

1813

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and,
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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1813

CITY ENGINEER'S OFFICE

INDEXED

to page 65

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

149.67

8.85

158.52

13.02

145.50

2.07

147.57

13.00

134.57

0.73

135.30

2.57

132.73

10.31

143.04

6.10

136.94

F + 40

s.w.

47.57

4.92

142.65

25.30

3.47

131.83

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1

	Page
Fence Marks - Check - 30th & Meade	2
Sever - Pelton - Levels Block 87 - E.M. MORSE'S	3
X-Section Dickens - Evergreen to Plum	9-25
X-Section - Intersection Eads + Rushville	54-57
X-Section Hill Top et al (F.O.)	26

Walker Handrick Ecker Johnson 12-1-47	Check Bench Marks - Meade Ave from Kansas to 32nd.			
	32nd - From Meade to Adams.			
	Adams - from 32nd to 30th			
	30th - from Adams to Meade			
chk. Starting B.M.	4.79	366.78 = B.M.		
chk B.M.	5.81	366.80		
		365.76 - Bottom of 365.78 Page		
T.P.	1.62	371.59	10.28	369.90
T.P.	1.12	380.18	8.10	378.95 - Record
T.P.	0.75	387.16	6.40	379.06
T.P.	3.34	387.16		386.41
- chk B.M.	3.92	381.81	5.96	389.88 - Record
T.P.	4.61	392.81	5.96	389.47
chk.		395.43	5.68	390.82
			5.19	390.96 = Record
T.P.	6.70	396.50	3.99	391.31
T.P.	7.69	393.72	4.36	389.80
T.P.	5.53	390.46	4.06	385.80 = Record
T.P.	5.33	388.99	4.72	386.10
check			5.67	382.39 = Record
T.P.	6.25	388.38	3.65	382.71
			5.24	382.13
T.P.	2.98	385.78	5.40	380.54
chk.			4.81	389.22 = Record
T.P.	4.90	388.20	0.32	382.80
check			8.18	383.39
T.P.	11.99	381.62	1.83	379.63
check			5.70	373.44
	4.68	371.46		379.52 = Record
				365.80 = Record
				365.76
				366.78

Indexed
B

INDEXED

- ✓ Chk Starting B.M. S.E. BR MEADE & KANSAS
- check S.E. Brass Plug Meade & 30th
- S.E. Brass Plug MONROE & 30th
- S.E. B.P. ADAMS & 30th
- S.E. B.P. ADAMS & BOUNDARY
- B.M. S.E. B.P. ADAMS & 32ND
- 90 Conc Wall 5' East east edge Walk 4533-32ND
- B.M. S.E. B.P. MONROE & 32ND
- ✓ B.M. N.W. B.P. Meade & 32ND
- ⊙ B.M. N.W. Meade & ~~32ND~~ Jovia
- Brass Plug gone
- N.W. Hole in Curb Meade & ~~32ND~~ Boundary
- plug gone S.E.
- hd = Hole Meade & Ohio.
- ✓ B.M. S.E. Brass Plug Meade & 30th
- ✓ B.M. S.E. Brass Plug Meade & Kansas

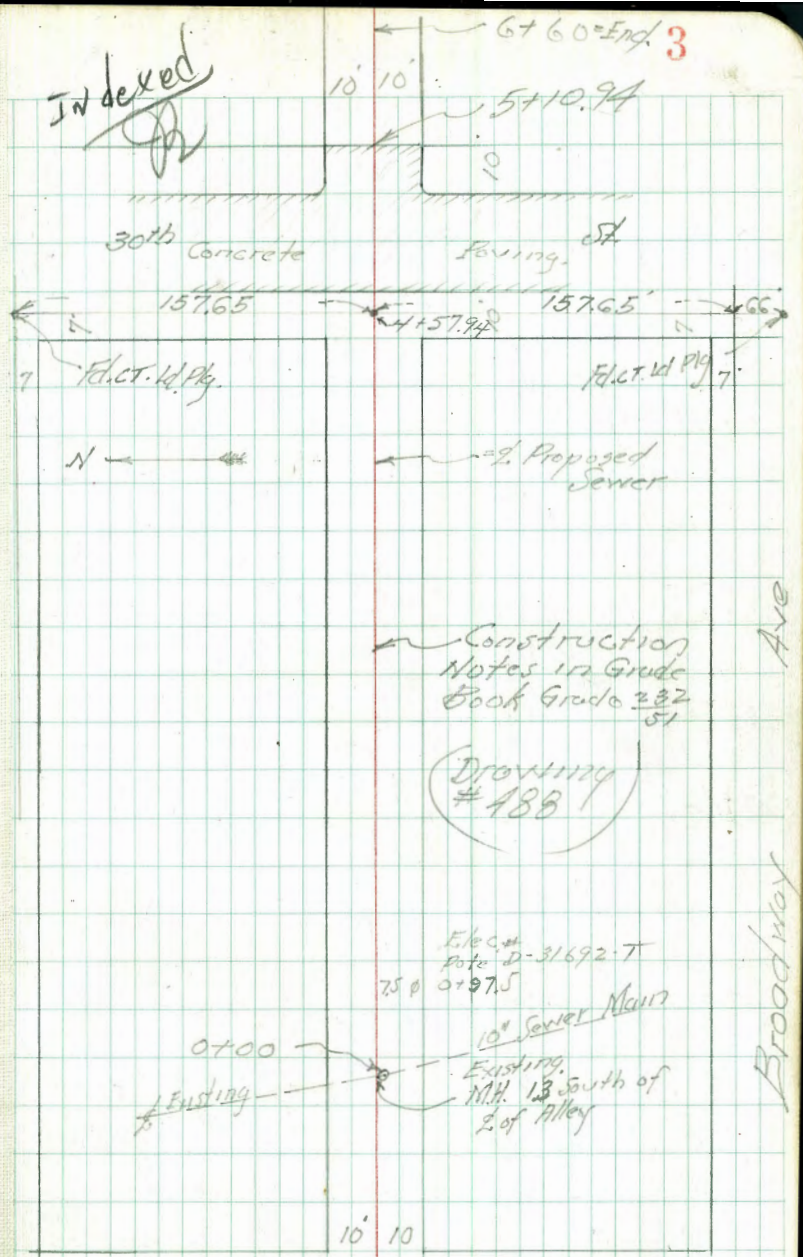
Walker
Hendricks
Becher
Johnson
12-7-47
Preliminary Levels - Sewer
in Block 87 - E. V. MORSE'S SUBD.
Between Broadway & C. St.

(W.O. 80079)

4757.94 = POT. Spike

INDEXED

0+00
= Existing M.H.



0+40

0+35

0+26

0+16

0+00 Existing MH

T.P. -0.01 161.84 11.29 161.85

T.P. 0.07 173.14 13.05 173.07

T.P. 0.64 186.12 12.37 185.48

chk St. Brass Pkg. 2.61 195.08 Record

2.89 197.85 194.96

Lt

L

Rt

4

148.0
13.8

148.4 147.2 148.9 149.2 148.8 148.4
14.4 14.6 12.9 12.6 13.0 13.4
20 10 20 50
Channel in channel

150.7
11.1

150.7 150.7 149.6 149.9
11.1 11.1 12.2 11.9
100 50 25
Too Fill

158.48 146.42
9.36 154.2
with MH 1.3
161.84 2 MH on Flow line

Broadway & 30th
B.M. 5th B.P. C.S. & 30th

TP 11.55 185.19 0.21 173.64
1+80

1+57

02.11

1+00

T.P 12.00 173.85 +0.01 161.85

0+85

0+65

0+50

161.84

L

5

172.1

18

169.2 165.2 163.3 160.4 153.1

42 82 105 135 185
50 20 50 125
700

157.7

165

161.4 159.3 156.8 153.9 153.3 151.8 148.0 148.4
175 145 175 200 205 225 250 255
46 40 15 21 46 79 116
700

173.85

7

1600 156.6 153.3 152.8 147.7
18 52 85 90 141
50 19 4 50

149.7 149.5 150.0 150.1 149.3 149.1 148.3
121 123 118 117 125 127 135
50 44 38 20 20 50

149.0

12.8

161.84

Alley Block 87 - Sewer
E.V. MORSE'S SUB.

2+90

INDEXED

2+51.5 End of Sidewalk 5.5 LTR

2+51 Power Pole 8.7 RTR A-2780

2+50 8" Peppertree 5' LTR

2+47.5 End House 8.5 LTR

2+35 Dead Man to Pole 9.2 LTR

TP. 9.88 192.30 2.77 182.42

2+31 Beg House 8.5 LTR

2+25 Beg side walk on Lt. 5.5

2+00

185.19

Lt L Rt 6

187.4
48

188.25 188.20
4.05 4.10
85 55
5.11 5.11

187.99	187.97	87.5	186.5	176.7	171.7	157.6	158.0
4.31	4.21	4.8	6.9	15.6	21.0	34.2	34.2
85	55		11	50	78	108	123
5.11	5.11						700

192.30

185.07	184.65	184.5	175.2	163.1	153.5	153.7
0.12	0.54	1.7	10.0	18.1	29.2	29.5
21	55		47	84	114	125
5.11	5.11					700

179.2	176.0	170.0	160.8	157.0
6.0	9.2	15.0	24.4	28.2
25		40	90	115
				700

185.19

Alley Block 87 - Sewer
 E.H. MORSE'S SUB

INDEXED

4+52.4 W. Edge of ^{Asphalt} Sidewalk west side 30th St.

4+20

3+88 Top of fill

TP. 9.05 199.64 1.71 190.59

3+63 Toe of fill

3+53 End of Board Walk

3+50

3+38 @ 5° Wooden Stairway 46 L.L. @

3+28 Beg 3.5 Board Walk South edge on @

3+00

192.30

6

7

193.75 193.46 193.57

58⁸ 61⁸ 61²
 177 10
 Beg Cont Beg Cont
 Walk Walk

193.9 192.5 191.8

57 7¹ 7⁸
 50 50

193.4 192.6 190.8 187.0

62 7⁰ 8⁸ 12⁼
 25 199.64 50 130
 77

180.4

11⁹

182.1 177.1 171.0

10² 15² 21³
 17 45

189.6 185.3 176.5 164.3

27 7⁻ 15⁸ 28⁰
 18 43 83

192.30

77

Alley Block 87 - Sewer
E.V. MORSE'S SUB.

INDEXED

5+20

5+10.8 E Line South Edge of Conc. Drive

5+00.8 E Curb 30th St.

4+80.8 E 30th St.

4+60.8 W Curb Line 30th St.

4+57.94 East Edge of Sidewalk.

19964

8

8

1946 192.8 1916 194.8 194.6
5° 68 8° 48 5°
72 50 26 17

194.68 194.30 194.41
49 534 523
10 10

193.59 193.84 193.81 193.77 194.48
505 580 583 587 516
10 10 10 10
Cb. Gut Gut Cb.

194.17 194.10 194.03
547 554 561
18 10

193.67 193.11 192.91 192.78 193.17
597 653 673 686 647
18 18 193.47 10 10
Cb. Gut Cb. Gut Cb.

193.75 193.46 193.35
588 618 629
177 10
Beg Conc. Beg Conc.
Walk Walk
19964

Alley Block 87 - Sewer
E. W. MORSE'S SUB.

INDEXED

9

CE BM 466 194.98 194.96

6+60

SWBP 30th & C Sts.

204.8	204.6	204.1
+5 ²	+5 ⁰	+4 ²
10		15

6+35

205.1	204.3	204.0
+5 ⁵	+4 ⁷	+4 ⁴
30		15

6+10 Power Pole 8' R.I.E. A3020

5+65

1974	1971	197.1	197.2	196.2
2 ²	2 ⁵	2 ⁵	2 ⁴	3 ⁴
50	18		17	100

19964

19964

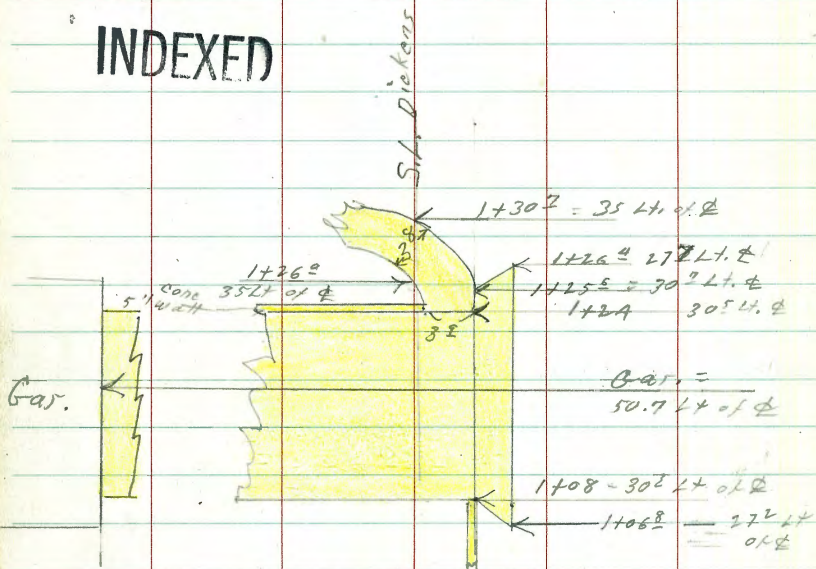
CrossSec. Evergreen to Clove

1-26-48

W.O. 25001

Sammelmeyer
McCoy
W Moore
E Sherman

INDEXED



Note

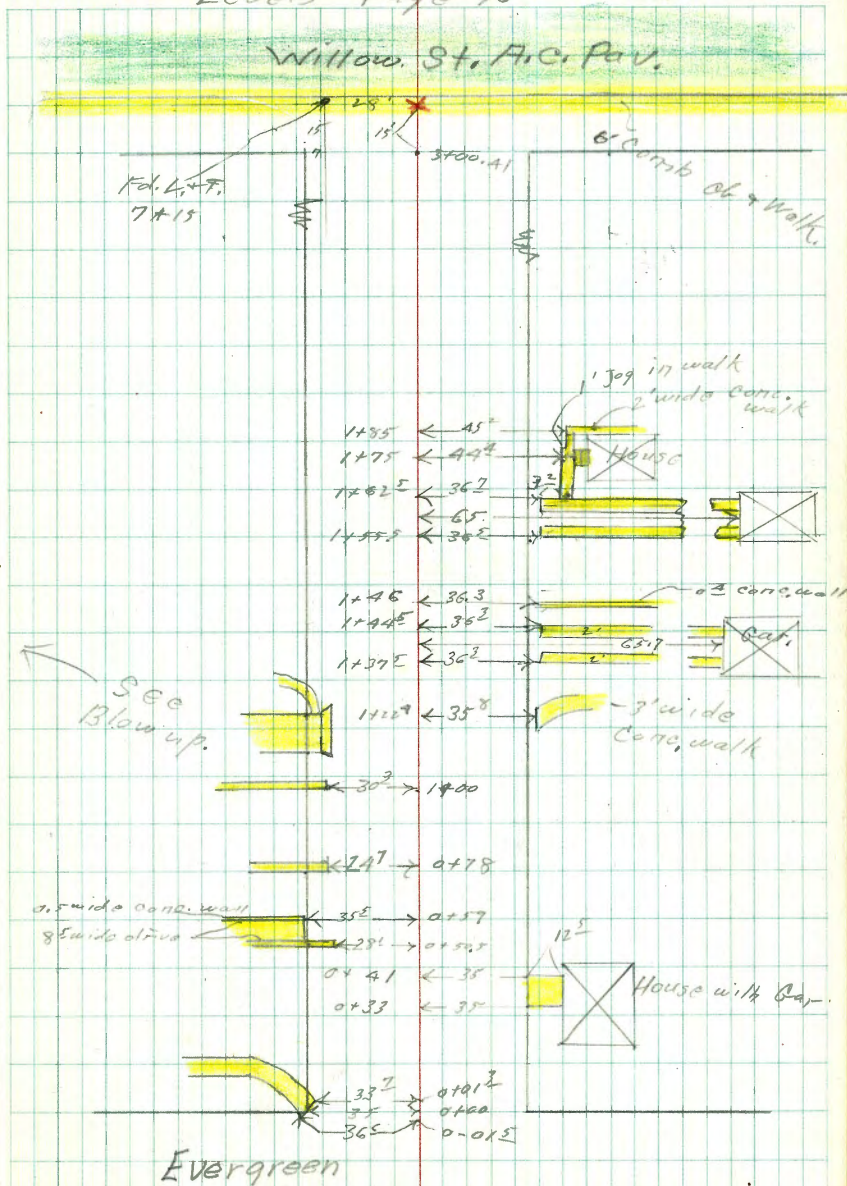
Why line Evergreen + 1+50
checked 4/29/49. No changes.

For Sta. 2+00 - 2+01 + 2+02

See F.B. 1854

47459

off



Dickers

INDEXED

0+00

0-15 = 36° Lt. Sly. Cor. walk (P-10)

0-35 = ϕ Evergreen

0-52 = 60° Rt. = Cl. EC. E. Cl. line Evergreen

0-70 = 25' Lt. = End exist. Cl. E.L. Evergreen = end A.C. Pav.

0-95 curb B.C. 25' East of S. line Evergreen

S-P Emerson
SAP-4 Evergreen
DISK
0130-21
7.11 25.61 — 18.50

23.08	22.91	22.31	22.31	22.61	22.51
$\frac{2.53}{35}$ walk	$\frac{2.7}{35}$ Dirt	$\frac{3.3}{17}$	3.3	$\frac{3.0}{12}$	$\frac{3.1}{35}$
23.08	22.11	20.61	20.61	20.51	20.41
$\frac{2.53}{35}$	$\frac{3.5}{135}$	$\frac{5.0}{35}$	5.0	$\frac{5.1}{35}$	$\frac{5.2}{135}$
19.81	19.91	19.91	19.81	19.71	19.61
$\frac{5.8}{35}$	$\frac{5.7}{17}$	5.7	$\frac{5.8}{17}$	$\frac{5.9}{35}$	$\frac{6.4}{20}$ Dirt
19.63	19.17	19.25	19.21	19.11	18.96
$\frac{5.98}{25}$ 00	$\frac{6.44}{25}$ 0	$\frac{6.36}{17}$	$\frac{6.31}{85}$	$\frac{6.50}{85}$	$\frac{6.65}{17}$
19.26	18.85	18.95	18.94	18.98	18.51
$\frac{6.95}{17}$ 0	$\frac{6.76}{17}$ 0	$\frac{6.66}{85}$	6.67	$\frac{6.83}{85}$	$\frac{7.18}{17}$ 0
19.25	19.25	19.25	19.25	19.25	18.94
$\frac{6.36}{17}$	$\frac{6.31}{85}$	$\frac{6.40}{85}$	$\frac{6.50}{85}$	$\frac{6.65}{17}$	$\frac{6.81}{24.8}$ 0
19.25	19.25	19.25	19.25	19.25	19.25
$\frac{6.36}{17}$	$\frac{6.31}{85}$	$\frac{6.40}{85}$	$\frac{6.50}{85}$	$\frac{6.65}{17}$	$\frac{6.81}{24.8}$ 0

25.61

0+51 35' Lt. = start. Conc. drive

0+50^S Cont.0+50^E 35' Lt. = stop up in top of wall.
28' Lt. = 6" wide conc. block wall

0+50

0+41 35' Rt. = End same

0+33 35' Rt. = start Conc. Apron

T.P. 12.13 36.23 1.51 24.100+01² 33' Lt. = Nly. Cor 4' walk (P. 10)

25.61

$$\begin{array}{r} 26.63 \\ 9.60 \\ \hline 30 \\ \hline \text{on drive} \end{array}$$

$$\begin{array}{r} 30.11 \\ 6.12 \\ \hline 30 \\ \hline \text{top wall} \end{array}$$

25.63

$$\begin{array}{r} 10.6 \\ 9.5 \\ \hline \text{Base of wall} \end{array}$$

$$\begin{array}{r} 25.83 \\ 10.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 28.05 \\ 8.18 \\ \hline 30 \\ \hline \text{top wall} \end{array}$$

$$\begin{array}{r} 25.73 \\ 10.5 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 25.63 \\ 10.6 \\ \hline 30 \\ \hline \text{Base of wall} \end{array}$$

$$\begin{array}{r} 25.23 \\ 11.0 \\ \hline 15 \end{array}$$

25.23

$$\begin{array}{r} 25.73 \\ 10.5 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 25.29 \\ 10.94 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 25.21 \\ 11.02 \\ \hline 35 \end{array}$$

30.23

23.07

$$\begin{array}{r} 2.54 \\ 392 \end{array}$$

25.61

$$\begin{array}{r} 26.63 \\ 9.72 \\ \hline 35.5 \end{array}$$

$$\begin{array}{r} 30.02 \\ 6.21 \\ \hline 35.6 \\ \hline \text{top of top} \end{array}$$

25.63

$$\begin{array}{r} 10.6 \\ 9.1 \\ \hline \text{Base of wall} \end{array}$$

$$\begin{array}{r} 25.83 \\ 10.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 28.05 \\ 8.18 \\ \hline 30 \\ \hline \text{top wall} \end{array}$$

$$\begin{array}{r} 25.73 \\ 10.5 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 25.63 \\ 10.6 \\ \hline 30 \\ \hline \text{Base of wall} \end{array}$$

$$\begin{array}{r} 25.23 \\ 11.0 \\ \hline 15 \end{array}$$

25.23

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30.23

23.07

$$\begin{array}{r} 2.54 \\ 392 \end{array}$$

25.61

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25.63

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$$\begin{array}{r} 25.21 \\ 11.02 \\ \hline 35 \end{array}$$

30.23

23.07

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25.61

$$\begin{array}{r} 26.63 \\ 9.72 \\ \hline 35.5 \end{array}$$

$$\begin{array}{r} 30.02 \\ 6.21 \\ \hline 35.6 \\ \hline \text{top of top} \end{array}$$

25.63

$$\begin{array}{r} 10.6 \\ 9.1 \\ \hline \text{Base of wall} \end{array}$$

$$\begin{array}{r} 25.83 \\ 10.0 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 28.05 \\ 8.18 \\ \hline 30 \\ \hline \text{top wall} \end{array}$$

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$$\begin{array}{r} 25.23 \\ 11.0 \\ \hline 15 \end{array}$$

25.23

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30.23

23.07

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$$\begin{array}{r} 25.73 \\ 10.5 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 25.29 \\ 10.94 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 25.21 \\ 11.02 \\ \hline 35 \end{array}$$

30.23

23.07

$$\begin{array}{r} 2.54 \\ 392 \end{array}$$

25.61

INDEXED

1+00 Cont.

