

1824

DIETZGEN

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ENGINEERS  
FIELD BOOK  
No. 103F

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# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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499.86  
90  
579.86

789  
187  
642  
79.9  
143

INDEXED

to page # 78

This Field Book is manufactured of a High  
Grade 50% Rag Paper having a WATER  
RESISTING SURFACE, and is sewed with  
Bing Special Enamel Waterproof thread.

Made in U. S. A.



Index

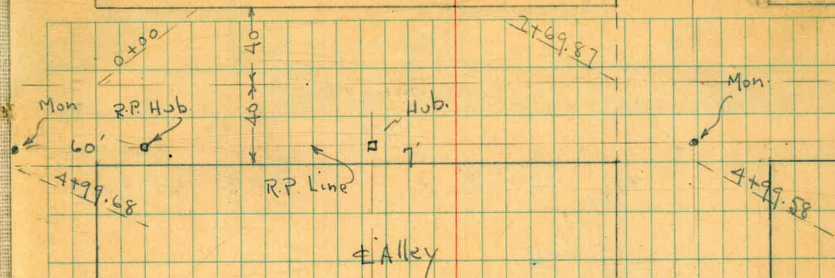
Pages

1-29 X-Sect. Thomas } Lamont to Olney.  
Reed }  
Oliver }

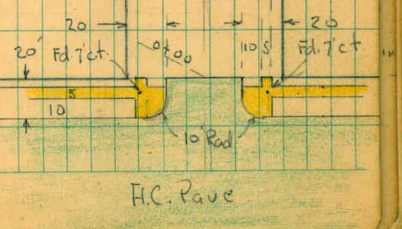
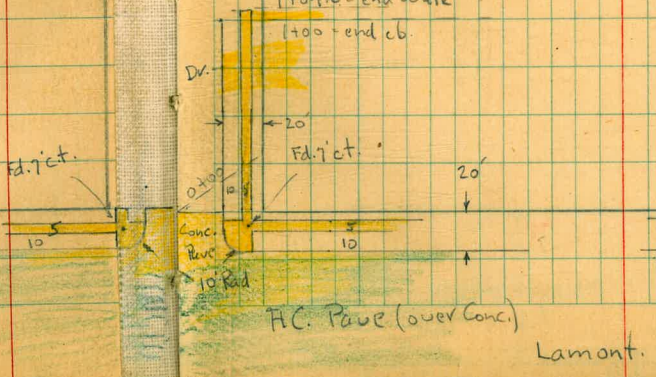
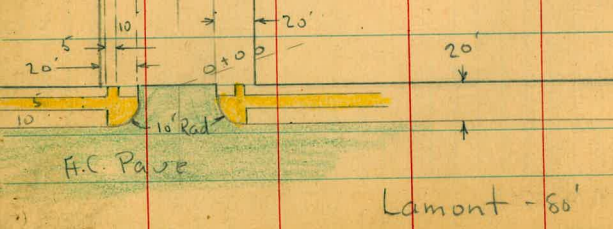
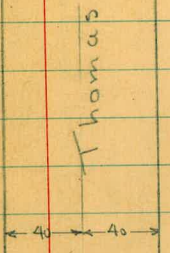
29-46 X-Sect. Morrell } Grand to Pac. Beach Dr.  
Noyes }  
Olney }

58-68 Diamond Oresham to 58-71  
Haines

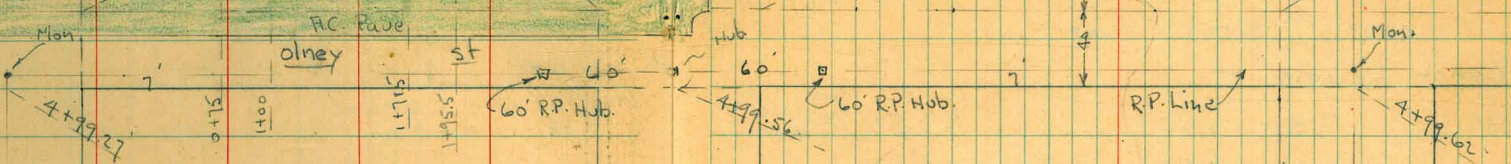
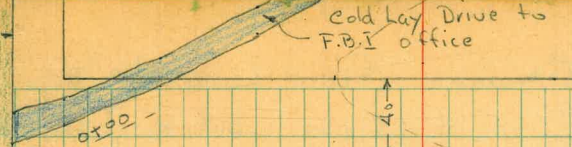
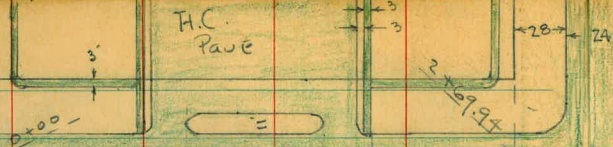




INDEXED  
MAY 21 1918







Edge of Tidal flats

INDEXED

← 40 → 40 →

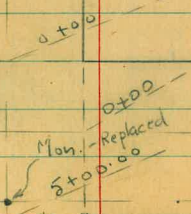
← 40 → 40 →

← 40 → 40 →

Thomas

Reed

Oliver



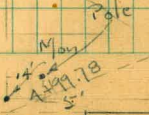
Noyes

2+69.92



70 R.P. Hub.

2+69.83



RP. Line

Fd. old Hub

Fd. old Hub

70 R.P. Hub.

90 R.P. Hub.

70 R.P. Hub.



X-Sect. Thomas - from Lamont  
to Olney - 80' st. 20' cbs. - Dirt Rough Graded.  
Levels - Next Page

W.O. 25001

4-30-48  
Osborne  
Hardin  
Worrell  
Rorer

Bench Levels -

B.M.	7.51	31.04		23.53
	9.76	38.70	2.60	28.44
	8.00	45.46	0.74	37.46
N.E. 7' ct. - Oliver + Lamont		5.11		40.35
T.P.	4.90	45.27	5.09	40.37
	10.36	52.12	3.51	41.76
	0.64	51.19	1.57	50.55
	3.38	45.14	9.43	41.76
	3.94	44.71	4.37	40.77
	3.37	38.65	9.43	35.28
	0.26	31.02	7.89	30.76

SW 7' Mon.  
Pac. Beach Dr.  
& Morrell

SE 7' ct.  
Reed + Lamont  
NE 10' in Ret.  
Thomas + Lamont  
NW B.P.

Thomas

N.E. 7' ct.

SW 7' Mon

Lamont

Grand + Lamont  
in Ret.

Pac. Beach Dr. + Lamont

Pac. Beach Dr.  
& Morrell

50.87 = Book elev. (seems to be wrong.)

35.28 - Book

23.53

check Starting B.M.



2.03

44.79

41.76 = Din Ret.

Rods around Returns - Thomas

+ Lamont.

S.E. Ret. 35.5 around - 5 parts - 7.1 each

Req - S. end = S.L. Thomas	4.08	40.71	T = Top
	4.64		q = gut.
7.1 N.	4.04	40.75	T
	4.60		q
"	3.97	40.82	T
	4.58		q
"	4.00	40.79	T
	3.49		q
"	4.02	40.77	T
	4.56		q
7.1 = end = E.L. Lamont	4.11	40.68	T
	4.56		q

N.E. Ret - 35.6 around - 5 - 7.1 each

Req - E. end = E.L. Lamont	3.03	41.76	T
	3.70	41.09	q
7.1 W	3.10	41.69	T
	3.74		q
"	3.16	41.63	T
"	3.78		q
"	3.16	41.63	T
	3.84		q

44.79

4

7.1

3.12

41.67

T

3.77

q

7.1 = end = N.L. Thomas

3.16

41.63

T

3.64

q















1+00

1+50

1+25

T.P. 6.94 31.98 13.27 25.04

1+00

0+84 - 28' Rt. - ± 18" Conc. walk

0+50

80' E = E.L. Morrell = 0+00 ahead.

60' E = E. cb.

40	32.61	31.01	24.71	11.2	27.11	50	28.58	29.08	Rt
20	33.11	31.01	27.61	11.4	26.91	40	27.98	28.38	
38.31	32.91	31.31	27.71	12.6	25.71	20	25.08	25.78	
20	33.11	31.71	28.81	13.8	24.81	50	27.58	27.98	
20	33.81	31.71	29.91	13.8	24.38	6	24.38	24.38	
20	34.71	31.21	29.91	13.8	25.31	20	23.98	23.08	
		31.21	28-walk	13.8	26.89	20	23.98	23.38	
		31.21	28-walk	12.2	26.11	40	24.48	24.28	
		31.21	28-walk	11.4	26.91	50	24.58	24.88	88
		31.21	28-walk	11.4	26.11	20	24.58	24.88	
		31.21	28-walk	11.4	26.11	20	24.58	24.88	











4+74- 21.2 Rt. = end Brick wall

4+71 - 22.1 Rt. = ± 3' Brick walk - Thru wall

4+50

4+49- 20.7 Rt. = Beg. 8' Brick wall - 2' High

4+36- 25.2 Rt. = ± 24' Pepper

4+12- 25.2 Rt. = ± 8' Pepper

4+00

3+75- 26.5 Rt. = ± 6' Pepper

T.P. 5.16 28.71 12.78 23.55

3+50

3+00

2+50

2+00

5 07	30.63	5 00	27.43	5 00	28.41	5 00	26.61
4 03	30.03	5 00	28.33	5 00	28.43	4 00	26.11
5 05	28.63	4 00	27.73	4 00	27.13	4 00	24.71
5 02	28.53	4 00	26.83	4 00	25.13	4 00	23.81
5 02	28.53	5 00	24.53	5 00	24.83	5 00	23.21
5 00	28.33	5 00	24.33	5 00	23.83	6 01	22.61
5 00	27.53	5 00	24.83	5 00	24.13	5 00	22.41
5 00	30.23	5 00	26.63	5 00	24.53	6 00	22.21
4 00	31.43	4 00	27.83	4 00	23.93	6 00	21.71
5 00	31.53	5 00	28.83	5 00	24.03	7 00	21.11
						5 00	20.91

36.33

Lt. Rt.

11

6.55  
21.2  
21.71  
22.1 walk  
22.21  
21.16  
21.91  
21.88  
21.2  
along wall  
20.91  
20.7  
along wall  
20.7  
21.16  
21.91  
21.88  
21.2  
along wall  
20.91  
20.7  
along wall



Lt.

±

Rt.

OLNEY Bet Grand + Thomas  
Set. B.M. - Top Hyd. - E. side 3.33 25.38

E. side OLNEY + Reed  
Set. B.M. on Top Hyd. Bet. Thomas 10.41 18.30

4 + 99.27 = w.l. Olney - See Olney Sect. for Int.

24.01

4.7  
40

23.21

5.5  
25

22.21

6.5  
20

21.41

7.3  
5

21.41

7.3

21.51

7.2  
20

20.61

8.1  
40

28.71



2.54 42.91

40.37 SE. 7' ct.

X-Sect. Reed - from Lamont to Olney  
Rods around Returns -

S.E. Return - 36 around. 5 parts - 7.2 each.

Beg. S. end = S.L. Reed. 2.68 40.23 T

3.28 9

7.2' W. 2.75 40.16 +

3.28 9

2.78 40.13 +

3.28 9

2.88 40.03 T

3.35 9

2.87 40.04 T

3.41 9

7.2' end = E.L. Lamont 2.90 40.01 T

3.48 9

NE Return - 36.3 around. 5 7.2 each.

Beg. E. end = E.L. Lamont. 3.33 39.58 T

3.88 9

7.2' W. 2.31 39.60 T

3.92 9

2.25 39.66 T

3.81 9

2.15 39.76 T

3.73 9

SEE ALSO PAGE 75

W.O. 25001

S-3-48

7.0.

13

7.2' 3.15 39.76 T

3.66 9

7.2' end = U.L. Reed. 3.11 39.80 T

3.67 9



Req. Reg. X - Sections of Reed - 80' st. - 20' cb.  
 Dirt - Rough Graded - checked 9-23-49,  
 7.0.

1+00 - end of cb. on Rt. } Sections Marked ✓  
 are the same  
 Changes shown in Red ✓  
 All figures are elevations  
 No Rods.

0+75 - ± 12' Conc. Dr. on Rt.

0+50 - 84.2 Rt. - ± 3.5 Conc. Walk

0+25

Joins N+5 walk at 0+50

0+12 - 39.1 Lt. - Sly, 2' Conc. walk along House +

cb. and walk in on Rt.

0+00 = E.L. Lamont - edge of Conc. Pav.

0-20 = E. cb.

0-40 = ± Lamont.

2.39 100	40.52	39.93	40.01	39.51	39.21	35.41	33.71
2.59 65	40.32	39.47	39.92	38.51	37.26	35.21	33.91
2.76 40	40.15	39.84	39.80	38.72	37.26	35.31	34.31
2.72 20	40.19	39.58	39.58	38.61	37.01	35.91	33.51
2.49	40.42	39.24	39.03	38.21	36.81	34.61	32.91
2.30	40.61	39.46	39.58	37.61	36.01	33.61	32.41
2.11 40	40.80	40.13	39.83	38.01	36.71	35.01	33.11
1.96 65	40.95	39.84	39.79	38.31	37.01	35.61	33.81
1.63 100	41.28	40.23	39.43	38.21	36.91	35.31	34.21
		39.88	40.01	38.78	37.30	36.32	34.45
		40.49	40.36	38.80	37.30	36.55	34.79
		40.27	40.49	38.01	36.71	35.55	34.83
		40.82	40.31	38.01	36.71	35.55	34.83







80' E. = E.L. Morrell = 0+00 ahead.

60' E. = E. cb.

40' E. =  $\Phi$  - change shown in red.

20' E. = w. cb.

1' E. = 26' Rt. =  $\Phi$  16" Pepper  
4+99.68 = W.L. Morrell

4+97- 243 Rt. = Nly P. pole # J.P. - 1999  
4+79- 39.8 Rt. =  $\Phi$  3' Conc. walk

4+50 = 40' Lt. =  $\Phi$  6 Dr. - 2-18" Conc. Strips  
to Sing Gar. - Conc. floor

4+26- 26' Rt. =  $\Phi$  18" Pepper

4+15- 40' Lt. =  $\Phi$  7 Conc. Dr. - To Sing Gar. - Conc. floor

4+05- 67.5' Rt. =  $\Phi$  Sing. Gar. Conc. floor - Dirt Dr.

