

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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CITY ENGINEER'S OFFICE

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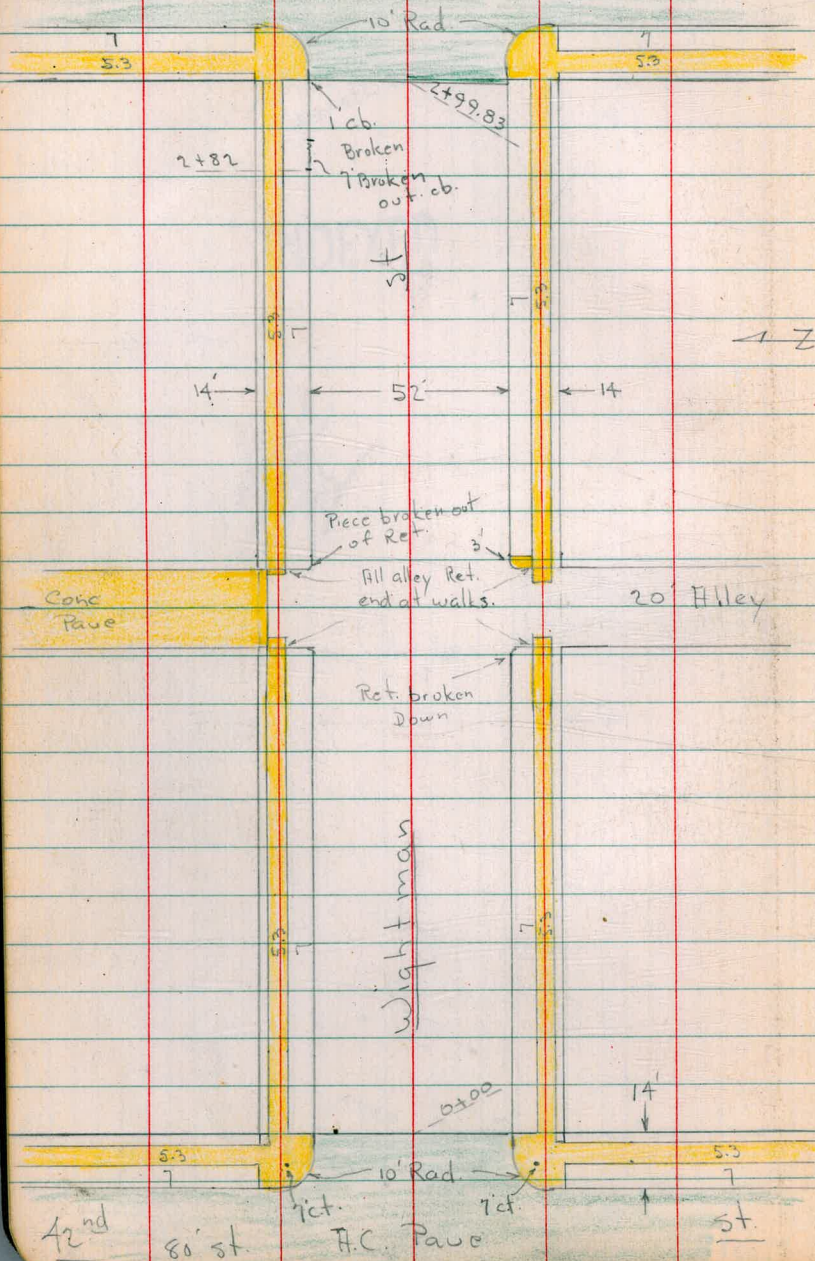
Made in U. S. A.

48 Curb Levels East Side Columbia 100' W Broadway
49 " " North " Broadway 100' E Columbia
7A Alley BIK 13 - Ocean Beach Park. 2 Sec.

Jan Dyke

Hue

H.C. Pave



42nd

80 st

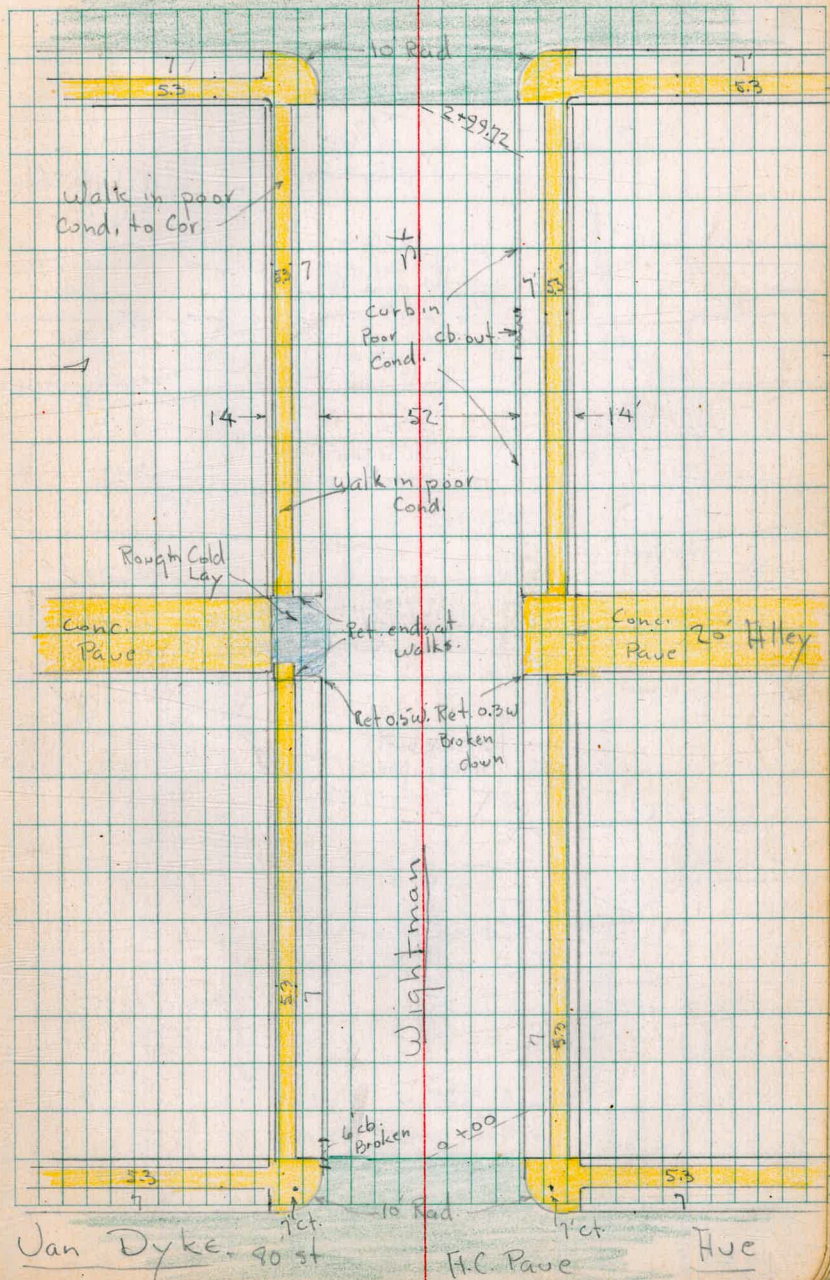
H.C. Pave

st

43nd

H.C. Pave

2 st



Jan Dyke 80 st

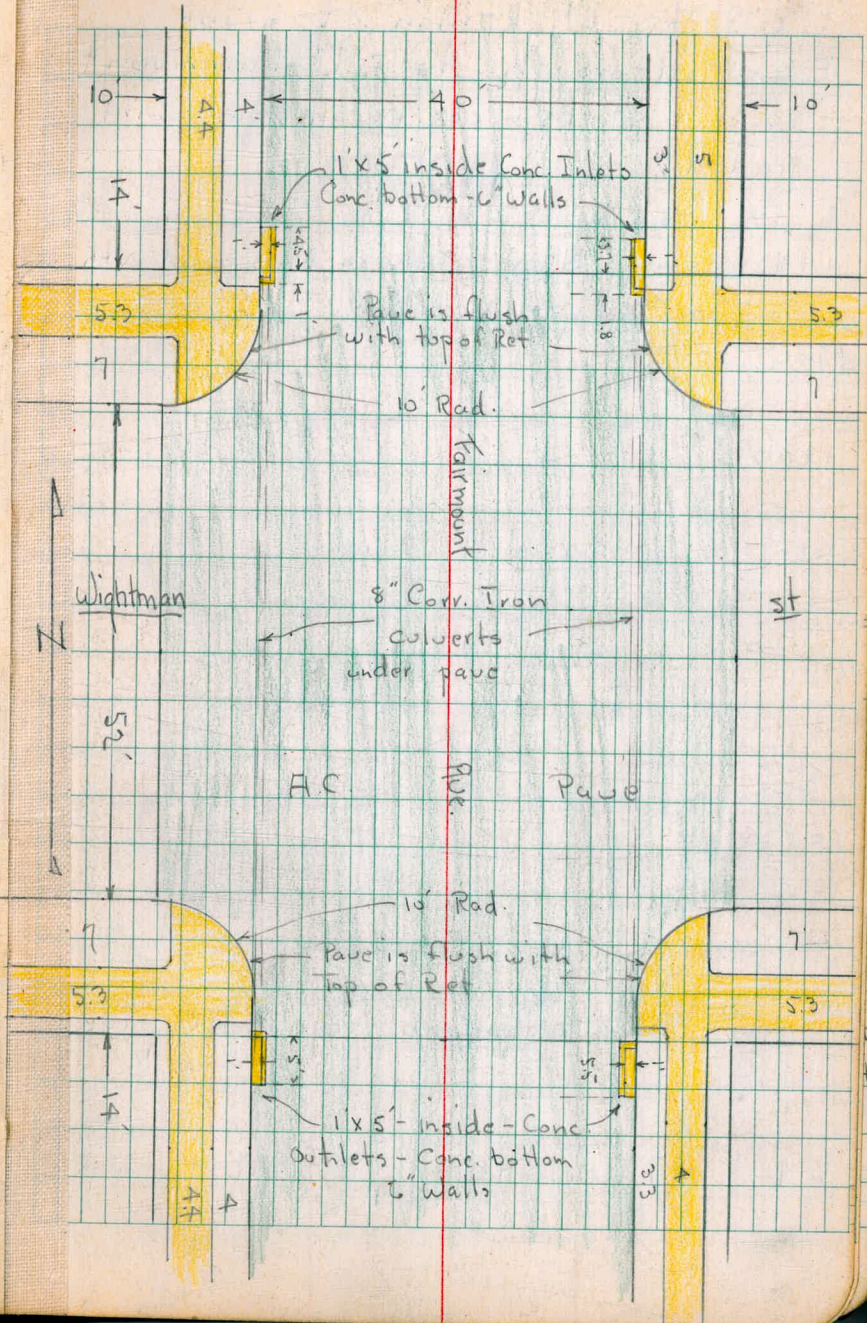
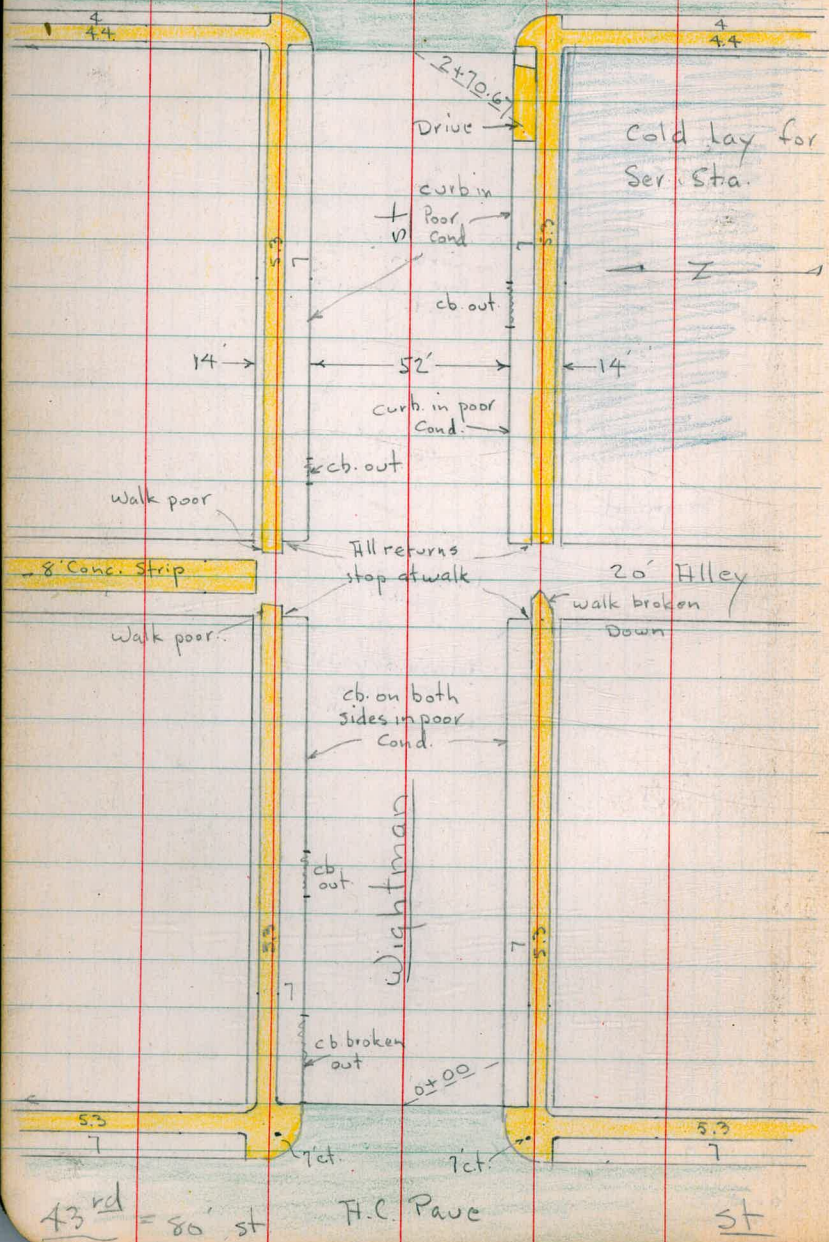
H.C. Pave

Hue

Fairmount = 60 st.

Hue

F.C. Pavc



0+73 = ± 7' Dirt Dr. on Lt. - 2' - 2' Conc. strips out to
26.2 Lt. (cb. broken out.)

0+60

0+50 = ± 10' Dirt Dr. on Rt. - cb. broken out.

0+38 = ± 8' Dirt Dr. on Lt. - cb. broken out.

0+20

86' E. = E.L. 42nd = 0+00 ahead.

66' E. = E. cb. - cross gut.

40' E. = ±

14' E. = w. cb. 42nd - cross gut.

