8 \\ 4.8 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 7.3 \\ 7.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6.79 \\ 6.7 \end{array}$$

$$\begin{array}{r} 8.3 \\ 6.3 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 6.4 \\ 8.2 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 9.7 \\ 6.9 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 8.66 \\ 8.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 8.66 \\ 8.0 \end{array}$$

$$\begin{array}{r} 8.66 \\ 8.4 \\ \hline 25 \end{array}$$

14.63

Bench Levels along Lamont - from
Diamond to Beryl

w.o. 31584 3-13-50 7.0.

INDEXED

W.K.

MAR 14 1950

| | | | | |
|------|-------|--------|------|-----------------------|
| B.M. | 12.56 | 114.59 | | 106.03 - S.W. B.P. |
| | | | 2.36 | 116.23 - S.E. 3 B.ct. |
| T.P. | 10.07 | 128.30 | 0.36 | 118.23 |
| | | | 1.98 | 126.32 - S.W. 7'ct. |
| | | | 2.03 | 126.27 - S.E. 7'ct. |
| T.P. | 13.05 | 140.95 | 0.40 | 127.90 |
| T.P. | 11.96 | 152.31 | 0.60 | 140.35 |
| | | | 9.57 | 142.74 - S.W. 7'ct. |
| | | | 8.90 | 143.41 N.W. 7'ct. |
| T.P. | 12.83 | 164.66 | 0.48 | 151.83 |
| | | | 2.32 | 162.34 N.E. 7'ct. |
| | | | 2.32 | 162.34 N.W. 7'ct. |

Note diff. between B.M.'s + different
level circuits - See B. 1775 + 1807 for
.10 diff. in level circuits - This line
checks diff. shown in various Books.

Diamond + Lamont - 10591 = My Bench Book
on 7 line - Missouri - 10595 = 1743-36
11590 - 1837-72

Chalcedony - 126.00 - 1807-25 - 126.31 = 1767-73
" 126.22 - 1743-36

Law 142.55 - 1807-41
Law 142.10 1837-72

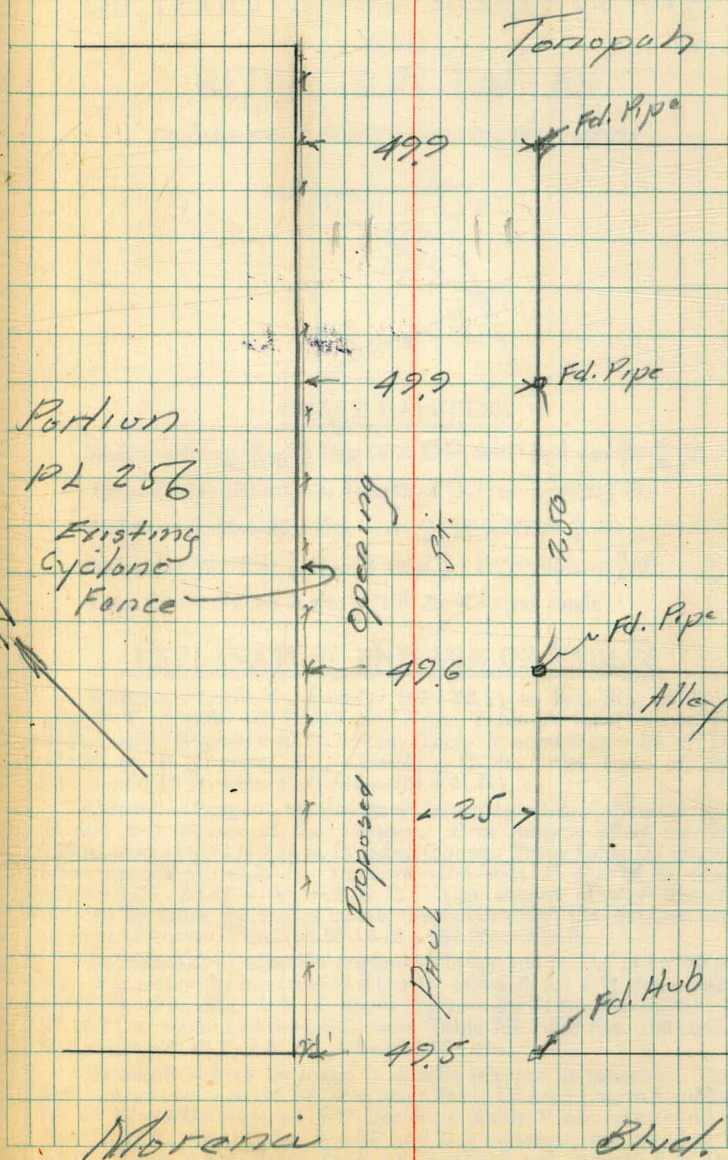
Beryl 162.14 - 1807-40
162.28 - 1743-41

PAUL-ST.