4+00

50	34.66	32.01	30.70	29.10	29.00
40	30.40	31.32	30.60	29.60	29.50
30	28.80	30.00	30.20	30.00	29.50
20	27.70	29.00	30.00	29.20	29.50
10	27.20	28.60	29.80	29.60	29.10
0	27.20	28.50	29.70	29.60	29.00
10	26.90	28.90	29.70	29.60	29.00
20	26.70	28.40	29.70	29.60	29.00
30	26.80	28.00	29.70	29.60	29.00
40	26.96	28.44	29.70	29.60	29.00
50	26.96	28.44	29.70	29.60	29.00



2+32-28' Lt. = \$ 8" Tree  
 2+26-21.6 Lt. = end fence  
 2+00

1+58-28.5' Lt. = \$ 24" Palm  
 1+50

1+37-28.5' Lt. = \$ 30" Palm  
 1+47-40.6 Lt. = \$ 3' Conc. walk  
 1+25-22.4 Lt. = Beg. Picket fence

T.P. 0.22 21.74 12.38 21.52

1+00  
 0+85-24.5 Rt. = Nly. P. pole - \$ P-20 17

0+75

0+50

0+25

0+22-40.2 Rt. = \$ 3.3 Conc. Walk

50	30.01	50	28.90	50	27.40	50	22.64	50	22.64
40	29.60	40	28.40	40	27.20	40	21.14	40	21.14
30	29.30	30	27.70	30	26.60	30	21.74	30	20.24
20	28.70	20	26.80	20	25.80	20	19.44	20	19.44
10	28.20	10	26.20	10	25.10	10	18.74	10	18.74
0	28.10	0	26.70	0	25.00	0	18.54	0	18.54
50	28.00	50	26.60	50	25.10	50	18.84	50	18.84
40	28.30	40	27.00	40	25.50	40	19.44	40	19.44
30	28.14	30	26.80	30	25.10	30	19.34	30	19.34
20	28.20	20	27.20	20	24.90	20	19.24	20	19.24
10	28.19	10	27.20	10	24.90	10	19.24	10	19.24
0	28.19	0	27.20	0	24.90	0	19.24	0	19.24







T.P. 6.90 26.34 1.08 19.44

0+26 - 37.8 Lt. = 3 Conc walk

80' E. = E.L. Noyes = 0+00 ahead.

60' E. = E. cb.

40' E. =  $\pm$  -  $\pm$  Sewer M.H.

20' E. = W. cb.

4+99.78 = W.L. Noyes

4+99 - 24.9 Rt. =  $\pm$  Pipe # P-2099

4+60

4+30 - 54.7 Rt. =  $\pm$  Uly. Long. Bldg.

4+25

5.9	12.62	12.72	15.62	17.32	17.02	18.52	20.25
5.0	8.3	8.3	8.9	8.2	4.0	4.0	5.0
8.3	12.22	12.22	14.72	14.72	16.52	16.52	19.40
8.3	8.3	8.3	8.9	8.2	4.0	4.0	5.0
9.1	11.42	11.42	13.12	13.12	14.42	14.42	15.72
9.1	8.8	8.8	9.0	9.0	9.0	9.0	9.0
10.0	10.52	10.52	12.22	12.22	13.57	13.92	14.42
10.0	9.0	9.0	9.0	9.0	9.0	9.0	9.0
10.8	10.72	10.72	12.6	12.6	13.72	13.72	14.22
10.8	9.9	9.9	10.6	10.6	11.22	11.22	11.72
10.8	11.22	11.22	12.6	12.6	13.22	13.22	14.02
10.8	9.9	9.9	10.6	10.6	11.22	11.22	11.72
10.9	10.92	10.92	12.6	12.6	13.22	13.22	14.02
10.9	9.9	9.9	10.6	10.6	11.22	11.22	11.72
11.0	11.0	11.0	12.6	12.6	13.22	13.22	14.02
11.0	9.9	9.9	10.6	10.6	11.22	11.22	11.72
11.0	10.92	10.92	12.6	12.6	13.22	13.22	14.02
11.0	9.9	9.9	10.6	10.6	11.22	11.22	11.72
11.7	11.7	11.7	12.6	12.6	13.22	13.22	14.02
11.7	9.9	9.9	10.6	10.6	11.22	11.22	11.72

20.52



2+58- ~~54.6~~ Lt. # 8' Conc. Dr. to Sing. Gar-  
 Been Extended. Conc. floor

2+50 ✓

2+13 - 39.8' Lt. = # 3.5 Conc. Walk

2+00 ✓

1+75 ✓

1+50 ✓

1+20 ✓

1+00 - 25.4 Rt. = # of P. pole # 2121

0+90 ✓

0+50 ✓

26.34	20.54	23.64	24.34	24.01	23.69
17	50	50	50	50	50
9.2	6.4	23.64	24.34	24.01	23.69
19.14	19.94	24.24	24.19	23.33	23.26
6.5	40	40	40	40	40
19.84	22.09	23.64	23.04	23.16	23.26
6.6	40	40	40	40	40
19.74	21.04	22.84	22.54	22.84	21.84
6.6	50	50	50	50	50
19.84	19.74	21.74	22.04	22.24	21.04
6.5	60	60	60	60	60
19.84	20.94	20.64	21.64	21.84	21.04
6.5	50	50	50	50	50
16.34	18.94	21.04	21.54	20.24	20.94
17	60	60	60	60	60
16.64	19.44	19.84	20.34	19.84	20.19
20	60	60	60	60	60
15.64	18.84	19.14	19.84	19.74	19.94
40	40	50	50	50	50
15.14	18.64	19.74	19.74	19.74	19.94
50	50	50	50	50	50







Dirf - Samples taken for Reed  
175' E. of E.L. Noyes - S. side

80' W. of W.L. Morrell - S. side

Set T.P. 12.85 8.67

check B.M. - Top Hyd. Bet. Reed + Thomas 3.21 18.31 P. 12 14.30

4+99.56 = W.L. Olney

4+89 - 26' Lt. =  $\pm$  - end Tree in Row - 1" Hacia

4+83 - 41.6 Rt. =  $\pm$  25' Conc. walk

4+75

4+63 - 38.4 Lt. =  $\pm$  3' Brick walk

Lt.

Rt.

1.15	12.4	1.5	19.82	1.7	19.62	1.9	18.72	4.2	17.32	3.1	18.42	4.2	17.32	4.5	17.02
48.4	38.4	15	19.82	17	19.62	28	18.72	12	17.32	20	18.42	12	17.32	50	17.02
walk	walk	50	20.02	40	19.62	20	18.72	36	17.92	20	18.42	40	17.62	50	17.30

21.52



X-Sect. Oliver - Lamont to Olney  
Rods around Returns

S.E. Return 35.7 Ground - 5 parts - 7.1 each

Req. S. end - S.L. Oliver	4.69	40.12	T
	5.30		g
7.1 N.	4.64	40.17	T
	5.20		g
"	4.70	40.11	T
	5.31		g
"	4.65	40.16	T
	5.31		g
"	4.64	40.17	T
	5.28		g
7.1 = end = E.L. Lamont	4.62	40.19	T
	5.22		g

4.46 44.81

40.35

N.E. Tct.  
Oliver +  
Lamont.

44.81

N.E. Return 35.5 around - 5' - 7.1 each

Req. E. end = E.L. Lamont	4.79	40.02	T
	5.36		g
7.1 - W	4.71	40.10	T
	5.32		g
"	4.67	40.14	T
	5.27		g
"	4.71	40.10	T
	5.30		g
"	4.65	40.16	T
	5.15		g
7.1 = end = N.L. Oliver	4.55	40.26	T
	5.10		g











3+00

2+50

2+00

1+50

1+00

0+91 - 51.6 Lt. = ± 3' Conc. walk

0+50

80' E. = E.L. Morrell = 0+00 ahead.

60' E. = E. cb.

40' E. = ±

19.16  
2.24  
61.6  
walk

50	13.30	50	18.65	50	18.00	50	16.30	50	17.00	50	17.00	50	18.50	50	18.65	50	18.00		
40	12.80	40	18.50	40	16.70	40	16.30	40	16.70	40	16.30	40	16.70	40	18.50	40	16.70	40	16.30
30	12.30	30	17.40	30	15.30	30	16.00	30	15.70	30	15.30	30	16.00	30	17.40	30	15.30	30	15.70
20	11.80	20	14.40	20	14.10	20	14.90	20	15.20	20	14.90	20	14.10	20	14.40	20	14.90	20	15.20
10	11.50	10	14.00	10	13.80	10	14.50	10	15.20	10	14.50	10	13.80	10	14.00	10	14.50	10	15.20
0	10.20	0	13.80	0	12.70	0	13.60	0	13.80	0	13.60	0	12.70	0	13.80	0	13.60	0	13.80
10	9.70	10	13.50	10	12.20	10	12.80	10	12.70	10	12.80	10	12.20	10	13.50	10	12.80	10	12.70
20	9.30	20	12.90	20	10.90	20	12.50	20	11.80	20	12.50	20	10.90	20	12.90	20	12.50	20	11.80
30	9.30	30	14.40	30	10.50	30	11.60	30	11.80	30	11.60	30	10.50	30	14.40	30	11.60	30	11.80
40	10.00	40	14.00	40	10.40	40	11.00	40	10.80	40	11.00	40	10.40	40	14.00	40	11.00	40	10.80
50	10.00	50	13.70	50	10.00	50	10.70	50	10.00	50	10.70	50	10.00	50	13.70	50	10.70	50	10.00

21.40











check T.P. P. 22

3.43 8.67

T.P. 5.53 12.04

2.62 6.51

B.M. on  $\pm$  W. 7 Mon.

11.03 -1.90  
-1.84

4+99.62 = W.L. Olney

4+50

4+15 - 40' Lt. = E. edge of Slough

3+65 =  $\pm$  on E. edge of Slough

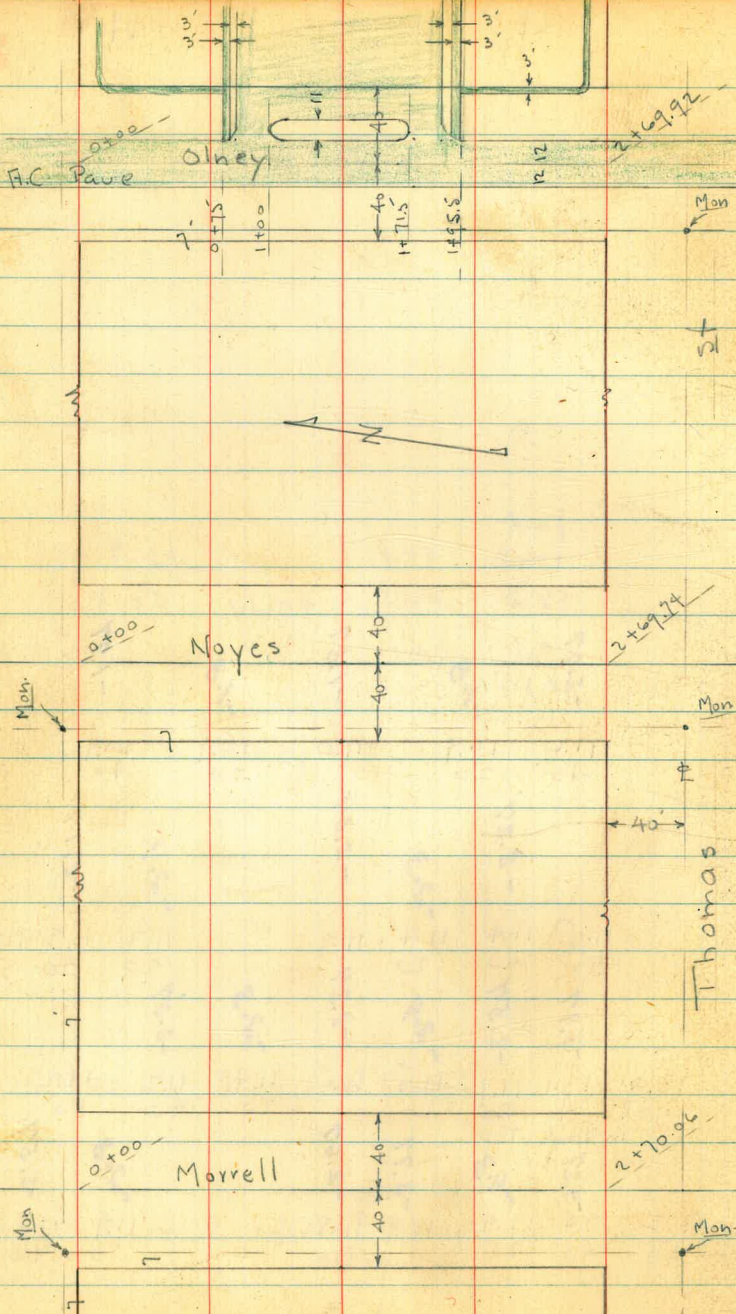
13.0	13.0	13.0	11.4	11.4	11.0	10.9	10.9
50	50	50	40	20	40	40	40
3.97	3.97	3.97	2.57	2.4	2.07	1.8	1.8
-2.27	-2.27	-2.27	-2.3	-2.3	-1.87	-1.8	-1.87
13.2	13.4	13.4	12.9	11.8	11.4	11.2	11.2
50	40	20	in slough	top	20	40	50
3.77	3.77	3.77	2.67	2.3	2.07	1.8	1.8
-2.67	-2.67	-2.67	-2.3	-2.3	-1.87	-1.8	-1.87
11.9	11.7	11.6	11.9	11.7	11.2	11.3	11.4
20	40	50	20	40	40	40	50
2.8	2.57	2.57	2.1	2.17	1.8	1.87	1.87
-2.8	-2.57	-2.57	-2.1	-2.17	-1.8	-1.87	-1.87

