

1828

STEADY  
STATE

ENGINEERS'  
LEVEL BOOK

No. 410F

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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# 1828

## CITY ENGINEERS OFFICE

INDEXED

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5  
3-67  
-73

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

xsec alley Blk 15 Bird Rock add -2

YAMA ST. 11

Prop. train <sup>20243</sup> Met. CTR. 12

xsec Alley 253 U.H. 17

" " 206 Pac. Beach 26

Additional Notes ally 15 Bird Rock 35

xsec Curlew St <sup>North</sup> Laurel St to Canyon 63-67

Canyon & Catalina <sup>xsec</sup> Pave. 72-73



INDEXED

JAN 19 1948

1 sec alley 15' wide  
Blk 15 Bird Rock Add.  
MAP NO 1083

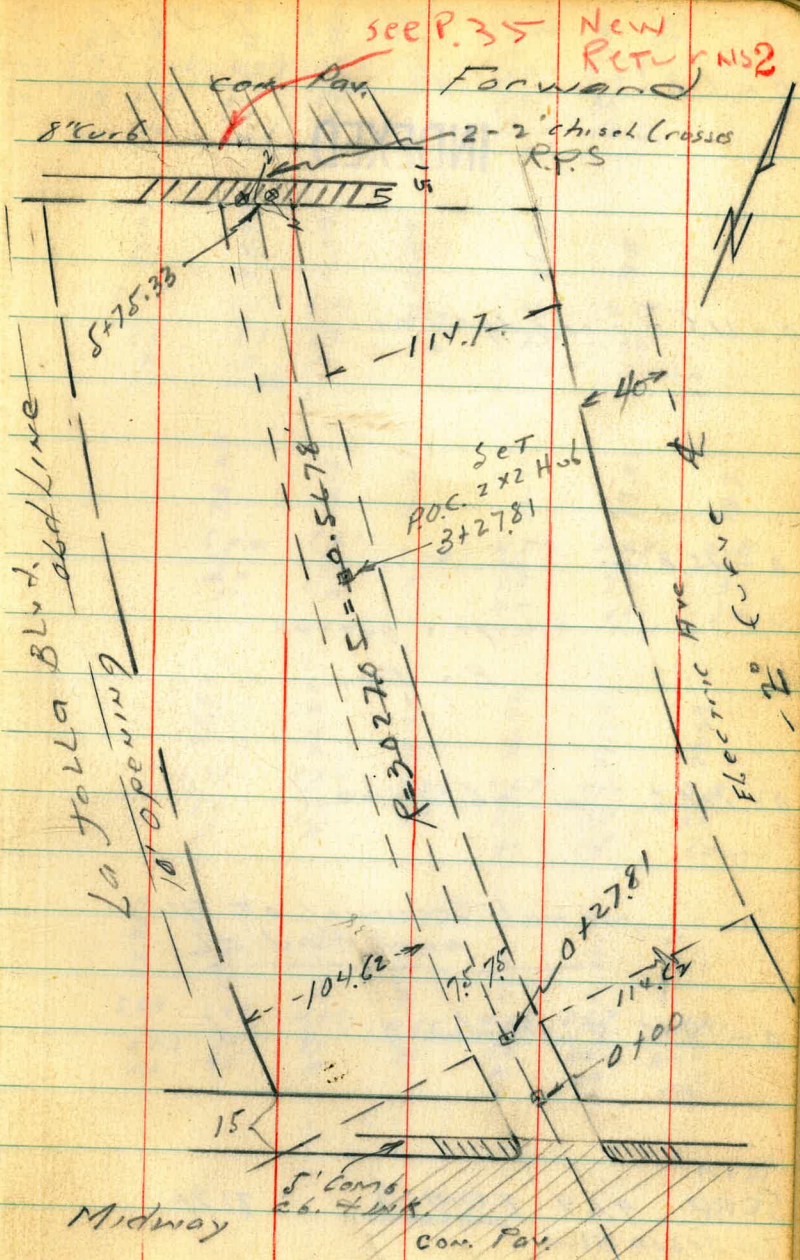
W 0 2500,

Moore  
Begg  
Green  
Roberts

1-15-48

0° 14.2 - 25'

0° 56.78 - 100



02104 Blk 15 Bird Rock

0-6.8±

# INDEXED

0-11.6± N. edge Pav

0-15.8±

gt. = gutter  
P. Pav.

0-17.6± N c6 line

Note! Sections at 90°  
and Radial

0-34.7± & Midway

B.M.  
SEBP 9.69 81.49 71.80  
La Jolla Blvd.  
Midway

75.27	75.52	76.23	76.70	76.37	77.18	77.90	
30	17.9	17.8	8.3	47.3	3.7	27.5	
P	97	66	end	P	dir	30	Lawn
75.4	75.99	76.09	76.57	77.5	78.8		
6.0	5.50	5.76	4.92	4.0	2.7		
30	8.7	7.5	P	7.5	30		
P	14.97	P	P	dir	Lawn		
75.49	76.18	76.41	76.90	77.41	78.7		
6.0	5.31	5.08	4.59	4.08	2.8		
30	7.5	7.3	7.3	7.4	30		
P	P	gt.	edge P.	66	Lawn		
75.52	76.25	76.35	76.82	77.39	78.69		
5.97	5.24	5.14	4.67	4.10	2.8		
30	7.5	97	7.4	7.5	30		
P	P	P	97	66	Lawn		
75.85	75.26	76.53	77.13	77.82	78.52		
5.64	4.23	4.96	4.36	3.67	2.97		
30.1	30	7.5	7.5	30	30.1		
66	97	P	P	97	66		

81.49

0+80.3 end garage

0+64.6 beg dbl garage 11.6 R

+60.5 7.6 R end of fence

T.P. 486 81.98 4.37 77.2  
84. Hub

0+52.81

0+28 8' Pt Beg. C' Bd fence

0+27.81 B.C. Pt

0+04.5 7.6 Lt Beg. Bd. fence C' High

0+00 = 1/2 Midway  
Sec. at 90°

81.49

Lt

R

Rt

4

5.7  
20

fence  
7.7

77.1  
4.9  
7.5

77.4  
4.6

77.96  
4.02  
5  
edge of pen

78.33  
3.65  
7.5

78.89  
3.09  
11.2  
floor

75.9  
6.1  
20

76.7  
5.3  
7.5  
fence

77.2  
4.8

77.7  
4.32  
5  
edge of pen

78.07  
3.91  
7.5

78.75  
3.23  
11.6  
floor

81.98

76.0  
5.5  
20  
Yard

76.8  
4.7  
7.5  
fence

77.3  
4.2

77.5  
4.0  
7.5

Fence  
7.0

78.0  
3.5  
1.5

76.2  
5.3  
20  
in yard

76.7  
4.8  
7.5  
Fence

77.1  
4.4

77.8  
3.8  
7.5

78.3  
3.2  
1.4  
against  
house

75.9  
5.7  
2.5

76.9  
4.6  
7.5

77.3  
4.2

77.8  
3.8  
5.6

78.1  
3.4  
1.4  
Sw. cor  
house

81.49

1+77<sup>81</sup>

1+57<sup>81</sup>

1+27<sup>81</sup>

1+24 7.9 L P. Pole PA 5511

1+16<sup>6</sup> 7.8 R beg of fence

1+16<sup>5</sup> 6.0 R end of fence

1+02<sup>81</sup>

at 84 { 7.8 R beg fence board  
7.5 L end of fence picket

81.98

L+

#

R+

5

78.0	78.5	79.0	79.3		78.8
4.0	3.5	3.0	2.7	fence	3.7
2.0	7.5		7.5	8.4	20

77.5	78.0	78.4	78.9		79.7
4.5	4.0	3.6	3.1	fence	2.3
2.0	7.5		7.5	8.0	20

77.2	77.8	78.1	78.5		79.3
4.8	4.2	3.9	3.5	fence	2.7
2.0	7.5		7.5	8.0	20

76.4	77.3	77.6	78.1		78.6
5.6	4.7	4.4	3.9	fence	3.4
2.0	7.5		6.6	7.5	20

81.98



+	#1	-	E1
4.72	<u>86.15</u>	0.55	81.43

2+77.81

2+71.7 7.5A beg Picket fence  
7.5A end of fence board

2+52.81

2+31.6 6.6L Pole A 55.77

2+27.81

202.81

91.98

L R 6

79.2	80.1	80.4	81.1	81.4
2.8	1.9	1.6	0.9	fence 0.6
20	7.5		7.5	20

79.3	79.9	80.4	80.8	81.4
2.7	2.1	1.6	1.2	0.6
20	7.5		7.5	fence 20
				7.7

79.1	79.6	80.0	80.5	81.1
2.9	2.4	2.0	1.5	fence 0.9
20	7.5		7.5	8.0 20

78.6	79.2	79.6	80.0	80.5?
3.4	2.8	2.4	2.0	fence 1.5
20	7.5		7.5	8.6 20

81.98

3+71 7.0 R end of Picket

3+58.81

3+35 8.0 L P Pole A55-63

3+27.81 POC. Set 2x2 RW Hub

3+10.5 11.7 R 2.9 wide steps Top of Step

3+10 7.0 R 9" Euc 24"

3+02.81

2+87 7.5 R 9" 24" Euc.

86.15

7

79.7	80.5	81.1	81.2		81.5
6.5	5.7	5.1	5.0	fence	4.7
20	7.5		7.5	7.8	20

79.5	80.0	80.6	80.9		81.9
6.7	6.2	5.6	5.3		4.3
20	7.5		7.5	fence	20

				81.97	
				4.18	
			lower	step	

79.6	80.1	80.3	80.8		81.6
6.6	6.1	5.9	5.4		4.6
20	7.5		7.5	fence	14.5
					Cor. house

86.15

4+77.81

4+73 7.2 R end bd fence

4+59 8.8 L P. Pole A5575

4+52.81

4+47 8.0 R beg. bd fence

4+27.81

4+22.81

3+77.81

86.15

L

A

F

8

80.4

5.8

20

81.2

5.0

7.5

81.9

4.3

82.4

3.8

7.5

80.1

6.1

20

80.6

5.6

7.5

81.1

5.1

81.8

4.4

7.5

fence

7.5

82.6

3.6

20

79.8

6.4

20

80.5

5.7

7.5

80.9

5.3

81.3

4.9

7.5

81.9

4.3

20

80.1

6.1

20

80.4

5.8

7.5

80.8

5.4

81.2

5.0

7.5

81.6

4.6

20

80.1

6.1

20

80.6

5.6

7.5

81.1

5.1

81.2

5.0

7.5

81.7

4.5

20

86.15

75  
5 + 91.3 ± 5 of Forward

5 + 7533 intsec. of alley & S Prop line Forward  
S.L. can. sidewalk  
NO RETURNS

5 + 5781

5 + 2781

4 + 98 end of garage

4 + 85 11.1 beg dbl garage

86.15

LT	5.81.2	4.81.5	4.81.7	5.81.02	4.81.51	5.82.33
	20	7.5	Top	0.1	7.5	20
		dir	6	97.		
	81.4	82.1	82.22	82.47	83.1	
	4.8	4.1	93	3.68	1	
	20	7.5		7.5	20	
		dir			dir	
	81.6	82.2	82.6	82.8	83.4	
	4.6	4.0	3.6	3.4	2.9	
	20	7.5		7.5	20	
	81.7	82.1	82.6	83.2	84.0	
	4.5	4.1	7.6	3.0	2.2	
	20	7.5		7.5	20	
	81.1	82.3	82.6	83.0	83.7	
	5.0	3.9	3.6	2.2	2.78	
	20	7.5		7.5	16.0	
					floor	
	80.8	82.0	82.5	82.9	83.37	
	5.4	4.2	3.7	3.3	2.78	
	20	7.5		7.5	11.1	
					floor cont	
			86.15			