353.16
4.34
100
Top

352.93
352.37
4.57 5.13
100 100
Top gut

Rt. 6

353.45 405 33 walk	352.90 Lt. 4.60 26.2 end of Conc. strips	353.32 4.18 25.8	352.6 4.9 25.8	352.9 4.6 13	353.1 4.4	352.7 4.8 13	352.2 5.3 26 gut	352.94 4.56 26 Top		
353.37 4.13 33 walk	352.60 4.90 25.8 Dr - Bottom of cb.	352.5 5.0 13	352.7 4.8	352.4 5.1 13	351.9 5.6 26 gut	352.2 5.3 26 Dirt - Dr	353.01 4.49 33 walk			
353.02 4.48 25.8 Top	352.3 5.2 25.8 gut	352.5 5.0 13	352.7 4.8	352.4 5.1 13	351.9 5.6 26 gut	352.2 5.3 26 Dirt - Dr	353.01 4.49 33 walk			
352.89 4.61 25.8 Top	352.23 5.27 25.8 gut	352.31 5.14 13	352.36 5.14	352.27 5.28 13	351.81 5.63 26 gut	352.2 5.3 26 Dirt - Dr	353.01 4.49 33 walk			
352.60 4.90 100 gut	352.94 4.52 65 Top	352.44 5.96 40 gut	352.86 4.64 40 Top	352.31 5.19 40 gut	352.22 5.28 26 13	352.27 5.28 13	351.81 5.63 26 gut	352.43 5.07 40 Top	351.39 6.11 65 Top	351.94 5.56 13
353.21 4.29 100	352.96 4.54 65	352.78 4.72 40	352.64 4.86 26	352.50 5.00	352.39 5.11 26	352.34 5.16 40	352.03 5.17 65	351.94 5.56 13	351.81 5.63 26 gut	351.68 5.18 13
352.64 4.86 65 Top	352.05 5.45 65 gut	352.60 4.90 40 Top	352.03 5.47 40 gut	351.90 5.60 26 13	351.68 5.82 13	351.72 5.17	351.52 5.98 13	351.54 5.96 26	351.34 6.16 40 gut	351.02 5.43 40 Top

357.50

1+60 = E.L. Alley

352.78
 4.77 5.00 5.09
 65 38.1 38.1
 edge edge
 Conc. walk

1+59 = Beg. walk on Lt. - poor cond.

1+563 = Beg. walk on Rt. - poor Cond. to Alley line

1+50 = # Alley

1+442 = end of walk on Rt.

1+432 = end of walk on Lt.

into alley but in poor Cond.

Note: Ret. on Rt. broken down + walks extend

1+40 = WL 20' Alley - Conc. pave in Alley to N.

1+31 = Brk. in cb. on Rt.

1+11 = Brk. in cb. on Rt.

T.P. 5.78 359.05' 4.23 353.27

1+00

353.80 353.60 Lt 353.58 353.2 353.2 353.3 353.3 352.9 353.99 Rt. 353.69 353.69

5.25 5.45 5.47 5.8 5.8 5.7 5.7 6.1 5.56 5.41 5.36
 32.8 32.8 26 26 13 13 13 26 26 33 -walk 38.3
 edge end Top gut
 walk Ret. 1' Rad 9ut Top end Ret

353.85 353.80
 5.20 5.75
 38.1 31.8
 Beg. walk

354.05 353.75 353.4 353.2 353.2 353.1 352.9 353.4
 5.02 5.30 5.6 5.8 5.8 5.9 6.1 5.6
 65 38.3 26 13 13 13 26 40
 edge
 Conc.

353.92 353.60
 5.13 5.45
 38.3 33
 end walk

edge
 Pave

353.27 353.91 353.72 353.61 353.1 353.3 353.3 353.1 352.6 353.08 353.42 353.43
 4.73 5.14 5.33 5.44 5.9 5.7 5.7 5.9 6.4 5.97 5.63 5.62
 65 38.3 33 25.8 25.8 13 13 26 26 33 38.3
 Walk end of Ret. 1' Rad 9ut end ret. walk

edge of Conc.
 Pave

Top-1 Rad.
 Ret. - broken down

353.75 353.99
 5.80 26 6.08
 Top 26 Top

353.43 352.8 353.1 353.2 352.9 352.3 352.98
 4.07 4.7 4.4 4.3 4.6 5.2 4.52
 25.9 25.9 13 13 26 26
 Top gut Top

359.05

357.50

14 E = W. cb. = cross gut.

354.79
4.26 4.73
100 100
Top gut.

Rods on W.L. 6W. of W.L. at s.cb.

2+99.83 = W.L. Van Dyke - edge of A.C. Pavc

2+89 - end broken cb. on Lt.

2+82 - Beg. cb. broken on Lt.

2+80

1+62 = ± 9' Conc. Dr. on Lt.

2+40 = ± 11' ^{New} Conc. Dr. on Rt.

2+16 = ± 10' Dr. on Rt - Dr. sect. in cb. - Dirt to walk

2+00

1+96 = ± 10' Dirt Dr. on Lt. - cb. broken out.

1+65 - Brk. in cb. on Lt.

354.73 354.15 Lt. 354.62 354.09 353.93 353.85 353.82 353.70 353.65 Rt. 353.56 354.12 353.17 353.67

4.32 4.90 4.43 4.96 5.12 5.20 5.23 5.35 5.40 5.49 4.91 5.88 5.38
65 65 40 40 26 13 13 13 26 26 40 40 65 65
Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top gut. Top

354.53 353.87 354.07 354.20 353.99 353.69 354.11
4.52 5.18 4.98 4.85 5.06 5.38 4.94
25.8 25.8 13 13 13 26 26
Top gut. Top gut. Top Top

354.39 353.7 354.0 354.0 353.8 353.4 353.88
4.66 5.3 5.0 5.0 5.2 5.6 5.17
25.9 25.9 13 13 13 26 26
Top gut. Top Top

354.49 353.73 353.73
4.58 5.32
33 25.9
walk Dr.

354.17 353.6 353.7 353.7 353.4 353.15 353.74
4.88 5.4 5.3 5.3 5.6 5.90 5.31
25.9 25.9 13 13 13 26 33
Top gut. Dr. walk

354.20 353.8 353.6 353.5 353.6 353.4 353.09 353.69
4.85 5.2 5.4 5.5 5.4 5.8 5.96 5.36
33 26 13 13 13 26 26 33
Walk in Dr. Top on Dr. Sect. walk

353.72 354.18 353.8
5.33 4.87 5.2
26 33 26
Top walk Dr. dirt

359.05

T.P. 4.77 358.88 4.94 354.11

1+00

0+93 = ± 14' Conc. Dr. on Lt.

0+80 = ± 1' broken cb on Lt.

(note: - extra Conc. slab poured in gut.

0+60 = 2' w. of ± of 9' Conc. Dr. on Rt.

0+48 = ± 2' Broken cb. on Rt.

0+45 = End. broken cb. on Lt.

0+25 = Beg. cb. broken on Lt.

0+20

0+19 = ± 1.5' broken cb on Rt.

End cb broken 0+2.5' Pave

80' E. = E.L. Van Dyke = 0+00 ahead = edge of AC.

NW.

check B.M. Van Dyke 4.40 354.65 354.61

66' E. = E.cb. = Cross gut.

40' E. = ±

Lt. Rt. 9

354.23	353.8	353.9	353.9	353.8	353.3	353.91
4.82	5.2	5.1	5.1	5.2	5.7	5.14
25.9	25.9	13	13	13	26	26
Top	gut.				gut	Top

354.35	353.80
4.70	5.17
33	25.9
walk	Dr.

354.33	353.7	354.0	354.1
4.72	5.3	5.0	4.9
26	26	13	
Top	gut.		

353.9	353.63	353.98
5.1	5.42	5.07
13	26	33
	on conc.	walk
	slab in Dr.	

354.47	353.8	354.1	354.1
4.58	5.2	4.9	4.9
25.9	25.9	13	
Top	gut.		

353.9	353.6	354.14
5.1	5.4	4.91
13	26	26
	gut.	Top

354.62	354.04	354.14	354.24
4.43	5.01	4.91	4.81
25.8	25.8	13	
Top	gut.		

354.13	353.69	354.17
4.92	5.36	4.88
13	26	26
	gut.	Top

354.83	354.29	354.69	354.14	354.03	353.89	353.85	353.69	353.67	353.56	354.19	353.20	353.71
4.12	4.76	4.36	4.91	5.02	5.21	5.10	5.36	5.38	5.49	4.86	5.85	5.28
65	65	40	40	26	13	13	13	26	40	40	65	65
Top	gut.	Top	gut.					gut.	Top	gut.	gut.	Top

355.25	355.06	354.94	354.82	354.58
3.80	3.99	4.11	4.23	4.47
100	65	40	26	

354.42	354.31	353.95
4.63	4.74	5.10
26	40	65

359.05

2+40

2+34 = End. cb broken out on Rt. - cb. in poor Cond. ahead.

2+21 = Beg. cb. broken out on Rt.

2+15 = Brk. in cb. on Lt.

2+00

1+60 = E.L. Alley = Beg walk on Lt in poor Cond. 4.25
65

1+50 = Alley

Line - out

1+44 = end of walk on Lt. - poor cond. from Alley

Ret. on Rt. is p.3' W. of line

+out to cb. on Rt. - Alley Ret. on Lt. is 0.5 W. of line

1+40 = W.L. Alley - Conc. pave on Lt. to 1' out 4.21
65

1+35 = end Broken cb. on Lt.

1+25 = Beg broken cb. on Lt.

1+15 = Brk. in cb. on Rt.

354.61

353.54 Lt. 353.1 353.3 353.4 353.4 Rt. 353.2 10 352.9 353.41

5.34 5.8 5.6 5.5 5.7 6.0 5.47
25.8 25.8 13 26.2 26.2
Top gut Top

353.61 5.27 25.8 Top
353.20 353.3 353.4 353.4 353.3 353.0 353.47
5.08 5.6 5.5 5.5 5.6 5.9 5.41
25.8 25.8 13 26.1 26.1
Top gut Top

354.28 354.11 354.08 353.92 353.85 353.7 353.7 353.7 353.35 353.53 353.92 353.66 354.00 353.84 353.06
4.60 4.77 4.80 4.96 5.4 5.2 5.2 5.2 5.53 5.30 5.06 5.22 4.88 5.04 3.82
39 38.3 33 25.8 25.8 13 13 25.8 25.8 33 33 40 40 60
edge Conc. walk Top gut Top gut Top gut Top gut Top gut

end Ret 1' Rad. edge Conc. Rad.
354.33 354.00 353.6 353.7 353.9 353.8 353.34 353.32 354.91
4.55 4.88 5.3 5.2 5.0 5.1 5.54 5.06 3.97
65 39 26 13 13 13 25.8 40 60
edge Conc. edge of Conc.

354.18 354.00
4.70 4.88
38.3 33
end walk

354.42 354.37 354.30 354.02 353.6 353.7 353.9 353.8 353.25 353.69 354.01 353.60 354.11 353.91
4.46 4.51 4.58 4.86 5.3 5.2 5.0 5.1 5.63 5.19 4.87 5.28 4.77 5.07
39 38.3 33 26 26 13 13 25.8 25.8 33 33 40 40
edge Conc. walk end Ret Top gut Top gut Top gut Top gut Top gut Top gut Top gut Top gut Top gut

edge Conc. Pave walk Ret 1' Rad. Conc. pave 1' Rad.
354.18 354.00
4.70 4.88
38.3 33
end walk

354.18 5.09 26 Top

358.88

poor Cond.

Beq. cb on Lt. - broken out + cb. on Rt. = in
80' E. = E.L. 43rd = 0+00 ahead = edge of H.C. Pavc

66' E. = E. cb.

40' E. = E

14' E. = W. cb. = Cross gut.

2+99.72 = W.L. 43rd = edge of H.C. pave

Check BM. 4.67 358.36 5.19 353.69 353.57 NW. 43rd

2+80

2+68 = Brk.in cb. on Rt.

Lt. E Rt.

	353.72	353.36	353.45	353.50	353.35	353.18	353.28
	4.64	5.00	4.91	4.86	5.01	5.18	4.98
	25.7	25.7	13		13	25.9	25.9
	Top	gut				gut	Top
354.22	353.64	353.78	353.30	353.26	353.15	353.13	353.05
4.14	4.72	4.58	5.06	5.10	5.19	5.21	5.23
6.5	6.5	4.0	4.0	2.6	1.3	1.3	2.6
Top	gut	Top	gut				gut
	353.42	353.42	353.42	353.42	353.42	353.42	353.42
	4.14	4.53	4.66	4.89	4.94	4.96	5.02
	6.5	4.0	2.6		2.6	4.0	6.5
	Top						Top
352.94	352.28	353.62	353.18	353.08	352.96	352.89	352.84
4.42	5.08	4.74	5.18	5.28	5.40	5.47	5.52
6.5	6.5	4.0	4.0	2.6	1.3	1.3	2.6
Top	gut	Top	gut				gut
	353.47	353.18	353.04	353.06	353.01	352.89	353.22
	4.89	5.23	5.32	5.30	5.35	5.47	5.14
	25.7	25.7	13		13	25.9	25.9
	Top	gut				gut	Top
	353.42	352.9	353.2	353.0	352.9	352.8	353.22
	5.46	6.0	5.7	5.9	6.0	6.1	5.66
	25.7	25.7	13		13	26.3	26.3
	Top	gut				gut	Top
							353.10
							5.78
							26.2
							Top

358.88

(dip sect.)
 1+30.6 = W. side of 8' Conc. strip in Alley on Lt.

1+27.2 = end of walk on Lt.

Ret. on Lt. = 0.4 W. of Line - Ret. on Rt. = 0.5 W. of Line
 of walk - both sides

1+25 = W.L. 20' Alley - Returns stop at outside

T.P. 5.07 359.05 4.38 353.98

1+00

0+86 = Brk. in cb. on Rt.

0+76.5 = end cb. but on Lt. - Beg. poor cond.

0+60 = 3' W. of \pm of 9' Conc. Dr. on Rt.

0+58.5 = Beg. cb. broken out on Lt.

0+57 = Brk. in cb. on Rt. - Between Drives

0+52 = \pm 9' Conc. Dr. on Rt.

0+35.5 = end cb. out on Lt. - beg. poor cond.

0+20

354.68 Lt 354.35 RT 12
 4.37 4.72

65 391.7 = edge Conc.