9.13



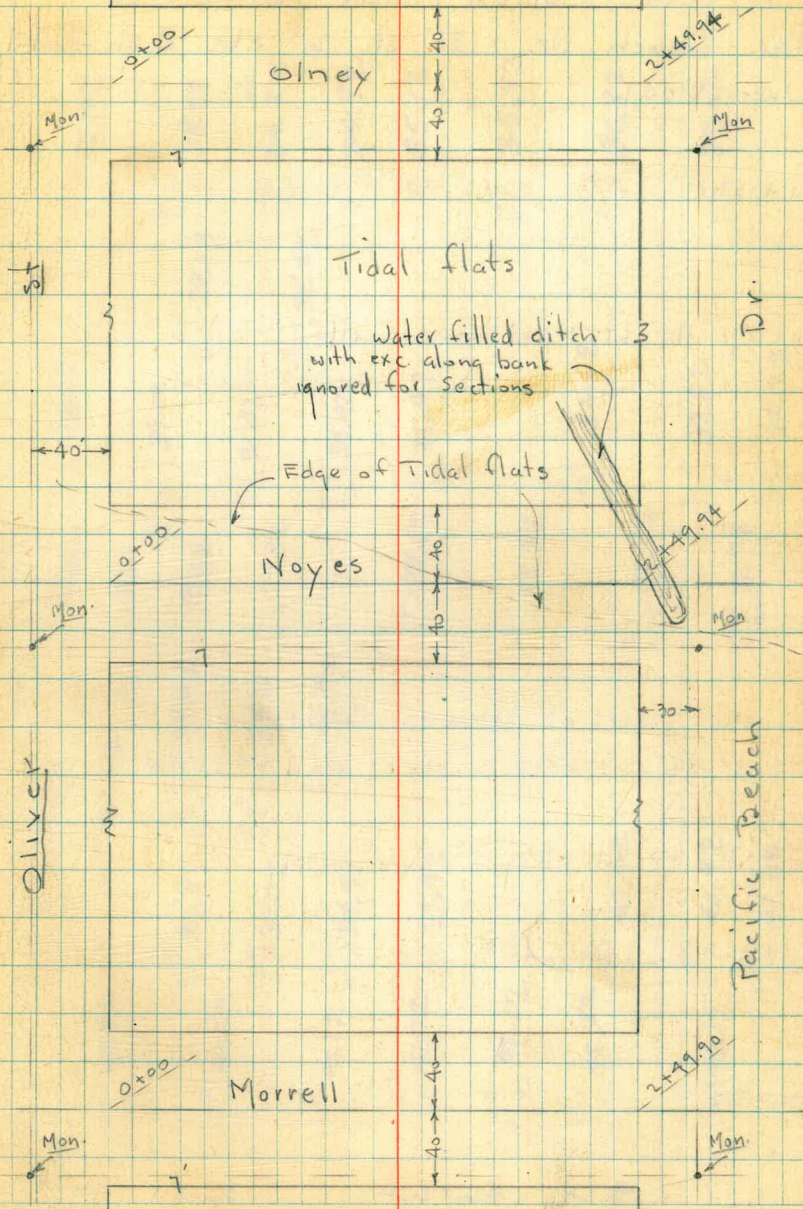
Hue

Grand



See Page 1+2 for other streets.

Tidal flats









1+00

to be Gar.)

0+91- 34.8 Rt. = 12' Conc. apron to House (used

0+75- 40.9 Rt. = Sing. Car - Conc floor

Dirt Drive

0+59- 69.2 Rt. = Sing. Car - Conc floor

0+50

0+00 = SL Thomas

See Thomas Sections for Int.

2+70.06 = NL Thomas

T.P. 3.11 39.61 9.62 36.50

2+40

2+00

55 0	29.82	55 0	33.82	55 0	34.82	55 0	34.82	55 0	34.82	55 0	34.82
45 0	30.42	45 0	30.82	45 0	31.42	45 0	31.82	45 0	32.42	45 0	32.82
35 0	31.01	35 0	31.01	35 0	31.01	35 0	31.01	35 0	31.01	35 0	31.01
25 0	31.01	25 0	32.61	25 0	34.21	25 0	34.21	25 0	34.21	25 0	34.21
15 0	32.62	15 0	32.52	15 0	34.71	15 0	34.51	15 0	34.51	15 0	34.51
5 0	34.42	5 0	34.42	5 0	35.01	5 0	34.81	5 0	34.81	5 0	34.81
45 0	34.82	45 0	34.52	45 0	35.21	45 0	35.21	45 0	35.21	45 0	35.21
35 0	34.42	35 0	35.92	35 0	36.81	35 0	35.11	35 0	35.11	35 0	35.11
25 0	35.72	25 0	36.52	25 0	36.41	25 0	35.91	25 0	35.91	25 0	35.91
15 0	36.42	15 0	36.42	15 0	36.31	15 0	35.71	15 0	35.71	15 0	35.71
5 0	36.42	5 0	36.42	5 0	36.31	5 0	35.71	5 0	35.71	5 0	35.71

46.12



0+29-39.8' Rt. = ± 3' Conc. walk  
T.P. 1.68 31.43 9.86 29.75

0+00 = 2.L. Reed.  
See Reed Sections for Int.

2+70.03 = N.L. Reed.

2+40

2+20-40 Rt. = ± 2' Conc. walk

2+00

1+82-39.7 Rt. = ± 4' Conc. Walk

1+62-38.7 Rt. = ± 7' Dr. - 2.2' Conc. strips

1+50

1+35-0.9 Rt. = ± Sewer M.H. 5.51 on rim

5 32.81	5 30.61	5 29.01	5 30.91	5 29.11	5 30.71	5 30.81	5 31.11	5 30.71	5 30.81	5 31.11	5 30.91	5 31.51	5 31.81	5 32.21
6 33.21	6 31.61	6 31.31	6 32.01	6 32.01	6 31.11	6 32.01	6 31.11	6 30.71	6 32.01	6 31.11	6 30.71	6 31.51	6 31.81	6 32.21
6 33.31	6 32.01	6 32.01	6 32.21	6 32.01	6 32.01	6 32.21	6 32.01	6 30.71	6 32.01	6 32.01	6 30.71	6 32.61	6 33.01	6 32.72
6 33.41	6 33.66	6 33.66	6 33.41	6 33.41	6 32.41	6 33.66	6 33.41	6 33.01	6 33.41	6 32.41	6 33.01	6 33.71	6 34.62	6 34.51
6 33.81	6 34.30	6 34.30	6 34.31	6 34.31	6 34.31	6 34.30	6 34.31	6 33.71	6 34.31	6 34.31	6 33.71	6 34.51	6 34.62	6 34.51
6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51	6 34.51



0+00 = S.L. Oliver

See Oliver sections for Int.

2+69.87 = N.L. Oliver

T.P. 7.72 26.38 12.77 18.66

2+40

2+00

1+75

1+50

1+00

0+65 = Sing. Gar. on Lt. - Conc floor + apron

0+50

30 28.42

43 28.29  
floor apron

50 28.43

60 28.23

70 28.33

80 28.43

90 25.23

100 27.43

110 24.83

120 26.63

130 24.63

140 27.63

150 23.53

160 26.23

170 22.83

180 21.83

190 21.53

200 21.43

210 23.23

220 20.13

230 23.43

240 19.43

250 26.93

260 15.18

270 16.53

280 16.63

290 19.83

300 16.53

310 16.38

320 15.48

330 13.48

340 17.38

350 15.28

360 15.08

370 17.28

380 17.28

34

31.43



check B.M. SW 7 Mon. Pac. Beach Dr. + Morrell 2.84 23.54 23.53

20'S

2+4990 - N.L. Pac. Beach Dr.

2+00

1+50

1+00

0+50

0+25

12.68	19.58	19.48
13.38	17.78	20.58
13.98	16.68	21.08
15.58	18.08	21.98
17.58	18.58	23.08
18.68	19.68	23.48
19.38	19.88	24.08
19.68	20.88	24.18
19.78	21.38	24.58
19.78	22.18	25.18

26.38



X-Sect Noyes - from Grand to  
Pac Beach Dr. - 80' st. - 20' cbs. - Rough  
Graded to Reed.

W.O. 25001

5-19-48  
7.0

1+50

1+35 = Sewer M.H. 9.35 on Rim

1+00

0+50

0+20

0+00 = S.L. Grand

0-25

8.41 41.51 4.52 33.10  
1.12 37.62 36.50

N.W. Pipe  
Thomas &  
Morrell

Indep

36

Lt. = E. #

Rt. = W.

34.31	34.71	34.81	34.51	34.01
34.41	34.71	34.81	34.21	33.91
35.71	33.81	32.21	33.31	33.51
35.21	33.01	31.41	32.41	33.01
35.51	32.51	30.81	31.61	32.31
32.81	31.71	30.41	30.81	31.61
36.61	30.61	30.01	30.81	30.41
36.51	30.51	29.51	30.81	29.51
35.71			29.51	

41.51



2+17 - 51.7 Lt. = ± 2' Conc. walk

2+00 = ± Prop. Gar. on Lt. - Conc found.

1+50

1+35 - 1' Rt. = ± Sewer M.H. 8.09 on Rim

1+00 = Nly. of House on Lt. - Conc floor + apron

0+50

0+00 = S.L. Thomas

T.P. 0.91 34.01 8.41 33.10

See Thomas Sections for Int

2+69.74 = N.L. Thomas

2+40

2+00

50	7.4	34.11	5.5	34.01	2.3	31.41	3.0	31.01	4.9	29.72	4.9	29.72	11.2	24.55	1.7	22.85
40	32.81	33.71	4.0	33.11	3.3	30.71	4.0	30.71	4.6	29.41	4.6	29.41	10.6	23.41	1.7	22.45
33	32.11	32.91	3.3	32.41	2.8	29.91	2.8	29.91	5.0	29.01	5.0	29.01	10.6	23.41	1.7	22.45
20	32.91	32.31	2.8	31.71	2.0	29.71	2.0	29.71	2.9	28.91	2.9	28.91	2.0	22.71	1.7	22.45
8	32.61	32.31	2.3	31.31	1.0	29.61	1.0	29.61	6.3	27.71	6.3	27.71	11.2	22.81	1.7	22.45
20	31.51	30.91	1.0	30.21	2.0	27.61	2.0	27.61	8.5	25.51	8.5	25.51	13.1	20.91	1.7	22.45
40	30.61	29.41	1.0	30.21	4.0	26.41	4.0	26.41	10.5	23.51	10.5	23.51	15.0	19.01	1.7	22.45
11	30.11	28.71	1.2	28.91	5.0	24.11	5.0	24.11	11.2	22.31	11.2	22.31	16.0	18.01	1.7	22.45
6	30.11	28.91	1.2	28.91	11.2	22.91	11.2	22.91	12.9	21.11	12.9	21.11	16.0	18.01	1.7	22.45

41.51



2+40

2+00

1+50

1+00

T.P. 0.58 9.55 12.43 8.97

0+50

0+00 = S.L. Reed - Not Graded from Here S.

See Reed for Int.

2+70.21 = N.L. Reed

2+40 Sly. of House on Lt

T.P. 0.42 21.40 13.03 20.98

23.95	20.10	18.00	15.60	14.60	13.35	11.15	9.45	8.35	7.35	6.35	5.55	4.65	3.35	2.15	1.15	0.45
20.90	19.80	17.90	17.30	15.70	14.70	13.70	12.70	11.70	10.70	9.70	8.70	7.70	6.70	5.70	4.70	3.70
20.40	19.40	17.40	16.40	15.40	14.40	13.40	12.40	11.40	10.40	9.40	8.40	7.40	6.40	5.40	4.40	3.40
20.00	19.00	17.00	16.00	15.00	14.00	13.00	12.00	11.00	10.00	9.00	8.00	7.00	6.00	5.00	4.00	3.00
12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80	12.80
10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30	10.30
8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80	8.80
8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50	8.50
7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30	7.30
6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30	6.30
5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55	5.55
4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65	4.65
3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35
2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15	2.15
1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15	1.15
0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40	21.40
34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91	34.91



30' S.

2+49.94 = N.L. Pac. Beach Dr.

T.P. 5.91 5.23 10.23 -0.68

2+00

1+50

1+24.8 - 0.4' Rt. =  $\pm$  sewer 9.94 <sup>M.H.</sup> Top Rim

1+00

0+50

0+00 = S.L. Oliver.

check B.M. - spike in pole <sup>P. 27</sup> 4.96 4.59 ✓ 4.63  
~~4.57~~

See Oliver for Int.

2+69.83 = N.L. Oliver

8.4 50	8.5 40	8.4 20	8.4 40	8.1 20	4.7 40	4.8 40	6.0 30
	-3.27		-3.17		-1.57	Sledge Sewer Rim	2.939
8.4 50	8.5 40	8.4 20	8.4 40	7.9 20	6.8 40	6.0 30	6.0
	-3.15		-3.15		-1.65		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-2.95		-2.85		-1.45		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-2.76		-2.15		0.23		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-2.76		-2.85		1.25		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-2.15		-1.75		0.15		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-2.65		-1.95		2.55		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-1.55		0.55		2.35		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-0.55		1.85		3.75		
12.5 50	12.6 40	12.3 20	12.4 40	12.0 20	10.6 40	9.7 30	
	-0.05		1.7		5.15		

9.55



X- Sect. Olney - from Grand to  
 Pac. Beach Dr. - 80' St. - 20' cbs. 24' strip  
 of H.C. Pavc in Middle to Reed.  
 W.O. 25001 5-20-48  
 7.0

1+00 = Nly Dirt Island on Lt.

0+81 = Nly of H.C. Parking Area. - See sketch P. 30

3' H.C. walk

0+75 = 27' Lt. end 3' walk at N. edge of F+W

0+50

0+14 = 27' Lt. = Wly. 3' Coldlay Walk

0+00 = S.L. Grand

0-25

5.92 31.30

25.38

Top Hyd.  
 S. Grand  
 P. 12

Lt. = F. INDEFINITE = W. 40

	22.87	23.06	24.23	24.55	24.17	24.81	25.10	26.70	26.50	26.80
8.43	8.24	7.7	6.75	7.13	6.49	6.2	4.6	4.8	4.6	4.5
50	40	17.5	12.75	12	12	20	25	40	40	56
23.26	23.26	23.45	25.09							
8.04	8.04	7.85	6							
87.5	87.5	40	2							
N.E. Cor.										
H.C.										
24.20	24.22	24.26	25.50	26.08	25.50	26.11	26.70	28.00	28.40	28.90
7.1	7.04	7.04	5.8	5.52	5.19	4.6	3.3	2.9	2.4	
50	40	37	20	2	580	20	27	40	50	
25.18	25.70	25.90	26.60	27.44	26.77	27.46	27.90	29.30	29.90	30.40
6.12	5.4	4.7	3.86	4.53	3.90	3.4	2.0	1.4	0	
27' walk			edge	edge	edge	edge	30	40	50	
26.60	26.80	27.30	27.96	27.46	27.98	28.30	28.50	28.60	28.60	30.40
4.90	4.5	4.0	3.34	3.84	3.32	3.0	2.8	2.7	2.7	
	40	20	12	12	12	20	40	40	50	
			edge	edge	edge	edge	edge	edge	edge	
			Pave.	Pave.	Pave.	Pave.	Pave.	Pave.	Pave.	
					31.30					



20' S. = N. cb.