Location Existing Fence

Walker
R. Sisson
Pope
7-21-50

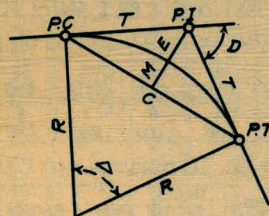
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14
17
1
7

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R \left(1 - \cos \frac{\Delta}{2}\right) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R + \cos \frac{\Delta}{2} - R \quad (8) = R \text{exsec} \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. — $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 \left(\frac{54.50}{100}\right)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

6.02

- 0.48

| |
|--------------|
| 88.46 |
| 3.15 |
| <hr/> 85.31 |
| 10.79 |
| <hr/> 96.10 |
| 3.42 |
| <hr/> 92.68 |
| 8.19 |
| <hr/> 100.87 |
| 0.77 |
| <hr/> 100.10 |

1775

Page 13 142.57 = s.w.7' Lamont + law

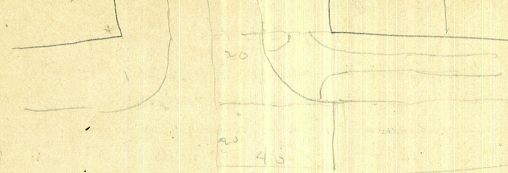
3 - 125.08 s.w.7' Ingraham + Berl

8.69

| |
|--------------|
| 108.68 |
| 1.58 |
| <hr/> 110.26 |
| 8.69 |
| <hr/> 101.57 |

196.04 = Pin

202.19 = H.S. b. S.W. Malden & E. Melrose



1.4142
99999

20
400
400
800
400
380
1280

50
20
1000
2.00
204.00

4.000

1280
20
256.00
170
426

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2 For Single Track Embankment.