354.58
 4.47 354.39
 38.1 32.8
 end walk

354.68 354.50 354.37 353.8 354.2 354.0 353.9 353.4 353.80 354.09 354.10
 4.40 4.55 4.68 5.2 4.8 5.0 5.1 5.6 5.25 4.96 4.95
 38.1 32.8 25.7 25.7 13 13 26.1 26.1 33.2 38.6
 walk end ret. Top gut gut Top end of walk
 at walk Rad. Ret at walk

359.05 ✓

354.33 354.21 353.7 354.0 354.6 353.8 353.6 353.84 353.95
 3.98 4.15 4.7 4.4 4.4 4.6 4.8 4.52 4.41
 33 25.8 25.8 13 13 26.2 26.2 33.2
 walk Top gut Top walk gut

4.32
 26
 Top

354.15 353.94 353.5 353.7 353.8 353.6 353.40 355.04
 4.21 4.42 4.9 4.7 4.6 4.8 4.96 33.2
 32.9 25.7 25.7 13 13 26 33
 walk approx Top gut in Dr. walk

353.68
 4.68
 26
 Top
 352.25 353.79
 5.11 4.57
 26.2 33.2
 Dr. walk

353.91 353.77 353.3 353.5 353.4 353.4 353.0 353.49 353.57
 4.45 4.59 5.1 4.9 5.0 5.0 5.4 4.87 4.79
 33 25.8 25.8 13 13 26 26 33
 walk approx top gut Top walk

358.36

Rest in another Book

60' E = E.L. of Fairmount = edge of H.C. Pavc

Rods on ϕ of Ret.

50' E = E. cb.

355.05
5.10
65
gut.

30' E = ϕ Fairmount

355.40	355.25	355.10	355.15	354.86	354.68	354.97
4.75	4.90	5.05	5.00	5.29	5.47	5.18
25.8 Top	25.8 gut	13		13	26.2 gut	26.2 Top

355.45	354.89
N.E. Ret. 4.70	5.26
Top + pavc	Top + pavc
	S.E. Ret.

355.57	354.61	354.55	355.41	355.38	355.18	355.12	354.94	354.87	354.94	354.07	354.06	354.74	354.08
4.58	5.54	5.60	4.74	4.77	4.97	5.03	5.21	5.28	5.21	6.13	6.09	5.41	6.07
65 Top	45 F.L.	40 F.L.	40 Top	26	13		13	26	40	40 Top	45 F.L.	65 Top	65 gut.
		Inlet.								outlet			

354.67	355.52	355.45	355.24	355.03	354.95	354.73
4.48	4.63	4.70	4.91	5.12	5.20	5.42
65	40	26		26	40	65

360 15

X-Sect. 20' Alley in Blk. 5 - Mt. View

1976

INDEXED

1-5-48

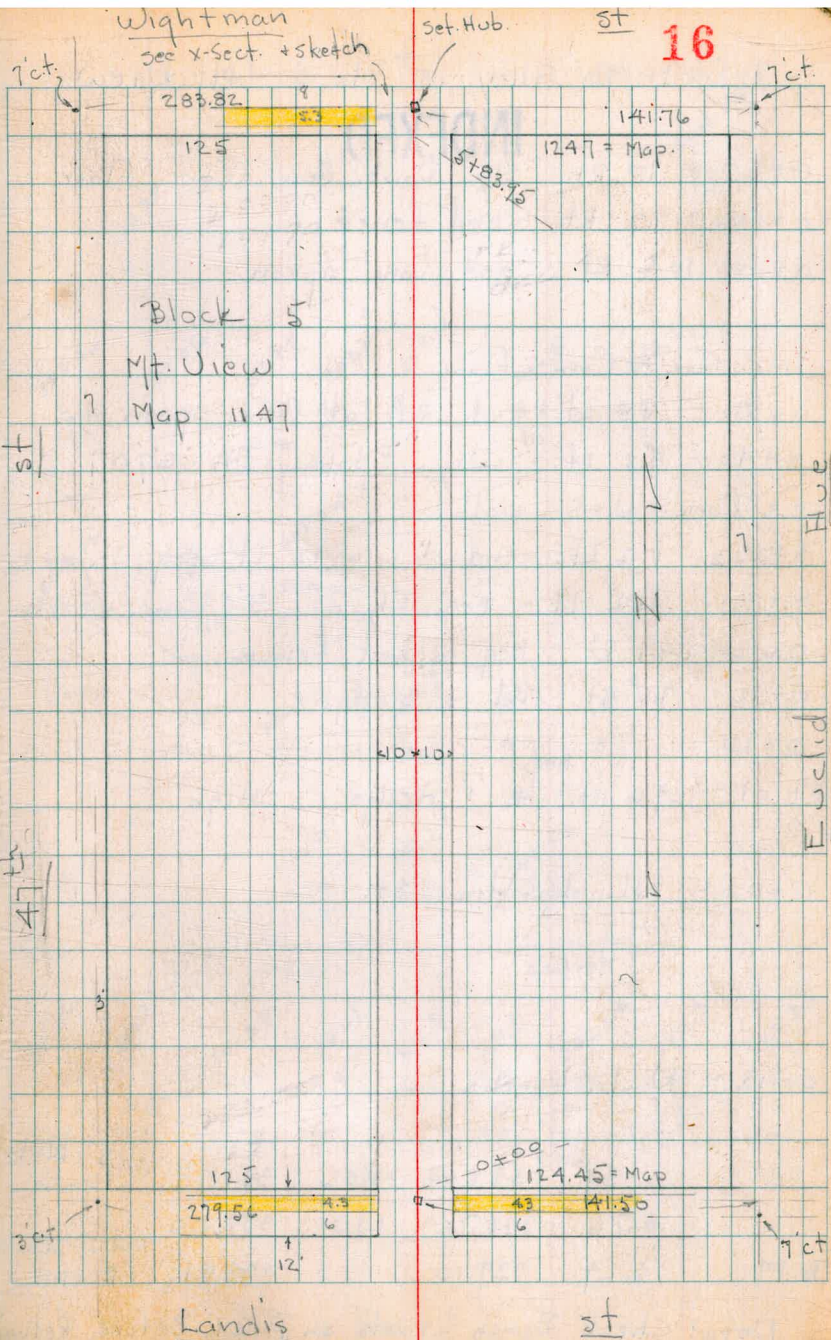
W.O. 31459 }
25001 }

Osborne
Hardin
Worrell

~~Indexed~~
B

Note LANDIS B.M's ave .10 ± Higher
than Wightman -
LANDIS USE HERE.

Notes Reduced 1-21-48 Wherry.



4+00 - 9' Lt. = fence
 3+85 - 9.5 Lt. = Beg wire fence
 3+74 = Sly. House on Rt. - 16.7

3+70 - ^{sly.} Conc. Slab on Rt. 4.5 wide
 3+60 - 9.9 Lt. = wly. P. pole # PA 3759
 3+46 - 14' Lt. = Sly. House

3+40
 shed with toilet
 3+28 - 9.9 Lt. = end of fence + Sly. of 5' Wood

T.P. 1.07 348.16 2.91 347.09.

Conc. found. - floor - below ground.
 2+00 - Very low ceiling House on Lt. -
 2+95 - 9.1 Lt. = Beg wire fence
 2+90 - 9.8 Lt. = Sing. Star. - Dirt floor.

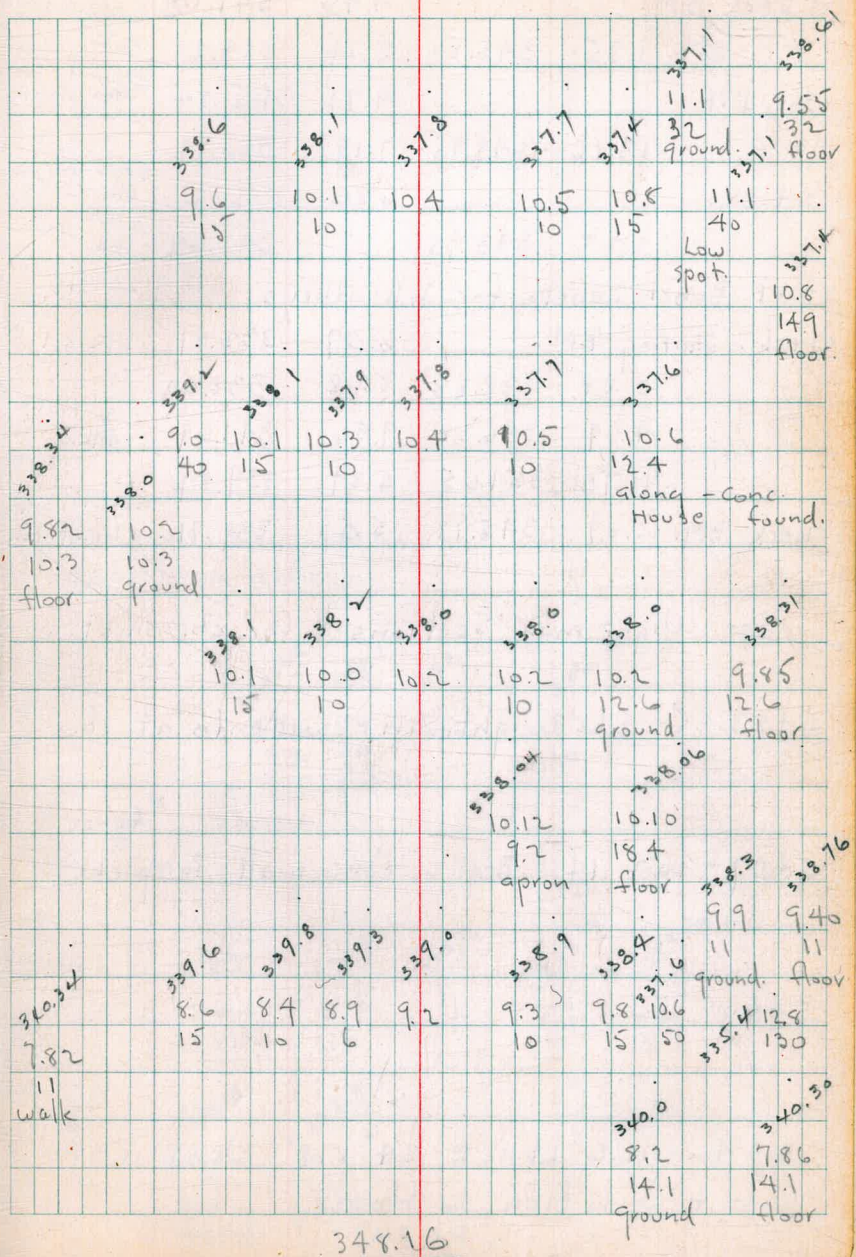
2+50
 2+34 - 9.4 Lt = wly. P. pole # PA 3737
 2+26 - 10.2 Lt. = #15 House

	342.7 5.5 15	Lt. 342.3 5.9 10	341.4 6.8 6	341.2 7.0 6	341.3 6.9 10	Rt. 341.2 7.0 16.7 along House 5.04 16.7 floor	19	
		344.6 3.6 14	344.3 3.4 10	344.3 3.9 6	344.0 4.2 6	343.8 4.4 10	343.61 4.55 12.4 Conc. Slab.	342.96 5.20 20 on slab
347.26	0.90 14 floor	346.3 1.9 15	346.3 1.4 10	346.3 1.9 6	346.1 2.1 6	346.0 2.2 10	344.2 4.0 30	
346.26	1.30 9.9 floor shed							348.16
		346.70 3.30 15.3 floor House	346.95 3.05 15.3 along House = Top conc found.	347.2 2.8 10	347.1 2.9 6	347.3 2.7 10	346.7 3.3 17.6 along House	345.24 1.76 17.6 floor
		346.0 4.0 30	346.0 4.0 10	346.1 3.9 6	346.3 3.7 10	346.3 3.7 15		
346.13	3.87 10.7 floor	345.9 4.1 10.7 ground						350.00

T.P. 5.32 345.21 8.27 339.89 ^{Hub-7'}
= 5790.95

- 5+45 - 32' Rt. = \pm Small House
- 5+41 10' Lt. = end fence
- 5+30 = Drainage problem
- 5+17 - 14.9 Rt. = \pm Sing. Gar. - dirt floor - unused.
- 5+09 - 9.9 Lt. = Beg. wire fence
- 5+00
- 4+90 - 10.3 Lt. = \pm House
- 4+82 - 9.3 Lt. = wly. P. pole = PA. 3783
- 4+84 - 10.2 Lt. = end fence
- 4+70 = Sly. House on Rt. - 12.6
- 4+65 = \pm Sing. Gar. on Rt. - Conc. floor + apron
- 4+53 - 12.6 Rt. = \pm 11' shed - Toilet
Conc. floor +
- 4+40 - outs show low drainage along Euclid.
- 4+24.5 - 11' Lt. = \pm 2' Conc. walk
- 4+23 - 10' Lt. = fence
- 4+12 - 14.1 Rt. = Sly. Small House

Lt. \leftarrow Rt. 20



Check B.M.		4.46	341.10		
T.P. = B.M.	1.35	345.56	5.74	344.21	
Set B.M.		4.71	345.24		
T.P.	13.16	349.95	7.19	336.79	
set B.M.		6.86	337.12		
	2.29	343.98		341.69	
Start Bench Levels for All Alleys - along Landis					
check starting B.M.		6.07	332.81	332.81	
	0.88	338.88	8.38	338.00	
	4.69	346.38	9.96	341.69	
	11.76	351.65	5.89	339.89	
check B.M.	6.07	345.78	5.50	339.71	

see Wightman Sections - for cb on Lt.

5+83.95 = S.L. Wightman - wall ends at cb.

5+67 - 10.2 Lt = Beg. 6" Conc. wall - for picket fence

5+60

5+46 - 12.6' Lt. = # 24" x 18" Vent in Conc. Foundation to House

341.00 = Book

339.61 = our Elev. = 10 Lower! from Wightman Levels.