Lr

Q

Fr 10

FOR NEW ALLOY  
RETURNS  
see P. 35

check to orig. BM. 5.84 71.73 71.80  
Midway 0.07

Sw BP 2.42 77.57 74.95

check to BM BP  
Sw La Jolla Blvd  
Forward 11.14 75.01 74.95  
0.06

L + 07.03! Q Forward

86.15

5.84  
20 80.34

5.10  
25 81.11

4.66  
P 81.49

1.25  
P 81.9

2.00  
P 82.41

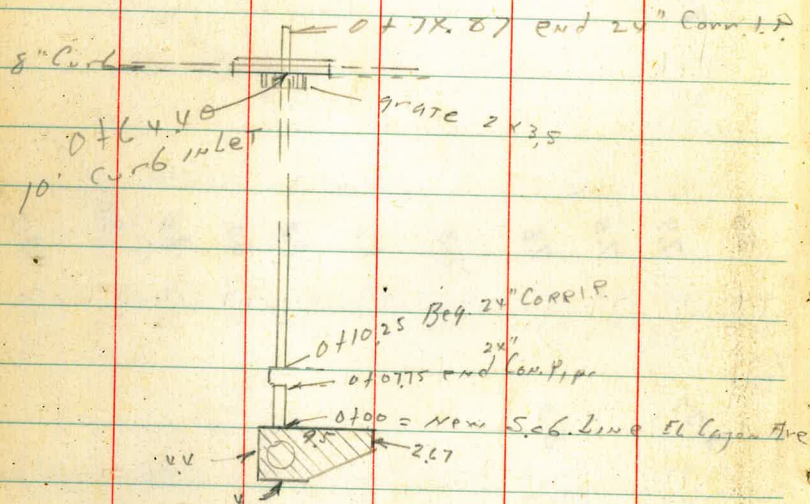
86.15



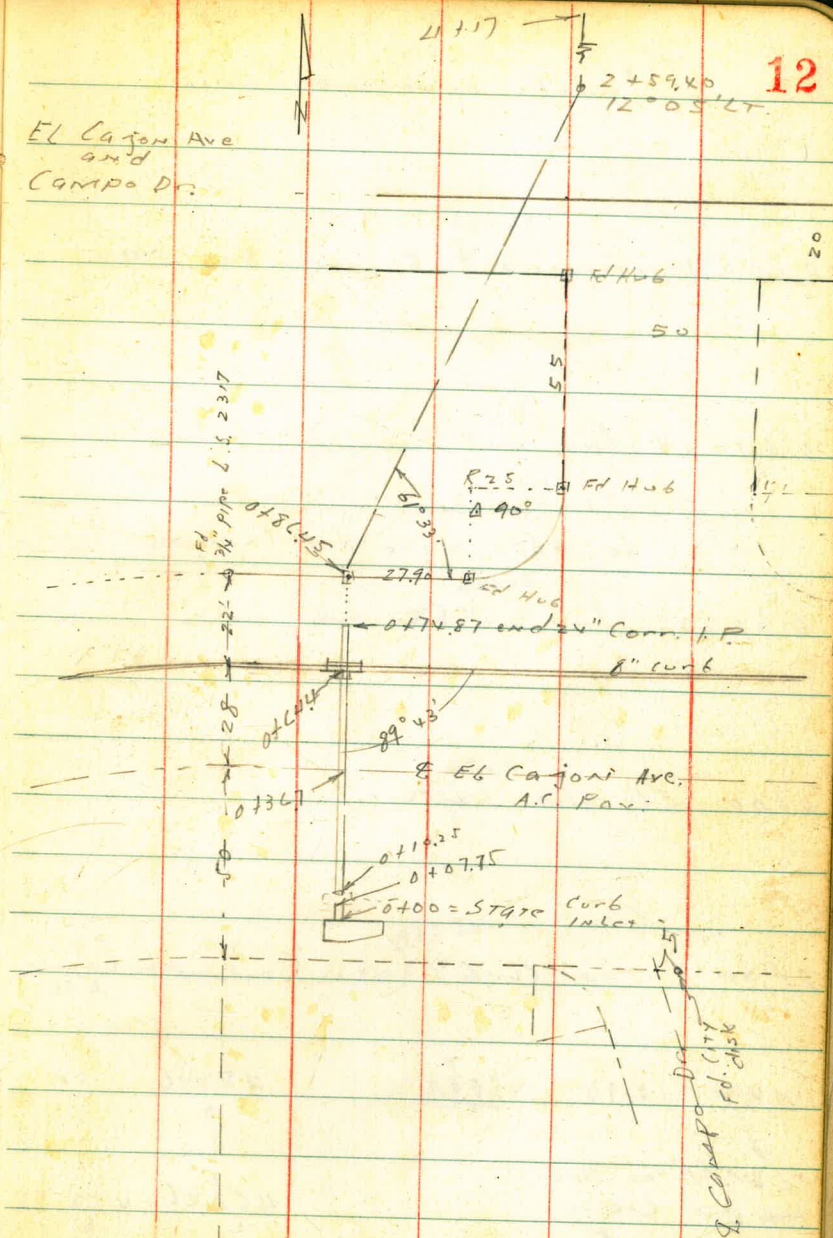
Proposed drain across  
 Lots 2 + 3 Metropolitan CTR.  
 W.O. 80143

MOORE Notes  
 BE99 = 1/4 note  
 SHORRMAN  
 BUNICK  
 2-28-49.

INDEXED  
 WK  
 MAR 1 1949



El Cajon Ave  
 and  
 Campo Dr.



Levels proposed drain

0+36.7 approx E El Cajon Ave. Pav.

452.88  
2.51

0+10.25 Inv. 24" Conn. 1P Curb

445.89  
9.50

This old Con. Box

will be abandoned and connection to old 24" Conn. 1P

0+07.75 Inv. 24" Con. pipe Curb,

446.18  
9.21

0+00 Fl. inlet. future Pav. gut.

451.19  
4.20

0+00 Top Curb (New So. curb El Cajon Ave.)

452.22  
3.17

SW B.P. 293 455.39

452.46

455.39

FD. BM. B.P. on SWly

of B.P. COR. 7

Rolando Dr.

and

El Cajon Ave.

452.46 452.53

Corrected

old

1301-47



0+86.5  $\Delta$  N.L. EL Cajon Ave

0+74.87 Inv. end 24" Conn. I.P. Culv.

0+68

0+64.4 Top curb inlet

0+64.4 Top iron grating

0+64.4 N 66 EL Cajon Ave ~~Box~~ Box

455.39

← \$ R 14

A52.3	A51.1	A46.9	A46.5	A45.6
$\frac{3.1}{20}$	$\frac{4.3}{10}$	8.5	$\frac{8.9}{10}$	$\frac{9.8}{20}$

A52.8	A52.0	A45.62	A46.3	A48.20
$\frac{2.6}{20}$	$\frac{3.4}{10}$	9.77	$\frac{7.1}{10}$	$\frac{7.2}{20}$

A52.6  
2.8

A52.77  
3.2

A51.77  
3.2

A46.1  
9.3

Box Full of  
Mud  
and Water

455.39

2 + 5940 Δ 12° 05' LT. ON SPLIT

2 + 20

1 + 90

1 + 60

T.P. 329  $\sqrt{445.92}$  12.76  $\sqrt{42.63}$

1 + 30

1 + 00

$\sqrt{55.39}$

15

437.6	435.1	436.3	442.3	443.6
$\frac{8.3}{30}$	10.8	$\frac{9.4}{10}$	$\frac{3.6}{30}$	$\frac{2.3}{20}$

440.2	438.2	437.6	437.5	443.6	443.9
$\frac{5.7}{30}$	$\frac{7.7}{15}$	8.3	$\frac{8.4}{10}$	$\frac{2.3}{20}$	$\frac{2.5}{25}$

442.3	440.0	439.2	439.9
$\frac{3.6}{30}$	$\frac{5.9}{15}$	6.7	$\frac{6.0}{59}$

440.9	440.9	440.7	440.5
$\frac{3.0}{25}$	$\frac{5.0}{8}$	5.2	$\frac{5.6}{20}$

$\sqrt{445.92}$

449.7	449.2	442.6	442.1	442.6
$\frac{5.7}{25}$	$\frac{6.2}{12}$	$\frac{12.8}{12}$	$\frac{13.0}{30}$	$\frac{12.8}{20}$

451.4	450.2	445.4	445.1	445.3	445.8
$\frac{4.0}{25}$	$\frac{5.2}{15}$	$\frac{10.0}{3}$	10.3	$\frac{10.1}{10}$	$\frac{9.6}{20}$

$\sqrt{55.39}$

check to orig. BM 313 452.45 452.46

T.P. 1109 455.58 ✓  
456.58 256 444.49 ✓  
~~454.9~~

T.P. 1176 447.05 ✓  
448.05 117 435.29 ✓  
436.29

4 + 17 Run to here to show creek

3250

3100

T.P. 162 436.91 ✓  
437.91 10.63 435.29 ✓  
463 436.29 ✓  
445.92  
Mis-Read Rod

15 16

428.4  
8.5 5' di. Equal. 425.8 428.1 428.2  
20 15 11.1 8.8 8.7  
10 13

431.0 429.5 427.9 432.5  
5.9 7.4 9.0 4.4  
30 10 3 10

433.8 433.0 432.0 434.6  
3.1 3.9 4.9 2.3  
30 10 15

436.91 ✓  
437.91 ✓

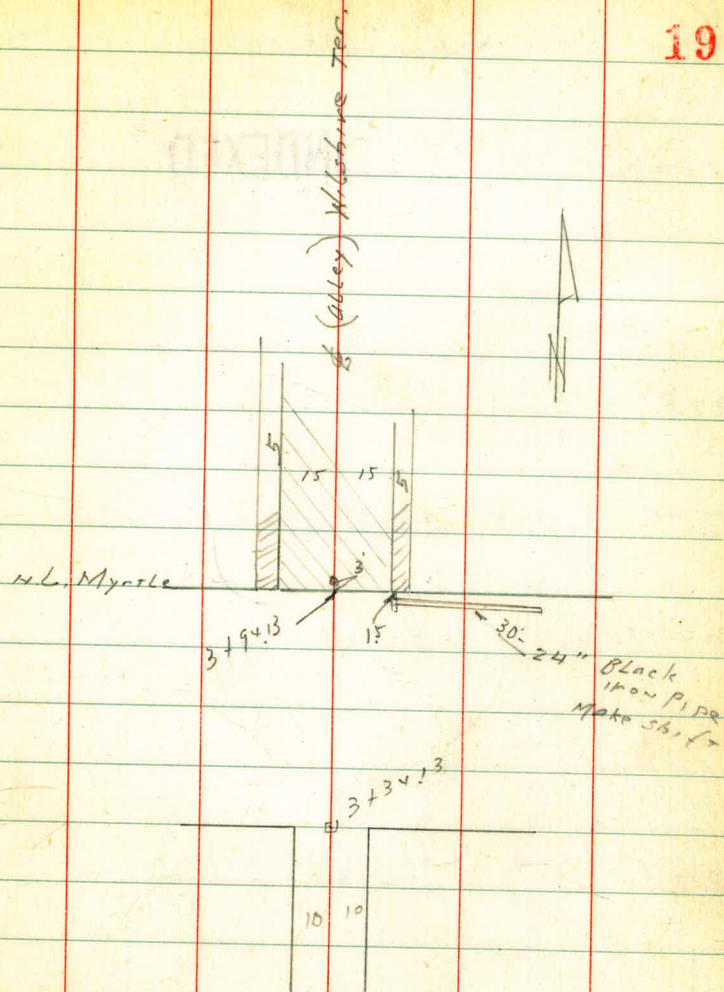




Alley 253 U.S.M.

INDEXED

19



1/5 sec Alley Blk. 253 Univ. Hts

LT

R

Rt

20

0-22

INDEXED

0.2228  
30

2.4202  
10

2.3165  
10

4.5213  
10

20.21025  
40

0-37

4.32185  
30

5.82120  
10

7.2215  
10

10.3215  
10

23.01995  
40

T.P.

1125 222.81 028 211.50

222.81

0-40

1.02125  
30

1.42103  
10

2.6212  
10

4.52093  
10

11.12002  
40

0-60

0.0219  
30

2.8209  
10

4.52073  
10

7.32045  
10

11.52002  
40

T.P.

11.98 211.84 138 199.80

211.84

BM.

SW BP 325 201.24

197.99

Myrtle  
Florida

0+59.5 NL CONWALK + SL GAR. APPROX

0+54.5

T.P. 7.88 239.73 0.16 231.85

0+40 Beg. 2" Cold Lay 10' to 20' LT.

T.P. 11.48 232.01 2.28 220.53

0+00 N.L. UPAS ST.

0-15

222.81

3.15 4.42  
28.5 20  
GAR. FLOOR APPROX

235.01	234.5	234.0	233.5	233.0	232.5	232.0	231.5
4.72	5.1	5.2	8.2	13.7	13.52	11.5	29.6
20	10	3		10	11.5	10	40
SL 5' CON. WALL	C.L.	C.L.			TOP WALL		

239.73

234.0	233.5	233.0	232.5	232.0	231.5	231.0	230.5
+2.4	+1.8	+1.8	3.1	7.9	7.68	20.8	
20	20	10		10	11.5	40	
TOP WALL	C.L.	C.L.			TOP WALL		

232.01

232.3	232.2	232.1	232.0	231.9	231.8	231.7	231.6
+9.5	+7.0	+4.9	1.7	6.7	6.07	18.2	
20	20	10		10.36	11.7	40	
TOP WALL				TOP 3" PIPE	TOP CON. WALL		

231.0	230.9	230.8	230.7	230.6	230.5	230.4
+6.0	+4.0	+2.3	3.1	8.3	19.2	
30	19	10		10	40	

222.81





2+734  $\varnothing$  Top Wall between steps

2+68.6 S.L. do. con steps

T.P. 5.30 240.92 4.11 235.4

2+25  $\frac{+0.8}{30}$

164 ft 14" dia

2+22 P.P. P.A. 34.67

2+11 26.34 E garage con floor

2+00 26.34 E garage con floor

1+89 26.34 E garage con floor

1+85

239.73

23

$\frac{237.45}{3.47} \frac{5.2}{13} \frac{235.2}{10}$   
Top Wall

$\frac{238.40}{2.52} \frac{236.0}{4.89} \frac{235.5}{5.2} \frac{235.2}{5.2} \frac{235.2}{5.5} \frac{235.3}{5.6} \frac{231.2}{9.6} \frac{232.8}{12.0} \frac{232.2}{12.7} \frac{232.5}{14.3}$   
Top Bot  
Step.

Top 3x3  
con landing  
then steps  
cont. up  
 $\frac{238.2}{2.0} \frac{238.2}{2.0} \frac{235.2}{4.4} \frac{235.2}{4.1} \frac{235.3}{4.4} \frac{235.2}{4.4} \frac{230.7}{8.8} \frac{235.2}{11.5} \frac{234.2}{14.8}$   
25 20 14 10 14 10 10 20 30

P.P.  
 $\frac{240}{1.0} \frac{237}{2.2} \frac{235}{4.3} \frac{235.5}{4.2} \frac{235.5}{4.2} \frac{235.2}{4.2} \frac{234.2}{5.5} \frac{235.2}{10.9} \frac{234.2}{15.1}$   
30 20 14 10 3 3 10 20 30

$\frac{239.2}{+0.1} \frac{237.2}{2.8} \frac{235.5}{4.2} \frac{235.5}{4.2} \frac{235.5}{4.2} \frac{235.2}{4.5} \frac{231.2}{7.9} \frac{230.2}{9.1} \frac{229.2}{11.6} \frac{228.2}{14.8}$   
30 20 14 10 3 3 10 20 30

239.73

376413 ♀ Myrtle

TP disk  
5.45 241.56 4.81 236.11  
Myrtle

3764

3719 P.P. P. 1949 1424 12" dia

373413 SL Myrtle

3700

27945 HL Steps

240.92

244	241	236	236	236	236	235	237	24
+ 2.9	0.0	5.4	5.7	5.0	5.0	6.6	9.9	11.3
30	20	13	10	7	7	10	20	30

241.56

12" d. Pepper  
Tree  
7.61

P.P.