Also: start 8' wide E.+W. Conc. wall

1+00 30³ Lt. = £ 8" wide Conc. wall0+78 2A¹ Lt. = £ 3' wide Conc. wall

0+60

0+59³ = 35⁵ Lt. = £ 5" wide N+S Conc. wall0+59 35⁵ Lt. = End Conc. drive

36.23

4.80	4.78	6.3	5.0				
50	52	35	35				
top	top	base	Dir				
wall	wall	wall					
31.11	29.93	30.23	30.13	29.03	29.23	29.73	30.23
5.12	6.3	6.0	6.1	7.2	7.0	7.5	6.0
30.3	30.2	30	19	13		15	35
top	Base						
wall	wall						
28.79	28.33	28.10					
7.74	7.90	8.13					
47.7	35.5	24.7					
at stops	Brk. in						
grade							
27.83	26.53	26.23					
8.4	9.7	10.0					
35	24	15					
28.08	27.99	26.13					
8.15	8.24	10.1					
49	35.5	35.5					
top wall	top wall	Base of wall					
26.76	26.55						
9.41	9.68						
10	35.5						
at drive							

36.23

INDEXED

1+24 { 34th Lt. = East face 5" wide Conc. wall.
28" wide conc. walk.
30th Lt. = End main drive & start

1+22^A 35th Rt. = ϕ 3' wide Conc walk

1+08 Cont

main conc. drive

1+08 30th Lt. = End Conc. wall. also = start

Apr-17 to driveway

1+06^S 29th Lt. = start. Conc. placed

36.23

31.94	32.43	32.13
4.29	3.80	4.10
50.7	50	34.4
Drive	top	top of
# + Car.	wall	wall

31.33	31.59	31.42
4.9	4.64	4.81
34.2	30.3	27.6
Base wall	End	Appro
	drive	

32.85	33.17
3.38	3.06
35.8	47
* walk	walk at house

31.95	31.53
4.28	4.70
50.7	35
at Car.	drive

31.41	31.90	30.83	31.05
4.92	4.83	5.4	5.18
30.3	30.3	32.3	27.2
drive	Top wall	Base	Appro
		wall	

31.05
5.18
27.2

36.13

Dickens
INDEXED

1+75^E 47th RT. = 5th wide Conc. steps
44th RT. = S. Edge 3' wide walk

1+62^E Cont.

1+62^E 39.9 = S.E. Cor walk - 43.2 = N.E. Cor ^{walk}
36th RT. = End same

1+55^E 36th RT. = start conc. ribbon drive
2' wide ribbons

T.P. 11.83 46.30 1.76 34.47

1+46^E 36th RT. = 0th wide Conc. wall

1+44^E 36th RT. = End ribbon drive

	38.57	38.70	41.20
	<u>7.73</u>	<u>7.60</u>	<u>5.1</u>
	44.4	47.4	51.4
	walk	walk	at porch
		at steps	
	39.70		
	<u>8.60</u>		
	65.1		
	at Bar		
	36.16	36.66	37.05
	<u>9.84</u>	<u>9.69</u>	<u>9.11</u>
	36.7	39.9	43.2
	Drive	walk	walk
			at Drive
	36.18	37.13	37.40
	<u>10.12</u>	<u>9.17</u>	<u>8.00</u>
	36.5	45.6	65.1
	at	ribbons	at Bar
	16.30		
	34.63	34.89	36.03
	<u>1.6</u>	<u>1.34</u>	<u>0.2</u>
	36.3	36.3	65
	Base	top	at top of
	wall	wall	wall
	34.58	35.33	
	<u>1.64</u>	<u>0.70</u>	
	36.3	65.7	
		at par.	

T.P. 12.33 66.21 0.37 53.88

2+15

INDEXED

T.P. 12.68 54.25 4.73 41.57
N. Edge.
M.H.

(see F.B. 1854 4/29/49)
47+59

1+86 45° Rt. = End 1' wide E+W. walk

1+85 45° Rt. = $\frac{1}{2}$ 2' wide N+W. walk

1+80 Cont.

1+80

45° Rt. = start 2' wide conc. walk

1+77 44° Rt. = End 3' walk (conc.)

46.30

<u>50.05</u>	<u>48.35</u>	<u>47.95</u>	<u>48.95</u>	<u>48.35</u>	<u>44.05</u>	<u>43.65</u>	<u>42.25</u>	<u>43.55</u>
$\frac{42}{75}$	$\frac{59}{35}$	$\frac{6.8}{25}$	$\frac{5.8}{14}$	5.9	$\frac{10.2}{15}$	$\frac{10.6}{35}$	$\frac{12.0}{30}$	$\frac{10.7}{75}$

54.25

39.43
6.87
45.2

39.86
6.94
75.2

40.06
6.24
56.2
on walk

39.00
7.30
46.30

39.20
7.1
30

41.50
7.8
75

39.20
7.1
35

38.00
8.3
17

40.40
5.9
11

39.90
6.4
8

40.30
6.0
27

37.60
8.7
35

38.50
8.3
45

38.40
7.9
45

38.58
7.72
44.4
3' walk

38.66
7.64
47.2
2' walk

38.76
7.54
47.2
Back
of walk

46.30

INDEXED

S.W.B.R
Willow + Dickens 1.22 76.40 76.40

3+18^E = Ely. gutter willow, In gutter

3+18^W = Ely. Cb. line willow Top of Ch.

3+00^W = E. Line willow

2+83

T.P. 11.70 77.62 0.29 65.92

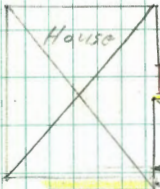
2+50 87 Lt. = N.E. Cor. House, Faces Willow St.
66.21

76.46	77.26	77.82	78.62	78.62	58.41
1.16	4.36	11.8	7.8	7.8	7.8
100	100	75	75	75	87
77.47	75.26	67.62	65.82	56.91	56.91
3.15	2.36	1.0	11.8	7.3	7.3
60	60	75	75	35	35
73.87	77.51	44.32	72.52	56.01	56.01
3.75	3.11	3.3	7.1	10.2	10.2
35	35	35	35	23	23
73.37	74.07	44.32	72.52	59.31	59.31
4.25	3.55	3.3	7.1	4.9	4.9
17	17	35	35	12	12
72.92	73.67	43.52	71.92	58.61	58.61
4.70	3.95	4.1	5.7	7.6	7.6
17	17	35	35	15	15
72.54	73.23	72.72	71.72	54.31	54.31
5.08	4.89	5.4	6.5	11.9	11.9
35	35	35	35	35	35
71.85	72.57	69.82	61.32	53.21	53.21
5.77	5.05	7.8	16.3	13.0	13.0
60	60	75	35	100	100
70.10	70.86	69.82	56.52	51.11	51.11
7.52	6.76	7.8	24.1	15.1	15.1
60	60	75	75	100	100
66.64	67.41	57.82	57.82		
10.98	10.21	12.8	12.8		
100	100	110	110		

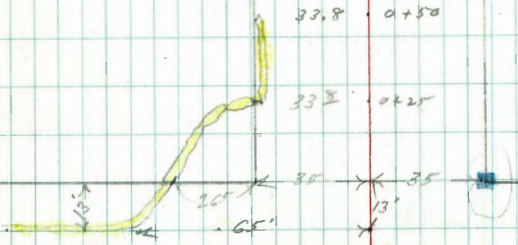
CLARK ST.

3100.8

INDEXED
FEB 3 1948



8' wide brick steps



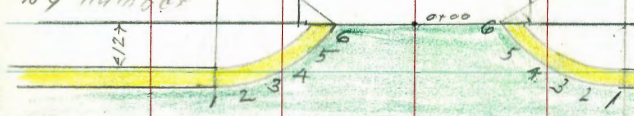
PLUM ST.

← 35 → ← 35 →

PLUM ST.

DICKENS

R=43
L=41.4
5 Equal Pts.
by number



R=43
L=41.4
Equal Pts.
By number
6' comb.
Cb. + Walk

WILLOW ST.

6 = End-curbs.

74.84

75.14

$\frac{4.35}{\#6 BC}$

$\frac{4.05}{\#6 pav}$

$\frac{5.44}{\#6 pav}$

$\frac{4.65}{\#6 BC}$

5

75.24

$\frac{3.75}{\#5 BC}$

$\frac{4.43}{\#5 pav}$

$\frac{5.85}{\#5 pav}$

$\frac{5.08}{\#5 BC}$

4

75.36

$\frac{3.83}{\#4 BC}$

$\frac{4.40}{\#4 pav}$

$\frac{6.34}{\#4 pav}$

$\frac{5.55}{\#4 BC}$

3

75.65

$\frac{3.54}{\#3 BC}$

$\frac{4.32}{\#3 pav}$

$\frac{6.95}{\#3 pav}$

$\frac{6.12}{\#3 BC}$

2

75.91

$\frac{3.22}{\#2 BC}$

$\frac{4.02}{\#2 pav}$

$\frac{7.56}{\#2 pav}$

$\frac{6.78}{\#2 BC}$

1 on returns (page 19)

B.C. Cba

$\frac{2.90}{\#1 BC-BC}$

$\frac{3.67}{\#1 pav}$

$\frac{8.20}{\#1 pav}$

$\frac{7.40}{\#1 BC-BC}$

Southwest return

Northwest return

0-18 Conf.

$\frac{9.70}{100 BC}$

$\frac{1.70}{100 pav}$

$\frac{2.71}{60 Top of B.C.}$

$\frac{7.40}{80 Top of B.C.}$

$\frac{11.49}{100 pav}$

$\frac{10.70}{100 BC}$

0-18 Wly. curb. lime willow

$\frac{3.68}{60 pav}$

$\frac{4.42}{35 pav}$

$\frac{4.25}{17 pav}$

$\frac{5.05}{pav}$

$\frac{5.50}{17 pav}$

$\frac{6.25}{35 pav}$

$\frac{8.20}{60 pav}$

Willow + Dickens 2.79 79.19 — 76.40 S.W.B.P.

79.19

INDEXED

-1+00

T.P. 12.44 103.55 0.12 91.11

0+60

0+30

T.P. 12.81 91.23 0.77 78.42

0+02

0+00 Cont.

paving + curbs.

0+00 = Wly. line Willow = Ehd

79.19

	105.05		98.65		98.35		88.25		80.75		84.75	
	$\frac{+5.0}{75}$	$\frac{+2.5}{35}$	$\frac{+1.6}{25}$	4.9	$\frac{5.2}{19}$	$\frac{15.3}{35}$	$\frac{22.8}{25}$	$\frac{15.3}{35}$	$\frac{22.8}{25}$	$\frac{15.3}{35}$	$\frac{15.8}{35}$	
				<u>103.55</u>								
		98.13		89.73		89.43		86.23		76.33		84.33
		$\frac{+7.5}{70}$	$\frac{+6.9}{35}$	$\frac{+4.6}{19}$	1.5	$\frac{1.8}{27}$	$\frac{5.0}{35}$	$\frac{14.9}{43}$	$\frac{5.9}{100}$	$\frac{14.9}{43}$	$\frac{5.9}{100}$	
		91.23		83.33		81.73		71.63		70.23		74.23
		$\frac{+3.7}{70}$	$\frac{+3.0}{35}$	$\frac{+2.3}{26}$	7.9	$\frac{9.5}{35}$	$\frac{19.6}{64}$	$\frac{24.0}{82}$	$\frac{17.0}{100}$	$\frac{24.0}{82}$	$\frac{17.0}{100}$	
					<u>91.23</u>							
				75.19		74.39		70.39		69.09		69.19
		$\frac{+9.2}{75}$	$\frac{+8.0}{35}$	$\frac{4.0}{16}$	4.2	$\frac{4.8}{35}$	$\frac{8.8}{60}$	$\frac{10.1}{80}$	$\frac{9.5}{100}$	$\frac{4.8}{35}$	$\frac{9.5}{100}$	
		78.09		76.99		74.29		70.59				
		$\frac{4.1}{75}$	$\frac{2.2}{35}$			$\frac{4.9}{35}$	$\frac{8.6}{75}$					
	75.74		74.84		74.97		74.75		73.75		74.54	
	$\frac{4.05}{24.7}$	$\frac{4.35}{24.7}$	$\frac{4.22}{17}$	4.20	$\frac{4.74}{17}$	$\frac{5.44}{24.8}$	$\frac{4.65}{24.8}$	$\frac{5.44}{24.8}$	$\frac{4.65}{24.8}$	$\frac{5.44}{24.8}$	$\frac{4.65}{24.8}$	
	Ehd	Par	Par	Par	Par	Par	Par	Par	Par	Par	Ehd	
											cl.	
					<u>79.19</u>							

INDEXED

- 0+00 } 615 ft. = Face Rock + Corro. wall.

3+70⁰⁷ } = Wly line PlumN.W. Mon. }
T.P. } 13.00 140.79 0.63 127.79 Plum + Dickens3+35⁰⁷ = \pm Plum.3+00⁰⁷ = Ely. line Plum

T.P. } 12.99 128.42 0.12 115.43

2+50

2+00

1+50

12.07 115.55 0.07 103.48
103.55

135.39	133.19	133.59	123.29	123.69	128.09	129.89
$\frac{5.4}{81.5}$	$\frac{7.6}{61.5}$	$\frac{7.2}{61}$	$\frac{17.5}{35}$	17.1	$\frac{12.7}{35}$	$\frac{10.9}{80}$
T.P. wall	Bottom wall			140.79		
		119.02	115.32	117.52	121.42	124.42
$\frac{+6.0}{100}$	$\frac{+2.5}{55}$	$\frac{9.4}{35}$	$\frac{13.1}{25}$	10.9	$\frac{7.0}{35}$	$\frac{9.6}{53}$
		120.82	113.22	110.82	115.82	121.42
			128.42			
		120.05	107.05	105.45	106.25	108.85
	$\frac{+11.5}{75}$	$\frac{+4.5}{35}$	8.5	$\frac{18.1}{27}$	$\frac{9.3}{35}$	$\frac{6.7}{50}$
	117.55	109.75	106.75	105.75	98.65	98.85
		112.95	111.45	105.65	100.25	98.85
						100.45
	$\frac{+7.0}{75}$	$\frac{+2.0}{35}$	$\frac{5.8}{8}$	$\frac{8.8}{7}$	9.8	$\frac{15.3}{20}$
	115.55	112.95	111.45	105.65	100.25	98.65
						98.85
						94.05
						91.05
						95.75
	$\frac{9.0}{75}$	$\frac{2.6}{35}$	$\frac{4.5}{25}$	9.9	$\frac{14.8}{15}$	$\frac{20.3}{29}$
	115.55	112.95	111.45	105.65	100.25	98.65
						98.85
						94.05
						91.05
						95.75
						19.8
						80

INDEXED

1+22^z 56' Lt. = End double garage ^{Floor} Corro.
32' Lt. = End oil drive

1+04^z 56' Lt. = Start double Gar. ^{Floor} Corro.

1+02^z 56' Lt. = ~~2~~ 2' wide conc. walk
32' Lt. = start oil drive to double Gar.

T.P. 148.14 8.24 0.89 139.90

1+00

0+50 33^z Lt. = End rock wall.

0+25 33^z Lt. = k in wall.

140.79

11.85 56 Gar. Floor	12.0 54 Drive	7.9 34 Drive	7.9 32 Drive	136.29	136.14	140.24	140.24
11.85 56 Gar. Floor	12.2 54 Drive	9.9 33 Drive	10.0 32 Drive	136.29	135.94	138.24	138.14
11.99 56 Drive * + walk	12.2 54 Drive	10.1 35 Drive	10.2 32 Drive	136.15	135.94	138.04	137.94
5.0 35	5.0 35	6.0 33.8 Top of Wall	6.0 33.8 Bottom Wall	135.79	135.79	134.79	135.29
4.7 50	5.4 38	7.6 33.8 Bottom Wall	7.4 33	136.09	135.89	137.19	136.29
9.3 35	9.3 35	9.0	9.0	131.49	131.49	131.79	131.79
8.9 70	8.9 35	14 8.14	14 8.14	139.89	139.89	140.19	140.19
				140.79			

Dickens

24

Check N.W. Men.

Close + 0.10 = 1.84

1.84

155.42

4.30

0.10 off.

153.58

~~153.68~~

INDEXED

(Closest.)

3+00³ 60⁵ Lt. = Line of house (Faces)

2+50

2+03 35² Lt. = Pole # 3457

2+00

T.P. 9.94 157.88 0.20 147.94

1+90 35² Lt. = Ctr. Deadman

1+50

49² Lt. = Edge porch

1+27⁵ 45² Lt. = 8' wide Brick steps

1' Below top.

property owner says it is approx

Bottom of wall but dug up!

1+23 35² Lt. = 10" Conc. Wall

148.14

4.12	6.5	10.15		
48	33.2	35.2		
Top of wall	Top of wall	Bottom of wall		
143.92	141.64	137.64	148.14	
144.29	141.99	141.99		
5.7	5.1	4.1	3.3	3.4
30	35		35	50
142.74	143.04	144.04	144.84	147.74
11.8	10.4	9.2	9.3	10.0
60	35		35	60
146.08	147.48	148.68	148.58	147.88
7.7	6.7	5.9	6.8	7.2
60	35		35	60
150.18	151.18	151.98	151.08	150.68
5.1	4.3	3.9	5.3	5.6
60	35		35	60
152.78	153.58	153.98	152.58	152.28

INDEXED

Check S.W.B.P.
Evergreen + Fenelon 2.66 25.09 (25.11)

Orig B.M.
Page 11 9.26 27.75 5.61 18.49 (18.50)

T.P. 2.63 24.10 7.85 21.47

T.P. 0.20 29.32 12.68 29.12

T.P. 0.24 41.80 12.26 41.56

T.P. 0.91 53.82 12.36 52.91

T.P. 1.37 65.27 12.79 63.90

S.W.B.P.
Willow + Dickens 0.30 76.69 5.99 76.39 (76.40)