	340.68	340.1	340.0	340.0
	4.56	5.1	5.2	5.2
	9.9	9.9		10
	Top cb.	put		
	Top wall			
340.60				
4.64	5.4			
10.2	10.2			
Top wall				
	339.1	339.1	338.5	338.3
	6.1	6.1	6.7	6.9
	12.6	10		10
				6.6
				15
340.34				
	339.38	338.9		
4.40	5.86	6.3		
12.6	12.6	12.6		
Top-Conc. found.	Bottom of vent.	ground		
				345.24

X-Sect. 20 Alley in Block 6

1-6-48
Osborne
Hardin
Worrell

1976

INDEXED

W.D. 31459 }
25001 }

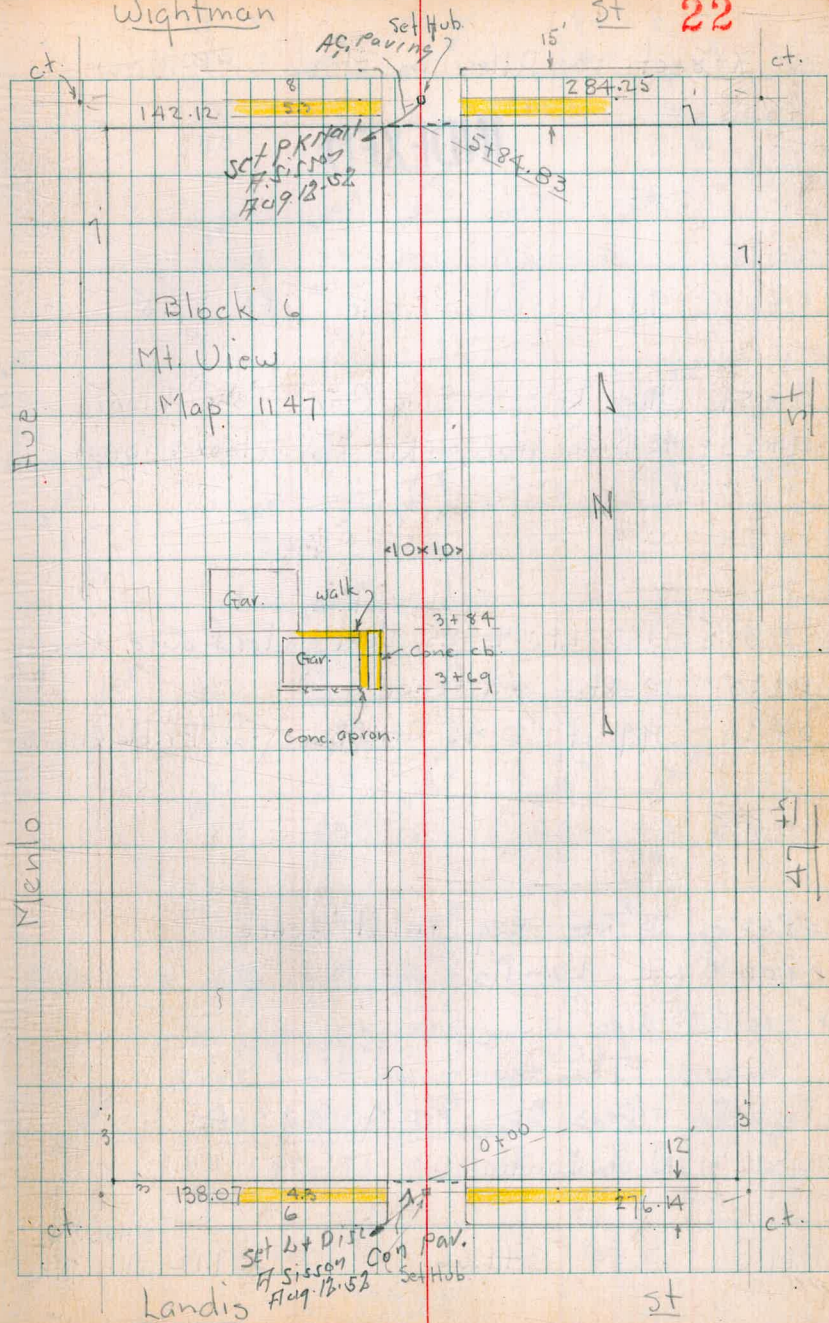
~~Indexed~~
98

This ties in the two circuits
0.10 High at SW. Euclid + Wightman - P. 21
Note: checks 0.09 High on Wightman Levels

		Wightman		our elev.
check B.M.	N.W. B.P. 45 th +	3.97	347.48	347.39
T.P.	6.44	351.45	3.87	345.01
BM - B.P.	N.W. 45 th	5.78	343.10	
T.P.	7.08	348.88	3.76	341.80
T.P.		345.56		
	from P. 21			

Wightman

St 22



X-Sect. 20' Alley in Block 7 Mt. View

1-7-48

7.0

W.O. 31459 }
25001 }

INDEXED

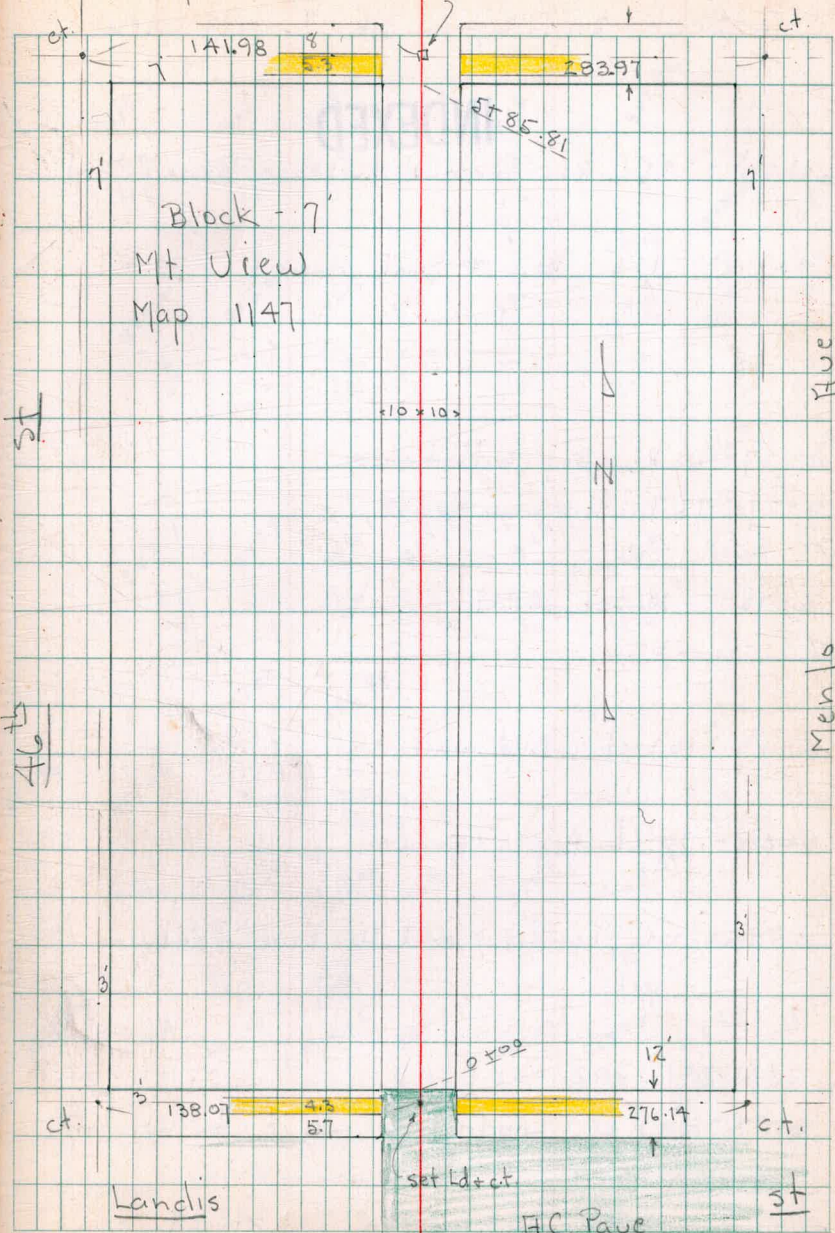
~~Indexed~~

Wightman

Set Hub

15'

ST 28



Block - 7
Mt. View
Map 1147

10 x 10

Hue

Menlo

Landis

Set Id. ct.

H.C. Paue

ST

Should be 0.10 Higher

Mento + Wightman
Check B.M. - N.W. 7'ct. 4.85 342.74 342.65

See Wightman Sections for obs.

5+85.81 = S.L. Wightman + 8' Lt.-end Ely. Hedge

T.P. 5.69 347.59 6.71 341.90 = Hub # + 7'line

5+70

5+50 - 11.5 Rt. = ± 6.5 Conc. walk

5+47 - 6.1' Lt. = Ely. of 4' Hedge - 6' High

Lt. Rt.

= Wightman
Levels

542.86 343.88		342.4 343.4		342.78 343.80
4.73		5.2		4.81
9.9	9.9			10
Top end Ret.	5.0 9.4			Top + out. end Ret.
		347.59		
343.0	342.6	342.6	343.1	343.1
5.6 15	6.0 10	6.0 10	5.5 10	5.5 10.6

along House:

343.61
5.00
11.5
walk

348.61

X-Sect. 20' Alley in Block 8 - Mt. View

1-8-48

W.O. 314597
25001

7.0

INDEXED

~~Indexed~~

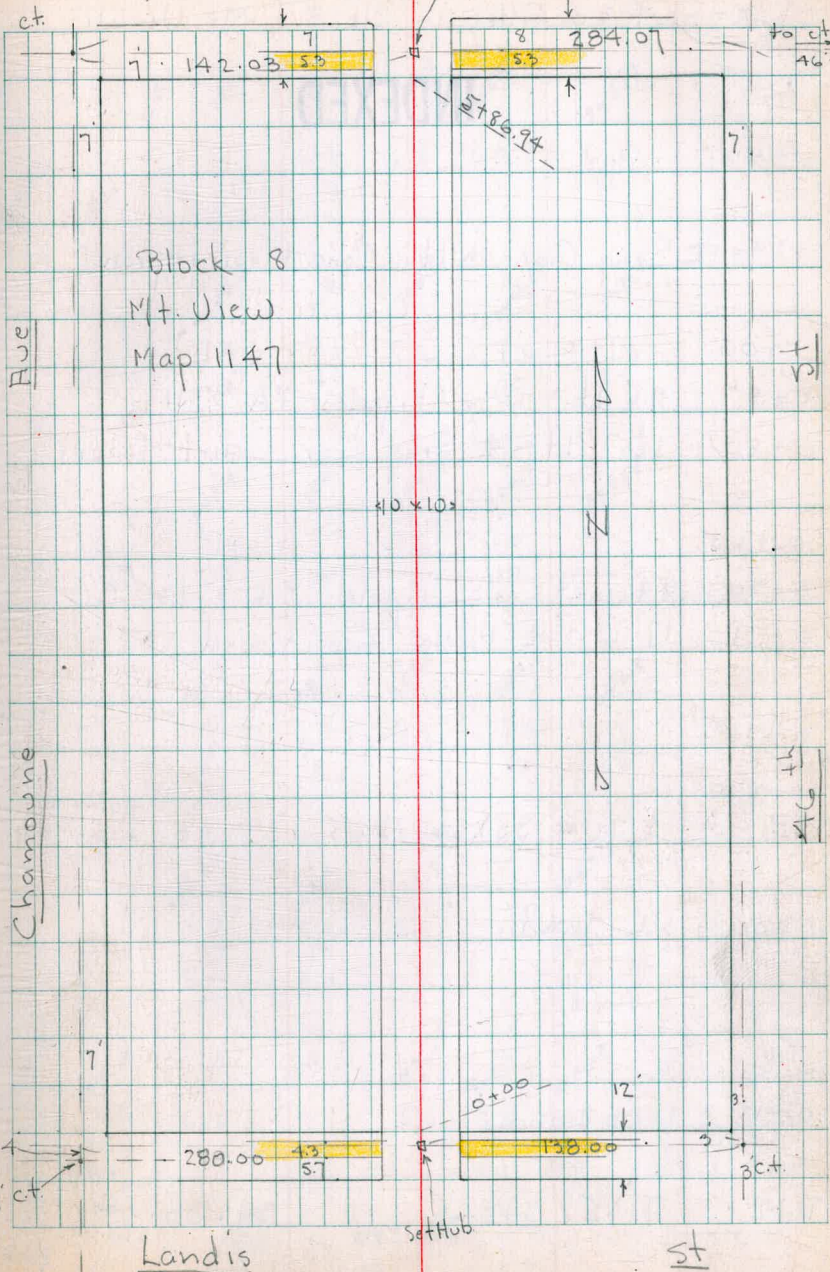
Notes Reduced 1-22-48 Wherry-

Wightman

Set Hub.

St

34



3+00 - Low House on Lt.

2+92 - 10.4' Rt. = Beg. Conc. apron to Doub. Gar.
T.P. 6.96 355.64 2.98 348.68

2+87 - 10' Lt. = Wly. P. pole # P.A. 3751

2+86 - 87' Rt. = end fence

2+77 - 13.7 Lt. = Small House

2+70 - 8.6 Rt. = fence

2+65 - 10.2' Lt. = 5' Conc. slab

2+56 - 23.2 Lt. = Sing. Gar. - Conc. floor

2+44 - 25.5 Lt. = Sing. Gar. - Conc. floor

2+36 - 92' Rt. = Beg. board. fence

2+30 = Sing. Gar. on Lt. - Conc. floor + apron

2+00 = House on Rt. - Conc. found.

1+95 - 10' Lt. = 18" Conc. strip.

