EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

1814

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade **50%** Rag Paper having a **WATER RESISTING SURFACE,** and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Index on page 1

9

. Xsec Hayes, Vermont To 10 Tp, 20

Kello

Alley Blk. 47 Ocean Beach

Cross Section

12-4-47

W.O. 31431

Sommermeyer
W Moore
E Sherman

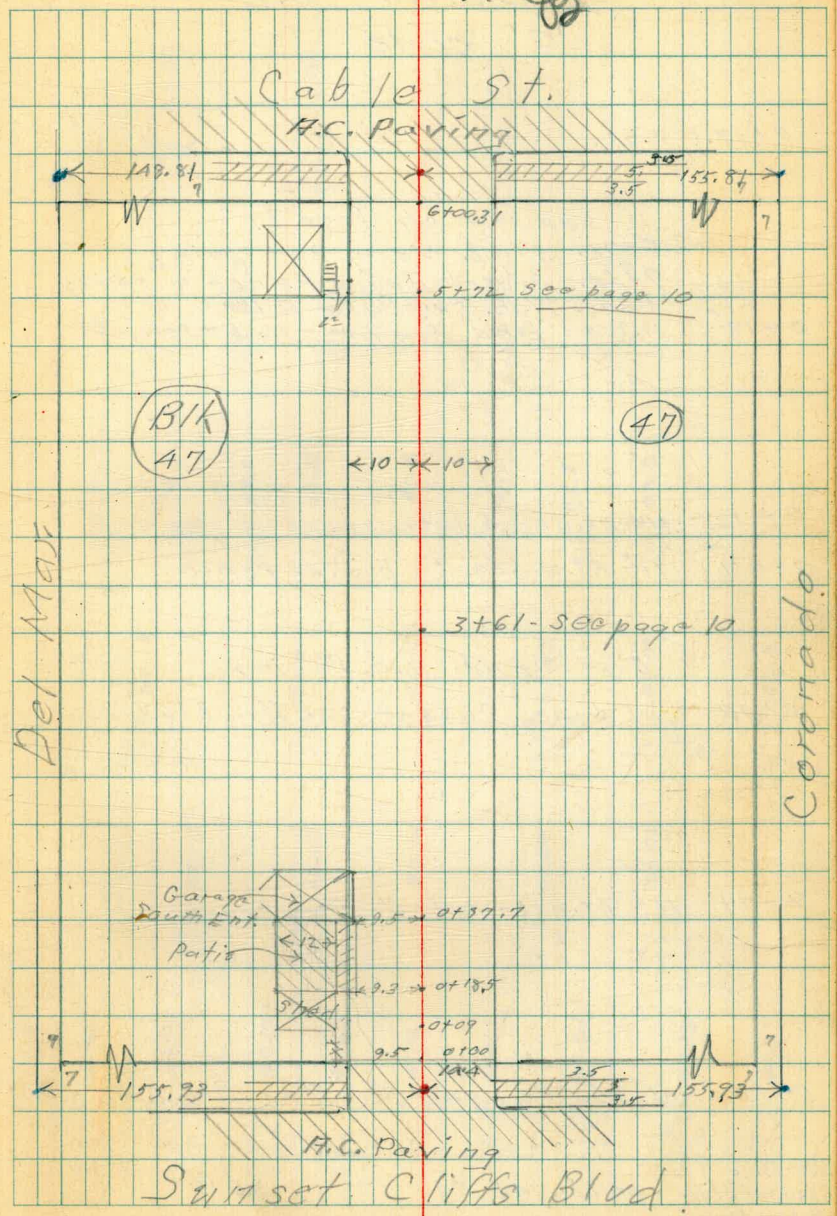
• = Fd. L&T.

• = Set Conc. Nail.

All distances chained unless otherwise noted.

Indexed

2



Alley Blk. 47 O.B
20' Wide

0+18.5 Cont.

see sketch on Page 2.

Conc. Slab. Very poor mix.

0+18[5] 9[3] Lt.= Start Board fence & rough Conc. Slab. For Patio also.
11.3 Lt= End frame shed + start

0+12 11[4] Lt.= End lath fence & start Frame shed

0+09 11[E] Rt.= Start picket fence

Also= End A.C. Paving

0+00 = W. Line Sunset Cliffs Blvd

0-01 11[L] Lt.= start lath fence.

0-12 = W. Cl. Sunset Cliffs Blvd.

NW. B.P. Sunset Cliffs & Del. Mar 10.72 46.91 — 36.19

Lt. ℄ Rt.

9.04/24 37.87 — 8.93/12 slab 37.98

9.0/9.3 Rough conc 37.9 — 8.0/9 38.9 — 7.1/7 39.8 — 6.8 40.1 — 6.3/7 40.6 — 4.2/10 42.7

9.2/40 37.7 — 8.6/11 38.3 — 7.7/10 39.2 — 6.4/6.5 40.5 — 6.1 40.8 — 5.8/5 41.1 — 4.1/10 42.8 — 3.7/15 43.2

4.8/12 Grd. 42.1 — 4.76/9.50 End Cl. 42.15 — 4.88/Pav. 42.03 — 4.89 42.02 — 4.38/10.4 Pav 42.53 — 3.94/10.40 End Cl. 42.97 — 3.7/12 Grd. 43.2

4.76/9.50 Cl. 42.15 — 4.86/9.5 pav 42.05 — 4.77 42.14 — 4.37/10.4 Pav 42.54 — 3.91/10.40 Top Cl. 43.00

6.49/50 top Cl. 40.42 — 6.94/50 Cutt 39.97 — 4.84 Top 1E Cl. Ret 42.07 — 5.22/10 Pav 41.69 — 4.85 42.06 — 4.44/10 Pav 42.47 — 3.90 Top 1E Cl. Ret 43.01 — 2.62/50 Cu th pav 44.29 — 2.14/50 Top Cl. 44.77

46.91

Alley Blk. 47 O. B.

Gar. Conc. floor.

1+19 21° Rt. = Start door to double

1+00 9° Lt. = line of picket fence

0+99 9½ Lt. = Pole # P.H. 4820
start picket fence.

0+50 9° Lt. = End frame Gar. also

0+46 11° Rt. = End picket fence

T.P. 3.36 40.73 9.54 37.37

0+37.7 Cont.

start frame garage. South entorance

0+37 9° Lt. = End Conc. + Grout slabs

46.91

Lt. ℄ Rt.

36.0 35.9 36.2 37.7 37.63
4.7/10 4.8 4.5/10 3.0/17 3.10/21
Grd. + Conc. Floor

36.0 36.4 36.3 36.4 37.8
4.7/50 4.3/10 4.4 4.3/10 2.9/20

36.6 37.1 37.8 37.8 37.9 38.8 39.3
4.1/50 3.6/10 2.9/6 2.7 2.8/5 1.9/10 1.4/25

37.6 38.0 38.1 38.4 40.3 42.2 42.3
3.1/9.5 2.7/7 2.6 2.3/7 0.3/10 +1.5/12 +1.6/20

40.73

37.2 37.50
9.7/40 Grd. 9.41/24 Slab

37.69 37.6 38.0 38.5 38.6 38.9 41.8 42.7 43.1
9.22/12 Slab 9.3/9.5 Rough Conc. 9.7/9.5 Grd. 8.4/6 8.3 8.0/7 5.1/10 4.2/12 3.8/4.5

Alley Blk. 47 O.B.

garage Conc. floor
1+78 Rt. = start Conc. Apron to Sing

1+77 13' Lt. = ℄ 3rd door

1+67.8 13' Lt. = ℄ 2nd door

1+55 13.0 Lt. = Start A car Gar. Conc. floor

1+50 9.7 Lt. = End picket fence

Conc. floor
1+34.5 21.0 Rt. = End door to Doub Gar.

40.73

Station	Lt.			℄			Rt.
1+78			34.9 5.8 / 10	34.8 5.9	35.0 5.7 / 10	35.14 5.59 / 11.4 Edge Apron	35.41 5.32 / 13.5 Rt Gar
1+77	35.03 5.70 / 13 Floor	35.0 5.7 / 12	35.0 5.7 / 10	34.8 5.9	34.8 5.9 / 7	35.0 5.7 / 10	
1+67.8	35.04 5.69 / 13 Floor	35.1 5.6 / 12	35.0 5.7 / 10	35.0 5.7	35.0 5.7 / 7	35.2 5.5 / 10	
1+55	35.04 5.69 / 13 Floor	35.1 5.6 / 12	35.3 5.4 / 10	35.2 5.5	35.5 5.2 / 10	35.6 5.1 / 30	
1+34.5			35.8 4.9 / 10	35.7 5.0	35.8 4.9 / 10	37.4 3.3 / 18	37.6 3.1 / 21 Grd; 37.66 3.07 / 21 Floor

Alley Blk. A7. O.B.

2+03 4 10° = End lath fence

2+03 11 Lt. = start frame dwelling

1+01 5 8° Lt. = ℄ 3' Rough conc. stab walk.

2+00 10 Lt. = Lath fence

1+97 5 9 Lt. = Pole # P.A. 4834

1+93 10 5 Rt. = ℄ 2'4" wide Conc. walk.

1+91 11 Rt. = start board fence.

1+89 5 13 Lt. = End doors to 4 car Gar.

1+88 8 11 5 Rt. = End Conc. Apron

1+84 Rt. = ℄ Sing Gar.

40.73

	Lt.	℄	Rt.
2+03 4			
2+03			
1+01 5			
2+00			
1+97 5			
1+93			
1+91			
1+89 5			
1+88 8			
1+84			

34.0 6.7 30

34.1 6.6 10 conc.

34.2 6.5 8 conc

34.2 6.5

34.3 6.4 7

34.8 5.9 10

34.9 5.8 10

34.4 6.3

34.6 6.1 10

35.02 5.71 10.5 walk ℄

35.03 5.70 13.1 Floor

34.9 5.8 13

34.9 5.8 10

34.5 6.2

34.8 5.9 10

34.9 5.8 10

34.5 6.2

34.9 5.8 10

35.11 5.62 11.8 Apron

35.40 5.33 13.6 Rt Gar

35.0 5.7 10

34.6 6.1

34.9 5.8 10

35.11 5.62 11.4 Apron

35.41 5.32 13.5 Gar. Floor

Alley Blk. 47 O.B.

2+88.5 9.5 Lt. = pole # P.H. A850

2+86.5 10.1 Lt. = End Conc. Apron

2+81.5 14.1 Lt. = ℄ Sing Gar. door

Conc. Floor
Also start Conc. Apron to Sing Gar.

2+73.5 10.1 Lt. = End lath fence

2+50

2+25 10.8 Rt. = End board fence

2+23.1 10.1 Lt. = start lath fence

2+23 11.0 Lt. = End frame dwelling

40.73

Lt. ℄ Rt. 7

33.29 | 32.88 | 32.9 | 32.9 | 33.2
7.44 / 14.1 Back Edge Apron | 7.85 / 10.1 Apron | 7.8 / 10 | 7.8 | 7.5 / 10

33.32 | 32.94 | 32.9 | 33.0 | 33.1
7.41 / 14.1 Gar Floor | 7.79 / 10.1 Apron | 7.8 / 10 | 7.7 | 7.6 / 10

33.30 | 32.97 | 33.0 | 33.0 | 33.2
7.43 / 14.1 Back Edge Apron | 7.76 / 10.1 Apron | 7.7 / 10 | 7.7 | 7.5 / 10

32.6 | 33.2 | 33.2 | 33.5
9.1 / 50 | 7.5 / 10 | 7.5 | 7.2 / 10

Alley Blk. 47 O.B.

T.P.	4.08	36.46	8.35	32.38 Conc. Floor
3+41^5	18^3 Lt. = ℄ Sing Gar. door. no Apron			
	12^7 Rt. = End doors to 3 car Gar.			
3+36	9^8 Rt. = End Conc Apron			
3+34^5	8^8 Lt. = End picket fence			
3+32	10^1 Lt. = Ctr. 18" Cypress tree			
3+25	8^8 Lt = start picket fence			
	12^7 Rt. = ℄. Ctr. door. Gar.			
3+21	16.9 Lt. = End doors to 3 car Gar			
3+08	16^8 Lt. = Ctr. Center. door.			
3+06	9^8 Rt. = Start Apron to 3 Car Gar.			
2+93	16^7 Lt = Start doors to 3 Car garage.			
	40.73			

Lt.			℄	Rt.			
32.50 8.23 / 18.3 Floor	32.4 8.3 / 18	32.2 8.5 / 10	32.1 8.6	32.3 8.4 / 10			
		32.4 8.3 / 10	32.3 8.4	32.4 8.3 / 9.5 Grd	32.68 8.05 / 9.8 End Apron	32.71 8.02 / 10	33.00 7.73 / 12.7 at Gar
33.03 7.70 / 16.9 Floor	32.9 7.8 / 16	32.3 8.4 / 10	32.4 8.3	32.5 8.2 / 9.5 Grd	32.76 7.97 / 9.8 Apron	32.79 7.94 / 10 Apron	33.08 7.65 / 12.7
Grd.	33.00 7.73 / 16.7 Floor	32.5 8.2 / 10	32.6 8.1	32.3 8.4 / 9.5 Grd	32.81 7.92 / 10 9.8 Apron		
	32.9 7.8 / 15	32.5 8.2 / 10	32.7 8.0	32.7 8.0 / 9.5	32.80 7.93 / 9.8 Apron		33.12 7.61 / 12.7 at Gar
32.86 7.87 / 16.7 Gar Floor	32.7 8.0 / 16	32.6 8.1 / 10	32.8 7.9	33.0 7.7 / 10			

Alley Blk. 47 O. B.

14[E] Rt. = Start board fence.
sketch page 10
13[E] Rt. = Start Conc slab. See
3+61 11[E] Rt. = End Apron +

3+55 14[E] Rt. = ℄ Gar. door.

Sing Gar.
3+50[E] 11[E] Rt. = Start Conc Apron to

8[E] Lt. = Start board fence
3+50[E] 9[E] Rt. = End Conc. slab Also =

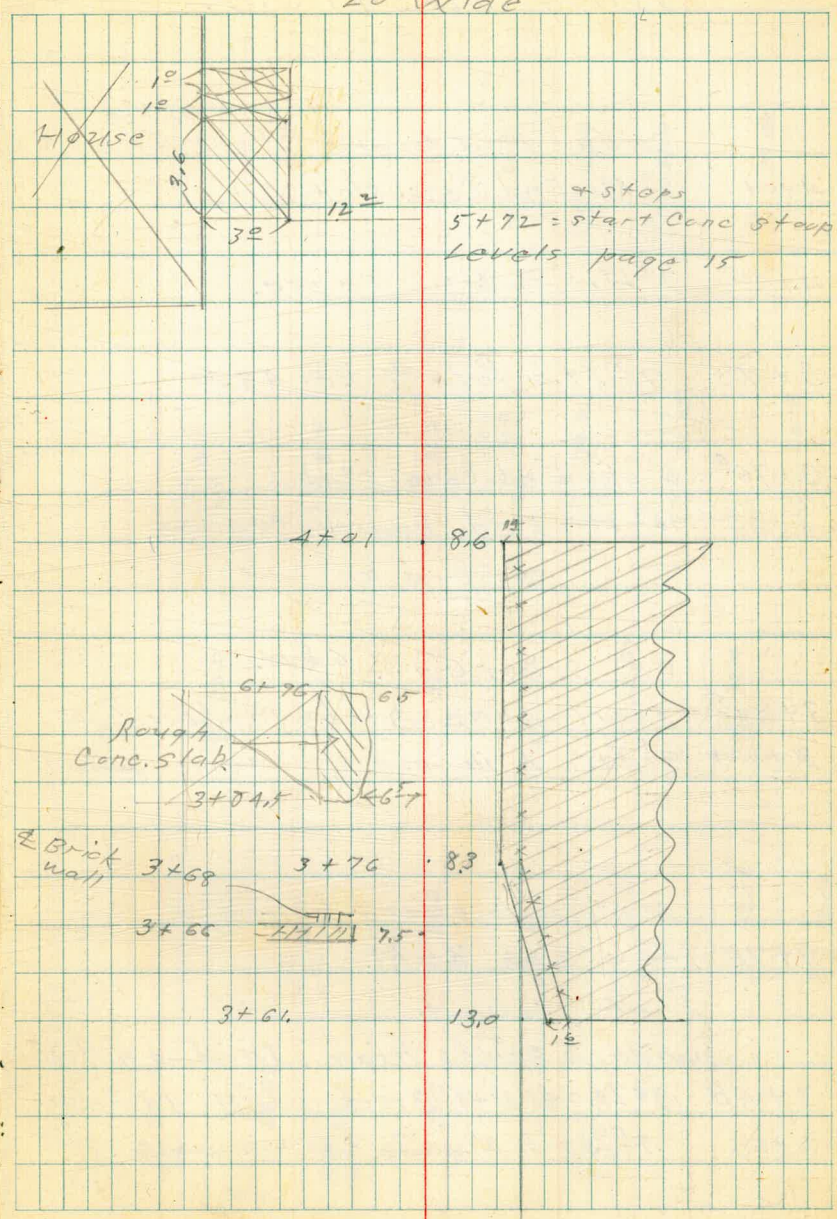
3+45 9[E] Rt. = Start Conc Slab

36.16

Lt. ℄ Rt. 9

32.29 4.22 13 Edge Slab
32.28 4.18 14.7 Gar Floor + Slab to West.
32.3 4.2
32.1 4.4 10
32.08 4.37 11.6 Apron
Slab Floor
32.0 4.5 10
32.1 4.4 8.9
32.2 4.3
32.1 4.4 10
32.08 4.38 11.6 Apron
32.26 4.20 14.7 Gar Floor
31.9 4.6 9.5
32.1 4.4 10
32.2 4.3 8.9
32.2 4.3
32.1 4.4 10
32.10 4.36 11.6 Apron
32.28 4.18 14.7 Gar
32.2 4.3
32.2 4.3 9.5
32.43 4.03 9.9 Conc.
10
32.4 4.1 10
32.2 4.3
32.3 4.2 9.5
32.37 4.09 9.9 Conc.

Alley Blk. 47. O.B.



3+66

Alley Blk. 47 O.B.

10' Rt. = End board start wire Fence

4+01 8^6 Rt. = End Conc. slab

4+00 9^3 Lt. = ℄ N+S. Fence.

3+98 9^3 Lt. = Pole # P.A. 4860

3+96^0 6^5 Lt. = End conc. slab

3+88 12^8 Lt. = End board fence

see page 10

Ex Sing. Gar. 6^5 Lt.

3+84^5 = start conc slab in front of

3+84 9^1 Lt. = Δ in board fence ~~also~~

10' Rt. = Δ in board fence

3+76 = Δ in slab 8^3 Rt.

of ground.

wide, 4 Bricks High. laid on top

3+68 9^0 Lt. = ℄ N+S Brick wall 1 Brick

3+66 7^5 Lt. = ℄ 2' wide Conc. walk.

36.46

Lt. ℄ Rt.

31.9 4.6/10 — 31.9 4.6 — 31.9 4.6/8 — 31.94 4.52/8.3 Conc. — 32.14 4.32/10 Conc. — 32.06 4.40/25

32.1 4.4/12.9 Rt Bldg. — 31.9 4.6/6.5 Conc. — 31.9 4.6 — 31.9 4.6/8 — 32.01 4.45/8.3 Conc — 32.15 4.31/10 conc. — 32.19 4.27/20

32.1 4.4/12.9 Rt Bld — 32.0 4.5/10 — 31.9 4.6/6.5 Conc — 32.0 4.5 — 31.9 4.6/8 — 31.97 4.47/8.3 Conc — 32.14 4.32/10 Conc

31.9 4.6/8.9 — 32.0 4.5 — 32.1 4.4/8 — 32.13 4.33/8.3 Conc. — 32.18 4.28/10 — 32.00 4.26/20

32.12 4.34/10 — 32.07 4.39/7.5 Conc — 32.1 4.4/7.4 — 32.1 4.4 — 32.1 4.4/10

Alley Blk. 47 O.B.

9.8 Rt. = start latt fence double Car.

4+49.5 — 10.2 Rt. = End Conc. apron to
8.8 Lt. = ℄ N. & S. board fence.
11.3 Lt. = start board fence

4+48.8 — 9.0 Lt. = ℄ 3' wide conc walk

4+47 — 9.3 Lt. = End board fence

T.P. Nail in pole	4.03	36.17	4.32	32.14

4+36 — 15.3 Rt. = ℄ Double Car doors.

9.8 Rt. start of apron to double Car.

4+23 — 10.0 Rt. = End wire fence ℄

4+16.5 — 9.8 Lt. = End Conc. slab

9.8 Lt. = start Conc. slab.

4+11.5 — 9.3 Lt. = start board fence. in Conc. posts

36.46

Lt ℄ Rt. 12

31.84 4.62 10
31.84 4.62 9 walk
31.8 4.7 8
31.7 4.8
31.8 4.7 10
31.8 4.7 C
32.1 4.4 10 ord
32.12 4.34 10 Apron
32.1 4.4 10
31.6 4.9 10
31.5 5.0
31.6 4.9 9.9 ord
31.83 4.63 9.9 Apron
31.99 4.47 15.3 Car floor
31.7 4.8 10
Rain drops
31.6 4.9
31.5 5.0 9.5
31.84 4.60 9.8 conc
31.84 4.62 9.8 conc.
31.7 4.8 9
31.7 4.8
31.8 4.7 10
31.85 4.61 9.8 conc
31.8 4.7 9
31.7 4.8
31.8 4.7 10

Alley Blk 47. O.B.

double Gar.

4+99⁵ 14⁰ Rt. = End Conc. Apron, 14⁴ Rt. = End

4+99 9⁵ Lt. = Pole # PA4882

double Gar & 14⁶ Rt = double garage

4+83 14¹ Rt. = Start Conc. Apron to

4+77⁹

6" Conc. slab.

4+76² 9⁷ Rt. = End shed also end

shed.

0+68 9⁷ Rt. = Start 6" slab under

Frame shed.

4+62 9⁸ Rt. = End lath fence + start

36.17

℄

31.6 4.6/10 | 31.4 4.8/6 | 31.2 5.0 | 31.3 4.9/10 | 31.22 4.95/14 Apron | 31.32 4.85/14.4 Gar Floor

31.5 4.7/10 | 31.4 4.8/6 | 31.3 4.9 | 31.4 4.8/7 | 31.5 4.7/10 | 31.4 4.8/14 | 31.22 4.95/14.1 Apron | 31.38 4.79/14⁶ Floor

31.7 4.5/40 | 31.1 5.1/14 | 31.4 4.8/10 | 31.4 4.8/6 | 31.1 5.1 | 31.3 4.9/6 | 31.4 4.8/9.7 | 31.45 4.72/9.7 ℄ walk | 31.45 4.72/10 on walk

31.4 4.8/10 | 31.4 4.8/6 | 31.1 5.1 | 31.3 4.9/6 | 31.4 4.8/9.7 | 31.53 4.64/9.7 top 6" Conc slab

31.3 4.9/10 | 31.3 4.9/6 | 31.2 5.0 | 31.3 4.9/5 | 31.3 4.9/9.7 Grd | 31.45 4.72/9.7 top. 6" slab

31.4 4.8/40 | 31.3 4.9/10 | 31.3 4.9 | 31.3 4.9/10 | 31.0 5.2/40

36.17

Alley Blk. 47 O.B

garage. dirt floor

5+31 14.4 Rt. = ℄ 2nd door to double

5+30 14.2 Lt. = Start 4 car Gar.