T.P. 0.40 82.38 12.71 81.98

T.P. 0.40 94.69 12.90 94.29

T.P. 0.05 107.19 12.73 107.14

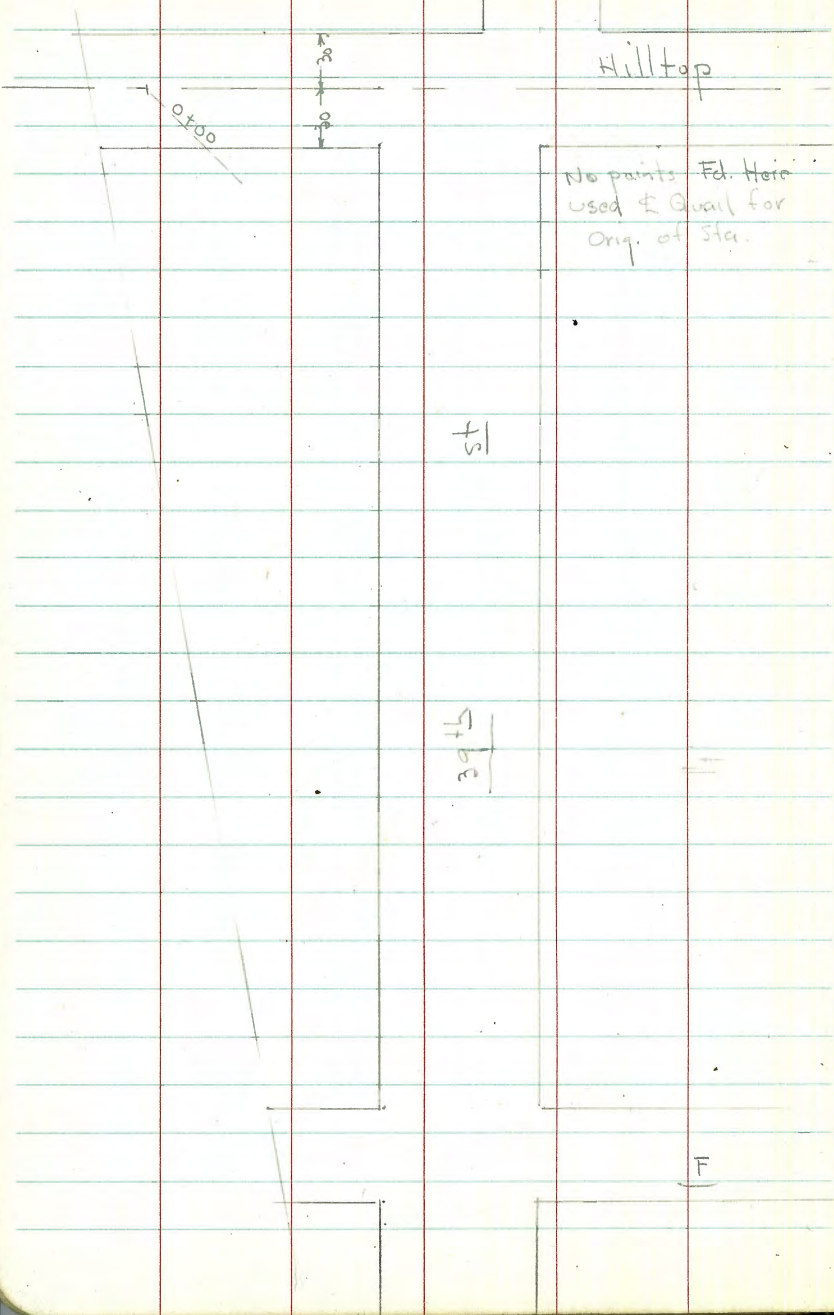
T.P. 0.30 119.87 12.81 119.57

N.W. Mon.
Plum + Dickens 4.60 127.78 127.79

T.P. 2.10 132.38 12.88 130.28

T.P. 0.16 143.16 12.42 143.00

155.42



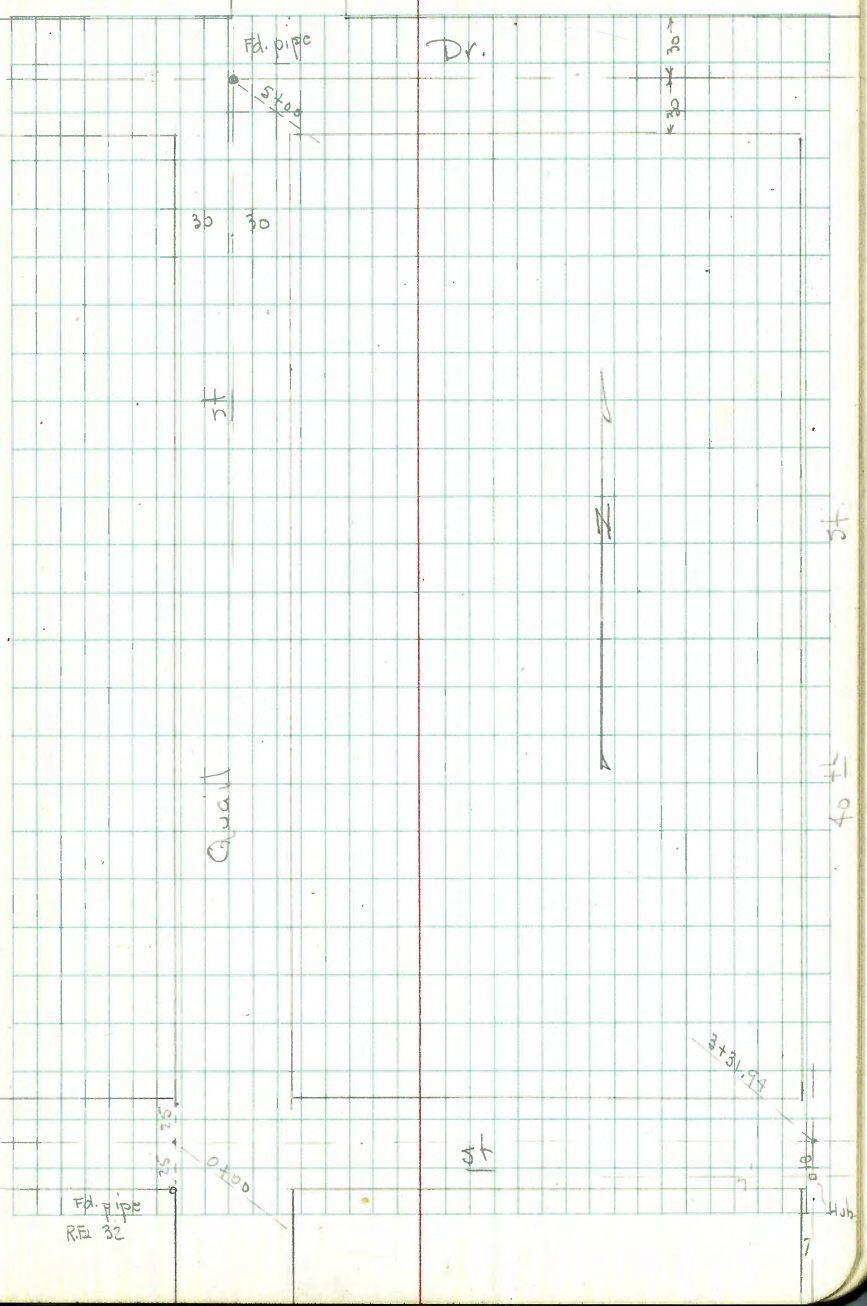
Hilltop

No points Fd. Here used & Quail for Orig. of Sta.

5f

5f

F



Fd. pipe

Dr.

30 30

5f

Quail

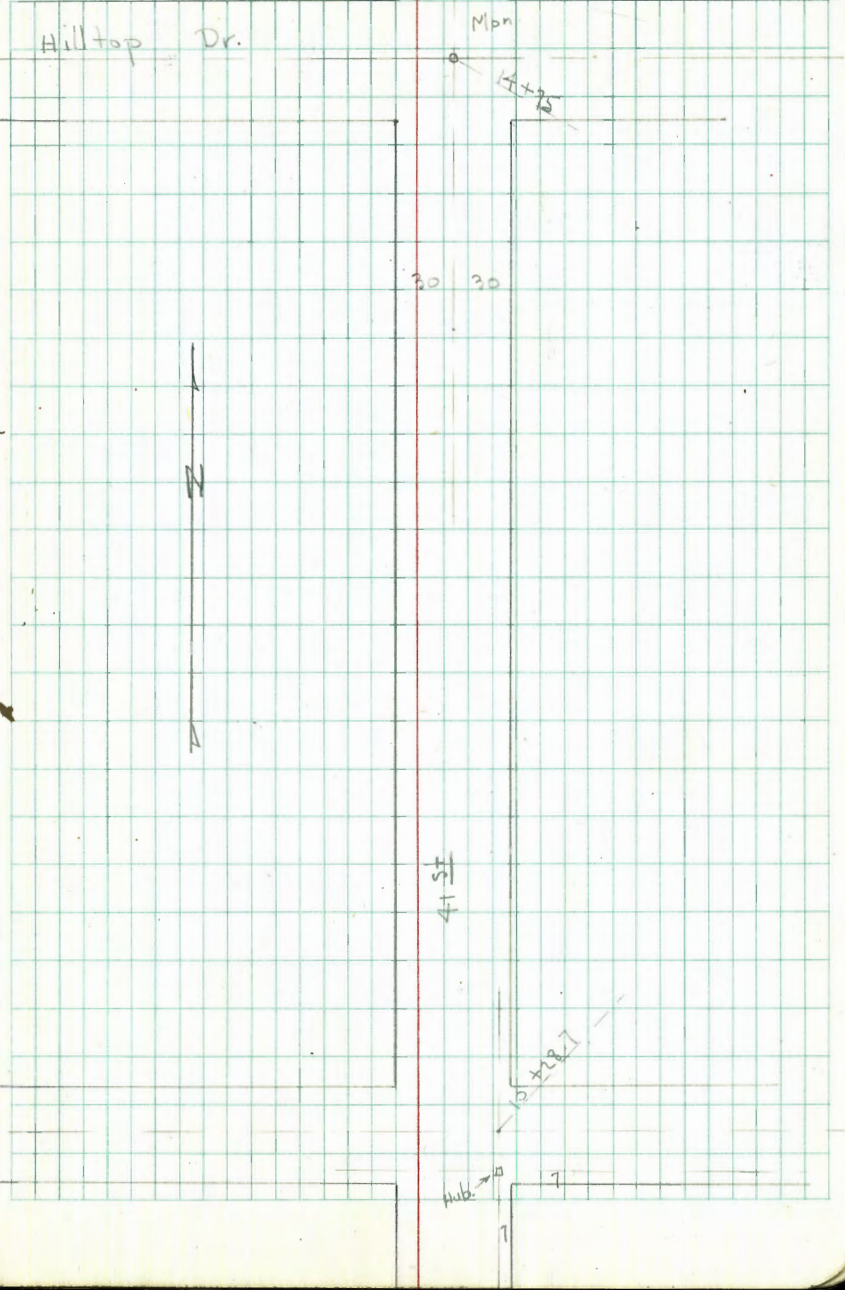
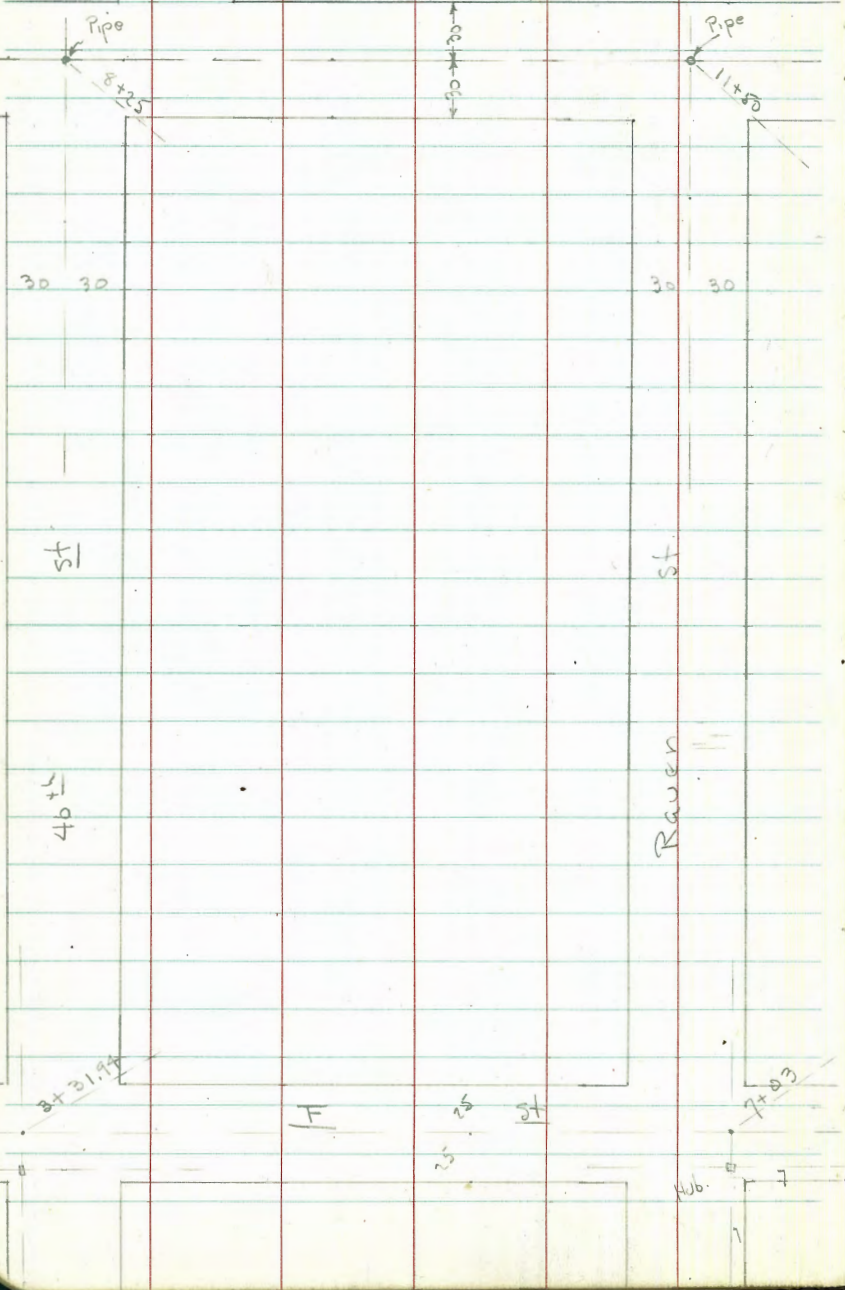
Fd. pipe
RE 32

5f

40f

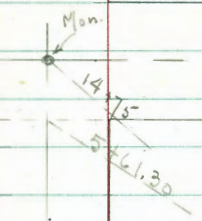
5f

Hub



Hilltop

Dr.



30 30

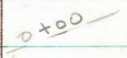
of.

st

st

41 st

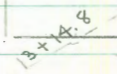
Morrison



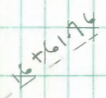
H



Hub



st



16 + 68.76 wherry-

dd Hub.

21 + 38

of.

st

42nd



Levels on Drives and Walks - on
Hilltop - Boundary to 42nd

W.O. 25001

3-9-48

Osborne
Hardin
Worrell
Rorer

bank - to Houses High on bank - way back
12+45 - 20.6 Lt. = \$ 5.3 Conc Steps - in Cut in

T.P. 0.37 171.48 13.16 171.11

11+63 - 54.6 Lt. = \$ 8' Conc. Dr. - 2^{strips} Car way back

10+43 - 56' Lt. = \$ 8' Dr. - 2 Conc. Strips

9+22 - 20' Rt. = \$ 8' Conc. Dr. to Sing. Gar. Conc. Floor

9+10 - 29.2 Rt. = \$ 2.8 Conc walk

7+15 - 55.3 Lt. = \$ Stucco House - Conc Found

T.P. 13.14 184.27 9.10 171.13

3+00 - 45.9 Rt. = \$ Small House in low spot

0+53 - 28.8 Rt. = \$ 4.8' Conc. walk

0+47 - 28.5 Lt. = \$ 2.5 Conc. walk

\$ Quail - 5+00 - no ties found w. of there.

B.M. 9.10 180.23 171.13 \$ Pipe Quail + Hilltop

171.07

5.41
35.5
Top of
step

178.75
5.52
5.6
Top Dr.

181.87
2.70
55.3
floor

177.05
3.18
28.5
Top walk

169.21

2.27
30.6
Bottom Step

172.18
6.09
54.6

179.3
5.0
55.3
ground

171.48

184.27

160.98
19.3
45.9
ground

175.78
4.45
28.8
Top walk

180.23

RT 29

INDEXED

MAR 8 1948

180.56
3.71
2.0
Dr

181.17
3.10
29.2
walk

181.20
3.07
3.2
floor
Gar

162.43

17.80
45.9
floor
House

I.P.

9.86

154.82

Dail in Pote
S.W. 42nd
+ Hilltop

16+81- 30.1 Rt. - ± 3' Conc. walk

16+59- 30.1 Rt. - ± 15' Conc. Dr. to ^{Conc. floor} Doub. Gar.

15+77- 30.1 Rt. = ± 15' Conc. Dr. to ^{Conc. floor} Doub. Gar.

T.P.

5.92

164.68

12.72

158.76

14+17.5- 29.9 Lt. = ± 2.7' Conc. walk

158.03

13.45

46.1

walk at
Steps

156.78

14.70

29.9

walk

164.68

171.48

30

157.31
7.37
30.1
Dr.

157.50
7.18
30.1
walk

156.98
7.70
40.2
floor.

157.08
7.60
40.2
walk
at House

152.34
12.34
30.1
Dr.

152.15
12.53
40.1
floor
Gar.

Levels on Drives + Walks - on F St.

Boundary - to 42nd - Sketch P. 26

W.O. 25001

8+24 = 23.3 Rt = Fly Conc. Dr. Conc. floor

8+08 = 23.2 Rt = Wly. Conc. Dr. to Doub Gar.

8+06 = 25.3 Rt = end Conc. wall

footing near ground surface

7+67 = 25.3 Rt = Req. 6 Conc. base for fence

T.P. 2.07 147.57 13.02 145.50

6+12 = 32.7 Lt = House - Conc. found.

6+12 = 33' Rt = Stucco House - Conc. found.

5+47 = 25.2 Lt = 4' Conc. walk

5+41 = 40.4 Rt = Sing Gar. - Conc. floor

5+36 = 30.7 Lt = Sing. Gar. - Conc. floor

4+97 = 38' Lt = Doub. Gar. - Conc. floor - under Const.

0+00 = W.L. Quail - No walks or Drives

w. of 40th

B.M. 8.85 158.52

149.67

sw. Nail in
Pole 40th
+ F

Lt = N.

Rt = S 31

INDEXED

143.96

3.61

23.3

Dr.

144.3

3.3

25.3

ground.

144.96

2.61

25.3

Top

144.07

3.50

23.2

Dr.

146.7

0.9

25.3

ground.

147.17

0.40

25.3

Top

144.30

2.27

27.5

floor

147.57

141.42

+2.90

32.7

floor

159.7

+1.2

32.7

ground

153.0

0.5

33

ground

159.72

+1.20

33

floor

156.82

170

29

Top

steps

157.52

2.96

25.2

Walk

154.35

2.17

30.7

floor

157.12

1.40

38

floor.

153.56

4.96

40.4

floor

158.52

14+55 - 15.1 Lt. = Φ 10' Conc. Dr. - (was to Gar.)

14+48.5 - 25.5 Lt. = Beg. 4" Rock + Conc. wall

14+16 - 15.8 Rt. = Φ 11.5' Conc. Dr. ^{Conc. floor.} to Doub. Gar.

14+15.5 25.7 Lt. = Φ 4' Conc. walk

14+07.5 25.1 Rt. = end wall

13+79 - 25 Rt. = Φ 2.5' Conc. walk thru wall

13+71 - 25' Rt. = Beg. 6" Conc. Block wall

T.P. 10.31 143.04 2.57 132.73

11+16.5 - 24.9 Lt. = Φ 15' Conc. Dr. to Doub. Gar. ^{Conc. floor.}

11+16.5 - 25.1 Rt. = Φ 15' Conc. Dr. to Doub. Gar. ^{Conc. floor}

10+96.5 - 25 Rt. = Φ 3' Conc. walk

check B.M. = ^{SE pipe - 41st} 1608-P.33 2.47 131.83 131.82

T.P. 0.73 135.30 13.00 134.57 = Nail in ^{115' pile}

8+90 - 26.7 Rt. = Φ Small House - Conc. found.

136.49	135.20	134.43		
7.84	7.84	8.61		
25.7	25.7	15.1		
at wall	at wall	Dr.		
6.57	8.0			
25.5	25.5			
Top	ground.			
134.44	134.0	134.15	133.21	
8.30	9.0	8.89	9.83	
25.7	25.7	15.8	39.4	
Top	ground.	Dr.	Floor	152.9
walk				131.48
		132.42	10.1	5.56
		10.62	25.1	Top
		25	ground	walk
		walk		
			132.8	151.42
			10.6	5.62
			25	Top
			ground.	walk
131.31	130.84	143.04		
3.99	4.48			
34.9	24.9			
floor	Dr.			
		129.83	129.78	
		5.47	5.52	
		25.1	35.3	
		Dr.	floor	
			130.26	130.26
			4.82	5.02
			25	34.2
			walk	walk
				at steps
		135.30		
			138.0	138.23
			9.6	9.34
			26.7	26.7
			ground	floor.
		147.57		

end.

16+63.5 - 25.6 Lt. = Ely 10' Conc. Dr.

Sing. Gar. - way back
16+53.5 - 25.6' Lt. = end walk at Conc. Dr. to

to House
16+32 = 25.4 Lt. = wly of 3' Conc. along steps

15+58 - 25' Lt. = end Wall

15+00 - 24.6 Lt. = Brk. in wall

14+58 - 35' Rt. = Gar. under Const.

Lt.

Rt.

Rt.

