

**EUGENE DIETZGEN CO.**  
DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on 1  $\frac{1}{2}$  see inside of back cover.  
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# 1812

INDEXED  
to page #74

36 + 76.76  
+ 14.05  
-----  
62.71

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

1

Handwritten notes and diagrams on the right page of the notebook, including a small sketch of a structure and the word "Draper" written vertically.

Cross Sec. Alley Bk 10	La Jolla Park	1
" " J St - 20 <sup>th</sup>	Silver Street to Bancroft.	12-24
Stake Set back	Olvera and Santa Isabel	39
Cross Sec. Alley Bk C	Belmont	40-48
Cross Sec. Sutherland St.	Pacific to Kurtz	49-53
Cross Sec. Hrdot's Road		54-69
Survey lot 27-28-29	Bk 117 Pacific Beach	70
Cross Sec. Kloubert Ave	19 <sup>th</sup> to	71-74
Topog. Proposed Tunnel	Pacific to Torrey Pines	75-79

ition  
 Dredg  
 Cold Bay  
 3400 ft. Par.  
 45

2175  
2160

Cross Section Silver St.  
& Alley Bk. to La Jolla Park

Oct. 22, 1947

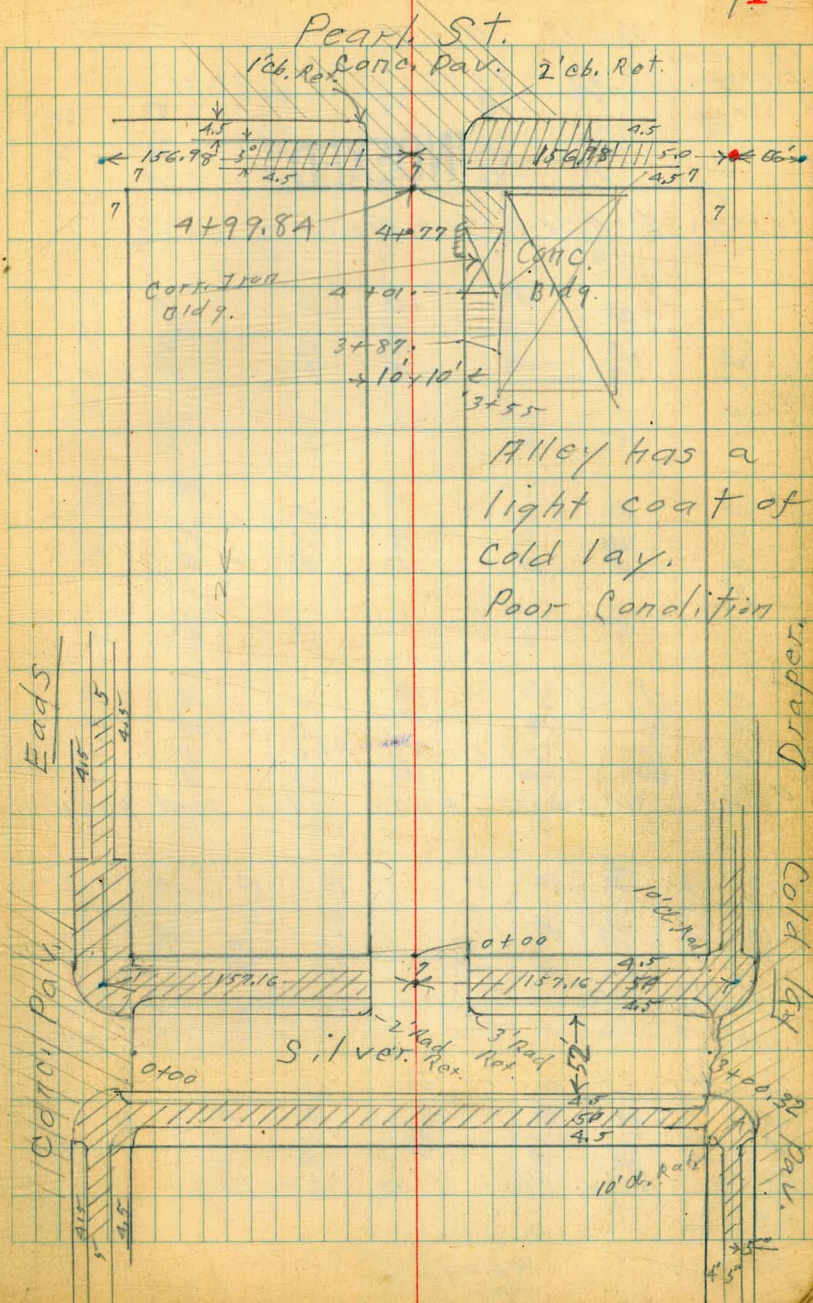
V.V.D. 31334

Sommer Meyer  
W. Moore  
E. Sherman

- = Found L+T.
- = Set. Lead & Dist
- = " Nail

INDEXED

S.W.B.P. Silver & Eads	3.84	86.84	9.63	83.00
T.P.	0.79	92.63	10.94	91.84
Set. B.M. on old B.P. N.E. Eads & Pearl	0.74	102.78	1.88	102.04
T.P.	3.27	103.92	8.50	100.65
T.P.	1.57	109.15	7.80	104.58
S.E.B.P. Bird & Pearl	0.21	115.38	—	115.17



Levels Silver St. (80' wide)

1/4 = 13' G. + Cl. = 26'

+ P. 2 x 2 1/4  
S.P. Silver  
Alley  
3.A7 83.18 7.13 79.71

INDEXED

1+50 1/4 Alley to south

1+00

0+50

0+00 = Wly. Line Ends also End paving

0-1A Cont.

0-1A = Wly. curb line Ends

86.84

indexed  
O.S.K.

4

22

83.02	84.65	84.19	83.05	82.65	80.91	81.25	80.74	80.96	81.01
3.82 36 top cl.	2.17 90 top cl.	2.65 90 cl.	3.79 70 cl.	4.19 80 cl.	5.93 36.1 20.	5.57 13 1/4	6.10 40 cl.	6.38 36 cl.	5.83 36 cl.
82.57	82.98	82.59	82.31	81.94	81.42	80.73	80.74	80.96	81.01
4.30 36 cl.	3.86 cl.	4.25 cl.	4.53 1/4	4.90	5.42 1/4	6.19 cl.	6.10 40 cl.	6.38 36 cl.	5.83 36 cl.
82.39	82.13	81.3	81.1	80.7	80.1	79.3	80.65	80.97	80.97
4.45 26	4.71 cl.	5.5 cl.	5.7 1/4	6.1	6.7 1/4	7.5 cl.	6.19 cl.	5.87 cl.	5.83 36 cl.
81.95	82.13	81.3	81.1	80.7	80.1	79.3	80.65	80.97	80.97
4.89 13 1/4	4.71 cl.	5.5 cl.	5.7 1/4	6.1	6.7 1/4	7.5 cl.	6.19 cl.	5.87 cl.	5.83 36 cl.
81.58	82.13	81.3	81.1	80.7	80.1	79.3	80.65	80.97	80.97
5.26	4.71 cl.	5.5 cl.	5.7 1/4	6.1	6.7 1/4	7.5 cl.	6.19 cl.	5.87 cl.	5.83 36 cl.
80.2	81.23	80.3	80.1	79.8	79.2	78.4	77.7	78.42	78.42
5.6 40	5.61 cl.	6.5 cl.	6.7 1/4	7.0	7.6 1/4	8.4 1/4	8.3 cl.	8.12 cl.	8.12 cl.

86.84

T.A 2x2  
S. 75 Silver  
#71127

829 88.00 3.47 79.71

Silver St.

3+14<sup>32</sup> Cont.

INDEXED

cold lay from here on is O.K.

3+14<sup>32</sup> = Fly. Ch. line Draper.

rather poor condition

start of cold lay. in

3+04<sup>32</sup> = B.C. Comb. Returns Also Approx.

3+00<sup>32</sup> = Fly. line Draper

2+50

2+00

83.18

	L	R	R+	3
78.71	78.71	77.55	77.55	76.71
147 70 Cl.	5.3 90 Cl.	5.63 40 Cl.	6.4 40 Cl.	7.8 40 Cl.
76.7	76.7	76.3	75.8	75.4
5.13 36 Cl.	6.5 36 Cl.	6.9 26	7.4 14	7.5 14
76.4	76.4	76.2	76.1	75.9
5.60 Cl.	6.8 Cl.	7.0 14	7.1	7.3 14
77.59	77.59	76.4	76.2	75.6
5.59 Cl.	6.8 Cl.	6.9 14	7.0	7.3 14
78.48	78.48	76.3	76.1	75.6
4.90 Cl.	6.0 Cl.	6.9 14	7.0	7.3 14
77.2	77.2	76.3	76.2	75.9
5.60 Cl.	6.0 Cl.	6.9 14	7.0	7.3 14
79.39	79.39	76.1	76.1	76.1
3.79 Cl.	5.2 Cl.	5.1 14	5.2	5.8 14
78.0	78.0	76.6	76.6	76.6
5.2 Cl.	5.2 Cl.	5.1 14	5.2	5.8 14
77.4	77.4	76.1	76.1	76.1
5.8 14	5.3 Cl.	5.2 Cl.	5.2	5.8 14
76.9	76.9	76.9	76.9	76.9
5.3 Cl.	5.3 Cl.	5.2 Cl.	5.2	5.8 14
77.86	77.86	76.05	76.05	76.05
5.52 Cl.	5.52 Cl.	5.2 Cl.	5.2	5.8 14

83.18

Alley Bk. 10. La Jolla Park

Lt.

¢

Rt.

44

# INDEXED

0+29<sup>5</sup> 27' Rt. =  $\Phi$  Sing. Car. door

0+26 10<sup>8</sup> Lt. =  $\Phi$  doorway in Bldg.  
<sup>1<sup>1</sup>/<sub>2</sub>' wide</sup>

0+22 10<sup>2</sup> Rt. = end Conc. Wall.  
95' Rt. = start Conc. Apron to Sing. Car

0+04 10<sup>2</sup> Lt. start Frame Bldg.

0+00 Cont. 10<sup>2</sup> Rt. = start 6" Conc. wall

0+00 = Sty. Line Silver

0-14 = Sty. Cb. line Silver St.

88.00  
mm

Indexed  
e.s.k.

81.83

6.17  
<sup>27</sup>  
Cone Floor

82.21

5.76  
<sup>10.9</sup>  
sill

81.7

6.3  
<sup>10</sup>

81.7

6.3  
<sup>9</sup>

81.1

6.9  
<sup>8</sup>

81.3

6.7

81.33

6.67  
<sup>9.5</sup>  
<sup>Apr 100</sup>

81.2

6.8  
<sup>10</sup>

80.5

7.5  
<sup>10.2</sup>  
Base  
wall

81.81

6.19  
<sup>10.2</sup>  
top  
wall

79.5

8.5  
<sup>10.4</sup>  
Bottom  
wall

81.36

6.69  
<sup>10.4</sup>  
top  
wall

80.71

7.26  
<sup>10</sup>  
End of

80.5

7.5  
<sup>10</sup>

80.1

7.9  
<sup>6</sup>

80.3

7.7

80.1

7.9  
<sup>10</sup>

80.29

7.71  
<sup>10</sup>  
End of

80.1

7.9  
<sup>10.9</sup>  
End

79.0

9.0  
<sup>10</sup>

80.14

7.86  
<sup>7.0</sup>  
3' Rad  
ket

80.48

7.52  
<sup>7.0</sup>  
2' Rad  
ket

79.5

8.5  
<sup>10</sup>

79.3

8.7

88.00

rug cleaning plant

1+42 25<sup>E</sup> Lt. = End service door to

**INDEXED**

1+30

door to rug cleaning plant.

1+20 25<sup>E</sup> Lt. = start double service

11<sup>E</sup> Rt. = start board pence

1+02 11<sup>E</sup> Rt. = End board shed

1+00 10' Rt. = P. pole # A 7579

0+88 10<sup>E</sup> Rt. = start board shed

0+52 8<sup>E</sup> Lt. = T. pole 305944H

0+50

0+49 10<sup>E</sup> Lt. = End Frame Bldg.

0+37 9<sup>E</sup> Rt. = End Conc. Apron

88.00  
~~~~

2.21  
25.5  
Conc. Floor  
85.79

85.3

2.7  
20

84.7

3.3  
10

84.6

3.4  
7

85.0

3.0

84.6

3.4  
7

84.9

3.1  
10

2.26  
25.5  
Conc. Floor  
85.74

84.8

3.2  
10

84.0

4.0  
10

84.0

4.0

83.8

4.2  
7

84.2

3.8  
10

83.2

4.8  
30

82.9

5.1  
10

82.3

5.7  
8

82.5

5.5

82.1

5.9  
8

82.4

5.6  
10

82.1

5.9  
30

6.38  
9.2  
81.62

88.00  
~~~~



INDEXED

2+66 on shed.  
End 1<sup>2</sup> Faves start 0<sup>2</sup> Faves

board fence.

start core wall topped by

2+50 = 10<sup>4</sup> Lt. = End  $\Phi$  Hedge also =

T.P. 7.93 94.64 1.29 86.71

2+24 10<sup>3</sup> Lt. =  $\Phi$  4' wide Hedge start hedge

12 Faves (Eaves on line)

11<sup>2</sup> Rt = start board barns

2+20 12<sup>2</sup> Rt = End board fence

2+09 15<sup>1</sup> Lt. =  $\Phi$  double Gar. Dirt floors

2+00 9<sup>2</sup> Rt. = P pole # H 7563

1+98<sup>5</sup> 8<sup>3</sup> Lt. = T. pole # D19072T + JAH 7564

1+60

88.00  
~~~~~

|                         |                          |           |       |           |           |
|-------------------------|--------------------------|-----------|-------|-----------|-----------|
| 96.1                    | 87.5                     | 87.6      | 88.0  | 87.7      | 87.9      |
| 4.5<br>10.4<br>top wall | 7.1<br>10.4<br>base wall | 7.0<br>10 | 6.6   | 6.9<br>8  | 6.7<br>10 |
|                         |                          |           | 94.64 |           |           |
|                         | 86.9                     |           |       |           |           |
|                         | 1.1<br>15.1<br>87.1      |           |       |           |           |
| 87.4                    | 86.8                     | 86.4      | 86.6  | 86.6      |           |
| 0.6<br>3.0              | 1.2<br>10                | 1.6<br>8  | 1.4   | 1.4<br>10 |           |
|                         | 85.8                     | 85.6      | 85.6  | 85.4      | 85.7      |
|                         | 2.8<br>10                | 2.4<br>7  | 2.4   | 2.6<br>7  | 2.3<br>10 |

88.00  
~~~~~

Alley BIK 10 La Jolla Park

3+26 11<sup>2</sup> Lt. = start lath fence

**INDEXED**

and board fence. N.B.

12<sup>E</sup> Rt. = start. wire, slat, lath,

3+17 8<sup>3</sup> Lt. = T. pole # 897724.

3+12 22<sup>2</sup> Rt =  $\Phi$  Sing. Gar. dirt floor.

3+10 17<sup>4</sup> Lt. =  $\Phi$  Sing. Gar. dirt floor

12.4 Rt. = End Frame @ barns

3+00 10<sup>3</sup> Lt. = End Conc. Bldg.

2+96<sup>E</sup> 10<sup>0</sup> Rt. = P. pole # A 7537

2+89 10<sup>4</sup> Lt = start Conc. Bldg.