5+26 10' Lt. = ℄ Pipe + wire N.T.S. Fence.

5+25 13.1 Lt. = End double Gar. Conc. Floor.

garage - dirt floor.

5+20 = 14.4 Rt. = ℄ 1st door to double

5+14.5 12.9 Lt. = ℄ double Gar.

= start double Gar. Conc. floor.

5+05 12.6 Lt. = End board fence. Also

36.17

31.8 / 4.4 / 10
31.5 / 4.7 / 6
31.3 / 4.9
31.4 / 4.8 / 10
31.5 / 4.7 / 14.4 at Gar.

32.34 / 3.83 / 14.2 Gar Floor
32.1 / 4.1 / 14
31.8 / 4.4 / 10
31.5 / 4.7 / 6
31.3 / 4.9
31.4 / 4.8 / 10

31.91 / 4.26 / 13.1 Gar Floor
31.8 / 4.4 / 10
31.5 / 4.7 / 6
31.3 / 4.9
31.4 / 4.8 / 6
31.3 / 4.9 / 10

31.8 / 4.4 / 10
31.57 / 4.7 / 6
31.3 / 4.9
31.4 / 4.8 / 5
31.4 / 4.8 / 10
31.3 / 4.9 / 14.4

31.89 / 4.28 / 12.9 Conc. Floor
31.9 / 4.3 / 12
31.8 / 4.4 / 10
31.4 / 4.8 / 6
31.3 / 4.9
31.4 / 4.8 / 10

31.95 / 4.27 / 12.6 Conc Floor
31.8 / 4.4 / 12
31.7 / 4.5 / 10
31.4 / 4.8 / 6
31.2 / 5.0
31.2 / 5.0 / 10
31.6 / 4.6 / 2.5

36.17

Alley Blk. 47 O.B.

T.P. 4.71 35.60 5.28 30.89

5+90

5+77.6 12.2 Lt. = End Conc. Stoop & steps

5+72 12.2 Lt. = Start of Conc. Stoop & steps

5+65.5 14.2 Lt. = End 4 car. Gar.

5+51.5 14.2 Lt. = ℄ 3rd door to 4 car Gar.

5+42.5 14.2 Lt. = ℄ 2nd door to 4 car Gar.

36.17

℄							
5+90	3.9/14 (32.3)	4.4/10 (31.8)	5.3/5 (30.8)	5.2 (31.0)	5.1/10 (31.1)	4.8/15 (31.4)	
5+77.6	3.02/12.2 (33.15) top of Bottom step	4.8/12.2 (31.4) Base of Conc.	4.2/12 (32.0)	4.5/10 (31.7)	4.8/5 (31.4)	4.8 (31.4)	4.8/6 (31.4); 4.8/10 (31.4)
5+72	1.85/12.2 (34.32) on step	4.8/12.2 (31.4) Bottom of Conc	4.2/12 (32.0)	4.5/10 (31.7)	4.7/6 (31.5)	4.7 (31.5)	4.8/10 (31.4)
5+65.5	3.79/14.2 (32.38) Gar. Floor	4.0/14 (32.2)	4.5/10 (31.7)	4.7/6 (31.5)	4.7 (31.5)	4.8/10 (31.4)	4.9/20 (31.3)
5+51.5	3.80 [4.82]/14.2 (32.37) Gar. Floor	4.0/14 (32.2)	4.2/10 (32.0)	4.7/6 (31.5)	4.8 (31.4)	4.9/10 (31.3)	4.8/20 (31.4)
5+42.5	3.83/14.2 (32.34) Floor	4.0/14 (32.2)	4.2/10 (32.0)	4.7/6 (31.5)	4.8 (31.4)	4.9/10 (31.3)	5.0/20 (31.2)

36.17

Alley Blk 47. O.B.

				0.03 Error	
				36.19	
orig BM			3.65	36.22	(36.19)
T.P.	5.59	39.87	3.94	34.28	
T.P. = SEBP. Del Mar + Cable	5.00	38.22	2.38	33.22	(33.12)
6+12[3] Cont.					
6+12[3] Ely. Ch. line Cable.					

A.C. Paving + Curb.

6+00[31] = Ely line Cable = start

35.60

℄

32.06	31.55	31.36	30.88	29.49	29.97	28.70	29.20
3.54 / 100 cb.	4.05 / 100 pav	4.24 / 50 top cb.	4.72 / 50 pav	6.11 / 50 pav	5.63 / 50 cb.	6.90 / 110 pav	6.40 / 110 Curb

30.91	30.87	30.32	30.15	30.08	30.66	30.54
4.67 / 13.5 Cl. E.C. top cb.	4.73 / 11.5 Ctr. Rot 3.5 Rad Curb. Rot	5.28 / 10	5.45	5.52 / 10	4.94 / 11.5 Top. 3.5 Rad Curb. Rot	5.06 / 13.5 E.C. top Curb

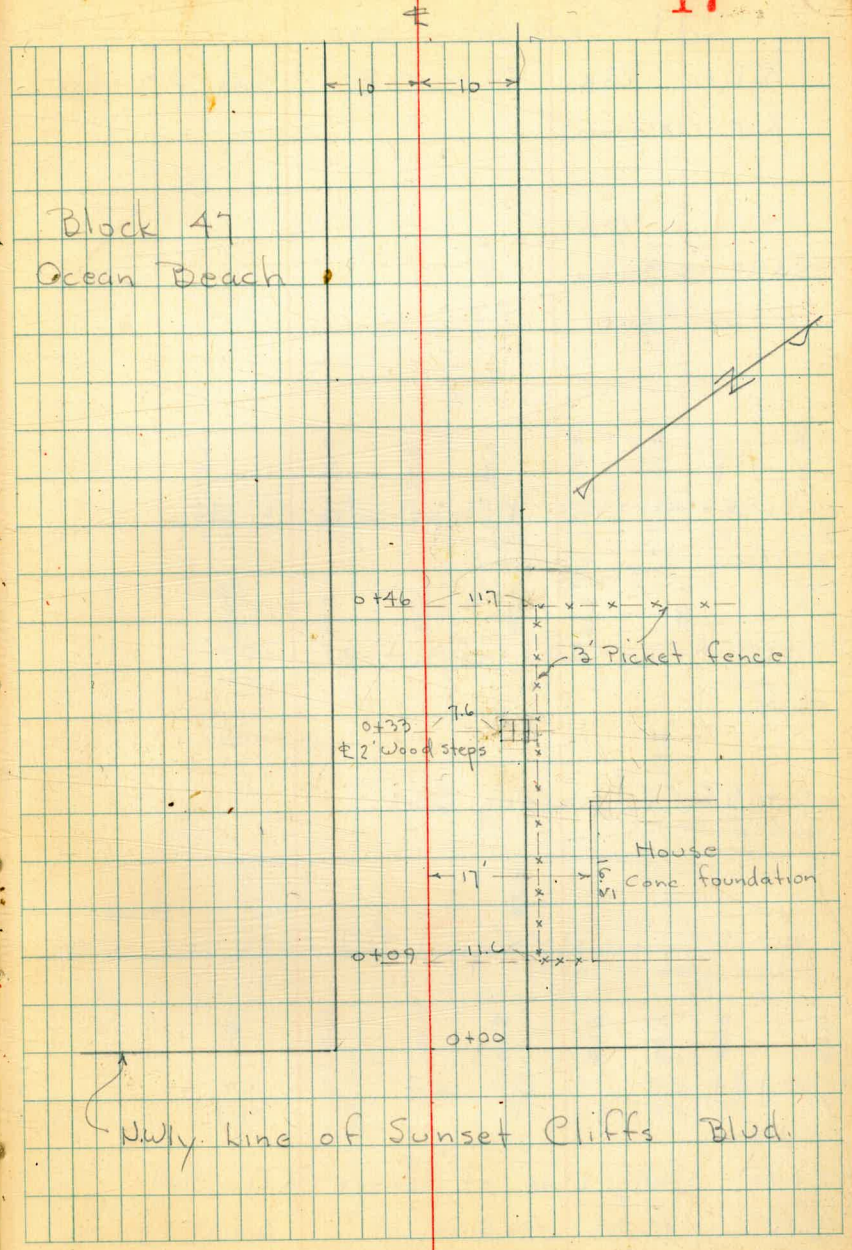
30.95	30.77	30.42	30.40	30.59	30.88
4.65 / 10.08 top. cb.	4.83 / 10 pav	5.18 / 3	5.20	5.01 / 9.90 pav	4.72 / 9.93 Top cb.

35.60

Detail of House and fence
for Prop. Retaining Wall Sections.
Alley - Blk. 47 - O.B.
W.O. 25001 See, P. 2

1-9-47
7.0.

Levels - P. - 18



Add. Sections - 0+00 - W. in Alley Blk. 47 - O.B. - See P. 2 for Req. Sections

0+50 is O.K.

0+46 is O.K.

0+33 Cont.

0+33 = ℄ 2' Wood steps on Rt. - 3 steps

0+25.5 = opp. Wly. of House

0+18.5 = finish orig. Sect.

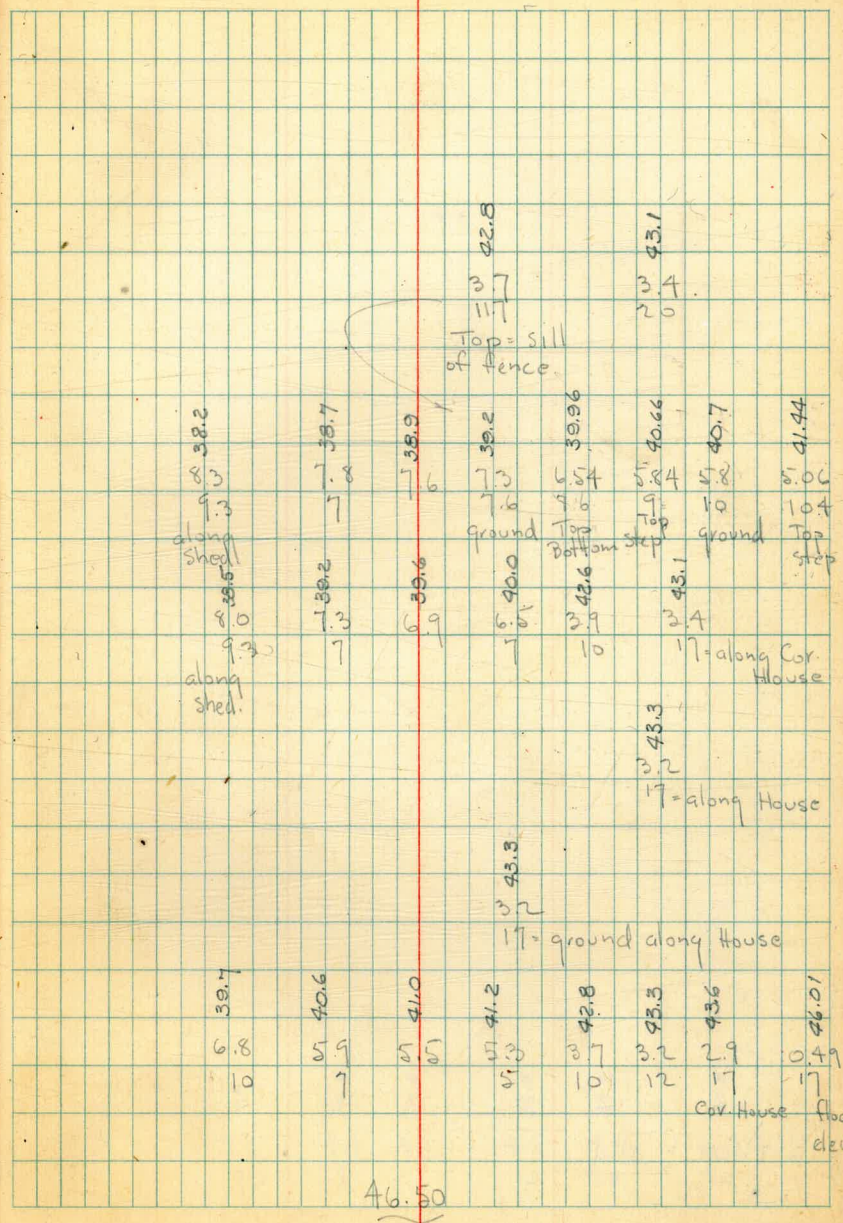
0+12 = finish original Sect. with rod along House

0+09

0+00 = NWly. Line of Sunset Cliffs Blvd.

B.M. 10.31 46.50 36.19 NW. BP. Del Mar.

Lt. = S ℄ - Rt. = N. 18



Lt. ℄ Rt

0 + 00 = end.

37.1	37.4	37.4	38.0	38.3	40.5
9.4	9.1	9.1	8.5	8.2	6.0
10	7		10	20	10

46.50

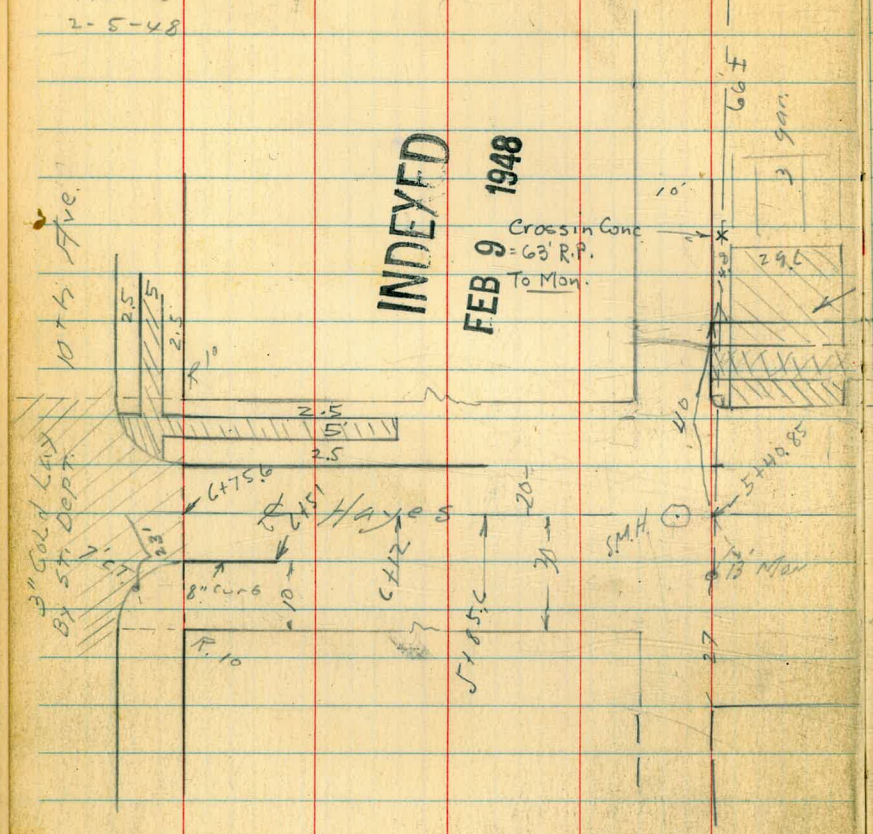
Cross Sec. Hayes Ave.

VERMONT to 10th.

W.O. 60138

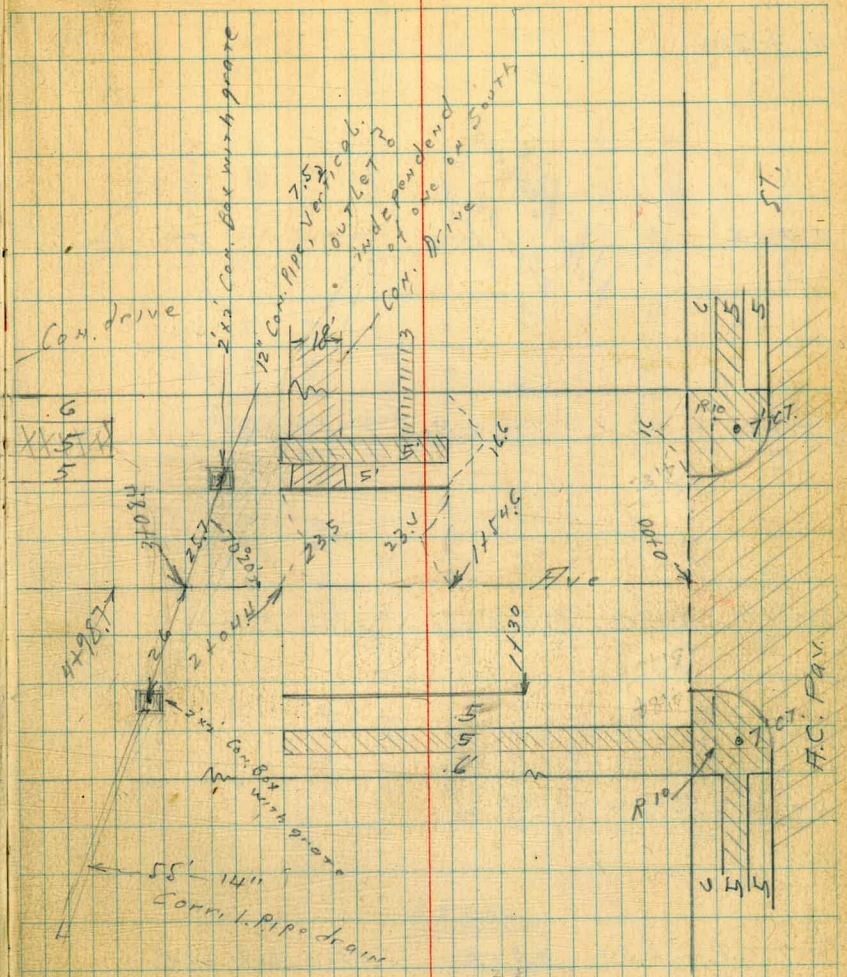
Moore
Begg
Greer
Roberts

2-5-48



1259

20



Xsec Hayes

0 + 50					291.2 3.3 / 40 Terrace
0 + 16					Ter. Lawn
0 + 00 = W.L. Vt. = Beg. 8" Con. Ret. wall on Rt.					
0 - 16	W. curb Vt.				
0 - 40	℄ Vt.				
T.P. SW 7 C.T.	3.36	294.50	5.43	291.14	
T.P. on B.P.	3.73	296.57	7.65	292.82	292.85 P 37
B.M. Ld. C.T. N.W. Cor. Pl. Lincoln and Johnson	2.92	300.49		297.57	

Notes Reduced 2-10-48 O.T.I.

21

Lt. ℄ Rt.

	288.45 6.05 / 34	288.29 6.21 / 29	287.4 7.1 / 24	287.0 7.5 / 23	287.8 6.7 / 12	287.9 6.6	287.7 6.8 / 12	287.2 7.3 / 23	288.1 6.4 / 24	288.9 5.6 / 40	288.50 6.0 / 40 Bot. wall	291.2 2.3 / 40 Top
291.9 2.6 / 40	290.23 4.27 / 34	290.09 4.41 / 29 walk	289.4 5.1 / 24	288.8 5.7 / 23	289.6 4.9 / 12	289.8 4.7	289.7 4.8 / 12	289.4 5.1 / 23	289.9 4.6 / 24	290.6 3.9 / 40	289.9 4.6 / 40 Bot. wall	293.40 1.10 / 40 Top
		291.29 3.21 / 40 Sdw.	290.99 3.51 / 24 CG	290.29 4.31 / 24 GT	290.71 3.79 / 12	290.97 3.53	290.79 3.71 / 12	290.22 4.28 / 24 GT	290.94 3.56 / 24 CG	291.26 3.24 / 40 Sdw.	293.44 1.06 / 40 Top wall	290.9 3.6 / 40 Bot.
291.27 3.23 / 90 CG	290.81 3.69 / 90 GT	290.99 3.51 / 40 CG	290.51 3.99 / 40 GT	290.54 3.96 / 24	290.99 3.51 / 12	291.18 3.32	291.00 3.50 / 12	290.56 3.94 / 24	290.41 4.09 / 40 GT	290.97 3.53 / 40 CG	291.11 3.39 / 95 GT	291.60 2.90 / 95 CG
		291.82 2.68 / 90	291.35 3.15 / 40	291.14 3.36 / 24	291.39 3.11 / 12	291.61 2.89	291.40 3.10 / 12	291.16 3.34 / 24	291.45 3.05 / 40	292.35 2.15 / 90		

294.50

SW 7' C.T. Vermont and Hayes

Fd. B.P. on curb S.E. Cor. Lincoln & Vermont

Hayes

1+30	Beg. curb on Lt	284.5 / 10.0 / 40 / Lg into
1+16	end wall on Rt.	
1+11	Sin. gar on Lt Cor	
1+00	℄ sin. gar on Lt	285.5 / 9.00 / 40.3 / Cor.
0+97.7	℄ 3.3 wide con. steps thru wall	
+79	24.6 Lt. P.P. P.1085	
0+75	Sin. gar cor ft.	