33

143.09	142.02		
+0.05	1.00		
40.6	25.6		
on Dr.	Cor. Dr.		
143.03	142.03		
+0.04	1.01		
40.6	25.6		
on Dr.			
142.11	142.11		
0.93	0.93		
28.5	25.4		
walk at	Cor. walk		
Steps			
146.73	138.3		
2.81	24.7		
25	25		
Top	ground		
end wall	136.1		
131.63	6.9		
5.41	24.6		
Top	ground		
wall			
		133.7	134.02
		9.8	9.02
		35	35
			Top
			Conc. found
		143.04	

2+50

2+12.5 - 30.3 Lt. = end fence

2+06 - 30.1 Rt. = \$ 7.5 Conc Dr. - Doub Gar. ^{back way}
11.84 148.14 2.28 136.30

2+00

1+57 - 30.1 Rt. = \$ 7.5 Conc Dr. - Doub Gar. - back

1+50

1+05 - 30.1 Rt. = \$ 7.5 Conc Walk - to Doub Gar. ^{way back}

1+00

0+78 - 29.9 Lt. = \$ 4 Conc. walk

0+61 - 30 Lt. = Reg. Picket fence

0+50

0+29 - 29.8 Rt. = \$ 3 Conc. walk

131.0	131.3	131.4	131.7	132.3	132.7	132.6	132.3 Rt	132.9	35	132.9
11.1	10.8	10.7	10.4	9.8	9.9	9.5	9.8	9.2	9.2	9.2
100	40	30	20	5		10	20	30	40	
Low Point										
								137.17		137.36
								10.97		10.78
						148.14		30.1		50
								Dr.		Dr.
	135.3	135.9	136.1	136.1	136.7	137.2	137.7			
	2.3	2.7	2.5	2.5	2.4	1.4	1.4			
	40	30	20		20	30	40			
								135.55		135.55
	134.4	134.5	134.8	134.6	134.7	135.4	135.5	30.3		29.3
								Dr.		Dr.
	4.2	4.1	3.8	4.0	3.9	3.2	3.1			
	40	30	20		20	30	40			
								134.15		134.13
								4.43		4.45
								Dr.		Dr.
	133.7	133.7	133.7	133.7	133.6	134.0				
	4.9	4.9	4.9	4.9	5.0	4.6	4.6			
	40	30	20		20	30	40			
132.10	133.75									
44.8	4.83									
48.6	2.99									
at walk	132.3	132.8	132.5	132.3	132.7	133.0	132.1	132.1		
Porch	4.3	4.8	5.1	5.3	5.9	5.6	5.5	5.5		
	40	30	20		20	24	30	40		
								132.90		132.14
								5.48		5.44
								2.98		4.9
								walk		at Porch

138.58

4+75

4+56 - 30.1 Rt. = E 7.5' Conc. Dr. - Doub. Gar - back

4+50 - 29.6 Lt - fence

4+06 - 30.1 Rt. = E 7.5' Conc. Dr. - Doub. Gar. - back

4+00

3+56 - 30.1 Rt. = E 7.5' Conc. Dr. - Doub. Gar. - back

3+50

3+36 - 30' Lt. = Beg. Wire fence

3+06 - 30' Rt. = E 7.5' Conc. Dr. - Doub. Gar. - back

3+00

2+57 - 30.2 Rt. = E 7.5' Conc. Dr. - to Doub. Gar. - back

145.7	144.8	144.7	144.5	144.6	144.5	144.7	145.6	146.7	36
2.4	3.3	3.4	3.6	3.5	3.6	3.4	2.5	1.6	1.4
4.8	3.0	2.0	1.0	1.0	2.0	2.0	3.0	3.2	4.0
144.1	143.7	143.8	143.8	143.8	143.7	143.8	144.9	145.10	145.26
4.0	4.4	4.3	4.3	4.3	4.4	4.3	3.2	3.0	2.86
4.0	3.0	2.0	1.0	1.0	2.0	2.0	3.0	4.0	5.0
142.7	142.0	142.0	142.0	142.3	142.4	142.4	143.4	143.3	143.34
5.4	6.1	6.1	6.1	5.8	5.7	5.7	5.7	4.9	4.8
10.0	4.0	3.0	2.0	1.0	1.0	2.0	3.0	4.0	4.0
140.0	140.3	140.7	140.9	141.1	141.3	141.1	142.0	142.1	142.34
8.1	7.8	7.4	7.2	7.0	6.8	7.0	6.1	6.0	4.51
4.0	3.0	2.0	1.0	1.0	2.0	3.0	4.0	4.0	5.0
138.6	139.9	139.4	139.4	139.9	139.9	140.4	139.9	140.6	140.5
9.5	9.2	8.7	8.7	8.2	8.2	7.9	8.2	7.5	7.6
4.0	3.0	2.0	1.2	1.4	1.0	2.0	2.0	3.0	4.0
137.0	137.0	137.0	137.0	137.0	137.0	137.0	137.0	137.0	137.0
9.12	8.96	8.96	8.96	8.96	8.96	8.96	8.96	8.96	8.96
3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0
Dr.	Dr.	Dr.	Dr.	Dr.	Dr.	Dr.	Dr.	Dr.	Dr.

148.14

Rt. on walk opp Sta 5+41-

Set B.M. on 70' R.P. Disk 10.03 150.36

Check B.M. Top of Mon. 751 152.88 -152.94

Top has been scraped since last Read.

85' N. = 25' N. of N.L. for Profile

60' N. = N.L. Hilltop

50' N. = N. cb.

42' N.

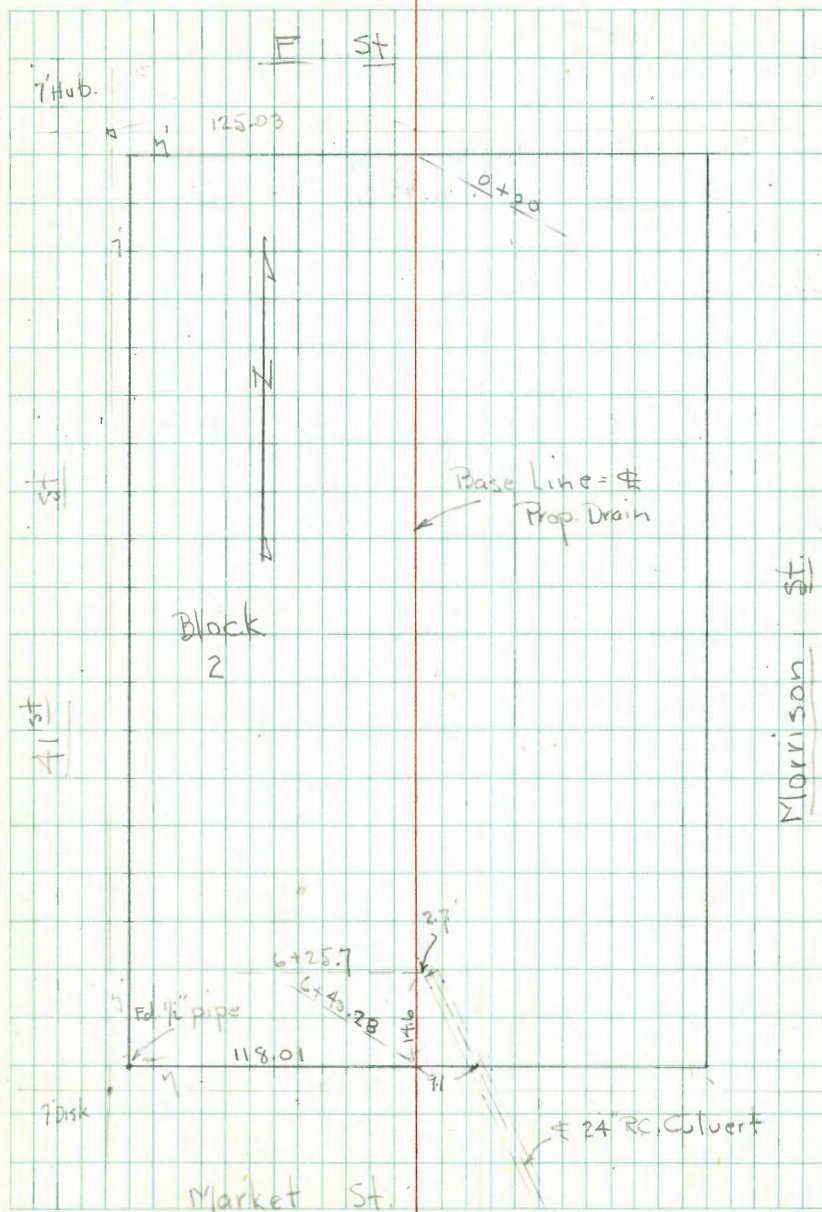
158.8	158.7	158.5	158.3	158.5	158.4	159.0	158.9	158.4
1.6	1.7	1.9	2.1	1.9	2.0	1.4	1.5	2.0
40	30	20	10		10	20	30	40
156.6	156.7	156.2	155.7	155.8	155.6	156.7	154.5	155.1
3.8	3.7	4.2	4.7	4.6	4.8	3.7	3.9	4.5
50	30	20	10		10	15	20	30
155.8	155.7	155.2	154.8	154.6	154.4	155.2	154.7	154.2
4.6	4.7	5.2	5.6	5.8	6.0	5.2	5.7	6.2
50	30	20	10		10	20	30	50
154.4	154.0	153.9	153.9	154.0	153.8	153.8	153.6	153.6
6.0	6.4	4.5	6.5	6.4	6.6	6.6	6.8	6.8
50	20	20	10		10	20	20	50

160.39

Profile levels Thru Middle of Block 2

W.O. 31342 - 4-6-48 - 7.0

INDEXED



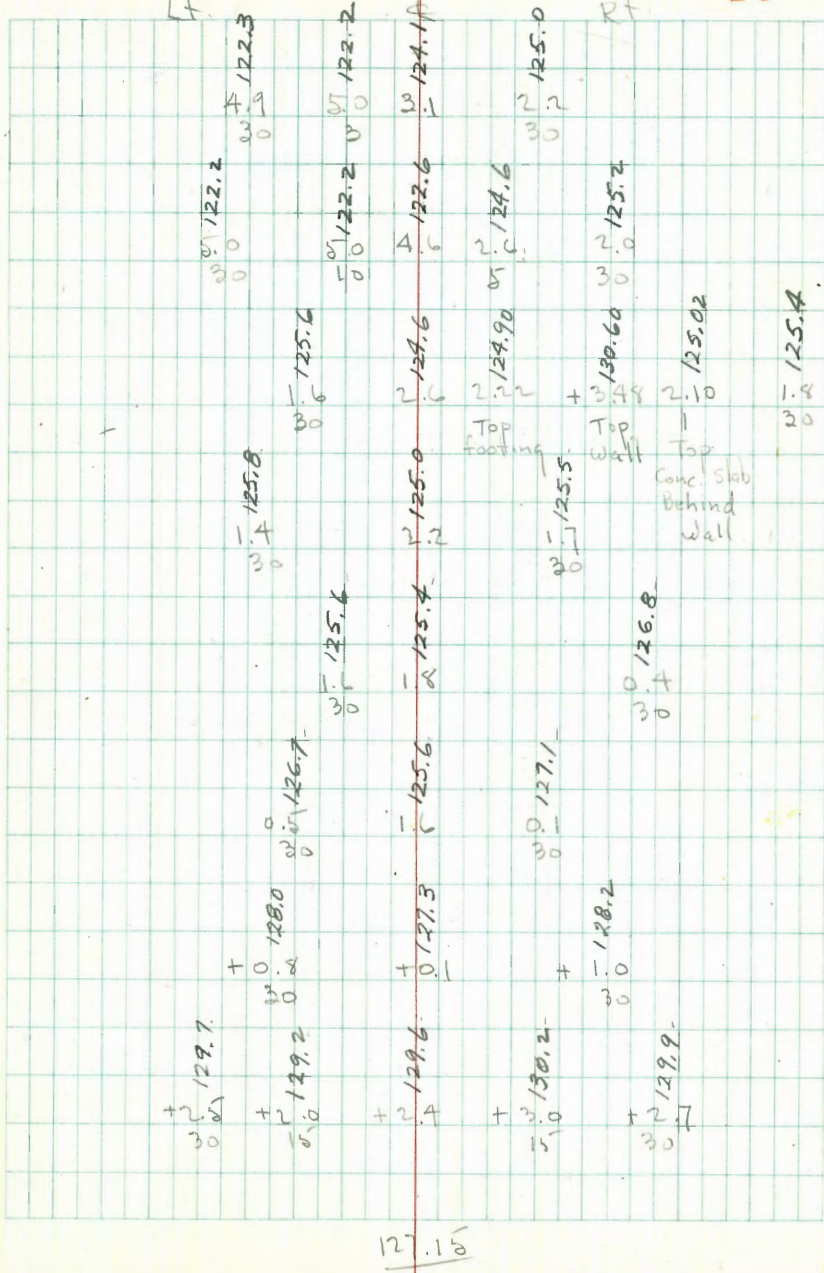
Levels - for Profile thru E of Blk. 2.

INDEXED

3+50
 3+15.5 - 1.7 Lt. = Beg. Wire fence
 3+14 - 0.6 Rt. = Ely. P. pole
 3+00
 2+6 C = end of Conc. Wall
 2+59.1 - 0.3 Rt. = Sewer M.H. in arch in Conc. Wall
 2+50
 2+13.5 - = End Wire fence + Beg. 6' High Conc. Wall
 2+09 - 0.6 Rt. = Ely. P. pole
 2+00

1+50
 1+09 - 4 Rt. = Ely. P. Pole
 1+10 - 0.2 Rt. = end Picket + Beg. Wire Fence
 1+00
 0+60 - 12 Rt. = Beg. Picket fence
 0+50
 0+00 = S.L. F St.

1.76 127.15 125.39 NW. 4th + Market.



127.15

6+40 2.8 = N.L. Market = end.

See sketch for Line of Pipe

6+28.7 - 2.7' Lt. = \pm inlet of 24" R.C. Pipe

5+90

5+60

5+43.5 = \pm Sewer M.H.

6.44

on Rim

5+40.4 = end fence

5+40

5+39 - 12' Rt. = Ely. P. pole

5+08.5 - 0.4' Rt. = Ely. P. pole

5+00

4+65.5 - Beg. wire fence on line

4+50

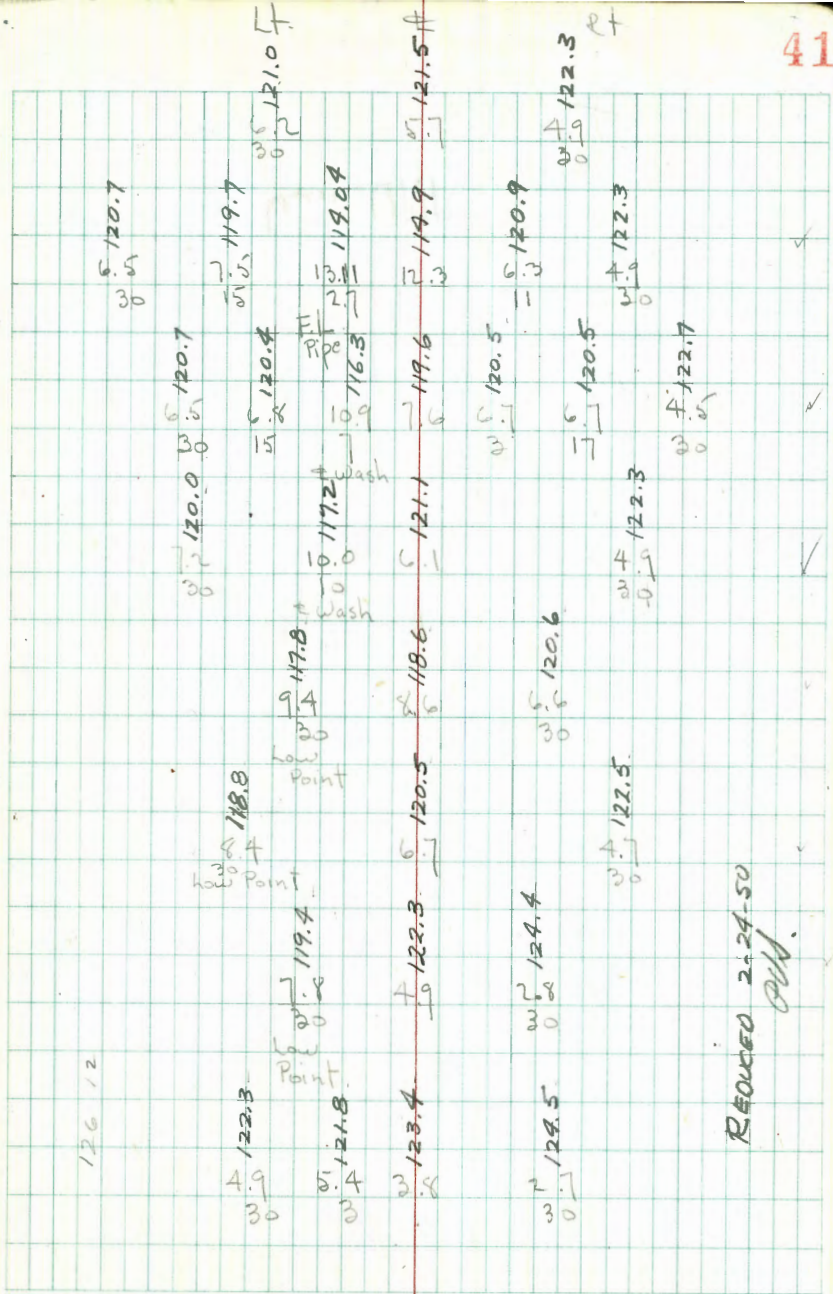
4+17.5 - 0.5 Rt. = Ely. P. pole

+ 3' Rt. =

4+15.5 - 1.8' Lt. = end wire fence

4+00

3+65 - 1.6' Rt. = Beg. wire fence



127.15

9-8-48

Levels Cbs. & Gutters

Hendricks

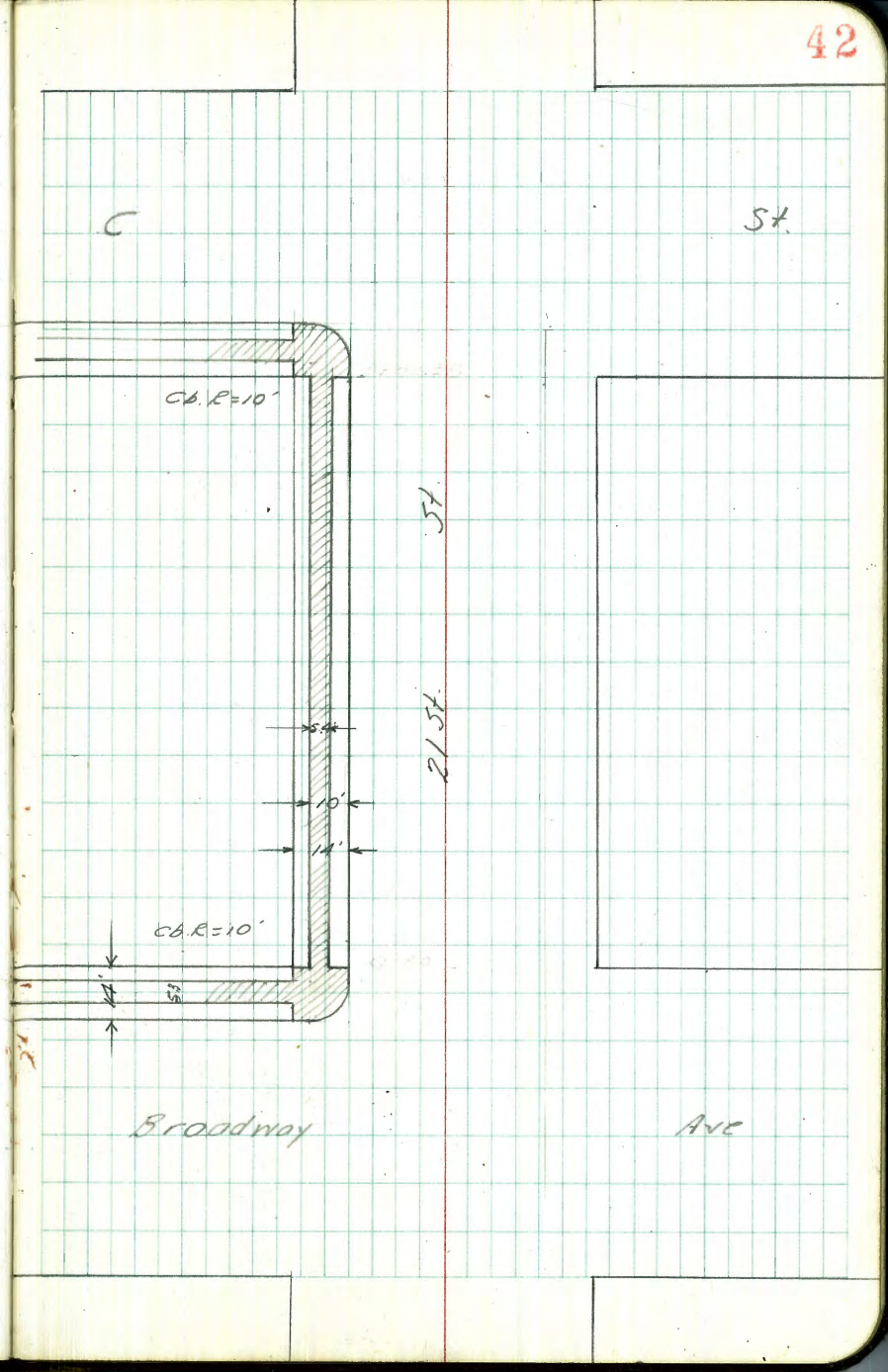
West Side 21st St.

Roberts

Broadway to C

Rorer.

INDEXED



O+OD Ho Line Broadway

EC 10' Radius on 21st St

②

①

BC 10' Radius on Broadway

West Line 21st St on Ho. Ch. Broadway

BM 6.46 121.33

114.87

608	615	624	625	627
14	10	45	6	66
J-W	2W	J-W		

621	620
6	66

629	624
6	66

628	625
6	66

625	626
6	66

626	631
6	66

SWBP Broadway & 21st St

3+00.38 Jo. Line E. 5L

2+50

2+00

1+50

1+00

0+50

12133
T

831 841 851 862 855
10 10 46 G CB
SW SW SW

781 791 854 800
10 46 G CB
SW SW

743 745 816 769
10 46 G CB
SW SW

714 720 785 734
10 46 G CB
SW SW

670 686 741 704
10 46 G CB
SW SW

636 655 720 673
10 46 G CB
SW SW

B17. 8.19 113.14 113.01

West Line 21st St. on So. Co. E St.

EG 10' Radius on E St.

②

①

BC 10' Radius on 21st St.