244	241	236	236	236	235	237	237	51
+ 5.1	3.6	6.8	4.7	5.0	8.5	11.6	12.7	13.4
20	15	10	7	7	10	14	20	30

237	238	236	235	236	235	232	230	237
+ 3.6	2.4	4.5	5.0	5.3	5.4	8.7	12.9	13.6
30	20	17	10	5	5	10	20	30

236	237	236	236	235	236	230	229	229
2.45	4.73	5.3	5.3	5.4	5.4	10.3	11.5	14.0
19.8	14.8	13	10	3	3	10	20	30

3x3 cov. Top  
Landing Bot.  
STEP

240.92

67

8

R

check to DR 19. Bx	743	197.94	197.99
T.P.	5.58	205.37	1085 199.79
T.P.	1.22	210.64	1155 209.42
T.P.	1.07	220.97	1086 219.90
T.P.	0.72	230.76	1154 230.04

4 + 94.13 100' N of N.L. to show pav. cb, etc

3 + 94.13 N.L. Myrtle Beg. Con. Pav. and Comb. cb. and Walk

3 + 92.6

3 + 80

241.56

20	20	20	20	20	20	20	20	20
3.24	3.30	3.88	3.76	3.83	4.19	4.81	4.16	4.14
20	15	15	7.5		7.5	15	15	20
Walk	cb	90T				90T	cb	Walk

20	20	20	20	20	20	20	20	20
4.79	4.90	5.51	5.44	5.50	5.87	6.49	5.88	5.84
20	15	15	7.5		7.5	15	15	20
Walk	cb	90T				90T	cb	Walk

20	20	20	20	20	20	20	20	20
4.31	4.0	5.4	5.3	5.4	6.0	6.65	6.3	6.5
30	21	14	10	10	10	15	17	20
						Inv. in L	24" Pipe	OT

20	20	20	20	20	20	20	20	20
4.3	2.0	5.4	5.4	5.2	5.2	6.6	8.3	9.2
30	20	12	10		6	10	20	24
								30

241.56

33333

1 sec 20' Alley

BLK 206 Pacific Beach

Moore  
Be99  
D. JISSON  
4-C-49.

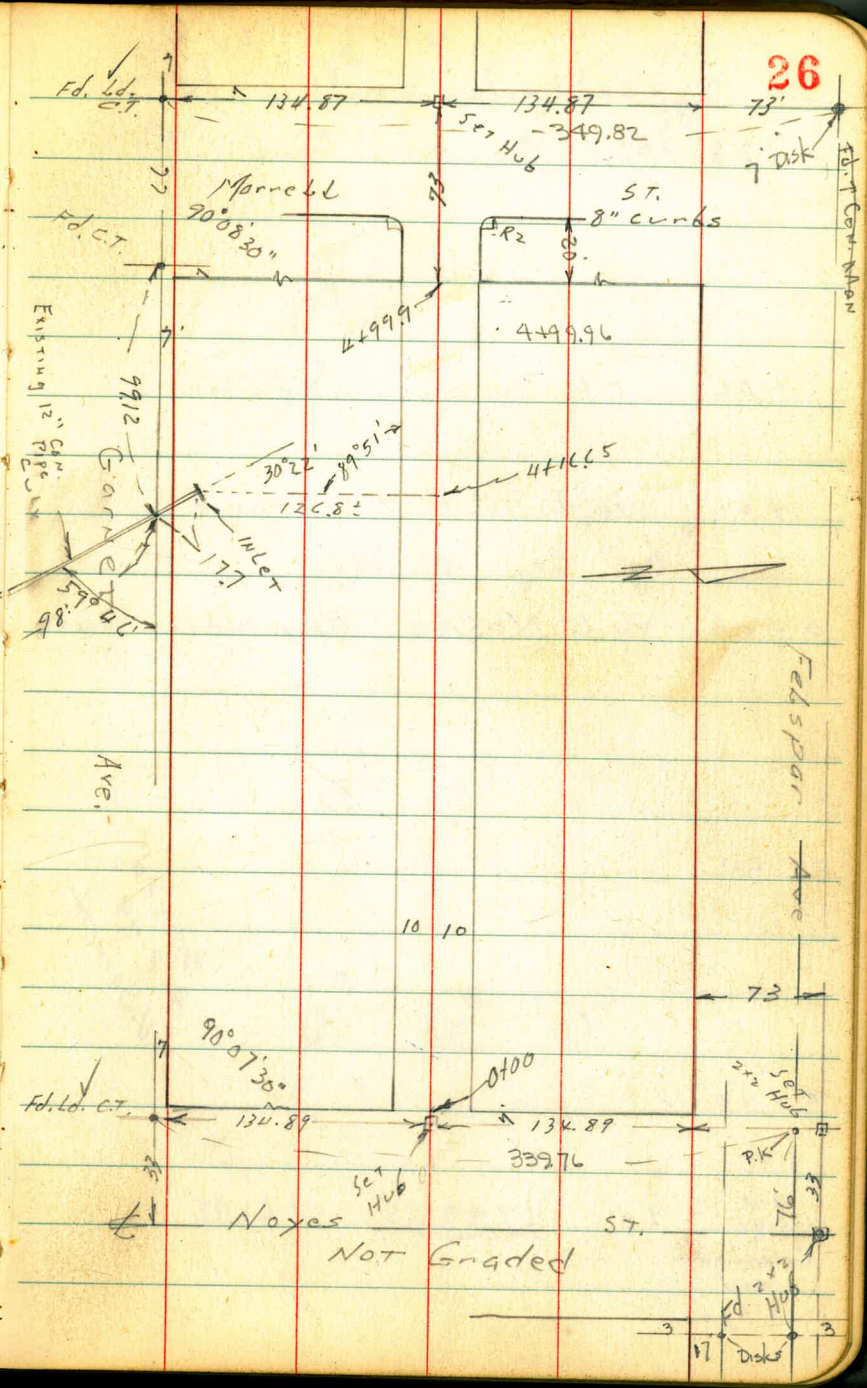
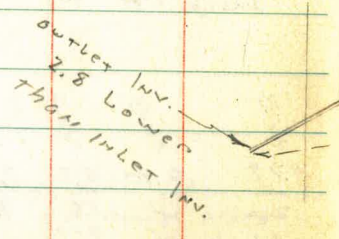
W.O. 25001

INDEXED  
WK  
APR 8 1949

134.87	349.82
269.74	66
73	28382
34274	141.91
14	66
5674	20791

339.76
56
28376
141.88
56
197.88

99.9  
166  
+833



$\begin{matrix} L \\ 63.92 \\ 4.07 \\ 16.9 \end{matrix}$ 
 $\begin{matrix} 63.8 \\ 4.2 \\ 10 \end{matrix}$ 
 $\begin{matrix} 63.8 \\ 4.2 \\ 10 \end{matrix}$ 
 $\begin{matrix} 63.9 \\ 4.1 \\ 10 \end{matrix}$ 
 $\begin{matrix} R \\ 64.8 \\ 3.2 \\ 20 \end{matrix}$ 
27

Xsec alley 206  
 0 + 28 W.L. Do. gar. Cont.

+ DL E.L. Do. gar. Cont. floor

+ 04 14" di. Tel. P. # 5057004

0 + 00 W.L. Noyes. Beg. picket Fence  
 10.1 R+

0 - 20

Reduced  
 8-49  
 U. Barrett

0 - 40

B.M. NW 1/4 601 67.99 61.98  
 Garnet and Noyes

$\begin{matrix} 63.92 \\ 4.07 \\ 16.9 \end{matrix}$

$\begin{matrix} 63.8 \\ 4.2 \\ 25 \end{matrix}$ 
 $\begin{matrix} 63.5 \\ 4.5 \\ 10 \end{matrix}$ 
 $\begin{matrix} 63.3 \\ 4.7 \\ 10 \end{matrix}$ 
 $\begin{matrix} 63.6 \\ 4.4 \\ 10 \end{matrix}$ 
 $\begin{matrix} 63.9 \\ 4.1 \\ 25 \end{matrix}$

$\begin{matrix} 62.7 \\ 5.3 \\ 25 \end{matrix}$ 
 $\begin{matrix} 63.1 \\ 4.9 \\ 25 \end{matrix}$ 
 $\begin{matrix} 63.4 \\ 4.6 \\ 25 \end{matrix}$

$\begin{matrix} 62.3 \\ 5.7 \\ 50 \end{matrix}$ 
 $\begin{matrix} 62.9 \\ 5.1 \\ 50 \end{matrix}$ 
 $\begin{matrix} 63.5 \\ 4.5 \\ 50 \end{matrix}$

67.99

0791 10.2 Lt NW Con Shed  
 0784 10.2 Lt NE Con Shed  
 0783 10.2 Lt NW Con. Shed

0777

0752 NE Con Shed 10.2 Lt.  
 Beg. wire fence 10 Lt.

0775 Con. end Con. Blk Wall 10.1 Lt.

T.P. 8.12 74.76 135 66.64

0764 Beg. Con. Blk. Wall 10.1 Lt.

0758 Beg. Picket fence 10.1 Rt

0750

0746 end Picket fence 10.2 Rt

67.99

28

68.3	67.8	67.8	68.2	68.1	66.0
6.5	7.0	7.0	6.6	6.7	8.8
10	7	7	7	10	20

65.4	65.3	68.1	68.4	67.1	68.0	66.9	65.5
9.4	9.5	6.7	7.4	7.1	6.8	7.9	9.3
15	10.1	10	7	7	8	10	20

Base Wall

65.4	65.2	66.6	74.76	66.7	65.5	65.1
2.6	2.8	1.4	1.5	1.3	2.5	2.9
15	10.1	10	10	8	10	20

Base Wall

65.4	65.6	65.1	65.0	64.9	65.1
2.6	2.4	2.9	3.0	3.1	2.9
20	10	7	10	10	20

67.99

1195 E Singar Con Floor No  
9' wide Aprons

1189 end fence 10.8 Lt

1153 Beg. Bd fence 11 Lt

1147.5 E 10' wide Con. Apron Level S. N. 9' wide

1141 10.9 Lt end Bd. fence

1125 Beg. Bd. fence 10.9 Lt  
77.84 Lt A 2074 - 91 Ft. TELP. 505726

1123 WL Singar.

1114 E.L. Con apron Singar.

1111 10.1 Lt end fence

1100

7476

68.81  
5.95  
12.7  
CON Floor

6.1  
10

5.9  
5.68.4

5.3  
10

69.5

4.5  
20

69.8  
29

69.79  
4.97  
19  
CON FL.

69.78  
4.98  
10.9  
Apron

69.7  
5.1  
10

69.8  
5.0

70.0  
4.7  
10

70.2  
4.5  
12

69.5  
5.3  
12

69.8  
4.9  
20

TOP CON. W/ 11 WITH ALLEY

69.42  
4.94  
14  
940

69.70  
5.00  
11.5  
Apron

69.8  
4.9  
10

69.8  
4.9

70.0  
4.7  
10

Picket Fence  
10

69.3  
5.5  
20

69.81  
4.95  
14  
940

69.68  
5.08  
11.5  
Apron

69.1  
5.7  
20

69.3  
5.5  
10

69.5  
5.3

69.5  
5.3  
10

67.6  
7.2  
17

67.3  
7.5  
23

7476



2 + 50 P.P. A 2050 9.2 Lt. 9" di

+ 49.6 105 Lt Beg. wire fence

2 + 49.5 end Bd fence + Blk. wall

67  
65.6  
5.9  
11  
Base  
Wall

2 + 39 end picket fence 10' Lt.

65.6  
5.9  
10  
Base  
Wall

2 + 28 11' Lt. Beg. fence +  
Com Blk Wall

67.0  
67.0  
5.5  
11  
Base  
Wall

2 + 22 W. do. gar. + Apron  
Com

67.55  
3.90  
19.8  
gar.

2 + 03 E. do. gar. Com. Apron + FL

67.56  
3.89  
19.8  
gar.

2 + 00 N end Top 6" Com. Blk Wall

68.40  
3.05  
10.4

T.P. 312 71.45 643 68.33

74.76

71.45

3106 WL 3 car gar.

3132 E. Con. Apron <sup>8' wide</sup> and <sup>and</sup> gar. Level

3119 E.L. 3 car gar. dirt floor

3100 end wire fence 10.4 L.

2175

2174 Tel. Pole 5057-7 H 8.7 Pt  
12" dia.

71.45

31

$\frac{6.1}{11.7}$	$\frac{6.2}{10}$	$\frac{6.5}{10}$	$\frac{6.7}{10}$	$\frac{6.5}{20}$
dirt floor				
	$\frac{6.3}{10}$	$\frac{6.3}{10}$	$\frac{6.6}{10}$	$\frac{6.8}{30}$
			Apron Level	gar. fl.