294.50

283.70 / 283.58 / 283.47 / 282.9 / 282.8 / 283.5 / 283.3 / 283.0 / 283.3 / 284.2 / 284.1

10.80	10.92	11.03	11.6	11.7	11.2	11.2	11.5	11.2	10.5	10.0	
34	29	24 CG	24	12		12	23	24	28	40	

285.41 / 285.10 / 284.97

8.8	9.5	4.4
39.3	39.3	39.3
End	Bot.	Top

284.76 / 284.68 / 284.55

9.74	9.82	9.95
40.2	34	29
C	wk	walk

285.42 / 285.07 / 285.0 / 284.85 / 284.6 / 285.0 / 284.9 / 284.5 / 285.0 / 285.7 / 286.5 / 286.9 / 290.1

8.98	9.13	9.5	10.0	9.9	9.5	9.6	10.0	9.5	8.8	8.0	8.6	4.4
34	29 wk	24	23	12		12	23	24	26	40	40 Bot	40 Top

286.80

7.70	
40.2	
Top	Bot. step

287.04 / 287.02 / 286.82

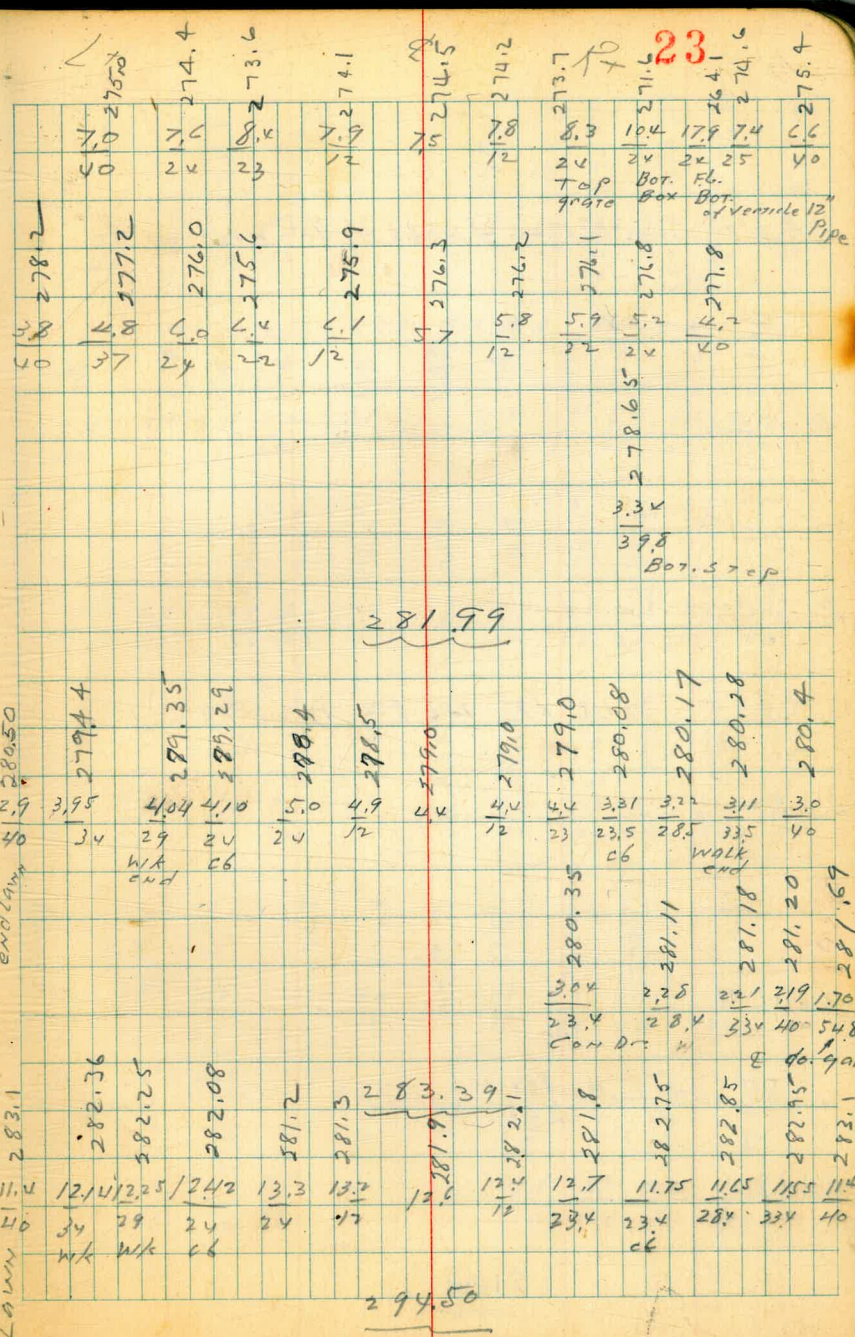
7.46	7.48	7.68
40	34	29
Cor. Floor	Sdw	Sdw

294.50

22

Hayes

2+99.8					
+80	40 Rt end Picket Fence				
2+50					
2+37.5	3' wide Con Stairs, up, On Rt				
T.P.	1.55	281.99	2.95	280.44	Scram Rain
2+06	26.7 Lt, Tel P. D 28497 P				
2+04.4 =	end of 8" curbs and walks and Beg. Picket Fence 40' Rt	(Rt + Lt)			
1+87	℄ of 16' wide drive thru curb				
T.P.	1.81	283.39	12.92	281.58	
1+54.6	Beg. c6 on Rt 0.6 out of Line				
	294.50				



Hayes

4+77 Beg. 8" Curb & Walk & Ret. Con. Wall on Rt.

T.P. 6.18 281.53 L.C.x 275.35

4+50

4

+55 26 Lt. Tel.P. D28796 P

3+50

3+16.98

55' out from Box on Sc6. 31.2 F.6. outlet of 14" Pipe

3+08.4

281.99

+64.5 Beg. 6" Con. Ret wall 30' Rt

+59 (5.5) ℄ Sing gar. and apron, 11.x wide

+53 22.6 Lt P.P. P 1015

5+50.85 = W.L. alley

5+40.85 = E.L. alley 10' 15.x/50

5+26.3 = W edge Con dr. thru curb

5+10

5+06 21.5 Lt Tel P D-28795 P

4+98.7 E edge of wide dr. thru curb

281.53

Lt ℄ Rt

4.83/30 apron 276.70; 4.52/34.5 gar. FL 277.01

5.7/30 275.8; 5.5/21 276.0; 6.0/20 275.5; 4.9 276.6; 5.0/20 276.5; 4.5/30 277.0

8.9/40 272.6; 5.6/34 275.9; 5.8/20 275.7; 5.8/21 275.7; 6.2/20 275.3; 5.6/12 275.9; 5.0 276.5; 5.1/12 276.4; 4.9/24 276.6; 4.56/24 Ret. 276.97; 4.39/40 end Ret. alley 277.14

5.30/24 dr. 276.13; 4.70/29 276.83; 4.52/34 276.91; 4.57/40 276.86; 4.50/50 gar. FL 276.93

5.7/40 275.7; 6.3/24 275.1; 6.5/21 274.9; 6.0/12 275.4; 5.5 275.9; 5.7/12 275.8; 5.52/24 Con drive 275.91; 4.68/29 276.75; 4.60/34 276.83; 4.64/40 276.79; 4.52/50 gar. FL 276.91

5.55/24 Con drive 275.88; 4.75/29 276.68; 4.68/34 276.75; 4.64/40 276.79; 4.48/50 gar. FL 276.95

281.53

Hayes

6+56 22.3 Lt P.P. T.P. 1005 P. 6653 P

6+51 Beg. 8" curb on Lt.

6+12 Beg. s'dw on Rt.

5+85.6 Beg. 8" Curb on Rt 52.2/100 Toe Slope

5+83 ℄ 3' stairs, up.

5+64.5 Beg. 6" Conc. wall Rt

T.P. 5.79 283.88 3.44 278.09
281.53

Lt ℄ Rt

	5.8/30 277.1	5.86/20 cb 278.02	6.6/20 277.3	5.8 278.1	6.1/20 277.8	5.33/20 cb 278.55	5.33/22.5 278.55	5.19/27.5 278.69	5.1/30 278.8
	7.1/30 276.8	6.8/28 277.1	6.8/20 277.1	7.5/19 276.4	6.3 277.6	6.8/20 277.1	5.96/20 277.92	5.79/22.5 278.09	5.72/27.5 walk 278.16	5.7/30 278.2
8.9/33 275.0	8.2/30 275.7	7.3/27 276.6	7.3/20 276.6	8.1/19 275.8	6.9 277.0	7.2/20 276.7	6.35/20 cb 277.53	6.2/30 277.7	

6.31/30 Bot. step 277.57

6.8/30 grd 277.1 7.1/30 Bot wl 276.8 3.95/30 Top wl 279.93

283.88

check to NWBP 10th & Johnson 4.98. 282.44 = 282.44 0.00

T.P. 5.89 287.42 2.35 281.53

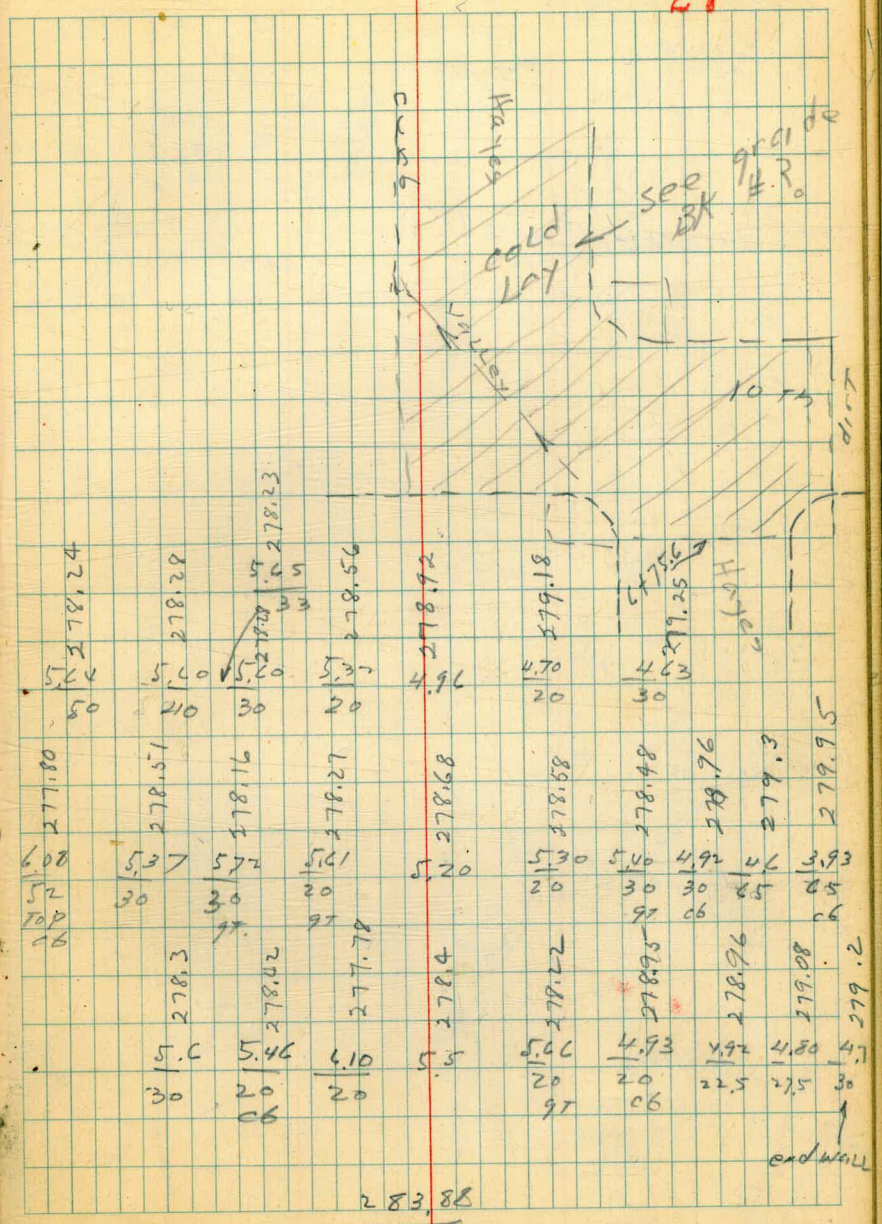
7+00.6 ℄ 10th

6+85.6 = E.6 10th

575
57
Pav.
Highes

6+75.6 = E.6. 10th Ave (Cold Lay)

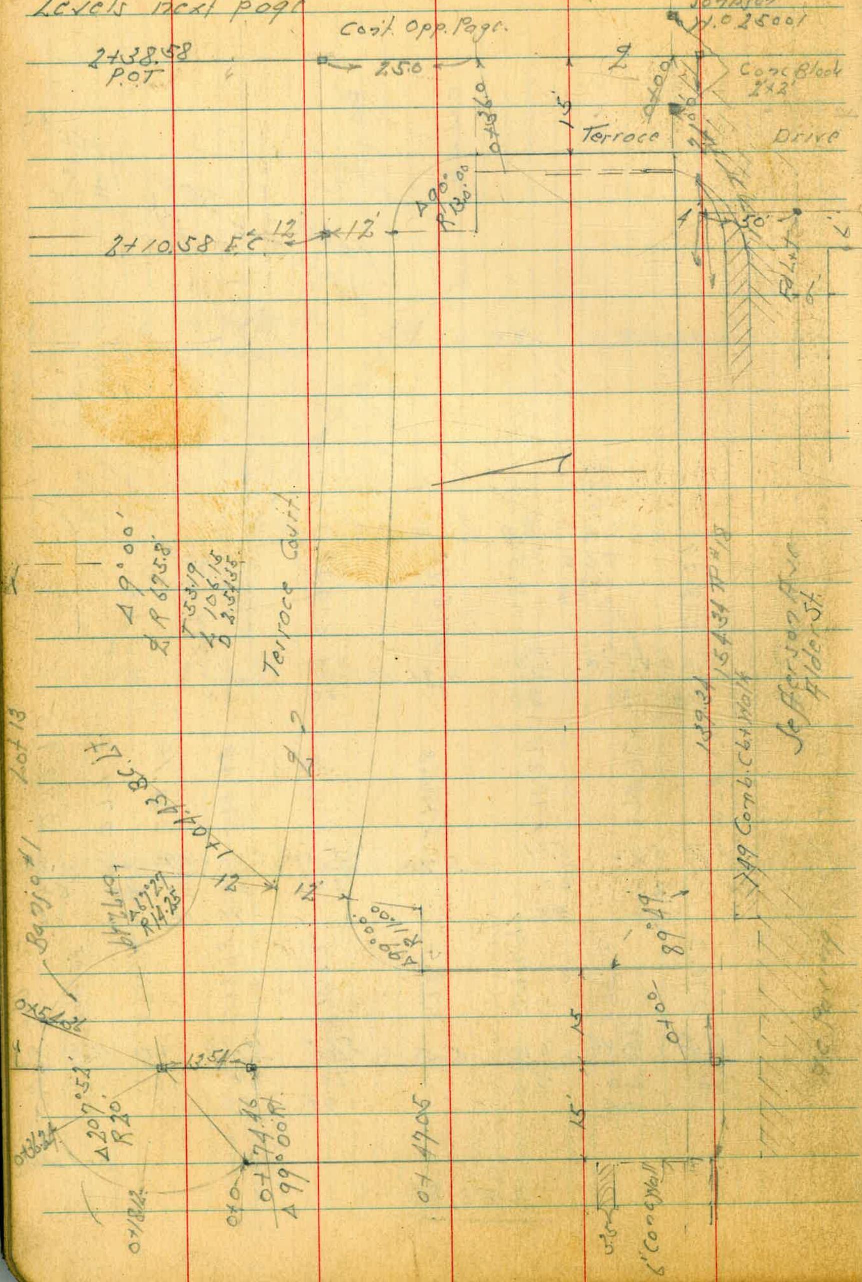
283.88



Cross Section Terrace Court

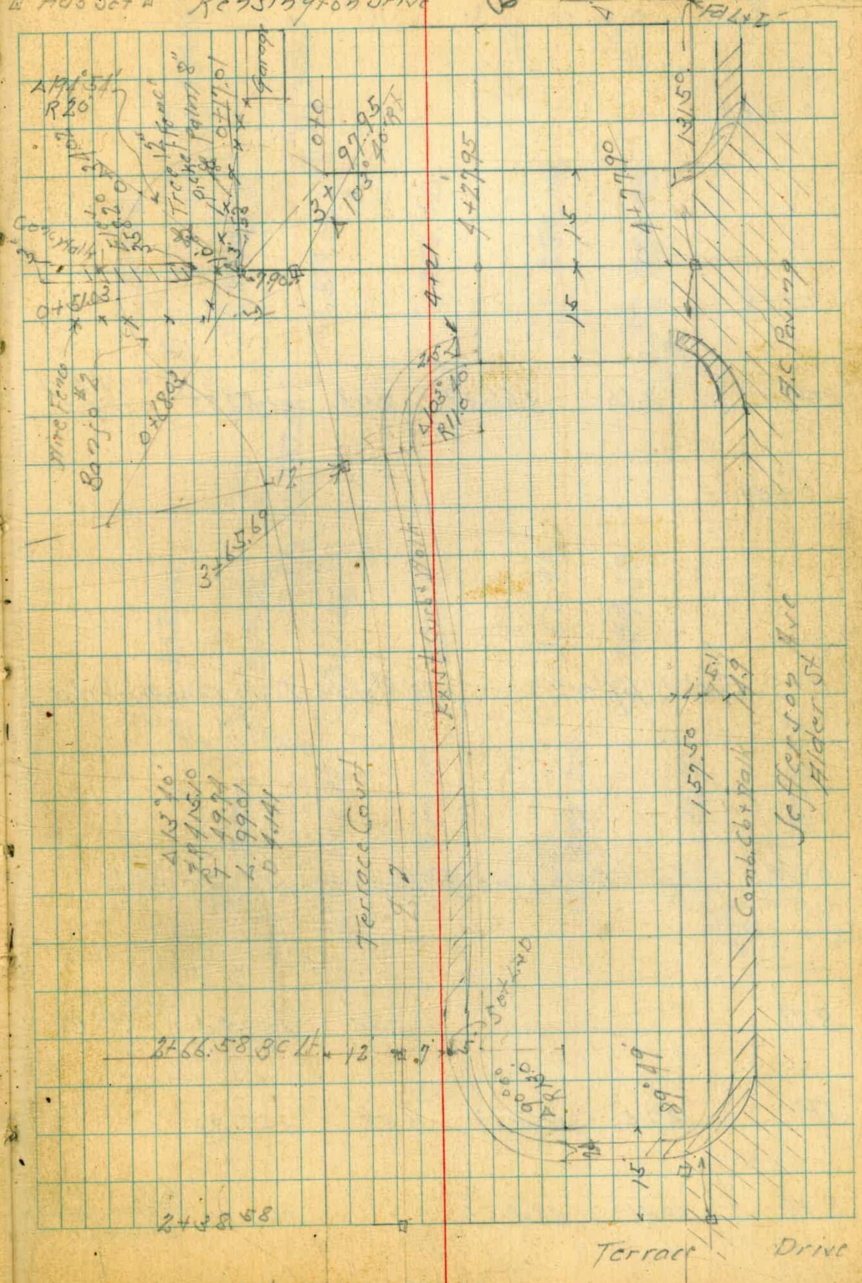
Levels next page

March 25-48
Sissig
Smith
Allen
Johnson



Indicates
Hub Set

Indexed



Brit Ford opp. Page

Cross Section Terrace Court
Jefferson Ave. to
Sketch Page 28

	B.S.	H.I.	F.S.	B.M.	
0+33					
0+18					
TP	8.66	361.38	8.96	352.72	on ℄ Hub 0-04.0'
0+07					
0+0 = N.L Jefferson			14.8 Rt of ℄ = Loose Conc Brick Wall		
0-14 = North Curb Line Jefferson = N'ly A.C. Paving					
BM			3.84	357.84	on ℄ Hub Terrace Dr.
TP	3.75	361.68	6.58	357.93	
BM	11.41	364.51		353.10	L&T So. 16' Line Adams N'y 6' Line Terrace Dr.

Lt. N. ℄ Rt. S

0+33: 6.50 / 21.8 = N'ly Do. Garage Conc Floor 354.88 — 6.59 / 15.2 = N.E'ly Conc Apron 354.79

0+18: 6.50 / 21.8 = S'ly Garage Conc Floor 354.88 — 7.02 / 15 = S.E'ly Conc Apron 354.36 — 7.2 / 12 354.08 — 6.9 354.48 — 7.3 / 12 354.08 — 6.4 / 14 = Base Loose Conc Brick Wall 354.98

361.38

8.15 / 14.9 = E'ly Conc Walk 353.53

0+0: 8.22 / 15.1 Top Conc Wall 353.36 — 9.0 / 15.1 Ground 352.68 — 9.0 / 12 352.68 — 8.5 353.18 — 8.7 / 12 352.98 — 7.1 / 16 354.58

0-14: 9.38 / 24.5 = S'ly Do. Garage Conc Floor 352.30 — 9.59 / 15 = E'ly Conc Apron 352.09 — 9.57 / 12 352.11 — 9.53 352.15 — 9.44 / 12 352.24 — 8.97 / 22.2 = Gutter Edge 352.71 — 8.66 / 22.6 = Cb. Wall End 353.02

361.68

Terrace Court

Station	Remarks	Lt			℄	Rt		
0+72.49	= P.R.C.	349.28 12.1/40	355.08 2.6/25	355.28 6.1/20				
0+51.36		345.78 15.6/40	345.78 15.6/30	352.28 9.1/25	353.98 7.4/20			
0+36.24		349.38 12.0/30	354.38 7.0/20					
0+18.12		354.78 6.6/40	355.48 5.9/20					
0+0.	Banjo #1	356.08 5.3/20			355.28 6.1			
0+71.46	Δ 99°00' Rt	356.04 5.34/14 Lt of Garage	355.28 6.1/12		355.58 5.8	356.08 5.3/12		
0+47.65	= B.C. on Rt	355.74 5.64/48 Lt SE of Garage Conc Floor	355.51 5.87/15 Lt Sh 8.5 Conc Apron	355.18 6.2/12	355.68 5.7	355.28 6.1/7	355.28 6.1/12	355.88 5.5/14 Bar Drive wall

361.38

361.38

Terrace Court

Lt. N — ℄ — Rt. S

1+71 — 11.7 Rt of ℄ = NWly Stucco Wall 8"

1+67
- 349.38 — 12.0 / 3.0
- 349.58 — 11.8 / 19
- 355.68 — 5.7 / 16
- 356.78 — 4.6 / 12
- 357.08 — 4.3
- 357.08 — 4.3 / 6
- 357.58 — 3.8 / 12
- 357.69 — 3.69 / 12.6 = NEly Conc. Apron
- 357.81 — 3.57 / 14.7 = NEly Dbl Garage Conc. Floor

1+56
- 349.58 — 11.8 / 25
- 355.58 — 5.8 / 18
- 357.09 — 4.29 / 12 on Walk
- 357.05 — 4.33 / 8.4 = SEly Conc Walk 3.5
- 356.78 — 4.6 / 8.4
- 356.58 — 4.8 / 7
- 356.98 — 4.4
- 357.28 — 4.1 / 12
- 357.69 — 3.69 / 13.5 = NWly Conc Apron
- 357.84 — 3.54 / 15.5 = Garage Floor

1+47
- 357.72 — 3.66 / 14.3 = NWly Conc Apron
- 357.82 — 3.56 / 16.2 = NWly Dbl Garage Conc Floor

1+33
- 357.63 — 3.75 / 15.8 = at Sly Stucco House 1st Floor
- 356.65 — 4.73 / 9.3 = Sly Conc Walk
- 356.48 — 4.9 / 9.3
- 356.58 — 4.8
- 356.18 — 5.2 / 6
- 356.68 — 4.7 / 11.1 = Base Dry Wall
- 357.48 — 3.9 / 12

1+14
- 356.38 — 5.00 / 12 on Walk
- 356.41 — 4.97 / 9.6 = SWly Conc Walk 3.5'
- 355.98 — 5.4 / 9.6
- 356.38 — 5.0
- 355.78 — 5.6 / 6
- 356.88 — 4.5 / 10.8 = Base Dry Wall
- 357.08 — 4.3 / 12

1+01.43 = BC Lt.
- 355.98 — 5.4 / 12
- 355.78 — 5.6 / 9 = Sly 2.1" Hedge
- 356.28 — 5.1
- 355.68 — 5.7 / 6
- 356.48 — 4.9 / 10.8 = Base Dry Wall
- 356.88 — 4.5 / 12

361.38

361.38

Terrace Court

Station			Lt			℄		Rt=5
2+66.58	BC Lt. 15.6 Lt o/℄ = Picket Fence		6.0/25 356.38	3.9/12 357.48	3.9 357.48	4.1/6 357.28	3.78 6 = Top cb 357.60	2.5/12 358.88
2+52.6		11.8/30 349.58	10.6/20 350.78	4.1/12 357.28	3.9 357.48	4.3 11 = Gutter 357.08	3.69 11 = Top cb + walk 357.69	
2+38.58	= ℄ Terrace Drive to South	11.5/30 349.88	10.6/19 350.78	4.4/12 356.98	3.9 357.48	3.7/12 357.68		
2+10.58	= EC	12.0/30 349.38	11.7/16 349.68	4.4/12 356.98	4.0 357.38	3.7/12 = Base Stucco wall 357.68		
2+02						3.52 11.6 = 2 ft ½ x 25' Conc walk 357.86		
1+84.05	12.0/30 349.38	11.8/13 349.58	4.8/13 356.58	4.7/12 356.68	4.2 357.18	3.9 11.7 = Base Stucco wall 357.48		

361.38

361.38

Terrace Court

3+84

3+65.69 = B.C. on Rt. 20.2 Lt of ℄: Wire Fence

TP 5.39 363.36 5.41 357.97

3+40.83

26.1 Lt " " Wly Wire Fence
3+37 20.1 Lt of ℄: Ely Picket Fence

3+27

3+08

24.2 Lt " " " to End
2+91.33 18.3 Lt of ℄: Picket Fence Wly

361.38

Station	Lt.			℄			Rt.		
3+84		358.14 (5.22 / 7.6: ℄ to Sly Conc. Drive)	358.36 (5.0 / 12)	358.36 (5.0)	358.26 (5.1 / 9)	358.33 (5.03 / 9: Cb)	358.56 (4.8 / 12)		
3+65.69		358.36 (5.0 / 20)	358.26 (5.1 / 12)	358.06 (5.3)	357.66 (5.7 / 5.6)	358.14 (5.22 / 5.6: Cb)	358.26 (5.1 / 8)	359.46 (3.9 / 12)	
TP				363.36					
3+40.83		358.18 (3.2 / 20)	357.98 (3.4 / 12)	357.98 (3.4)	357.48 (5.9 / 5.4)	357.94 (3.44 / 5.4: Cb)	358.08 (3.3 / 8)	359.28 (2.1 / 12)	
3+37	358.18 (3.20 / 21.7 on Drive)	358.08 (3.38 / 20.3 ℄ to Sly Rt. Rubber Conc Drive)	357.68 (3.5 / 12)	357.88 (3.5)	357.48 (5.9 / 5.2)	357.87 (3.51 / 5.4: Cb)	357.98 (3.4 / 8)	359.78 (1.6 / 12)	359.88 (1.5 / 13.8: Hly Garage So. Entrance)
3+08		358.08 (3.30 / 21.7 ℄ to Sly Conc Walk Landing)	357.78 (3.6 / 12)	357.58 (3.8)	357.18 (4.2 / 5.2)	357.70 (3.68 / 5.5: Cb)	357.88 (3.5 / 8)	358.88 (2.5 / 12)	359.88 (2.5 / 13.3 Hly Garage So. Entrance)
2+91.33		357.48 (3.9)	357.58 (3.8 / 12)	357.58 (3.8)	357.28 (4.1 / 5.8)	357.60 (3.78 / 5.8: Cb)	357.88 (3.5 / 8.5)	358.78 (2.6 / 12)	

361.38

Terrace Court

3797.95 Taken 90° From South

0768.03 = P.R.C.