T.P. 2.63 22.37 11.56 19.74

2+69.92 = N.L. Thomas

2+56-37' Lt. = end wly, 3' walk

12.90  
37  
walk

2+40 = Govt. House on Lt.

2+00

of 3' AC walk to S.

1+95.5 = sly. 3' E+W. AC Walk + 37' Lt. = Beg. Wly.

1+89.5 = sly. of AC Parking

1+71.5 = S. end Island.

1+35 - 0.2 Lt. = Sewer M.H.

6.4	15.97
100	
5.1	16.27
70	
5.3	17.07
40	
3.7	18.67
20	
2.18	20.19
12 edge	
2.63	19.74
208	
12 edge	
1.7	20.29
20	
0.2	20.67
40	
0.2	22.17
40	
	41
14.0	20.96
50	
13.5	18.10
40	
12.62	18.68
40	
12.58	18.72
20	
10.62	20.20
12	
11.1	21.46
20	
9.90	20.82
2	
10.48	21.75
2	
9.85	21.45
12	
10.54	21.90
12	
10.3	21.00
20	
8.1	23.20
28	
7.2	24.10
40	
7.1	24.20
28	
6.1	25.20
40	
5.7	25.50
55	
5.7	26.50
55	
10.84	20.46
50	
13.2	18.10
50	
12.62	18.68
40	
12.58	18.72
20	
10.62	20.20
12	
11.1	21.46
20	
9.90	20.82
2	
10.48	21.75
2	
9.85	21.45
12	
10.54	21.90
12	
10.3	21.00
20	
8.1	23.20
28	
7.2	24.10
40	
7.1	24.20
28	
6.1	25.20
40	
5.7	25.50
55	
5.7	26.50
55	
10.91	20.89
40	
10.86	20.44
37	
9.54	21.76
20	
8.89	22.41
12	
8.90	22.46
2	
8.98	22.32
12 edge	
8.38	22.92
12 edge	
8.0	23.30
20	
6.8	24.50
35	
6.1	25.20
40	
5.1	25.80
55	
5.1	25.80
55	
11.54	19.76
85	
11.25	20.05
50	
10.91	20.39
40	
9.54	21.76
20	
8.90	22.46
12 edge	
8.98	22.32
12 edge	
8.38	22.92
12 edge	
8.0	23.30
20	
6.8	24.50
35	
6.1	25.20
40	
5.1	25.80
55	
5.1	25.80
55	
10.6	20.62
50	
10.31	20.99
40	
9.07	22.23
20	
8.46	22.85
12 edge	
7.99	23.96
12 edge	
7.99	23.31
12 edge	
8.38	22.92
12 edge	
8.0	23.30
20	
6.8	24.50
35	
6.1	25.20
40	
5.1	25.80
55	
5.1	25.80
55	
10.31	20.99
40	
9.07	22.23
20	
8.46	22.85
12 edge	
7.99	23.96
12 edge	
7.99	23.31
12 edge	
8.38	22.92
12 edge	
8.0	23.30
20	
6.8	24.50
35	
6.1	25.20
40	
5.1	25.80
55	
5.1	25.80
55	

31.30



1+16 = 41.3 Rt = \$ Shed - Conc floor.

1+00 = Nly. of Dirt Island on Lt.

0+81 = Nly. of F.C. Pavc - Parking area.  
see sketch P 2

0+75 = 37 Lt. = end N+S. walk at Nly. of E+W. walk

0+50

0+28 = 49.8 Lt. = \$ Gowt House

0+14 = 37 Lt. = Beg Wly. of 3' HC walk

80' S. = S.L. Thomas = 0+00 ahead.

60' S = S.cb

40' S = \$

6.9	15.47	7.8	15.07	6.26	16.11	5.4	14.97	2.5	14.87	8.39	13.02	13.98
100	70	6.5	15.87	6.9	15.47	5.4	14.97	2.5	14.87	8.39	13.02	13.98
40	5.7	16.67	16.97	6.3	16.07	4.0	15.37	1.3	15.03	7.86	14.85	14.51
20	4.0	18.37	18.27	4.4	17.97	2.0	15.42	6.0	16.28	6.56	16.21	15.81
20	2.6	19.75	19.25	3.4	18.90	2.0	17.68	5.5	17.20	6.25	16.12	16.12
20	3.1	19.27	18.83	4.0	18.35	2.0	17.13	5.5	17.20	5.53	16.83	16.54
20	3.0	19.36	18.80	3.5	18.80	2.0	17.60	5.5	17.20	6.09	16.28	16.28
20	2.6	19.76	19.17	3.2	19.17	2.0	17.77	5.4	17.77	5.58	16.79	16.79
20	2.0	20.24	20.27	2.1	20.27	2.0	18.47	4.8	18.47	5.4	16.97	16.97
40	1.0	21.37	20.67	1.7	20.67	5.0	18.77	4.4	18.77	4.8	17.57	17.57
40	1.0	21.37	20.67	1.7	20.67	5.0	18.77	4.4	18.77	4.4	17.97	17.97

Lt

Rt

Rt

42

4.00

41.3 = floor

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

U.F.C.

= end walls

floor

ground

edge

edge



T.P. A.78 18.33 8.82 13.55

2+69.94 = N.L. Reed

2+56 - 37' Lt. = Wly. end 3' walk

9.72  
3'  
walk

2+40 - 49.8 Lt. = ♀ Gout. House

8.92  
49.8  
floor

2+00

AC N+S Walk

1+95.5 = Sly. 3' AC-E+W. Walk. + 37' Lt. = Beg. Wly. of 3'

1+89.5 = Sly. of AC. Pave - Parking

1+71.5 = Sly. of Island

1+35 = 0.3 Lt. = ♀ Sewer MH.

check B.M. Top Hyd. in Island. P. 12 4.07 18.30 18.30

11.67	12.17	12.76	12.87	14.27	14.47	15.33	17.51	15.77	19.47
6.7 50	10.2 49.8 ground	9.6 40 walk	9.50 37	8.0 20	7.52 12	8.66 12	7.43 12	6.1 20	3.3 40
12.17	12.76	13.11	13.29	14.37	14.85	14.31	14.94	16.27	18.57
10.2 50	9.6 40	9.50 37	8.0 20	7.52 12	8.66 12	7.43 12	6.1 20	3.3 40	19.37
13.09	13.33	14.88	15.07	15.46	14.87	15.49	16.97	18.57	19.47
9.28 40	9.04 37	7.49 20	6.91 12	7.50 12	6.88 12	5.4 20	3.3 40	2.9 40	19.97
10.33	12.96	14.86	15.49	15.51	15.51	15.51	16.77	18.37	19.77
12.04 80 50	9.41 40	7.51 20	6.88 12	6.88 12	7.16 12	6.42 12	5.6 20	4.0 40	4.3 40
12.57	13.37	15.35	15.59	15.21	15.89	16.77	18.37	18.87	19.77
9.8 50	9.00 40	7.02 20	6.1 12	7.16 12	6.42 12	5.6 20	4.0 40	4.3 40	5.0 50
13.13	13.73	15.25	16.20	15.64	16.27	16.77	18.07	18.97	
9.24 50	8.64 40	7.12 23	6.17 12	6.73 12	6.10 12	5.6 20	4.3 40	5.0 50	
		end Island	edge of Island.	on MH					
				22.37					











30' S. = end.

2+49.94 = N.L. Pac. Beach Dr.

2+00

1+50

0.16

1+24.7 - 0.4 Lt. Sewer M.H. 5.86

on Top  
Rim

1+00

0+50

	-2.1	-2.4							
7.8	8.1	8.4	9.6	9.4	6.9	6.9	7.1	7.0	7.0
50	40	30	20	13	9	20	20	40	50
7.9	7.5	3.9	3.9	1.5					
7.6	8.2	8.3	9.6	9.6	7.2	7.0	7.1	7.3	7.4
50	40	30	20	15	11	20	20	40	50
	-2.2	-2.8	-3.9	1.4					
	7.9	8.5	9.6	7.1					
	50	40	30	20					
	2.5	3.8	1.5						
8.2	9.5	7.2							
60	40	20							
	3.3	-2.8	-2.5						
	9.0	8.5	8.1						
	50	40	20						
	3.1	-3.1	-2.8						
8.8	8.8	8.5							
50	40	20							

57.0



X-Section Grand Ave. from  
Pendleton to Lamont

N.O. 25001

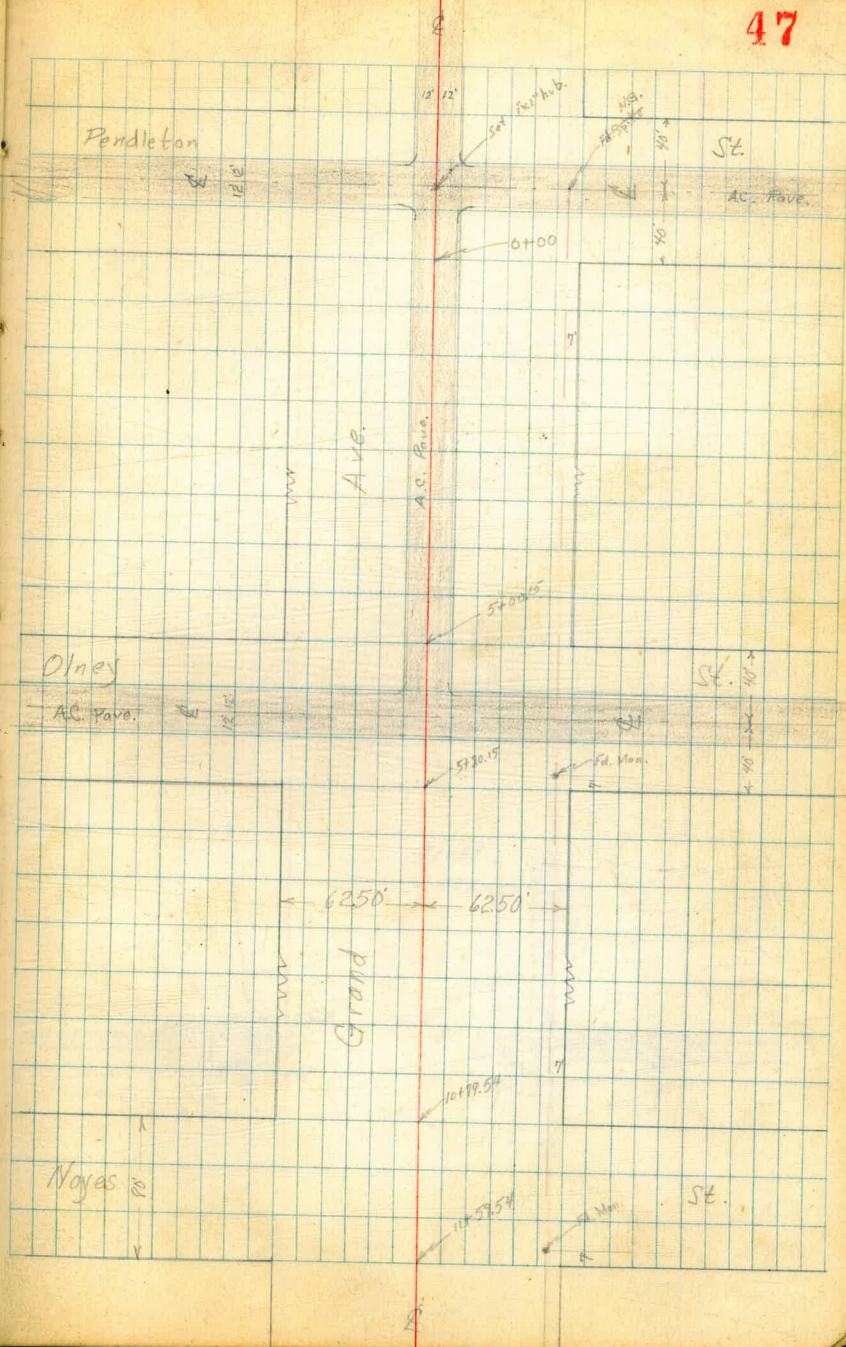
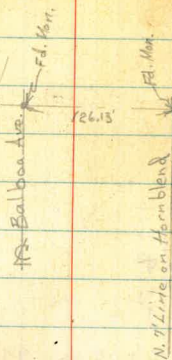
7-1-48