1+90 - 10' Lt. = 18" Conc. strip for Dr. to Gar. way

1+87 - 9.6 Lt. = Wly. P. pole # P.A. 3731

1+78 = Sing. Gar. on Lt. - Conc. floor + apron

346.30
5.36
15.2
Conc.

back

347.55	347.0	347.8	348.6	348.9	349.2	349.48	36
8.09 floor	8.6 ground	7.8 15	7.0 10	6.7	6.4 10	6.16 10.4 apron	349.43 6.21 10.4 Con. apron
349.13	347.0						350.79 4.85 19.3 floor
2.53 13.7 floor	4.7 13.7 ground	346.7	347.9	348.2	348.5	348.6	
346.61		5.0 15	3.8 10	3.5	3.2 10	3.1 15	
5.36 15.2 Conc.	345.99						
345.71	5.67 23.2 floor						
5.75 25.8 floor	345.98	345.98	346.2	346.9	347.3	347.6	
	5.68 17 floor	5.68 14.5	5.5 10	4.8	4.4 10	4.1 15	
345.57		345.7	345.7	345.8	346.4	347.1	
6.09 10.9 floor		6.0 10.9 along house	6.0 10	5.9	5.3 10	4.6 15	
345.03	345.16						
6.63 10 Conc.	6.50 10 Conc.						
344.97	344.78						
4.69 18.2 floor	6.88 10.5 apron						
							351.66

X-Sect. 20' Alley in Block 9 - City Hts

Annex # 1

W.O. 31459
25001

INDEXED

1-8-47

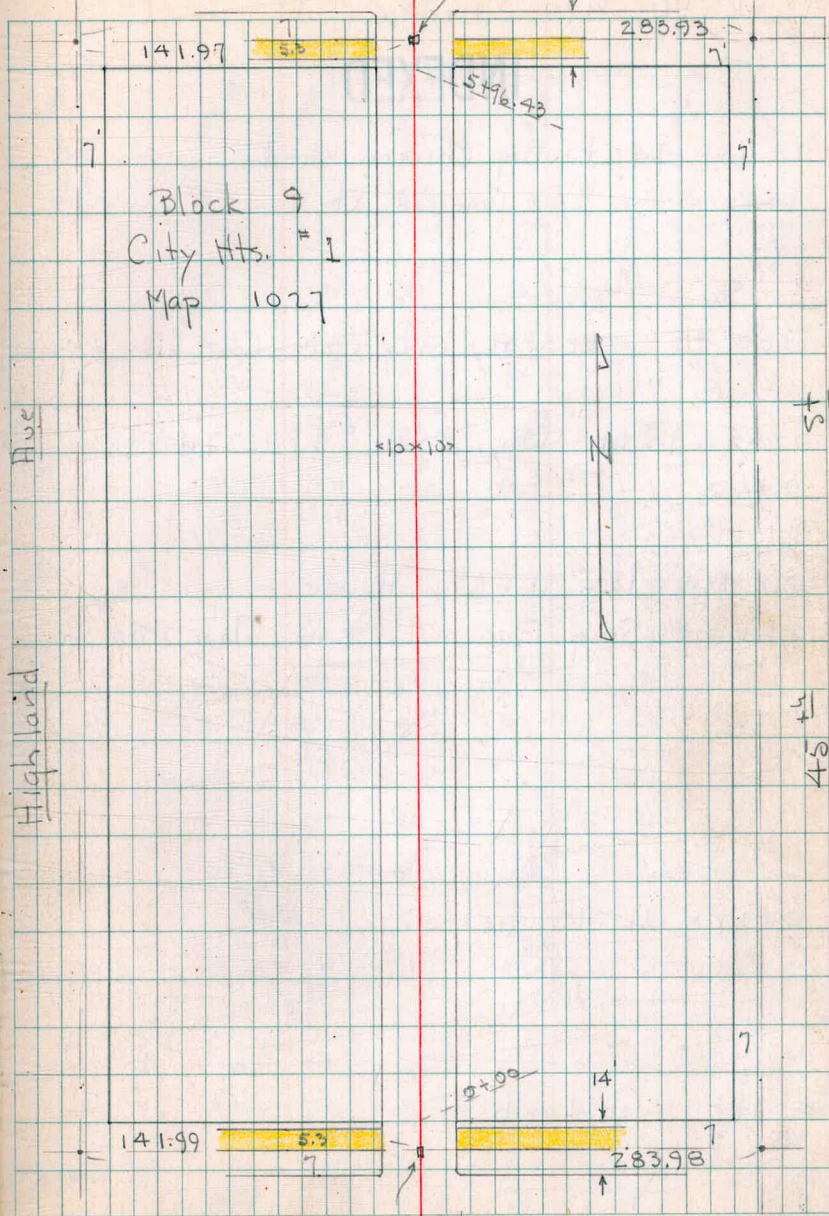
Osborne
Hardin
Worrell
Johnson

~~Indexed~~

Wrightman

Set Hub

ST 39



Block 9
City Hts. # 1
Map 1027

Ave

10x10

N

ST

Highland

45 ft

141.99

7

Set Hub

283.98

7

Landis

ST

X-Sect. 20 Alley
City Hts. Annex # 1

INDEXED

1+70 - 9.4 Lt. - Brg. Chicken shed.

1+50 - sly. Sing Gar. on Rt.

1+00 - Rt. - sly. Sing Gar. - Conc. floor + apron

0+65 - 9.5 Lt. - Wly. P. pole # JPH 37H

0+60

0+48.5 - 13.6 Rt. - Nly. House

0+41 - Sing. Gar. on Lt. - Conc. floor + apron

0+20

0+00 - N.L. Landis

0-14 - N. cb Landis

10.63 353.73

343.10

B.P. NW. 45th
+ Landis

check and
0.10 Higher than Wightman
P 22

Lt. = W. #

Rt. = E 40

349.0 4.7 9.4 floor	349.2 4.3 15	349.1 4.6 10	349.0 4.9	348.6 5.1 10.3 floor	346.8 6.9 40 - shows low ground.
349.5 4.2 15	349.3 4.4 10	349.1 4.6	348.9 4.8 10	348.97 4.76 10.3 apron	348.98 4.75 14.4 floor
350.1 3.6 15	349.8 3.9 10	349.3 4.4	348.9 4.8 10	348.6 5.1 15	
349.87 3.86 13.4 floor	349.59 4.14 10.2 apron	349.5 4.2 10	349.4 4.5	349.0 4.7 10	348.8 4.9 13.6 ground.
	350.4 3.3 11.7 along House			348.9 4.8 13.8 along House	349.83 3.90 13.6 floor
	348.85 4.88 9.9 Top + gut end Ret.	348.5 5.2		348.05 5.68 9.8 Top + gut end of Ret.	
349.72 4.0 4.0 Top	349.2 4.5 4.0 gut.	348.93 5.00 10 Top 2 Rad.	348.1 5.6 10 gut	347.7 6.0	347.3 6.4 10 gut
				347.80 5.93 10 Top 2 Rad.	346.1 7.6 4.0 gut
					346.68 7.05 4.0 Top

353.73

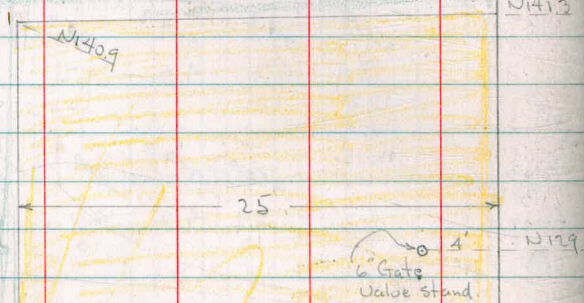
Grid Layout for Topo of Wash Bldg.
in City Shops Scale - 1" = 10'

INDEXED

N 148.18

N 144.0 1 1/2' Lid Elev. 52.06 =
55.8 Gas Tank = Bottom of Tank

A.C.
Pave



Conc. Slab

N 125

Steel Grate over Drain

0.8

0.5

1x1' Iron Lid to Sump 0.7' deep

6" Pipe - 12' High for chain Hoist.

N 110.5

1.1

2.8

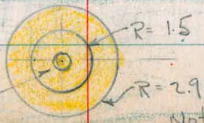
Gas & water inlets

N 100

E 100

N 85.1

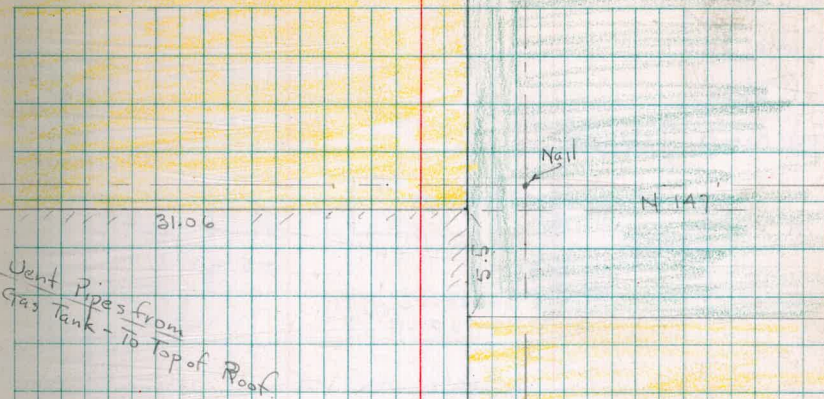
Conc. Air & water stand.



Not to scale

Conc. Slab

43



Bldg.

INDEXED
WK
FEB 1 1949

Conc. Slab.

47.0

Grate over Drain

15'

1'

31.0

Cross

A.C. Pave

E 100

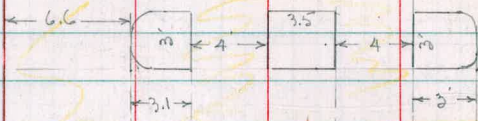
5.0

Detail of Conc. Slab

N. of Bldg

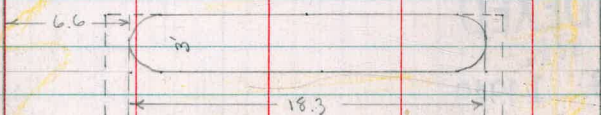
+ Gas Pump Islands

N 2008



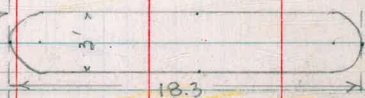
0
100
111

N 1739

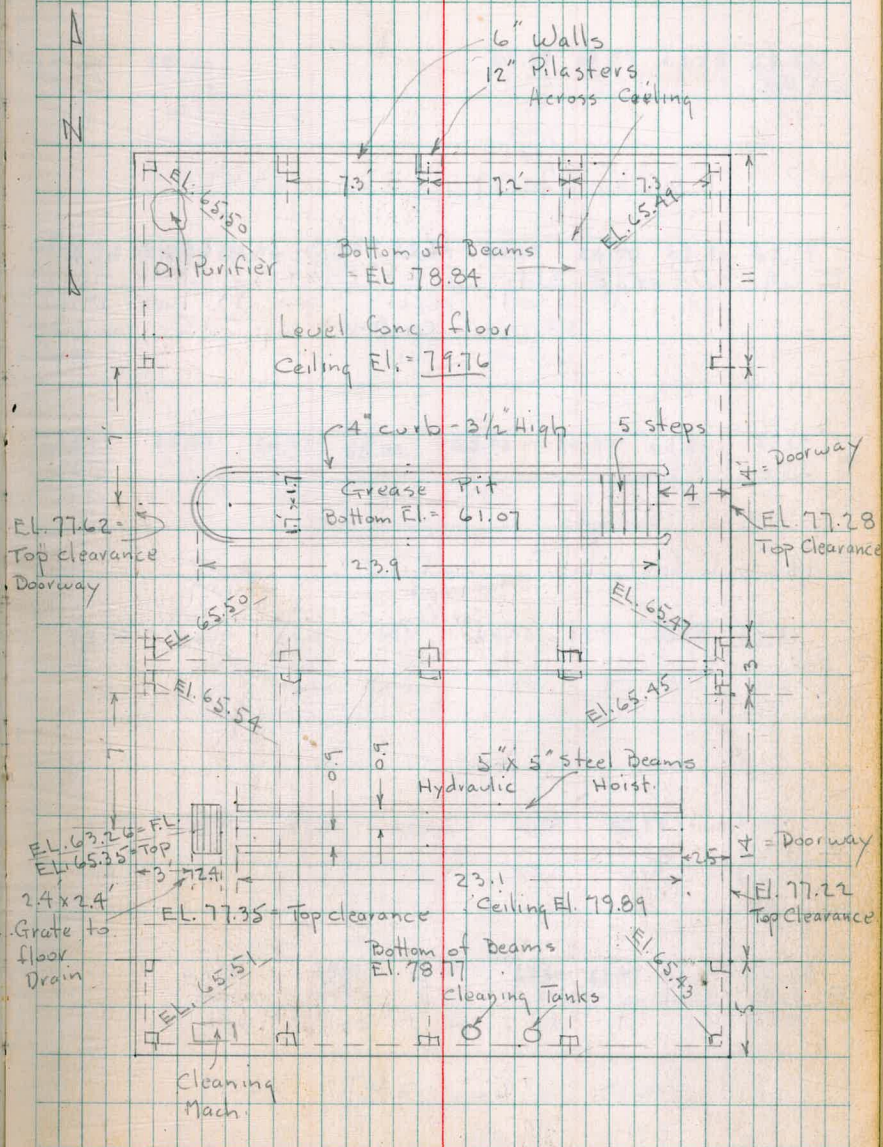


5.1 Canopy

6.5
N 1589
E 69.9



Detail of inside of Bldg.



2851

11-1-48

W.O. 60127

7.0

F 80

T.P. 6.35 70.77 5.24 64.42

F 69 = W. edge Bldg

65.07	65.12	65.35	65.40	65.45
4.59	4.37	4.31	4.26	4.21
210	200	180	160	147
Cor. Conc. Slab.	edge Conc.			Cor. Bldg on Conc.

F 60

5.13
216

F 44 = W.L. Conc. Slab.

5.61	5.40
N 100 = Cor. Conc.	N 40.9 Cor. Conc.

F 40

F 20

F 0.0 = along Drive

4.33	69.66	5.67	65.33
0.77	71.09		70.23

Northings 45

0
0
Z

65.44	65.46	65.57	64.89	63.78	63.95
5.33	5.31	5.20	5.88	5.99	6.82
155	147	100	95	80	60
	along Bldg.		along Bldg.		

70.77

65.51	65.48	65.51	65.49	65.49	65.49	64.70	63.86	63.79
4.15	4.18	4.15	4.17	4.17	4.17	4.96	5.80	5.87
141.3	136	122	119	105	100	95	80	60
edge Conc.		Drwy		Drwy		= Cor. Bldg on Conc.		

64.62	64.90	64.93	65.00	65.02	64.97	63.80	63.61
5.04	4.76	4.73	4.66	4.64	4.69	5.86	6.05
200	180	160	140	120	100	80	60
						edge Conc.	

63.96	64.10	64.10	64.01	64.03	63.91	63.68	63.51
5.70	5.56	5.56	5.65	5.63	5.75	5.98	6.18
200	180	160	140	120	100	80	60

63.88	63.71	63.71	63.66	63.55	63.38	63.47
5.78	5.95	5.95	6.00	6.11	6.28	6.19
180	160	140	120	100	80	60

64.13	63.91	63.75	63.60	63.49	63.37	63.29
5.53	5.75	5.91	6.06	6.17	6.29	6.37
180	160	140	120	100	80	160

69.66

E 103

65.33	65.32	65.37	65.34	65.31	64.77	64.03	64.06
4.60	4.61	4.56	4.59	4.62	5.16	5.90	5.87
155	147	141.5	120	100	95	80	60
		edge Conc.		edge Conc.			

E 100

65.14	65.40	65.42	65.03	65.45	65.43	64.91
4.79	4.53	4.51	4.50	4.49	4.50	5.02
216	155	147	141.5	136	122	119.6
Cor. Conc.	edge Conc.	on Conc.	edge Conc.	Drwy.	F.L.	

T.P.

5.81 69.93 6.35 64.42

E 84.8 - N 809 = \pm of 34' x 22' Grate to inlet (34' E + W)

65.41	65.43	65.42	64.20	65.37	65.43	64.80	64.0	64.0
4.52	4.50	4.51	5.73	4.56	4.50	5.13	5.93	5.93
119.6	119	105	104.6	104.6	100	95	80	60
Top Grate	Drwy.	F.L.	F.L.	Top Grate	= Cor. Bldg			

69.9363.58
7.19

80.9 = Top
Grate = Bottom filled
with grease

20.77

Additional Levels for Wash Bldg.

Roberts
W. Moore
Clark
Gregory
12-9-48

in City Shops

INDEXED

E 125

64.28	64.26	64.27	64.18	64.21	64.31
<u>6.44</u>	<u>6.36</u>	<u>6.61</u>	<u>6.64</u>	<u>6.61</u>	<u>6.51</u>
N100	N70	N80	N70	N60	N50
Edge Conc.					