$\frac{6.1}{11.7}$	$\frac{6.4}{10}$	$\frac{6.4}{10}$	$\frac{6.6}{10}$	$\frac{6.6}{20}$
gar. dirt				

$\frac{6.5}{7.0}$	$\frac{6.8}{10}$	$\frac{6.9}{10}$	$\frac{6.3}{10}$	$\frac{6.6}{20}$
-------------------	------------------	------------------	------------------	------------------

$\frac{6.4}{7.5}$	$\frac{6.5}{10}$	$\frac{6.5}{10}$	$\frac{6.5}{10}$	$\frac{6.8}{20}$
-------------------	------------------	------------------	------------------	------------------

71.45

474

and Bog. Wine Fence 10.7 R<sub>7</sub>  
4725 Tel. P. 12" di. 9.2 R<sub>7</sub> 505728 H

4716.65

Inv. meter  
12" P. <sup>CON.</sup>  
PIPE

T.P. 608 70.55 698 64.47

4701 10" di. P.P. 9.1 LT A2020

4700 WIL do. gas dirt floor.

3783 EL. do. gas. dirt floor

3765 9.3.2 Con. slab

71.45

63.8	64.4	64.6	64.8	65.6	32
6.8	6.2	5.8	5.8	5.0	
15	10	10	10	25	

58.35	60.0	62.6	64.1	64.8	64.9	65.1
12.20	10.6	8.0	6.5	5.8	5.9	5.5
126.8	100	50	70	58	70	25

70.55

65.3	64.9	64.1	64.1	64.1	64.9
6.2	6.6	6.8	6.8	6.6	6.6
14	10	10	10	10	25

dirt floor

65.3	65.0	65.0	65.0	65.4
6.2	6.5	6.5	6.5	6.1
14	10	10	10	20

dirt floor

65.71	65.71
5.74	5.74
14.2	11.6

CON. slab

71.45

4+99.9 E.L. Morrell

4+85

4+65 10' Rt Beg. 6" Con. Ret. Wall

4+63 & 3' Con. Walk

4+61.5 10' Rt end wire fence

70.55

Lt

&

Rt

33

67.90	67.5	67.3	67.8	67.40
$\frac{2.5}{10}$	$\frac{3.1}{10}$	3.3	$\frac{2.8}{9.9}$	$\frac{2.15}{9.9}$
Top curb				Top curb

67.0	67.0	66.0	65.9	66.7	68.08	67.9
$\frac{2.6}{20}$	$\frac{3.1}{10}$	$\frac{4.1}{7}$	4.7	$\frac{3.9}{10}$	$\frac{2.7}{10}$	$\frac{2.7}{11}$
				dirt	Top wall	

65.8	65.4	67.40
$\frac{4.8}{10}$	$\frac{5.2}{10}$	$\frac{3.5}{10}$
dirt	Base wall	Top

66.9	66.1	64.9	65.0	65.8	66.11	66.42
$\frac{3.7}{20}$	$\frac{4.5}{10}$	$\frac{5.7}{2}$	5.6	$\frac{4.8}{10}$	$\frac{4.4}{10}$	$\frac{4.13}{20}$
					con.	con. walk

70.55

check to Starting  
B.M. 602 61.99 61.98  
001

T.P. 3.11 68.01 1050 64.90

Check to Top curb, 456 70.84 70.83  
001

T.P. 7.30 75.40 245 68.10

cut dirt

E 20' curb line Marrell

70.55

E cb. on SL Felspan, at Marrell  
FB 1701 page 42

66.2	67.11	67.11	67.6	67.8
4.4	3.5	3.5	3.0	2.8
40	10	dirt	10	40

67.00	67.57	67.1	68.19	68.74
3.55	2.98	3.5	2.36	1.81
40	10	dirt	10	40
cb	cb		cb	cb

70.55

W.O. 25001

CSM ADDL, NOTES ON ALLEY  
BLK 15 Bird Rock Add  
FROM P. 2 THIS BOOK

0411.7 end cb RETURN ON LT.

### INDEXED

0410.2 end cb. RETURN ON RT

SECTIONS II WITH FORWARD

0405.4 = H. edge sdw.

0400  
5+75.33 S.L. FORWARD = S edge sdw

T.P. 82x (87.05) 1.34 78.81

BM.  
SE BP 835 8015 71.80

La Jolla Blvd  
and  
Midway

Notes Reduced  
and 6/30/49

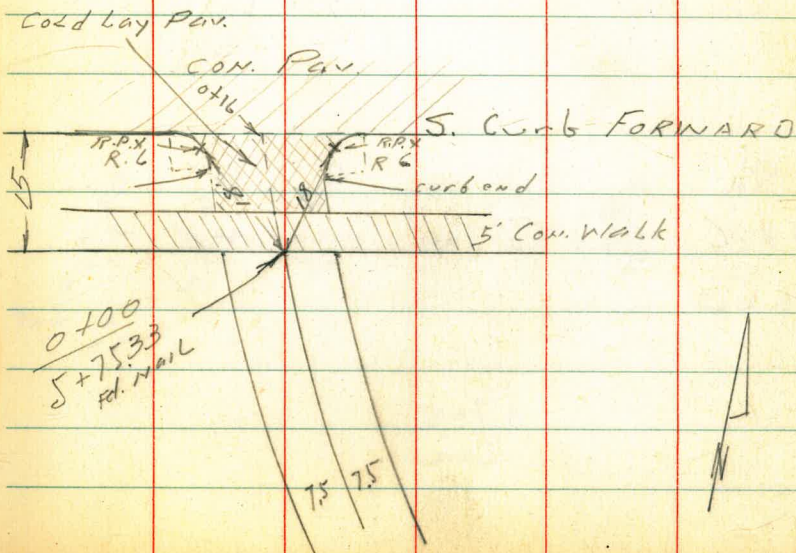
35

LT	E	RT
8141 5.64 TOP cb end 8.3	8106 5.99 8.3 P	8148 5.57 P
8183 5.22 9.5 P	8229 4.76 9.5 cb	

8156 5.49 7.8 P	8129 5.76 7.7 P	8165 5.40 7.4 P	8193 5.12 8.8 P	8230 4.75 8.9 TOP cb end
--------------------------	--------------------------	--------------------------	--------------------------	-----------------------------------

9112 5.88 20	8155 5.50 10	9202 5.03	9245 4.60 10	8282 4.10 20
--------------------	--------------------	--------------	--------------------	--------------------

8155 5.70 20	8125 5.30 10	9224 4.83	9264 4.41 10	8302 3.98 20
--------------------	--------------------	--------------	--------------------	--------------------



Alley Blk 15 Bird Rock

36

0+16 sly cb of Forward

87.5

81.15	80.45	80.23	81.02	81.55	81.21	82.38
5.90	4.60	4.22	6.03	5.50	5.30	4.67
12.6	12.6	2.5	P	12	10.0	16.0
→	P	P	P	P	P	
Top cb						Top cb B.C.
B.C.						

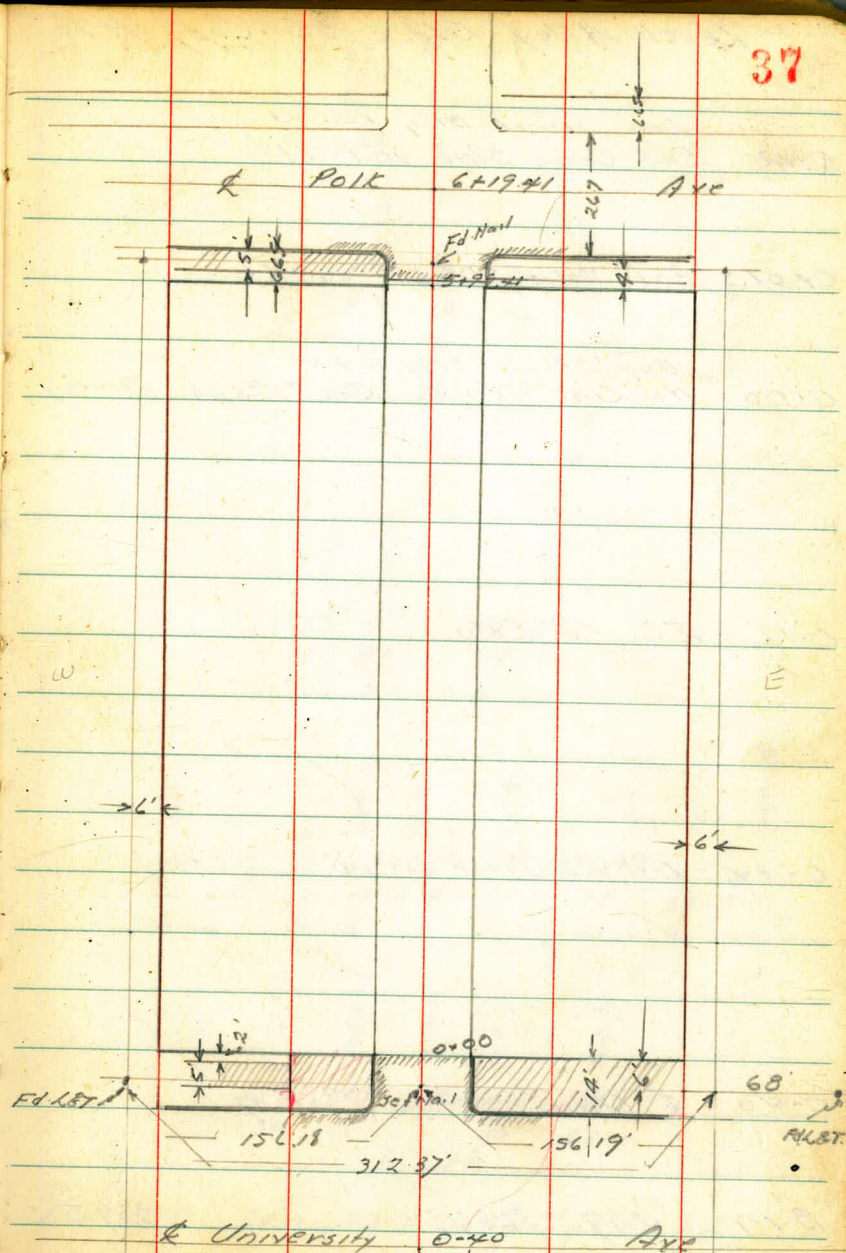
9-29-49  
Hendricks  
Roberts  
Greer  
WO# 31771

Re-Cross section Alley  
Block 35 City Hts.  
(Original Notes FB 1571 P-57)

INDEXED

W.K.  
SEP 30 1949

NOTES REDUCED BY MORGAN 9-30-49.





Levels Alley Block 35 City Hts.

0+12 Beg Stucco Bldg 10.1 Lt.  
End. Conc. Slab 10.1 Lt.

0+01.5 Gate Valve SDG&R 4.4 Lt.

0+00 Beg Stucco Bldg. 99 Rt.  
No. Line Univ. End Asph. Paving

0+12 EC Cb. Ret.

0+14 No. Cb. line Univ.

0+40 R Univ. Asph. Paving

B.17 4.19 363.73

359.54

76

359.07  
1.06  
10.1

358.72

5.01  
99  
G&C

358.26

5.47  
99  
Cb

358.11

5.62  
60  
Cb

358.87

5.84  
50

358.06

5.47  
99  
G

358.57

5.16  
60  
G

358.69

5.04  
10

358.10

5.47  
99  
G

357.88

5.77  
60  
G

358.63

5.11  
10

358.42

5.47  
99  
Cb

357.76

5.77  
60  
G

358.61

5.12  
10

358.23

5.24  
99  
G

357.84

5.89  
60  
G

358.38

5.35  
50

358.49

5.13  
99  
Cb

357.97

5.42  
60  
Cb

358.31

5.35  
50

358.60

5.13  
99  
Cb

357.62

6.11  
55  
G

358.04

5.19  
55  
Cb

UNBP University & 36th St.

363.73

Block 35 City Hts. Contd.

1+13 E Double Garages Lt & Rt.

1400

0+66 R 15 Drive 11' Rt

0+58 End Stucco Bldg. 10' Lt.

0+52 End Stucco Bldg 10' Rt.

0+50

0+49 Power Pole # JP. 4009 9' Lt.

T.P. 7.17  $\frac{366.29}{x}$  4.61 359.12  
363.73

361.12  
5.17  
14.3  
Fl  
360.69  
360.59  
360.49  
360.29  
360.29  
360.59  
360.59  
5.17  
5.17  
20 10 6 10 20

360.74  
5.17  
11  
Ramp.  
360.78  
5.21  
20.5  
Fl.

360.29  
359.79  
359.89  
359.79  
360.29  
6.1  
6.4  
6.4  
6.1  
6.10

366.29  
x



Block 35 City Hts. Contd.

TP. 7.54 370.57 2.26 364.03

4+00

3+93 E Single Garage 16.4 Rt.

3+50

3+25 End 5' Conc. Block Wall 10.1 Lt.  
Power Pole # PAM 605 9.5 Lt.

3+00

2+75 Beg 5' Conc Wall 10.1 Lt.

2+64 End Conc. Ramp 10.4 Lt.

366.29  
A

20 364.29  
20 364.09  
20 364.09  
20 364.09  
20 364.09  
20 364.09

363.78

2.5  
16.4  
Fl.

27 363.39  
31 363.19  
32 363.19  
32 363.09  
29 363.39  
30 363.29  
27 363.59

34 362.89  
36 362.69  
35 362.79  
35 362.79  
37 362.59  
37 362.99  
37 362.99  
37 362.99

362.35  
362.29

39.4  
15 10.4  
Fl. Ramp

366.29  
A

Block 35 City Hts. Contd.

4165 & Double Garage 15.2' Lt

4163 & Double Garage 96' Rt.

4150

4132 & Single Garage Divt Fl. 11' Lt

4125 Power Pole # PA 4065 9.3' Lt

4109 & Single Garage 16.2' Rt

371.57  
K

365.25  
32  
18.2  
Fl.

364.99

5.18  
96  
Fl.

364.67	364.67	364.77	364.67	364.87	364.97
67	67	68	67	67	66
20	10		5	10	20

364.67  
67  
11  
Fl.

364.90

7.17  
16.2  
Fl.

371.57  
K

Alley Block 35 City Hts. Contd.