Roberts  
Greer  
Rorer

2440

INDEXED

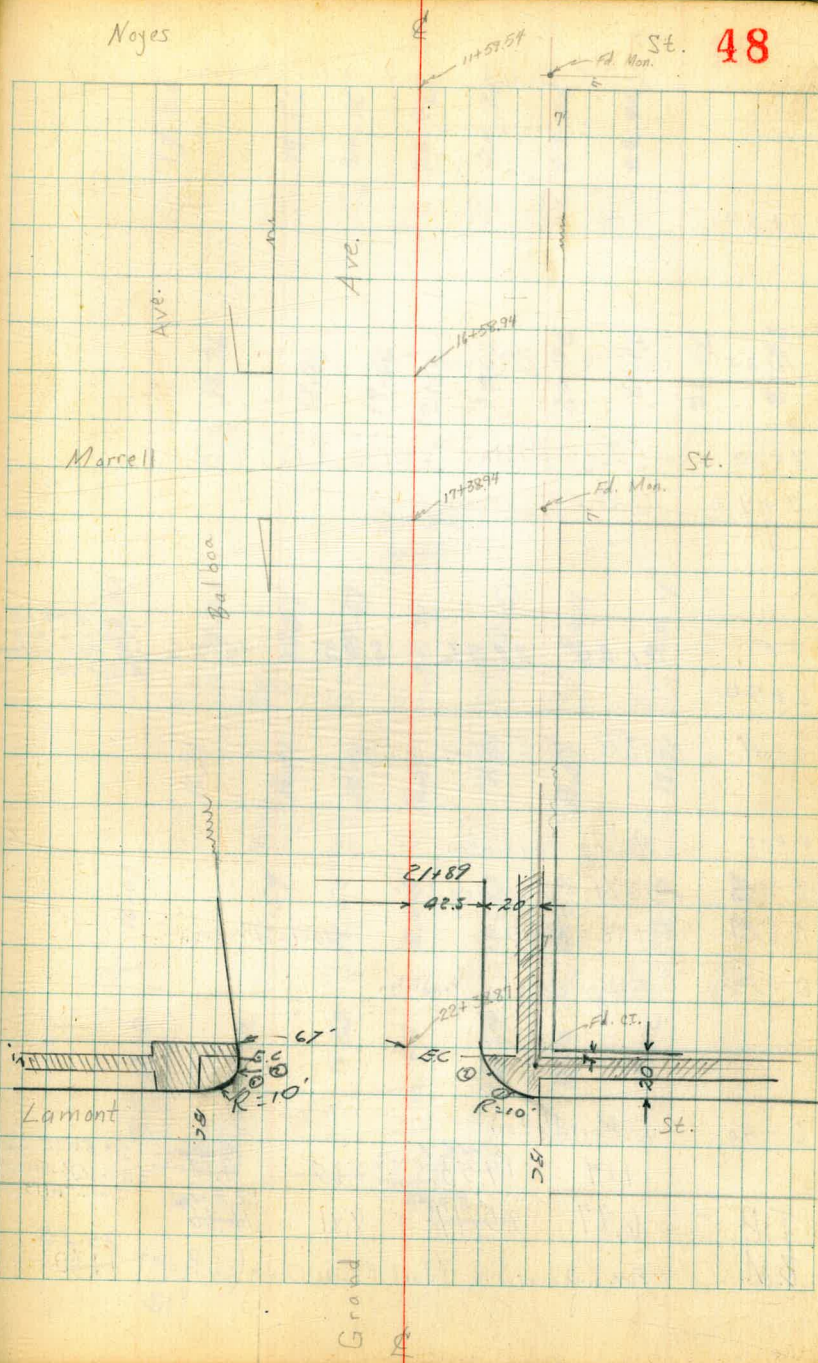
JUL 12 1948





Nojes

48





X-Section Grand from W. line Pendleton  
to E. line Lowmont.

1+50

1+03 45.5' Lt. = 3" Cypress Tree

1+00 45.5' Lt. = P. Pole #2271

0+92 42' Rt. = 8" Cypress Tree

TP 11.30 27.56 8.35 16.26

0+50

0+41 47' Lt. = 3" Eve. Tree

0+00 W. Line Pendleton

0-03 44' Lt. = 6" Cypress tree

0-21 61' Rt. = P. Pole 40' Rt. = Dead man

0-28 W. Edge paving on Pendleton

0-40 & Pendleton

1.17 ~~24.61~~  
~~17.53~~ 8.35

T.P. 6.87 ~~25.17~~ 8.81 ~~23.44~~  
~~16.36~~

B.M. Fire hydrant in Island E. Side Olney (See Pg. 43)  
12

Set BM in  
Pole #413  
SE Pendleton  
& Grand

Set BM in Pole  
Spoke SE Pendleton  
& Grand #413

25.38  
19.30

Lt.

Rt.

Rt. 49

17.26  
8.3  
72.5

19.56  
8.0  
62.5

20.76  
6.8  
72

20.96  
7.1  
72

20.96  
6.6  
72

22.06  
5.5  
28

22.96  
5.1  
62.5

18.76  
8.8  
72.5

18.96  
8.6  
62.5

19.66  
7.9  
72

19.66  
8.4  
72

19.66  
7.9  
72

20.76  
6.8  
20

21.16  
6.4  
35

21.66  
5.9  
62.5

21.86  
5.9  
72.5

27.56  
1.40

17.81  
6.8  
72.5

18.01  
6.6  
62.5

18.51  
6.1  
32

18.57  
6.1  
72

17.71  
6.7  
67

18.57  
6.1  
72

22.11  
4.5  
62.5

20.11  
4.5  
72.5

16.31  
8.3  
72.5

16.61  
8.0  
62.5

17.41  
7.2  
72

16.81  
7.8  
72

17.71  
7.2  
72

18.57  
6.1  
62.5

18.71  
5.9  
72.5

16.01  
8.60  
72.5

16.59  
8.02  
32

16.55  
8.06  
72

16.25  
8.36  
72

16.73  
7.88  
72

18.57  
7.92  
32

18.19  
6.42  
62.5

18.37  
6.24  
72.5

15.38  
9.23  
82.5

15.62  
8.99  
62.5

16.23  
8.38  
72

15.97  
9.64  
72

16.54  
8.07  
72

17.89  
6.72  
62.5

18.02  
6.59  
72.5

24.61



4+00

3+98

44' Lt = P. Pole #P2215

3+95

44' Lt = 6" Cypress tree

T.P.

9.75 34.78  
27.70 2.53 25.03  
14.95

3+50

3+17

15.2' Lt. = End Picket Fence

3+00

2+67

15' Lt. = Begin Picket Fence

2+50

2+00

1+79.5

43.5' Rt. = 8" Cypress Tree

20.48  
25.62

24.78	25.28	26.18	25.98	26.48	25.88	27.28	28.78
$\frac{10.0}{72.5}$	$\frac{9.5}{62.5}$	$\frac{8.6}{57}$	$\frac{9.8}{52}$	9.3	$\frac{8.9}{52}$	$\frac{7.5}{44}$	$\frac{6.0}{32.5}$
23.86	24.36	25.36	25.16	<del>24.56</del>	25.06	26.26	27.56
$\frac{3.7}{72.5}$	$\frac{3.2}{62.5}$	$\frac{2.2}{49}$	$\frac{2.4}{42}$	3.0	$\frac{2.5}{42}$	$\frac{1.3}{29}$	$\frac{0.0}{62.5}$
22.76	23.06	24.16	24.16	23.66	24.16	24.96	26.06
$\frac{4.8}{72.5}$	$\frac{4.0}{62.5}$	$\frac{3.4}{47}$	$\frac{3.4}{42}$	3.9	$\frac{3.4}{42}$	$\frac{2.6}{31}$	$\frac{1.5}{62.5}$
20.16	20.46	21.76	21.96	22.56	23.16	24.86	24.86
$\frac{2.4}{72.5}$	$\frac{2.1}{62.5}$	$\frac{5.8}{47}$	$\frac{5.6}{42}$	5.0	$\frac{4.4}{33}$	$\frac{2.9}{62.5}$	$\frac{2.7}{72.5}$
20.96	21.76	21.96	21.96	21.96	22.06	22.86	23.76
$\frac{2.4}{72.5}$	$\frac{2.1}{62.5}$	$\frac{5.8}{47}$	$\frac{5.6}{42}$	6.1	$\frac{5.5}{42}$	$\frac{4.7}{30}$	$\frac{4.1}{62.5}$

34.78

27.70

27.56

20.48







9+00

1.9  
72.5

41.93

8+50

8+00

7+95

58' Lt. = 8" Kopper Tree

T.P.

12.39

~~23.83~~  
~~36.00~~

3.34

~~31.44~~  
~~24.36~~

7+50

7+00

6+92

49.5' Lt. = 2 Board Steps

6+63

53' Lt. = 4 Conc. Steps 4.3 wide

6+63

6+50

~~34.78~~  
~~34.78~~

42.43	40.23	35.53	33.13	33.53	32.13	33.53	33.13	33.13	34.23	31.13	39.03
1.4 72.5	3.6 72.5	8.5 72.5	10.1 72.5	10.3 72.5	11.2 72.5	10.3 72.5	10.7 72.5	10.7 72.5	9.6 72.5	6.1 72.5	4.2 72.5
40.73	40.73	36.53	33.23	33.73	32.53	32.93	32.93	32.93	33.93	31.13	45.33
2.9 72.5	3.1 72.5	7.3 72.5	10.6 72.5	10.1 72.5	11.3 72.5	10.9 72.5	10.8 72.5	10.7 72.5	9.9 72.5	6.1 72.5	4.5 72.5
38.23	38.03	38.08	33.03	32.23	32.43	32.33	32.33	32.33	33.33	35.53	40.13
5.6 72.5	5.8 72.5	5.4 72.5	18.8 72.5	11.6 72.5	11.4 72.5	11.5 72.5	11.2 72.5	10.6 72.5	10.5 72.5	8.3 72.5	3.7 72.5
37.38	37.18	29.98	29.38	30.68	30.68	31.68	31.58	32.18	32.28	32.68	39.78
1.25 72.5	4.2 72.5	3.8 72.5	3.7 72.5	3.1 72.5	3.1 72.5	3.2 72.5	3.2 72.5	3.2 72.5	2.1 72.5	4.7 72.5	4.8 72.5
32.78	32.78	28.38	28.38	29.78	29.78	29.78	29.78	30.78	30.78	32.78	31.18
2.0 72.5	2.0 72.5	6.4 72.5	6.4 72.5	5.3 72.5	5.3 72.5	5.3 72.5	5.3 72.5	4.0 72.5	4.0 72.5	2.0 72.5	2.4 72.5

34.78

Rt. 52



12+50

12+08

11+59<sup>54</sup> W. Line Noyes

T.R 10.63 43.55 10.91 52.92 = Mon. SW Cor Noyes + Grand

11+19<sup>54</sup> E Noyes

10+79<sup>54</sup> E. Line Noyes

10+50

10+00

9+50

43.83

10.6	9.2	7.4	7.6	6.9	7.0	7.1	5.3	4.3	6.0	6.7
72.5	62.5	24	18	10	7.0	7	15	49	62.5	72.5
32.95	34.35	36.15	35.95	36.65	36.55	36.45	38.25	39.25	37.55	36.85
12.4	10.3	6.9	6.2	7.6	7.6	4.9	5.1	4.3	5.3	6.7
72.5	62.5	35	22	17	7.4	17	20	63	62.5	72.5
31.15	33.25	36.65	37.35	35.95	36.15	38.15	38.15	39.25	38.25	39.15
12.4	10.3	6.9	6.2	7.6	7.6	4.9	5.1	4.3	5.3	6.7
72.5	62.5	35	22	17	7.4	17	20	63	62.5	72.5
32.63	32.83	34.03	34.33	37.23	35.83	35.83	37.13	39.03	40.13	40.63
11.2	11.0	9.8	9.5	6.6	8.0	8.0	4.8	3.4	3.2	3.2
72.5	63	62.5	46	23	16	8.0	38	62.5	72.5	72.5
37.13	37.63	35.83	34.13	37.43	35.13	36.13	36.53	37.13	39.63	40.43
9.6	9.5	8.8	7.6	7.6	8.2	7.3	6.7	6.0	4.2	3.4
72.5	62.5	53	23	23	8.2	8	10	37	60	72.5
37.03	37.63	35.83	34.13	37.43	35.13	36.13	36.53	37.13	39.63	40.43
10	6.2	8.0	9.7	9.4	8.7	7.7	7.3	7.2	4.7	3.4
72.5	61	59	47	30	8.7	12	30	49	61	72.5
41.63	42.23	34.63	34.53	34.03	34.13	34.13	36.13	41.13	43.63	43.63
2.3	1.6	7.2	9.3	10.0	9.4	9.5	7.4	2.7	9.2	9.0
72.5	64	66	50	30	30	30	57	60	66	72.5
42.13	42.33	37.83	38.13	33.13	35.83	35.83	37.83	40.53	43.63	43.63
1.7	1.5	6.0	10.1	10.1	8.7	10.1	6.0	3.5	0.6	0.5
76	67	59	45	27	18.0	33	59	64	67	72.5

43.83

53















Cross section Diamond St.