121.33

NW BP E St. & 21st

921 842
G CB

924 842
G CB

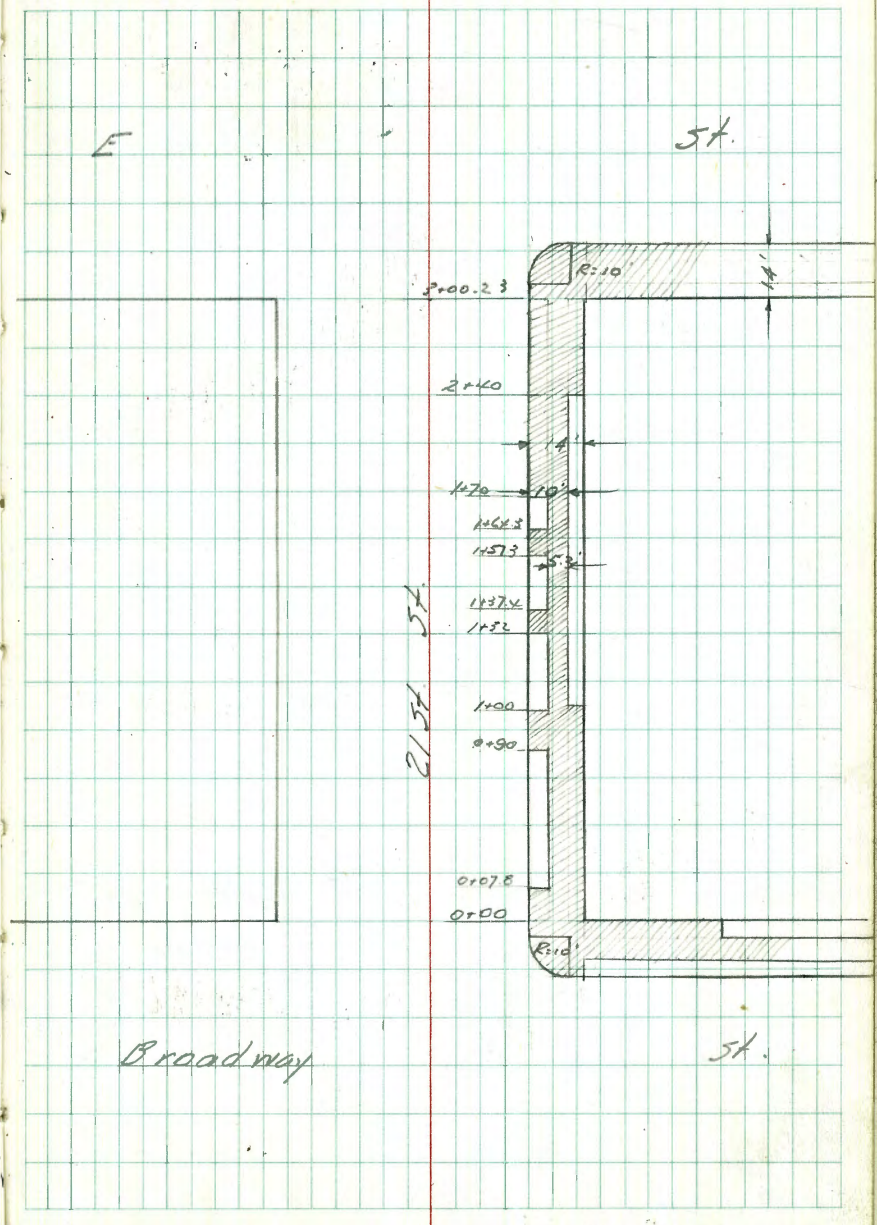
902 846
G CB

899 844
G CB

900 846
G CB

9-8-48 Levels Curb, Gutter & Sidewalk
Hendricks on 21st Broadway to E
Roberts
Rorer
No. 25001

INDEXED
W.R.
SEP 10 1948



0100 So. Line Broadway

EC 10' Radius on 21st

②

①

BC 10' Radius on Broadway

West Line 21st St. on So. Curb Broadway

BM 6.56 121.43

114.87

6.15	175.27
14	10
SW	SW
6.18	175.18
14	10
SW	SW
6.18	113.05
14	10
SW	SW

6.18	114.93
14	10
SW	SW
6.18	114.40
14	10
SW	SW

6.18	115.03
14	10
SW	SW
6.18	114.35
14	10
SW	SW

6.18	115.06
14	10
SW	SW
6.18	114.41
14	10
SW	SW

6.18	114.97
14	10
SW	SW
6.18	114.24
14	10
SW	SW

6.21	115.02
14	10
SW	SW
6.21	114.16
14	10
SW	SW
6.21	114.10
14	10
SW	SW

SWBP Broadway @ 21st

BM 6.93 114.50 114.45

West Line 21st St. on No. Ch. E St.

EC 10' Radius on E St.

②

①

BC 10' Radius on 21st St.

121.43

NW 1/4 21st & E

6	121.10.61	6	114.58	6	113.66
27	6	27	6	27	6
27	114.54	27	113.84	27	113.66
27	114.57	27	113.99	27	113.66
27	114.57	27	114.03	27	114.03
27	114.54	27	114.03	27	114.03

Proposed drain thru
Lots 16-17 Blk 2 Univ. Place
W.O. 60348

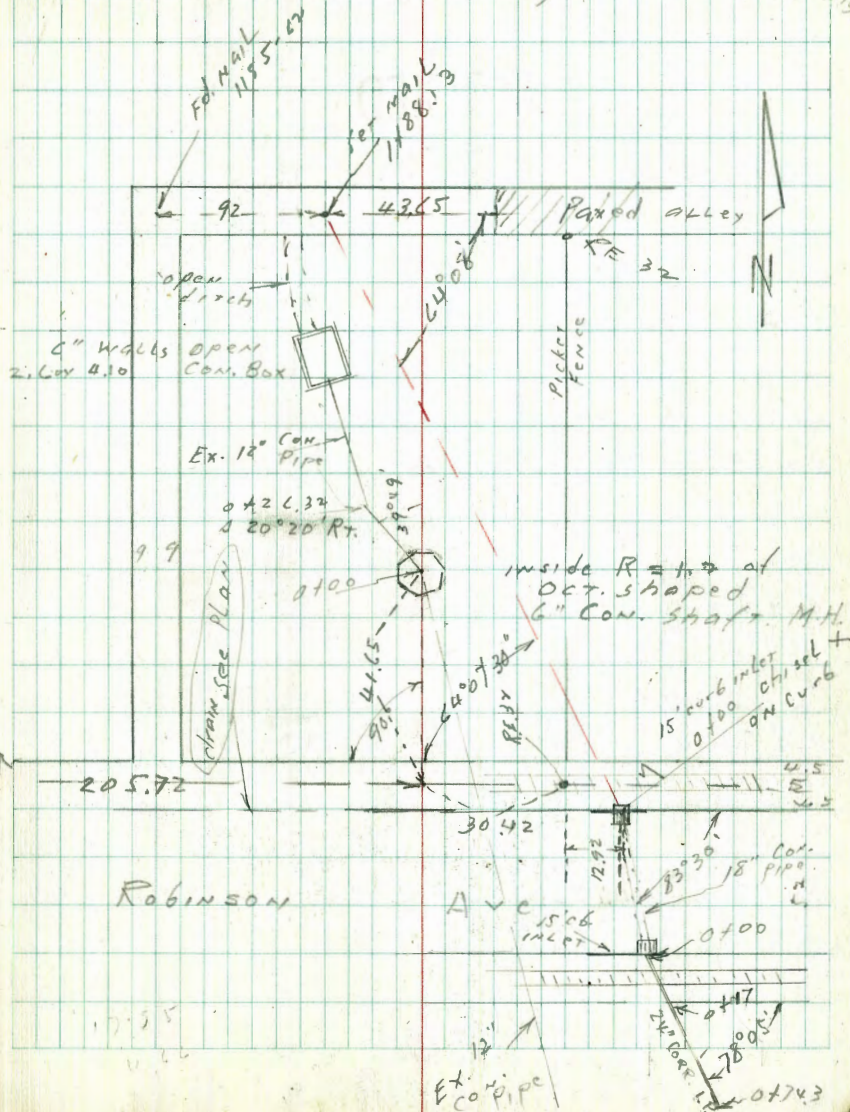
Levels on Ex. 12" drain			
B.M.	1.90 (295.95)		294.05 Robinson and Richmond
SW BP			
0+00	ground	7.3	288.6
"	Top Ex. MH	7.11	288.84
"	FL. 12" IN "	11.77	284.18
"	" " out "	24.96	270.99
0+26.32	20'x20' Rt ground	8.0	287.9
"	Top 12" pipe	10.3	285.6
0+63.40	Top Con. Box	8.60	287.35
"	FL. 12"	10.83	285.12

INDEXED
WK
FEB 24 1949

RICHMOND
Mid. Lt. Rd.

Sketch, Locally F.B. 1155-62 51.

Moore
B.P. 9.5
Shant.
Bunch
2-23-49
Use Red Line for drain.
12" line has been choked up
with debris during flood periods
according to local residents.



NOTE: NO CONNECTION WITH 12" DRAIN

Proposed drain:

BLK - UNIV. PL.

14773 - NE Cor Dwelling

INDEXED

1450

1412 SxI Cor shed

0493

0486

0450

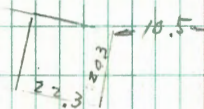
D400 CROSS & Box.
N.C.B. ROBINSON

295.95

Lt

Rt

52



$$\begin{array}{r} 286.9 \\ 9.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 287.1 \\ 8.8 \\ \hline \end{array}$$

$$\begin{array}{r} 287.7 \\ 8.0 \\ \hline 10 \end{array}$$


$$\begin{array}{r} 287.6 \\ 8.3 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 287.5 \\ 8.4 \\ \hline \end{array}$$

$$\begin{array}{r} 289.6 \\ 6.3 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 288.7 \\ 7.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 289.3 \\ 6.6 \\ \hline \end{array}$$

$$\begin{array}{r} 290.2 \\ 5.7 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 290.1 \\ 5.8 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 290.4 \\ 5.5 \\ \hline \end{array}$$

$$\begin{array}{r} 291.2 \\ 4.7 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 289.95 \\ 6.00 \\ \hline \text{CURB} \\ \text{TOP} \end{array}$$

$$\begin{array}{r} 288.95 \\ 7.00 \\ \hline \text{95470} \end{array}$$

$$\begin{array}{r} 286.89 \\ 15.06 \\ \hline \text{807} \\ \text{150X} \end{array}$$

295.95

24" Conn. IP drain on
S side Robinson

Check to	Orig B.M.	343	294.05	294.05
T.P.	523	297.48	341	292.25
T.P.	792	295.66	047	287.74
T.P.	1253	288.21	038	275.68

0+743 Inv. outlet 24"

T.P.	015	276.04	1164	275.41
T.P.	045	287.05	935	286.60

0+117

5 curb
0+100 ROBINSON

1+8813 Alley

178

295.95

8

53

261.66
14.40
Inv. outlet

275.06

288.9
70

278.17	287.99	288.91
17.76	7.95	7.04
Box Box	9.97	26

295.95

287.0
8.9

287.5
8.4

295.95

3/8/49

X-Section Intersection
Eads and Trushville

(no. 60356)

McCoy
Allen
Jones

LH.

E

RT.

54

0+14 Continued

INDEXED
W.K.
MAR 9 1949

0+14 East Curb Line on Eads

0+11 Mid Points 10' Rad. Returns

0+04 10' Radius Ch. B.C.s on Trushville

0+00 East P.L. of Eads

0-50

0-1+00

Notes Reduced 4-11-49
for W.D.NEBP
Eads +
Trushville

5.07

136.52

131.50

sketch pg. 57

129.90 $\frac{6.62}{80}$ C6	129.09 $\frac{7.23}{80}$ G	130.65 $\frac{5.87}{30}$ C6	130.17 $\frac{6.35}{30}$ G	131.06 $\frac{5.74}{28}$ G	131.49 $\frac{5.03}{28}$ C6	131.05 $\frac{5.47}{30}$ G	131.48 $\frac{5.07}{30}$ C6	131.43 $\frac{5.09}{80}$ G	131.86 $\frac{4.66}{80}$ C6
Patch									
130.80 $\frac{5.72}{25}$ C6	130.32 $\frac{6.20}{25}$ G	130.64 $\frac{5.88}{18}$ G	131.02 $\frac{5.50}{25}$ G	131.35 5.77	131.36 $\frac{5.16}{7.5}$ G	131.27 $\frac{5.25}{15}$ G	131.08 $\frac{5.44}{25}$ G	131.51 $\frac{5.01}{25}$ C6	
	131.01 $\frac{5.51}{18}$ C6	130.41 $\frac{5.81}{18}$ G			131.31 $\frac{5.21}{18}$ G		131.76 $\frac{4.76}{18}$ C6		
131.19 $\frac{5.33}{15}$ C6	130.82 $\frac{5.69}{15}$ G	131.34 $\frac{5.78}{25}$ G	131.62 4.90		131.69 $\frac{4.83}{25}$ G		131.64 $\frac{4.88}{15}$ G	132.01 $\frac{4.57}{15}$ G	
131.33 $\frac{5.19}{15}$ C6	130.91 $\frac{5.61}{15}$ G	131.41 $\frac{5.11}{25}$ G	131.71 4.81		131.77 $\frac{4.75}{25}$ G		131.75 $\frac{4.77}{15}$ G	132.17 $\frac{4.35}{15}$ C6	
133.60 $\frac{2.92}{15}$ C6	133.19 $\frac{3.33}{15}$ G	133.59 $\frac{2.93}{25}$ G	133.87 2.65		133.86 $\frac{2.66}{7.5}$ G		133.70 $\frac{2.82}{15}$ G	134.17 $\frac{2.35}{15}$ C6	
135.43 $\frac{0.59}{15}$ C6	135.47 $\frac{1.02}{15}$ G	135.72 $\frac{0.80}{25}$ G	135.84 0.68		135.87 $\frac{0.65}{25}$ G		135.73 $\frac{0.79}{15}$ G	136.18 $\frac{0.34}{15}$ C6	

MO.60356

Eads + Rushville

INDEXED

0+69 Midpoints of 10' Rad Cb. Returns

0+66 Continued

0+66 West Curb Line on Eads

0+53 West 1/4 of Eads

0+40 1/2 of Eads

0+27 East 1/4 on Eads

136.52

LT,

1/2

RT

55

129.80 6.72 18 5.8 Mid. Pt.	129.40 7.12 18 5 G	130.15 6.37 18 5 G	130.61 5.91 18 5.8 Mid. Pt.								
128.83 7.69 80 Ck G	128.47 8.05 80 G	130.29 6.23 30 G	130.67 5.85 30 Ck FC	130.75 5.77 80 G	131.00 5.52 80 Ck						
129.56 6.96 30 Ck	129.15 7.37 30 G	129.66 6.86 25 Ck FC	129.26 7.26 25 G	129.62 6.90 15	129.96 6.52 20	130.21 6.31	130.22 6.30 20	130.13 6.39 15	130.26 6.26 25 G	130.62 5.90 20 Ck FC	
129.02 7.50 80	129.82 6.70 30	129.84 6.68 25	130.03 6.99 15	130.31 6.21 25	130.49 6.03	130.56 5.96 25	130.49 6.03 15	130.74 5.78 25	130.87 5.65 30	131.36 5.16 80	
129.27 7.25 80	130.26 6.26 30	130.31 6.21 25	130.43 6.09 15	130.67 5.85 25	130.80 5.72	130.87 5.61 25	130.82 5.70 10	130.94 5.53 25	131.07 5.71 50	131.55 4.97 80	
129.34 7.18 80	130.30 6.14 30	130.45 6.07 25	130.61 5.91 15	130.86 5.66 20	131.06 5.76	131.09 5.73 25	131.03 5.79 15	130.96 5.52 21.5	131.11 5.71 25	131.13 5.39 30	131.54 4.98 80
							1/2 Patch				
								1/2 Patch			

INDEXED

1+80

1+30

0+80

West Prop Line of Eads

0+76

Curb B.C.s on Rushville (10' Rad)

136.52

Lt.

±

Rt.

56

$$\begin{array}{r} 125.53 \\ 10.99 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 125.21 \\ 11.31 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 125.64 \\ 10.86 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 126.03 \\ 10.49 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 126.11 \\ 10.71 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 126.02 \\ 10.50 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 126.50 \\ 10.02 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 127.58 \\ 8.74 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 127.20 \\ 7.32 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 127.61 \\ 8.91 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 127.97 \\ 8.55 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 128.09 \\ 8.73 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 128.03 \\ 8.49 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 128.50 \\ 8.02 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 129.55 \\ 6.77 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 129.15 \\ 7.37 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 129.59 \\ 6.93 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 129.91 \\ 6.61 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 129.95 \\ 6.57 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 129.83 \\ 6.69 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 130.39 \\ 6.13 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 129.69 \\ 6.83 \\ \hline 15 \\ \text{Ck} \end{array}$$

$$\begin{array}{r} 129.30 \\ 7.22 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 129.71 \\ 6.81 \\ \hline 15 \\ \text{G} \end{array}$$

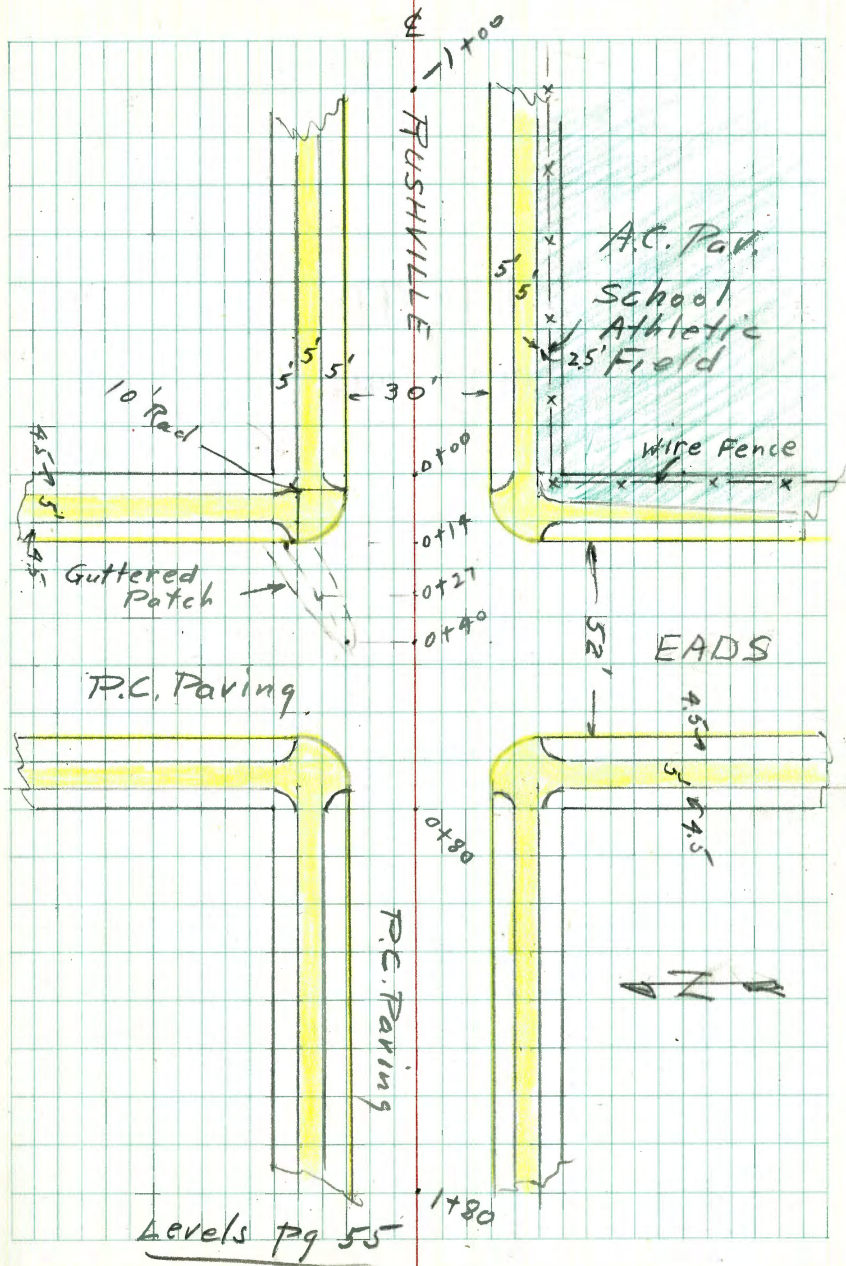
$$\begin{array}{r} 130.06 \\ 6.76 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 130.07 \\ 6.95 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 130.00 \\ 6.52 \\ \hline 15 \\ \text{G} \end{array}$$

$$\begin{array}{r} 130.52 \\ 6.00 \\ \hline 15 \\ \text{Ck} \end{array}$$

136.52



12-13-49
Roberts
Garber
Moore
Clark
W.O.#206d

Survey for Proposed Storm Drain
Midway St. from La Jolla Blvd to
Pacific Ocean

Maps 1565 & 1083

T.R. 1707 & 1708

SEE FD 2214

12

INDEXED
W.K.
DEC 14 1949

La

Jolla

Blvd. 58

Fd. Conc. \square 0+00
Mon. Disc.
City

Line

60'

Fd. Conc. \square 2+53.71
Mon. Disc.
City Disc.