5+75 End Frame Garage 9.5 Rt. opens North

5+55 End Wire fence 9.5 Rt.  
Beg Frame Garage 9.5 Rt. opens to North

5+56 & Single Garage 10.4 Lt.

5+15 Beg Wire fence 10.2 Rt.

5+50

5+24 Power Pole # PA 4085 9' Lt.

5+16 & Single Garage 15.9 Lt.

5+00

371.57  
X

366.77  
366.57  
366.47  
366.17  
365.97  
366.27  
366.37  
366.07

2.8 5.0 5.1 5.1 5.6 5.1 5.2 5.5  
15 10 7 6 8 9.5 14  
FI

366.29

5.28  
10.4  
FI

365.97  
365.97  
365.67  
365.87  
365.77  
365.87

5.6 5.1 5.9 5.7 5.8 5.7  
10 6 8 10 20

365.62

5.99  
15.9  
FI

365.37  
365.37  
365.27  
365.07  
365.37  
365.27  
364.97

6.10 6.10 6.10 6.10 6.10 6.10 6.10  
16 10 6 6 8 10 20

371.57

Piley Bk 35 City Hts. Co. Ill

B. 17

989 359.55 359.54

T.P. 1.14 371.41 3.27 368.30

6+19.41 E Polk Ave

6+06.50 So. Cb line Polk Ave

6+04.00 BC Cb Pkls

6+01.41 Reg Cb & Asphalt Paving

5+99.41 So. line Polk

371.57

NWBP Univ & 3674 St

44

366.70	366.05	366.05	365.49	365.57	365.31	365.22	365.20	365.73	364.69	365.38
4 <sup>87</sup>	5 <sup>52</sup>	5 <sup>52</sup>	6 <sup>08</sup>	6 <sup>06</sup>	6 <sup>26</sup>	6 <sup>34</sup>	6 <sup>37</sup>	5 <sup>84</sup>	6 <sup>88</sup>	6 <sup>12</sup>
60	60	12	12	10	6	10	12	12	50	50
Ch	G	Ch	G				G	Ch	50	50
			366.02	365.64		365.34		365.75		
			99	99		10	10			
			Ch	G		G	Ch			
	366.03	365.82	365.81	365.69	365.62	365.77				
	5 <sup>52</sup>	5 <sup>55</sup>	5 <sup>76</sup>	5 <sup>88</sup>	5 <sup>95</sup>	5 <sup>10</sup>	5 <sup>10</sup>			
	98	98	4		10	10				
	Ch	G			Ch	Ch				
	366.27	365.97	365.67	365.67	365.87	365.97				
	5 <sup>13</sup>	5 <sup>15</sup>	5 <sup>9</sup>	5 <sup>9</sup>	5 <sup>1</sup>	5 <sup>6</sup>				
	10	9			7	10				
						16				

371.57

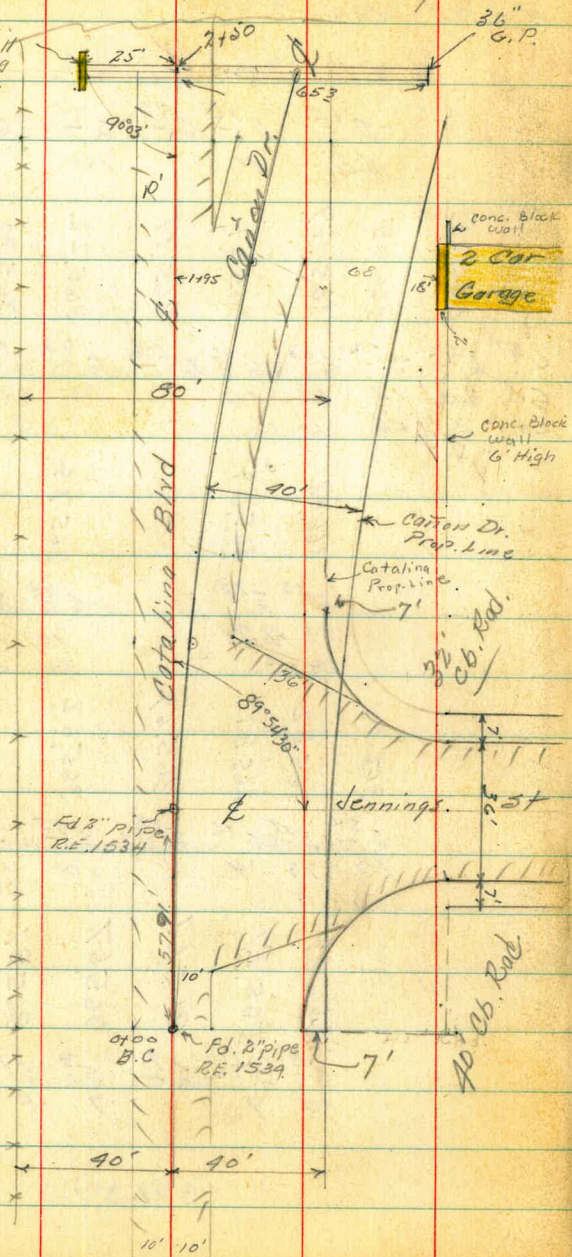
Johnson  
Greer  
Cota  
Fay  
2-2-50  
W.O. 25020

4-section Catalina Blvd. for 200'  
+ Cañon Drive for 200' NE1/4

INDEXED

FEB 8 1950

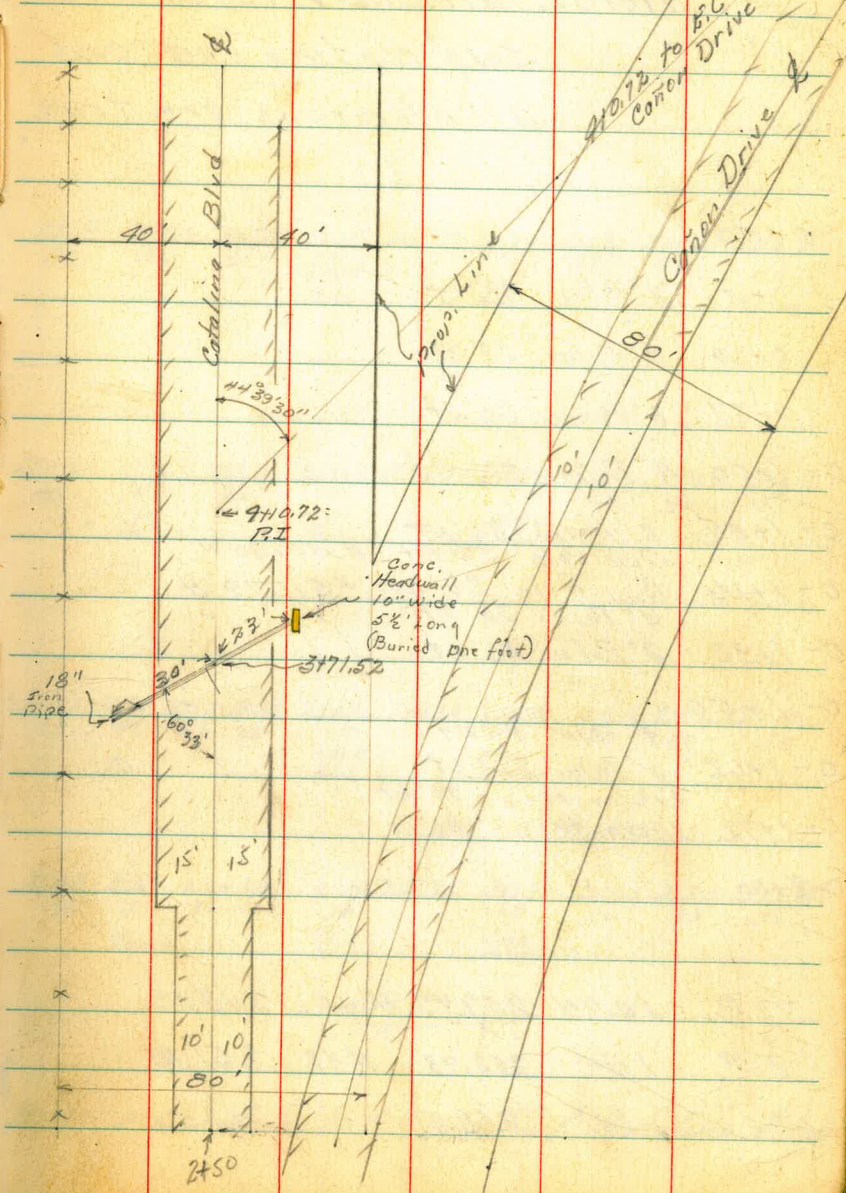
Conc.  
Headwall  
10' Long  
10" wide



Additional Notes

45

P. 72





4-section Catalina Blvd.  
Cañon Drive

Note!! All shots taken with  
self reading rod and  
all elevations are true.

0+50

0+51 = 2' Palm 26' Lt

0+69 = 3' Palm 33' Rt

0+77 = 2' Palm 26' Lt

0-1+00 4' Palm - 32' Rt

0-1+05 2' Palm 26' Lt

Guy Pole 39' Rt # 511180 H

0-1+16 Guy Pole 29' Lt # 511179 H

4' Palm 33' Rt

0-1+32 = 2' Palm 26' Lt

0-1+50

4' Palm 33' Rt

0-1+62 = 2' Palm 26' Lt

4' Palm tree 33' Rt

0-1+92 = 2' Palm tree - 26' Lt

0-2+00

T.P. 10.94 259.47 4.40. 248.53

T.P. 1.44 252.93 11.42 251.49

1.41 262.91 261.50

Lt.

+

Rt.

46

251.8	251.8	251.8	251.70	251.77	251.56	251.2	252.2	252.6
80	40	21	10	10	10	27	40	50
			Edge		Edge			
			Pave		Pave			

252.3	252.1	253.2	253.23	253.34	253.19	253.1	254.9	256.0
80	40	22	10		10	28	40	50
	fence		Edge		Edge			
			Pave		Pave			

254.1	255.9	256.2	254.8	254.86	254.98	254.86	254.9	256.6	257.9
75	40	29	22	10		10	26	40	50
	fence			Edge		Edge			
				Pave		Pave			

254.9	256.8	256.9	256.3	256.37	256.55	256.37	256.2	258.1	259.1
90	40	30	22.5	10		10	26	40	50
	fence			Edge		Edge			
				Pave		Pave			

259.47  
1

B.M. Mon. t. talbot & west of Catalina Blvd.

4-section Catalina Blvd &  
Canyon Drive

1+01

0+89 = 4' Palm 30.5' Lt

0+60 = 4' Palm 30.5' Lt

0+57.91 =  $\frac{1}{2}$  Jennings St. & Catalina Blvd.

0+30 = 3' Palm 27' Lt

0+15.5

T.P. 9.02 253.27 4.89 249.25  
D = 44°39'30"

0+00 = B.C. Canyon Drive to Rt.

T.P. 4.84 254.09 10.22 249.25

0-02 = Power Pole 40' Rt #511177 H

0-03 = Power Pole 29.3' Lt #511178 H

0-23 2' Palm 26' Lt

0+44 =  $\frac{1}{2}$  8' cemo. drive 49.6' Rt

259.47  
/

Lt. \$ Rt.

47

249.8 246.6 246.9 249.2 249.05 248.79 248.34 248.08 247.86 248.74  
80 40 26 20 10 10 157.5 9 CB  
fence 42.4

249.4 248.8 249.6 249.62 249.35 248.77 248.61 248.87  
80 40 21 10 10 26 40  
fence

250.8 250.0 250.4 250.08 249.85 249.41 249.20 249.34 249.96  
80 40 27 10 10 28 G CB  
fence 44.6

251.0 250.3 251.0 250.33 250.15 249.70 249.5 250.26  
80 40 25 10 11.5 G CB  
fence Edge Pavc. Edge Pavc. 35.6

251.4 251.0 250.9 250.65 250.41 250.07 249.86 250.64  
80 40 21 10 10 33 CB  
fence Edge Pavc. Edge Pavc. Conc. CB

2" pipe & Catalina Blvd. & Jennings St.

253.30 254.37  
49.6 60

259.47  
/

4-section Catalina Blvd

Canyon Drive

3490 = 3' Palm 30' Lt  
 3' Palm 32' Rt ✓  
 3471.52 = 4 18" pipe on diagonal  
 3461 = 3' Palm 31' Rt ✓  
 3458 = 3' Palm 33' Rt ✓  
 3450  
 3430 = 4' Palm 31' Lt  
 3408 = widening of Catalina Blvd 248.6  
 80  
 3400 = 3' Palm 31' Lt  
 2470 = 3' Palm 31' Lt  
 2449 = 4 36" G.P. Culvert 248.9 247.7  
 80 47  
 2439 = 3' Palm 30' Lt  
 2420 = Guy Pole 30' Lt # 511176 H  
 2410 = 4' Palm 31' Lt  
 2400  
 1480 = 3' Palm 30' Lt  
 1450 = 4' Palm 30' Lt 247.4  
 80  
 1419 = 3' Palm 31' Lt

St. E. Rt. 48

244.51  
 I.F.  
 18" Pipe  
 24715  
 Headwall

245.8 244.7 244.9 248.2 248.49 249.40 249.25 247.8 248.2 247.95  
 80 40 30 23 15 16 30 40 53  
 Fence Edge Pipe Edge Pipe Canyon Dr.