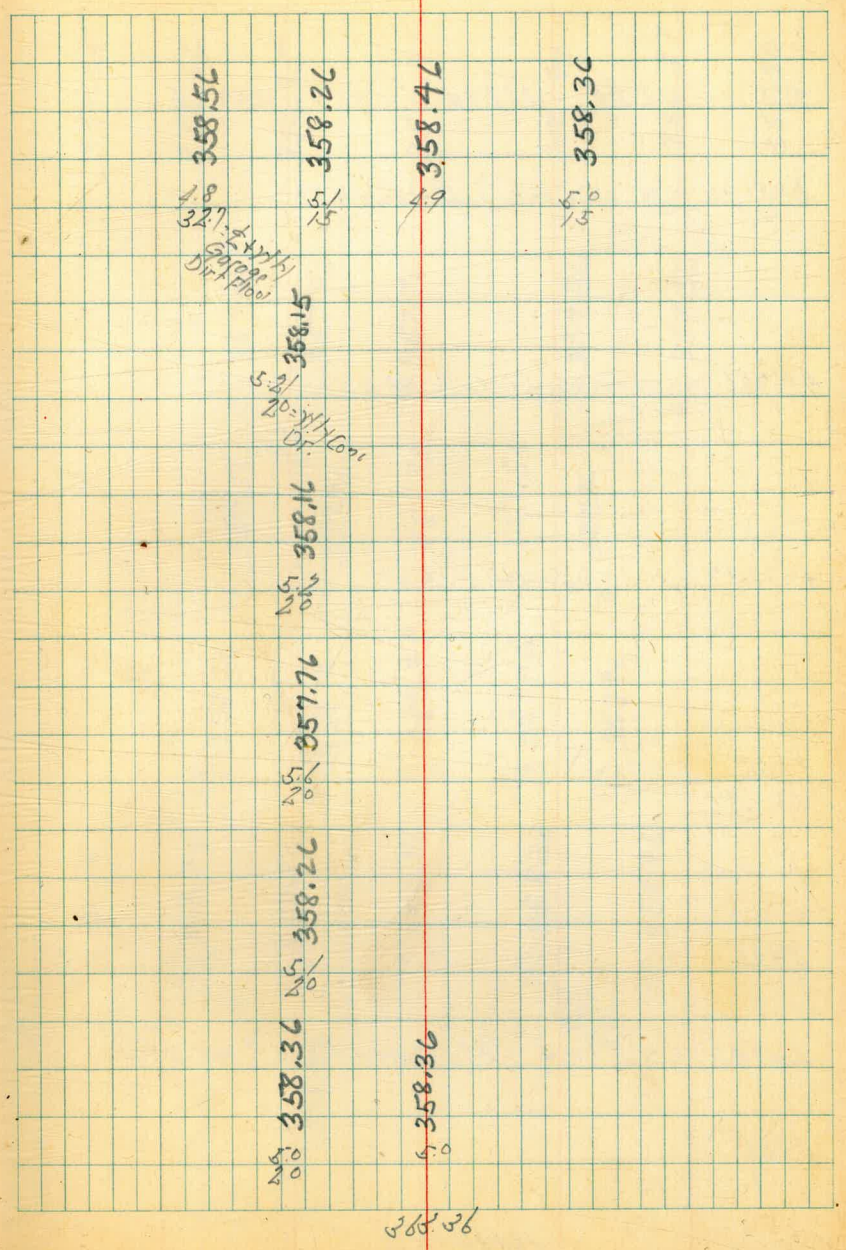
0751.03

0734.03

0717.01

076 Banjo #2

360.36



Terrace Court

TP	5.29	362.94	5.71	357.65
4+91.90 = N cb Line Jefferson Ave				
4+78.6 = Nly Curb + Walk Rt + Lt				
4+77.90 = N.L. Jefferson Ave				
4+62				
4+21				
4+19	7' Rt of ℄ = Ely Power Pole # P.A 4811			
4+06				

363.36

Lt = E ℄ Rt = W

Station	Readings (Lt to Rt)
4+91.90	357.05 (6.31, 22.2 = Cb); 356.66 (6.70, 22.5 = Gutter); 356.75 (6.61, 12); 356.91 (6.45); 356.91 (6.45, 12); 356.97 (6.39, 19.5 = Gutter); 357.30 (6.06, 19.5 = Cb)
4+78.6	357.49 (5.87, 12.8 = Nly Cb Also Gutter); 357.76 (5.6, 6); 357.76 (5.6); 357.36 (5.97, 8 = Nly Cb Also Gutter); 357.56 (5.8, 15)
4+77.90	357.56 (5.8, 15); 357.76 (5.6, 7); 357.76 (5.6); 357.56 (5.8, 9); 358.16 (5.2, 15)
4+62	358.26 (5.1, 15); 358.46 (4.9, 8); 358.36 (5.0); 358.16 (5.2, 7); 358.96 (4.4, 15)
4+21	358.78 (4.58, 18 = S Ly Do. Garage Conc Floor); 358.31 (5.05, 15.7 = S Ly Conc Apron); 358.36 (5.0, 15); 358.56 (4.8); 358.38 (4.98, 8.2 = S Ly Conc Cb + Walk); 358.86 (4.5, 15)
4+06	358.73 (4.63, 17.8 = N Ly Do. Garage Conc Floor); 358.42 (4.94, 15.8 = N Ly Conc Apron)

363.36

Cross Section Terrace Drive
Jefferson Ave to Terrace Court

BM			7.62	358.51	SE 6" PLCT. Adams & Edgemore Rd. 358.50
TP	3.51	366.13	2.10	362.62	
TP	11.61	364.72	11.20	353.11	SW Lt & Adams & Terrace Dr. 353.10
TP	5.41	364.31	4.04	358.90	
0+36 = B.C. Rt & Lt.					
0+18					
0+0 = N.L. Jefferson Ave					
0-14 = North Curb Line Jefferson					

362.94

Indexed

Lt = W | 2 | Rt = E

Station									
0+36			357.94 (5.0 / 15.3 = Base Stucco Wall)	357.84 (5.1 / 12)	357.79 (5.2)	357.24 (5.7 / 8)	357.67 (5.27 / 8 = Cb)	358.24 (4.7 / 15)	
0+18		358.41 (4.53 / 15.2 = Hi Cb & Stucco Wall)	357.89 (5.1 / 15.2)	357.79 (5.2 / 12)	357.74 (5.2)	357.34 (5.6 / 8 = Gutter)	357.82 (5.12 / 8 = Cb)	358.14 (4.8 / 15)	
0+0	358.15 (4.99 / 15 = Cb)	357.84 (5.1 / 15.1 = Gutter)	357.64 (5.3 / 12)	357.88 (5.06 / 7.2 = Lt & Top Conc Block)	357.94 (5.0)	357.86 (5.07 / 6.9 = Rt & Top Conc Block)	357.55 (5.39 / 8 = Gutter)	357.89 (5.05 / 8 = Cb)	358.34 (4.6 / 15)
0-14		357.91 (5.03 / 22.7 = Cb)	357.60 (5.34 / 22.7 = Gutter)	357.71 (5.23 / 12)	357.86 (5.08)	357.63 (5.31 / 12)	357.48 (5.46 / 19.7 = Gutter)	357.85 (5.09 / 19.7 = Cb)	

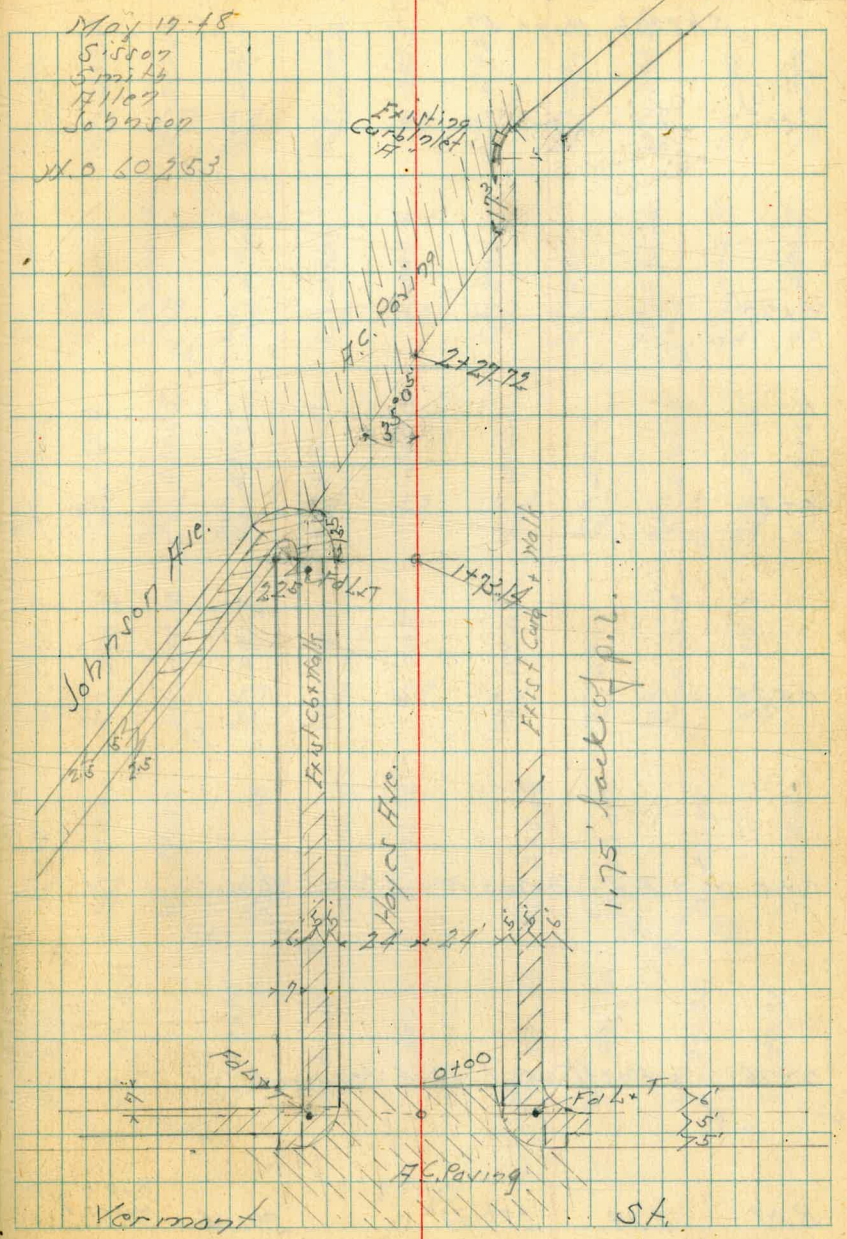
362.94

Cross Section Hayes Ave
Vermont St to Johnson Ave.
Levels next page

297.43 ∧ Bl. Ford Page 38

TP	5.68	297.25	5.86	291.57	
BM			4.40	292.85	SE BP Lincoln & Vermont 292.84 Page 21

INDEXED
MAY 18 1948



Cross Section Hayes Ave
Vermont St to Johnson Ave.
Sketch Page 37

1+0					
0+75					
0+50					
0+25					
0+0	= E.L. Vermont = Ely A.C. Paving				
0-16	= East Curb Line of Vermont				
BM	6.29	297.43		291.14	SW n' LAT Hayes + Vermont Page 21

L = H ℄ Rt = 5

Sta.	40	34	24 Cb	24	12	℄	12	24	24 Cb	34	40
1+0	1.0/40 296.9	4.6/34 292.8	4.87/24 = Cb 292.56	5.4/24 292.0	5.3/12 292.2	4.9 292.5	5.1/12 292.3	5.4/24 292.0	4.86/24 = Cb 292.57	4.7/34 292.7	2.8/40 294.6
0+75	1.6/40 295.8	4.8/34 291.6	4.99/24 = Cb 292.44	5.6/24 291.8	5.3/12 292.1	5.0 292.4	5.3/12 292.1	5.5/24 291.9	5.07/24 = Cb 292.36	4.9/34 292.5	2.9/40 294.5
0+50	1.8/40 295.6	5.0/34 292.4	5.18/24 = Cb 292.25	5.8/24 291.6	5.4/12 292.0	5.2 292.2	5.4/12 292.0	5.7/24 291.7	5.18/24 = Cb 292.25	4.9/34 292.5	3.0/40 294.4
0+25	2.2/40 295.2	5.1/34 292.3	5.30/24 = Cb 292.13	5.7/24 291.7	5.4/12 292.0	5.3 292.1	5.4/12 292.0	5.8/24 291.6	5.34/24 = Cb 292.09	4.5/40 292.9	
0+0	2.4/40 295.0	5.2/34 292.2	5.46/24 = Cb. 291.97	5.75/24 = Gutter 291.68	5.28/12 292.15	5.09 292.34	5.38/12 292.05	5.98/24 = Gutter 291.45	5.44/24 = Cb. 291.99		4.6/40 292.8
0-16	5.43/40 = Curb 292.00	6.01/40 = Gutter 291.42		5.98/24 291.45	5.55/12 291.88	5.42 292.01	5.60/12 291.83	6.03/24 291.40	6.10/40 = Gutter 291.33		5.51/40 = Curb 291.92

297.43

Hayes Ave.

Curb Inlet "A" on Right

2+27.72 = Wly AC Paving on Johnson Ave Taken on Bsl Line

2+27.72 Taken 90°

2+0

1+73.14 = Curb BC on Lt.

1+50

1+25

29743

Lt. Rt

29743

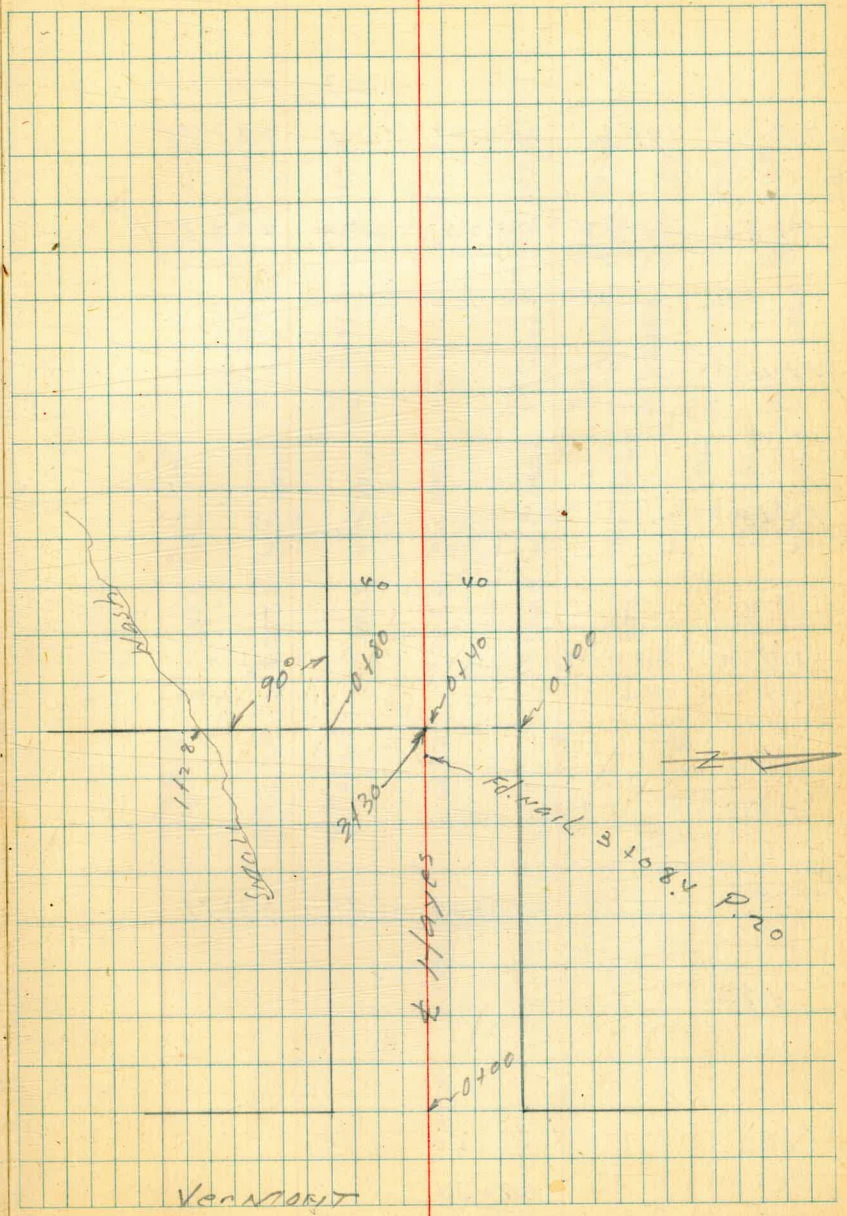
Levels Proposed drain on Hayes West of Vermont

Moore Bragg Shannon Bunch

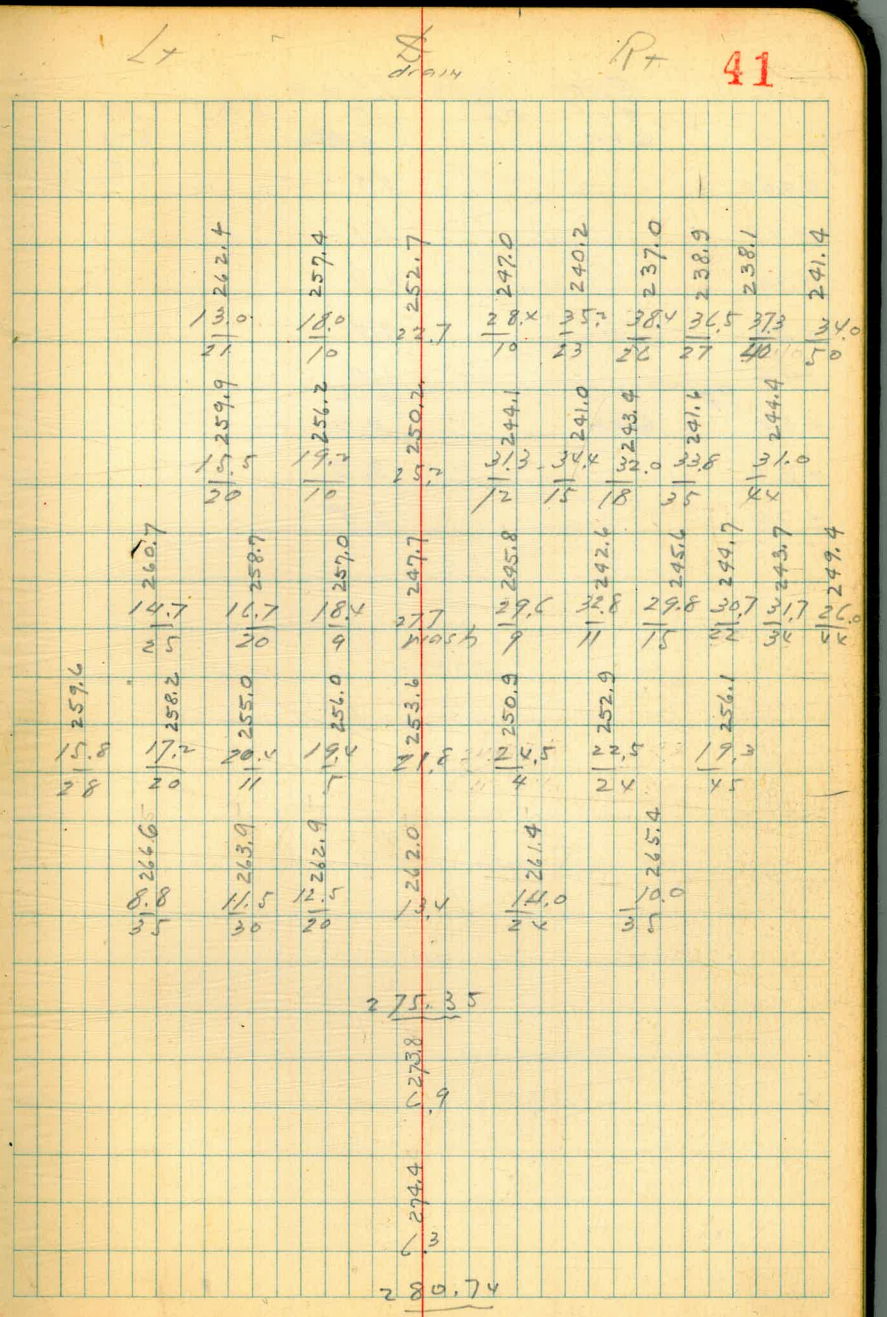
6-22-x8. W.O. 60138

			274.3	
+68			6.4	
			273.3	
+63			7.4	
			274.1	
0+40	E Hayes		6.6	
			274.1	
+17			6.6	
			275.2	
+14			5.5	
			275.1	
0+00	N.L. Hayes		5.6	
T.P.	1.58	280.74	1.303	279.16
B.M. S.W.T. Hayes & Vermont P.21	1.05	292.19		291.14

Indexed C.S.K.