2+84<sup>E</sup> 10<sup>5</sup> Lt. =  $\Phi$  9' wide board gate

2+80 10<sup>5</sup> Lt. = End Conc. wall + fence

94.64

89.2  

---

5.4  
22.7

89.44  

---

5.2  
17.4

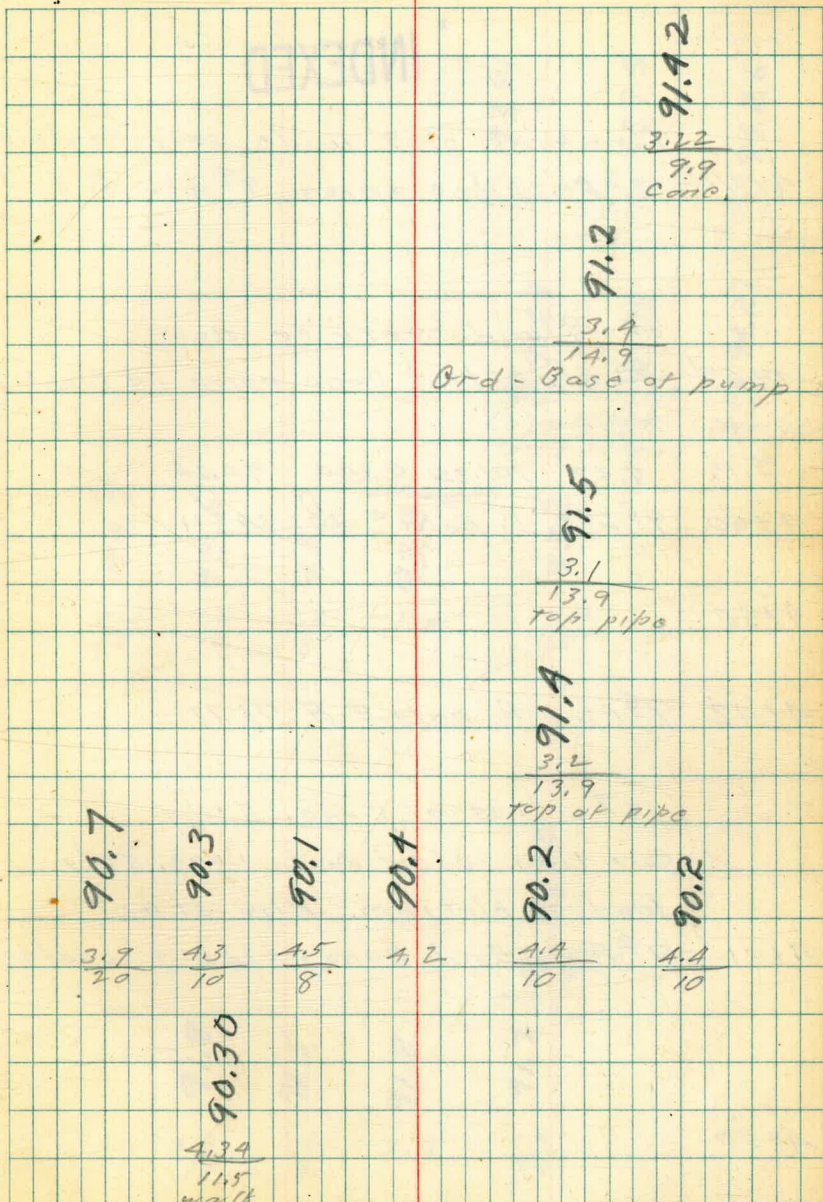
89.1	88.8	89.0	88.8	89.1
<hr/> 5.5	<hr/> 5.8	<hr/> 5.6	<hr/> 5.8	<hr/> 5.5
10	8		8	10

90.1	88.2	88.7	88.5	88.5	88.4	88.6
<hr/> 4.5	<hr/> 6.4	<hr/> 6.0	<hr/> 6.1	<hr/> 6.1	<hr/> 6.2	<hr/> 6.0
10.5	10.5	10	8		8	10
Wall	Wall					

94.64

- platform over conc. slab.
- 3+87 9<sup>2</sup> Rt. = start wooden loading
- 3+85 9<sup>2</sup> Rt. = start Conc. slab
- 3+77 14<sup>2</sup> = Ctr. Visual Gasoline pump.
- 3+73 13<sup>2</sup> Rt. = Gasoline tank Fill pipe
- 19<sup>2</sup> Rt. = Start conc. bldg
- 3+55 13<sup>2</sup> Rt. = oil tank Fill pipe
- lath, slat, + board fence.
- 12<sup>2</sup> Rt. = End peer. Comb. wire,
- 3+50 11<sup>2</sup> Lt. = End lath fence
- 3+36<sup>E</sup> 11<sup>2</sup> Lt. =  $\pm$  18" wide Conc. walk.

94.64



94.64

INDEXED

Threshold of 8' wide service door,  
 A+71<sup>E</sup> 8<sup>2</sup> Rt. = Edge apron 9<sup>2</sup> Rt. =  $\Phi$

of 8' wide service door  
 A+67<sup>E</sup> 9<sup>2</sup> Rt. = Start Conc. Apron in front

T.P. 7.58 101.82 0.10 94.24  
 A+60 9<sup>2</sup> Lt. = T. pole # 402993H

A+50

A+42 9<sup>6</sup> Rt. = P. pole # A 7511

(199 = line of Conc. Bldg  
 Corr. iron addition to Conc. Bldg.  
 loading platform. Also start  
 A+01 } 9<sup>2</sup> Rt. = End Conc. slab + wooden

A+00

94.64

				93.81	93.95	94.26
				8.01 8.9 Edge Apron	7.87 9.8 At Bldg	7.56 9.9 $\Phi$ door- way
				93.68	93.78	94.27
				8.14 9.0 Edge at Apron	8.04 9.9 at Bldg Apron	7.55 9.9 Threshold
94.2	93.6	93.0	<u>101.82</u>	93.2	93.2	
0.4 50	1.0 10	1.6 8	1.4	1.4 10		
				91.8	91.8	91.8
				2.84 9.9 Conc.		
91.8	91.5	91.8		91.7		
2.8 10	3.1 8	2.8		2.9 9.9		
			<u>94.64</u>			

INDEXED

With curb.

5+05 10' RT. = End Conc. slab, Level

5+00 = start. Conc. paving + Cbs.

4+99<sup>84</sup> = N. Line Pearl.

4+95 19<sup>5</sup> RT. = End Conc. Bldg.

9<sup>2</sup> RT. = start conc. slab

4+78 9<sup>2</sup> RT. = End conc. apron also

4+77 9<sup>2</sup> RT. = End Corr. Iron Bldg.

101.82

6.56 10 End cc	95.26	6.23 10 pav	94.89	7.45 10 pav	94.37	7.34 10 pav	94.98	7.24 10 Curb + slab	94.58
		6.59 10	94.9	7.14	94.4	7.3 9.9	94.5	7.11 10 on conc slab	94.71
		6.7 10	95.1	7.2	94.6	7.10 9.9 conc. slab	94.2	7.40 10 conc	94.42
						7.94 9.2 End Apron	93.88	7.93 9.9 start Conc. slab	93.89

101.82

INDEXED

S.E.B.P. Orig. B.M.  
Girard + Pearl. 0.75 115.17 115.17

T.P. 7.96 115.92 2.42 107.96

N.E.B.P.  
Pearl + Eads 8.34 110.38 0.27 102.04

T.P. 12.25 102.31 0.91 90.06

S.E.B.P.  
Pearl + Souier, 10.05 90.97 10.05 80.92

N.W. 111 Hack  
Pearl. + Draper (S. Shot) 1.89 89.08

T.P. 0.88 90.97 11.73 90.09

5 + 13<sup>84</sup> = Nly. Ch. line Pearl.

101.82

96.22	95.77	95.04	94.54	94.21	93.98	94.39	92.70	93.24
5.60	6.05	6.78	7.28	7.61	7.84	7.43	9.12	8.58
50	50	Top 1'	10		10	Top 2'	50	50
Ch.	B	Rd	B		A	Rad.	B	Ch.
		Ch. Ret.				Ch. Nay.		

101.82

7-Sect. J St. - 30<sup>th</sup> to Bancroft.

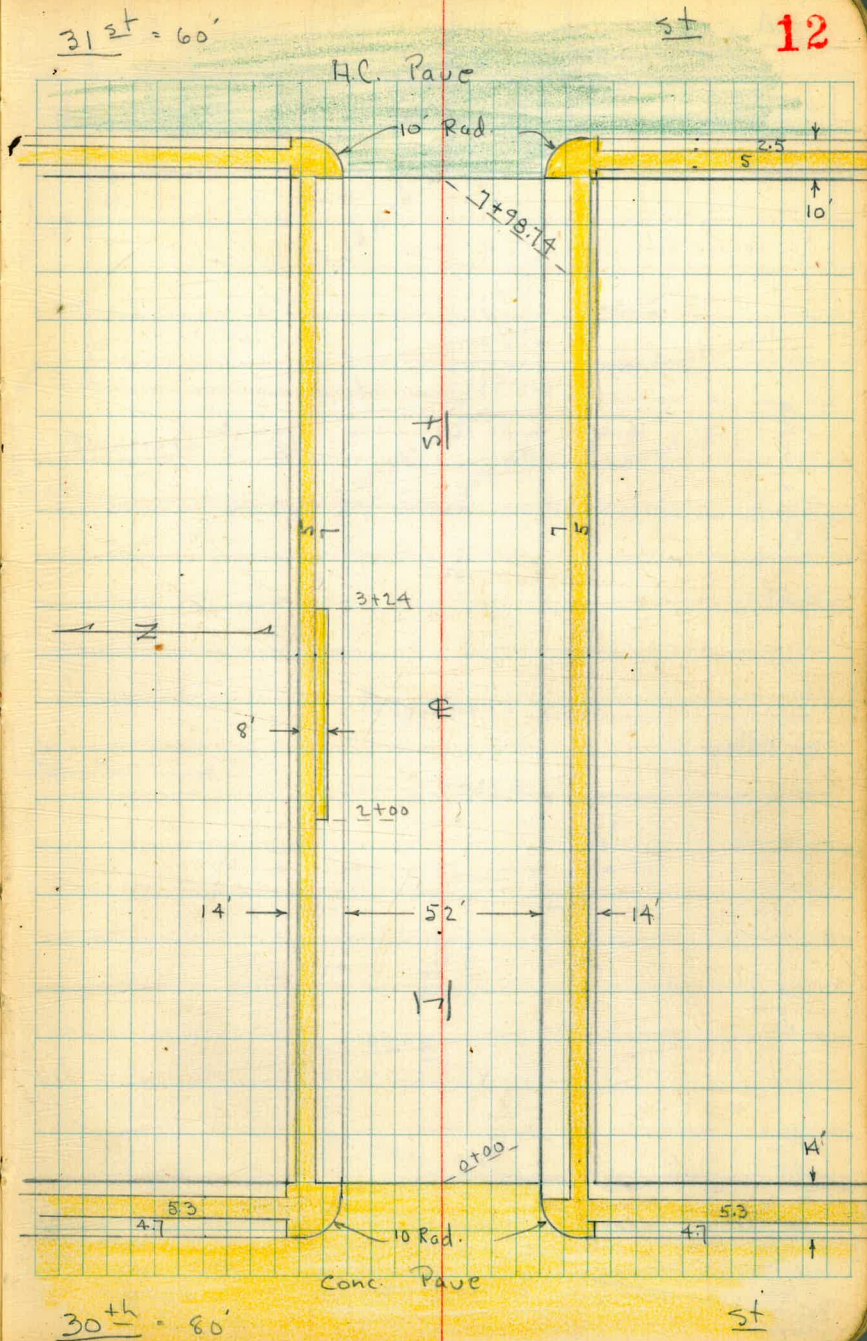
# 2011

W.O. 31209

1-28-48

Osborne  
Hardin  
Worrell  
Sherman

INDEXED  
JAN 29 1948



32<sup>nd</sup> = 60'

st

Conc. Pav

10' Rad

4+21.21

25

5

10

Grounds

4

52'

14

st

2+50

20' Alley

2+30

1 Z

School

17

17

0+50

0+00

10 Rad

10

31<sup>st</sup> = 60'

H.C. Pav

st

13

4+37.2  
End wall

= Bot of Steps

st

Prop  
Culvert

10'

Larens Lane

3.7' wood steps

3+81.5

8" Conc.  
Ret. Wall

Fd. Mon.

10'

0+83+64

Prop Culvert

28.61

Dancroft st

st

3+33.9 = End ab.

3+32.88

3+33.3 = End ab.

Fd. Mon.

90° 48'

14'

52'

14'

st

st

st

st

0+00

10 Rad

10

32<sup>nd</sup> = 60'

Conc. Pav

st





2+93 = ± 14' Conc. Dr. on Lt.

2+60

T.P. 5.48 80.13 7.50 74.65

2+20

2+01 = E. end of opening

1+96 = 4 New Inlets - Both Sides

11.22  
F.L.  
18" pipe

Sides - see New Plan

1+91 = w. end of 10' opening to inlets on Both

1+50

1+41 = ± 13' Conc. Dr. on Rt.

	Lt.	+	Rt.
Top	74.34		
Grate	74.61		
edge of Grate	73.89		
Top	74.10		
Grate	73.7		
edge of Grate	74.3		
Top	74.6		
Grate	73.8		
edge of Grate	73.2		
Top	73.32		
Grate	73.16		
edge of Grate	73.07		
Top	74.15		
Grate	73.27		
edge of Grate	74.2		
Top	74.2		
Grate	73.8		
edge of Grate	73.0		
Top	72.23		
Grate	72.25		
edge of Grate	73.03		
Top	73.07		
Grate	73.08		
edge of Grate	73.07		
Top	74.18		
Grate	73.46		
edge of Grate	73.11		
Top	74.7		
Grate	74.0		
edge of Grate	73.1		
Top	73.1		
Grate	73.53		
edge of Grate	73.77		
Top	73.27		
Grate	73.88		
edge of Grate	73.8		
Top	73.77		
Grate	73.8		
edge of Grate	73.33		





1+50

T.P. 5.83 83.95 2.97 78.12

1+00

0+50

check B.M.

444 76.65

76.57 = Book

SE. RP. / 31st + J

0+05 - 13' Rt = 8" Water Gate

4.58

Top of Cap

60' E. = E.L. 31st = 0+00 ahead.

Rods on 31 Returns:

50' E. = E. cb.

30' E. = 31st

4.76.06	4.76.42	4.76.15	4.76.37	4.76.53	4.76.34	4.75.84	4.76.18	4.76.44
90	40	26	12	5	5	25	40	90
Top	Top	Top	Top	Top	Top	Top	Top	Top
4.76.53	4.76.94	4.76.03	4.76.48	4.76.35	4.76.54	4.76.34	4.76.15	4.76.33
90	90	40	40	26	13	13	40	90
Top	Top	Top	Top	Top	Top	Top	Top	Top
4.76.04	4.76.59	4.76.72	4.76.78	4.76.49	4.76.09	4.76.10	4.76.62	4.76.57
126	25.9	13	13	13	25.9	95	25.9	25.9
Top	Top	Top	Top	Top	Top	Top	Top	Top
4.77.77	4.77.1	4.77.6	4.77.1	4.77.1	4.77.1	4.77.1	4.77.1	4.77.1
33	40	35	35	35	35	35	35	35
Top	Top	Top	Top	Top	Top	Top	Top	Top
5.78.10	6.77.5	6.77.9	6.77.9	6.77.9	6.77.9	6.77.9	6.77.9	6.77.9
26.5	25.5	31	31	31	31	31	31	31
Top	Top	Top	Top	Top	Top	Top	Top	Top

81.09



10' E. = W. cb.

Rods on ± 10 Rod. Returns.

81.06 = Book

NW. 7' ct.  
32<sup>nd</sup> + 5

check BM 4.99 86.17 5.18 81.18

6 + 01.21 = W.L. 32<sup>nd</sup> = edge of Conc. Pav

5 + 80

T.P. 5.11 86.36 2.70 81.25

5 + 50

5 + 00

4 + 50

	81.31	80.77	81.06	80.49	80.36	80.77	81.11	81.27	81.17	81.16	81.64	81.55	81.76
SW. A	4.86 91	5.40 90 put	5.11 40 Top	5.68 40 put	5.81 26	5.40 13	5.06 50	4.90 13	5.00 26	5.01 40 put	4.53 40 Top	4.82 90 put	4.41 90 Top
		81.73		81.08						80.41		81.05	
		4.44 Top		5.09 put						5.76 put		5.12 Top	N.W. ±
		81.08		80.35		80.82	81.13	96.17		81.28		80.89	81.68
		5.28 26 Top		5.01 26 put		5.54 13	5.23		5.08 13		5.47 26 put		4.68 26 Top
		80.94		80.9		81.1	81.4		81.2		80.9		81.35
		5.42 26 Top		5.0 26 put		5.3 13	5.0		5.2 13		5.5 26 put		5.01 26 Top
		80.69		80.2		81.0	86.36		81.1		80.7		81.08
		3.26 26 Top		3.8 26 put		3.0 13	2.7		2.9 13		3.3 26 put		2.87 26 Top
		80.39		79.9		80.4			80.5		80.2		80.58
		3.57 26 Top		4.1 26 put		3.6 13	3.2		3.5 13		3.8 26 put		3.37 26 Top
		80.06		79.5		80.1	80.3		80.2		79.8		80.06
		3.89 26 Top		4.5 26 put		3.9 13	3.7		3.8 13		4.2 26 put		3.89 26 Top

83.95





Improvements Extend Beyond.

3+32.88 = t + W.L. Bancroft St. - see sketch  
Sect along W.L.