247.5 245.0 245.0 247.7 248.10 248.22 248.07 247.74  
 48 40 30 21 10 16 40  
 Fence Edge Pipe

244.9 243.95 247.65 249.9 248.03 249.00 248.01 246.80 246.6 244.1 240.47  
 40 25 248.20 10 19 42 50 60 64  
 Fence I.F. Headwall Edge Pipe J.F. Pipe

244.7 247.9 245.3 245.6 248.1 248.09 248.15 247.89 246.92 247.0 247.8  
 80 47 40 24 19 10 10 33 40 50  
 Edge Pipe

245.9 245.6 246.4 248.7 248.60 248.42 247.99 247.50 247.25 247.5 247.8  
 59 40 25 19 10 10 20 25 34 40  
 Fence Edge Pipe

253.27

4-section Catalina Blvd &  
Cañon Drive

Lt

¢

Rt.

49

$\Delta 99^{\circ} 39' 30''$

410.72 = P.I. for Cañon Drive

245.6  
60

245.6 245.9 248.5  
40 30 25  
Fence

248.82 248.86 248.74  
15 15  
Edge Edge  
Pave Pave

248.4 248.5  
40 50

253.27  
\*

4-section. Cañon Drive

Lt.

\$

Rt.

50

4100

248.6 248.48 248.15 247.73 247.55 248.0 247.9 248.3  
 25 11 9 15 20 35 50

248.9  
 75

3150

248.2 247.94 247.58 247.15 247.01 247.4 240.2 239.7  
 25 11 9 15 20 39 55

T.P. 5.10 254.35 4.02 249.25

3100

248.21 248.11 247.72 247.34 246.87 246.75 249.5 242.4 242.4  
 50 30 9 10 14 20 32 42  
 Edge Pave

2143

247.9 248.02 248.00 247.31 246.86 246.62 246.80 248.3 243.9  
 50 40 17 10 13 19 32 40  
 Edge Pave

2133

248.0 248.03 248.11 247.40 246.70 247.4 247.7 247.6  
 48 39 23 12 26 40 50  
 Edge Pave

2117 = Power Pole 34.2' Rt + 45' 247 H  
 Int. of 4 Garage Produced

2100 = 4 2 car Garage 48.4 Rt to cone. Ramp.

245.1 248.2 248.06 248.12 247.51 247.10 246.83 247.1 248.1 248.4  
 48 40 31 18 9 13 20 40 50  
 Edge Pave

248.92 249.03  
 48.4 50.4  
 Ramp Floor

1150 on Cañon Drive

245.5  
 50

245.7 248.6 248.52 248.38 247.95 247.5 247.25 247.4 248.7 248.6  
 26 21 22 11 9 15 21 40 50  
 Edge Pave

Notes: Sections 0100 thru

1100 on Cañon Drive are same

as on Catalina Blvd

252.27

4-section Cañon Drive

check

248.87 248.86

5+00

4+50

Lt.

\*

Rt

51

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FEB 8 1950

Sta. 4110.72 = P.I. Cañon Drive Curve P-49

250.3	250.2	250.7	250.2	249.85	249.33	249.0	251.4	250.6
50	32	24	10		10	29	38	50

249.2	249.6	249.20	248.88	248.30	247.9	249.6	249.8	249.8
50	26	11		12	23	30	39	50

254.35  
/

Johnson  
Hendricks  
Greer  
COTG  
2-6-50

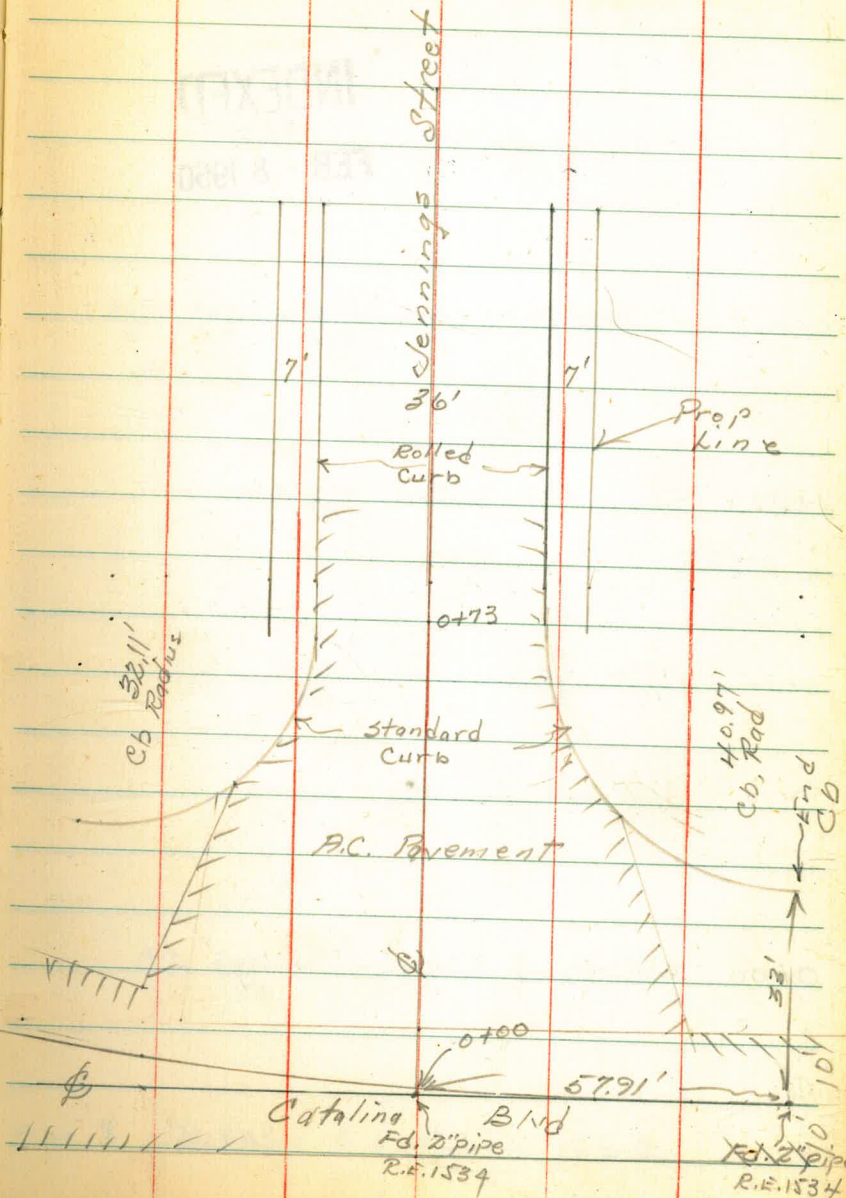
# Curb Returns on Jennings Street -

INDEXED

FEB 8 1950

52

Casson  
Drive



Vacation Jennings St from E  
Catalina Blvd 132' East  
of Existing Curb Returns.

INDEXED

FEB 8 1950  
M.K.

0+71.5 = B.C. on left

0+39.5 = End Existing Curb Left

0+23 = End Existing Curb Right

0+25 = M.H.

0+10

0+00 = E Catalina Blvd & Jennings St.

6.30  $\frac{255.55}{1}$

249.25

Lt.

¢

Rt.

53

249.11	249.61	249.69	249.71	250.19
G	cb		G	cb
	18.7		18.7	

247.7	248.50	248.17	248.89	249.32
G	cb.	32.8		30.2
	53.6			

248.0	248.01	248.72	249.29	249.8	250.65
50	35.5		31	36.	cb.
					53.2

248.0	247.98	248.61	249.30	249.0
50	39		32	50

248.22	248.82	249.68
44		43

248.71	249.33	250.32
50		50

Pipe & Jennings & Catalina Blvd





X-Sect: 20' Alley in Block 5  
Alhambra Park - Map No. 1488

# 4227

W.O. 31777

3-6-50

Osborne  
Hatch  
Shepard..

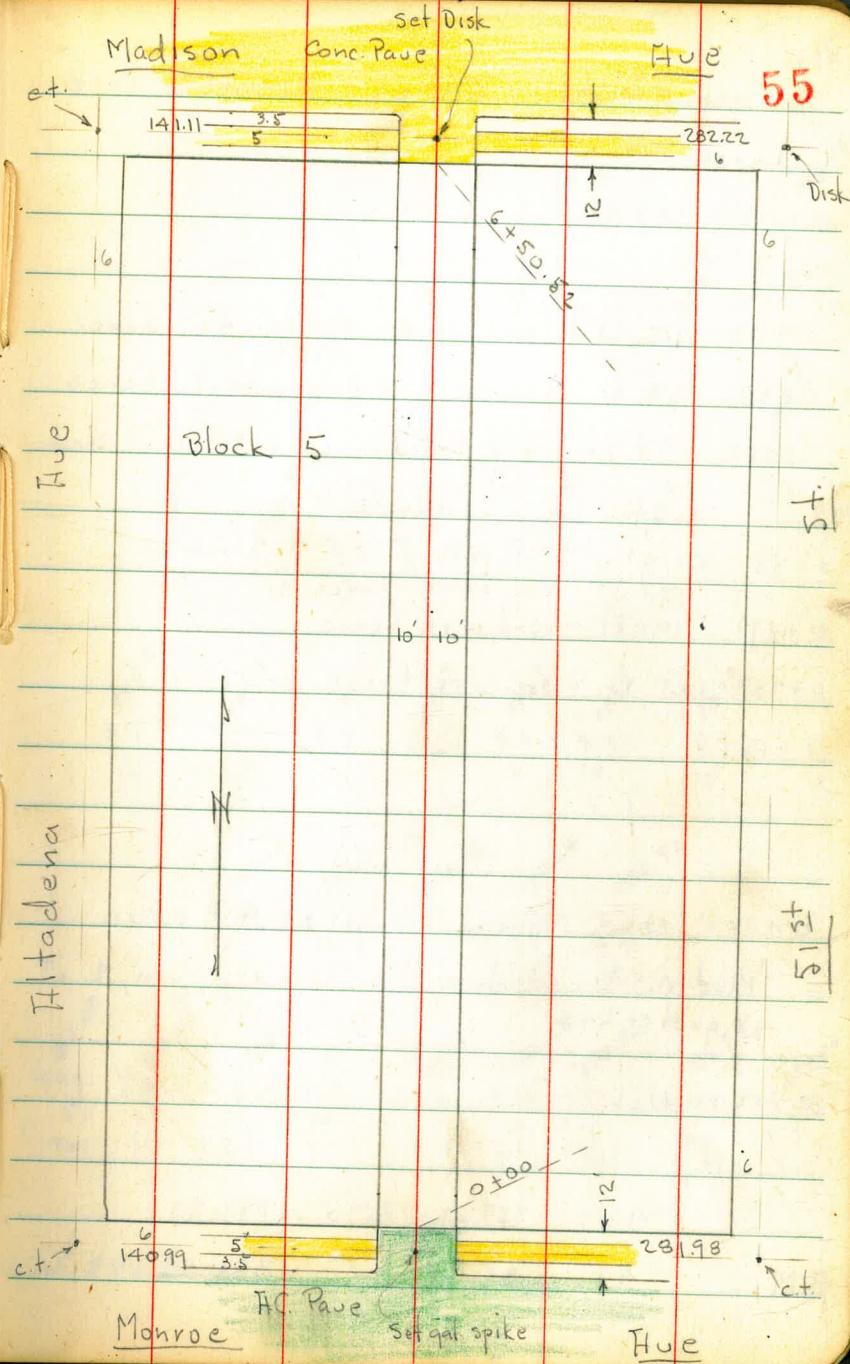
INDEXED

W.K.  
MAR 7 1950

Notes next page

Soil Sample - 5+50

REDUCED 3-7-50  
P.V.S.



X-Sect. Alley - Blk. 5. - Alhambra Park  
 Sketch - P. 55

1+03 - 10.2 Rt. =  $\pm$  4' Conc. walk

1+00 - 9.8 Lt. = end wire + beg picket fence

0+88 - 9.8 Rt. = end shed + Beg picket fence

0+80 - 9.8 Rt. = end Board fence + Beg small shed.

- 9.5 Lt. = Beg wire fence

0+50 - 8.6 Lt. =  $\pm$  P. pole + J.P.A. 4525

10.1 Rt. = Beg board fence

0+49 - 10.2 Rt. = end wire fence

0+25 - 10.1 Rt. = Beg wire fence

0+10

0+00 = N.L. Monroe = edge of A.C. pave

Pave in  $\pm$  is definitely lower than  $\pm$  at  
 N. gutter line

0-12 = N.cb.

4.69 387.67 7.90 382.98

B.M. 4 05 390.88 386.83 = S.E. Cct.