			1.23	291.14
T.P.	9.63	292.37	0.19	282.74
1+60	9.62	28.293	2.04	273.31
1+40				
1+28				
1+10				
1+00				
T.P.	1.56	275.35	6.95	273.79
+82				
0+80				
		280.74		

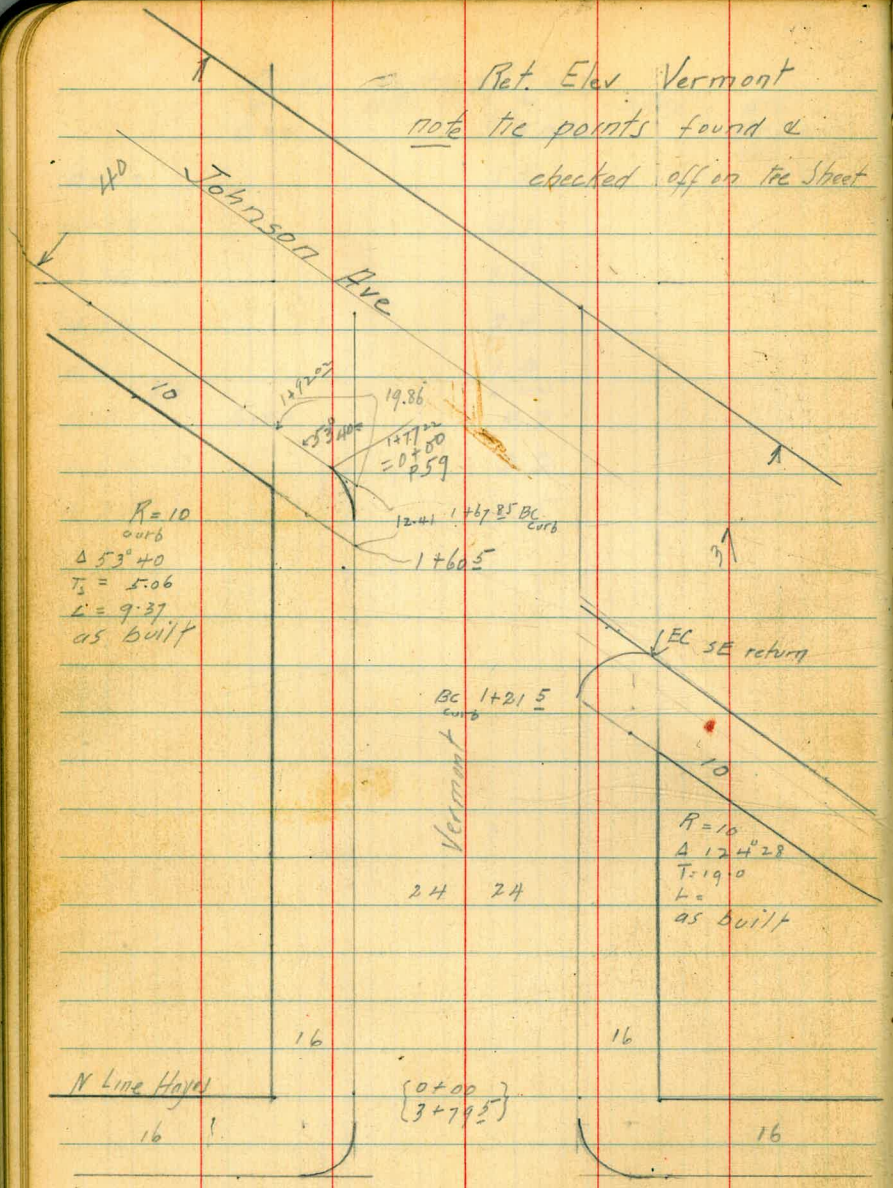


Alley North of Hayes

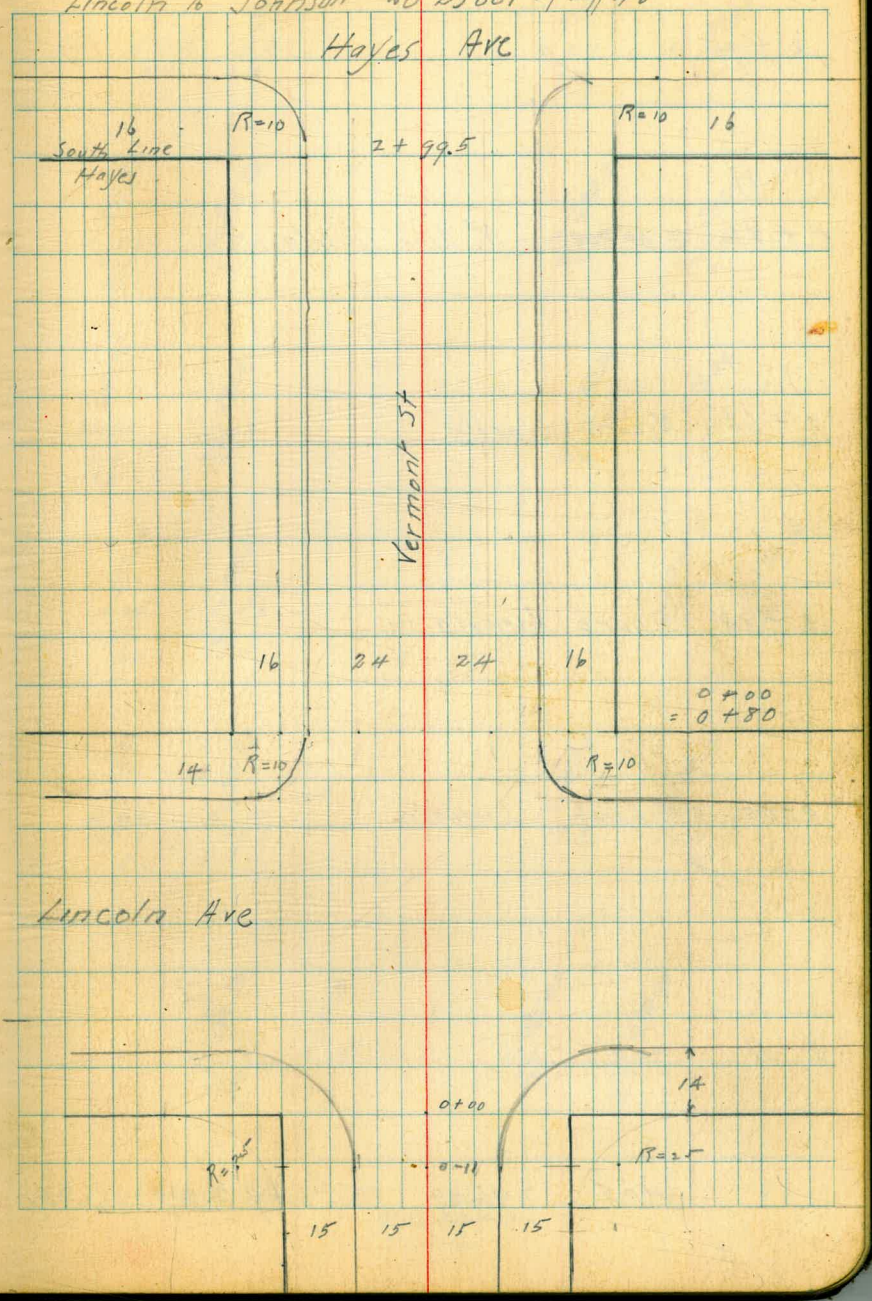
	+	HI	-	Elev	BM
	6.00		℄ Alley		Ecb Alley N of Hayes
0+00			5.5		
0+10			5.1		
+26			4.7		
+30			2.4		
+40			1.0		
+50 TP	6.00		0.00 5.7		
+60			3.7		
+70			3.5		

Ref. Elev. Vermont

note tie points found & checked off on the Sheet



Lincoln to Johnson WO 25001 6/29/48



0+95			
0+80	= 00+00	N. Line Lincoln	
0+66	N curb	Lincoln	
0+54	S. curb	Lincoln	
0+00	S. Line	Lincoln	
0-11			
	405	296.89	292.84

Lt

291.68 — 5.21 — 24 — cb

291.28 — 5.61 — 24

291.97 — 4.92 — 24 — cb

291.57 — 5.32 — 24

291.98 — 4.90 — 40 — cb

291.41 — 5.48 — 40

292.04 — 4.85 — 40 — cb

291.37 — 5.52 — 40

292.26 — 4.63 — 19.9 — cb

291.79 — 5.10 — 19.9

292.30 — 4.59 — 15 — cb

291.74 — 5.15

Rt

292.02 — 4.87 — 24

292.65 — 4.24 — 24 — cb

292.24 — 4.65 — 24

292.89 — 3.92 — 24 — c

292.34 — 4.55 — 40

293.04 — 3.85 — 40 — cb

292.18 — 4.71 — 40

292.76 — 4.13 — 40 — cb

292.29 — 4.60 — 19.9

292.96 — 3.93 — 19.9 — cb

292.24 — 4.65 — 15

292.80 — 4.09 — 15 — cb

BP Lincoln & Vermont SE

296.89

0+00

3.795 N Line Hayes

3

+63.5 N curb Hayes

3+155

3+995 S Line Hayes

BM 650 297.64 5-75 291.14 291.14

2+00

296.89

290.98 290.44 291.48 292.03
6.66 7.20 6.16 5.61
CB 24 24 CB

290.94 290.22 291.71 291.99
6.70 7.42 5.93 5.65
40 40 40 CB
CB

290.99 290.27 291.69 292.01
6.65 7.37 6.15 5.63
40 40 40 CB
CB

291.00 290.53 291.55 291.94
6.64 7.09 6.29 5.70
24 24 24 CB
CB

297.64

BM SW 7' Tack Vermont & Hayes

291.31 290.84 291.69 292.30
5.58 6.05 5.20 4.59
24 24 24 24
CB CB

296.89

EC 1+77.22

1+67.85 BC on Left

1+60.5 S Line Johnson

EC on right Hays & Johnson SE return

1+21.5 BC of curb on Right

0+95

397.64

292.99
4.65
CB

292.34
5.30

See P61

292.97
4.67
24
CB

292.49
5.13
24

292.96
4.69
24
CB

292.49
5.13
24

293.39
4.37

293.99
3.65
CB

293.24
4.40
24

293.95
3.69
24
CB

292.18
5.46
24
CB

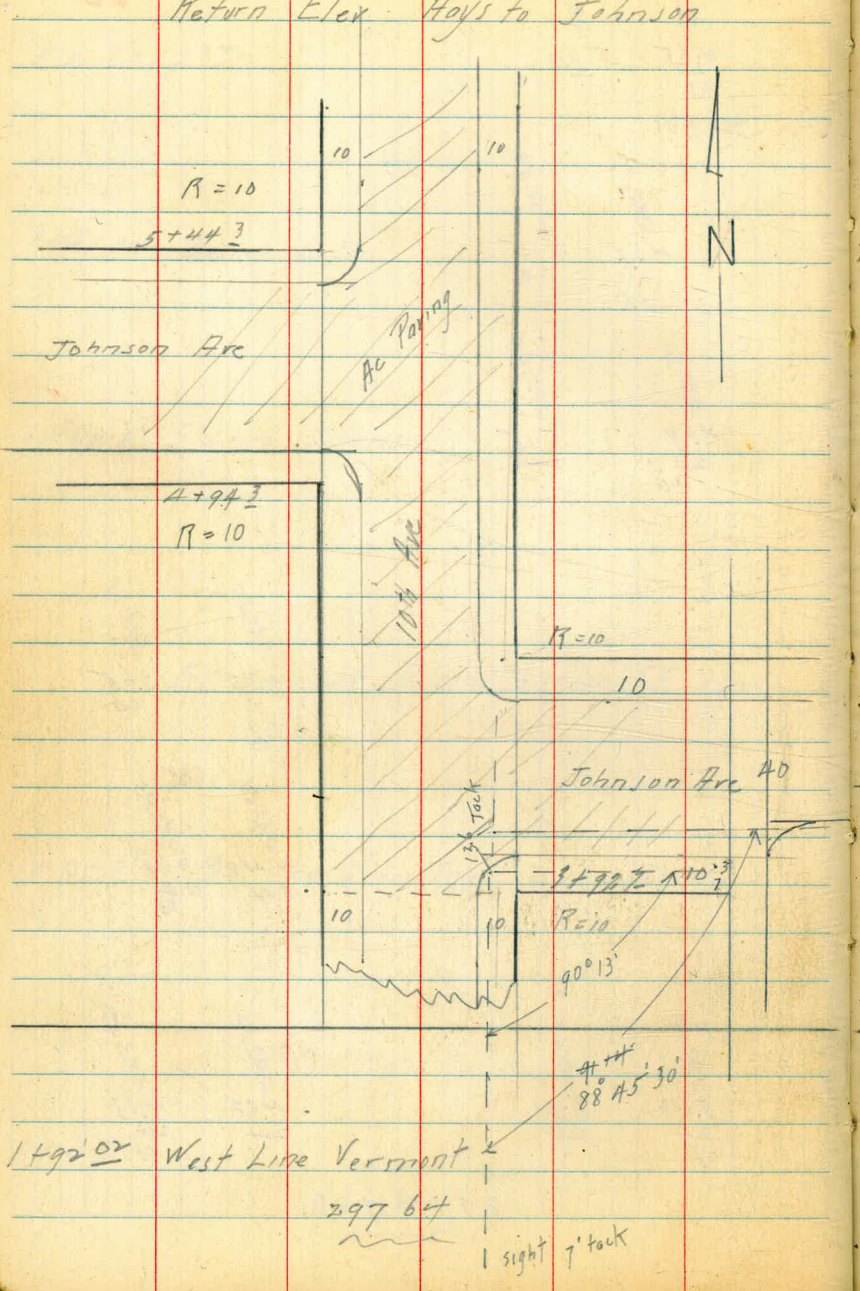
291.63
6.01
24

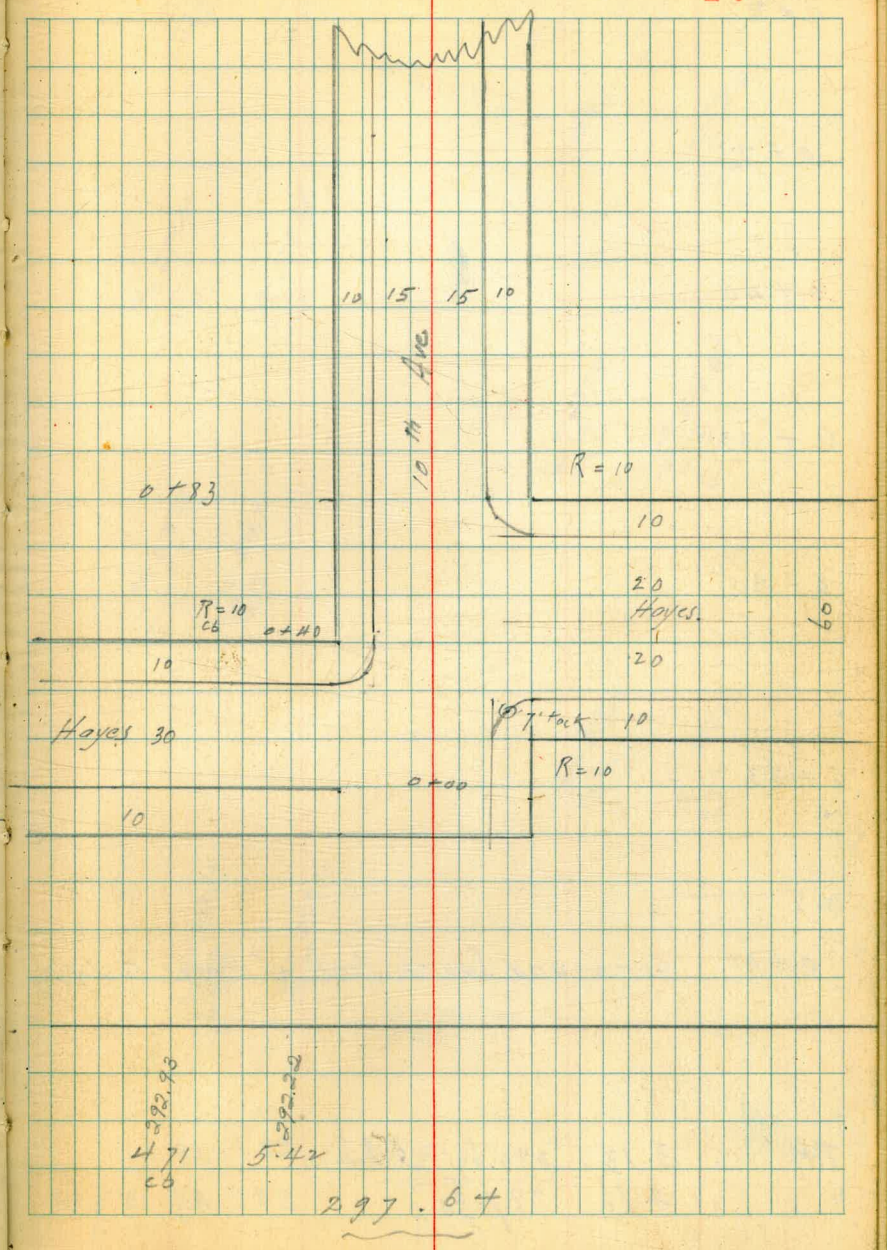
292.82
4.32
24

293.51
4.13
24
CB

297.64

Return Elec Hoys to Johnson





0+83				
0+73				
0+40				
0+33				
0+30				
0+23				
0+00	Curb end S. curb line of Hayes to Left			
T.P.	3.13	284.61	5.88	281.48
	4.86	287.30		282.44

279.78
4.83
15

279.2
5.4
15

278.5
6.1
15

278.97
5.64
15
cb

278.2
6.4
25
inl

278.97
5.64
25
cb

279.01
5.60
15
cb

278.58
6.03
15

277.91
6.70
25

278.49
6.14
25
cb

278.94
6.67
25
cb

278.28
6.33
25

278.16
6.45
15

278.52
6.09
15
cb

278.39
6.22
25
cb
end

277.81
6.80
25

284.61

see p 21

+75					
2+57					
+25					
2+00					
1+75					
T.P.	6.83	288.25	3.19	281.42	
1+46					
		284.61			

282.04 6.21 15 cb	281.6 6.7 15		282.1 6.2 15	282.63 5.62 15 cb
282.00 6.25 15 cb	281.4 6.9 15		281.75 6.50 15	282.47 5.78 15 cb
281.71 6.54 15 cb	281.2 7.1 15		281.6 6.7 15	282.00 6.25 15 cb
281.43 6.82 15 cb	281.0 7.3 15		281.1 7.2 15	281.64 6.61 15 cb
281.17 7.08 15 cb	280.6 7.7 15		280.8 7.5 15	281.28 6.97 15 cb
		288.25		
280.87 3.74 15 cb	280.1 4.5 15		280.2 4.4 15	280.75 3.86 15 cb
		284.61		

5+043 Curb line Johnson to W

4+943 BC Left 5 Line Johnson to W.

4+537 Ec North line Johnson to E

4+427

4.027

BM 4.90 287.34 5.81 282.44 282.44 00

3+927 BC on Right 5 Line Johnson to E

300

281.49 5.87 25 Cb

280.87 6.47 25

281.51 5.83 15 Cb

281.05 6.29 15

Check

281.91 5.43 15

282.49 4.85 15 Cb

281.97 5.37 25

282.56 4.78 25 Cb

X 15 Cb

15

282.86 4.48 25

283.45 3.89 25 Cb

282.46 5.79 15 Cb

281.99 6.26 15 Por

287.34

282.83 5.42 15 Por

283.50 4.75 15

283.12 6.13 15 Cb

281.8 6.5

282.4 5.9

282.85 5.40 15 Cb

BM 4.90 382.44

5+443 W Line of Johnson to W

5+343 N curb line Johnson to W.