T.P. 4.70 78.93 11.94 74.23 sq. in Eb.  
N.W. Cor.  
J + Bancroft

3+10

2+80

2+50

2+20

1+90

1+60

1+30

	Lt.				Rt.			
	90	20	44	42	49	45	42	42
	77.7	76.9	74.5	74.13	79.0	74.4	74.7	74.7
	55	40	26	26	13	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	78.31	76.13	75.2	75.6	78.93	75.9	76.0	76.76
	1.86	2.04	1.0	1.6	10.2	10.3	10.2	11.41
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	81.48	80.20	77.4	77.9	78.2	78.0	77.8	78.58
	1.69	1.97	1.74	1.3	8.0	8.2	8.4	8.59
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	81.48	80.20	79.3	79.8	80.0	79.6	79.1	80.00
	1.69	1.97	1.69	1.4	6.2	5.6	5.1	5.6
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	81.48	80.6	81.1	81.2	81.2	80.8	80.4	81.22
	1.69	1.66	1.1	1.0	5.0	5.4	5.4	5.9
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	82.41	80.6	81.7	81.8	81.9	81.5	81.1	81.90
	1.69	1.66	1.69	1.8	1.9	1.1	1.1	1.2
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	82.78	82.0	82.1	82.1	82.3	82.0	81.7	82.30
	1.69	1.2	1.1	1.1	1.9	1.2	1.5	1.3
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	82.75	81.9	82.2	82.2	82.4	82.1	81.8	82.30
	1.69	1.3	1.0	1.0	1.4	1.1	1.1	1.1
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top
	82.75	81.9	82.2	82.2	82.4	82.1	81.8	82.30
	1.69	1.3	1.0	1.0	1.4	1.1	1.1	1.1
	26	26	26	26	26	26	26	26
	Top	Top	Top	Top	Top	Top	Top	Top

86.17

4+15

3+80

place to dump the water  
along Mc Larens Lane - Seems to be a poor  
3+64 - 10' Rt. of  $\pm$  = Beg. Profile for Prop Culvert.

to the East.

Conc. wall acting as a cb., and goes down "J"  
now turns to the North along Bancroft - the  
approx. E.L. of Bancroft. - Note: the water  
3+63.7 = W. face of 8" Conc. Ret. wall = along the

3+45 = Sect. - Normal to Bancroft

3+33.9 = end of cb. + walk on Lt.

3+33.3 = end of Curb + Walk on Rt.

6.88	7.2	6.35	6.8	6.17	6.5	6.72.3	5.88	5.5	5.73.05	5.5	5.73.05	72.05	72.60
Top wall	gr.	Top wall	gr.	Top wall	ground	ground	Top wall	Top wall	Top wall	Top wall	Top wall	Top wall	Top wall
9.0	9.0	4.0	4.0	2.6	2.6	2.6	10.8	10.8	10.8	10.8	10.8	10.8	10.8
72.05	71.7	72.58	72.1	72.76	72.4	72.3	73.05	71.4	70.9	70.3	70.4	70.4	70.4
74.41	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5
4.52	9.0	4.0	2.6	1.1	1.9	4.7	2.6	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05
endwalk													
74.30	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5
4.63	9.0	4.0	2.6	1.1	1.9	4.7	2.6	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05
74.10	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5
4.83	9.0	4.0	2.6	1.1	1.9	4.7	2.6	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05
Top end cb.													
75.09	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5
3.84	9.0	4.0	2.6	1.1	1.9	4.7	2.6	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05
Top end cb.													
75.29	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5
3.64	9.0	4.0	2.6	1.1	1.9	4.7	2.6	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05
Top end walk													
75.30	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5
3.63	9.0	4.0	2.6	1.1	1.9	4.7	2.6	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05	7.3.05
Top end													
78.93	71.9	72.9	73.2	73.8	74.0	74.2	73.9	73.05	70.5	69.2	68.3	69.4	68.5

				sw. 30 <sup>th</sup>
check Starting B.M.	2.97	77.00	77.01	
5.49	79.97	6.12	74.48	
3.95	80.60	6.96	76.65	SE. 31 <sup>st</sup>
2.43	83.61	4.18	81.18	NW. 7 <sup>th</sup> 32 <sup>nd</sup>
T.P.	11.13	85.36	74.23	= BM in cb. Bancroft.

A+65 = end.

A+37.2 = End of Wall = Toe slope

41.9  
43.53  
35.40  
0.8  
Top  
wall  
end.

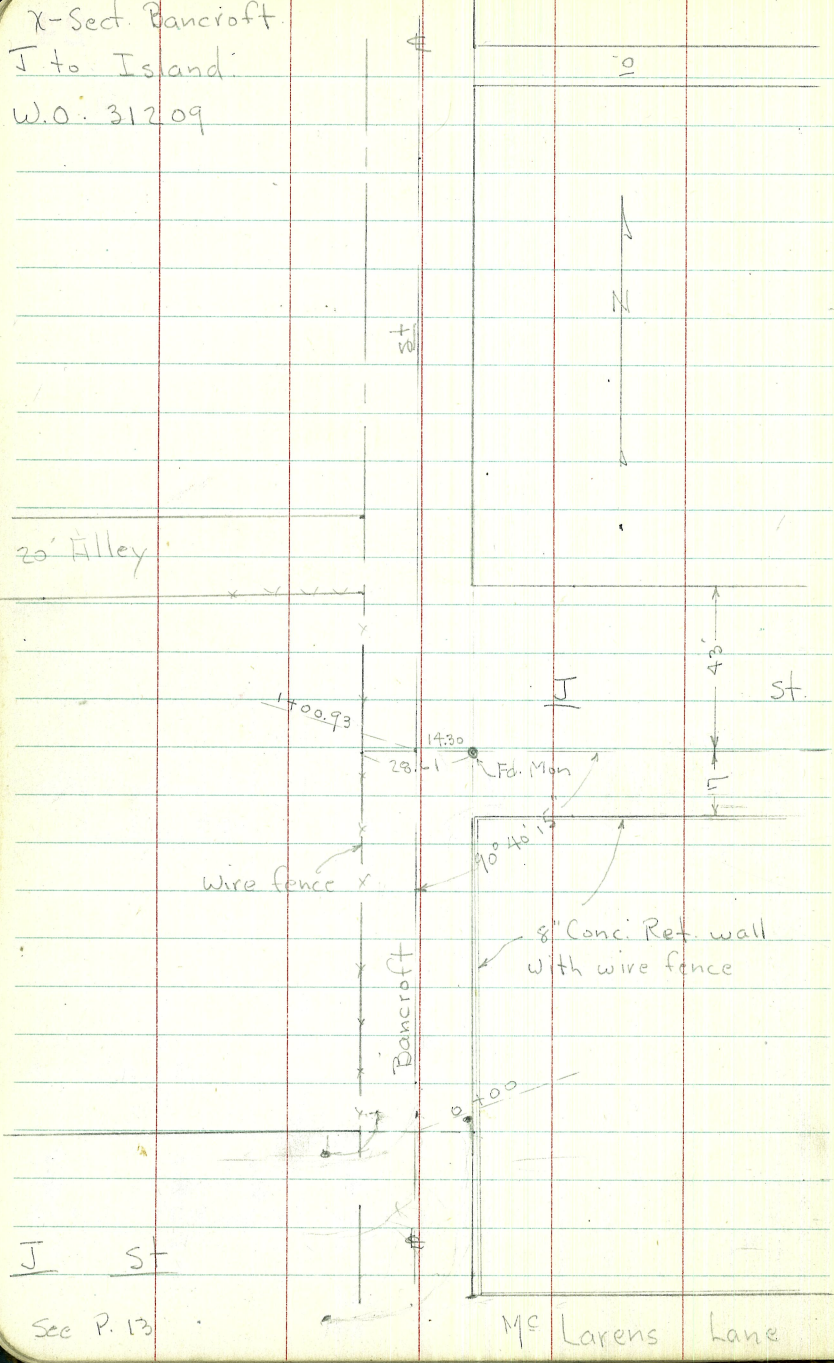
42.4  
36.5  
A  
10  
37.3  
0.8  
9.1

42.4  
36.5  
A  
15  
37.8  
A  
10

40.5  
38.4  
15

78.93

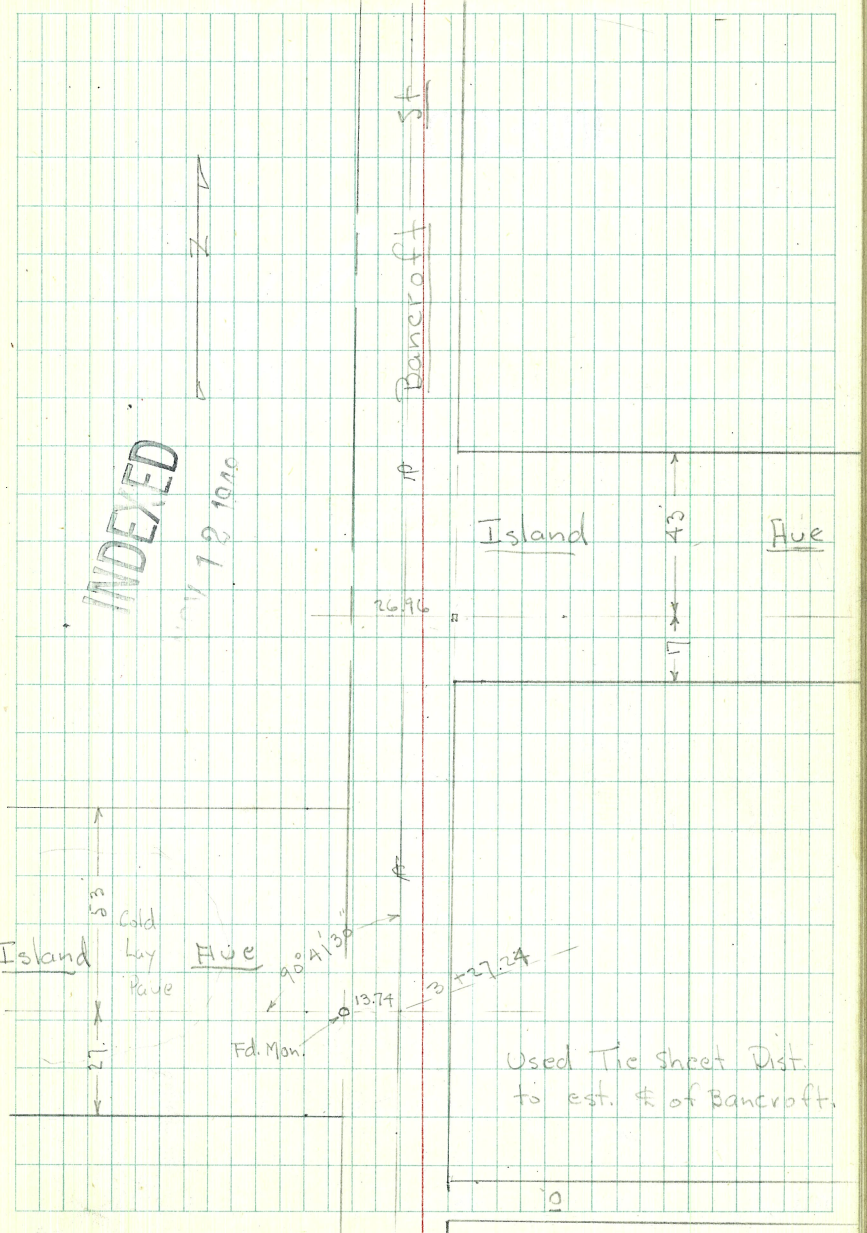
X-Section Bancroft.  
 J to Island.  
 W.O. 31209



See P. 13

M<sup>c</sup> Larens Lane

3-3-48  
 70.



Used Tie Sheet Dist.  
 to est. # of Bancroft.

X-Sect. Bancroft - from N.L. J st.  
to the W. to Island - to the E.

# INDEXED

1+13.93 =  $\pm$

~~Indexed~~

0+93.93 = S. cb Line J

1+11 - 15.5 Lt. =  $\pm$  8" Pepper

0+83.93 = S.L. J to E. + 14.9' Rt = end = Cor. of  
Conc. Wall - goes E. along S.L. of J. st

0+60

0+40 - 12.2 Lt. =  $\pm$  8" Pepper

0+36 - 15.4 Lt. = wly P. pole - # J.P. 418

0+25

<sup>6' Long</sup>  
brick wall - + wire fence

0+00 = N.L. J st. to W. - 14.2 Lt. = Cor. Small

B.M.      2.80      77.03      74.23      on cb.  
at J.

Lt. = W.

Rt = E. 26

	+0.77.9 20.9	0.77.0 14.3	0.74.9 0	0.70.0 0	0.69.0 0	0.68.2 14.3	0.65.7 25	0.54.3 18.7
	+2.1 20	+1.78.0 14.3	0.75.4 0	0.70.6 4	0.69.5 0	0.68.6 14.3	0.67.4 25	0.54.3 18.7
	+2.79.5 20	+1.78.5 14.4	0.76.1 0	0.71.3 0	0.70.8 0	0.70.3 14.9	0.71.82 14.9	0.67.1 25
	+2.79.9 20	+1.78.3 14.4	0.76.2 0	0.71.8 0	0.71.6 4	0.71.4 14.4	0.71.95 14.4	0.67.8 18.7
	+1.78.3 20	+0.77.5 14.5	0.75.7 0	0.73.2 0	0.72.4 6	0.72.3 10	0.72.35 15.6	0.68.0 25
	+0.77.9 14.2	0.74.6 14.2	0.73.8 10	0.72.8 4.2	0.72.5 10	0.72.2 14.5	0.72.59 16	0.71.3 17
	Top-Cor. Wall	Ground					Top 8' wall - Conc. Wire fence	
				77.03				

2+61 - 13.5 Rt = End Wire fence at Cor. Gar.

1+59 - 13.7 Rt = 4.5 Conc. Slab along Small Gar.  
used as House - wood floor

2+40

2+00

1+92 - End picket + beg. Wire fence - Beg. walk = 2'  
T.P. 8.29 76.59 8.73 68.30

1+60 - 17.2 Rt = wly. 1.5' Conc. walk along House

1+43.93 - 14.2 Rt = Beg. Picket fence  
to W.

1+43.93 = N.L. J. - also Profile in 20' Alley

1+40 - 15.6 Lt = wly. P. pole # P 424

1+39 - 14.3 Lt = end wire fence

1+33.93 = N. cb.

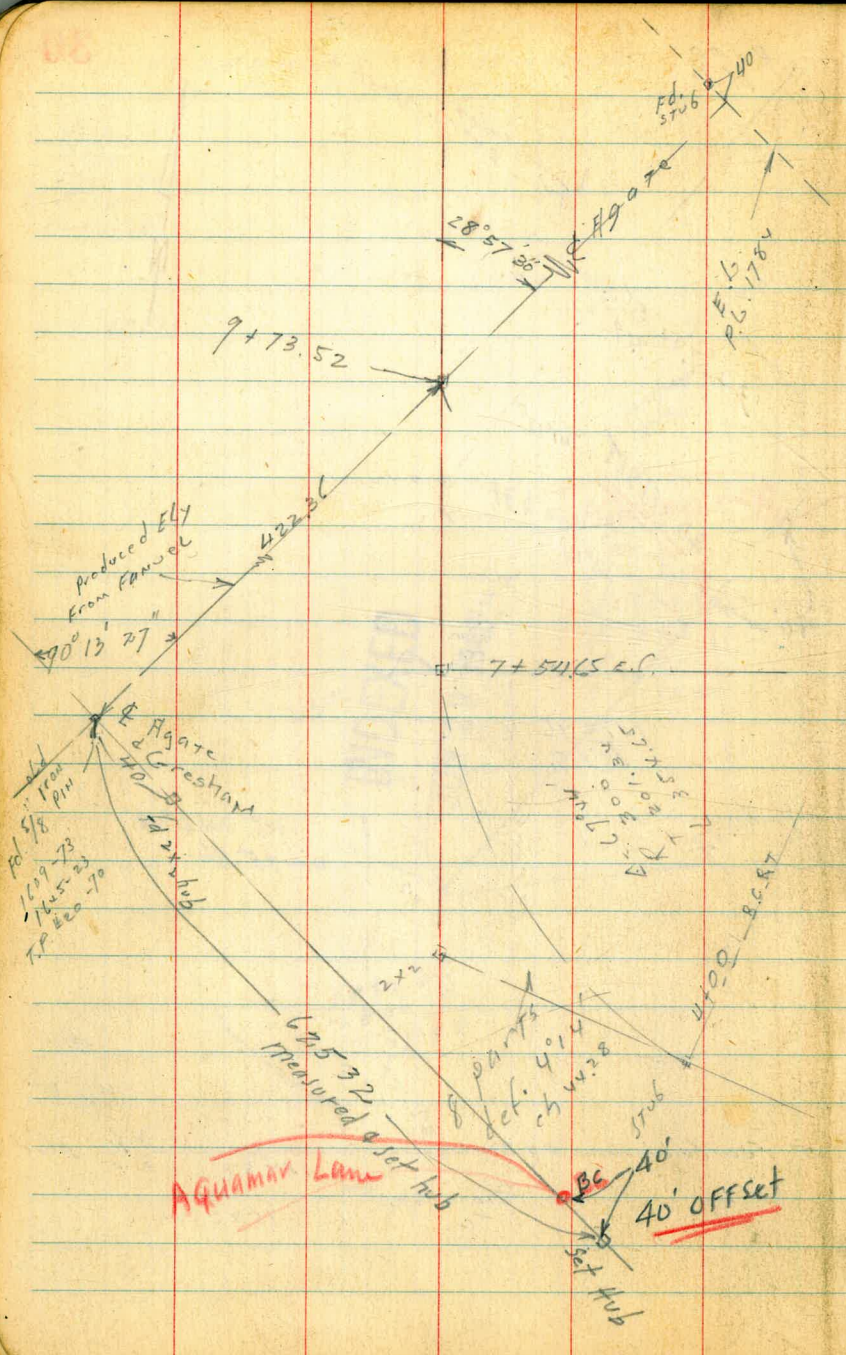
	Lt.	R	Pt.	
			66.0	
			10.6	10.66.58
			13.5	13.5
			ground	floor
				10.65.64
				10.95
				Top
				Conc.
			73.8	
			2.8	69.2
			24	13.9
			along fence	
			8.6	68.0
			0.0	0.66.6
			10.66.1	
			10.5	10.59
			13.9	11.46
			edge walk	
			65.15	
			47.3	
			72.2	
			70.2	
			47.3	
			66.8	
			10.66.6	
			10.0	
			13.9	
			10.65.77	
			16.8	
			edge walk	
			75.2	
			74.3	
			72.6	
			68.1	
			67.9	
			66.76	
			10.7	66.33
			9.6	67.4
			10.7	66.60
			20.6	20.6
			Top walk	ground floor
				House
			84.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	
			67.8	
			66.1	
			57.8	
			7.8	
			100	
			84.4	
			77.3	
			75.8	
			72.9	
			69.9	
			68.4	