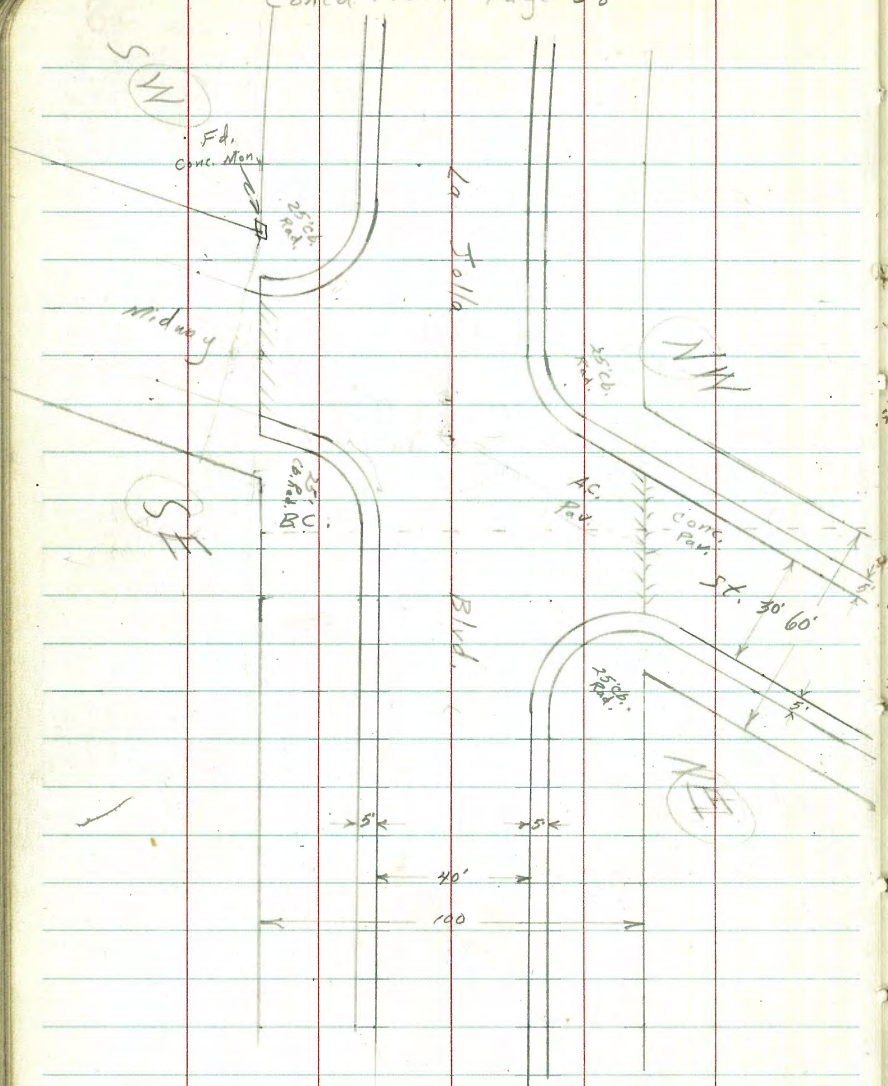
St.

Fd. 222 Hub \square 4+34.90
No tack

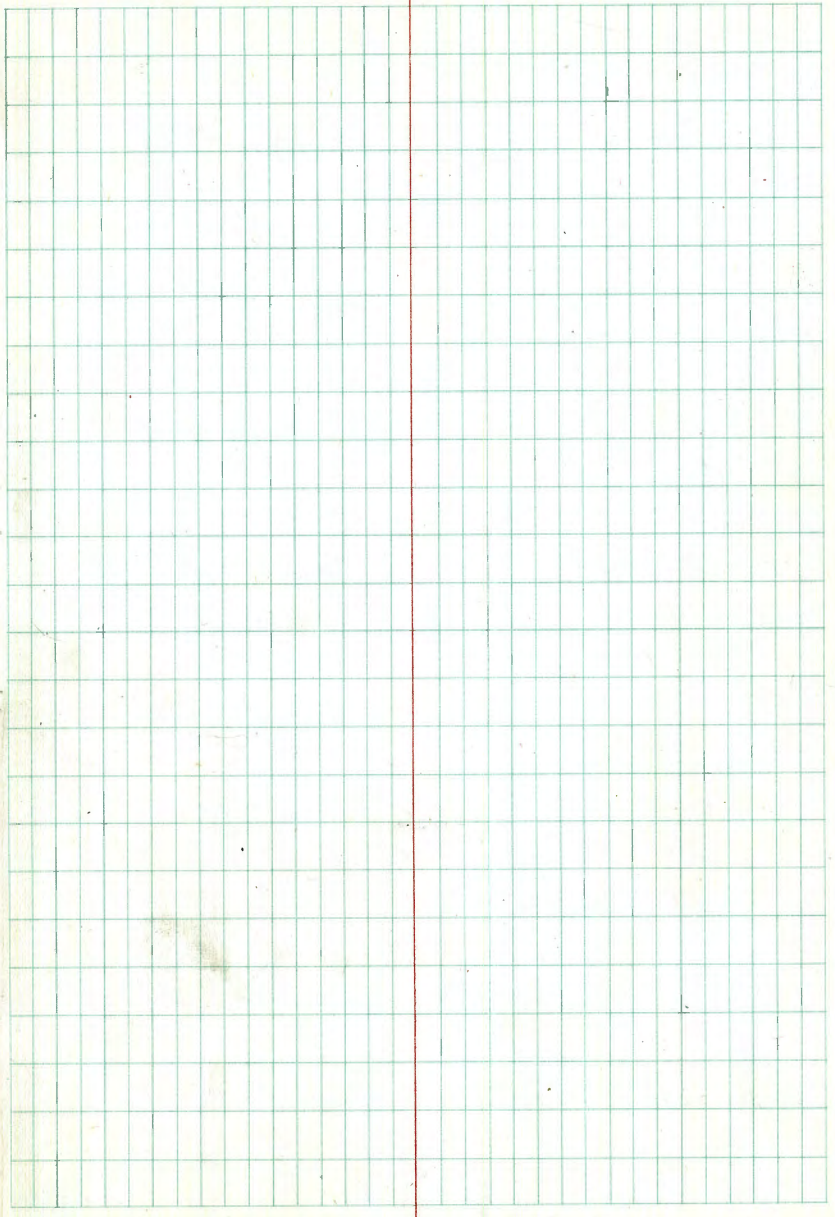
Base

Fd. 221 giff \square 4+76.32
No Nail

Midway



(Sketch Intersection)



CB. BC. SW. Cb. Ret. L.J. Blvd.

50' No. Cb. BC. W. Cb. Line L.J. Blvd. No. Mid. St.

100' No. Cb. BC. W. Cb. Line L.J. Blvd. No. Midway St.

100' No. E.C. Cb. Ret. E. Cb. Line L.J. Blvd. No. Mid. St.

50' No. E.C. Cb. Ret. E. Cb. Line La. J. Blvd. No. Midway

E.C. Cb. La. Jolla Blvd.

2nd. Part

1st. Part

Cb. BC. NW. Cb. Ret. Midway

50' E. Cb. BC. No. Cb. L. Mid. E. L.J. Blvd.

100' E. Cb. BC. No. Cb. Line Midway E. L.J. Blvd.

75' East Cb. EC. So. Cb. Line Mid. St.

EC. Cb. Ret. So. Cb. Line Midway St.

4th. Part

3rd. Part

2nd Part

1st. Part. NE. Cb. Ret. from L.J. Blvd.

Cb. BC. E. Cb. L.J. Blvd. So. Mid. St.

50' So. Cb. BC. East. Cb. L.J. Blvd. So. Mid. St.

100' So. Cb. BC. East. Cb. La Jolla Blvd. So. Midway St.

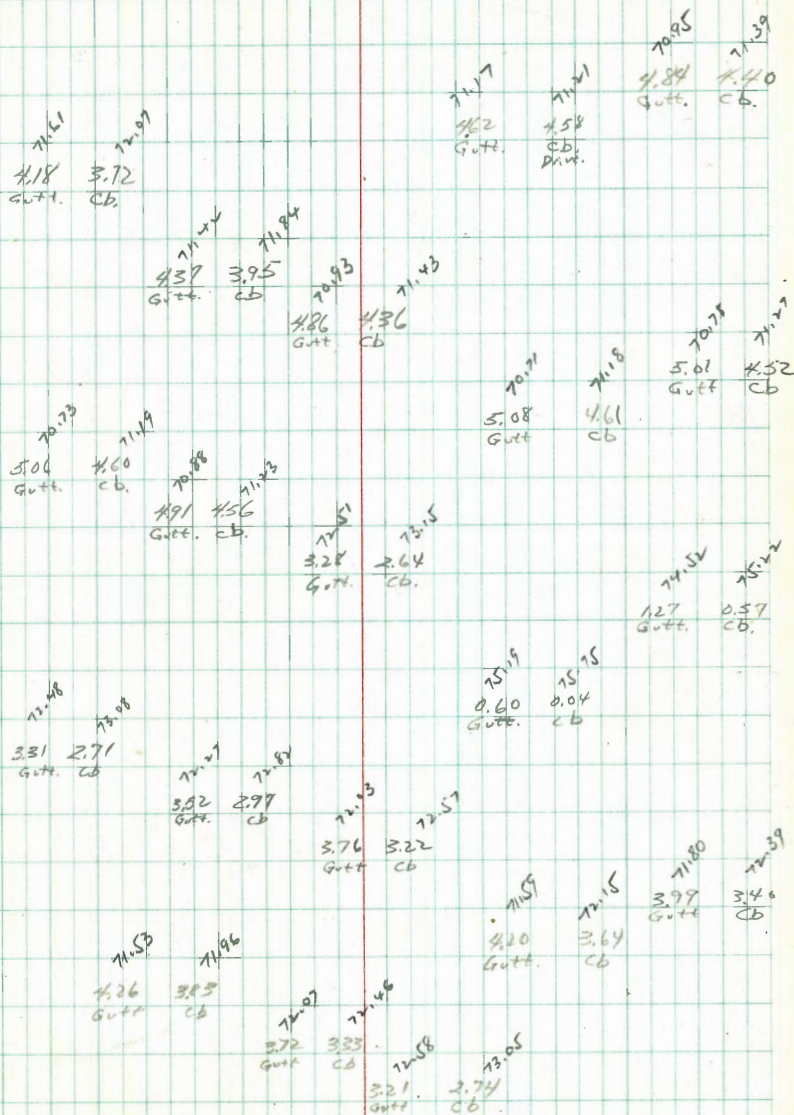
BM

3.73

75.79

76.86

NE. B.P. La Jolla & Midway (Walker's BM)



& Midway from East 100' East & L.J. Blvd.
 & Midway from East 50' East & L.J.
 & Midway from East. 16' East & L.J.

& L.J. 100' No. & Mid. from East
 & L.J. 50' No. & M.d. from East
 & L.J. & Mid. from East
 & L.J. 50' So & M.d. from East
 & LaJolla Blvd. 100' So & Midway (from East)

100' So. Cb. E.C. W. Cb. Line L.J. Blvd. So. Midway
 50' So. Cb. E.C. W. Cb. Line L.J. Blvd. So. M.d. St.
 E.C. Cb. LaJolla S.E. Ret.

2nd. Part

1st. Part

BC. Cb. Mid. St. S.E. Ret.

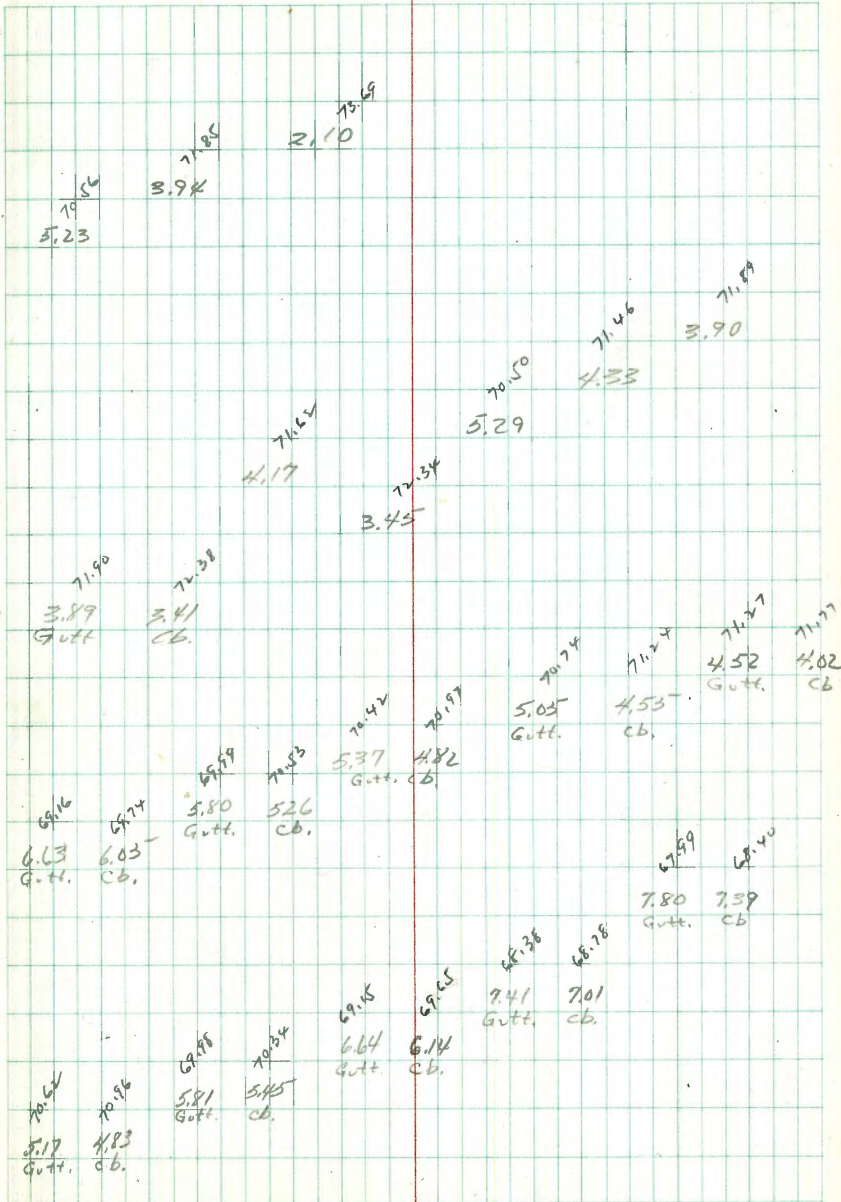
End. Cb. on Midway ^{So.} 14' So. BC. Cb. S.E. Ret.

End. Cb. on Midway. SW. Ret.

3rd. Part

2nd. Part

1st. Part



T.P. 0.86 55.06 10.46 54.20 Cont. Mon 2753.71

2400

1450

1400

T.P. 0.48 64.66 11.61 64.18

0450

0400 Prop. Cor. S.W. Cor. Intersection
Midway St. & 24th St. Blvd.

↳ Mid. from East, 56' West & L.S. Blvd. End. Pav.
↳ Mid. from East 39' West & L.S. Blvd
↳ Midway from East 23' West & L.I. Blvd.

(Gutter follows & Mid. from East to End)
Paving on West.

25.79

54.8
9.9
50

54.2
10.2
25

54.5
9.2

57.0
7.7
25

57.4
7.3
50

56.9
5.8
25

57.2
5.5

60.5
7.2
25

60.5
7.2
50

61.4
3.3
25

61.5
3.2

61.9
2.8
25

64.66

64.1
10.7
50

62.8
13.0
25

64.7
11.1

65.2
10.2
25

61.0
8.8
50

61.0
7.8
25

66.5
7.3

70.1
5.7
25

69.99
5.82

69.25
6.54

67.95
7.84

25.79

5+00

4+90

4+50

TP 0.19 42.26 12.99 4207 WINDS STATE 4734.90

4+00

3+50

3+00

2+70

2+50 Old Ditch filled in to here
Ave. of fill shown

55.06

Lt.		Rt.	
4.2	7.5	14.9	9.1
35	24	21	19
3.3	3.2	3.2	3.0
3.0	3.6	3.0	2.6
1.8	1.6	1.6	1.4
5.0	4.2	3.5	2.9
12.7	20.6	11.8	11.7
4.6	3.8	3.1	2.5
7.4	15.8	9.0	9.2
5.4	4.9	3.9	2.5
6.4	10.6	10.5	6.3
5.1	5.0	4.1	4.0
5.8	9.7	10.8	5.4
3.1	5.0	4.6	3.7
3.2	2.8	1.4	1.8
5.0	2.5		2.5

55.06 ✓

Check			4.83	72.07 = 72.06
T.P.	10.26	76.90	0.83	66.64
T.P.	13.26	67.47	0.45	54.21
T.P.	12.59	54.66	0.19	42.07

Starting BM

5792 Bottom of Cliff Cobble Stone Beach

0.44
41.5

5787

	29.3	27.8	27.8	24.5	21.5	28.3	29.3
	13.0	14.5	14.5	17.8	26.8	14.0	13.0
	29.5	23	13	3		11	25

5749

	27.4	26.4	26.4	24.7	20.5	29.0	21.0	26.6	26.2
	14.9	5.9	6.1	7.6	11.6	12.1	21.8	13.3	5.7
	55	41	36	21	15	6	3	20	25

5712

	37.5	34.5	34.8	37.9	31.6	31.8	34.3	32.9	25.4	32.4	34.9	34.6	36.7	38.9
	4.8	7.8	7.5	11.4	4.7	4.5	8.0	9.4	15.9	8.9	7.4	7.8	3.6	3.4
	60	55	50	46	37	29	24	16	12	8	14	20	25	

42.26
1

42.26
1

Notes Reduced 1.12-50

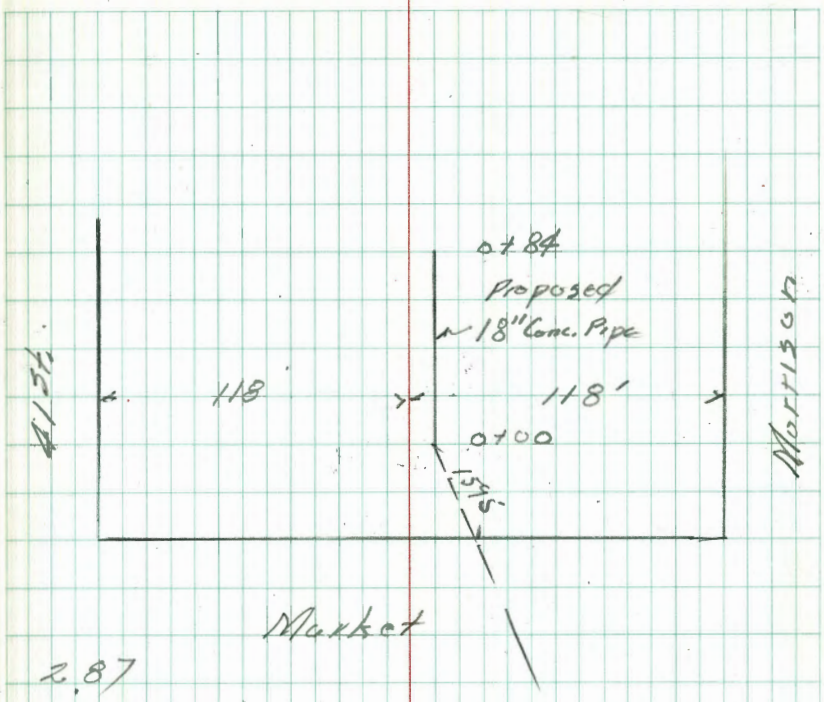
Culvert Const. Blk 2
Marrison's Mercantile Park
Check and Replace
Lost Stakes; this job staked
by another party

Walker Plan #3927-B
Pope
K. Sisson
7-11-50

INDEXED
JUL 12 1950

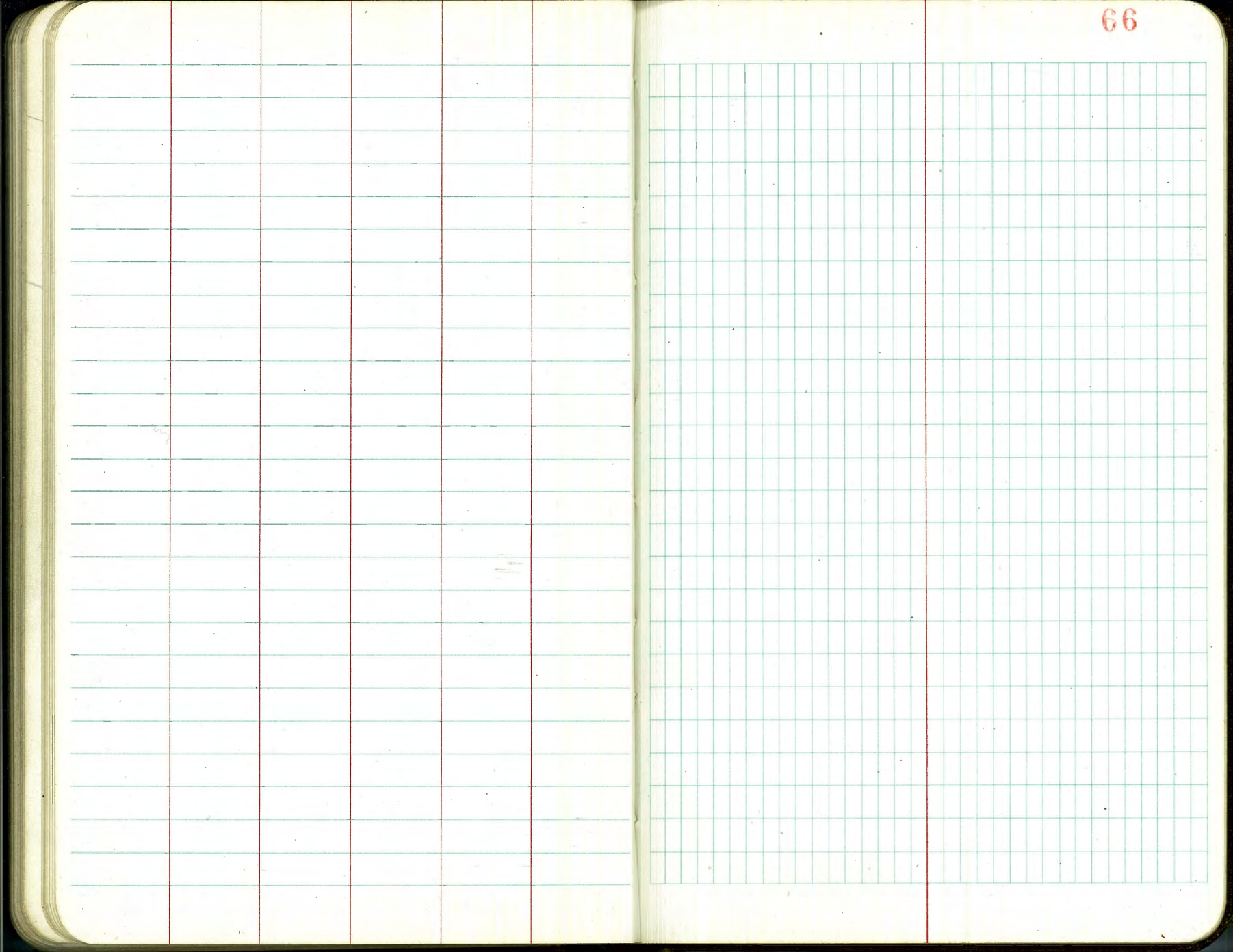
0784-End	223	19.87	117.00
0763	4.76	117.34	116.30
0742	5.17	116.93	115.62
0721	5.24	116.86	114.93
0700			114.23