387.34

NW BP 10th & Johnson p 27

382.47 381.95 382.39 281.90

4.87 5.39 4.95 5.44

1.5 1.5 1.5 1.5

66

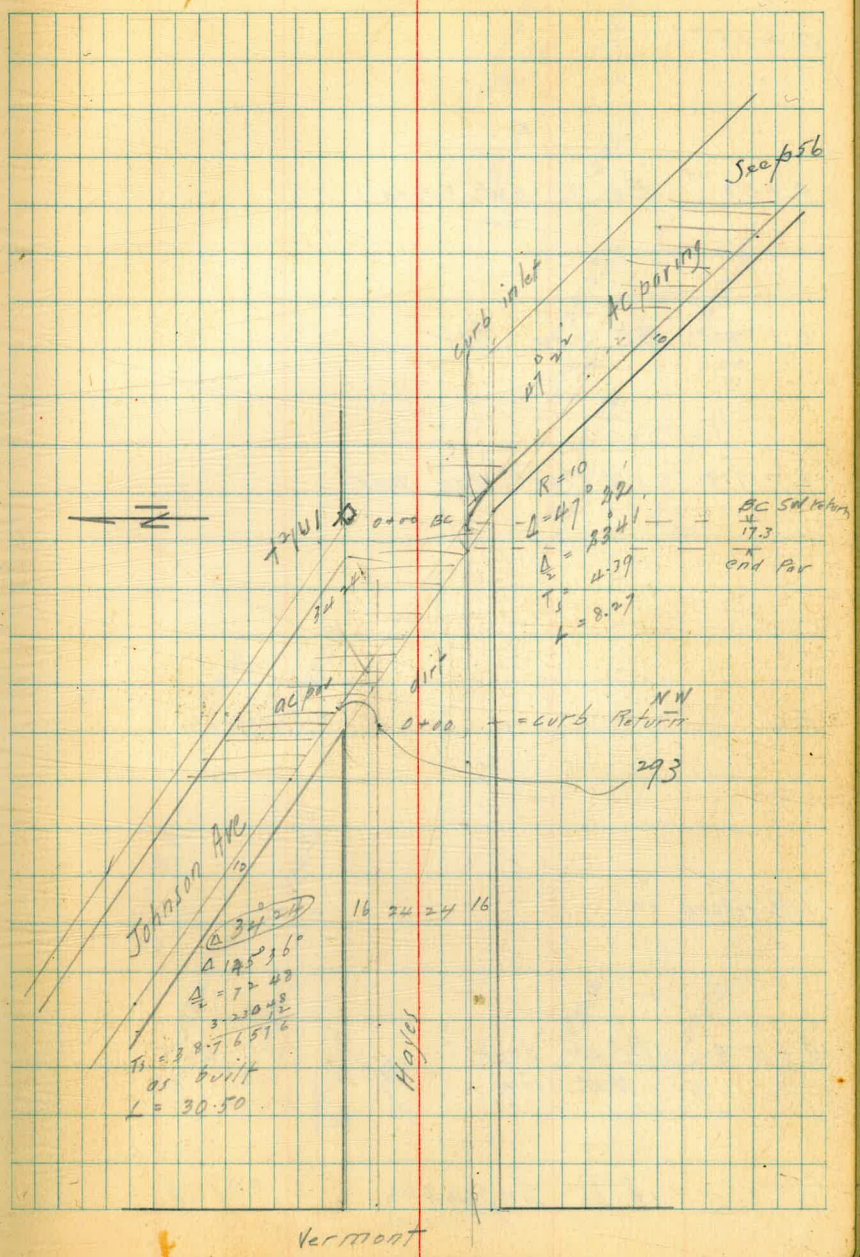
382.43 281.77

4.91 5.57

2.5 2.5

387 34

Curb Elev Johnson & Hays at returns



0+18.27

0+08.27 EC SW Return

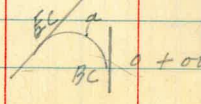
0+00 BC on Right

0-17.3 on right beg par

EC

1/2 return = a

0+00 BC on Left
NW return



6 30 297.44 891.14

291.24
6.20
par

292.08
5.36
cb

291.14
6.30
par

292.14
5.30
cb

291.23
6.21
24

292.15
5.19
24
cb

291.52
5.92
24
par

292.17
5.27
24
cb

293.00
4.44
24

292.57
5.17

292.97
4.47
cb

293.35
5.09

293.00
4.44
24

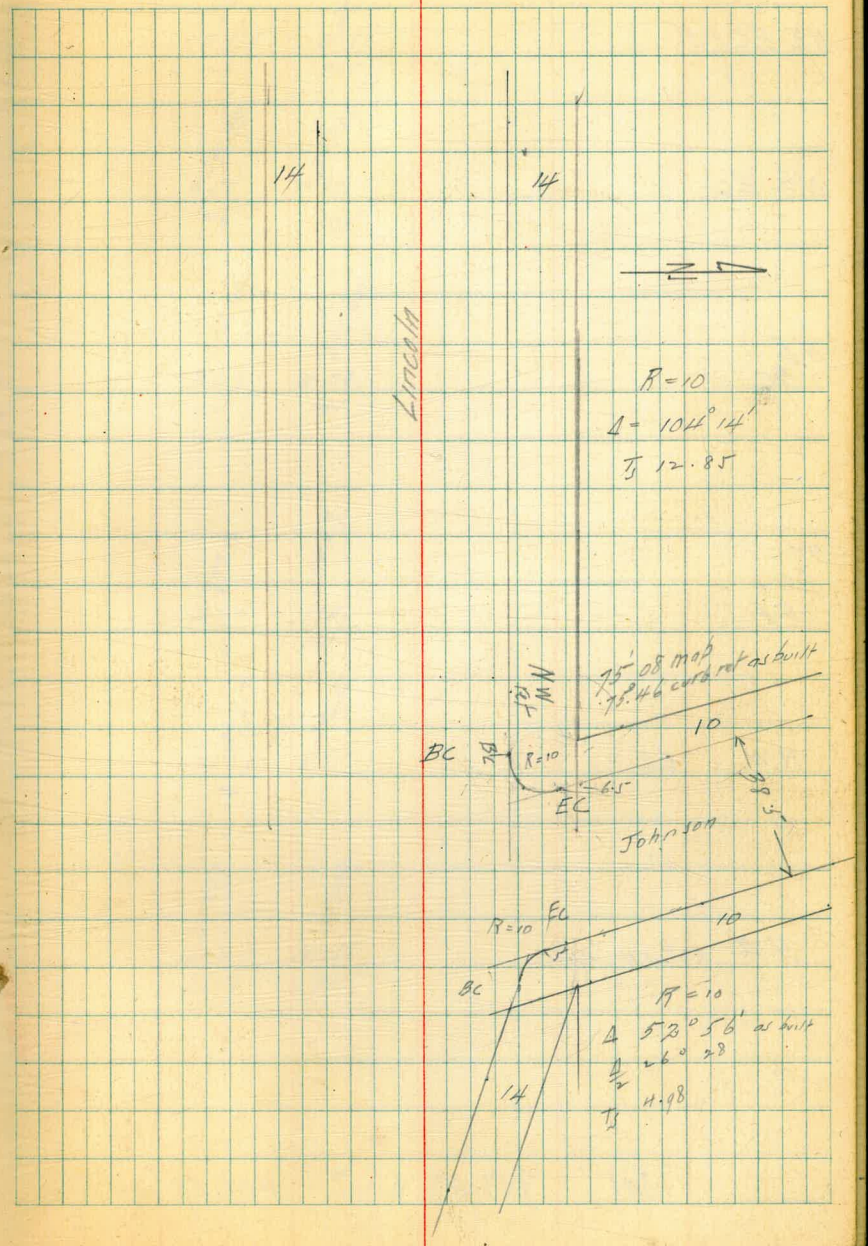
292.1
5.3
24

292.2
5.2
24

293.01
4.43
cb

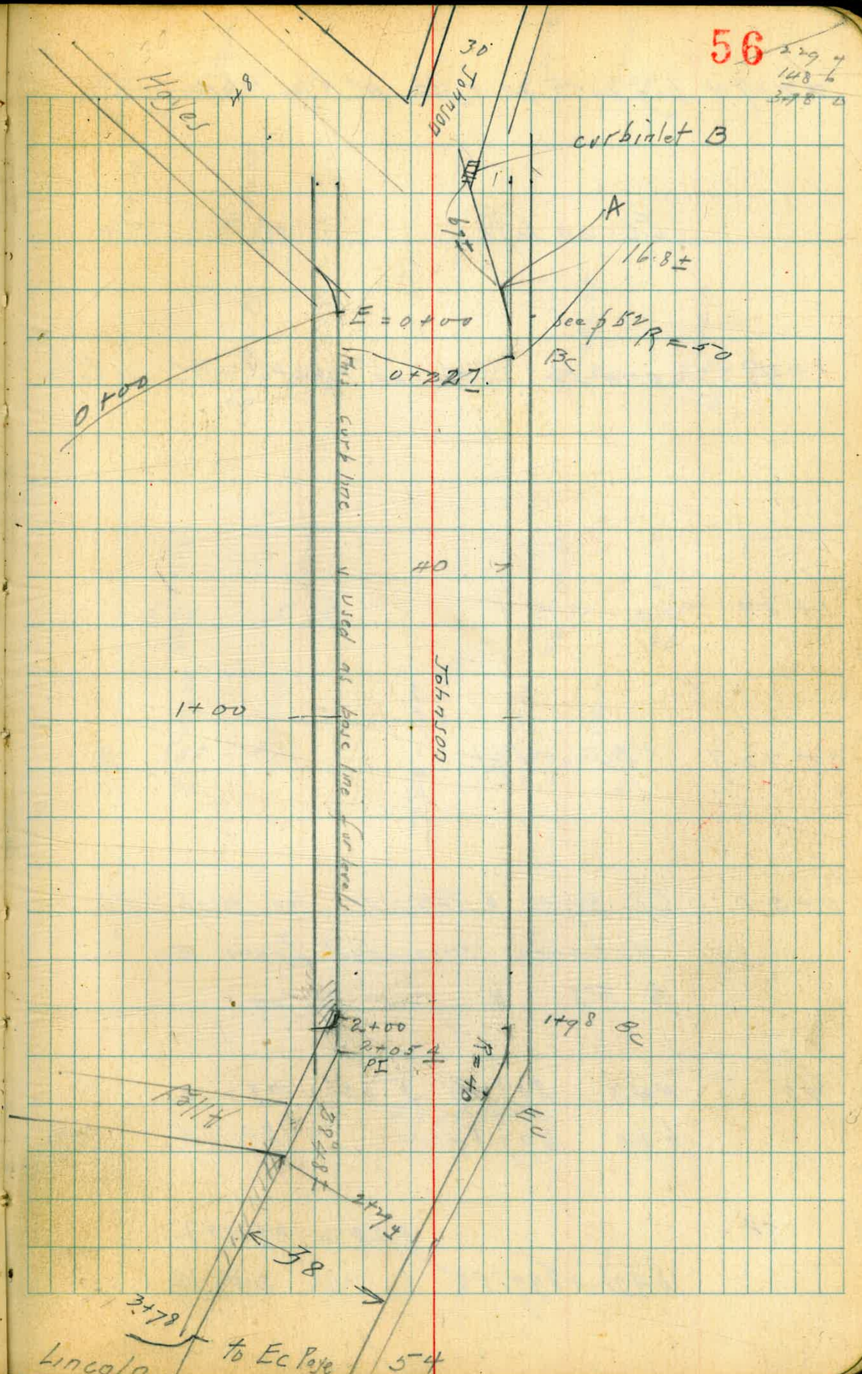
297.44

Elev returns Lincoln & Johnson



NE EC+5				297.93 3.55 cb	297.17 4.31 Pav
NE EC				297.95 3.53 cb	297.21 4.27 Pav
N.E BC				298.00 3.48 cb	297.40 4.08 Pav
NW EC+ 6.5				297.11 4.37 cb	296.69 4.79 Pav
N.W. EC				297.17 4.31 cb	296.81 4.67
N.W. return BC				297.39 4.09 curb	297.00 4.48 Pav
	3.91	301.48		297.57	

Lincoln & Johnson Tack N W 9.21


229.4
148.6
378.0
Hayes
30'
Johnson
curb inlet B
A
16.8±
E = 0+00
see p 52
R = 50
BC
0+22.7
0+00
this curb line used as base line for levels
40
Johnson
1+00
2+00
2+05±
PI
1+98 BC
R = 40
EC
38
3+78
to EC Page 54
Lincoln

2+29.4 beg curb on right at Alley return

EC on left

1+98 end of curb on right BC on Left

1+00

0+22.7 BC on Left.

0+00 EC Hayes & Johnson see map p56
distances measured from EC
to PI & from PI on.

T.P.	4.43	296.55	5.62	292.12
	6.60	297.74		291.14
TP			~~5.49~~	~~292.07~~
	6.42	297.56		291.14

4.56 Cb (291.99)	5.15 (291.40)		3.79 (292.76)	3.08 (293.47)
4.71 (291.84)	5.30 (291.25)			
4.70 Cb (291.85)	5.35 (291.20)		4.30 (292.25)	3.51 Cb (293.04)
5.09 Cb (291.46)	5.70 (290.85)		4.71 g (291.84)	4.05 Cb (292.50)
BC 5.30 Cb (291.25)	5.90 (290.65)	Johnson	5.19 (291.36)	4.51 Cb (292.04)

BM 296.55

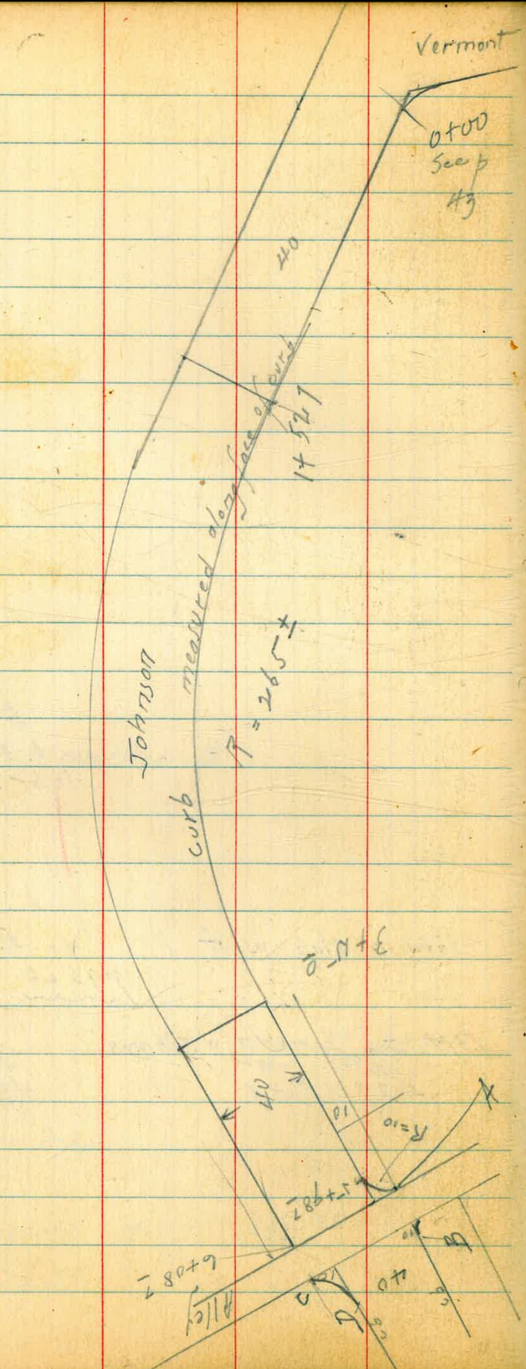
BM Vermont & Hayes p45
T.tack

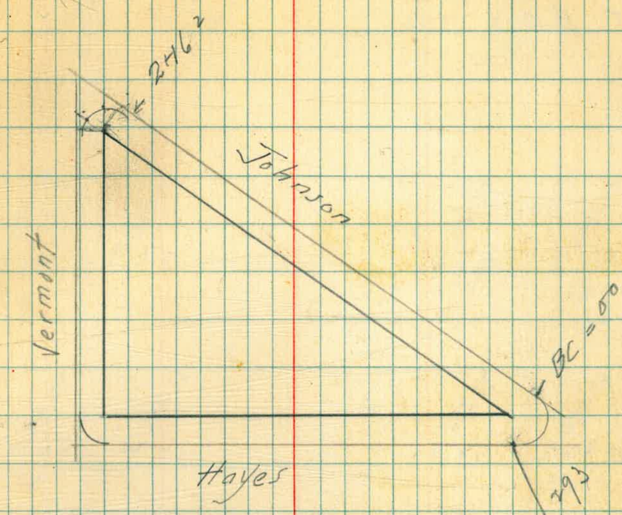
+67	curb inlet marked B				
T.P.	4.14	296.26			292.12
			2.83	297.57	297.57
100	from PI	see map			
	8.02	300.40	4.17	292.38	
		296.55			

289.96
6.30 inlet B
291.01
5.25 CB

show in Map as A
290.60
5.66
291.21
5.05
29626

BM tack Lincoln & Johnson
295.53
4.87
295.91
5.49
295.68
4.92
296.22
4.18 CB





293.00 curb at 00 p 52
3.99
296.99 HI (2+16²

2+16²	293.96 / 303 cb	293.25 / 374	292.29 / 470	293.00 / 399 cb
150	293.65 / 334 cb	292.94 / 405	291.89 / 510	292.60 / 439 cb
1+00	293.47 / 352 cb	292.72 / 427	291.49 / 550	292.19 / 480 cb
+50	293.26 / 373 cb	292.53 / 446	291.13 / 586	291.84 / 515 cb
0+00 Hayes & Johnson	292.99 / 400 cb	292.27 / 472	290.78 / 621	291.44 / 555

H.I. 296.99

3+15 EC

3+00

2+00

BC 1+52 L

1+00

0+00

2.48 295.47 292.99

290.41 5.06 CL 289.69 5.78

290.53 4.94 CL 289.84 5.63

291.39 4.08 CL 290.76 4.71

291.82 3.65 291.15 4.32

292.31 3.16 CL 291.56 3.91

292.99 2.48 CL

EC 4+77.22 / 6.46

Johnson

288.64 6.83 289.25 6.22 CL

288.78 6.69 289.39 6.08 CL

289.79 5.68 290.39 5.08 CL

290.29 5.18 290.83 4.64 CL

290.73 4.74 291.42 4.05 CL

291.67 3.80 292.27 3.20 CL

		H			
C					
B					
6+087					
5+987					
TP	2.34	290.19	7.62	287.85	
5+00					
4+00					
		295.47			

3.91 (286.28) C · 3.62 (286.57) C
See map

2.60 (287.59) B · 3.21 (286.98) B
See map

3.10 (288.09) A See map · 2.69 (287.50) gutter A · 3.79 (286.40) · 3.08 (287.11)

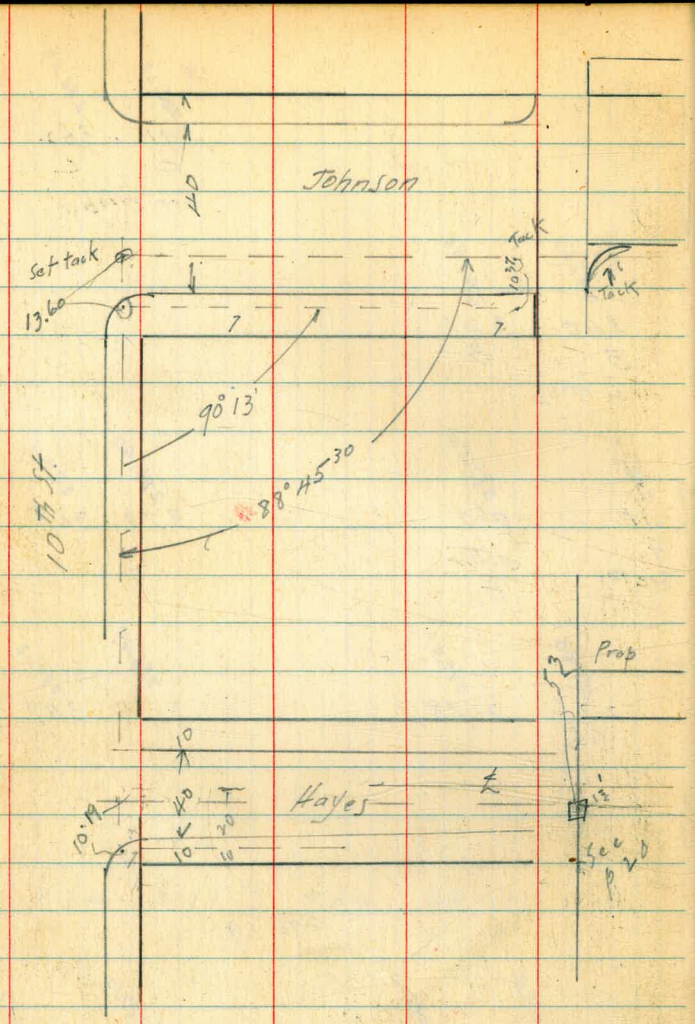
2.16 (288.03) cb · 2.78 (287.41) · 3.70 (286.49) · 3.07 (287.12)

290.19

6.66 (288.81) cb · 7.34 (288.13) · 8.35 (287.12) cb · 7.82 (287.65) cb

5.82 (289.65) cb · 6.47 (289.00) · 7.52 (287.95) · 7.06 (288.41) cb

295.47

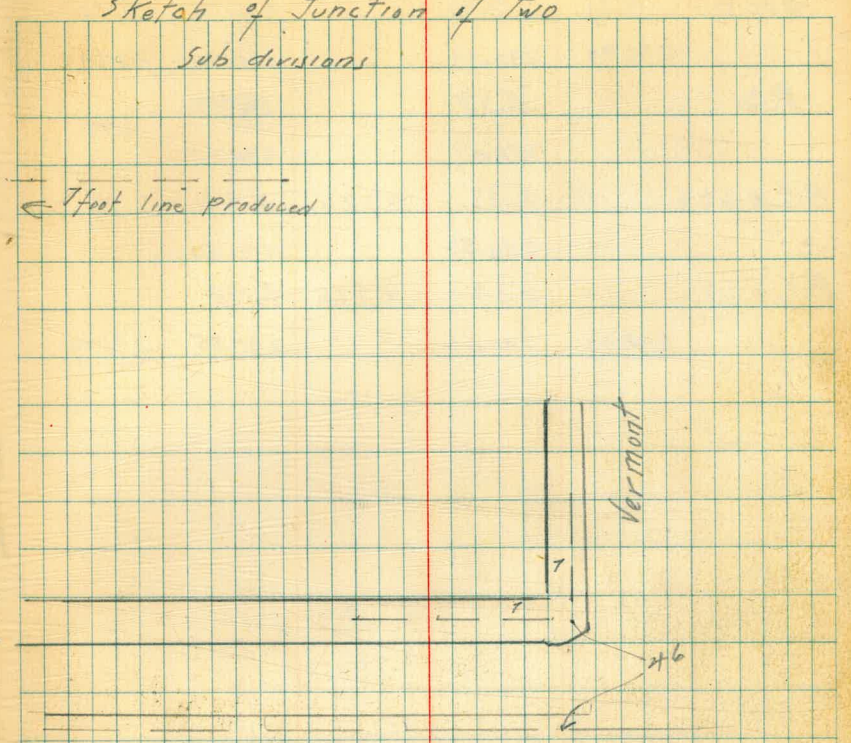


check on N Line Johnson to E

See p 50

~~295.47~~
290.19

Sketch of Junction of two Sub divisions



~~295.47~~ 290.19

	North Curb	Side Gutter		South Gutter	Side Curb
0+00	4.91	5.41		5.54	5.00
	290.99	290.49		290.40	290.94
P.C.		5.39		5.49	
		290.51		290.45	
B.C.+7.33		5.37	+7.26	5.44	
		290.53		290.50	
B.C+7.33		5.34	+7.26	5.59	
	295.90	290.56		290.35	295.94

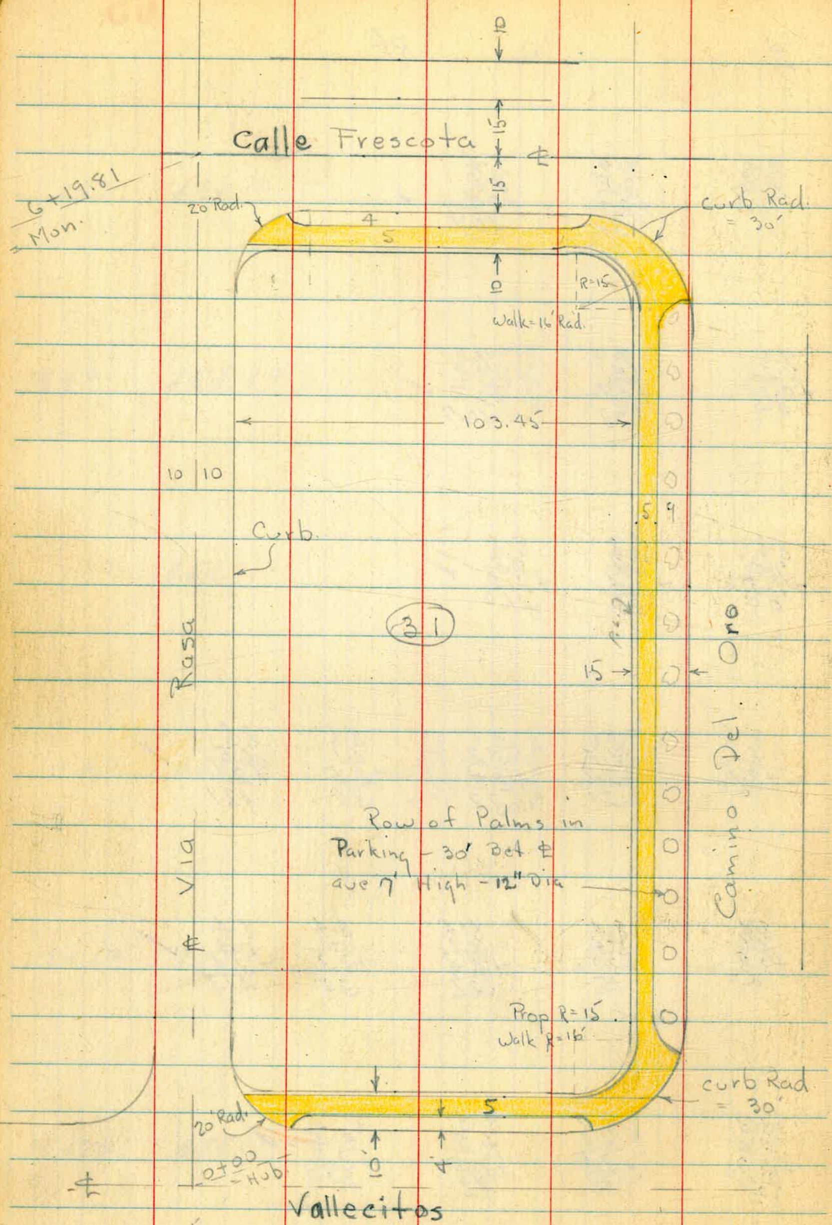
Re. Cross Section Montezuma Road
At 63rd & Montezuma Road 15+15.19 to 18+50