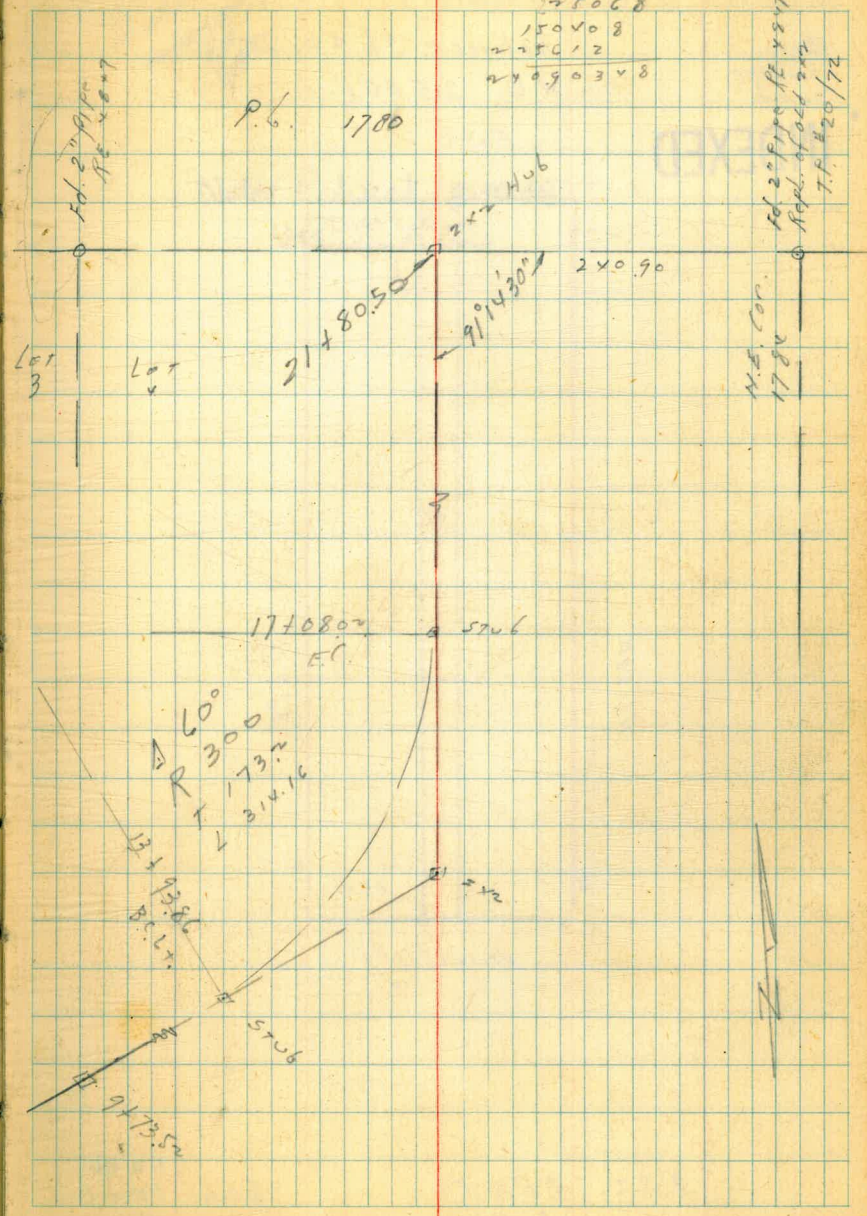


**Aquamarine Lane**  
 Measured offset hub  
 40' offset

16° 03' 250.68  
 261

→ 1068  
 150 408  
 2250 12  
 2409 03 48

31



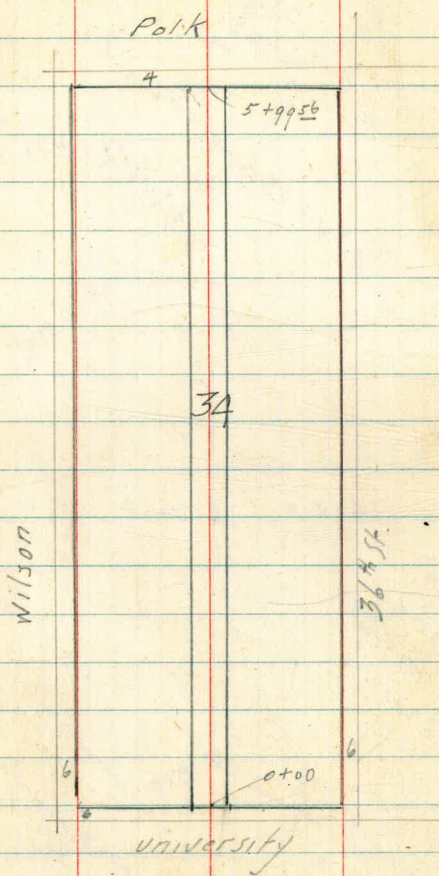
p.l. 1780

14.5 Cor  
 1780  
 16.2° Pipe ft. x 197  
 Red. of old ans  
 T.P. 20/72

60°  
 300  
 173.2  
 314.16

A Section Alley 34 University to Polk 12/7/48  
Begg  
Sherman  
Bunch  
between 36 & Wilson  
W O 25001

**INDEXED**



393

36454

360.61

NW BR  
Univ &  
Wilson

~~Indexed~~  
B

32

Notes Reduced 8-30-48  
Hemmington

TP 5.98 367.42 3.10 361.44

1+00 10.19 end Cal B/H

+80 10.19 Cal B/H House beg

0+50 9.3 Lt 477771 H

0+27 8.8.19 P. Pole JP A 4004

0+25

0+00 N. of Univ

0-14

364.54

361.9

2.6  
30

361.4

3.1  
10

361.2

3.2

361.3

3.2  
10

361.1

3.4  
30

361.0

3.5  
10

360.6

3.9

360.6

3.9  
10

361.0

3.5  
25

360.4

4.1  
30

360.3

4.2  
10

360.3

4.2

360.1

4.4  
5

360.5

4.0  
10

360.3

4.2  
30

360.15

4.39  
10

end CB

360.15

4.39  
10

9

360.0

4.5

360.0

4.5  
10

9

360.15

4.39  
15

CB end

359.50

5.04  
40  
9

360.07

4.47  
40  
CB

359.39

5.15  
12  
9

359.69

4.85  
12  
CB

359.46

5.08

359.33

5.21  
10  
9

359.72

4.82  
12  
CB

359.69

4.85  
40  
CB

359.21

5.33  
40  
9

364.54

2+03 <sup>corn</sup> beg apron 10.2 ft beg Stuc Bldg 13.1

2+00 end of garage

1+92 1/2 garage

13.8 ft dbl gar

1+83 end Bd fence 10 ft. beg dbl garage

9.8 ft beg bk fence

1+50 8.4 ft 47777 2 ft. Pale

1+48 14.6 end Shed

1+46 14.5 end Stuc Ho

1+30 14.6 ft Beg Shed

1+20 11.9 ft Beg Stuc Ho

1+11 11.5 apron Rt 1/2 garage single

367.42

362.2

5.2

30

362.1

5.3

10

362.0

5.4

362.71

4.71

10.2

362.3

5.1

10

362.94

4.48

13.1

362.2

5.2

13.8

362.0

5.4

10

361.6

5.8

361.6

5.8

10

361.38

6.04

11.5

apron

361.87

5.55

14.8

367.42

+50 9.1 Lt Pole Power & Tel No number  
 +50 end fence 10 Rf  
 3+49 end bd fence 9.8 Lt  
 } beg bd fence 19.5 L  
 3+00 } beg bd shed 12.5 R  
 2+99 end 2 door gar  
 97 end shed 12.5 R  
 +84 beg shed 12.5 R  
 2+79 beg 2 door gar  
 2+74 end both fence 10"  
 +52 beg both fence 10 R  
 } 8.8 Lt PA 4049  
 2+49 end of corr apron & Bldg Struc.  
 North end has 3 door gar.

367.42

364.14	363.96	363.7	363.5
3.28	3.46	3.7	3.9
14.8	9.8		10

364.14	363.44
3.28	3.98
14.9	9.9
	apron

363.0	362.90	362.84	362.92
4.4	4.52	4.58	4.58
10		10.2	13.1
		apron	

367.42

+94 17.0 R  $\pm$  sing gar

+83 9.3 Rt end bd fence

+76 9.1 Lt Pole PA 4079

+66 14 Lt end Picket fence

+50 9.3 Rt beg bd fence

+43 15.2 Rt Sing gar

+33 end wire fence beg picket 135H

4407 Sing gar 15.8 R

TD 6.55 373.58 0.39 367.03

4408 beg wire 13.7 Lt

3450

367 42

369.02

36

4.56

17

368.3

5.3  
10

368.6

5.0

368.5

5.1  
8

369.0

4.6  
10

368.72

4.86  
15.2

367.48

6.10  
15.8

373.58

367.2

0.2  
10

367.1

0.3

367.2

0.2  
10

365.4

2.0  
10

365.2

2.2

365.2

2.2  
10

367 42

5+9956 Prop Pole 10.844.

+85

+70

+63 10.2 Lt beg pickat fence

+57 12.8 Rt of 3.3 wide walk

+56 sing garage

+50

5+11 sing garage

5+00

37358

369.15

4.43

CB

10

368.88

4.70

9

369.8

3.8

10

370.1

3.5

10

370.53

3.05

14.0

370.02

3.52

10.1

369.9

3.7

10

369.23

4.35

14.3

369.01

4.57

12.1

apron

368.7

4.9

10

368.73

4.85

369.7

3.9

370.1

3.5

369.9

3.7

369.1

4.5

368.80

4.78

9.10

369.8

3.8

10

369.8

3.8

10

370.12

3.46

12.8

369.9

3.7

10

369.0

4.6

10

368.94

4.64

CB end

37

373 58



BM. 4.74 359.60 B.M. 36  
 3.73 364.34 360.61 B.M. Wilson

flat check

BM 3.30 367.92 8.32 359.60 359.54  
 TP 4.14 373.47 8.85 364.62 .06

TP on t. 4.25 369.33 Mail Power Pole

Profit 07.0

373.58

a unit  
 a unit

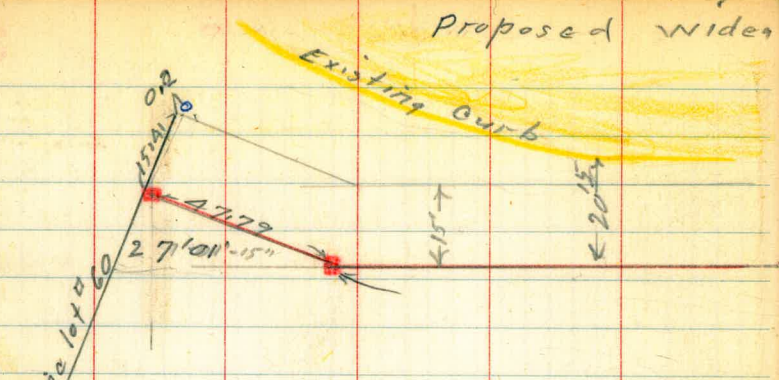
Note There is an error of .04 between these two benches as listed in Bench Book Bgg

BM N.W. unit. 236

at end of Job

368.89	368.47	368.36	368.41	368.82
4.69	5.11	5.22	5.17	4.76
CB	9		J	CB
12			12	

373.58



Thru. Lots 59 + 60 - Las Alturas

- O = Fd. Pipe. No. L.S. or R.E. number
- D = Fd iron pin.
- = Fd Pipe & disk L3 2317
- = set 1/2 Hub & city disk
- = " " " & tack
- = " " " Load & tack in pavement.
- X = set<sup>1</sup> chiseled cross in curb.

INDEXED

WIK  
NOV 12 1948

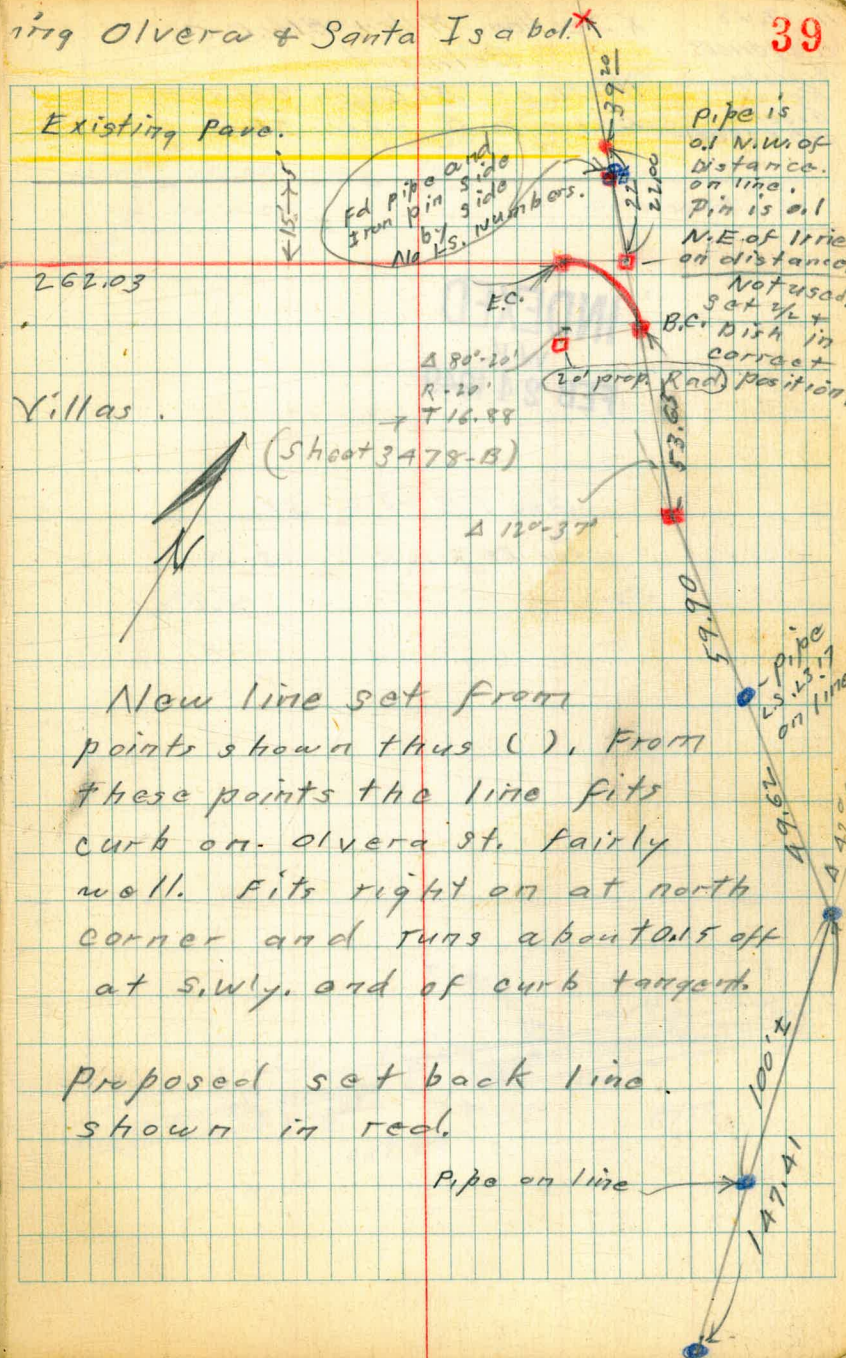
11-10-48

N.O. 27188

Sommermeyer  
McCoy  
Allen  
Jones

Stakes set from  
data on 3478-B.

Found several pipes and  
pins in ground as much as  
5' off line & on no distance that  
could be checked against  
anything shown on 3478-B,  
R.S. 1154; - or Map # 501.



New line set from  
points shown thus ( ), From  
these points the line fits  
curb on Olvera st. fairly  
well. Fits right on at north  
corner and runs about 0.15 off  
at S.W. end of curb targets.