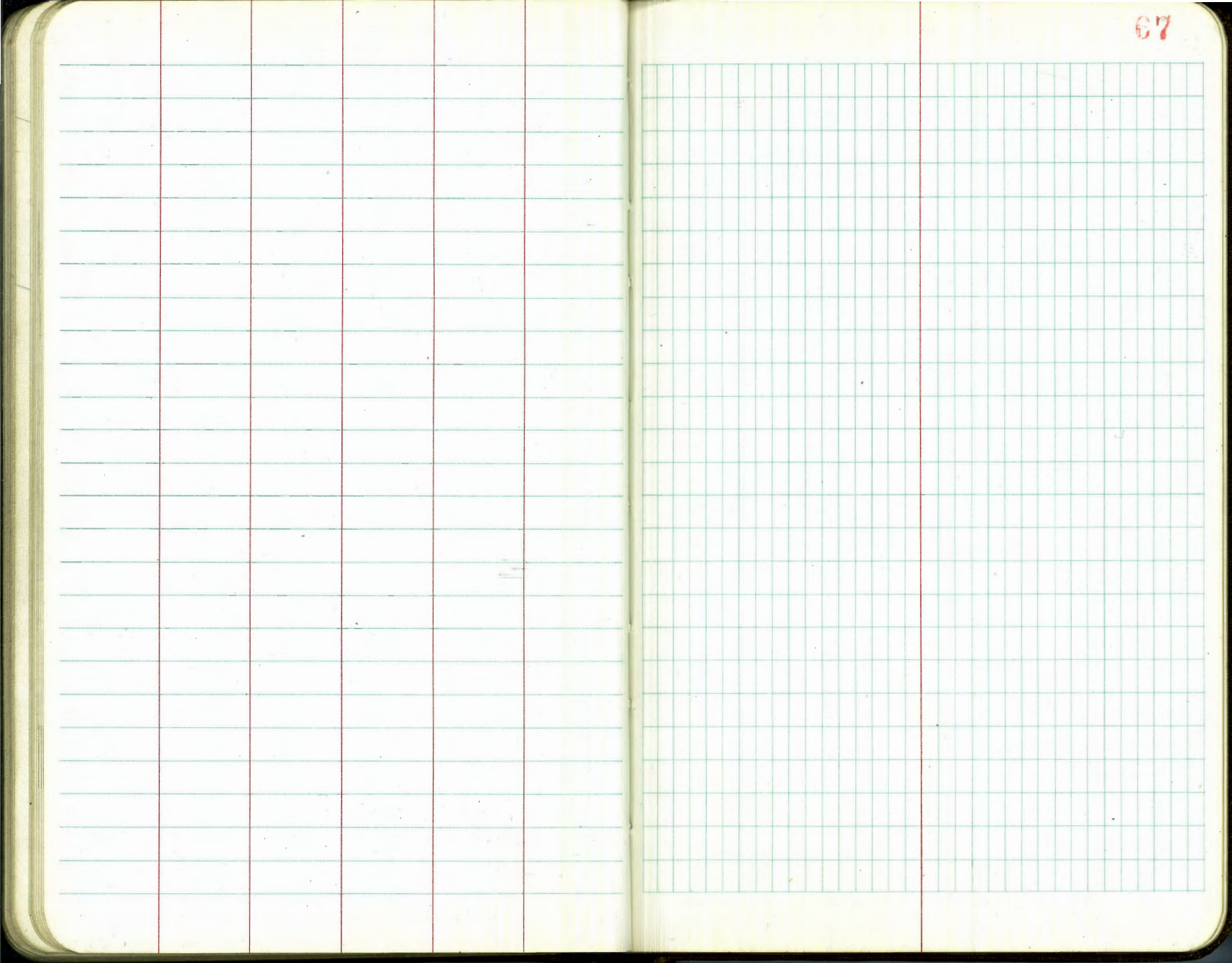
5.17 122.10 116.93

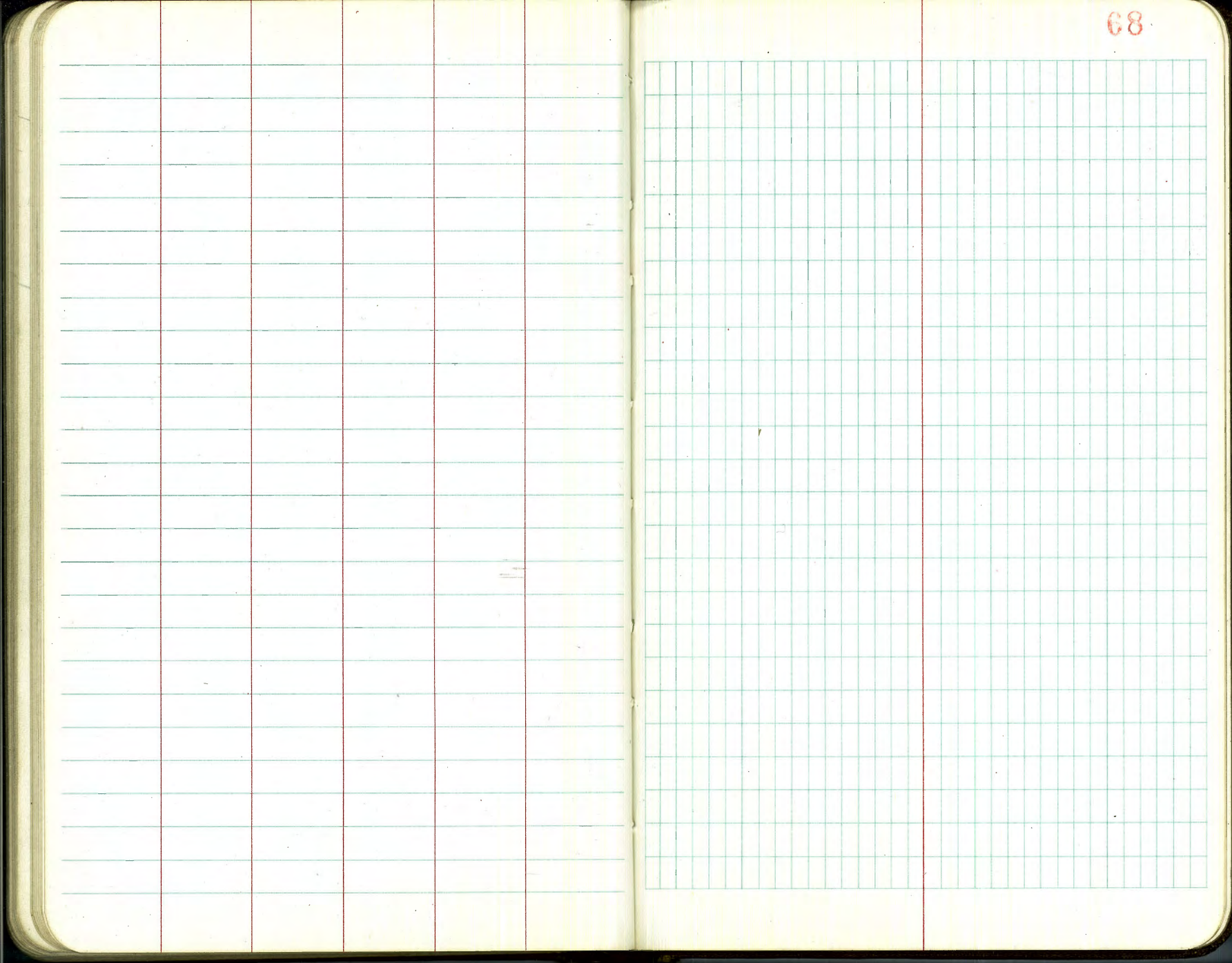


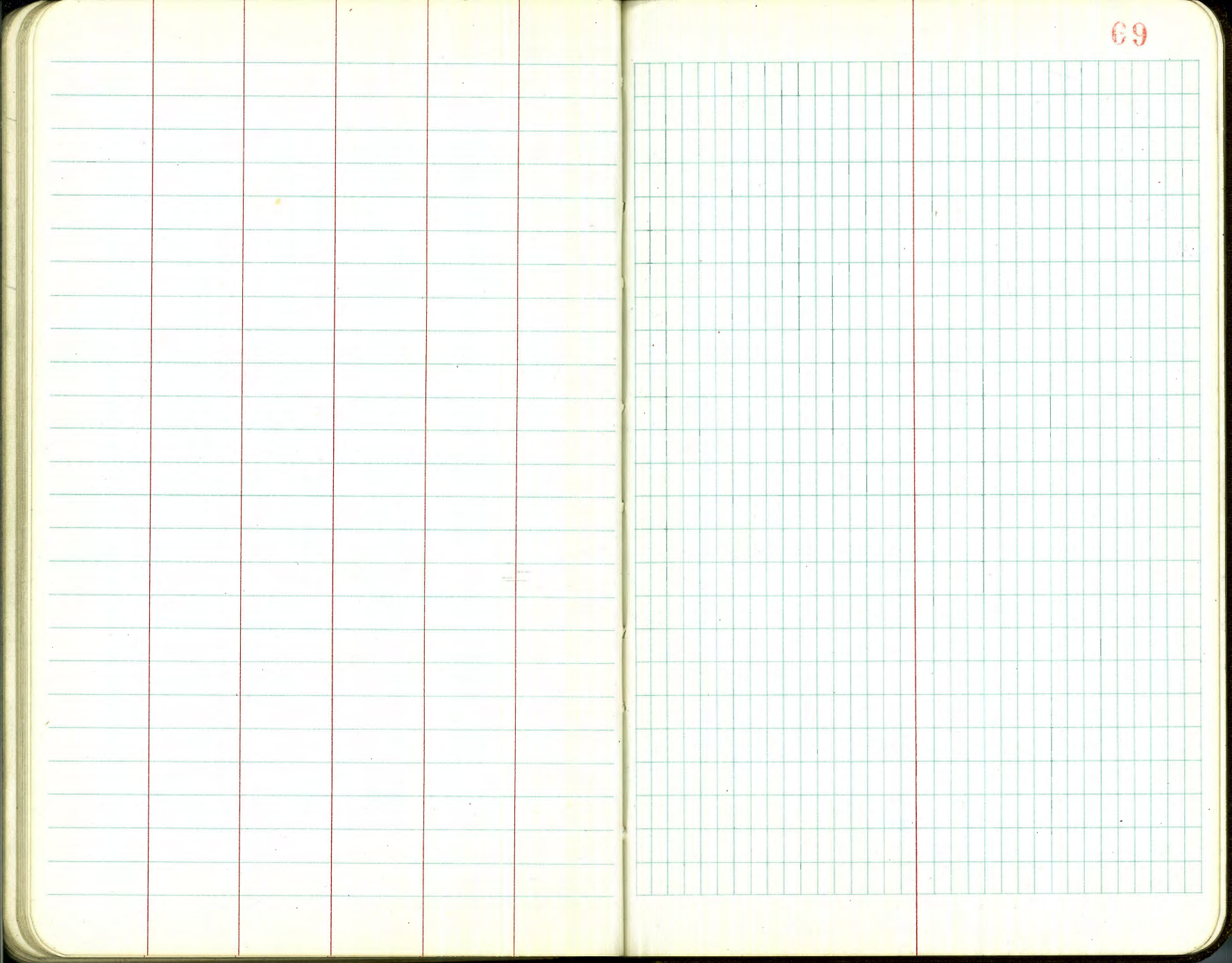
2.87
1.64
1.31
1.93 chks.
B.M. on Stake 0742

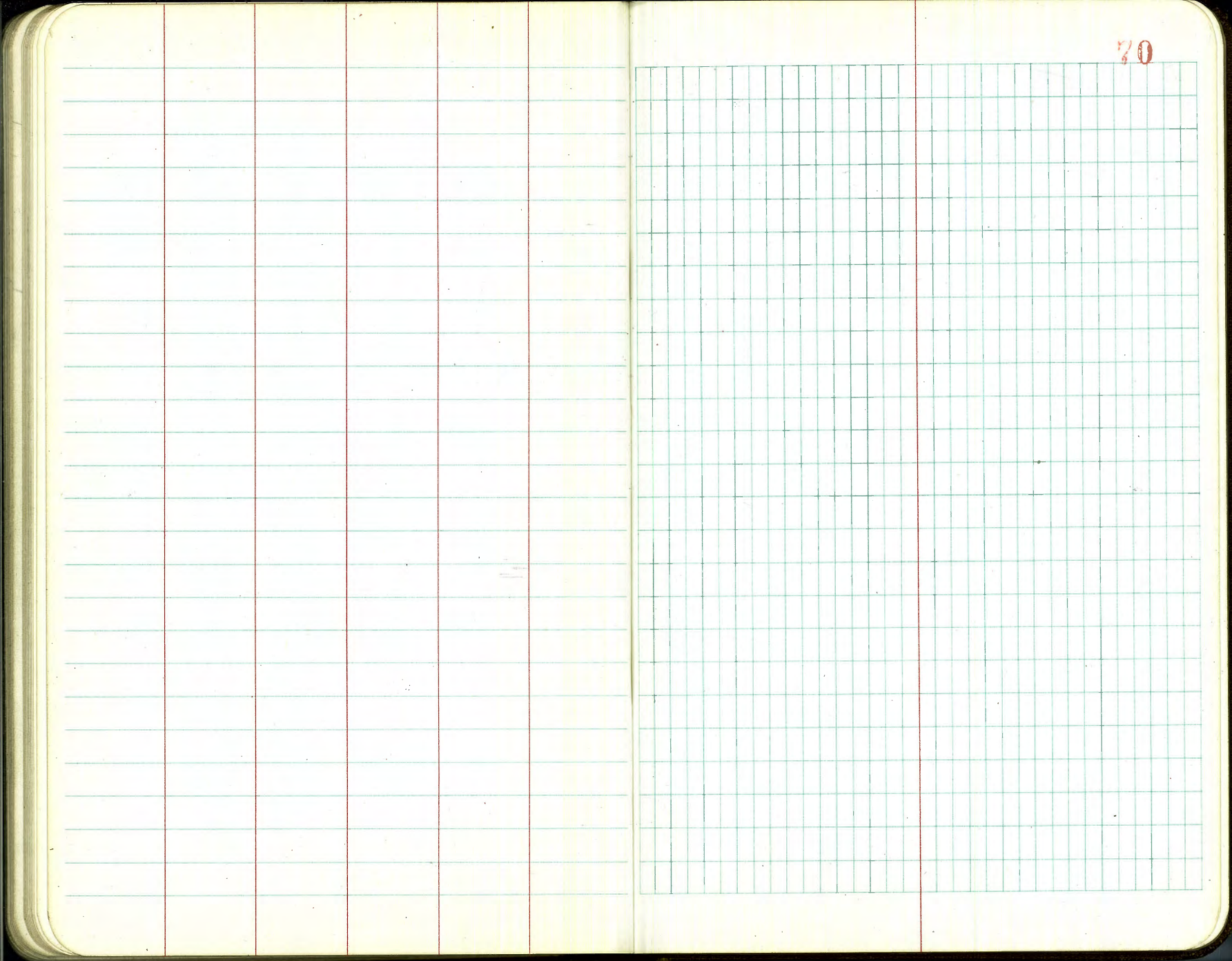
11562 = Grade
131 = Cut Mud
11693 = Elev. Stake