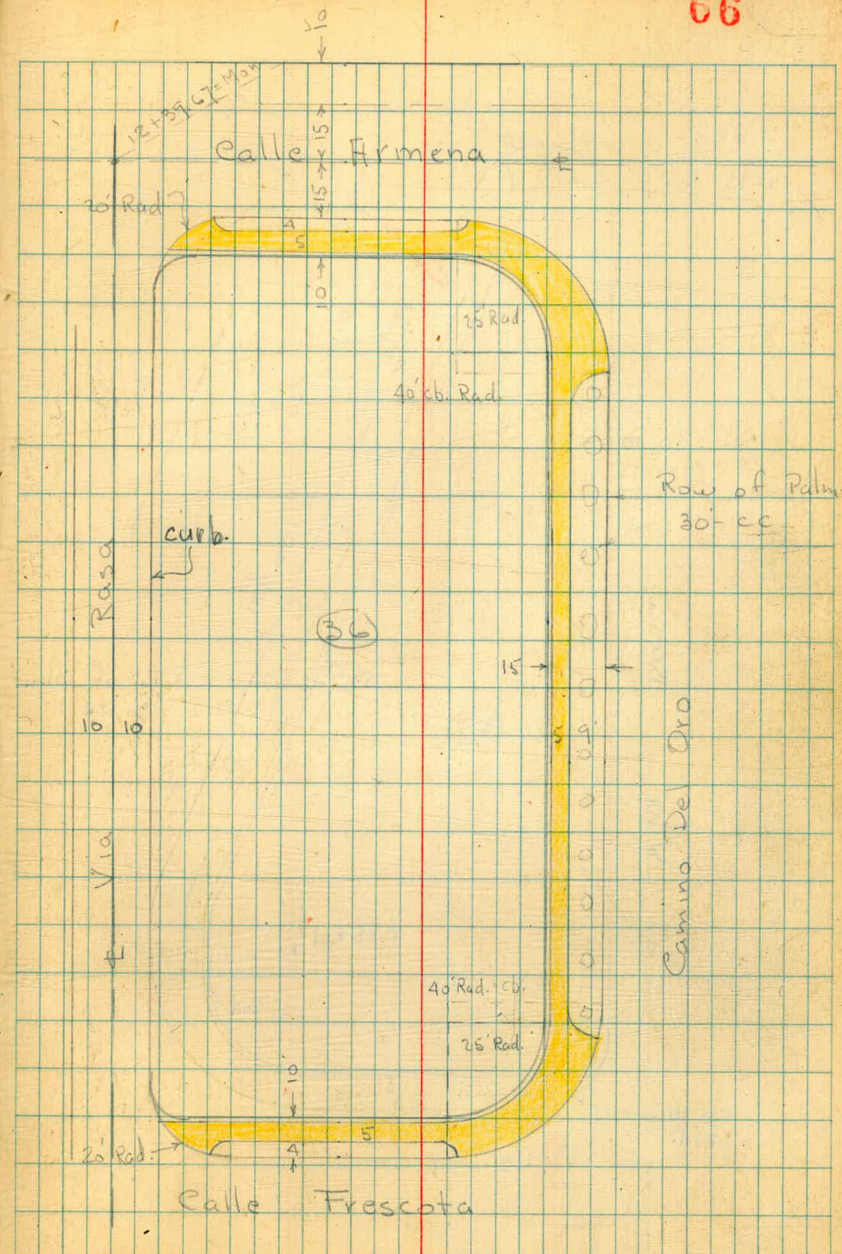
Sept. 2-48
Sisson
Smith
Becker
Barger

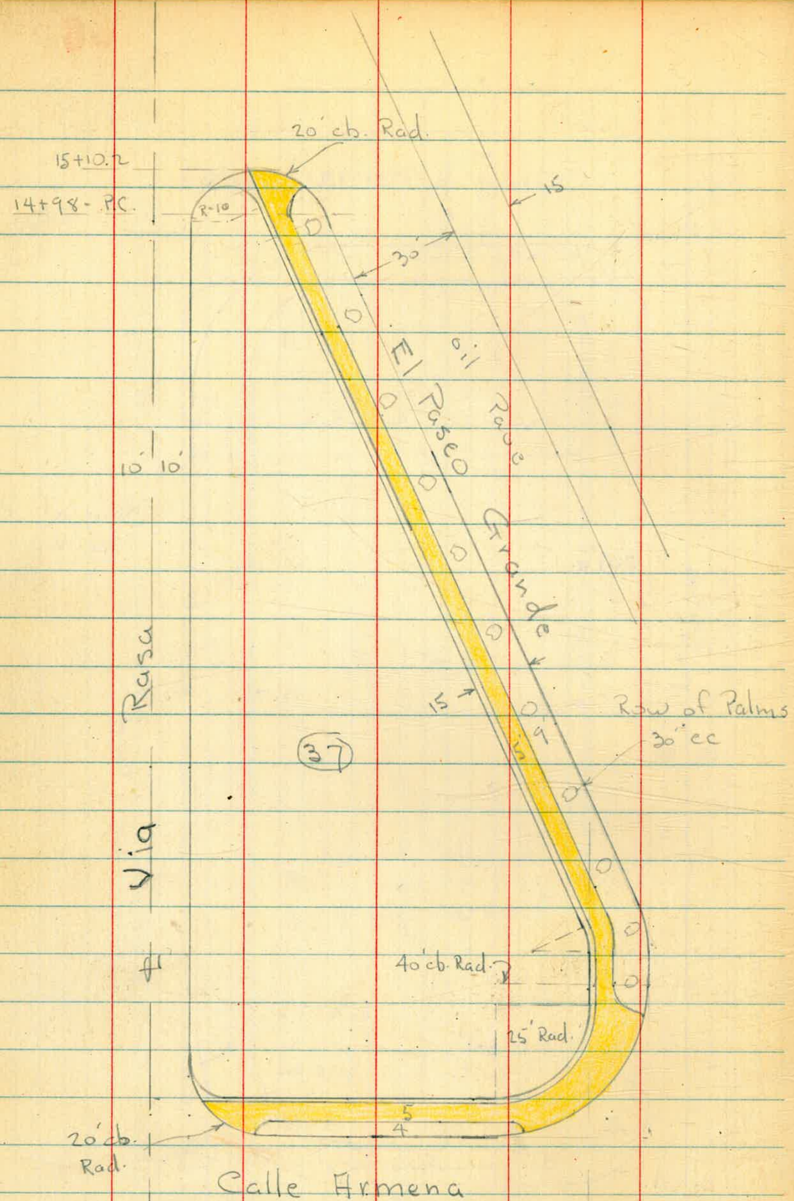
	Curb Grade			Lt.		℄			Rt.	
+50	454.27			8.2 5.1 +3.1 42.1	8.2 5.2 +3.0 33	8.2 5.1 +3.1 0.0	8.2 5.0 +3.2 33	8.2 4.9 +3.3 43.3		✓
16+01.44	454.35			8.1 5.6 +2.5 42.5	8.1 5.6 +2.5 33	8.1 5.5 +2.6 0.0	8.1 5.3 +2.8 33	8.1 5.0 +3.1 43.1		✓
+50.96	454.32	8.2 6.0 +2.2 42.2	8.2 6.9 +1.3 33	8.2 7.7 +0.5 16	8.2 5.8 +2.4 11	8.2 5.3 +2.9 0.0	8.2 5.1 +3.1 31	8.2 5.2 +3.0 43.0		✓
+22	454.28			8.2 7.5 +0.7 40.7	8.2 8.0 +0.2 33	8.2 8.0 +0.2 0.0	8.2 8.0 +0.2 33	8.2 6.0 +2.2 41	8.2 5.7 +2.5 42.5	✓
15+15.19	454.27			8.2 7.7 +0.5 41	8.2 8.3 -0.1 33	8.2 7.9 +0.3 0.0	8.2 8.2 0.0 33	8.2 7.7 +0.5 40		✓
BM	1.28	462.47		456.19	on R.P. 155 Rt ℄ 15+09.96					

			Lt.		
+50	453.10			9.4 9.2 +0.2 40.2	9.4 9.2 +0.2 33
18+0	453.49		9.0 5.2 +3.8 43.8	9.0 8.2 +0.8 43	9.0 8.5 +0.5 33
+70	453.71			8.8 4.6 +4.2 42.2	8.8 7.0 +1.8 33
+40	453.90	8.6 4.9 +3.7 43.7	8.6 4.8 +3.8 33	8.6 5.8 +2.8 31	8.6 5.7 +2.9 16
17+10	454.05	8.4 4.9 +3.5 43.5	8.4 4.7 +3.7 40	8.4 5.9 +2.5 33	
16+80	454.18			8.3 4.9 +3.4 43.4	8.3 4.9 +3.4 33
		468.47			

Lt.	Rt.
9.1 9.1 +0.0 40.2	9.1 8.5 +0.6 33 / 9.1 8.2 +0.9 40.9 ✓
9.0 9.2 +0.8 0.0	9.0 8.1 +0.9 33 / 9.0 8.3 +0.7 40.7 ✓
8.8 3.5 +5.3 0.0	8.8 3.4 +5.4 33 / 8.8 7.8 +1.0 41.0 ✓
8.6 6.5 +2.0 0.0	8.6 6.4 +2.2 31 / 8.6 5.2 +3.4 33 / 8.6 6.1 +2.5 36 / 8.6 6.5 +2.1 42.1 ✓
8.4 4.6 +3.8 0.0	8.4 5.4 +3.0 15 / 8.4 4.3 +4.1 32 / 8.4 5.3 +3.1 35 / 8.4 5.3 +3.1 40.1 ✓
8.3 4.4 +3.9 0.0	8.3 4.8 +3.5 33 / 8.3 4.8 +3.5 42 / 8.3 3.5 +4.8 43.8 ✓


Calle Frescota
6+19.81
Mon.
20' Rad.
curb Rad = 30'
R=15
Walk=16' Rad.
103.45
10 10
Curb
Rasa
31
15
Oro
Del
Camino
Row of Palms in
Parking - 30' Bet ℄
ave 7' High - 12" Dia
Via
℄
Prop R=15
Walk R=16'
curb Rad = 30'
20' Rad.
0+00 = Hub
Vallecitos


Calle Armena
20' Rad.
25' Rad.
40' cb. Rad.
Row of Palms
30' cc
curb.
Rasa
36
15
10 10
Via
℄
Camino Del Oro
40' Rad. cb.
25' Rad.
20' Rad.
Calle Frescota


20' cb. Rad.
15+10.2
14+98 - P.C.
R-10
15
30'
El Paseo
oil
Grande
10' 10'
Via Rasa
37
15
Row of Palms
30' cc
40' cb. Rad.
25' Rad.
5
4
20' cb.
Rad.
Calle Armena

W.O. 60323 — 11-5-48 — 7.0.

Grid Sections for Topo of Prop. Park - Blocks 31-36-37 - of La Jolla Shores - See Book 1877-56 for Area to W.

2+00

1+50

1+00

0+50

0+45 = opp P.C. 30' Rad Ret on Del Oro
0+35 = opp P.C of 20' Rad. Ret. on Via Rasa
0+24 = Back of 5' Conc. Walk along Vallecitos

0+15 = N. cb.

0+00 = ℄ Vallecitos
Base Line = ℄ Via Rasa

3.16	8.28	2.62	5.12	= Top F.H. s.w.
4.23	7.74		3.51	B.P. in Sea wall

Base Line = ℄ Via Rasa — Pt. = E.

2.4 / 5.9 — 2.2 / 6.1 / 10 / gut — 2.58 / 5.70 / 10 / Top — 3.2 / 5.1 / 40 — 3.50 / 4.78 / walk — 3.26 / 5.02 / Top — 2.2 / 6.1 / gut

2.5 / 5.8 — 2.2 / 6.1 / 10 / gut — 2.68 / 5.60 / 10 / Top — 3.4 / 4.9 / 60 — 3.48 / 4.80 / walk / W. edge — 3.25 / 5.03 / Top — 2.5 / 5.8 / gut

2.5 / 5.8 — 2.4 / 5.9 / 10 / gut — 2.60 / 5.68 / 10 / Top — 2.8 / 5.5 / 20 — 3.5 / 4.8 / 60 — 3.42 / 4.86 / walk / 114.45' — 3.13 / 5.15 / Top / See Below for outs — 2.1 / 6.2 / gut

2.5 / 5.8 — 2.3 / 6.0 / 10 / gut — 2.70 / 5.58 / 10 / Top — 3.2 / 5.1 / 20 — 3.5 / 4.8 / 60 — 3.23 / 5.05' / 114.45' / walk — 2.96 / 5.32 / 128.45' / Top cb. — 2.4 / 5.9 / 128.45' / gut

2.72 / 5.56 / 12.9 / walk at cb — 2.3 / 6.0 / 10 / gut — 2.80 / 5.48 / 10 / Top = P.C — 3.21 / 5.07 / 114.45 = walk — 2.80 / 5.48 / 50 / walk — 2.5 / 5.8 / 128.45' / gut — 2.94 / 5.34 / 98 = P.C. walk — 2.96 / 5.32 / 128.45 / Top = P.C

2.4 / 5.9 — 2.1 / 6.2 / 30 / gut — 2.61 / 5.67 / 30 / Top P.C. — 1.9 / 6.4 / 50 / gut — 2.64 / 5.64 / 50 / Top — 2.4 / 5.9 / 98.45' = gut — 2.87 / 5.41 / 98.45' / Top = P.C

2.4 / 5.9 — 2.4 / 5.9 / 50 — 2.5 / 5.8 / 100 — 2.8 / 5.5 / 143.45' = ℄

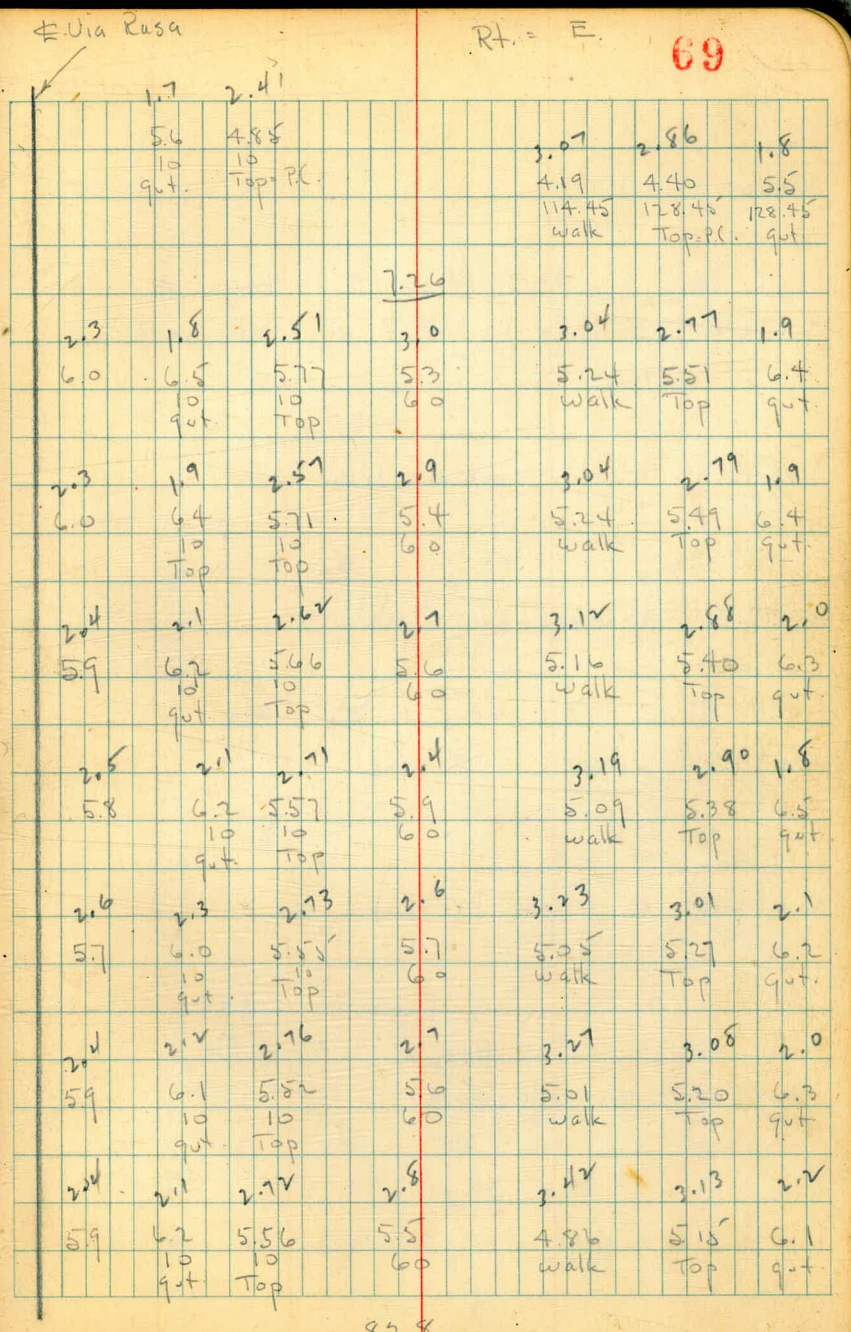
Del Oro
Vallecitos

8.28

5+84.81 = P.C. 20' Rad. Ret. on Via Rasa

5+74.81 = P.C. 30' Rad. Ret. on Del Oro

T.P.	2.41	7.26	3.43	4.85	Top. F.H. Via Rasa + Calle Frescata



7+00

6+74.81 = P.C. 40' Rad. Ret on Del Oro

6+54.81 = P.C. 20' Rad. on Via Rasa

6+43.81 = N. edge of 5' Walk

6+34.81 = N. cb.

6+19.81 = ℄ Calle Frescota

T.P. 2.34 7.19 2.41 4.85

6+04.81 = S. cb. Frescota

5+95.81 = S. edge of 5' walk along Frescota

℄ Via Rasa

Rt.

1.9	1.5	2.04		2.8	2.51	2.40	1.7
5.3	5.7	5.11.5		4.4	4.68	4.79	5.5
	10	10		60	walk	Top	gut
	gut	Top					
1.9	1.6	2.13	2.7	2.5	2.56	2.38	1.7
5.3	5.6	5.06	4.5	4.7	4.63	4.81	5.5
	10	10	20	60	114.45	128.45	
	gut	Top			wly walk	Top=P.C.	gut
	1.9	2.24					
	5.3	4.95					
	10	10					
	gut	Top=P.C.					
	2.09	2.28		2.52		2.36	
	5.10	4.91		4.67		4.83	
	13.7	50		87.45		113.6	
	walk at cb.			=P.C. walk		walk at cb.	
		2.07	1.5	2.16	1.5	2.44	1.6
		5.17	5.7	5.03	5.1	4.75	5.6
		30	30	50	50	88.45	88.45
		Top P.C.	gut	Top	gut	Top P.C.	gut
2.1	1.9	2.2			2.5		
5.1	5.3	5.0			4.7		
	50	100			143.45 = ℄ Del Oro		

7.19

	2.49	1.8		2.60	1.7	2.83	1.8
	4.77	5.5		4.66	5.6	4.43	5.5
	30	30		50	50	98.45	98.45
	Top=P.C.	gut		Top	gut	Top=P.C.	gut
2.51		2.70		2.00	3.09		
4.75		4.56		4.36	4.17		
13.3		50		98	119.6		
walk at cb.		walk		walk=P.C.	walk at cb.		

7.26

& Via Rasa

Rt.

11+00	2.1	1.9	2.27	1.8	2.39	2.32	1.7
	5.1	5.3	4.92	5.4	4.80	4.87	5.5
		10	10	60	walk	Top	gut.
		gut.	Top				
10+50	2.2	1.9	2.24	1.9	2.45	2.25	1.6
	5.0	5.3	4.95	5.3	4.74	4.94	5.6
		10	10	60	walk	Top	gut.
		gut.	Top				
10+00	1.9	1.7	2.21	1.9	2.44	2.27	1.3
	5.3	5.5	4.98	5.3	4.75	4.92	5.9
		10	10		walk	Top	gut
		gut.	Top				
9+50	1.9	1.9	2.23	2.2	2.40	2.29	1.6
	5.3	5.3	4.96	5.0	4.79	4.90	5.6
		10	10	60	walk	Top	gut
		gut.	Top				
9+00	1.9	1.8	2.17	2.6	2.41	2.29	1.6
	5.3	5.4	5.02	4.6	4.78	4.90	5.6
		10	10	60	walk	Top	gut.
		gut.	Top				
8+50	1.9	1.6	2.05	2.1	2.30	2.34	1.6
	5.3	5.6	5.14	5.1	4.89	4.85	5.6
		10	10	60	walk	Top	gut.
		gut.	Top				
8+00	1.9	1.7	2.09	2.4	1.99	2.31	1.7
	5.3	5.5	5.10	4.8	5.20	4.88	5.5
		10	10	60	walk	Top	gut
		gut.	Top				
7+50	1.9	1.7	2.05	2.6	2.29	2.24	1.7
	5.3	5.5	5.14	4.6	4.96	4.95	5.5
		10	10	60	walk	Top	gut.
		gut	Top				

7.19

12+63.67 = along N. edge of Walk

12+54.67 = N. cb.