E 115

64.80	64.35	64.14	64.07	64.09	63.15
<u>6.02</u>	<u>6.47</u>	<u>6.68</u>	<u>6.75</u>	<u>6.73</u>	<u>6.67</u>
N100	N90	N80	N70	N60	N50
Edge Conc.					

E 105

64.23	64.44	64.07	64.04	64.02	64.12
<u>5.59</u>	<u>6.38</u>	<u>6.75</u>	<u>6.78</u>	<u>6.80</u>	<u>6.70</u>
N100	N90	N80	N70	N60	N50
Edge Conc.					

E 95

65.58	64.53	63.89	63.92	64.00	63.95
<u>5.24</u>	<u>6.29</u>	<u>6.93</u>	<u>6.90</u>	<u>6.82</u>	<u>6.87</u>
N100	N90	N80	N70	N60	N50
Edge Bldg.					

E 85

65.58	64.48	63.58	63.83	63.88	63.89
<u>5.24</u>	<u>6.34</u>	<u>7.24</u>	<u>6.99</u>	<u>6.94</u>	<u>6.93</u>
N100	N70	N80	N70	N60	N50
Edge Bldg.		(GROSS)			

E 75

65.52	64.47	63.86	63.67	63.76	63.87
<u>5.30</u>	<u>6.35</u>	<u>6.96</u>	<u>7.15</u>	<u>7.06</u>	<u>6.95</u>
N100	N80	N80	N70	N60	N50
Edge Bldg.					

BM

5.51

70.82

65.31

Chisel cross
N100 = 103E
See pg. 46
this F.B.

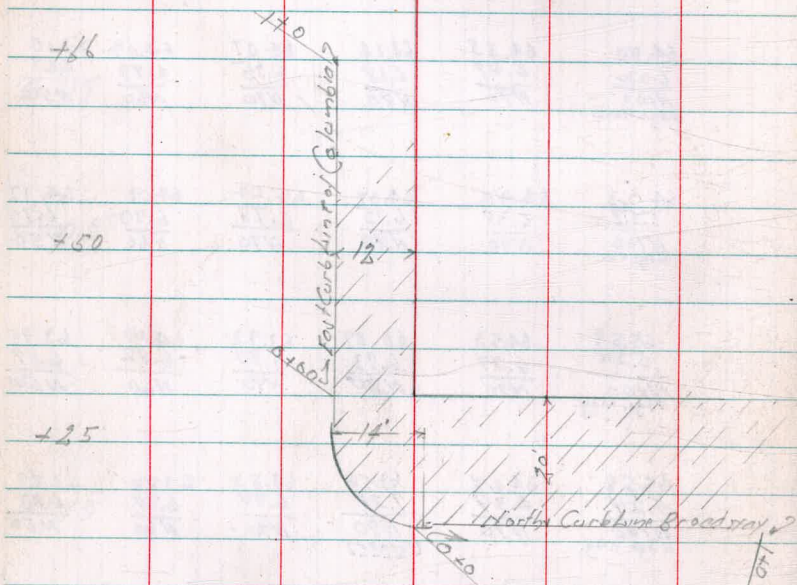
70.82

Cross Section at Curb Columbia
Broadway to 100 North

INDEXED

WK
FEB 8 1949

These curbs are in to practically
Established Grade @ J and 100



0+0 = N.G. Broadway

BM

7.17

23.36

16.19

SW 87
Broadway
Columbia

Feb. 7-49

48

S. 5507
Smith
Becker
Barger

W.O. 25001

Elev.	Notes	Elev.	Notes
18.82	18.82	19.46	19.46
18.39	18.39	19.00	19.00
18.25	18.25	18.90	18.90
18.01	18.01	18.65	18.65
17.82	17.82	18.41	18.41
18.01	18.01	18.74	18.74
18.95	18.95	18.99	18.99
19.36	19.36	19.57	19.57
19.70	19.70	19.72	19.72

Feb. Columbia

X-Sect. Alley Block 13
Ocean Beach Park

From Ebers to Sunset Cliffs
Roberts between Muir and Voltaire

W. Moore

Clark

2-17-49

W.O. 25001

T.P. 696

T.P. 13, FB 1251, 1338

INDEXED

WIK

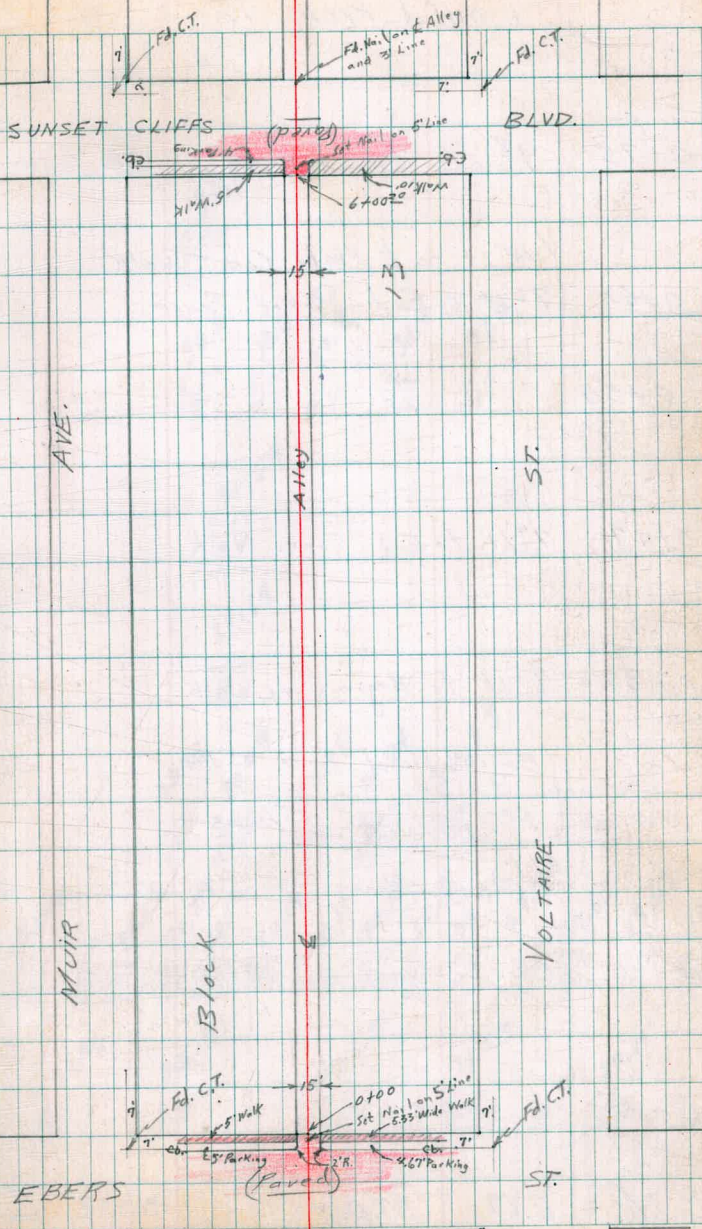
FEB 21 1949

Note

See page 7A for additional notes

CHD 5/4/50

50



Cont'd From Page 51

1737 115' Lt End. Conc. Apron.

1728 165' Lt to & Garage

1712 112' Rt to Opening Single Garage P to & Alley

1709 16.5' Lt to & Garage

1705 11.6' Lt. Begin Conc. Apron

T.P. 4.02 33.87 7.16 29.85

186' Lt. End Board Fence

1700 52' Lt Edge Board Fence Running N+S.

0799 7' Lt. to Center P. Pole # PA 4724

0792 8' Lt. to Begin Board Fence

0788 103' Lt to & 1' wide Walk

37.01

Lt.

30.37

Rt. 52

3.50
11.5
conc.

30.43

30.35

3.44
16.5
Floor

3.52
11.2
conc

30.3

3.6
11.2

30.46

30.37

3.41
16.5
Floor

3.50
11.6
conc.

30.39

3.48
11.6
conc.

33.87

30.4

30.0

29.8

29.8

30.1

4.6
15

7.0
25

7.2
22

7.2
25

6.9
15

30.21

4.80
103
conc.

37.01

Cont'd From Page 52

2719 18' Lt to W. End Double Garage

2701 { 6.7' Lt to Center P. Pole # PA. 4734
18' Lt to E. End Double Garage

270

2700 7.8' Lt End Board Fence

1794 12' Rt & Single Garage

1790 7.8' Lt to Begin Board Fence

1786 15' Lt to End 3 Car Garage

1762 15' Lt to Begin Three Car Garage

1750

1744 12' Lt to & Single Garage

33.87

Lt.

Rt 53

29.15
 $\frac{4.72}{18.4}$
Floor

29.08
 $\frac{4.79}{12.2}$
Comp.

29.19
 $\frac{4.68}{18.5}$
Floor

29.19
 $\frac{4.68}{12.3}$
Comp.

29.4

$\frac{4.5}{15}$

29.2

$\frac{4.7}{7.5}$

28.9

5.0

29.5

$\frac{4.6}{7.5}$

29.1

$\frac{4.8}{15}$

29.0

$\frac{4.9}{12.4}$

29.54

$\frac{4.34}{15.4}$
Comp.

29.59

$\frac{4.29}{7.6}$
Comp.

29.9

$\frac{4.0}{15}$

29.5

$\frac{4.1}{7.5}$

29.5

4.4

29.7

$\frac{4.2}{7.5}$

30.1

$\frac{3.8}{15}$

29.8

$\frac{4.1}{12.9}$

33.87

Cont'd From Page 53

2+94⁵ 17⁸' Rt to W. End Double Garage & Begin Board Fence

2+87. 7.6' Lt to Begin Board Fence

2+81 13⁴' Lt to & Single Garage

2+77 18¹' Rt E. End Double Garage

2+67 12³' Lt. to & Single Garage

2+55 12³' Lt to & Single Garage

2+50

2+43⁵ 8' Lt to W. End Porch (Bottom step)

2+34 7⁸' Lt to E. End Porch

33.87

Lt.

&

28.17 Rt 54
28.22

$\frac{5.70}{166}$
CONC.
 $\frac{5.65}{175}$
Floor

28.57
28.27
 $\frac{5.50}{134}$
Floor 1
 $\frac{5.60}{123}$
CONC.

28.22
28.33
 $\frac{5.65}{167}$
CONC.
 $\frac{5.54}{181}$
Floor

28.28
28.17
 $\frac{5.59}{123}$
Floor
 $\frac{5.79}{88}$
CONC.

28.3
 $\frac{5.6}{122}$

28.4
28.4
28.2
28.4
28.6
 $\frac{5.5}{15}$
 $\frac{5.5}{75}$
5.7
 $\frac{5.3}{75}$
 $\frac{5.3}{15}$

28.45
28.3
 $\frac{5.42}{8}$
CONC.
 $\frac{5.6}{8}$

30.19
28.1
 $\frac{3.08}{7.8}$
CONC.
 $\frac{5.2}{7.8}$

33.87

Cont'd From Page 54

3+70 78' Rt to & Single Garage

3+51

T.P. 4.52 32.27 6.12 27.95

3+50 72' Lt End of Picket + Begin Wire Fence

3+45 78' Rt to Edge Single Garage Tt to & Alley

3+29 { 75' Lt Begin Picket Fence
72' Lt. W. Edge Apron

3+18⁵ 132' Lt to & Single Garage

3+11⁵ 72' Lt End Board Fence + E. Edge Apron

3+01 62' Lt to Center P. Pole # PA 4750

3+00

33.87

Lt.

&

Rt. 55

27.3

5.0
7.8

27.1

4.6
1.8

27.5

4.8
7.5

27.9

4.9

27.8

4.5
7.5

32.27

27.7

6.2
7.8

27.70

6.17
7.2

conc.

28.13

5.74
1.2

floor

27.85

6.02
7.7

conc.

28.1

5.8
1.5

28.0

5.9
7.5

27.85

6.02
11.4.

27.9

6.0
7.5

28.2

5.7
1.5

33.87

Cont'd From Page 55

4+61 79' Rt Begin Board Fence

4+55 15 1/2' Lt to E. Edge Double Garage

4+50 13 1/2' Rt to E Double Garage

4+45 8 1/2' Lt End Board Fence

4+43 6 1/2' Rt End Wire Fence

8 1/2' Lt End Board Fence 8 1/2' Begin Board Fence

4+25 7 1/2' Rt End Board Fence Begin Wire Fence

4+66 1/2 7 1/2' Lt Begin Board Fence

4+00 7 1/2' Rt End Wire Fence Begin Board Fence

3+95 1/2 17 1/2' Lt to E Single Garage

3+90 1/2 8' Lt End Wire Fence

3+86 6 1/2' Lt to Center P. Pole # PA 4760

3+75 7 1/2' Rt Begin Wire Fence

32.21

Lt.

E

Rt.

56

27.63 27.38

4.64
15.4
Floor

4.89
12.3
conc.

27.4

27.3

27.0

27.2

27.54

4.9
15

5.0
7.5

5.3

5.1
7.5

4.73
13.5
conc.

27.2

27.2

27.1

27.6

27.6

5.1
15

5.1
7.5

5.2

4.7
7.5

4.7
15

27.51

4.76
17.2
conc.

32.27

Cont'd From Page 56

5721^E 7²' Lt Begin Board Fence

5715^E 6⁹' Rt Begin Board Fence

5710 10³' Lt & Double Garage

5706 12¹' Rt to & Single Garage

5706 6¹' Lt to Center P. Pole #PA4776

4799 8³' Rt End Board Fence

4797 7²' Lt End Board Fence

4787 7⁴' Lt Begin Board Fence

4765 10¹' Lt to & 3' wide Conc. Walk

4770 15⁴' Lt W. Edge Double Garage

32.27

Lt.

&

Rt. 57

26.9

5.4
10.3

27.32

4.75
12.1
Floor

27.2

5.1
15

27.0

5.3
7.5

27.0

5.3

27.0

5.3
7.5

27.53

4.74
10.7
conc.

27.62

4.65
15.4
Floor

27.37

4.90
12.3
conc.

32.27

Cont'd From Page 57

6+00.20 Prop. Line on Sunset Cliffs

86 to Bldg.

5+77 81' Rt to Edge Sidewalk continuation of Apron

5+71.5 98' Lt to Cor. Single Garage T.P. to E Alley

5+57 136' Rt E Single Garage

T.P. 4.50 31.37 5.40 26.87

5+51.5 68' Rt End Board Fence

5+50

5+49.5 75' Lt, End Board Fence

5+43 74' Rt End Apron

5+34 74' Rt Begin Apron on Foundation of Dwelling

32.27

58

26.98

4.39
8.9
conc.