| H | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | H |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0 | 8.0 | 8.2 | 8.3 | 8.5 | 8.6 | 8.8 | 8.9 | 9.1 | 9.2 | 9.4 | 0 |
| 1 | 9.5 | 9.7 | 9.8 | 10.0 | 10.1 | 10.3 | 10.4 | 10.6 | 10.7 | 10.9 | 1 |
| 2 | 11.0 | 11.2 | 11.3 | 11.5 | 11.6 | 11.8 | 11.9 | 12.1 | 12.2 | 12.4 | 2 |
| 3 | 12.5 | 12.7 | 12.8 | 13.0 | 13.1 | 13.3 | 13.4 | 13.6 | 13.7 | 13.9 | 3 |
| 4 | 14.0 | 14.2 | 14.3 | 14.5 | 14.6 | 14.8 | 14.9 | 15.1 | 15.2 | 15.4 | 4 |
| 5 | 15.5 | 15.7 | 15.8 | 16.0 | 16.1 | 16.3 | 16.4 | 16.6 | 16.7 | 16.9 | 5 |
| 6 | 17.0 | 17.2 | 17.3 | 17.5 | 17.6 | 17.8 | 17.9 | 18.1 | 18.2 | 18.4 | 6 |
| 7 | 18.5 | 18.7 | 18.8 | 19.0 | 19.1 | 19.3 | 19.4 | 19.6 | 19.7 | 19.9 | 7 |
| 8 | 20.0 | 20.2 | 20.3 | 20.5 | 20.6 | 20.8 | 20.9 | 21.1 | 21.2 | 21.4 | 8 |
| 9 | 21.5 | 21.7 | 21.8 | 22.0 | 22.1 | 22.3 | 22.4 | 22.6 | 22.7 | 22.9 | 9 |
| 10 | 23.0 | 23.2 | 23.3 | 23.5 | 23.6 | 23.8 | 23.9 | 24.1 | 24.2 | 24.4 | 10 |
| 11 | 24.5 | 24.7 | 24.8 | 25.0 | 25.1 | 25.3 | 25.4 | 25.6 | 25.7 | 25.9 | 11 |
| 12 | 26.0 | 26.2 | 26.3 | 26.5 | 26.6 | 26.8 | 26.9 | 27.1 | 27.2 | 27.4 | 12 |
| 13 | 27.5 | 27.7 | 27.8 | 28.0 | 28.1 | 28.3 | 28.4 | 28.6 | 28.7 | 28.9 | 13 |
| 14 | 29.0 | 29.2 | 29.3 | 29.5 | 29.6 | 29.8 | 29.9 | 30.1 | 30.2 | 30.4 | 14 |
| 15 | 30.5 | 30.7 | 30.8 | 31.0 | 31.1 | 31.3 | 31.4 | 31.6 | 31.7 | 31.9 | 15 |
| 16 | 32.0 | 32.2 | 32.3 | 32.5 | 32.6 | 32.8 | 32.9 | 33.1 | 33.2 | 33.4 | 16 |
| 17 | 33.5 | 33.7 | 33.8 | 34.0 | 34.1 | 34.3 | 34.4 | 34.6 | 34.7 | 34.9 | 17 |
| 18 | 35.0 | 35.2 | 35.3 | 35.5 | 35.6 | 35.8 | 35.9 | 36.1 | 36.2 | 36.4 | 18 |
| 19 | 36.5 | 36.7 | 36.8 | 37.0 | 37.1 | 37.3 | 37.4 | 37.6 | 37.7 | 37.9 | 19 |
| 20 | 38.0 | 38.2 | 38.3 | 38.5 | 38.6 | 38.8 | 38.9 | 39.1 | 39.2 | 39.4 | 20 |
| 21 | 39.5 | 39.7 | 39.8 | 40.0 | 40.1 | 40.3 | 40.4 | 40.6 | 40.7 | 40.9 | 21 |
| 22 | 41.0 | 41.2 | 41.3 | 41.5 | 41.6 | 41.8 | 41.9 | 42.1 | 42.2 | 42.4 | 22 |
| 23 | 42.5 | 42.7 | 42.8 | 43.0 | 43.1 | 43.3 | 43.4 | 43.6 | 43.7 | 43.9 | 23 |
| 24 | 44.0 | 44.2 | 44.3 | 44.5 | 44.6 | 44.8 | 44.9 | 45.1 | 45.2 | 45.4 | 24 |
| 25 | 45.5 | 45.7 | 45.8 | 46.0 | 46.1 | 46.3 | 46.4 | 46.6 | 46.7 | 46.9 | 25 |
| 26 | 47.0 | 47.2 | 47.3 | 47.5 | 47.6 | 47.8 | 47.9 | 48.1 | 48.2 | 48.4 | 26 |
| 27 | 48.5 | 48.7 | 48.8 | 49.0 | 49.1 | 49.3 | 49.4 | 49.6 | 49.7 | 49.9 | 27 |
| 28 | 50.0 | 50.2 | 50.3 | 50.5 | 50.6 | 50.8 | 50.9 | 51.1 | 51.2 | 51.4 | 28 |
| 29 | 51.5 | 51.7 | 51.8 | 52.0 | 52.1 | 52.3 | 52.4 | 52.6 | 52.7 | 52.9 | 29 |
| 30 | 53.0 | 53.2 | 53.3 | 53.5 | 53.6 | 53.8 | 53.9 | 54.1 | 54.2 | 54.4 | 30 |
| 31 | 54.5 | 54.7 | 54.8 | 55.0 | 55.1 | 55.3 | 55.4 | 55.6 | 55.7 | 55.9 | 31 |
| 32 | 56.0 | 56.2 | 56.3 | 56.5 | 56.6 | 56.8 | 56.9 | 57.1 | 57.2 | 57.4 | 32 |
| 33 | 57.5 | 57.7 | 57.8 | 58.0 | 58.1 | 58.3 | 58.4 | 58.6 | 58.7 | 58.9 | 33 |
| 34 | 59.0 | 59.2 | 59.3 | 59.5 | 59.6 | 59.8 | 59.9 | 60.1 | 60.2 | 60.4 | 34 |
| 35 | 60.5 | 60.7 | 60.8 | 61.0 | 61.1 | 61.3 | 61.4 | 61.6 | 61.7 | 61.9 | 35 |
| 36 | 62.0 | 62.2 | 62.3 | 62.5 | 62.6 | 62.8 | 62.9 | 63.1 | 63.2 | 63.4 | 36 |
| 37 | 63.5 | 63.7 | 63.8 | 64.0 | 64.1 | 64.3 | 64.4 | 64.6 | 64.7 | 64.9 | 37 |
| 38 | 65.0 | 65.2 | 65.3 | 65.5 | 65.6 | 65.8 | 65.9 | 66.1 | 66.2 | 66.4 | 38 |
| 39 | 66.5 | 66.7 | 66.8 | 67.0 | 67.1 | 67.3 | 67.4 | 67.6 | 67.7 | 67.9 | 39 |
| 40 | 68.0 | 68.2 | 68.3 | 68.5 | 68.6 | 68.8 | 68.9 | 69.1 | 69.2 | 69.4 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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