Proposed set back line  
shown in red.

Pipe on line

11-17-48  
Hendricks  
Bramby  
Korer  
Greer  
WD#25001

X Section Alley Block C  
Belmont  
North of El Cajon between  
Estrella & 49th St.

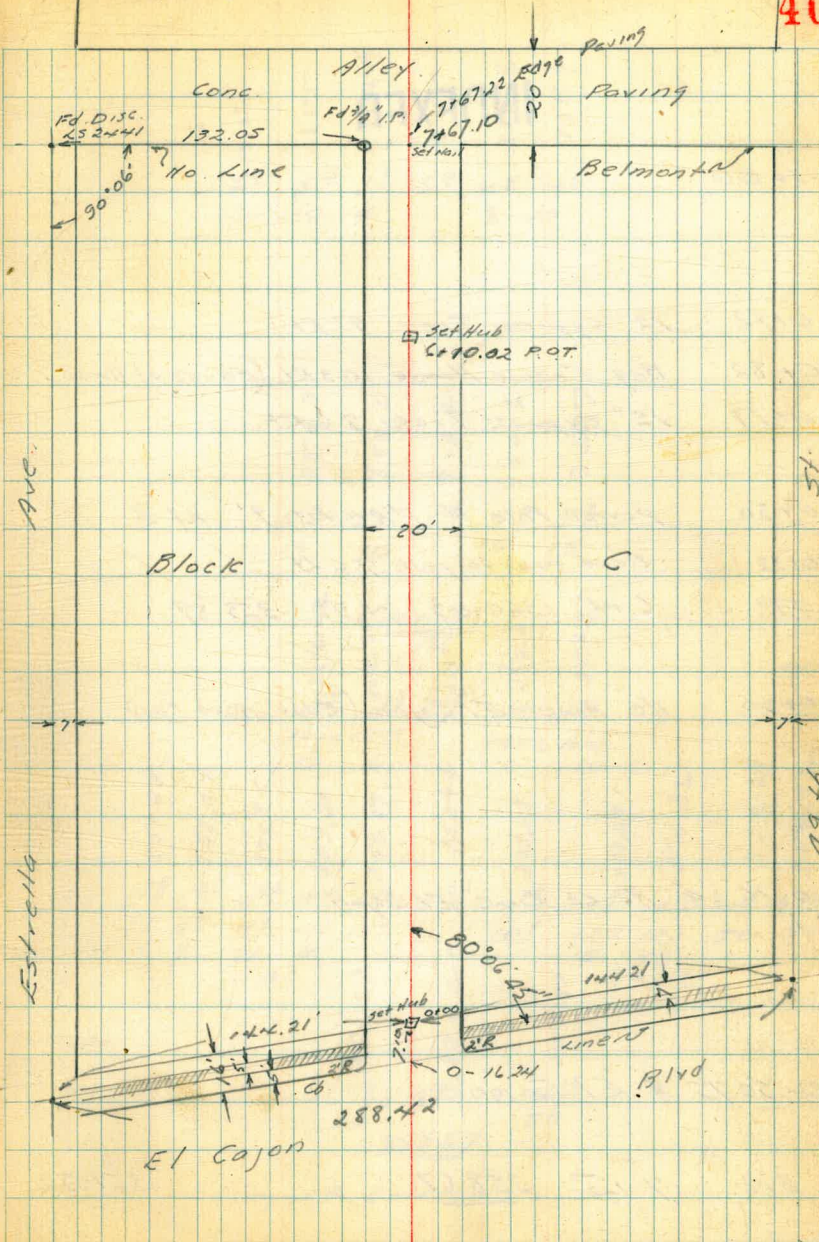
INDEXED

WK  
FEB 24 1949

See FB 2312-39

For RE-X-sec 12-28-54

40





2+01.1 £ MH 0.50 Lt.

2+00

1+68 £ 7.3' garage in 4 Lt. conc. FL

1+62 £ 1.3 Conc. Drain 10' Lt.

1+50 Power Pole # PA 4421.9.2 Lt

1+18 End. Board fence 10' Rt.

1+16 £ 3' Conc. Walk 109 Rt.

Req Board Fence 10' Rt.

1+14 End Frame House 109 Rt. (Edges of House 9612)

1+01 6" Apricot Tree 9.6 Rt.

360.03

10	356.0	10	357.23
X		X	
10	355.9	10	356.9
X		X	
10	355.7	10	357.38
X		X	
10	355.9	10	357.3
X		X	
10	356.0	10	357.3
X		X	
10	356.2	10	357.6
X		X	
10	356.5	10	357.9
X		X	

10 356.44

10 356.51

10 356.31

160.01

3+56

3+42 Power Pole # PAM443 8 8 Lt

3+17 8" Cypress Tree 8.1' Lt.

3+00

2+65

TP 995 369.11 0.87 359.16

2+50 Power Pole # PAM431 8 Lt

2+35

2+02 E Double Garage 15' Lt. Dirt floor

360.03

4	0	363.1
5	4	363.6
5	10	364.1
5	12	364.9
0	10	365.1
5	10	365.5

9.7	359.4	9.11	360.7
9.8	359.7	10.11	361.5
9.8	359.3	10.11	360.8
9.6	359.5	10.11	360.9
9.2	359.9	10.11	361.2
8.7	360.4	10.11	361.6
8.4	360.7	10.11	361.7
7.8	361.3	10.11	362.5

369.11

12	358.3
10	358.1
19	359.1
10	359.0
12	359.0
15	360.0

12 357.2

360.03

4442 \$ 10' Garage 15.3 Lt.

4478 10" Cypress Tree 9' Rt. 0.07

4407 \$ 10 Garage 15.2 Lt. Conc. Ft.

TP 7.72 376.22 0.61 368.50

4400

3498.5 End Conc Ramp 10.4 Lt.

3478 Beg Conc Ramp 10' Lt.

3474.5 \$ 10' Garage 15.4 Lt.

3466 12" Cypress Tree 8.7 Rt.

369.11

9.23  
15.3  
51  
367.00

10.13  
15.2  
51  
365.36

Ramp 376.22

Nail in Power Pole # PA 4459 Lt 4450

3.7365.4  
15  
3.1365.3  
10  
3.1365.3  
6  
3.1365.5  
5  
3.1365.7  
7  
2.8366.3  
7  
1.9369.2  
10  
1.0367.3  
15  
1.1367.7

3.1365.30  
10.4

1  
3.1364.88  
15  
4.48  
10

3.1369.27  
15.4

369.11  
/

5104 End. Garages 137 Rt

5100

4487.8 Garage Floors Step up on Rt.

4467 Req. Pickett fence 99 Lt

4469.8 Req. Garages 138 Rt. (out)

4468.4 E 28' Conc. Walk 179 Rt. - Out 12-28-54

4450 Power Pole #PA 4459 86' Lt.

376.22

9 <sup>10</sup>	366.9
20	
10 <sup>10</sup>	367.4
10	
X <sup>10</sup>	367.9
10 <sup>10</sup>	
11 <sup>10</sup>	367.7
10	
7 <sup>10</sup>	368.4
10	
6 <sup>10</sup>	369.4
10	

376.22

7 <sup>10</sup>	
20	
10 <sup>10</sup>	369.4
10	
6 <sup>10</sup>	369.5
10	
5 <sup>10</sup>	370.0
10	
5 <sup>10</sup>	370.9
10	
4 <sup>10</sup>	371.5
10	
4 <sup>10</sup>	371.64
10	

X <sup>10</sup>	371.63
10	
10	

5 <sup>10</sup>	370.82
137	
137	
X <sup>10</sup>	371.71
11	

5 <sup>10</sup>	370.76
137	
137	

6 <sup>10</sup>	370.15
137	
137	
X <sup>10</sup>	371.26
10	



5173 £ 10' Garage 14.5 Rt. Dirt fl.

5168 End Picket fence 9.6 Lt.

5165 Dead Man to Pole 9' Lt

5166 End Conc Apron to Garages

5150 Power Pole # PA 4479 8.6 Lt.

5135 Beg Picket fence 9.8 Lt.

5130

5127 <sup>18'</sup> £ Double Garage 13.1 Lt.

5197 Beg Conc Apron <sup>To Garages</sup> 10.2 Rt.

5117 End Picket fence 9.4' Lt.

5116 £ 4' Conc walk 13' Rt.

376.22

372.4  
372.7  
372.8  
373.64  
374.1  
372.81

370.69  
370.7  
371.0  
371.2  
371.5  
372.47  
372.80

370.69  
371.0

372.18  
372.82

371.64  
371.64

376.22

7467.22 Edge Conc. Paving East & West Alley

7+48 Tel. Pole # 430773H 8.2 Lt.

7+38

7+00

6+91 Dead Man to Pole 8.6 Lt.

6+67 Power Pole # 1A44589 8.2 Lt.

6+50

7P 195 376.21 196 374.26

6+10 E 14' Garage 16.1 Rt.

6+00

376.22

20	1.00	372.4	0	371.18
10	2.00	373.4	0	371.18
8	1.00	373.4	0	371.18
6	1.00	373.1	0	371.18
6	1.00	373.0	0	371.18
6	1.00	373.3	0	371.18
9	1.00	374.1	0	371.18
0	1.00	373.9	0	371.18

20	1.00	373.2	0	375.6
10	2.00	373.8	0	375.6
7	1.00	374.2	0	375.6
10	1.00	374.2	0	375.6
10	1.00	375.6	0	375.6
20	1.00	375.6	0	375.6

20	1.00	375.8	0	375.4
10	1.00	375.5	0	375.4
16	1.00	375.6	0	375.4
6	1.00	375.0	0	375.4
7	0.01	375.5	0	375.4
0	1.00	375.4	0	375.4
14	1.00	374.9	0	375.4

376.21  
On & Hub 6+10.02 POT  
10.3 Ramp  
16.1 Fl.

20	1.00	373.4	0	375.27
10	1.00	374.0	0	375.27
21	1.00	374.1	0	375.27
10	1.00	374.3	0	375.27

376.22

B.M.			8.46	351.50	351.52
T.P.	0.41	359.96	8.75	359.55	
T.P.	3.37	368.30	11.28	364.93	

71-77.22 & Paving East & West Alley

376.21

NVI BP El Cajon & Estrella

393	510	544	55	736
12	10	14	10	50
372.28	371.11	370.77	370.41	368.85

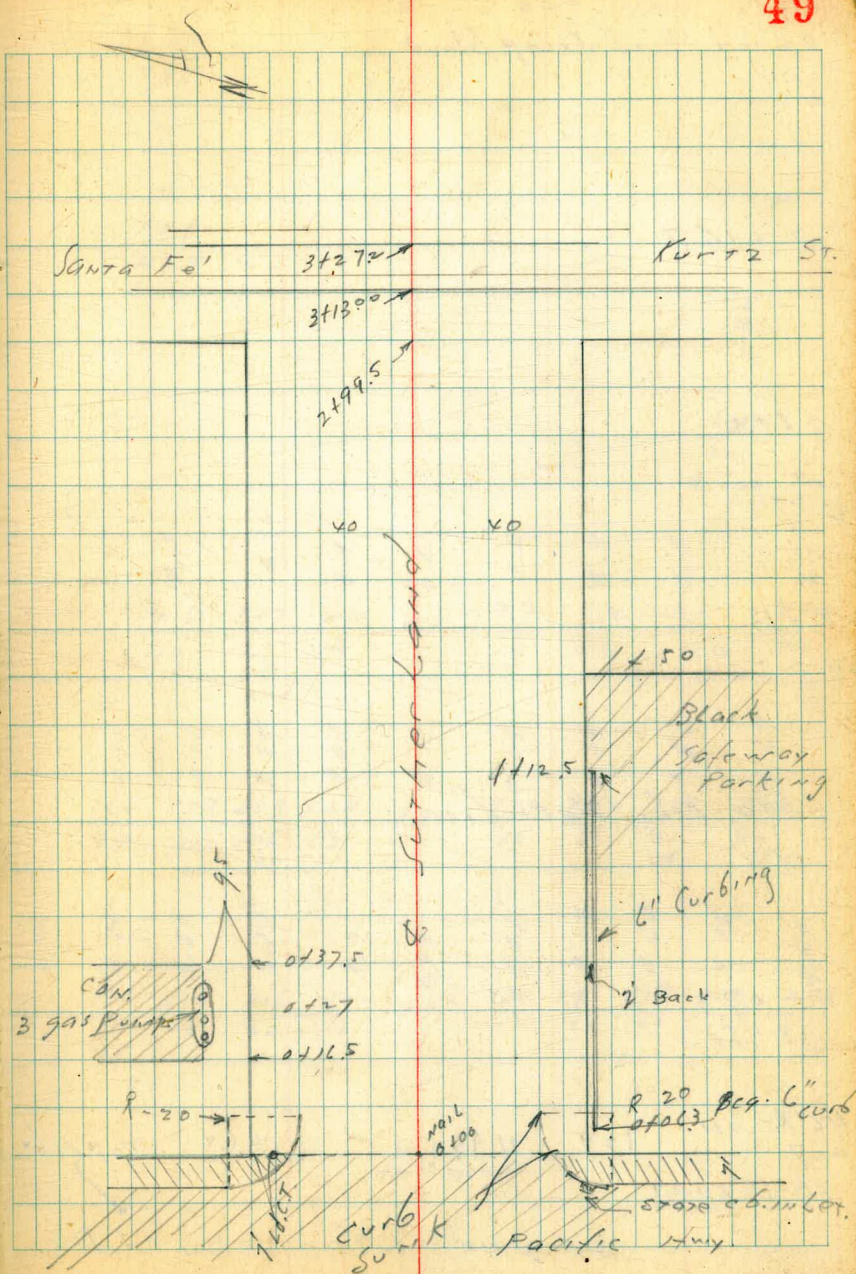
376.21

X sec Sutherland St.  
Pac. to Kurttz

Wo 80149

Moore  
Beg 9  
Sherman  
Bunick  
2-23-49

INDEXED  
WIK  
FEB 24 1949



Gas  
0+27 E of Pump Island

0+16.5

0+14

0+13

0+00 Ely Pacific

0-07

4C RT ON

0-7

FB 1589-39

7.29 11.93

4.6x top 6.6

BM gone as Handwritten + Pac.

L+ 5.29

49.5

4.84

4.1

7.09

49.5

CON.

5.46

(47)

Break Top  
cording

4.3	4.16	3.9	4.2	4.2	4.17	4.9	6.34
7.0	7.77	8.0	7.7	7.7	7.2	7.1	5.59
40	26	13		3	20	10	52
	end				dir	dir	curb
							Wall
							Top

4.31	4.16	3.85	4.05	4.13	4.04	4.09	4.56	4.69
7.6	7.77	8.08	7.88	7.80	7.89	7.80	7.87	7.24
40	30	30	13	13	31	31	30	50
	26	97				26		50

4.32	3.75	3.81	3.87	3.91	3.98	4.01	4.04	3.64	3.76	4.64
7.11	8.18	8.17	8.06	8.02	7.95	7.94	7.89	8.29	8.17	7.29
46	56	40	20	13	13	14	20	20	40	40
26	97								97	26

11.93

142

128

112.5 end curbing on B

100

07.50

0737.5

11.93

L

R

R

51

2 4.5 9.0  
40

2 9.1  
20

2 8.4  
13

4 7.8  
11

4 7.7  
13

4 7.7  
20

4 7.13  
40

3 8.1  
40

4 7.6  
20

5 7.5  
13

4 7.2  
11

5 7.1  
13

5 6.9  
20

5 6.86  
40

4 7.28  
13  
52.65  
16.

5 6.68  
43  
5.29  
16.

4 6.2  
40

5 6.1  
20

6 5.9  
13

5 5.8  
11

6 5.7  
13

6 6.2  
20

5 6.5  
40

7 6.3  
16  
4.90  
16

7 6.0  
40

7 6.3  
20

7 6.0  
13

7 6.6  
11

7 6.7  
13

5 5.4  
20

AP 3709  
28  
4.3  
40

5 6.18  
43  
5.75  
16

7 10 4.93  
40  
109.5  
10

11.93

2+50

T.P. 11.32 22.13 1.12 10.81

2+00

1+73 end walk

1+63 Beg. Cox walk II with N.L.

1+60

1+52.3 9 4.4 Cox steps

1+50

11.93

$\frac{9.6}{40}$   $\frac{10.0}{26}$   $\frac{10.3}{13}$  10.5  $\frac{10.7}{13}$   $\frac{11.7}{26}$   $\frac{11.2}{40}$

22.13

$\frac{1.1}{40}$   $\frac{1.2}{26}$   $\frac{1.9}{13}$  2.1  $\frac{2.0}{13}$   $\frac{2.3}{26}$   $\frac{2.6}{40}$

$\frac{1.30}{42.8}$

$\frac{1.55}{42.8}$

PP 3730  
25.9

PP 3729  
27.3

$\frac{1.6}{42.8}$   
Top  
Lower  
Step

$\frac{1.69}{41}$   
Top  
Walk

$\frac{1.8}{40}$   $\frac{2.5}{26}$

$\frac{3.8}{13}$   $\frac{3.6}{13}$

$\frac{8.0}{13}$   $\frac{3.9}{13}$

$\frac{1.8}{26}$   $\frac{3.8}{26}$   $\frac{4.65}{40}$   
Par

11.93

88  
 Check to Orig. B.M. 7.43 x .65  $\frac{4.60}{.001}$  9.50

T.P. 0.77 12.08 10.82 11.31

3 + 27.2 Top W. Rail of E track

3 + 13 Top W. Rail of W. track S.F. RR

3 + 07 Wly shoulder R.R. Embank

3 + 01

2 + 99.5 Wly Kuntz St.