27.00

4.37
9.8
conc.

26.79

26.95

4.58
8.8
conc.

4.92
13.6
Floor

31.37

27.3

27.0

26.7

26.9

5.0
15

5.3
15

5.6

5.2
7.5

26.90

5.37
7.4
conc.

26.91

5.36
7.4
conc.

32.27

Levels for Drainage of
Rear 4375-4414 St

1+50

TP 566 359.60 403 353.97

1+36 3rd Lt 5' high wire and wood fence

1+35 L. split of angle

1+50

0+50

0+10 East prop 4416 St

0+00 East curb line 4414 St.

BM 557 357.97 ✓ 352.40 NW.B.P. 4474 & Meade

Lt = North ✓ 2 354.2 Pt = South 61

54
10 54 354.2 354.2
52
85

359.60 ✓

354.0 353.94 354.17
42 403 38
10 10

353.4 353.6 353.9
42 44 44
10 10

353.4 353.4 354.2
42 42 42
10 8

353.7 353.5 353.9
46 45 42
10 10

357.99 352.74 352.64 354.18 353.53 354.98 354.27
5.98 5.23 5.23 3.79 4.44 2.29 3.20
50 50 50 50 50 50 50
100 100 100 100 100 100 100
NW.B.P. NW.B.P. NW.B.P. NW.B.P. NW.B.P. NW.B.P. NW.B.P.

357.97 ✓

2175

2150

2130 2nd Lt End wire fence begin 5th picket fence

2125

2195 1st Lt SE cor Shed wooden

2125 1st Lt NE cor wooden Shed

2100

1181 2nd Lt begin wire fence 3rd Lt End wire fence

1179 2nd Lt E power pole # PC 4383

1175

1168 5th Lt SE cor con porch

1162 5th Lt NE cor con porch

21	354.9	354.8	354.5	355.1	355.1
42	45	45	45	45	45
20	10	10	10	10	20

354.6	354.5	353.9	353.8	353.9
52	52	52	53	52
10	10	10	10	20

354.4	354.2	353.8	353.7	353.6
52	54	58	59	60
20	10	10	10	20

354.3	354.3	354.0	353.9	353.8
53	53	56	52	58
20	10	10	10	20

354.0	353.8	354.2	354.2
56	58	54	54
20	10	10	10

359.60

X sec Alleys
BLK 1 Alhambra Park

Moore
Begg
Shannon

W.O. 25020

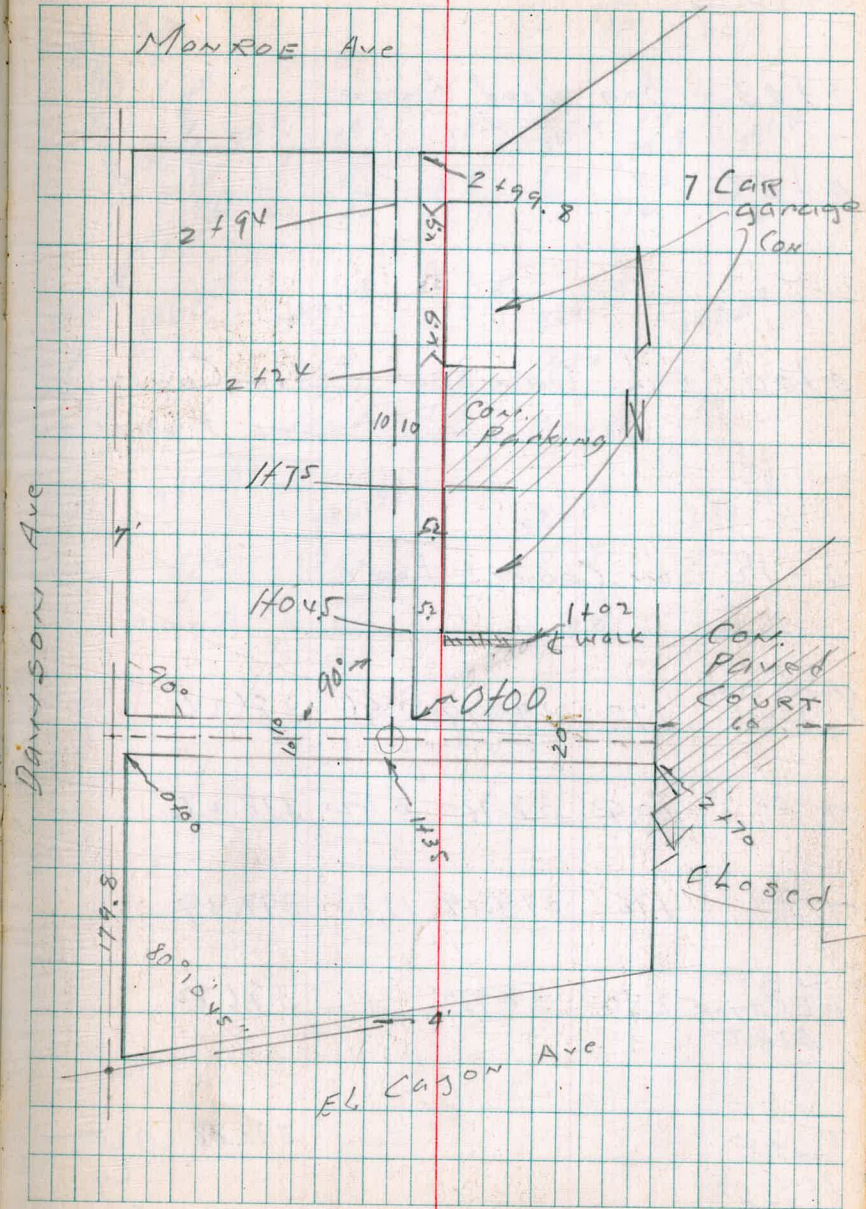
7-11-49

Ref. 1633-61

INDEXED

W.I.C.

JUL 12 1949



0711

0703 Beg. Wood fence

0702

0700 E.L. Dawson (under CONST.)
See PLAN

0-12 on Crown's Feet

T.P.
Chisel
S. RETURN
0-12

7.75 393.99 2.96 386.24

Use to
BM.

T.P. 10.93 389.20 0.92 378.27

T.P. 1.70 379.19 11.83 377.49

SWBP
EL CAYON 2.50 389.32 386.82
51ST

SWBP
EL CAYON
53rd
393.88 OUT
by
STATE

Reduced
by
J. Barnett

389.76 389.3 388.4 388.3 388.4 390.2 390.4
4.3 4.7 5.6 5.7 5.6 3.8 3.6

13.2 10 9 7 2 10 20
Sedge Drive

387.1 385.8 385.9 385.6 389.7 390.0
6.3 8.2 8.1 8.4 4.3 4.0
12 10 8 10 20

387.2 386.47 386.15 385.5 386.15 386.32
6.8 7.52 7.84 8.5 7.84 7.07
13.2 10 10 5.6 10 10
c6 crow ft. 9.1 crow ft.

385.83 386.37 386.24 385.74
8.16 7.62 7.75 8.25
12 10 10 12
crow ft. c6 c6 crow ft.

Sedge
El Yal Cond Dr.

393.99

2+70 = Wedge of Paired Count

2+59 CTR 18' Cabin

2+40

2+35 CTR 12' Cabin

2+15 CTR 12' Cabin

1+95 CTR 12' Cabin

1+70 CTR of 14' Cabin

1+65 S.E. Cor. Bd + Bar. House

1+57 NE Cor Stucco Motel

393.99

L

R

P 66

393.20

0.79

10
Car

392.5

1.5

20

392.7

1.3

10

393.16

0.83

10
Car.

392.6

1.4

10

393.09

0.90

10
Car.

392.8

1.2

10

Cabin
10.6

392.0

2.0

20

392.2

1.8

10

392.5

1.5

10

392.6

1.4

10

Cabin
10.6

Cabin
10.6

391.7

2.3

20

391.8

2.2

10

392.0

2.0

10

392.2

1.8

10

Cabin
10.6

Cabin
10.6

house
10.8

Motel
13

393.99

1700 Offsets to ctr of Poles

0475

0450 Bog. Wood fence

0434

0414 11.8 P. NW cor Cabin

0400 = N.L. E. W. alley Elev. P. 65

T.P. 4.42 $\frac{395.96}{343.99}$ 2.45 391.54

389.8 389.8 390.4 390.4
 $\frac{6.2}{20}$ $\frac{4.441}{10.1}$ $\frac{5.6}{10}$ 5.6

390.0 390.0 390.8 390.6 390.7 390.7
 $\frac{6.0}{20}$ $\frac{6.0}{12}$ $\frac{5.2}{10}$ 5.4 $\frac{5.3}{10}$ $\frac{5.3}{20}$

390.3 390.2 390.6 390.3 390.5
 $\frac{5.7}{20}$ $\frac{7.440}{11.2}$ $\frac{5.8}{10}$ 5.4 $\frac{5.7}{10}$ $\frac{5.5}{20}$

390.3 390.4 390.6 390.9 390.9
 $\frac{5.7}{20}$ $\frac{5.6}{10}$ 5.4 $\frac{5.1}{10}$ $\frac{5.1}{20}$

391.0 390.9 391.0 391.0 391.3
 $\frac{5.0}{20}$ $\frac{5.1}{10}$ 5.0 $\frac{5.0}{10}$ $\frac{4.7}{20}$

395.96

2 + 24

1799.5 C+R Con. Auto Park

200 end fence on Lt

1775 10.2 Lt to fence

1739.7 10.8 Lt. to fence

1704.5 Beg. 7' Can gar.

1702 & of 5' Can Walk

39596

68

390.5	390.6	391.0	391.2	391.5	391.99	Surf. Con.
$\frac{5.5}{20}$	$\frac{5.4}{10}$	$\frac{5.0}{8}$	4.8	$\frac{4.5}{10}$	$\frac{3.97}{14.9}$	gar. FC
390.3	390.3	390.8	391.1	391.6	391.95	
$\frac{5.7}{20}$	$\frac{5.7}{12}$	$\frac{5.2}{10}$	4.9	$\frac{4.4}{10}$	$\frac{4.01}{15.1}$	Con. Park Lot
		RP				
Fence		PA. 4x81				
$\frac{10.2}{10.2}$		$\frac{8.8}{8.8}$				
390.1	390.2	390.8	391.2	391.6	391.91	
$\frac{5.9}{20}$	$\frac{5.8}{11}$	Fence $\frac{5.7}{10.2}$	4.8	$\frac{4.4}{10}$	$\frac{4.05}{15.2}$	MW Con. gar.
389.9	389.9	390.5	391.1	391.5	391.91	
$\frac{6.1}{20}$	$\frac{6.1}{12}$	$\frac{5.5}{10}$	4.9	$\frac{4.5}{10}$	$\frac{4.05}{15.2}$	Con. gar. FC
389.7	389.8	390.4	390.6	391.0	391.90	
$\frac{6.3}{20}$	$\frac{6.2}{12}$	$\frac{5.1}{10}$	5.4	$\frac{5.0}{10}$	$\frac{4.04}{15.2}$	Surf. Con. gar. FC
					391.36	
					$\frac{4.60}{15.2}$	Walk.

39596

Check to Orig. B.M. 0.14 386.84 386.84
 T.P. 1315 386.94 11.00 373.81
 T.P. 075 384.81 10.34 384.06
 T.P. 282 394.40 4.38 391.58
 3+11.8 S. C. B. Monroe

2+99.8 S. C. B. Monroe See PLGN

2+94

2+82 P.P. J.P.A. 4491 8.5 LT

2+59

2+50 Beg. Picket fence

395.96

P 69

L E

390.0 390.36
 $\frac{5.96}{12}$ Crow ft. $\frac{5.60}{12}$ Crow ft.
 390.61 390.24 390.1 390.56 390.99
 End Fence $\frac{5.35}{10}$ $\frac{5.72}{10}$ $\frac{5.9}{10}$ $\frac{5.40}{10}$ $\frac{4.97}{10}$
 C6 Crow ft. Crow ft. C6
 391.2 391.4 391.8 391.9 392.04
 $\frac{4.8}{20}$ $\frac{4.5}{10}$ $\frac{4.2}{10}$ $\frac{4.1}{10}$ $\frac{3.92}{10}$
 NKV
 Cor
 7 Car-
 gar

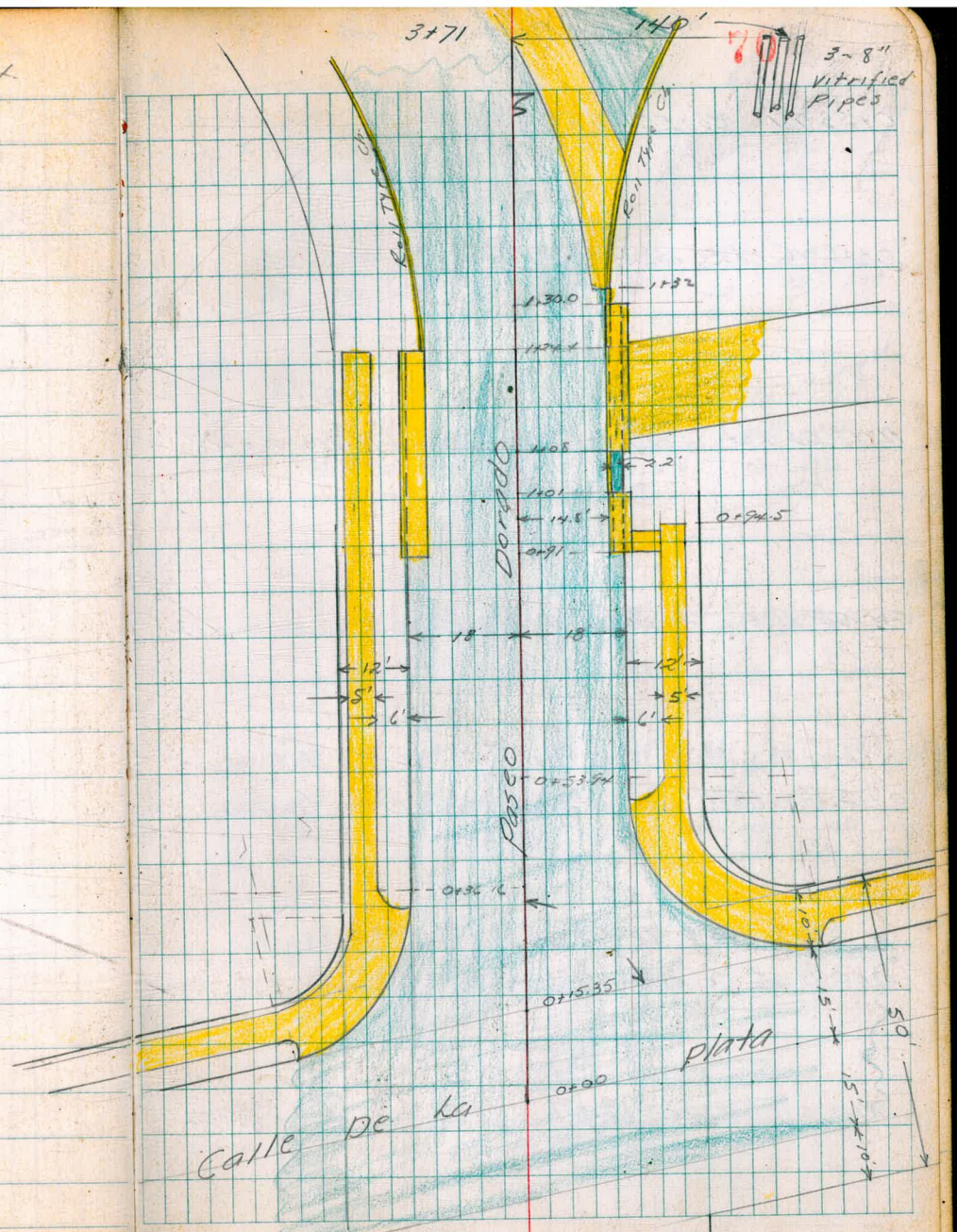
Fence
 $\frac{19}{10}$
 390.9 390.9 391.4 391.7 392.01
 $\frac{5.3}{20}$ $\frac{5.1}{10}$ $\frac{4.5}{10}$ $\frac{4.3}{10}$ $\frac{3.95}{10}$
 14.9 99-
 KC

Fence
10.1

395.96

9.21.49 X Sect Paseo Dorado
 Hendricks
 Roberts Calle De La Plata to West
 Greer
 Bunch
 WO# 25020

INDEXED
 W.K.
 SEP 22 1949



0+53.94 Cb. EC on Rt.