56

Lt. = W.  $\pm$  Rt. = E

Lt. = W.	$\pm$	Rt. = E
389.6 3.1 15	384.1 3.6 10	384.44 3.23 10.2 walk 3.3 15
384.4 3.3 15	384.3 3.4 10	384.7 3.20 20 walk 3.7 9.8 = Cor. shed.
389.2 3.7 15	384.3 3.4 10	382.1 4.2 10
382.2 4.8 7	382.1 5.0 6	384.6 3.1 15
382.68 7.99 50 Top	383.01 4.66 10 Top end cbl	382.9 4.8 6 10
382.21 5.46 50 Top	382.61 5.06 10 9.4	382.91 4.76 9.9 Top-end cb.
382.85 4.82 50 Top	382.48 5.19 10 9.4	382.64 5.03 9.9 9.4
382.57 5.16 50 Top	382.52 5.15 10 9.4	382.86 4.81 Top 2 Rad.
382.59 5.09 50 Top	382.96 4.61 50 Top	
	387.67	
	51st + Madison	

3+12 10.2 Rt. = end fence  
 3+02 - 10' Lt. = end fence  
 3+00  
 2+65- 10.1 Lt. = Beg. board fence  
 2+59- 10.1 Lt. =  $\pm$  Sing. Gar. - Conc. floor.  
 2+53- 10' Lt. = end fence  
 2+51- 8.8' Lt. =  $\pm$  P. pole # P.A. 4545  
 2+50  
 2+25- 10' Rt. = end Board + Beg. Lath fence  
 2+00 - 9.9 Lt. = fence  
 1+91- 10.2 Rt. = Beg. Rail fence  
 T.P. 6.20 390.27 2.60 384.07  
 1+84- 12.1 Rt. =  $\pm$  of Back of Sing. Gar. <sup>To E.</sup> -opens  
 1+75- 10' Rt. = end picket fence  
 10' Rt. = fence  
 1+50 - 9.8 Lt. = fence  
 1+47- 8.8' Lt. =  $\pm$  P. pole # P.A. 4535  
 1+15- 11.4' Rt. =  $\pm$  of 4' wing to House - conc. found

Lt.	$\pm$	Rt.	57
<del>384<sup>5</sup></del> 5.8 15	<del>384<sup>6</sup></del> 5.7 10	<del>384<sup>4</sup></del> 5.9 10	<del>384<sup>3</sup></del> 5.6 10
<del>384<sup>2</sup></del> 5.85 10.1 floor.			<del>385<sup>2</sup></del> 5.0 15
<del>384<sup>3</sup></del> 6.0 15	<del>384<sup>2</sup></del> 6.1 10	<del>384<sup>2</sup></del> 6.1 10	<del>384<sup>5</sup></del> 5.8 10
<del>384<sup>4</sup></del> 5.7 15	<del>384<sup>4</sup></del> 5.9 10	<del>384<sup>1</sup></del> 6.2 10	<del>384<sup>5</sup></del> 5.8 15
		<u>390.27</u>	<del>384<sup>3</sup></del> 6.0 15
			along House
			<del>384<sup>5</sup></del> 3.2 12.1 along Gar.
<del>384<sup>1</sup></del> 3.0 15	<del>384<sup>3</sup></del> 3.4 10	<del>384<sup>0</sup></del> 3.7 10	<del>384<sup>4</sup></del> 3.3 10
			<del>384<sup>1</sup></del> 3.0 13.9 = along House
			<del>384<sup>2</sup></del> 3.5 11.4 ground
		<u>387.67</u>	<del>384<sup>4B</sup></del> 3.19 11.4 floor.

T.P. 6.42 392.43 4.26 386.01

5+00

4+88- 10' Rt. = fence

4+75- 10' Lt. = end fence + 9.9' Lt. = beg. wire Cyclone fence

4+55- 9.8' Rt. = end Conc. for fence

4+50- 9.9' Rt. = fence - Conc. found. 6"

4+49- 7.9' Lt. = P. pole # P.A. 4565

4+25- 10' Lt. = Beg. board fence  
(dip Sect)

4+24- 10.4' Lt. = 2' Conc. Drain from Court

4+23- 10.4' Lt. = end House

4+00- 9.6' Rt. = end Cabin + Beg. picket fence

3+96- 10.2' Lt. = Beg. House - pier found.

3+88- 10' Lt. = 5' flagstone walk

3+86- 9.6' Rt. = end fence + Beg. Small Cabin

3+75- 10' Lt. = Beg. board fence

3+64- 9.8' Rt. = end Green house + Beg. Picket fence

3+51- 9.9' Lt. = P. pole - # P.A. 4555

3+50- 9.9' Rt. = Beg. Green House - Conc. floor

3+14- 11.3' Lt. = 2' Doub. Gar. Conc. floor

58

Lt. 385.8  
4.5  
15  
385.8  
4.5  
10  
385.6  
4.7  
10  
385.1  
4.6  
10  
Rt. 385.8  
4.5  
15

385.6  
4.7  
15  
385.6  
4.7  
10  
385.3  
5.0  
9.9  
386.28  
3.99  
10  
385.1  
4.6  
10  
385.7  
4.6  
15  
385.1  
4.6  
9.8  
Top Conc.

385.8  
4.5  
10.4  
ground.  
385.74  
4.53 = I.E. of  
10.4 Drain  
385.4  
4.9  
10  
385.2  
5.1  
385.2  
5.1  
9.6  
385.4  
4.9  
15

385.30  
4.97  
15  
walk  
385.25  
5.02  
10  
walk  
381.59  
2.68  
10.2  
floor  
385.2  
5.0  
10.2  
ground

384.95  
5.32  
11.3  
floor.  
384.9  
5.4  
15  
385.0  
5.3  
10  
384.6  
5.7  
385.3  
5.0  
9.9  
385.49  
4.78  
9.9  
floor.

390.27

386.29  
3.98  
9.8 = Top  
Conc.

385.3  
5.0  
9.6  
386.21  
4.06  
9.6  
floor

check Starting B.M. 5.59 386.84 386.83

6+62.52 = S. cb.

6+50.52 = S.L. Madison - edge Conc. pauc = 0.2 N. Rods on edge

6+35

6+00 - 10.1 Lt. = end fence

5+63 - 10.7 Rt. = 2' Conc. walk

5+57 - 11' Rt. = end House

8.5 Lt. = # of P. pole # BA 4585  
5+50 - 10.1 Lt. = endwire + Beg. board fence - 10' Lt.

5+25 - 10.2 Rt. = end fence + 10.6 Rt. = Beg. House

386.69	386.34	386.81	386.42	386.43	386.47	386.88	386.61	386.98
5.74	6.09	5.62	6.01	6.00	5.96	5.55	5.82	5.45
40	40	Top	10	10	10	Top	40	40
Top	9+.	2' Rad.				2' Rad.	9+.	Top

386.93	386.84	386.62	386.78	387.02
5.50	5.59	5.81	5.65	5.41
10	10	10	10	10
Top	9+.		9+.	Top

387.1	387.1	387.2	387.5	387.6
5.3	5.3	5.2	4.9	4.8
15	10		10	15

386.5	386.7	386.5	386.7	387.4
5.9	5.7	5.9	5.7	5.0
15	10			15

386.54	386.65	386.2
5.89	5.78	6.2
10.7	20	11
walk		at Cor.

385.9	386.0	385.8	386.0	386.2
6.5	6.4	6.6	6.4	6.2
15	10		10	11

385.9	386.28
6.5	6.15
10.6	10.6
ground	floor.

392.43

6:15.50 Re - Cross Section Alley  
 Hendricks  
 Johnsons BIK 35 City Hts.  
 Greer  
 Crawford for checking Quantities only  
 WO # 31.771

60

2150

362<sup>25</sup> 362<sup>22</sup> 362<sup>21</sup> 362<sup>15</sup> 362<sup>11</sup>  
 10 10 20

INDEXED  
 YK  
 JUN 16 1950

2100

361<sup>6</sup> 361<sup>4</sup> 361<sup>7</sup> 361<sup>5</sup> 361<sup>1</sup>  
 14 10 10 18

1150

361<sup>1</sup> 361<sup>9</sup> 361<sup>3</sup> 360<sup>9</sup> 360<sup>8</sup>  
 14 10 10 16

1100

360<sup>7</sup> 360<sup>7</sup> 360<sup>5</sup> 360<sup>5</sup> 360<sup>2</sup>  
 16 10 10 17

0150

360<sup>1</sup> 360<sup>1</sup> 360<sup>2</sup>  
 10 10

0100

358<sup>73</sup> 358<sup>73</sup> 358<sup>49</sup> 358<sup>60</sup>  
 99 99 99  
 68Cb 6 66

Alley Block 35 Contd.

4

61

5+50

366<sup>3</sup> 366<sup>1</sup> 366<sup>0</sup> 365<sup>2</sup> 365<sup>8</sup>  
14 10 10 14

5+00

365<sup>4</sup> 365<sup>1</sup> 365<sup>2</sup> 365<sup>4</sup> 365<sup>2</sup> 365<sup>0</sup>  
18 10 7 10 13

4+50

364<sup>9</sup> 364<sup>7</sup> 364<sup>9</sup> 364<sup>2</sup> 364<sup>8</sup> 365<sup>1</sup> 365<sup>0</sup>  
20 10 7 6 10 20

4+00

364<sup>4</sup> 364<sup>3</sup> 364<sup>1</sup> 364<sup>2</sup> 364<sup>1</sup> 364<sup>0</sup>  
20 10 8 10 15

3+50

363<sup>4</sup> 363<sup>2</sup> 363<sup>6</sup> 363<sup>4</sup> 363<sup>3</sup> 363<sup>3</sup> 363<sup>2</sup>  
20 10 7 6 10 15

3+00

362<sup>8</sup> 362<sup>8</sup> 362<sup>7</sup> 363<sup>0</sup> 363<sup>1</sup> 363<sup>0</sup>  
10 6 8 10 20



Alley Block 35 Cont'd

6+01.41

5+99.41 So. Line Pole

5175

£

62

Same

366<sup>±</sup> 365<sup>?</sup> 365<sup>?</sup> 365<sup>?</sup> 365<sup>?</sup> 366<sup>°</sup> 366<sup>°</sup>  
10 5 4 8 10

366<sup>±</sup> 366<sup>±</sup> 366<sup>±</sup> 366<sup>±</sup> 366<sup>±</sup>  
15 10 8 10



X Sec Curlew Laurel St

0+41 40<sup>4</sup> RT End new garages No floor  
Begin old garages con floor only

0+00 Prop cor to west

0-05<sup>60</sup> E int with paring edge.

0+08<sup>92</sup> 40<sup>4</sup> RT Begin garages new no floors as yet  
N Prophine Laurel to East also cbend

0-22<sup>22</sup> N c6 line Laurel to East

0-48<sup>22</sup> E Laurel

BM

6<sup>33</sup>

152<sup>45</sup>

146<sup>01</sup>

SE BP Laurel  
Curlew

to Canyon Lt. West E Rt. East

64

147.8	147.27	147.0	147.8	148.0	148.1	147.8	148.6	148.83
42	518	55	42	44	43	46	32	302
40	26	26	13	13	26	40	40	40
	26	26						

147.2	147.13	146.8	147.4	147.6	147.8	148.2	148.0
52	532	56	50	42	47	42	44
40	26	26	13	13	26	40	
	26	26					

147.59  
4<sup>26</sup>

146.81	147.16	147.50	147.65	147.74	148.03	148.31
504	529	490	480	472	442	412
26	13	13	26	26	40	40
			26	26	40	40

145.76	146.60	146.83	147.25	147.32	147.45	147.99	147.44	148.03	149.30	149.87
669	585	562	520	513	500	446	501	442	315	257
90	70	26	26	26	36	36	40	40	90	85
					26	26	26	26	26	26

145.69	146.70	146.84	147.08	147.27	147.52	149.24
626	525	561	537	518	483	321
90	40	26	26	40	90	

152<sup>45</sup>

0194 40 1/2 RT E 3 1/2' con steps

0186 E same garages

0177 E same garages

0170 2 1/2 ht Regia Picket Fence

0170 40 1/2 RT E 3 1/2' con steps

0165 E same garages

0156 E same garages

0147 40 1/2 RT E garage con floor

Lt = West

Rt = East

147.8	147.66	147.0	147.6	148.0	148.0	148.0	148.6	148.8165
46	42	54	42	44	45	44	39	34
40	26	26	13	13	24	40	40	40
	46	34						Top bottom step

148.81

364  
40  
Floor

148.82

363  
40  
Floor

147.6	147.44	147.4	147.8	148.0	148.2	148.4	148.8	149.04
48	52	54	46	44	43	44	36	34
40	26	26	13	13	26	40	40	40
	46	34						Top bottom step

148.82

363  
40  
Floor

148.83

362  
40  
Floor

148.83

362  
40  
Floor

152.45

1747 80° sw cor house

1741 26° RT E 9' via power pole = 2533

1726 26° Lt End cb also E int. guard fence

1717 26° Lt E 2' wide con walk

1713 40° RT End garages

1708 E garage

1700 40° RT E garage con floor

TP, 608 153<sup>64</sup> 4<sup>89</sup> 147<sup>56</sup>

Lt = West

RT = East

66

133.64	135.1	135.7	136.9	137.1	144.9	148.8	149.1	149.3
20°	18°	17°	16°	16°	8°	4°	4°	4°
40	26	13		13	26	32	40	80

147.4	147.21	147.1	147.9	148.5	148.7	148.6	149.0	151.7
6°	6°	6°	5°	4°	5°	4°		1°
40	26	26	13	13	26	40	45	
	obscured	set						

147.77	147.59
587	625
40	20
on walk	top of cb

148.79
485
40°
floor

148.78
486
40°

148.82
482
40°
floor

15364

Lt = West

2

Rt = East

67

BM

756

146<sup>08</sup>

146<sup>02</sup>  
Starting  
BM

1/2 Rt Fence & guard rail L. pt.

1467 86° Rt NW cor House

129.7	128.9	127.9	129.0	132.5	137.4	145.2	149.1	149.3
23 <sup>2</sup>	24 <sup>2</sup>	25 <sup>2</sup>	24 <sup>0</sup>	21 <sup>4</sup>	16 <sup>2</sup>	8 <sup>2</sup>	4 <sup>5</sup>	4 <sup>2</sup>
40	26	13	13	26	40	50	80	

153<sup>64</sup>

D. Smith  
 Wm Fay  
 F. Sherman  
 J. Crawford.

Re X sec Alley B/K 253 Univ Hts

0+70 22<sup>5</sup> Lt to cal decorate wall

0+80 25<sup>2</sup> Lt where carport decorate wall comes out from main wall

0+74 26<sup>2</sup> Lt Begin con brick wall

0+65 20<sup>3</sup> Lt & garage con floor & apron

0+54

0+40 10<sup>4</sup> Lt Begin Cold bay

BM 469 240<sup>18</sup> 236<sup>4</sup> on disk 31 W of Myrtle & Alley P. 24.