2 + 90

22.13

3.94 3.75  $\frac{3.58}{40}$

4.15 3.89  $\frac{3.82}{40}$

$\frac{4.8}{40}$   $\frac{4.8}{20}$   $\frac{4.6}{75}$  5.0  $\frac{4.6}{13}$   $\frac{4.6}{20}$   $\frac{4.6}{40}$

R.P.  
 $\frac{304}{}$

$\frac{6.8}{40}$   $\frac{7.4}{20}$   $\frac{6.8}{75}$  7.0  $\frac{4.7}{13}$   $\frac{4.5}{20}$   $\frac{4.9}{40}$

$\frac{8.1}{40}$   $\frac{8.4}{20}$   $\frac{9.0}{13}$  8.9  $\frac{9.5}{13}$   $\frac{10.0}{20}$   $\frac{10.0}{40}$

22.13



Walker  
Johnson  
Pope  
Crusford  
3-10-49

# CROSS SECTIONS - ARDATH ROAD

INDEXED  
WK  
MAR 23 1949

N-0°33'51"W

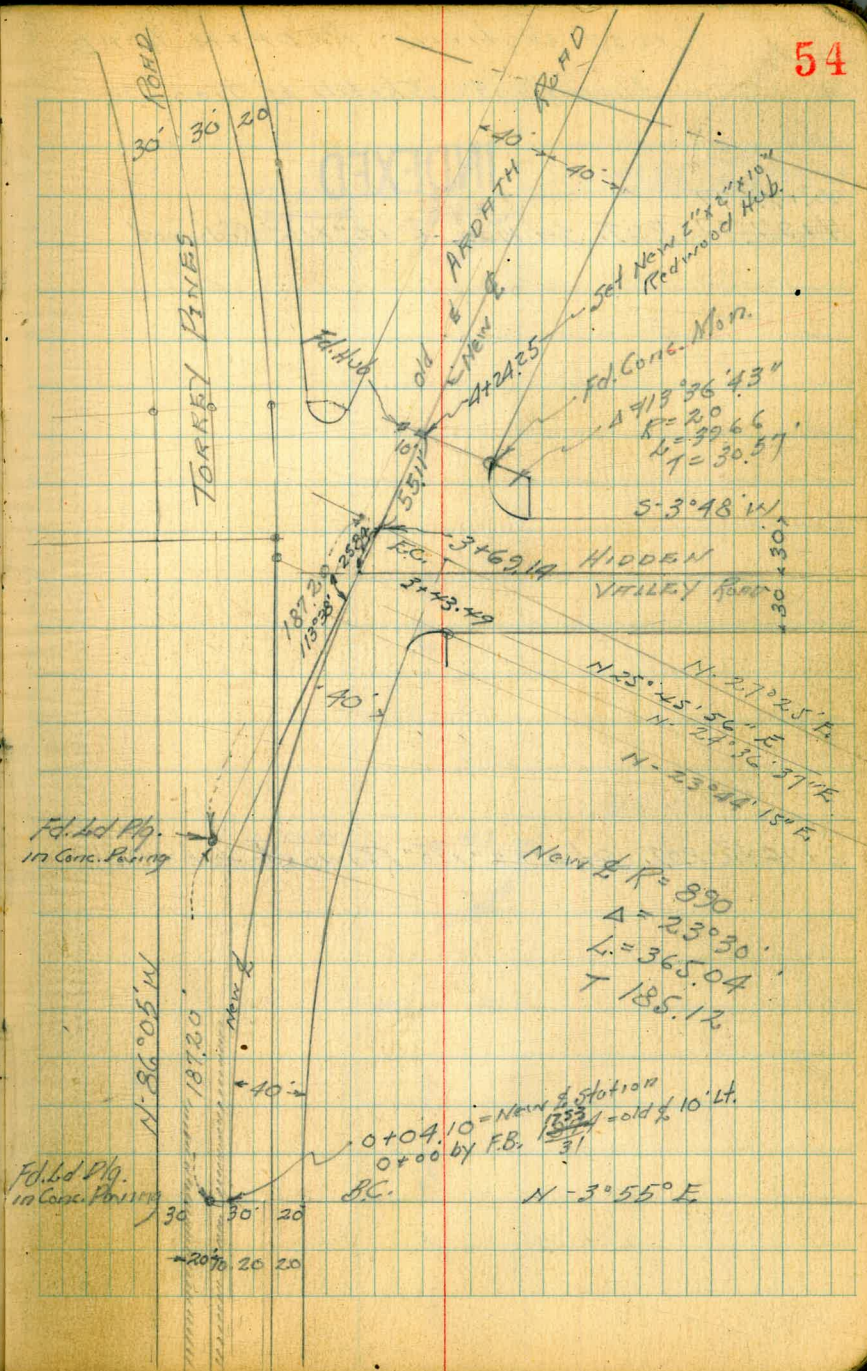
N-3°55'E



(Bearings Copied from Drawing #5846-L)

See FB 2055

54



Cross Sections - ARDATH ROAD.

Alignment Sketch of Ties

INDEXED

12+97.77  
~~11+97.77~~ = P.O.T. Set Hub 2" x 2" x 10" Redwood

8+74.33 = P.O.T. Set 2" x 2" x 10" Redwood Hub + Dist.

Cont'd. P-56

12+97.77  
~~11+97.77~~  
P.O.T.

out

535.13  
1.10  
90°00'

Set Cap Dist  
in Elec Pole #61523

535.13

8+74.33  
P.O.T.

40'  
90°00'

Fd. Conc. Mark  
L.S. #1880  
F.S. #990

40' x 40'

ARDATH

Cross Section Ardath Road  
Alignment

INDEXED

Set R.P. Hubs & Discs. 90° E&LT.  
25+53.04 Set 2x2 RW Hub & Disc. End.

24+53.13 Fd. Conc. Mon 39.84 Lt. (L.S. 1880)

12+97.77

14+97.77 P.O.T. 2x2 RW. Hub & Disc.

56

Cont Page 75

40' out 40' out  
25+53.04 Set 2x2 RW Hubs & Discs.

39.84 Nail 24+53.13 P.O.T.  
40.04 L.S. 1880

Road

Ardath

← 40' → 40' →

New

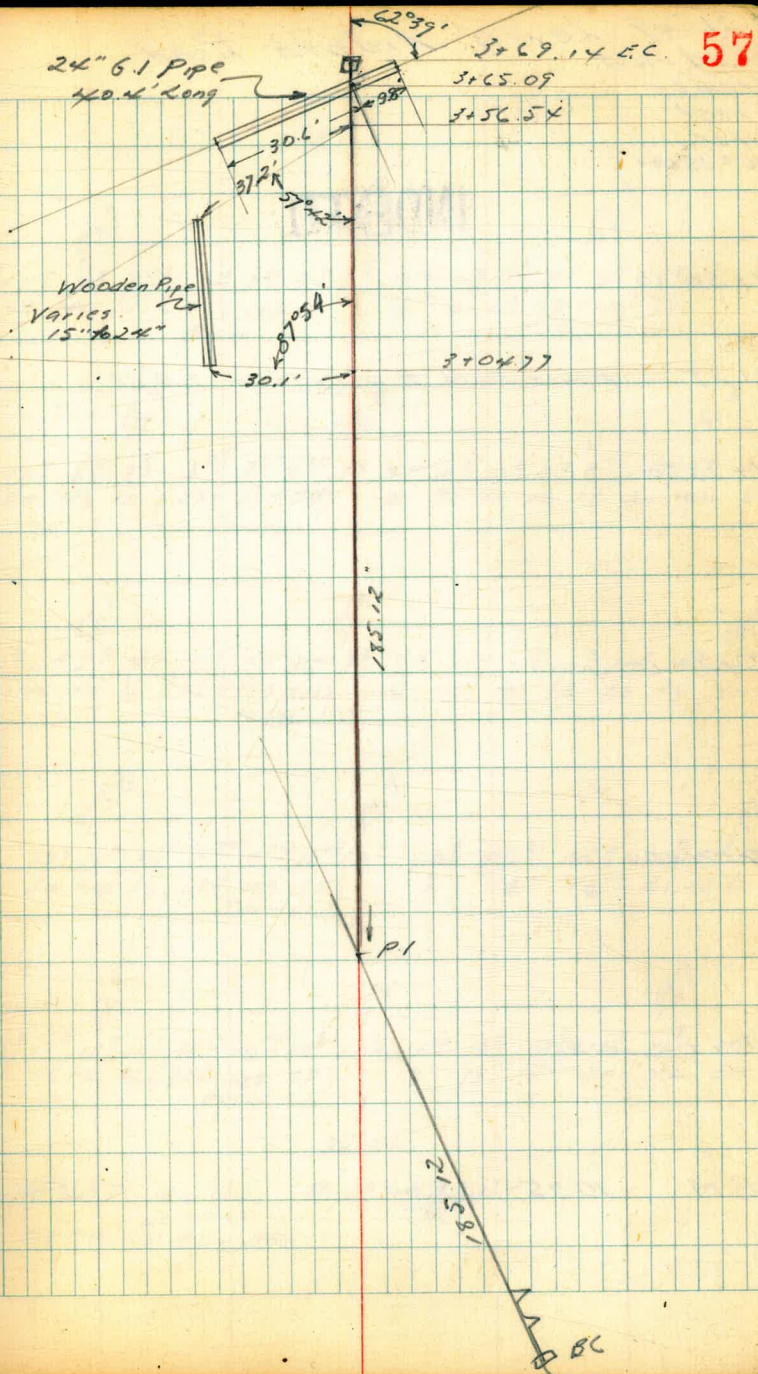
out

14+97.77 P.O.T.  
2x2 Hub & Disc

Contd from p. 55

Detail for Location of  
Pipes Hidden Valley Road & Ardath Rd.

INDEXED



3-21-49 Levels Ardath Road  
 Hendricks  
 Bramby  
 Greer  
 Lorier  
 NO # 2500

INDEXED

1+50.10

1+39 Power Pole # 447306H 1.0' LI

1+13.60

0+77.10

0+40.60

0+04.10 RC

B.M. 10.75  $\frac{65.00}{1}$

54.25

$\begin{matrix} 51.1 \\ 51.0 \\ 56.1 \end{matrix}$   
 $\begin{matrix} 9^E & 7^E & 7^E & 7^{23} & 7^{15} & 7^{30} & 7^E & 8^E & 9^E & 7^E & 8^E & 9^E & 8^E & 8^E \\ 57 & 48 & 40 & (35.6) & 25.6 & 15.5 & 10 & & 2 & 6 & 15 & 19 & 40 & 50 \end{matrix}$   
 Paving

$\begin{matrix} 56.5 \\ 56.0 \\ 51.2 \end{matrix}$   
 $\begin{matrix} 10^E & 8^E & 8^E & 8^{22} & 8^{14} & 8^{25} & 9^E & 9^E & 10^E & 10^E & 9^E & 9^E & 10^E & 9^E & 9^E \\ 50 & 43 & 40 & (29.9) & 19.9 & 9.9 & & 5 & 7 & 11 & 12 & 19 & 20 & 40 & 50 \end{matrix}$   
 Paving

$\begin{matrix} 55.1 \\ 51.1 \\ 51.1 \end{matrix}$   
 $\begin{matrix} 11^E & 11^E & 9^E & 9^E & 9^E & 9^E & 9^E & 9^E & 11^E & 11^E & 10^E & 10^E & 10^E & 10^E & 10^E \\ 50 & 46 & 40 & 35 & (25.9) & 15.9 & 5.9 & & 6 & 11 & 14 & 15 & 20 & 24 & 40 & 50 \end{matrix}$   
 Paving

$\begin{matrix} 53.7 \\ 51.1 \\ 51.1 \end{matrix}$   
 $\begin{matrix} 13^E & 11^E & 10^E & 9^E & 9^E & 10^E & 10^E & 10^E & 10^E & 12^E & 12^E & 12^E & 10^E & 11^E & 11^E & 11^E \\ 50 & 40 & 36 & (23.5) & 13.5 & 3.5 & & & 8 & 13 & 16 & & 21 & 25 & 40 & 50 \end{matrix}$   
 Paving

$\begin{matrix} 51.1 \\ 51.1 \\ 51.1 \end{matrix}$   
 $\begin{matrix} 13^E & 13^E & 13^E & 11^E & 10^E & 10^E & 10^E & 11^E & 11^E & 13^E & 12^E & 11^E & 11^E & 11^E & 11^E \\ 50 & 44 & 40 & 36 & (22.5) & 12.5 & 2.5 & & 8 & 13 & 17 & 21 & 40 & 50 \end{matrix}$   
 Paving

65.00

$\frac{65.00}{1}$   
 L&T 0+00: P. 33 FB 1750  
 0+04.10 out 54

INDEXED

2196.10

2180 Power Pole # 453620H 38' Lt

2164 Power Pole # 61527 24' Rt

2159.60

2123.10

1186.60

1168

1158

6500  
/

2.2  
62.1

28	29	50	65	65	54	70	30	28	29	50	60	50	51
50	42	37	35	31	30	25	19	2	9	18	40	40	50

51.1

60.7

38	40	46	46	68	75	68	58	44	43	59	67	62	59
50	42	34	30	26	24	21	20	11		9	18	40	50

58.7

51.9

50	50	51	50	55	71	77	62	61	60	70	74	70	69
(521	40	37)	26	20	16	12	4	4	16	25	40	40	50

Paving

51.0

51.8

62	63	60	62	68	67	80	82	73	74	80	89	79
50	(43	33	22)	16	12	8	3		9	21	40	50

Paving

56.5

56.1

67	67	65	62	71	71	85	88	75	80	91	85	82
50	(39	29	19)	16	9	6		4	16	17	40	50

Paving

56.2

51.1

71	62	69	68	70	75	79	92	79	80	95	88	80
50	40	(37	26	16)	11	3		5	15	18	40	50

Paving

65.00  
/

INDEXED

3+38.7± Wooden Pipe only.

3+32.60

3+29

3+27

3+18

T.P. 9.88  $\frac{74.27}{7}$  0.61 64.39

3+04.7± Wooden 24" D.  
Pipe only

6500  
7

11<sup>2</sup> 15<sup>2</sup>  
FL 2 22.3  
(HW) FL  
Stone

63.9

63.1

61.1

11<sup>0</sup> 10<sup>9</sup> 10<sup>8</sup> 10<sup>7</sup> 11<sup>4</sup> 10<sup>3</sup> 11<sup>1</sup> 12<sup>2</sup> 11<sup>2</sup>  
50 40 35 6 10 28 40 50

62.9

11<sup>4</sup>

63.6

60.1

11<sup>0</sup> 11<sup>0</sup> 10<sup>3</sup> 11<sup>4</sup> 10<sup>7</sup> 10<sup>7</sup> 12<sup>5</sup> 12<sup>7</sup> 14<sup>1</sup> 14<sup>3</sup> 14<sup>0</sup>  
50 40 9 2 6 14 24 24 40 50

63.1

60.0

11<sup>2</sup> 11<sup>0</sup> 11<sup>2</sup> 11<sup>2</sup> 10<sup>8</sup> 10<sup>4</sup> 10<sup>5</sup> 11<sup>7</sup> 13<sup>3</sup> 14<sup>2</sup> 14<sup>3</sup> 14<sup>1</sup>  
50 40 24 18 17 9 4 12 22 40 50

£ Hub 2+69.14

$\frac{74.27}{7}$

62.1

59.8

2<sup>2</sup> 2<sup>5</sup> 4<sup>4</sup> 3<sup>2</sup> 7<sup>6</sup> 6<sup>7</sup> 4<sup>4</sup> 3<sup>2</sup> 2<sup>3</sup> 2<sup>3</sup> 2<sup>5</sup> 4<sup>8</sup> 5<sup>5</sup> 5<sup>2</sup> 4<sup>2</sup>  
50 38 36 32 32 27 24 17 3 11 21 40 50

Stone FL  
HW 24" wooden  
Pipe

6500  
7

INDEXED

4+50

Anchor Pole 33.7 Lt  
Power Pole # 61526 35' Rt.

4+24.25

TP 11.70 77.18 8.79 6548

4+00

3+85 Power Pole # 50568 H 29.5 Lt.

Dead Man Pole 30' Lt.

3+69.14 EC. Pipe on Rt.