Gresham to Haines

W.O. # 31021

Sommermeier

9-2-48

McCoy

W. Meade

Notes reduced - 9-8-48 *W.K. Lear*

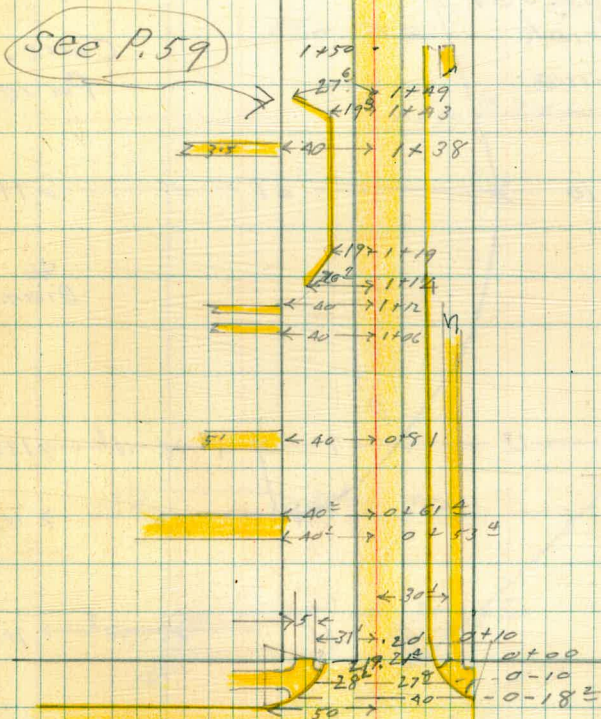
INDEXED

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SEP 7 1948

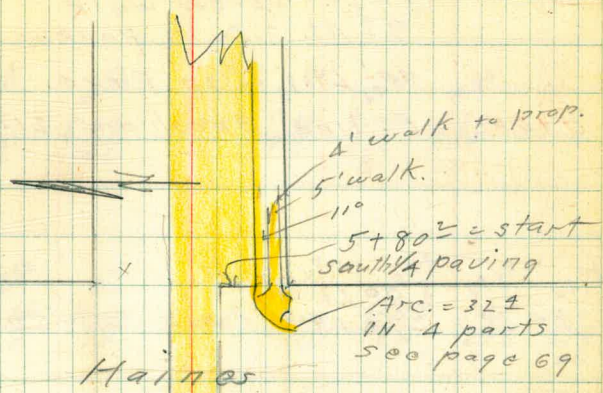
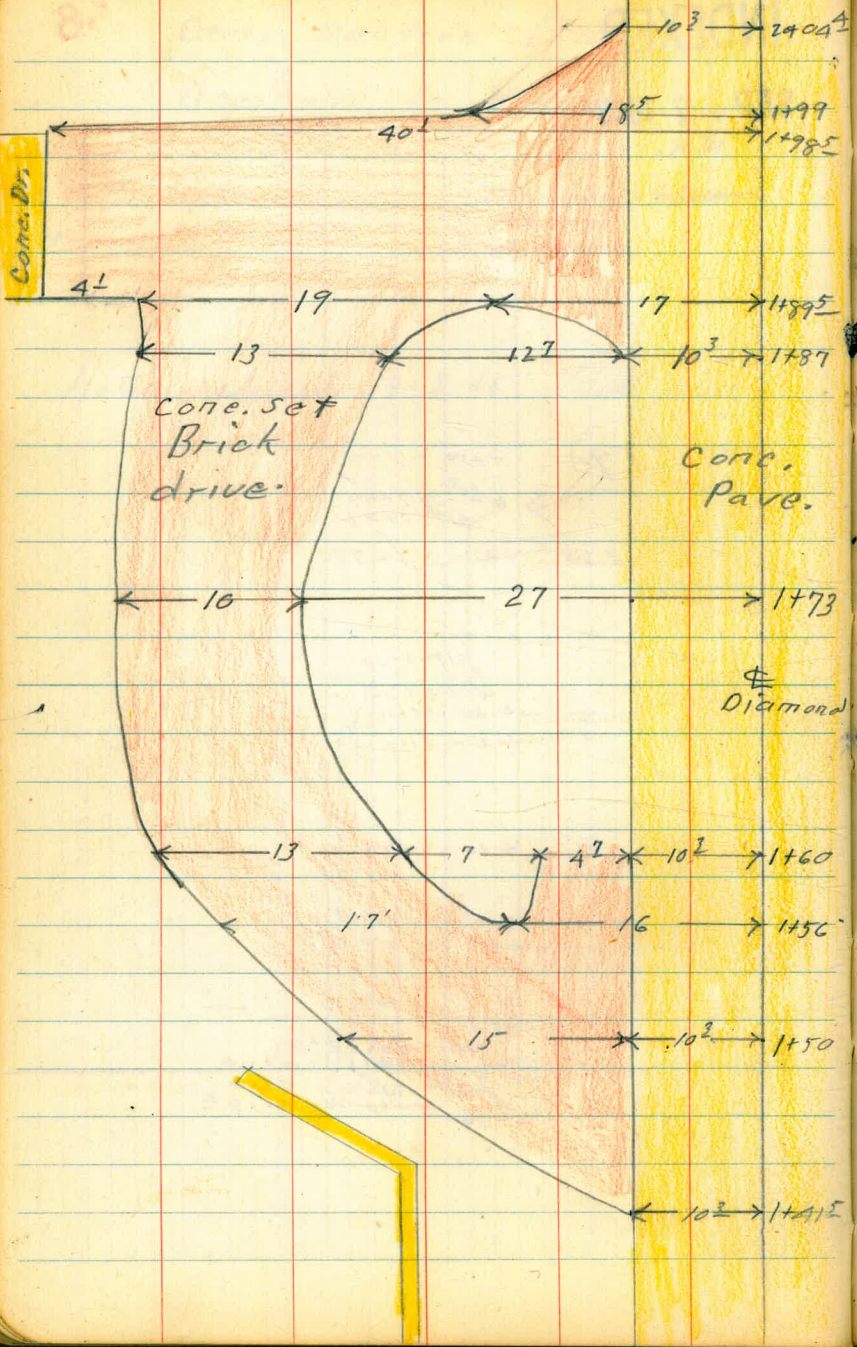
W.K.

Cont. on P. 60





Conc. Dr.



$4179^{86} = W.L. Haines$

$22^2 \rightarrow 39^2 \rightarrow 3131$

$39^2 \rightarrow 3108^2$   
 $15^2 \rightarrow 3102$



Diamond  
 305 Rt. = N.E. cor. walk  
 312 Lt. = S.E. cor. walk  
 92 Rt. = Δ in pave.  
 10' Lt. = Δ in pave.

0+00 = E. line Gresham 212 Lt. = End cb.

71.3	70.67	70.04	69.87	69.92	69.86	69.36	69.90
4.0	4.64	5.22	5.39	5.34	5.40	5.90	5.36
40	219	219	101		99	212	212
Grd	cc	G				G	cc

0-10 } 280 Lt }  
 278 Rt } = Face of curbs

70.52	70.01	69.96	69.77	69.78	69.67	69.48	69.21	69.78
4.74	5.25	5.30	5.49	5.48	5.59	5.78	6.05	5.48
29	280	20	70		10	20	278	278
cc	G						G	cc

0-18 = 40' Rt. = start curb return.

68.99	69.61
6.27	5.65
18	18
G	cc end.

0-20 Cont.

3.08	3.69
100	100
cc	G

0-20 = East Cb. line Gresham

70.6	70.39	70.21	69.95	69.71	69.75	69.65	69.49	69.05
4.20	4.87	5.05	5.31	5.55	5.51	5.61	5.77	6.21
50	50	40	20	10		10	20	40
cc, R.C.	G							

E.P. = Edge of pavement

0-40 = ± Gresham

71.07	70.94	70.66	70.18	69.95	69.92	69.86	69.68	69.30	67.8
3.19	4.32	4.60	5.08	5.31	5.34	5.44	5.58	5.96	7.5
100	50	40	20	10		10	20	40	100
								E.P.	

N.W. B.P.  
 Diamond 4.96 75.26 - 70.30  
 † Gresham

75.26  
 ↑



1+00

+99 36<sup>E</sup> Lt. = End picket fence0+97 30<sup>E</sup> Lt. = 2" diam. trunk - Tree0+81 40<sup>E</sup> Lt. = \$ 5' wide conc. walk

0+62 37' Lt. = start picket fence

0+61<sup>A</sup> 40<sup>Z</sup> Lt. = End same0+53<sup>A</sup> 40<sup>L</sup> Lt. = start conc. drive

0+50

0+10 20' Rt. = C.G. E.C.

75.26

72.2	72.0	71.5	71.2	71.44	71.45	71.30	70.9	71.17
3.1	3.3	3.8	4.1	3.82	3.81	3.96	4.4	4.09
50	40	18	11	10.3		9.8	20.1	20.1
				E.P.		E.P.		cc

72.31	72.16
2.95	3.08
50	40
	E walk

72.54	72.04
2.72	3.22
50	40.2

72.41	72.00
2.85	3.26
50	40.1

72.1	71.7	71.0	70.74	70.75	70.63	70.3	70.53
3.2	3.6	4.3	4.52	4.51	4.63	5.0	4.73
40	36	17	10.1		9.9	30	30
			E.P.		E.P.	20	cc

71.6	71.3	70.4	70.03	70.08	69.98	69.8	70.10
3.7	4.0	4.9	5.23	5.18	5.28	5.5	5.16
40	35	15	10.1		9.9	30	30
			E.P.		E.P.	20	cc E.C.

75.26



(Page 59)

1+41<sup>E</sup> 10<sup>3</sup> Lt. = start brick drive.1+38 40 Lt. =  $\Phi$  3<sup>E</sup> wide Conc. walk1+19 19 Lt. =  $\Delta$  in wall

sketch - P. 58

1+14 26<sup>2</sup> Lt. = start 5' wide Conc. Cl.

1+12 40 Lt. = S.E. Cor. same

V' Ribbons

1+06 40 Lt. = S.W. Cor. double ribbon drive

75.26

$$\begin{array}{r} 71.91 \\ 3.35 \\ \hline 103 \\ \text{E.P. + Brick} \end{array}$$

$$\begin{array}{r} 72.90 \\ 2.36 \\ \hline 50 \\ \text{walk} \end{array} \quad \begin{array}{r} 72.54 \\ 2.72 \\ \hline 40 \\ \text{walk} \end{array}$$

$$\begin{array}{r} 72.04 \\ 3.22 \\ \hline 19 \\ \text{top wall} \end{array} \quad \begin{array}{r} 71.6 \\ 3.7 \\ \hline 19 \\ \text{Base wall} \end{array} \quad \begin{array}{r} 71.7 \\ 3.6 \\ \hline 19 \\ \text{Grid} \end{array}$$

$$\begin{array}{r} 71.6 \\ 3.7 \\ \hline 262 \\ \text{Base wall} \end{array} \quad \begin{array}{r} 72.0 \\ 3.3 \\ \hline \\ \text{Grid} \end{array} \quad \begin{array}{r} 72.06 \\ 3.20 \\ \hline 262 \\ \text{top cl.} \end{array}$$

$$\begin{array}{r} 72.46 \\ 2.80 \\ \hline 50 \end{array} \quad \begin{array}{r} 72.17 \\ 3.09 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 72.46 \\ 2.80 \\ \hline 50 \end{array} \quad \begin{array}{r} 72.18 \\ 3.08 \\ \hline 40 \end{array}$$



1756 Cont. Diamond

1756 E.B = Edge brick

1750 Cont.

1750 Cont.

1750

see sketch - p. 59

1749 27<sup>s</sup> Lt. = End. of wall

1743 19<sup>s</sup> Lt. = Δ in wall

75.26

63

73.4	72.8	73.06
$\frac{1.9}{40}$	$\frac{2.5}{34}$	$\frac{2.20}{38}$
		E.B

71.7
$\frac{3.6}{40}$

72.82	71.86	72.04	72.09	72.01	71.8	71.5	72.00
$\frac{2.44}{23}$	$\frac{3.40}{16}$	$\frac{3.22}{103}$	3.17	$\frac{3.25}{92}$	$\frac{3.5}{10}$	$\frac{3.8}{14}$	$\frac{3.3}{20}$
	Brick	+ E.B. + Brick		E.B.			

71.7	71.1
$\frac{3.6}{40}$	$\frac{4.2}{60}$

72.9	72.7	72.4	71.85	72.00	72.04
$\frac{2.4}{50}$	$\frac{2.6}{40}$	$\frac{2.9}{26}$	$\frac{3.41}{192}$	$\frac{3.26}{31}$	$\frac{3.24}{36}$
		Ord	E incl ob	walk	walk

72.71	71.96	71.91	72.00	72.00	71.91	71.7	71.4	71.6
$\frac{2.55}{25}$	$\frac{3.30}{17}$	$\frac{3.85}{103}$	$\frac{3.26}{103}$	3.26	$\frac{3.35}{92}$	$\frac{3.6}{10}$	$\frac{3.9}{14}$	$\frac{3.7}{192}$
E Brick		Brick	E.P		E.P			

72.43	72.1	72.4
$\frac{2.83}{49}$	$\frac{3.2}{49}$	$\frac{2.9}{49}$
Top wall	Base wall	Ord

72.11	71.8	71.9
$\frac{3.15}{192}$	$\frac{3.5}{192}$	$\frac{3.4}{19}$
top wall	Base wall	Ord



1787 Cont.

1787 see page 59

1780 25' Lt. = Tree 2" diam trunk

1773 shots on brick drive

1765 25' Lt. = tree - 4" diam trunk

1760 Cont.

E.B. = edge Bricks ~~drive~~1760 (see page 59) ~~shots on brick~~

75.26

73.7	73.35	73.10	72.8	72.2
1.6	1.91	2.16	2.5	3.1
40	36	23	17	40
	E.B.	E.B.		

71.8	71.1	72.42	72.42	72.47	72.36	72.2	72.1
2.5	3.2	2.84	2.84	2.79	2.90	3.1	3.2
23	70	102	103		92	10	15
Ord	Ord	E.B.	EP		E.R.	Ord	

73.97	73.13
1.89	2.13
37	27
E.B.	E.B.

73.11
2.15
35
E.B.

71.89	71.6	71.65	71.22	71.09
2.37	2.7	3.38	3.24	3.17
22	22	15	102	103
E.B.	Ord.	E.B.	Brick	Pava.



2+50

T.P. 7.65 80.33 2.58 72.68

2+04 ± Cont

2+04 ± 10<sup>2</sup> Lt. = End of brick drive

(P. 59)

1+99 P.C. in line of brick drive

1+98 ± 40<sup>2</sup> Lt. = S.E. Cor. Conc. Dr.  
 a End Brick Dr.

1+89 ± 40<sup>2</sup> Lt. = S.W. Cor. Conc. Dr.  
 a End Brick Dr.

1+89 ± see P. 59

75.26

73.6	73.6	73.0	73.0	73.19	73.23	73.10	73.0	73.7	74.2
6.7	6.7	7.3	7.3	7.14	7.10	7.23	7.3	6.6	6.1
40	18	16	10.5	10.3		9.2	15	19	40
				E.P.		E.P.			

80.33

73.7	73.5	72.7	72.7	72.7	72.0
1.6	1.8	2.6	2.6	2.6	3.3
50	40	18	40	50	75

72.4	72.7	72.66	72.68	72.69	72.54	72.5	72.4	73.1
2.9	2.6	2.60	2.58	2.57	2.72	2.8	2.9	2.2
16	10.5	10.3	10.3		9.2	10	15	17
Ord	Ord	50 <sup>2</sup> Bricks	E.P.		E.P.			

72.8	72.96
2.5	2.30
18.5	18.5
Ord.	E.P.

73.74	73.49
1.52	1.77
50	40 <sup>2</sup>
Conc.	Conc. + Brick

73.83	73.60	73.35	72.66
1.43	1.60	1.91	2.60
50	40 <sup>2</sup>	36	17
Conc	E.P.	Brick	
Dr.	+ Done		



3+50

3+31 39<sup>z</sup> Lt. = 2<sup>z</sup> wide conc. walk.

3+08<sup>E</sup> 39<sup>E</sup> - S.E. Cor double ribbon drive

ribbon drive (P-59)

3+02 39<sup>E</sup> Lt. = S.W. Cor. double

3+00 Cont.