0+36.16 Cb. EC on Lt.

1111 Cb. Ret. 4 parts BC on La Plata L=48'

SW Cb. Ret. 4 parts BC on Calle De La Plata L=36'

0+15.35 West Cb. Line Calle De La Plata (Parallel to La Plata)

0+00 R Calle De La Plata (Parallel to La Plata)

BM L. 40 12.07
mm

7.67

5 ²³	5 ²⁹	6 ²⁵	6 ¹³	6 ¹⁵	6 ³⁷	6 ²¹	6 ¹⁹	6 ⁰⁹	6 ⁰⁷
29	24	18	18	8	9	18	18	24	29
SW	SW	Cb	G			G	Cb	SW	SW

5 ¹¹	5 ²³	5 ³⁰	5 ⁸⁸	5 ⁷⁶	6 ²²	6 ⁵⁶	6 ¹⁰	5 ⁶⁹
29	24	Cb	G		15	22	22	33.7
SW	SW	18	18		G	Cb		SW

5.84	6.41	5.74	5.53	5.95	5.88				
6 ²³	5 ⁶⁰	6 ³³	5 ⁸⁰	6 ¹⁴	6 ⁰¹	6 ⁵⁸	6 ¹²	6 ²¹	6 ¹⁹
G	Cb	G	Cb	G	Cb	G	Cb	G	Cb
BC									EC

5 ³⁰	5 ⁸⁸	5 ¹⁸	5 ⁴⁵	5 ⁹⁸	5 ⁴⁶	5 ⁷⁸	5 ²⁵	5 ²²	5 ⁰²
Cb	G	Cb	G	Cb	G	Cb	G	Cb	G
EC			(3)		(2)		(1)		BC

8.41	7.88	7.55	7.04	6.70	6.76	5.95	5.84	6.47	5.64	6.14
306	419	452	503	537	531	612	623	560	643	593
87	87	389	389	18		20	49.7	49.7	100	100
Cb	G	Cb	G				G	Cb	G	Cb
		BC						BC		

8.88	7.77	6.99	6.98	7.05	6.22	6.46	6.16
319	425	508	509	502	585	561	591
100	50	21	17		19	50	100

12.07

NEBP Pasco Dorado & Calle De La Plata

1430 End slab on Rt.

End SW on Lt.

1424.4 End slab & SW Lt.

1408 Beg. Slab over Drain on Rt.

1401 End slab on Rt.

0194.5 End SW on Rt.

0191 Beg. Conc. Slabs top of Drain 14.8' LL & RL

TP. 4.62 10.36 6.33 5.74
mm

4.39	4.71	4.62	5.22	5.0	6.98	5.20
15.9	15.2		14.6	14.6	16.6	18.6
CB	G		Pay	Slab	Drain	Slab
					€	Drain

A. 96

5.48	5.0	4.64	4.13	4.72	4.67	5.40	5.21	5.31	3.95
2.9	2.4	1.9	1.5	1.5		14.6	14.6	18.6	3.3
SW	Slab	Slab	Pay			Slab	Slab	Slab	Drain

5.23

4.70	4.69	5.09	4.77	4.78	5.50	5.13	5.62	6.21	6.38	5.83	5.0
18.61	14.8	14.8			14.8	14.8	(15.6	15.6	17.8	17.8	19.6
Slab	Slab	Pay			Pay	Slab	Top	Blm	(Blm Top)	(Blm Top)	Slab
							Drain		Drain		

5.24

4.71	4.67	5.20	4.81	4.82	5.19	5.08	5.42	6.13	6.26	5.68	5.06
18.6	14.8	14.8	6		14.8	14.8	15.6	15.6	17.8	17.8	19.6
SW	Slab	Pay			Pay	Slab	Top	Blm	(Blm Top)	(Blm Top)	Slab
							Drain		Drain		

5.45 5.34

2.4	2.9									5.22	5.33
SW	SW									2.9	2.4
											SW

A. 91

4.74	4.83	4.29	4.93	4.45	4.62	5.29	4.83	4.83	5.56	4.98	6.03	5.46	5.07	5.07
2.9	2.4	18.6	18	18	14.8	14.8	7		14.8	14.8	18	18	18.6	21.3
SW	SW	Slab	CB	G	Slab	Pay			Pay	Top	G	CB	Slab	
											Slab			

10.36
mm

BM 10.36 2.70 7.66

3+71 @ Dorado Projected
Outlet 3" 8" Vitrified Pipes 140' Rt.

1+50 @ Projected

Starting BM

112
140

5.81 6.18

4.50	4.72	4.56	4.55	4.55	4.5
192	185		10	21	22
C6	G			Per	C6

10.36

Alley BIK 13 Ocean Beach Park

Sommermeier

Begg

Allen

Sherman

5/4/50

INDEXED

W.O. 31 892

MAY 5 1950

Original notes on P. 50 - 58

top of. 0100 - 7¹/₂ ft. for chock 3.27 30.94 (30.93)

2+71 13⁵/₈ Rt. = end same

2+49 13⁵/₈ Rt. = start double Car. Conc. floor ^{no apron.}

1+00 7¹/₂ Rt. = end same

0+16 7³/₈ Rt. = start Conc. slab in back of ^{fire station}

T.P.	3.60	<u>34.21</u>	5.14	30.61
SW B.P.	5.63	35.75	—	30.12
Voltaire + Ebers				

74

Revised 5-5-50 P.K.S.

28.93
5.28
13⁵/₈
Car. floor

28.92
5.29
13⁵/₈
Car. floor

29.71
4.50
7¹/₂
on slab

29.88
4.33
15¹/₂
on slab

30.61
3.60
7³/₈
on slab

30.81
3.40
15⁵/₈
on slab at Bldg

34.21

Add. Elev. + Location of changes in
Data in Alley - Block 6 - Mt. View.

See Orig. X-Sect - P. 23

5635 9-13-51 - 7.0.

w.o. 31889

3+71 - 8.5 Rt. = ± w.M.

3+50 - 8.8 Lt. = ± w.M.

3+07 - 9.4 Lt. = ± w.M.

3+02 - 8.8 Rt. = ± w.M.

2+75 - 9 Rt. = ± w.M.

2+63 - 8.6 Lt. = ± w.M.

2+39 - 8.9 Rt. = ± w.M.

2+33 - 7 Lt. = ± w.M.

1+76 - 9.6 Rt. = ± w.M.

1+70 - 6.7 Lt. = ± w.M.

1+60 - 9 Rt. = ± w.M.

1+40 - 10.1 Lt. = ± w.M.

1+12 - 9.4 Lt. = ± w.M.

0+77 - 9.2 Rt. = ± w.M.

0+57 - 7.8 Lt. = ± w.M.

0+55 - 8.1 Lt. = ± w.M.

0+24 - 8.3 Rt. = ± w.M.

0+03 - 10 Rt. = end wall

0+00 - 10' Rt. = Beg. 6" Conc. wall

Actual Elev. shown

INDEXED

SEP 14 1951

			43.00 8.5 = pipe
42.31 8.8 pipe	42.18 9.4 = pipe		42.45 8.8 = pipe
		42.75 9 = pipe	
	41.62 8.6 = pipe		41.68 8.9 = pipe
41.65 7 = pipe		41.00 9.6 pipe	
	40.65 6.7 pipe		41.11 9 = pipe
40.30 10.1 pipe	40.19 9.4 pipe		
39.63 7.8 pipe	39.67 8.1 = pipe	40.70 9.2 pipe	
			39.44 = Top Pipe in Meter 8.3
		39.81 10 Bottom of wall at end.	40.11 10 = Top
			40.20 10 Top wall

5+60 - 9' Rt. = ± w.M.

5+44 - 8.4' Lt. = ± w.M.

4+99 - 8.5' Rt. = ± w.M.

4+95 - 7.5' Lt. = ± w.M.

4+77 - 8.1' Lt. = ± w.M.

4+64 - 8.8' Rt. = ± w.M.

4+38 - 9.6' Lt. = ± w.M.

4+10 - 9.8' Lt. = ± w.M.

Lt.

±

Rt. 76

46.36
9 = pipe

45.79
8.4 = pipe

44.93
7.5 = pipe

45.75
8.5
pipe

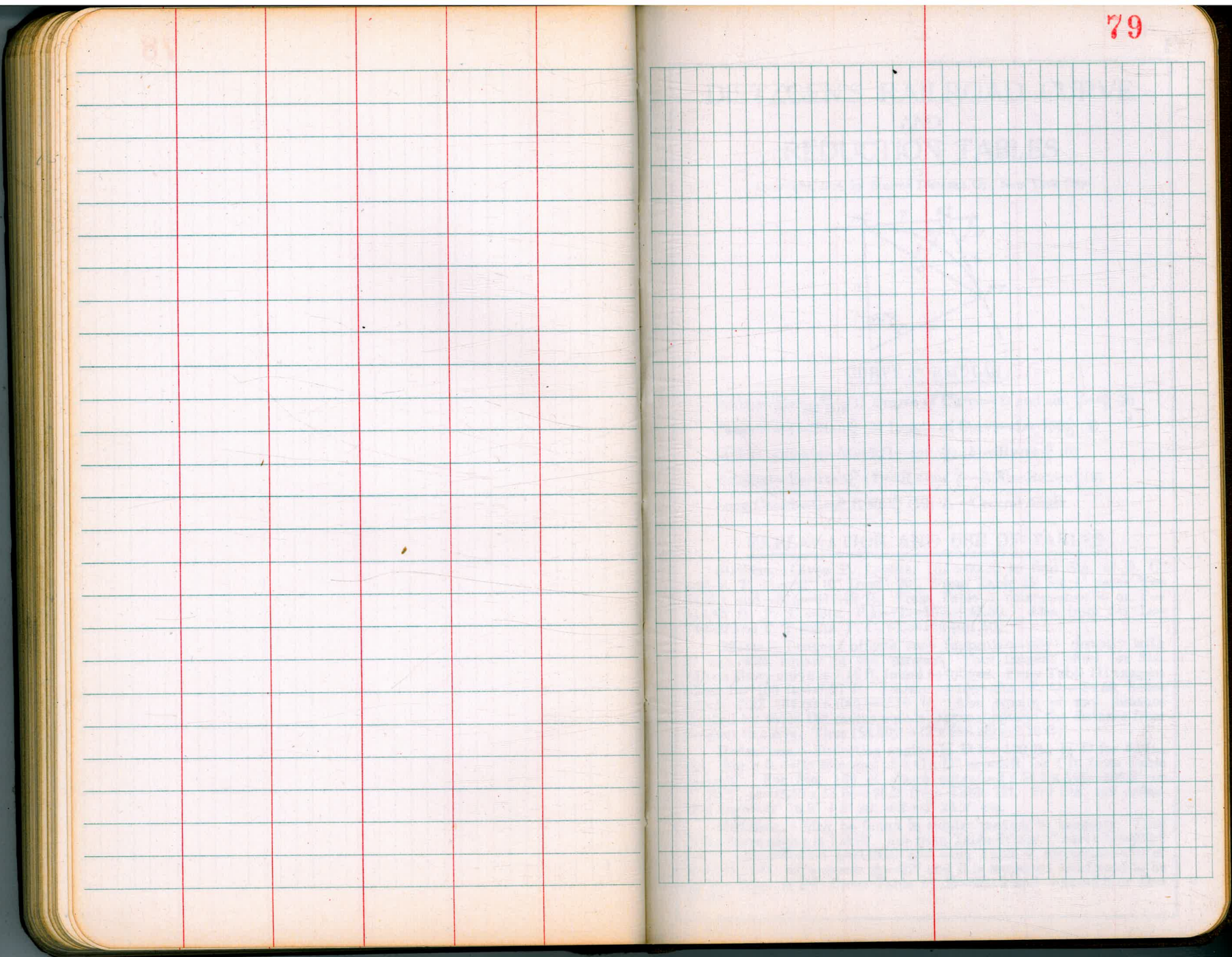
44.62
8.1 = pipe

44.51
8.8
pipe

43.63
9.6 = pipe

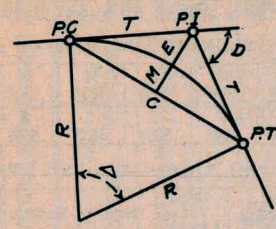
42.67
9.8 = pipe

A grid of 20 columns and 20 rows on a graph paper page. The grid is formed by light blue lines. A vertical red margin line is positioned on the left side of the grid, approximately one-fifth of the way across the page.



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

- Radius— $R = \frac{50}{\sin. \frac{D}{2}}$ (1) Degree of Curve— D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve— $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate— $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External— $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord— $C = 2 R \sin. \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction—.36 or $T = 414.85$ ft. P. C.—Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance—158—Sta. P. C.—54.50, hence offset— $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle— $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.—(in minutes) $.3 \times C \times D^\circ$ or—defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve—.3 $\times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or— $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction—.10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

Tank

Rack

High + wide - doors

4 - cove inside

702
633
269

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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