3+64 End Ditch on Lt

3+49 ± 24" GI Pipe on Lt 27.4'

3+43.49 & Intersection Hidden Valley Road

74.27

65.9 66.0 66.8

11.3	11.3	11.4	10.3	10.7	10.5	10.7	11.3	10.4	10.4	10.5
50	43	33	28	21	12	2	5	40	50	

77.18  
on Conc. Man 40' Rt 4+24.25

64.7 64.1 64.9

9.3	9.5	9.4	9.3	9.7	9.3	9.5	10.1	9.1	9.5	9.4
50	40	30	24	19	10		2	6	40	50

63.6 64.5 64.8

10.5	10.7	10.5	10.0	10.3	9.8	9.2	10.3	12.28	11.0	10.2	9.5	9.5
50	40	24	23	16		5	8.7	8.7	18	27	36	50

FL.

64.5 64.6

10.5	10.5	12.4	13.3	10.5	10.3	9.8	9.5	9.2	9.5
50	24	24	30	30	16		20	40	50

13.5  
27.4  
FL

62.9 64.0 63.8

10.9	11.4	12.5	14.5	13.5	11.3	10.2	10.3	10.5	11.3	10.5	10.5	10.5
50	40	24	30	28	26	10		20	28	32	40	50

74.27





INDEXED

9+56 End Driveway & 24" Iron Pipe

9+50

9+39 Beg Driveway & 24" Pipe 36' Lt.

9+00

TP. 12.37  $\frac{99.67}{1}$  1.52 87.30

8+50

Group

8+30 R 4 Trees (Width) 27' Lt.

8+25 Dead Man to Pole 23' Lt.

8+06 Power Pole # 505620 H 24' Lt.

8+00

$\frac{88.82}{1}$

87.0  
9.5 12.5  
28 38  
Dr. FL

90.1

90.1

90.9

94	95	96	94	100	95	96	98	99	84	87	88	89
50	40	25	22	16	7		10	11	19	23	40	50

89.4

87.4

98 12.5  
36 36'  
Dr. FL

86.9

87.6

88.1

88.0

94	100	12	13	11.5	11.2	12.4	12.1	12.4	12.3	11.2	11.5	11.5	11.2
50	45	38	25	25	19	15	5		8	9	30	40	50

85.3

$\frac{99.67}{1}$   
85.1

85.5

32	35	35	34	40	36	37	44	35	43	33	35
50	40	35	18	15	5		8	19	23	40	50

82.4

82.6

82.2

61	64	65	55	63	59	62	65	63	57	68	65	63
50	40	32	18	15	6		5	7	17	32	40	50

$\frac{88.82}{1}$

INDEXED

12+00

11+65

11+45

11+00

T.P. 1186 110.16 1.37 98.30

10+50

10+16 Dead Man to Pole 35' Rt

10+02 Power Pole # JP61741 24' Lt

10+00

9+97 Power Pole # 61524 35' Lt

99.67

103.6  
103.1  
103.8  
102.8  
99.7  
100.5  
103.3  
103.2  
104.0

6<sup>5</sup> 6<sup>5</sup> 6<sup>5</sup> 7<sup>8</sup> 10<sup>3</sup> 10<sup>3</sup> 6<sup>5</sup> 7<sup>0</sup> 6<sup>7</sup> 6<sup>5</sup> 6<sup>2</sup> 4<sup>2</sup> 4<sup>1</sup>  
50 40 31 18 13 11 3 6 12 26 32 44 50

102.5  
102.3  
103.9

7<sup>8</sup> 7<sup>8</sup> 14<sup>0</sup> 12<sup>8</sup> 7<sup>8</sup> 7<sup>7</sup> 8<sup>5</sup> 9<sup>2</sup> 8<sup>8</sup> 7<sup>5</sup> 6<sup>2</sup> 6<sup>3</sup>  
50 40 30 26 16 7 3 11 20 35 42 50

101.0  
100.3  
102.1

8<sup>5</sup> 9<sup>2</sup> 15<sup>4</sup> 15<sup>6</sup> 14<sup>6</sup> 8<sup>1</sup> 7<sup>7</sup> 9<sup>2</sup> 9<sup>2</sup> 10<sup>2</sup> 9<sup>2</sup> 8<sup>2</sup> 8<sup>1</sup> 7<sup>7</sup>  
50 38 33 30 29 14 9 2 8 24 28 40 50

98.6  
93.1  
98.1  
99.5  
99.8

11<sup>4</sup> 11<sup>2</sup> 17<sup>0</sup> 16<sup>5</sup> 10<sup>5</sup> 10<sup>5</sup> 11<sup>8</sup> 12<sup>4</sup> 12<sup>2</sup> 11<sup>9</sup> 10<sup>9</sup> 10<sup>7</sup> 10<sup>4</sup>  
60 50 45 40 27 18 12 11 15 22 40 50

110.16  
95.5  
95.2  
96.4

3<sup>8</sup> 8<sup>2</sup> 7<sup>6</sup> 4<sup>4</sup> 4<sup>2</sup> 3<sup>2</sup> 3<sup>6</sup> 4<sup>2</sup> 4<sup>5</sup> 4<sup>8</sup> 4<sup>2</sup> 3<sup>8</sup> 3<sup>2</sup> 3<sup>3</sup> 3<sup>3</sup>  
65 60 50 45 40 30 20 17 10 11 25 31 40 50

10.3  
93.2  
92.5  
93.3

6<sup>5</sup> 9<sup>8</sup> 9<sup>4</sup> 6<sup>5</sup> 6<sup>5</sup> 5<sup>8</sup> 5<sup>2</sup> 6<sup>5</sup> 7<sup>1</sup> 7<sup>2</sup> 7<sup>2</sup> 6<sup>5</sup> 6<sup>0</sup> 6<sup>2</sup> 6<sup>4</sup> 6<sup>5</sup>  
67 62 50 43 40 30 24 18 17 9 10 23 26 40 50

99.67

INDEXED

14+50

14+00

13+50

13+00

12+93 Power Pole # 61523 36' Rt.

T.P. 12.31  $\frac{120.17}{\uparrow}$  230 107.86

12+53 End Drive & 24" Conc. Pipe on Lt.

12+37 Bc9 Drive & 24" Conc. Pipe on Lt.

$\frac{110.16}{\uparrow}$

14 <sup>0</sup>	14 <sup>1</sup>	14 <sup>2</sup>	14 <sup>3</sup>	14 <sup>4</sup>	14 <sup>5</sup>	14 <sup>6</sup>	14 <sup>7</sup>	14 <sup>8</sup>	14 <sup>9</sup>	14 <sup>10</sup>	14 <sup>11</sup>	14 <sup>12</sup>	14 <sup>13</sup>	14 <sup>14</sup>	14 <sup>15</sup>
63	53	45	42	10	19	23	40	50							
113.9															
13 <sup>8</sup>	13 <sup>7</sup>	13 <sup>6</sup>	13 <sup>5</sup>	13 <sup>4</sup>	13 <sup>3</sup>	13 <sup>2</sup>	13 <sup>1</sup>	13 <sup>0</sup>	13 <sup>11</sup>	13 <sup>10</sup>	13 <sup>9</sup>	13 <sup>8</sup>	13 <sup>7</sup>	13 <sup>6</sup>	13 <sup>5</sup>
60	49	46	41	36	8	20	24	40	50						
109.8															
12 <sup>7</sup>	12 <sup>6</sup>	12 <sup>5</sup>	12 <sup>4</sup>	12 <sup>3</sup>	12 <sup>2</sup>	12 <sup>1</sup>	12 <sup>0</sup>	12 <sup>11</sup>	12 <sup>10</sup>	12 <sup>9</sup>	12 <sup>8</sup>	12 <sup>7</sup>	12 <sup>6</sup>	12 <sup>5</sup>	12 <sup>4</sup>
60	49	46	41	9	19	23	40	50							
109.5															
11 <sup>6</sup>	11 <sup>5</sup>	11 <sup>4</sup>	11 <sup>3</sup>	11 <sup>2</sup>	11 <sup>1</sup>	11 <sup>0</sup>	11 <sup>11</sup>	11 <sup>10</sup>	11 <sup>9</sup>	11 <sup>8</sup>	11 <sup>7</sup>	11 <sup>6</sup>	11 <sup>5</sup>	11 <sup>4</sup>	11 <sup>3</sup>
50	50	43	34	25	16	9	2	20	22	40	50				
107.4															
10 <sup>6</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>3</sup>	10 <sup>2</sup>	10 <sup>1</sup>	10 <sup>0</sup>	10 <sup>11</sup>	10 <sup>10</sup>	10 <sup>9</sup>	10 <sup>8</sup>	10 <sup>7</sup>	10 <sup>6</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>3</sup>
50	40	33	19	19	11	10	29	30	40	50					
106.5															
9 <sup>6</sup>	9 <sup>5</sup>	9 <sup>4</sup>	9 <sup>3</sup>	9 <sup>2</sup>	9 <sup>1</sup>	9 <sup>0</sup>	9 <sup>11</sup>	9 <sup>10</sup>	9 <sup>9</sup>	9 <sup>8</sup>	9 <sup>7</sup>	9 <sup>6</sup>	9 <sup>5</sup>	9 <sup>4</sup>	9 <sup>3</sup>
50	40	27	20	125	125	5	33	34	40	50					
105.6															
8 <sup>6</sup>	8 <sup>5</sup>	8 <sup>4</sup>	8 <sup>3</sup>	8 <sup>2</sup>	8 <sup>1</sup>	8 <sup>0</sup>	8 <sup>11</sup>	8 <sup>10</sup>	8 <sup>9</sup>	8 <sup>8</sup>	8 <sup>7</sup>	8 <sup>6</sup>	8 <sup>5</sup>	8 <sup>4</sup>	8 <sup>3</sup>
50	40	27	20	125	125	5	33	34	40	50					
104.9															
7 <sup>6</sup>	7 <sup>5</sup>	7 <sup>4</sup>	7 <sup>3</sup>	7 <sup>2</sup>	7 <sup>1</sup>	7 <sup>0</sup>	7 <sup>11</sup>	7 <sup>10</sup>	7 <sup>9</sup>	7 <sup>8</sup>	7 <sup>7</sup>	7 <sup>6</sup>	7 <sup>5</sup>	7 <sup>4</sup>	7 <sup>3</sup>
50	40	27	20	125	125	5	33	34	40	50					
104.2															
Gr. Fl.															
110.16															



INDEXED

20+50

136.7  
 12<sup>3</sup> 12<sup>4</sup> 10<sup>3</sup> 11<sup>7</sup> 11<sup>5</sup> 10<sup>8</sup> 8<sup>7</sup> 8<sup>4</sup> 7<sup>2</sup>  
 50 40 18 5 15 21 40 50

20+00

135.1 135.4 138.8  
 13<sup>2</sup> 13<sup>7</sup> 12<sup>4</sup> 13<sup>4</sup> 13<sup>4</sup> 12<sup>4</sup> 10<sup>8</sup> 10<sup>8</sup> 7<sup>2</sup>  
 50 40 15 5 18 21 40 50

T.P. 1167  $\frac{148.81}{\wedge}$  1.58 137.14

19+50

133.0 134.0 137.2  
 6<sup>2</sup> 5<sup>7</sup> 4<sup>7</sup> 3<sup>8</sup> 4<sup>5</sup> 4<sup>7</sup> 3<sup>8</sup> 1<sup>8</sup> 1<sup>5</sup> 1<sup>2</sup>  
 50 40 26 13 5 19 22 40 50

19+00

131.0 131.4 132.3 135.9 136.2  
 7<sup>2</sup> 7<sup>2</sup> 5<sup>7</sup> 5<sup>4</sup> 5<sup>7</sup> 6<sup>4</sup> 5<sup>6</sup> 3<sup>8</sup> 2<sup>8</sup> 2<sup>4</sup>  
 50 40 24 13 5 19 22 40 50

18798 Power Pole # 61521 35' ct.

18+50

130.1 130.5 134.2  
 9<sup>4</sup> 8<sup>5</sup> 7<sup>4</sup> 7<sup>4</sup> 8<sup>2</sup> 7<sup>7</sup> 4<sup>8</sup> 4<sup>5</sup> 4<sup>3</sup>  
 50 40 25 12 19 23 40 50

18+00

128.5 128.7 132.2  
 10<sup>7</sup> 10<sup>3</sup> 9<sup>2</sup> 9<sup>5</sup> 10<sup>8</sup> 9<sup>5</sup> 6<sup>7</sup> 6<sup>5</sup> 6<sup>2</sup>  
 50 40 25 10 19 23 40 50

$\frac{138.72}{\wedge}$

$\frac{138.72}{\wedge}$

INDEXED

23+37

23+00

T.P. 12.82 160.02 1.61 147.20

22+50

22+00

2+196 Power Pole # 61520 353' R+

21+50

21+00

148.81

150.3  
 9<sup>±</sup> 9<sup>±</sup> 10<sup>±</sup> 11<sup>±</sup> 10<sup>±</sup> 11<sup>±</sup> 10<sup>±</sup> 9<sup>±</sup> 9<sup>±</sup>  
 50 40 23 17 2 11 40 50

147.5 147.4 148.8 150.3  
 12<sup>±</sup> 12<sup>±</sup> 12<sup>±</sup> 12<sup>±</sup> 13<sup>±</sup> 13<sup>±</sup> 12<sup>±</sup> 11<sup>±</sup> 11<sup>±</sup> 10<sup>±</sup> 10<sup>±</sup> 11<sup>±</sup>  
 50 40 30 29 19 10 3 22 25 40 50

145.1 160.02  
 145.1 146.6  
 5<sup>±</sup> 3<sup>±</sup> 2<sup>±</sup> 3<sup>±</sup> 4<sup>±</sup> 3<sup>±</sup> 5<sup>±</sup> 2<sup>±</sup> 1<sup>±</sup> 2<sup>±</sup> 2<sup>±</sup>  
 50 40 26 17 10 6 12 23 40 50

143.0 142.1 144.8  
 6<sup>±</sup> 6<sup>±</sup> 5<sup>±</sup> 6<sup>±</sup> 5<sup>±</sup> 5<sup>±</sup> 6<sup>±</sup> 6<sup>±</sup> 5<sup>±</sup> 5<sup>±</sup> 3<sup>±</sup> 4<sup>±</sup> 3<sup>±</sup>  
 50 48 40 36 20 16 7 12 19 21 40 50

140.0 140.91 142.8  
 9<sup>±</sup> 8<sup>±</sup> 6<sup>±</sup> 8<sup>±</sup> 7<sup>±</sup> 7<sup>±</sup> 6<sup>±</sup> 6<sup>±</sup> 5<sup>±</sup>  
 50 40 20 7 15 22 40 50

137.5 139.0 141.4 142.1  
 11<sup>±</sup> 11<sup>±</sup> 10<sup>±</sup> 8<sup>±</sup> 9<sup>±</sup> 9<sup>±</sup> 9<sup>±</sup> 7<sup>±</sup> 7<sup>±</sup> 6<sup>±</sup>  
 50 40 34 20 5 16 22 40 50

148.81

**INDEXED**

	6.28	54.30	54.25 *
TP	320	60.58	12.08 57.38
TP	064	69.46	12.43 68.82
TP	012	81.25	13.20 81.13
T.P.	005	94.33	12.80 94.28
TP	0.27	107.08	13.25 106.81
TP	0.04	120.06	12.71 120.02
TP	0.25	132.73	12.79 132.48
TP	0.35	145.27	12.82 144.92
T.P.	2.04	157.74	4.32 155.70

25+00

24+51 Anchor Pole 335 L

24+46 Power Pole #61519 35' R

24+50

24+00

23+75

160.02  
T

LET 0400 = 0404.10 our station PP33 FB1753

Nail in Power Pole #61519 35' R 2x+4L  
 162.2  
 168.8  
 160.0  
 158.6  
 +9<sup>2</sup>+8<sup>5</sup>+11<sup>7</sup>+12<sup>2</sup>+11<sup>9</sup>+13<sup>5</sup>+12<sup>3</sup>+3<sup>2</sup>+12<sup>3</sup>+13<sup>3</sup> 0<sup>0</sup> 14  
 50 40 27 15 7 3 13 20 27 40 50

159.6  
 158.0  
 153.8  
 0<sup>0</sup> 0<sup>2</sup> 12 0<sup>2</sup> 14 2<sup>1</sup> 2<sup>0</sup> 2<sup>0</sup> 2<sup>0</sup> 4<sup>3</sup> 6<sup>3</sup> 6<sup>0</sup>  
 50 40 35 32 19 17 10 7 14 40 50

155.2  
 153.4  
 152.0  
 5<sup>1</sup> 4<sup>5</sup> 5<sup>3</sup> 6<sup>5</sup> 6<sup>5</sup> 6<sup>2</sup> 6<sup>6</sup> 8<sup>1</sup> 9<sup>4</sup> 8<sup>5</sup> 7<sup>3</sup> 8<sup>0</sup> 8<sup>1</sup>  
 50 40 30 27 20 4 8 18 25 20 40 50

152.6  
 151.4  
 151.6  
 7<sup>5</sup> 7<sup>4</sup> 7<sup>3</sup> 7<sup>9</sup> 9<sup>0</sup> 8<sup>6</sup> 8<sup>1</sup> 8<sup>6</sup> 9<sup>5</sup> 9<sup>1</sup> 8<sup>4</sup> 8<sup>4</sup>  
 50 40 33 30 16 6 3 8 17 40 50

160.02  
T



Survey Lots 27-28-29  
Blk 117 Pacific Beach

Moore  
Bogg  
Sherman  
D. Sisson

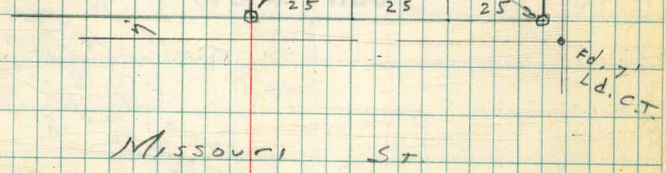
Map 943

4-19-49.