12+39.67 = ℄ Calle Armena

12+24.67 = S. cb. Calle Armena

12+15.67 = along S. edge of Walk

12+04.67 = P.C. 20' Rad. Ret. on Via Rasa

11+84.67 = P.C. 40' Rad. Ret. on Del Oro

11+80

T.P. 2.68 7.42 2.45 4.74 Hyd. - Rasa & Amena

11+50

℄ Via Rasa Rt. 72

2.1	2.27		2.35		2.39		2.20
5.3	5.15		5.07		5.03		5.22
	133 = walk at cb.		50		88.45'		113.4
			walk		walk at P.C.		walk at cb.
2.0	1.7	2.32	1.6	2.28	1.6		2.26
5.4	5.7	5.10	5.8	5.14	5.8		5.16
	30	30	50	50	88.45'		88.45'
	gut.	Top = P.C.	gut.	Top	gut.		Top = P.C.
2.0				2.0		2.1	2.2
5.4				5.4		5.3	5.2
				50		100	143.45'
							℄ Del Oro
2.0	1.6	2.29	1.5	2.25	1.6		2.34
5.4	5.8	5.13	5.9	5.17	5.8		5.08
	30	30	50	50	88.45'		88.45'
	gut.	Top = P.C.	gut.	Top	gut.		Top = P.C.
2.0	2.22		2.30		2.42		2.23
5.4	5.20		5.12		5.00		5.19
	13.4 = walk at cb.		50 walk		88.45' walk at P.C.		113.7 walk at cb.
	1.9	2.31					
	5.3	5.11					
	10	10					
	gut.	Top					
						2.29	1.4
						5.13	6.0
						128.45'	128.45'
						Top = P.C.	gut.
2.1	1.7	2.28	1.3	1.5		2.48	2.33	1.4
5.3	5.7	5.14	6.1	5.9		4.94	5.09	6.0
	10	10	35	60		114.45'	128.45'	gut.
	gut.	Top				walk	Top cb.	
				7.42				
2.2	1.9	2.27		1.7		2.41	2.27	1.5
5.0	5.3	4.92		5.5		4.78	4.92	5.7
	10	10		60		walk	Top	gut.
	gut.	Top						
				7.19				

14+98 = P.C. 20' Rad. Ret. on El Paseo Grande

14+94 = P.C. on Via Rasa

14+50

14+00

13+65

13+30

12+94.67 = P.C. 40' Rad. Ret. on Del Oro & Grande

12+74.67 = P.C. 20' Rad. Ret. on Via Rasa

℄ Via Rasa →

2.7	2.5	2.65	3.5	2.87	2.74	2.0
4.7	4.9	4.77	3.9	4.55	4.68	5.4
	11.2	11.2	25	31	46.5	gut.
	gut.			wly. walk	Top=P.C.	
	2.7	2.61				
	4.7	4.81				
	10	10				
	gut.	Top=P.C.				
2.7	2.3	2.49	2.7	2.64	2.55	1.8
4.7	5.1	4.93	4.7	4.78	4.87	5.6
	10	10	30	52.3	67.5	
	gut.	Top		walk	Top	gut.
2.4	2.2	2.44	2.5	2.55	2.38	1.6
5.0	5.2	4.98	4.9	4.87	5.04	5.8
	10	10	40	74.4	89.6	
	gut.	Top		walk	Top	gut.
2.4	2.1	2.38	2.2	2.55	2.45	1.6
5.0	5.3	5.04	5.2	4.87	4.97	5.8
	10	10	45	90=	105.2	
	gut.	Top		wly walk	Top cb	gut
2.4	2.1	2.40	2.2	2.49	2.37	1.7
5.0	5.3	5.02	5.2	4.93	5.05	5.7
	10	10	60	105.3=	120.4	
	gut.	Top		wly. walk	Top cb	gut
2.4	2.1	2.36	2.0	2.42	2.27	1.5
5.0	5.3	5.06	5.4	5.00	5.15	5.9
	10	TO	60	114.45	128.45	
	gut.	Top		=wly walk	Top=P.C.	gut.
	1.9	2.32				
	5.5	5.10				
	10	10				
	gut.	Top=P.C.				

7.42

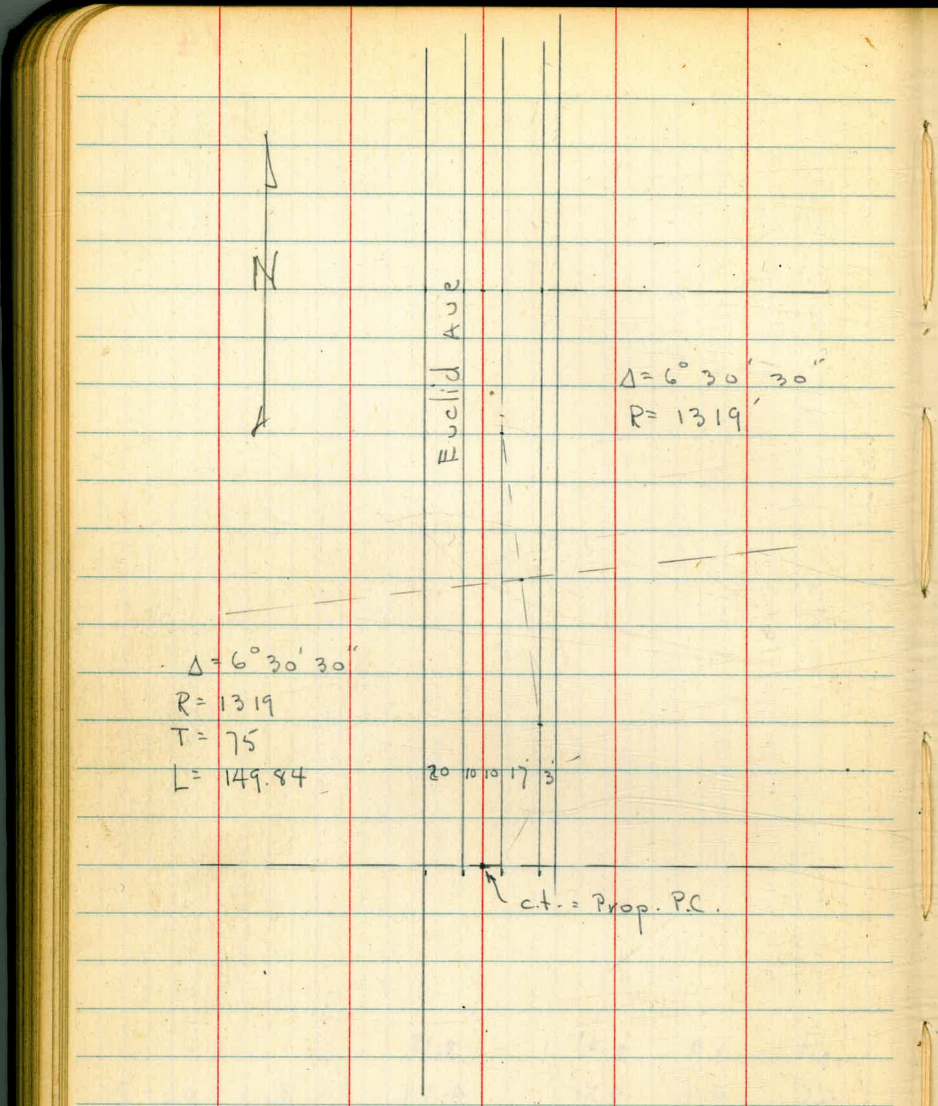
15+50 = end.

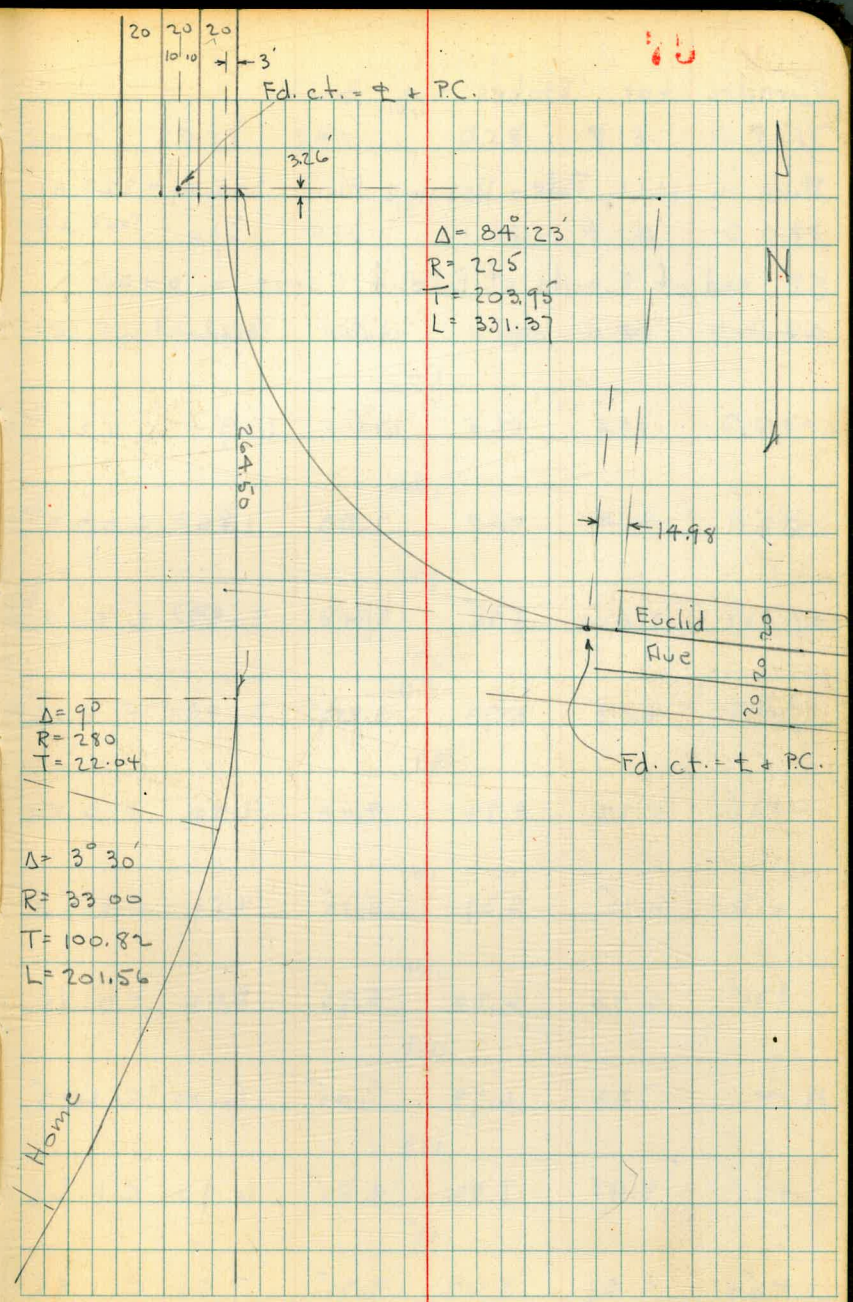
15+10.2 = Most Nly. of 20' Rad. Ret.

2.9 3.0 2.61 3.13
4.5 4.4 4.81 4.29
20 23.5 40
edge oil
Pave

2.66 2.0
4.76 5.4
28 28
Top Gut

7.42


N
Euclid Ave
Δ = 6° 30' 30"
R = 1319'
Δ = 6° 30' 30"
R = 1319
T = 75
L = 149.84
30 10 10 17 3'
c.t. = Prop. P.C.

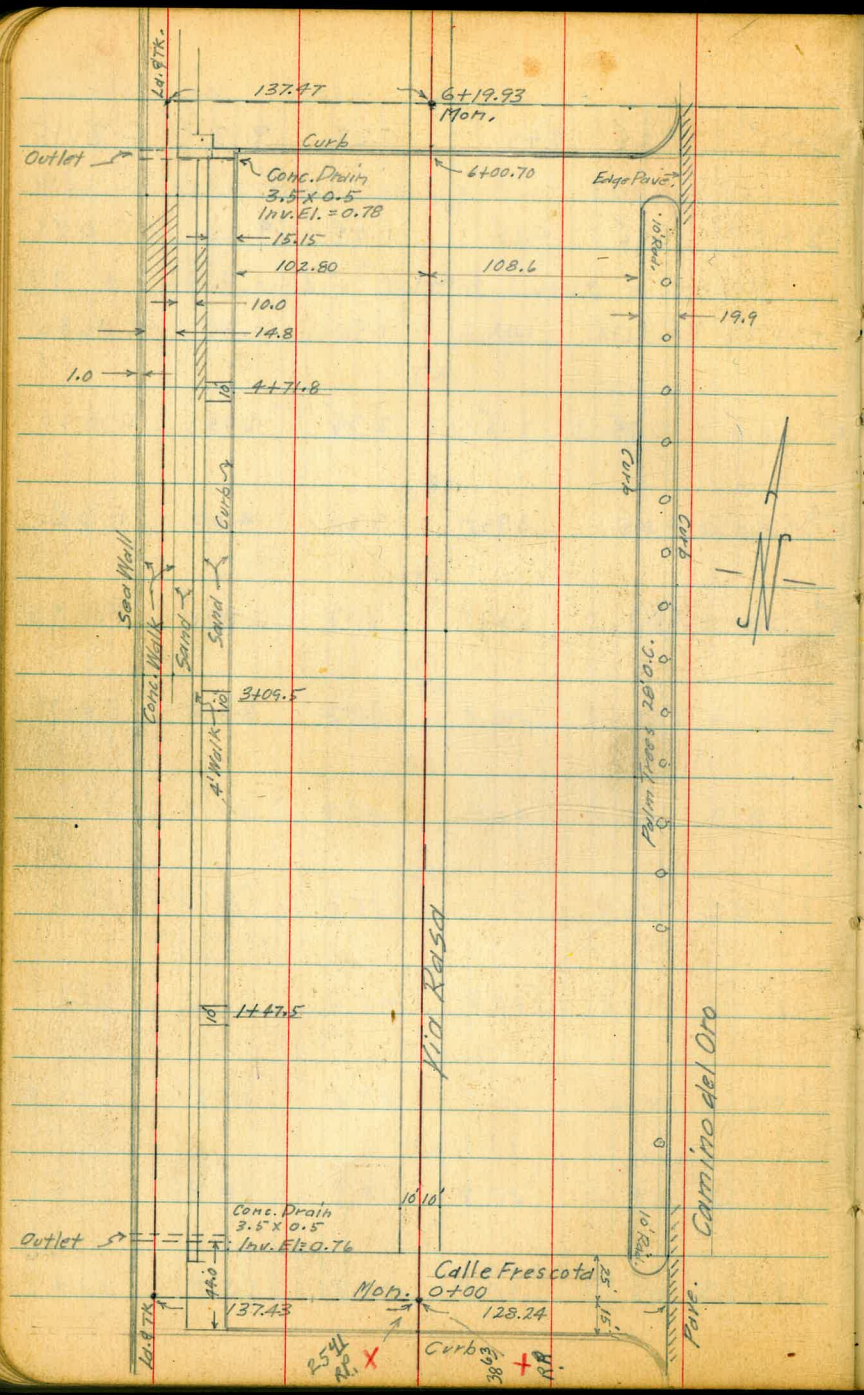

20 20 20
10 10
3'
Fd. c.t. = ℄ ± P.C.
3.26'
Δ = 84° 23'
R = 225'
T = 203.95'
L = 331.37
N
264.50
14.98
Euclid
Ave
20 20
20 20
Fd. c.t. = ℄ ± P.C.
Δ = 90°
R = 280
T = 22.04
Δ = 3° 30'
R = 3300
T = 100.82
L = 201.56
Home

Grades for Stakes - 2' Back.

Spike in N.W. Pole - Assume Elev. 200.00 = 227.01 True elev.

SE. end of E. side of Euclid Curve = 0+00

0+00	℄	edge	stake	Grade	
+25'	1.86	1.20 (10', 1.7)	1.35	1.09	C 0.26
+50	2.74	2.04 (3H)	2.03	1.80	C 0.23
+75'	3.52	2.85' (5')	2.62	2.52	C 0.10
1~	4.43	3.73 (6.7)	3.20	3.26	F 0.06
+25'	5.32	4.74 (8.7)	4.00	4.20	F 0.20
+50	6.15'	5.37 (10)	5.15'	4.59	C 0.55
+75'	6.90	6.20 (11.4)	5.95'	5.40	C 0.55
2~	7.73	6.98 (12.7)	7.05'	6.00	C 1.05
+25	8.47	7.82 (13.8)	8.55'	6.90	C 1.65
+50	9.37	8.62 (15')	9.35'	7.50	C 1.85
2+75'	0.25'	9.43 (15.7)	0.28	8.13	C 2.15
3~	0.95'	0.25' (16.4, 10')	1.08	9.20	C 0.88
+31.37 = E.C. 178		1.08 (16.8, 5S)	1.50	0.20	C 1.30
1 5+	2.75'	2.15' (16.7)	2.35'	2.15'	C 0.20
2 nd.	4.05'	3.70 (16.9)	3.50	4.00	F 0.50
3 rd	5.80	5.67 (14.9, 40')	5.17	6.07	F 0.90
4 +4	7.98	7.88 (13.4, 32)	7.42	8.20	F 0.78



X-Sec. Parking Area - Kellogg Park

77

Garber
Sheppard
Bruner
Bryson

Oct. 5, 51

W.O. 20426

2+00				
+50				
1+00				
+50				
+25				
+15				
0+00				
0-15				
	5.64	7.40	5.06	1.76
	3.31	6.82		3.51

B.P. Sea Wall

Lt. ℄ Rt

116 103

1.49	1.88	2.11	1.7	1.9	2.3	2.4	2.2	2.6	2.30	1.85	
5.91	5.52	5.29	5.7	5.5	5.1	5.0	5.2	4.78	5.10	5.58	
		Cb	G	50		50	G	Cb	Cb	G	
1.44	1.80	1.97	1.7	1.9	2.3	2.2	2.0	2.56	2.24	1.74	
5.96	5.60	5.43	5.7	5.5	5.1	5.2	5.4	4.84	5.16	5.66	
		Cb	G	50		50	G	Cb	Cb	G	
1.38	1.74	1.82	1.4	1.7	2.1	2.3	1.9	2.44	2.36	1.73	
6.02	5.66	5.58	6.0	5.7	5.3	5.1	5.5	4.96	5.04	5.67	
		Cb	G	50		50	G	Cb	Cb	G	
1.39	1.74	1.69	1.1	1.5	2.1	2.0	1.8	2.30	2.31	1.64	
6.01	5.66	5.71	6.3	5.9	5.3	5.4	5.6	5.10	5.09	5.76	
		Cb	G	50		50	G	Cb	Cb	G	
1.45	1.79	1.72	0.9	1.0	1.5	1.5	1.9	2.15	2.24	1.57	
5.95	5.61	5.68	6.5	6.4	5.9	5.9	5.5	5.25	5.16	5.83	
		Cb	G	50		50	G	Cb	Cb	G	
1.35	1.84	1.77	1.2	1.0	1.7	1.7	1.7	1.5	2.14	1.62	
5.95	5.56	5.63	6.2	6.4	5.7	5.7	5.7	5.9	5.26	5.78	
146.75	118	Cb	G	50		50	100	118 G	118 Cb	Pave	
1.48	1.76	1.95	1.4	1.8	2.2	2.2	2.3	1.76			
5.92	5.64	5.45	6.0	5.6	5.2	5.2	5.1	5.64			
146.75	117.95	Cb	G	50		50	100	Pave 128.24			
1.42	1.70	2.02	1.5	2.21	1.5	1.7	2.41	1.7	2.55	1.9	2.79	1.88
5.98	5.70	5.38	5.9	5.19	5.9	5.7	4.99	5.7	4.65	5.5	4.61	5.52
146.75	117.95	102.8	102.8	50	50	G	Cb.	50	50	96.6 B.C.	96.6 B.C.	Pave
											2.10	2.79
											5.30	4.61
											Cb E.C.	E.L. Pave Return

Sea Wall

Inside Edge of Walk

7.40

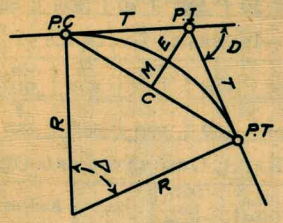
	Lt.				℄				Rt			
				2.0	2.1				2.1		1.50	2.17
				5.4	5.3				5.3		5.90	5.23
	1.49	1.85		50					50		Pave	Cb
+19.93	5.91	5.55									E.C.	E.C.
			09	09				12		15		
	1.55	1.93	1.77 ✓	0.8	0.8	1.74 ✓	1.0 ✓	1.77 ✓	1.1	1.97 ✓	1.2	2.12 ✓	1.48
	5.85	5.47	5.63	6.6	6.6	5.66	6.4	5.63	6.3	5.43	6.2	5.28	5.92
			Cb	E	G	Cb	G	Cb	E	Cb	G	Cb	Pave
					50	50			50	50	108	108	
				12	15				18				
	1.47	1.97	1.66	1.0	1.4	1.9 ✓			1.9		1.6 ✓	2.29	2.30	1.58
+50	5.93	5.43	5.74	6.4	4.0	5.5			5.5		5.8	5.11	5.10	5.82
			Cb	G	50				50		G	Cb	Cb	G
				13	17				20		18			
	1.46	1.81	1.79	1.4	1.8	2.2 ✓			2.1		2.0	2.15	2.29	1.68
5+00	5.94	5.59	5.61	6.0	5.6	5.2			5.3		5.4	4.95	5.11	5.72
			Cb	G	50				50		G	Cb	Cb	G
				14	✓	23			21		19			
	1.45	1.86	1.87	1.5	1.8	2.4			2.2		2.2	2.55	2.24	1.71
+50	5.95	5.54	5.53	5.9	5.6	5.0			5.2		5.2	4.85	5.16	5.69
			Cb	G	50				50		G	Cb	Cb	G
				✓	✓	22			✓		18			
	1.48	1.89	2.02 ✓	1.5	1.8	2.3			2.1		2.1	2.62 ✓	2.20	1.80
4+00	5.92	5.51	5.38	5.9	5.6	5.1			5.3		5.3	4.78	5.20	5.60
			Cb	G	50				50		G	Cb	Cb	G
				15	17	23			21		21			
	1.53	1.91	2.18	1.7	1.8	2.3			2.2		2.4	2.75	2.23	1.91
+50	5.87	5.49	5.22	5.7	5.6	5.1			5.2		5.0	4.65	5.17	5.49
			Cb	G	50				50		G	Cb	Cb	G
				17	18	✓			22		22			
	1.54	1.96	2.21	1.7	2.0	2.3			2.5		2.4	2.95	2.29	1.84
3+00	5.86	5.44	5.19	5.7	5.4	5.1			4.9		5.0	4.45	5.11	5.51
			Cb	G	50				50		G	Cb	Cb	G
				16	✓	✓			✓		20			
	1.50	1.99	2.33	2.0	2.0	2.2			2.2		2.4	2.75	2.30	1.90
+50	5.90	5.41	5.17	5.4	5.4	5.2			5.2		5.0	4.65	5.10	5.58
			Cb	G	50				50		G	Cb	Cb	G

7.40

Seal Wall

Inside Edge of Walk

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\sin. D/2}$(1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=Rtan$\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=Rvers $\frac{\Delta}{2}$ (6)

External=E=Ttan$\frac{\Delta}{4}$-(7)=R÷cos.$\frac{\Delta}{2}$—R(8)=Rexsec$\frac{\Delta}{2}$(9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

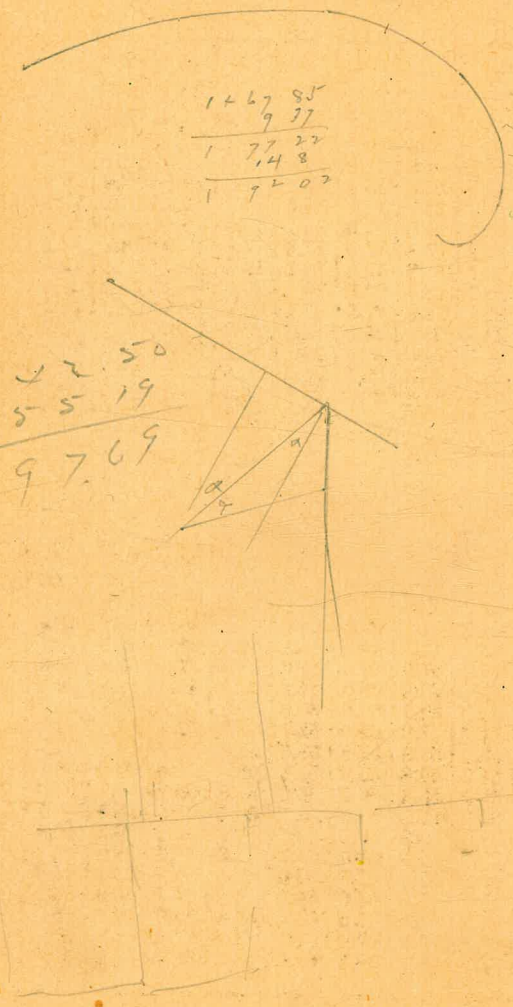
Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50\div100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2\div(2\times688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

	5.18	6.90	3.38	3.52	3.51
		7.40	5.68	1.72	B.P. Sea Wall



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)+2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.