3+00

80.33

75.4  
4.9  
30

75.6  
4.7  
40

75.8 4.5 40	75.3 5.0 18	74.1 6.2 15	74.46 5.87 102 E.P.	74.60 5.83	74.40 5.93 92 E.P.	74.7 6.1 10	74.0 6.3 15	74.9 5.4 18
-------------------	-------------------	-------------------	------------------------------	---------------	-----------------------------	-------------------	-------------------	-------------------

76.16 4.7 50 on walk	75.52 4.81 39 <sup>z</sup> 2 walk
-------------------------------	--

75.41 4.92 50 on Drive	75.04 5.29 39 <sup>E</sup> drive
---------------------------------	---

75.44 4.89 50 on Drive	75.07 5.26 39 <sup>E</sup> Drive.
---------------------------------	--

74.9  
5.4  
50

75.6 4.7 60	74.7 5.6 40	74.1 6.2 19	73.5 6.8 17	73.82 6.51 104 E.P.	73.88 6.45	73.73 6.60 965 E.P.	73.5 6.8 10	73.2 7.1 16	74.4 5.9 21	74.7 5.6 40
-------------------	-------------------	-------------------	-------------------	------------------------------	---------------	------------------------------	-------------------	-------------------	-------------------	-------------------

80.33



5+24<sup>85</sup>

5+10 Grade break in Pavc.

4+99<sup>86</sup>

4+99<sup>86</sup> = W. Line Haines

4+50

4.00

80.33

76.28	76.27	76.09
4.95	4.06	4.24
10.95		9.6
E.P.		E.P.

76.33	76.35	76.26
4.00	3.98	4.07
10.45		9.5
E.P.		E.P.

77.9	77.6	76.8	76.4
2.4	2.7	3.5	3.9
60	40	40	60

cont

cont

77.1	75.8	76.1	76.28	76.33	76.27	76.1	75.7	76.8
3.2	4.5	4.2	4.05	4.00	4.06	4.2	3.6	3.5
18	16	10.5	10.45		9.5	10	16	20
			E.P.		E.P.			

76.15

77.0	76.8	75.3	75.5	75.73	75.78	75.67	75.40	75.3	76.7	76.5
3.3	3.5	5.0	4.8	4.60	4.55	4.66	4.9	5.0	3.6	3.8
40	18	15	10.5	10.8		9.5	10	16	23	40
				E.P.		E.P.				

76.7	76.5	76.4	74.7	75.10	75.15	75.02	74.8	74.9	75.9	76.3	76.4
3.5	3.8	3.9	5.15	5.23	5.18	5.31	5.5	5.4	4.4	4.0	4.1
60	40	18	15	10.35		9.5	10	16	19	40	60
						E.P.					

80.33



Diamond

orig B.M.			5.74	70.31	0.01	70.30 orig B.M. page 60
T.P.	3.37	76.05	7.97	72.68		
T.P.	3.73	80.65	8.40	76.92		
T.P.	1.82	85.32	—	83.50		
Lt. East line diamond						
φ Ingraham			4.36	83.50		83.59
T.P.	5.69	87.86	1.51	82.17		
T.P.	6.67	83.68	3.32	77.01		

5+80

5+60

See Page 69

5+39<sup>80</sup> = φ Haines

80.33

Lt.

φ

Rt.

68

76.15  
4.18  
104  
E.P.

76.21  
4.12

76.12  
4.21  
965  
E.P.

76.00  
4.33  
1045  
E.P.

75.99  
4.34

75.75  
4.58  
965  
E.P.

76.4  
119  
100

77.6  
27  
40

77.2  
3.1  
25

76.20  
4.13  
104  
E.P.

76.15  
4.18

75.97  
4.36  
96  
E.P.

76.0  
4.13  
13

76.3  
4.0  
21

76.5  
3.8  
40

76.0  
4.3  
60



Additional notes Diamond

A + Haines -

10-6-48

5472<sup>2</sup> 21<sup>5</sup> RT. =  $\frac{3}{4}$  point on curve. on Ret.

5465<sup>6</sup> 26' RT. = Mid curve. or Ret.

5461<sup>2</sup> 32<sup>3</sup> RT. =  $\frac{1}{2}$  Arc. on. ob.

5460 - see Page 68

5459<sup>8</sup> 40<sup>5</sup> RT. = start Ob. Ret.

5439<sup>8</sup> & Haines (see page 68)

check 10<sup>4</sup> Lt. 4499<sup>8</sup> 1.96 76.28 76<sup>29</sup>  
P. 68

10<sup>4</sup> Lt. 5480 5.09 81.24 ~~5.~~ 76.15  
page 68

±

69

76.35  
4.89  
215  
top. ob.

76.27  
4.97  
26  
top. ob.

76.18  
5.06  
323  
top. ob.

76.2  
5.0  
40  
Obd.

76.15  
5.09  
405  
top. ob.

81.24



7+00

78.1	78.0	77.7	77.16	77.17	77.04	76.55	77.19
3.1	3.2	4.0	4.08	4.07	4.20	4.69	4.05
40	22	15	10.2		9.5	20	20
			E.P.			Q	CL

6+50

78.1	77.6	76.8	76.83	76.83	76.74	76.19	76.91
3.1	3.6	4.4	4.41	4.41	4.50	5.05	4.33
40	18	15	10.2		9.5	20	20
			E.P.			Q	CL

6+00

E.P. = edge paving

77.8	77.5	76.5	76.37	76.43	76.34	75.87	76.53
3.4	3.7	4.7	4.92	4.81	4.80	5.37	4.71
40	18	15	10.2		9.5	20	20
			E.P.			Q	CL

(page 59)

South Va and south curb.

5+80<sup>2</sup> = start paving between

5+80 = Curb. Ret. E.C.

5+80 See page 68

77.8	77.7	76.15	76.21	76.12	75.75	76.37
3.4	3.5	5.09	5.03	5.12	5.49	4.87
40	18	10.2		9.5	20	20
		E.P.		Q in Pav	Q	top CL



Proposed Storm Drain to Extend

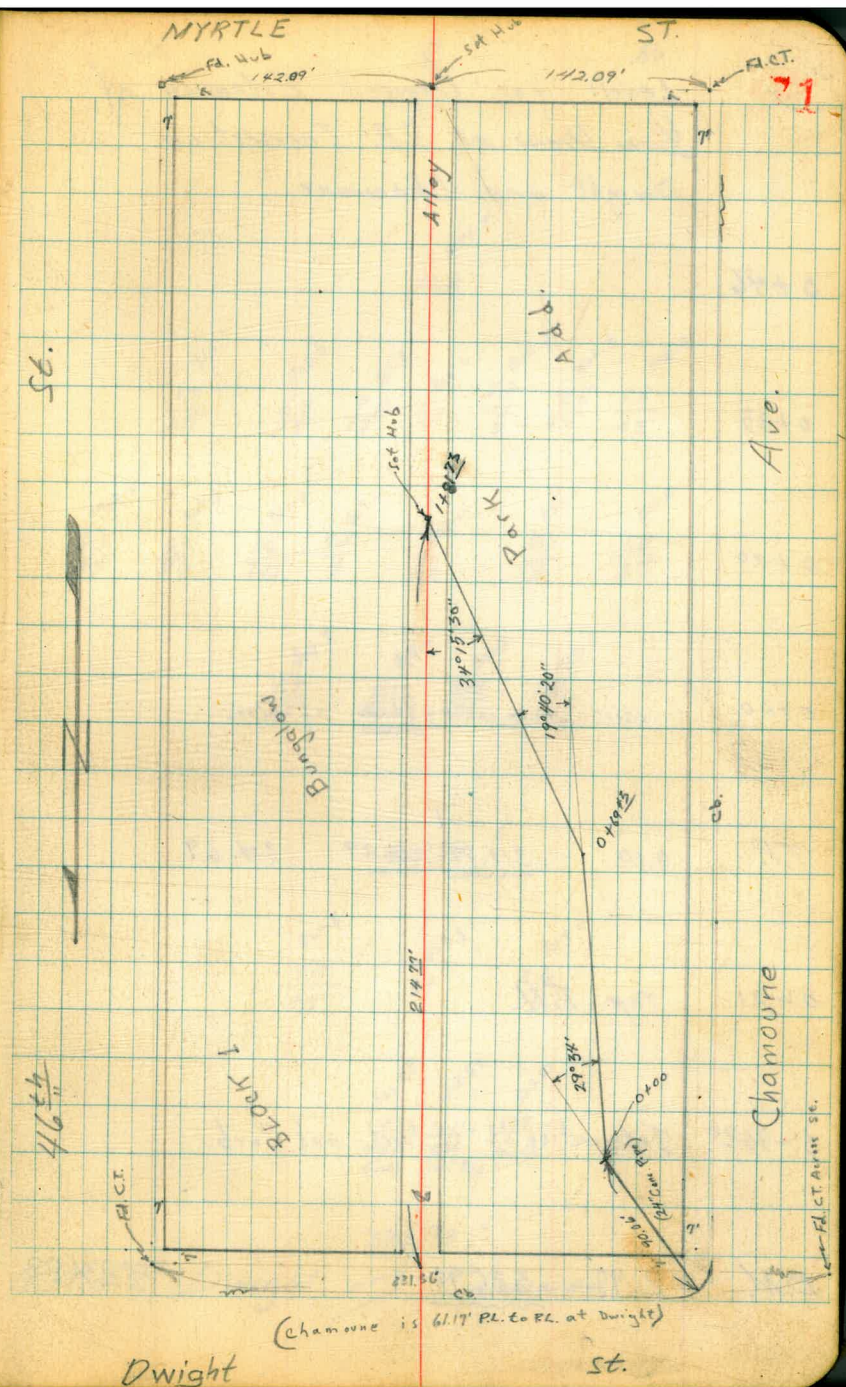
Culvert SE. Cor. Dwight and Chamone Block 1  
Bungalow Park

Roberts  
W. Moore  
Clark  
11-15-48

NO. # 80129

Map. Dwg. Nos. 3637, 2180B & 3067L 7120L

INDEXED  
WIK  
NOV 23 1948



(Chamone is 61.17' PL. to BL. at Dwight)

Dwight

St.



Levels for Proposed Extension of  
Storm Drain at S.E. Intersection  
Dwight and Chamoune

0+46

0+33

0+20

0+00

xsect at R.R. to line of pipe.

T.P. 0.10 314.79 12.29 314.69

0-21 Top Fill

0-90<sup>06</sup> Intersection of Culvert and Curb.

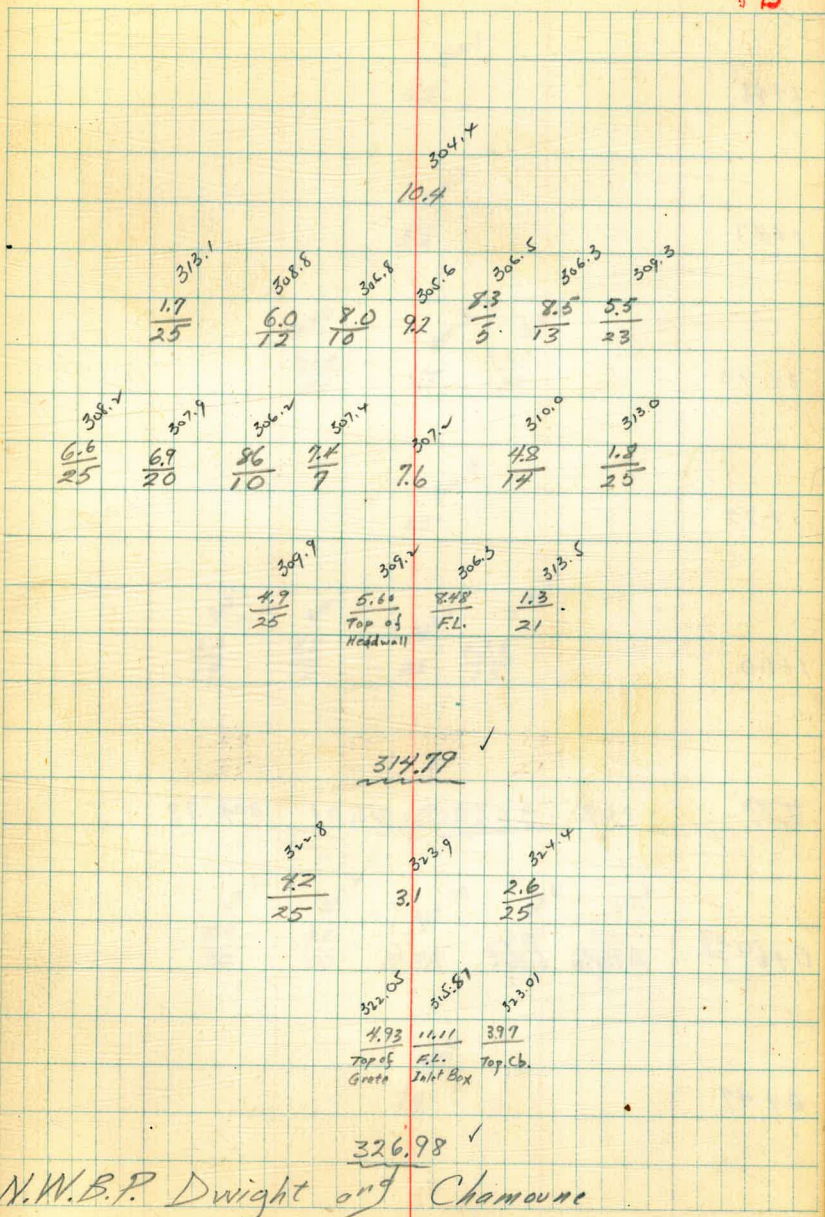
B.M. 2.98 326.98 324<sup>00</sup>

Lt.

Q

Rt.

12



N.W.B.P. Dwight and Chamoune



1+48

1+47

1+40

1+22

1+00

T.P. 1.49 306.27 10.01 304.78

0+69<sup>43</sup> Angle Left

0+47

314.79

Lt.

Rt.

Rt

13

302.1  
4.2

300.7  
5.6

301.5  
+1.2  
20

300.5  
5.8

310.3  
+4.0  
20

302.8  
2.5

303.1  
3.2  
19

302.0  
4.3  
12

303.1  
3.2

308.9  
+2.6  
15

306.27 ✓

310.1  
4.7  
30

307.0  
7.2  
20

304.79  
10.00

303.9  
10.9  
17

309.6  
5.2  
25

306.0  
8.8

314.79 ✓



Check			4.28	323.99 = 324.00
T.P.	10.52	328.27	0.13	317.75
T.P.	13.10	317.89 ✓	1.49	304.78

1481<sup>73</sup> Int. with  $\&$  Alley (xsect on line of Alley)

1462

306.27

Lt.