W.O. 21001

INDEXED  
WIK  
APR 20 1949

20' Alley



To 1st Ct.

Missouri Blvd.

To 1st Ct.

X-Sect Klauber - 500' S.W. from 69<sup>th</sup>

# 3618

6-7-49

W.O. 25001

Osborne  
Hardin  
Hatch  
Shepard

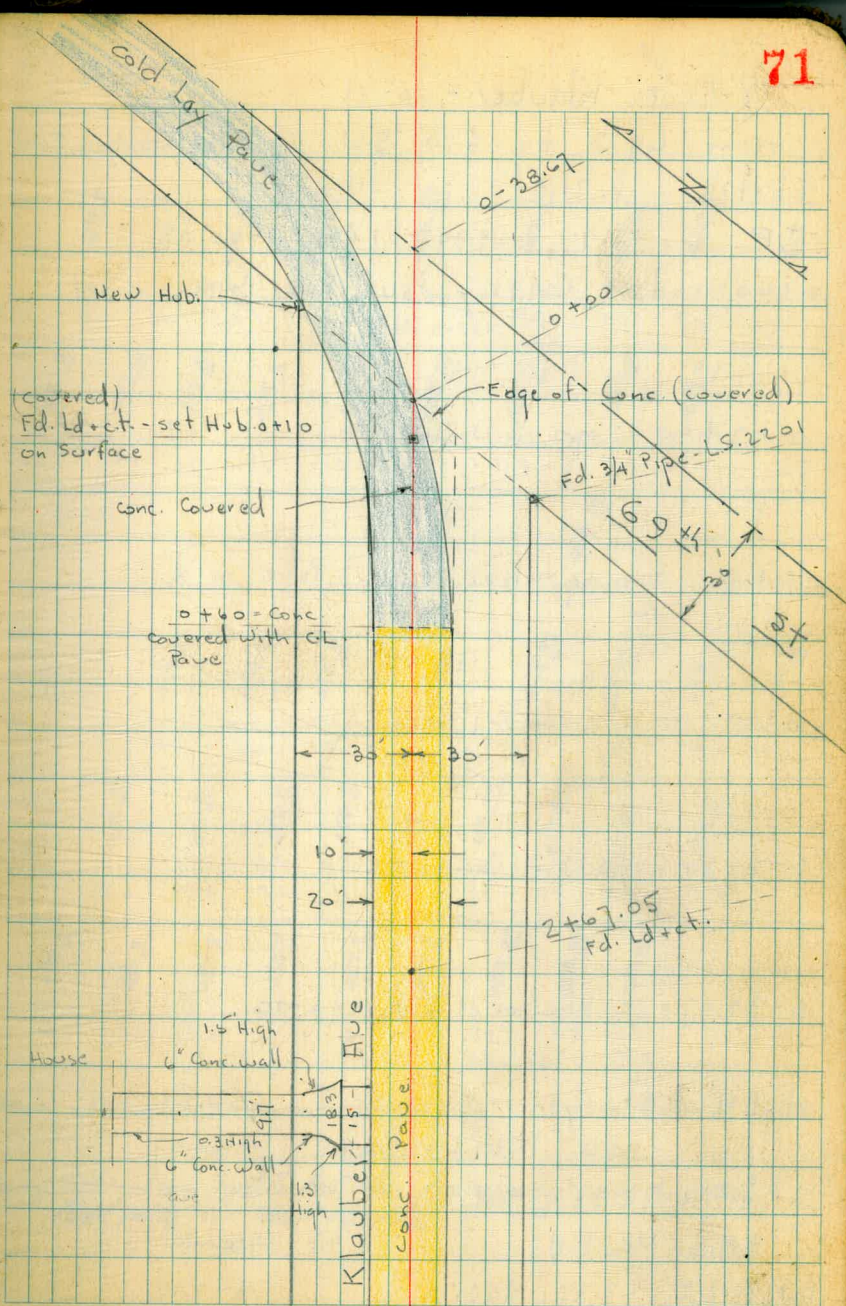
Levels - P. 72

INDEXED

WK  
JUN 8 1949

Notes Transcribed 6/17/49  
m. Clamen  
E & Paving edge profile 540 6/17/49  
m. Clamen

71





3+50

3+00

2+90 - 65' Lt. - ± New House under Const.

2+50

2+00

1+97 - 22' Lt. - ± P. pole # P-272504

1+75

1+50

1+25

1+00

40	400.6	463.5	465.0	465.7	465.3	467.36	462.9
30	461.3	464.0	464.9	465.7	465.5	464.4	464.0
20	461.7	463.7	465.2	467.1	466.8	463.9	463.1
10	459.1	460.5	461.8	462.7	463.0	464.8	462.4
edge	459.3	460.7	461.81	462.60	463.01	463.7	458.8
0	459.30	460.84	461.92	462.69	463.12	462.77	459.23
edge	459.29	460.75	461.82	462.60	462.99	461.92	459.35
0	459.4	460.8	464.6	464.2	463.2	461.9	459.27
10	462.7	464.3	464.8	464.5	463.9	461.3	459.7
20	463.2	464.6	464.8	464.4	462.7	461.0	459.2
30	463.6	464.6	464.8	464.4	462.7	461.0	458.8
40	463.6	464.6	464.8	464.4	462.7	461.0	458.8

469 34



Topography Proposed Tunnel  
Pacific Highway + Terry Piper Road

18.97

39+35.30 P.O.T.

321.25

36+76.76 = P.O.T.

36+14.05 P.O.T.

245.43

38+18.62 P.O.T.

30+31.78 = P.O.T.

30+23.49 = P.O.T.

30+20.00

29+14.63 P.O.T.

27+31.26 P.O.T. = 27+31.52 = dd sta.

25+52.04 P.O.T.

Bit Ford Page 56

Oct. 24-49.

H. Sisson

Garbar

Costa

Chavez

4/20/59

75

2914	63
117	06
<hr/>	
2031	69

✓ Set by C.A. 11/6/58

OUT. 11/6/58

✓

Set by Hatch 4/9/59

out.

56+09.50

54+12.79 P.O.T.

51+54.50 P.O.T.

50+63.29 P.O.T find to Here ✓

48+81.79 P.O.T ✓

47+03.64 P.O.T ✓

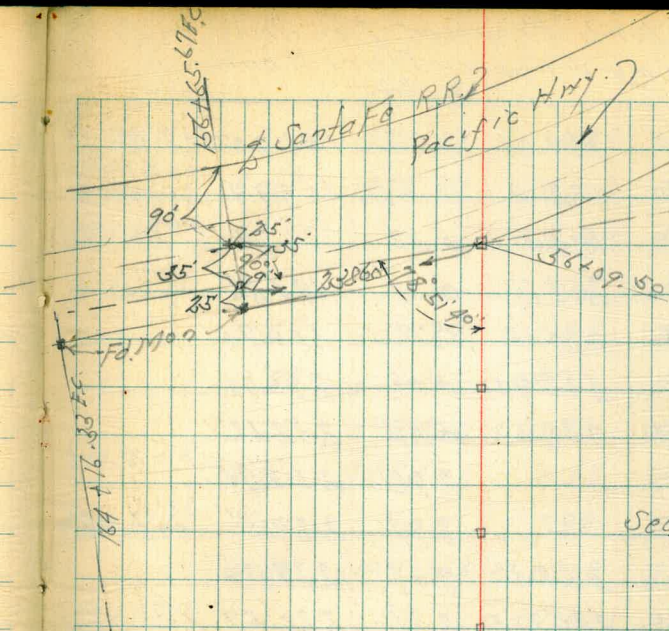
45+09.24 P.O.T ✓

Near Road  
506 ft.  
Here

42+34.27 P.O.T.

41+54.27 P.O.T (Here)

76



Control Levels Proposed Tunnel  
Pacific Hwy & Torrey Pines Road.

BM	12.31	169.01		155.70	Not Pmt Pol 358' 39" 96'
25+52.04	13.14	182.13	0.02	168.99	on Hub 25+53.04
	12.66	194.41	0.38	181.75	
	12.83	207.11	0.13	194.28	
	13.23	220.18	0.16	206.95	
	12.83	232.95	0.06	220.12	
	5.84	238.50	0.29	232.66	
29+14.63 P.O.T.			2.76	235.74	on Hub
30+20 P.O.T.			8.94	229.56	on Hub
	2.74	233.30	8.94	229.56	
	0.255	220.825	12.73	220.57	
	1.295	209.430	12.69	208.135	
33+18.62 P.O.T.			3.96	205.47	on Hub
	12.81	218.28	3.96	205.47	
	12.96	230.85	0.39	217.89	
	12.89	243.19	0.55	230.30	
	12.91	255.70	0.40	242.79	
36+14.05 P.O.T.			2.29	263.41	on Hub
	12.17	265.20	2.67	253.03	
	12.66	277.75	0.11	265.09	
	12.41	290.14	0.02	277.73	
	12.90	302.90	0.14	290.00	
	12.31	314.87	0.34	302.56	
	12.495	327.345	0.02	314.85	
	13.02	340.125	0.24	327.105	

Oct 27-47  
H.S. 5562  
Garber  
Cota  
Cota

		340.125			
	13.215	352.51	0.83	339.295	
	8.47	360.90	0.08	352.43	
39+35.30			8.00	352.90	on Hub
41+79.26			1.78	359.12	" "
	0.87	359.99	1.78	359.12	
	11.98	366.26	5.71	354.28	
	12.025	377.475	0.81	365.45	
	8.26	385.405	0.33	377.145	
47+27.76			7.89	377.515	on Hub
	12.59	397.265	0.73	384.695	
52+28.05			9.355	387.91	on Hub
	13.25	409.755	0.86	396.405	
	5.66	414.515	0.90	408.855	
55+65.04			5.85	408.665	on Hub
	1.115	403.465	12.165	402.350	
	0.92	391.515	12.870	390.595	
	3.77	382.16	13.125	378.390	
	1.375	370.53	13.005	369.155	
	2.085	359.650	12.965	357.565	
	0.61	348.07	12.19	347.460	
	0.44	335.53	12.98	335.09	
	0.16	322.68	13.01	322.52	
59+16.39			8.45	314.23	on Hub
	2.51	313.13	12.06	310.62	
	0.53	300.84	12.82	300.31	

Nov 9-49  
H.S. 5562  
Smith  
Cota  
Cota

77



300.84

2.85	291.23	12.46	288.38
2.64	282.16	10.71	280.53
1.36	271.96	12.56	270.60
1.06	260.37	12.65	259.31
0.94	248.86	12.45	247.92
1.59	237.78	12.67	236.19
1.39	226.505	12.665	225.115
1.96	215.760	12.705	213.800
0.51	202.97	12.30	202.46
1.10	191.47	12.60	190.37
1.18	180.65	12.00	179.47
0.33	169.01	11.97	168.68
0.47	156.42	12.06	155.95
63+85.34 POT		11.69	144.73 on Hub
1.62	146.35	11.69	144.73
1.43	134.80	12.98	132.37
66+40.63 POT		12.03	122.77 on Hub
2.015	124.785	12.03	122.77
6.26	119.68	11.365	113.42

BM

on May  
Parkside Park  
02702  
146+60.09 EC  
455122.82  
9.07  
13.81  
1408-51

Dec. 12-49  
H515509 Chavez  
D501124 Rorer

78

BM	12.57	135.34		122.77	87 1106 66+40.63 POT
65+66.35 A			5.71		
	11.31	144.81	1.84	132.50	
72+50 POT			6.44	138.97	on Hub
	13.34	157.74	0.41	144.40	
75+60.62 POT			0.06	157.68	on Hub
	0.97	152.65	0.06	157.68	on Hub 75+60.62
	3.69	149.66	2.68	145.97	
80+35 POT			9.74	139.92	on Hub
	1.59	138.12	13.12	136.53	
86+33.82 POT			9.33	128.79	on Hub on Hub
	9.93	138.72	9.33	128.79	86+33.82
88+0			2.05	136.67	on Hub
	1.60	127.32	13.00	125.72	
93+25.88			11.96	115.36	on Hub on Hub
	1.26	116.62	11.96	115.36	93+25.88
7+1408.52 BM	0.78	104.29	13.11	102.51	
			9.22	95.07	on Hub on Hub 102.51 9.22
	12.93	116.72	0.50	102.79	9.22
	7.40	123.25	0.87	125.85	
99+21.90			4.80	118.45	on Hub
102+35			8.48	114.77	on Hub

A ledger page with horizontal blue lines and four vertical red margin lines. The page is blank.

A ledger page with horizontal blue lines, a vertical red margin line, and a green grid pattern. The page is blank.

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II.—INCHES IN DECIMALS OF A FOOT.

1/16	3/32	1/8	3/16	1/4	5/16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Deg.	Radius	Mid. Ord.	Tan Offset	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan Offset	Def. for 1 Foot
0°	10'	34377.5	.036	.145	7°	819.02	1.528	6.105	2.10'
	20	17188.8	.073	.291		781.84	1.600	6.395	2.20
	30	11459.2	.109	.436		764.49	1.637	6.540	2.25
	40	8594.42	.145	.582		747.89	1.673	6.685	2.30
	50	6875.55	.182	.727					
1	10	5729.65	.218	.873	8	716.78	1.746	6.976	2.40
	20	4911.15	.255	1.018		688.16	1.819	7.266	2.50
	30	4297.28	.291	1.164		674.69	1.855	7.411	2.55
	40	3819.83	.327	1.309		661.74	1.892	7.556	2.60
	50	3437.87	.364	1.454	9	637.28	1.965	7.846	2.70
		3125.36	.400	1.600		614.56	2.037	8.136	2.80
2	10	2864.93	.436	1.745		603.80	2.074	8.281	2.85
	20	2644.58	.473	1.891		593.42	2.110	8.426	2.90
	30	2455.70	.509	2.036	10	573.69	2.183	8.716	3.00
	40	2292.01	.545	2.181		546.44	2.292	9.150	3.15
	50	2148.79	.582	2.327		521.67	2.402	9.585	3.30
3	10	1910.08	.655	2.618		499.06	2.511	10.02	3.45
	20	1809.57	.691	2.763		478.34	2.620	10.45	3.60
	30	1719.12	.727	2.908		459.28	2.730	10.89	3.75
	40	1637.28	.764	3.054		441.68	2.839	11.32	3.90
	50	1562.88	.800	3.199	11	425.40	2.949	11.75	4.05
4	10	1494.95	.836	3.345		410.28	3.058	12.18	4.20
						396.20	3.168	12.62	4.35
					15	383.07	3.277	13.05	4.50
						370.78	3.387	13.49	4.65
						359.27	3.496	13.92	4.80
					16	348.45	3.606	14.35	4.95
						338.27	3.716	14.78	5.10
					17	319.62	3.935	15.64	5.40
						302.94	4.155	16.51	5.70
5	10	1146.28	1.091	4.362		287.94	4.374	17.37	6.00
	20	1109.33	1.127	4.507		274.37	4.594	18.22	6.30
	30	1074.68	1.164	4.653		262.04	4.814	19.08	6.60
	40	1042.14	1.200	4.798		250.79	5.035	19.94	6.90
	50	1011.51	1.237	4.943		240.49	5.255	20.79	7.20
		982.64	1.273	5.088					
6	10	955.37	1.309	5.234		231.01	5.476	21.64	7.50
	20	929.57	1.346	5.379		222.27	5.697	22.50	7.80
	30	905.13	1.382	5.524		214.18	5.918	23.35	8.10
	40	881.95	1.418	5.669		206.68	6.139	24.19	8.40
	50	859.92	1.455	5.814		199.70	6.360	25.04	8.70
						193.18	6.583	25.88	9.00

NOTE. Chord Deflection=2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

3.27.74  
53  

---

380.24

83.64  
32.84  

---

58.76

3464.00  
32.88  

---

3111.2  
2932  

---

1180

10 2 25  
15 4 4 7  

---

2 1 2

65  
66  

---

132

1460

147 95  
65 7.2  

---

7.2 1.0

6.57  
7.15  
7.92  
6.57  

---

14.21

31  
6.22 35  
6.17  
6.57

24.40

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \div 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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