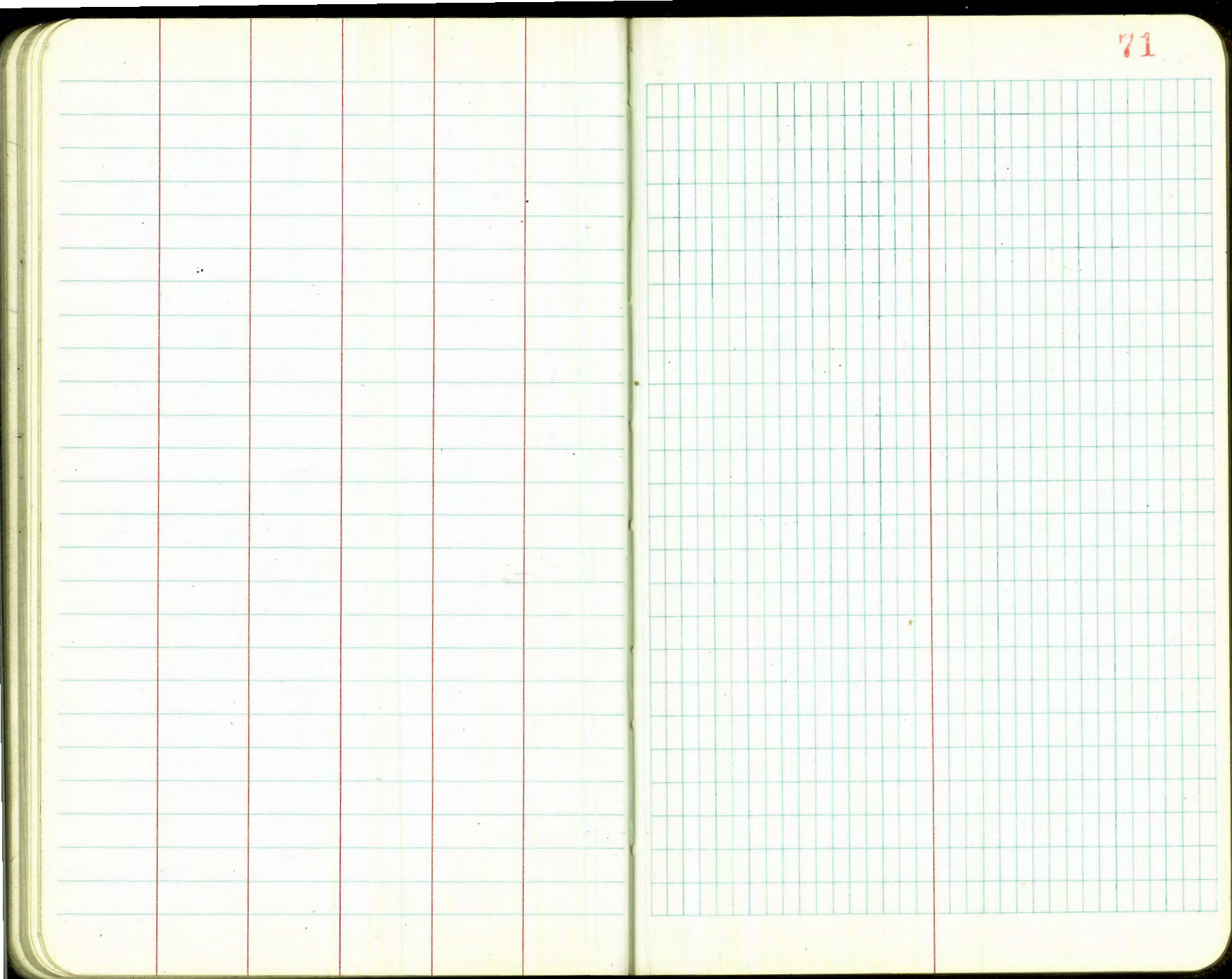


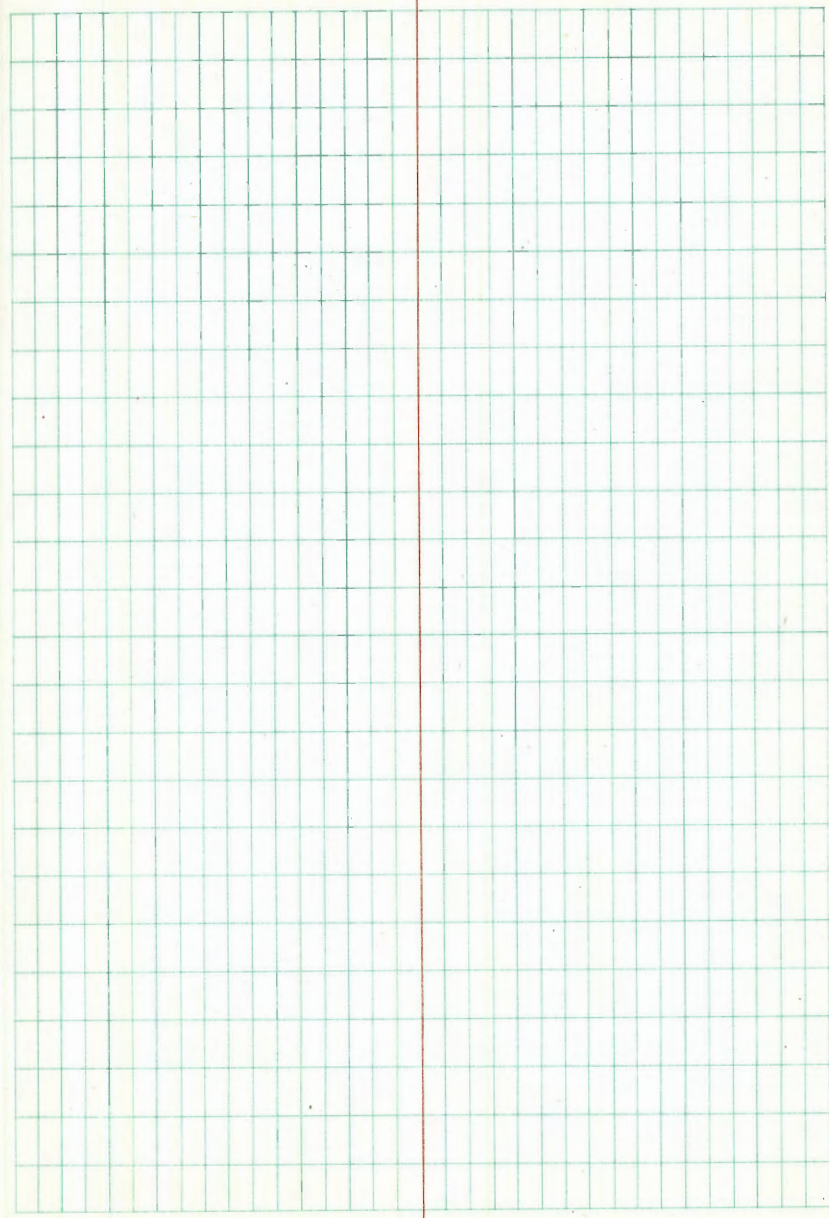
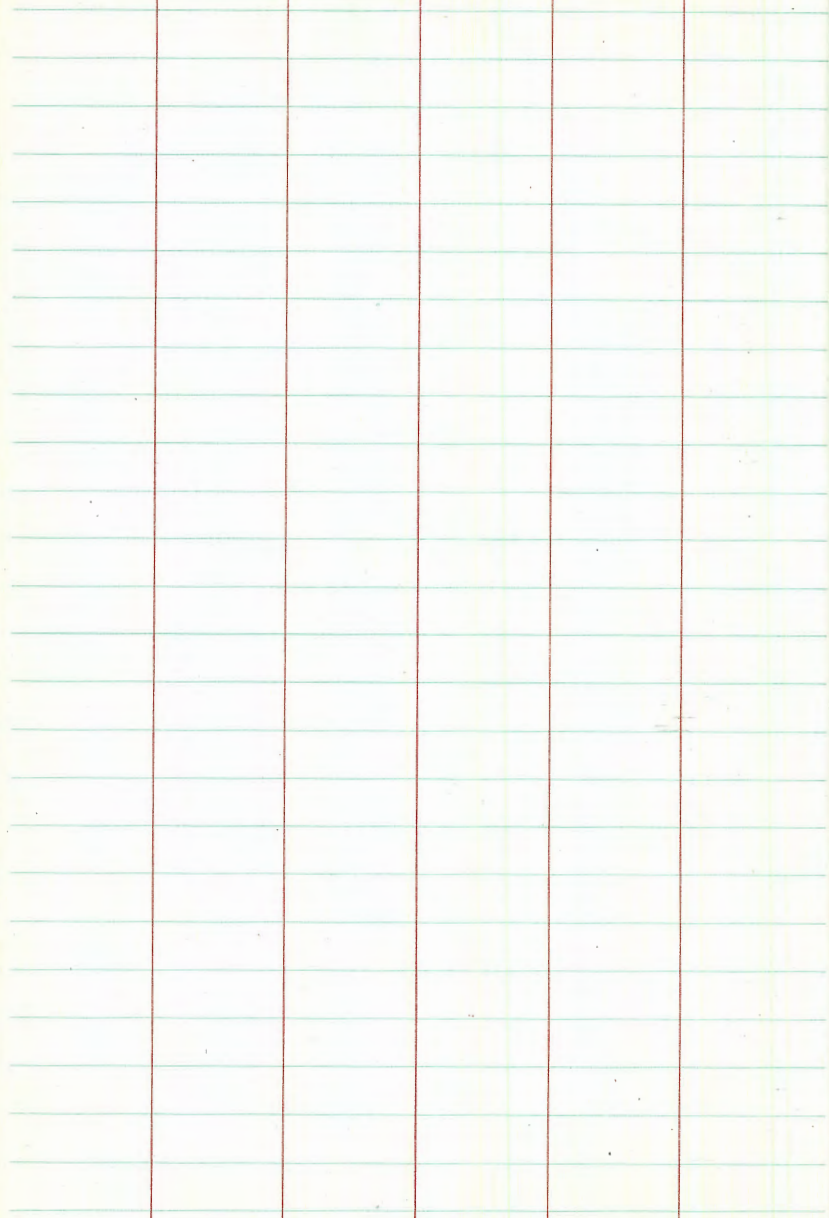


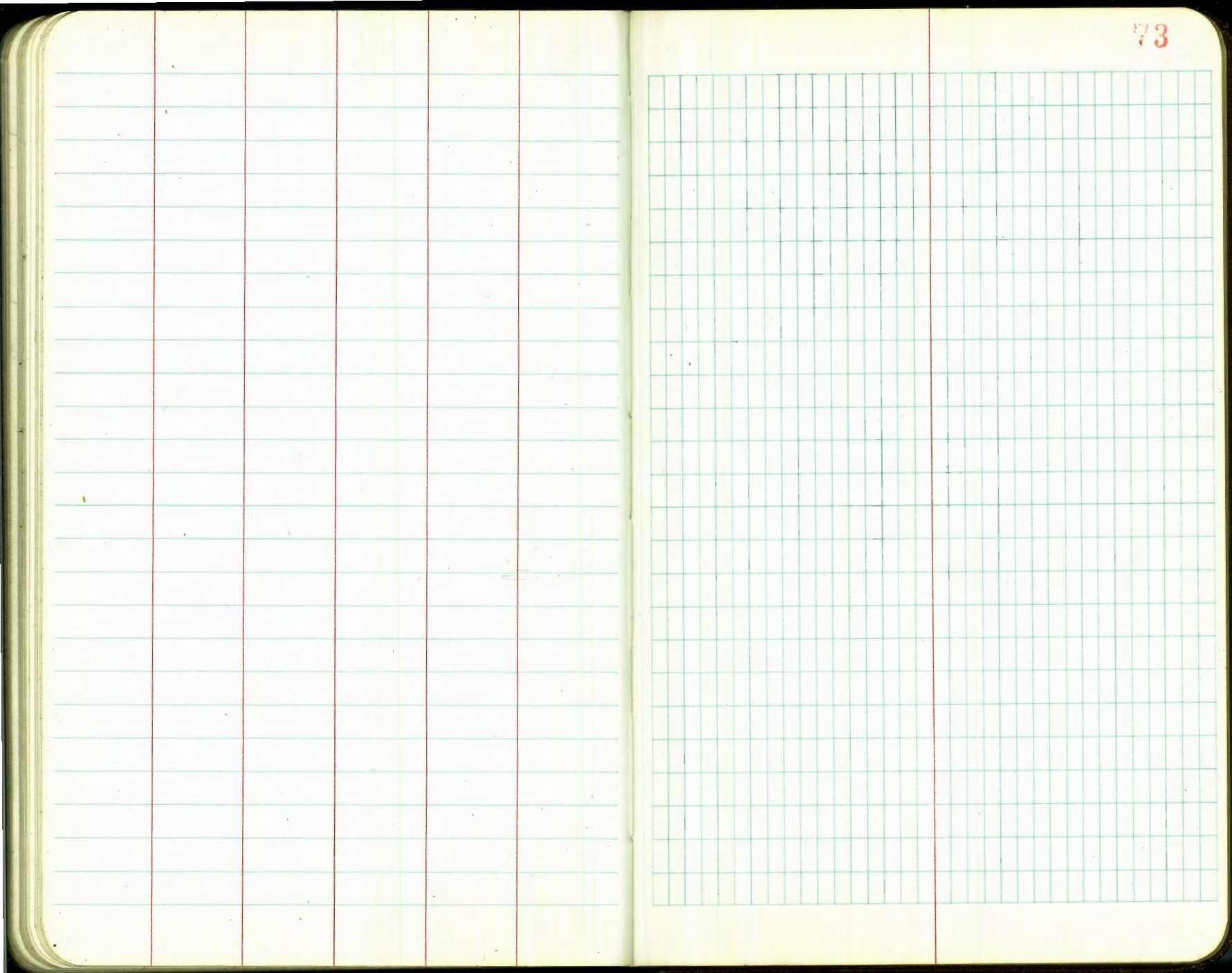


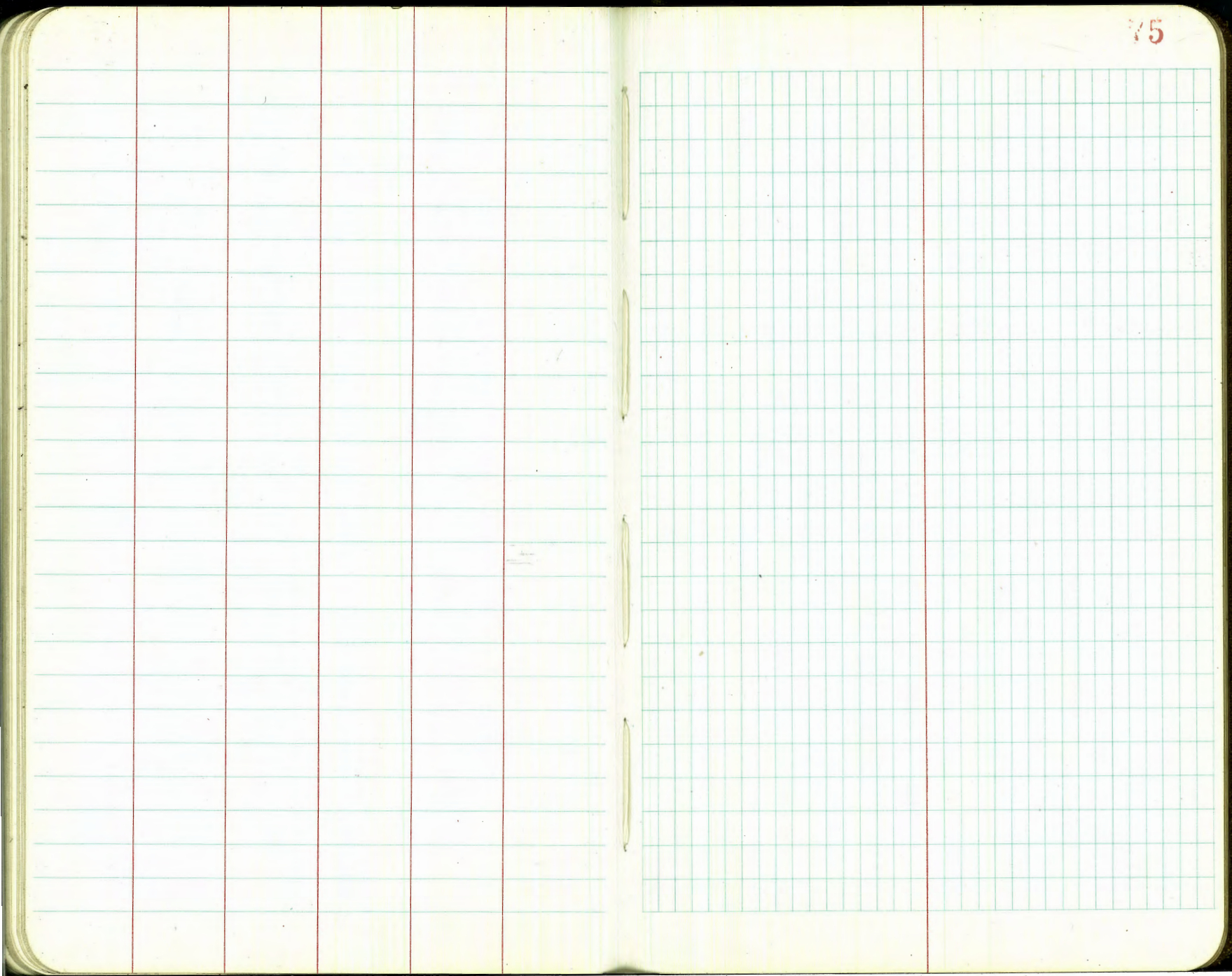


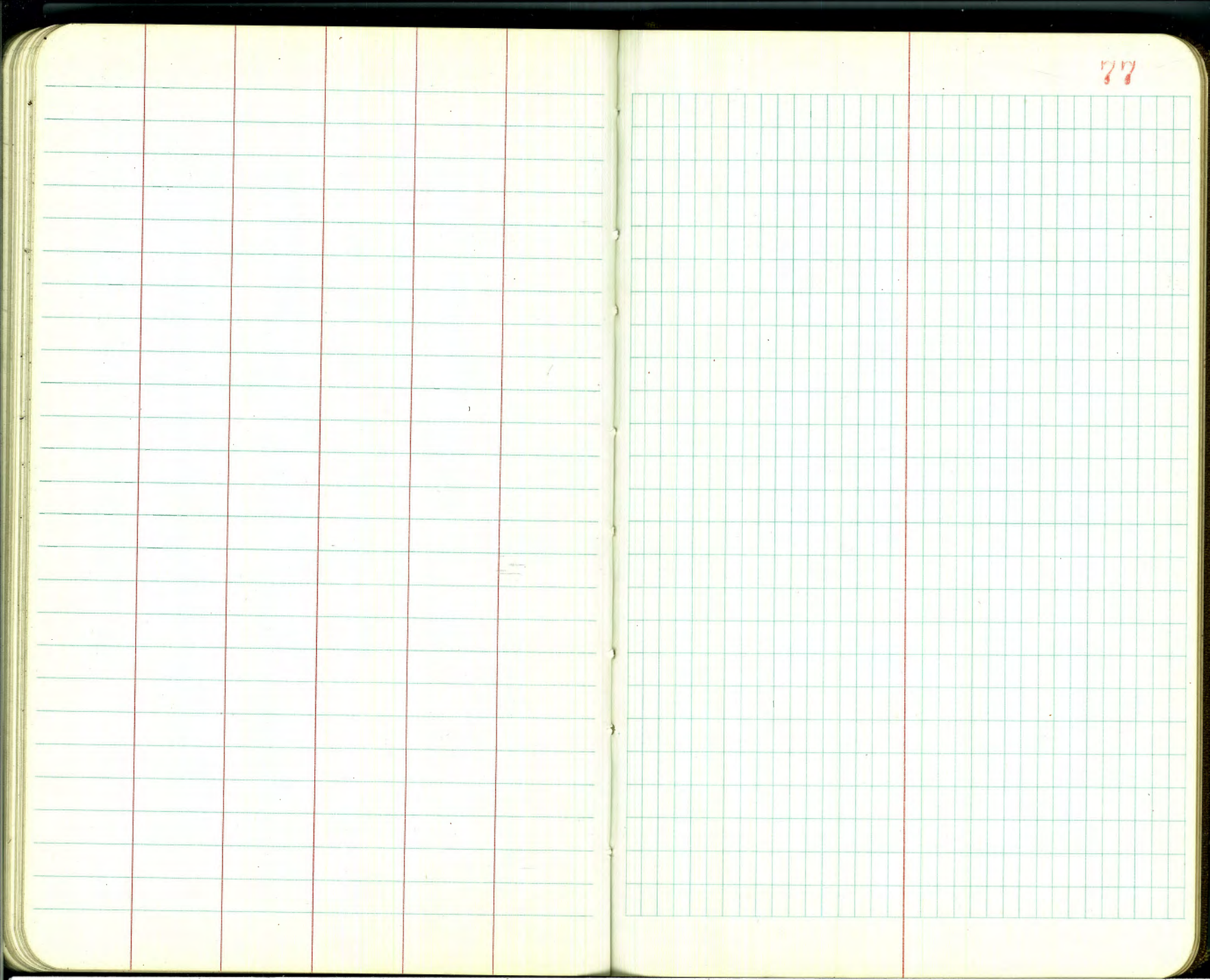


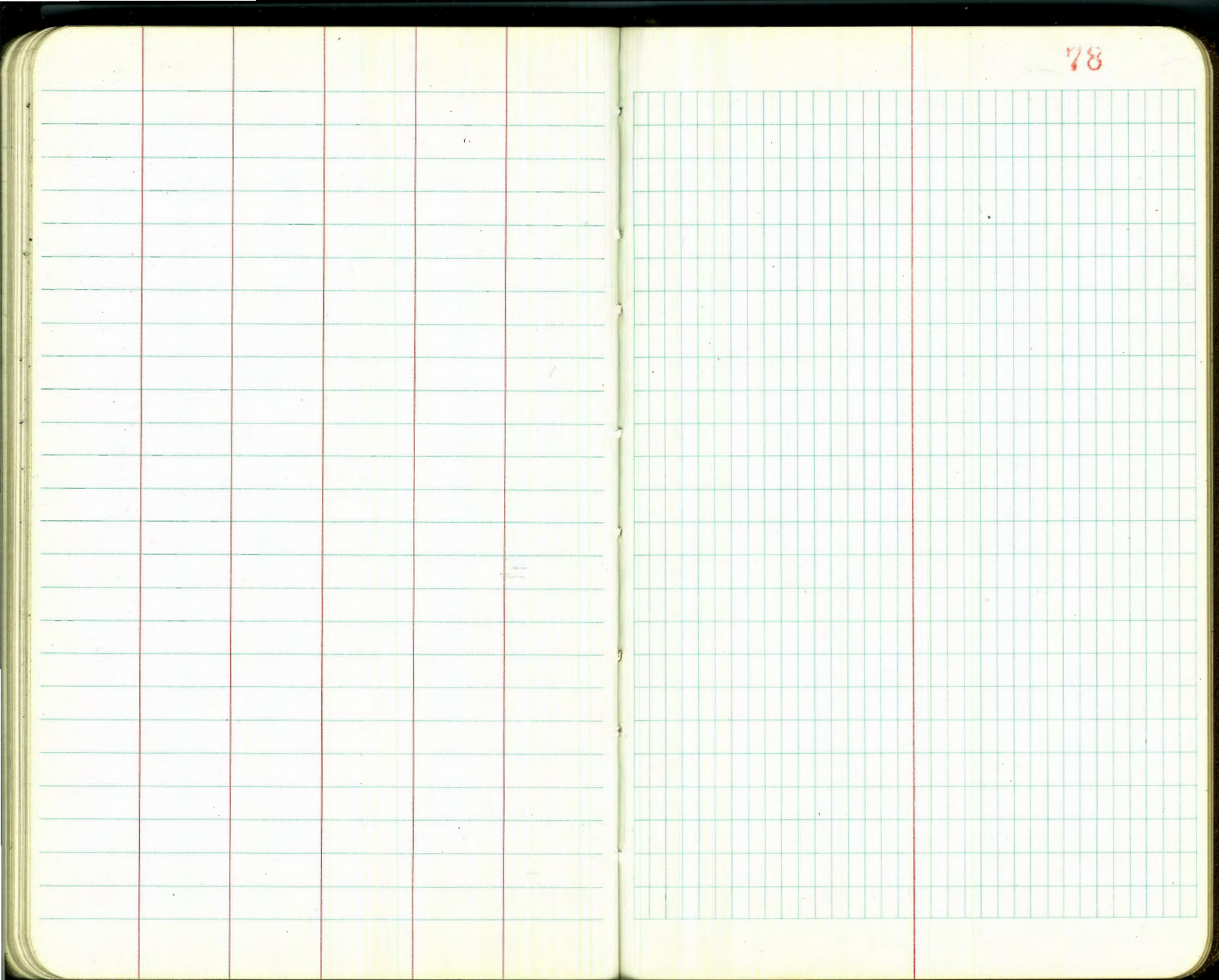






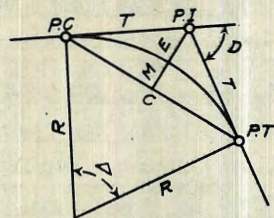






DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

Radius $= R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve $= D$ and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
 Tangent $= T = R \tan \frac{\Delta}{2}$ (3) Length of Curve $= L = 100 \frac{\Delta}{D}$ (4)
 Middle ordinate $= M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
 External $= E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
 Long Chord $= C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. $- T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. $+ L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 — Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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