$\&$

Rt.

74

N.W. B.P. Dwight & Chemoune

Notes Roadcut 11.23.98

305.4	302.7	298.7	299.0	300.6	
$\frac{0.9}{20}$	$\frac{3.6}{70}$	$\frac{7.6}{76}$	$\frac{7.3}{73}$	$\frac{5.7}{26}$	
308.3	303.4	301.7	299.8	302.1	308.1
$\frac{+2.0}{25}$	3.1	$\frac{4.6}{6}$	$\frac{6.5}{12}$	$\frac{4.0}{18}$	$\frac{+1.8}{27}$

306.27 ✓



Add. Sections over changed Part  
of Reed - Bet. Morrell + Noyes - See P. 18  
9-23-49 - F.O.

**INDEXED**

N.K.

SEP 26 1949

1+40- 40' Rt =  $\pm$  8' Conc. Dr.

0+21- 40' Rt =  $\pm$  3' Conc walk

Req. 0+00 = E.L. Noyes - E. to Olney - Sections <sup>O.K.</sup>

4+46- 38.7 Rt =  $\pm$  2' Conc walk

4+11- 35' Rt =  $\pm$  3' Conc. walk

3+84- 40.1 Rt =  $\pm$  3' Conc. walk

3+52.5- 37.4 Rt =  $\pm$  of 2.7 Conc. walk

SEE ALSO PAGE Bote.

Lt.

$\pm$

Rt.

75

20.03

40  
Dr.

19.83

40  
walk

25.1

38.7 = walk

10.9

35  
walk

11.08

40.1  
walk

11.52

37.4  
edge

19.86

54.9  
Gar  
floor

11.11

50 = walk

11.26

40

12.03

61.4  
walk at Porch.

12.35

40.4  
Top  
ramp

20.07

54.9 = Parch

11.70

50

12.30

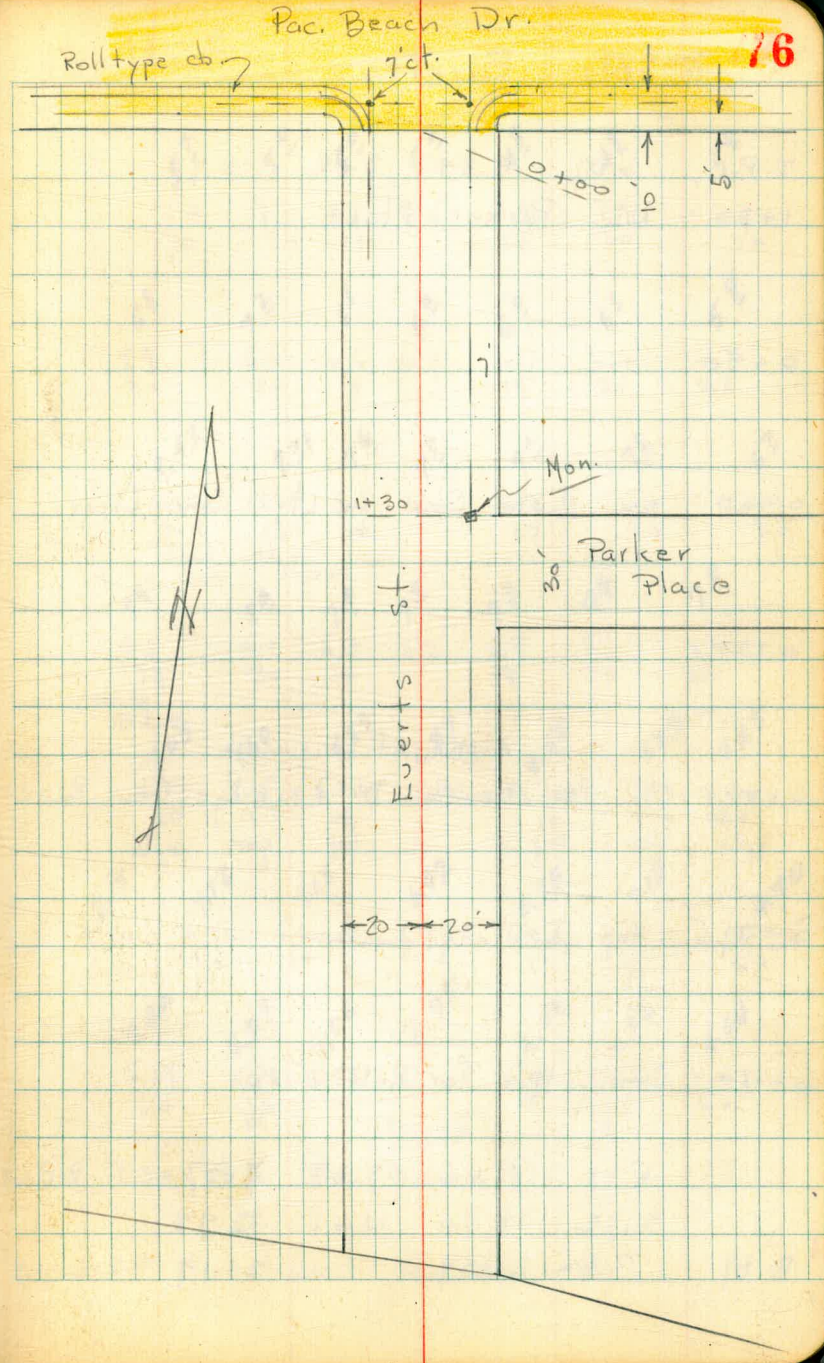
50

Note - These are elev. →



X-Sect. Everts - from Pac. Beach  
 Dr. to S. end.  
 # 4446  
 w.o. 25020  
 6-20-50  
 7.0

INDEXED  
 M.R.  
 JUN 22 1950





81. X-Sect. Everts.

T.P.	6.07	9.84	8.88	3.77
1+30 =	N.L. Parker Place			
0+90				
0+50 =	on Doub. Gar. on Lt. Conc. floor			
0+20				
	+ end of cb. + walk			
0+00 =	S.L. Pac Beach Dr. + = edge Conc. Pave			
0-09.5 =	Top cb. + edge walk			
0-11 =	Conc gutter for Roll curb.			
	5.28	12.65	8.33	7.37 = B.P.
	2.72	15.70	10.61	12.98
B.M.	2.40	23.59		21.19

Lt. = E.      ±      Rt. = W. 17

5.7	5.0	5.0	5.2	4.8	4.8	5.0
7.0	7.7	7.7	7.5	7.9	7.9	7.7
7.0	20	14		14	20	30
6.8	7.2	6.1	6.0	6.0	6.1	5.9
5.9	5.5	6.6	6.7	6.7	6.6	6.8
30	20	14		14	20	30
8.43	9.31	7.6	7.3	7.4	7.3	6.7
4.22	4.34	5.1	5.4	5.3	5.4	6.0
20.8	19.8	14		13	20	30
floor edge Gar.	top edge	top				
8.6	8.6	7.4	7.5	7.3	7.4	7.0
4.1	4.1	5.3	5.2	5.4	5.1	5.7
24.9	20	14		13	20	30
along						
House						
7.65	7.50	6.83	6.97	6.51	7.23	7.25
5.00	5.15	5.82	5.68	6.14	5.42	5.40
20	15.7	14		14	15.4	19.8
edge	Top	Top		Top	Top	edge
9.15	7.72	7.05	6.92	6.75	7.18	6.70
4.50	4.93	5.60	5.73	5.90	5.47	5.95
60	25	14		14	20	50
	PC				PC	
7.46	7.07	7.06	6.95	6.76	6.52	6.04
5.9	5.58	5.59	5.70	5.89	6.13	6.61
60	25	14		14	25	50
	PC				PC	
			12.65			

N.W. Everts + Pac Beach Dr

N.W. B.P. Gresham + Pac Beach Dr.



2+00 = on Beach = end.

2+70 = Guard Rail

2+57 - 14.6 Lt. = 5' Conc. walk

2+35

2+30 - 22.8' Lt. = end walk at Conc. steps  
of 3' Conc. walk

2+09 - 20.6' Lt. = end apron + 22.8' Lt. = Beg. wly

2+00

1+83 - 20.4' Lt. = Beg. Conc. apron to Doub. Gar.

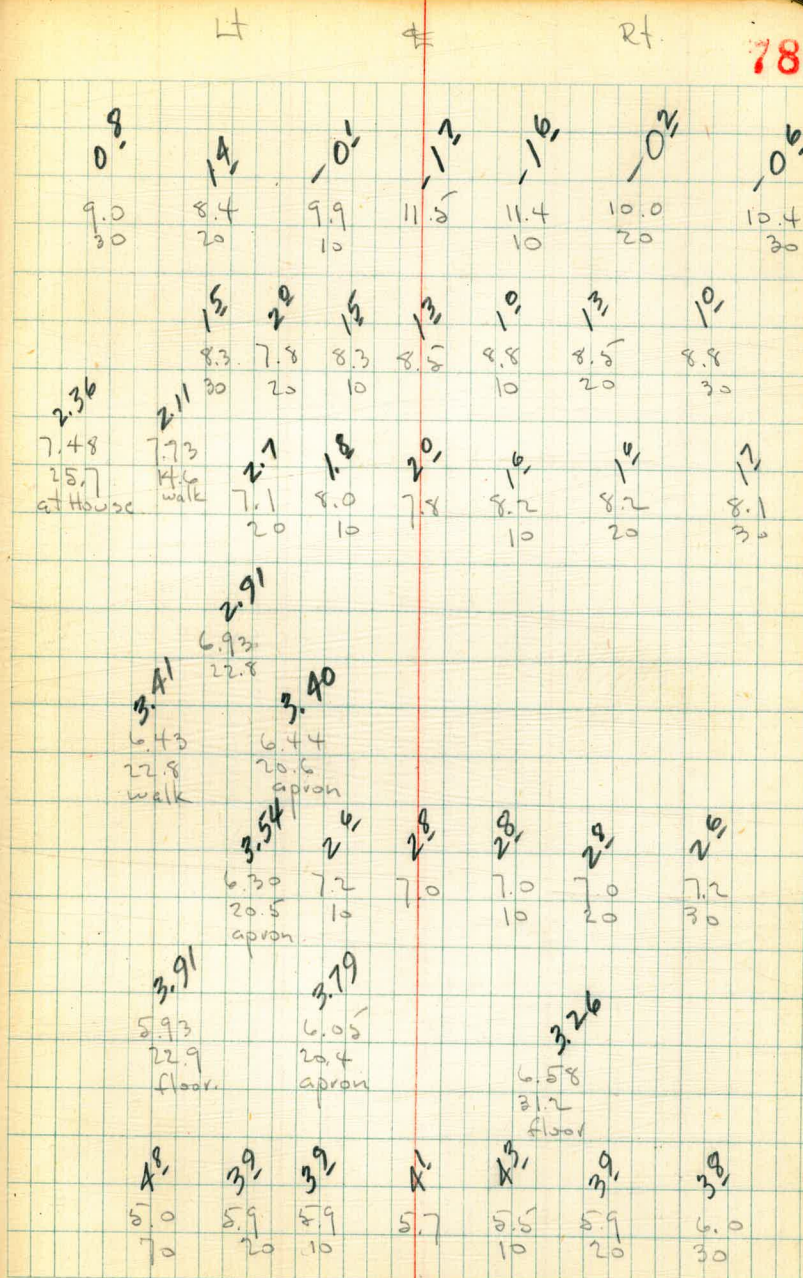
1+76 - 31.2 Rt. = 1/2 Sing. Gar. - Conc. floor

1+60 = S.L. Parker

1+45 = 1/2 Sewer M.H.

5.15 <sup>4.69</sup>

on Rim









28.71  
3.33  
25.38

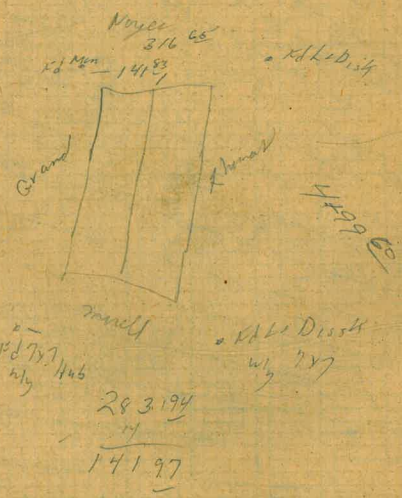
2+37- 40 Lt. = N. edge

25.38  
18.30  
7.08  
46.28  
53.26  
50.55  
2.71

H1

314  
126965  
134.23  
141.83

81.24  
7008  
A.96



44.79	40.37	40.38	36.00
10.82	2.54	4.46	98.00
33.97	42.91	44.81	✓
7.51	12.92	5.56	
41.48	29.99	39.25	3
4.98	3.91	3.36	
36.50	33.90	42.61	
1.81	12.38	12.93	
38.31	21.52	29.68	
13.27	0.22	0.52	
25.04	21.74	30.26	
6.94	9.85	13.16	
31.98	11.89	17.04	
2.20	8.63	4.36	
29.78	20.52	21.40	
6.55	1.08	11.22	
36.33	19.44	10.18	
12.74	6.90	0.77	
23.55	26.34	10.95	
5.16	7.99	6.38	
28.71	18.35	4.57	
10.41	3.17	4.56	
Hyd-s 18.30	21.52	9.13	
		6.51	
		5.53	
		12.04	
		3.43	
		9.61	
		25.38	
		5.92	
		31.30	
		11.56	
		19.74	
		2.63	
		22.37	
		9.92	
		13.55	
		4.74	
		18.33	
		12.66	
		5.67	
		5.70	
		7.51	
		1.85	

30.50	41.51	
9.62	33.10	
46.12	0.91	
	34.01	
36.50	13.03	22.37
3.11	9.94	40.7
39.61	20.98	48.30
9.86	0.42	
29.75	21.40	
1.68	12.43	
31.43	08.97	
12.77	9.55	
18.66	4.59	
7.72	-0.68	
26.38	5.91	
2.14	5.23	
23.54	0.70	
	5.70	
	7.51	
	1.85	



7319  
360  
6755

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)+2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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