At North Rt. East WO 21001  
 10-9-50 68

232<sup>15</sup> 235<sup>19</sup>  
 373 479  
 225 225  
 Top 204 234 25  
 234 235 19 233 58 226 98 228 18  
 409 424 5 506 6 3 11 2 14 2  
 26 20 8 3 cold bay 10 20  
 237 81  
 237 26 Top wall  
 236 58 230 22  
 366 476  
 295 302 Floor apron  
 235 87 234 21 234 49 231 28 220 68 226 14  
 481 547 562 8 2 145 1394 150 224 15  
 27 167 4 cold bay 115 115 Top wall 125  
 233 84 233 91 228 68  
 36 6 27 115 161 1580 204 38 18 21 58  
 21 10 cold bay 115 155 Top wall 125

240<sup>18</sup>

1775

1750

1720 End cold lay

1718 26° Lt end decorative wal

1710 20° Lt Begin con block wall

1709 22.5° Lt Begin decorative wall for entrance car port

1700 approx E car port

LT

232 48	236 7	236 0	235 6	235 3	236 0	235 9	231 9
22	35	42	46	49	42	43	83
23	16	14	3	6	10	20	

237 2	237 2	235 6	235 4	236 1	236 5	235 0	229 0
30	30	46	48	41	36	52	112
26	17	14		2	7	10	20

236 0	235 2	235 22	235 31	235 21	229 3	226 3
418	440	426	480	51	102	132
24	20	10	1		10	20

cold lay

238 61

138

26  
top wall

237 03	235 60
315	458
225	225

Top wall cold lay

235 26	235 21	235 15	235 24	235 3	230 4	230 84	225 4
422	494	503	499	49	48	93	148
35	20	10	1		1	10	20

cold lay

240 18



Lt

E

Tr

70

BM starting

407 236 ✓

2124 235 1/2 end west & east wall

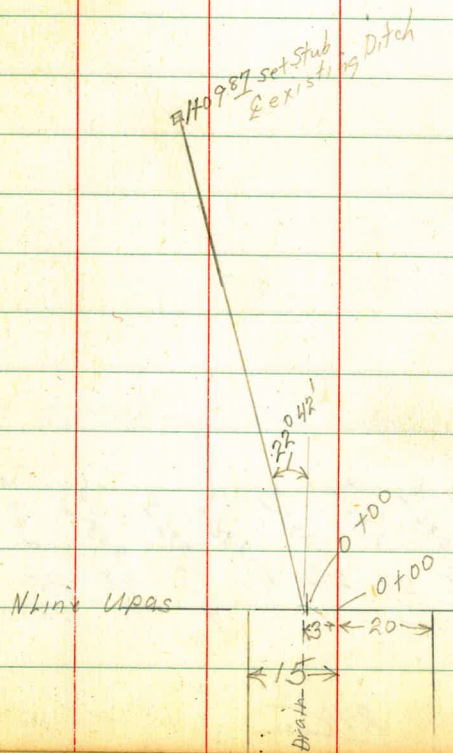
100  
235  
140

2400

	237 1/2	236 7/8	236 1/2	236 1/4	235 1/2	235 1/4	235 1/8	235 1/16	229 1/2
28	33	36	40	43	44	37	48	106	
26	20	16	14		5	9	10	20	

240 18

Drain Alley BIK 253 Univ. Hts



Lt = East

Drain Line

Rt = West

71

H09<sup>87</sup> Ditch

188 <sup>0</sup>	188 <sup>0</sup>	188 <sup>0</sup>	188 <sup>0</sup>	187 <sup>2</sup>	188 <sup>1</sup>
11 <sup>2</sup>	11 <sup>4</sup>	11 <sup>33</sup>	11 <sup>4</sup>	11 <sup>2</sup>	11 <sup>3</sup>
20	10	546	ground	10	20

0+97 Torban K

186 <sup>0</sup>	186 <sup>0</sup>	186 <sup>0</sup>	186 <sup>0</sup>	195 <sup>0</sup>
11 <sup>4</sup>	10 <sup>2</sup>	10 <sup>2</sup>	10 <sup>6</sup>	4 <sup>4</sup>
20	10	5	15	

TP

0<sup>45</sup> 199<sup>39</sup> 11<sup>87</sup> 198<sup>94</sup>

0+75

199 <sup>0</sup>	201 <sup>1</sup>	201 <sup>1</sup>	202 <sup>7</sup>	201 <sup>3</sup>
11 <sup>8</sup>	10 <sup>2</sup>	9 <sup>2</sup>	8 <sup>1</sup>	6 <sup>5</sup>
20	10	10	20	

0+43

201 <sup>2</sup>	203 <sup>1</sup>	205 <sup>2</sup>	207 <sup>1</sup>	208 <sup>7</sup>
9 <sup>6</sup>	7 <sup>2</sup>	5 <sup>6</sup>	3 <sup>8</sup>	1 <sup>9</sup>
20	10	10	20	

TP

0<sup>50</sup> 210<sup>81</sup> 11<sup>82</sup> 210<sup>31</sup>

0+35

205 <sup>13</sup>	205 <sup>03</sup>	211 <sup>1</sup>	213 <sup>9</sup>	216 <sup>5</sup>
17 <sup>2</sup>	14 <sup>4</sup>	11 <sup>0</sup>	8 <sup>2</sup>	5 <sup>6</sup>
20	10	10	20	

0+00

26  
219<sup>53</sup>

BM.

6<sup>09</sup>

222<sup>43</sup>

216<sup>14</sup>

Top 34 1010  
1030 East

Additional to P. 45 2 May '51  
Catalina to Canyon 20690

Sommermeier  
Bogg  
R. Sisson  
Telpooqoff

3+50

INDEXED  
MAY 1951

3+00

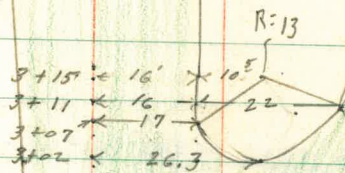
2+50

2+00

0+00 =  $\pm$  B.C. = Sta. at end Page 45

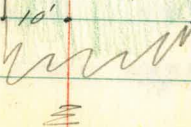
12

15' 16' ← 36' → 20'



A.C. Pavc.

10' 415'



3+50

<u>248.45</u>	<u>248.35</u>	<u>248.20</u>	<u>247.91</u>	<u>247.57</u>	<u>247.21</u>
15'		16	52	62	72
E.P.		E.P.	E.P.		E.P.

3+11 38' Rt. = E.C. pave. see sketch.

<u>247.97</u>	<u>247.70</u>
16	38
E.P.	E.P.

3+07 - 17 Rt. = E.C. pave.

<u>248.02</u>
17
E.P.

3+02 26<sup>3</sup> Rt. = Nose of curve  
see sketch

<u>248.02</u>
26 <sup>3</sup>
End pave

3+00

<u>248.04</u>	<u>248.17</u>	<u>248.07</u>	<u>247.72</u>	<u>247.33</u>	<u>246.74</u>
10		17	36	47	58
					E.P.

2+50

Base line =  $\pm$  Catalina.

<u>248.01</u>	<u>247.96</u>	<u>247.75</u>	<u>247.23</u>	<u>246.76</u>
10		25	35	45
E.P.				E.P.

2+00 E.P. = edge of pave

<u>248.06</u>	<u>248.13</u>	<u>247.87</u>	<u>247.48</u>	<u>247.00</u>
10		10	20	295
E.P.				E.P.

Clark  
Shepherd  
8/1/54  
D.W.B.  
5-18-54  
11/0.3/1982

ALLEY BLK 253 - UNIVERSITY HTS  
UPAS to MYRTLE

Ref: (See sketch pg. 17 - SAME S. USED FOR SECTIONS)  
NOTE: NO DATA GIVEN ON OPENINGS

O+40 9.8 LT = CRT IN wood Ret. wall  
20 LT = 4 LT IN CONC. WALL

O+39.5 9.2 LT = END 8" DRAIN PIPE

O+38 6.5 LT = 1 PT LT. IN 8" PIPE

O+21 9.8 LT Bay Wood Ret. wall (SUPPORTS BUILT UP PORTION OF ALLEY USED FOR PARK CAR GARAGE)

T.P. 10.92 234.90 0.35 223.98

O+00 20 LT Bay Conc. Ret. wall - 6" wide 1/2" wire fence along edge wall  
11.7 RT Bay Conc. Ret. wall 10" wide - 6" steel wire fence set to wall

O-15

O-25

(SECTION S. BY SAME AS PREVIOUS)  
(See pg. 20 etc)

T.P. 0.35 224.33 12.91 223.98

B.M. 0.78 236.89

236-11 = CITY DISC E WIL SHIRE PL  
3' (B) N. LINE MYRTLE

LT.

E

RT.

74

INDEXED  
SER

MAY 60

234.6  
234.20  
234.0  
233.8  
234.53  
228.9  
226.0  
223.9  
224.26  
221.20  
220.6

0.3	0.64	0.7	1.07	0.37	6.0	8.7	11.0	10.64	13.7	14.3
25	20	20	28	9.5		7	10	11.7	2.3	20
	TP	CLAY	CLAY	TP				10.4	9.1	
	WALL		WALL	WALL				WALL	WALL	

233.77  
233.46  
1.13  
98  
9.2  
CLAY  
FL  
PIPE

233.60  
233.5  
233.75  
233.6  
230.7  
224.1  
224.1  
223.0  
220.2  
220.26  
219.10  
215.30

1.30	1.4	1.3	4.2	2.0	10.8	11.9	14.7	14.64	15.8	18.6
20	20	9.6	9.8	9.8	9.2	4.4	6	10	11.7	12.3
TP	CLAY	TP	CLAY	TP	FL	E			TP	WALL
WALL		WALL		WALL				WALL	WALL	

234.67  
230.0  
233.25  
231.6  
227.3  
221.1  
216.7  
216.67  
214.6  
214.3  
210.5  
199.7

110.3	5.7	4.87	4.53	4.3.0	3.2	7.6	7.66	10.0	13.8	24.6
40	20	20	20	10		10	11.7	15	25	50
	TP	TP	TP	TP			TP	TP	TP	WALL
	WALL	WALL	WALL				WALL	WALL	WALL	

232.6  
226.3  
219.3  
214.3  
208.0  
199.1

4.3	7.2.0	5.0	10.0	16.3	25.2
40	10	50	100	25	50

220.8  
218.6  
216.2  
213.5  
211.4  
199.7

3.5	5.7	8.1	10.8	12.9	24.6
40	10		10	15	50
					CRK

224.33



ALLEY 253 (CONT)

1+23 { 3.2 RT E 2x5' CONC. STAIRWAY } Steps 11" deep  
 15.7 RT to 4.3 x 2.1 CON. LANDING at Bottom of series steps  
 and landing same dimensions adjacent to 1st  
 END of WALK 15.6 RT AGAINST SLY Edge of Landing's  
 on approx. same level as 2nd landing.

1+135 19.9 LT L. in 8" CBG

25.9 LT to FC. Beg CONC. BRK WALL 8" wide

1+12 26.6 LT END GAR

1+095 { 22.7 LT Beg Rocker Car Wall around shrubs  
 22.4 LT L. 1 1/8" CON. CBG }  
 26.6 LT Beg 8" wide CON. CBG  
 Extends Ely from gar  
 toward ally (see sketch)

1+03.5 { 15.6 RT Beg 4" CONC. WALL  
 11.6 RT 6" CONC. RET. WALL }  
 1+00

0+91 14.5 RT E 3" Tree

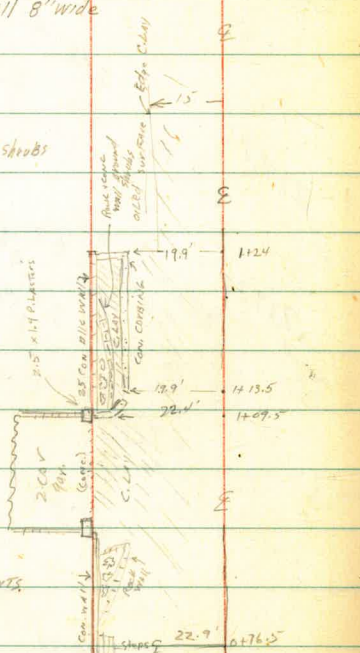
0+90 22.6 LT 1 1/4" Rocker Car Wall around plants

0+88 25.9 RT END CONC. BRK WALL 4.26 LT Beg CONC. BRK - 2 Car gar  
 (wall 4 gar meet) (open side Ely)

0+77.5 25.6 LT Beg CONC. BRK WALL around Red-shrubs etc. Average 8" high

19.9 RT Beg 4" steel wire Fence

0+77 15.2 RT to FC. Beg 6" CONC. RET. WALL  
 13.0 RT E 4" Tree



LT.

E

RT.

235.53  
 227.68  
 227.26'6

5.06  
 3.2  
 TP  
 Step

12.91  
 15.7  
 on 1st  
 landing  
 w/ledge

13.33  
 17.8  
 on  
 2nd  
 landing  
 w/ledge

236.32  
 235.66

4.27  
 1.79  
 TP  
 CBG

235.93  
 238.14  
 238.54  
 235.24

26.6  
 26.6  
 25.9  
 25.5

26.6  
 26.6  
 25.9  
 25.5

FL  
 BK  
 WALL

236.84  
 235.83

235.79  
 236.36

4.23  
 26.6  
 26.6  
 26.6

4.80  
 22.4  
 22.4  
 22.4

CLAY  
 TP  
 W/ledge  
 CON. CBG  
 IN GAR

235.97  
 235.57  
 235.14  
 235.19  
 235.19

1.62  
 26.6  
 FL GAR

5.02  
 20

5.45  
 10

5.40  
 5.44  
 5.5

1.15  
 Ely edge  
 CLAY

235.18  
 235.18  
 235.18  
 235.18

14.24  
 12.44  
 13.6  
 15.1

22.7  
 22.7  
 22.7

14.3  
 18.9  
 23.8

15.6  
 36  
 36  
 50

226.35  
 228.18

235.85  
 235.80

4.74  
 4.74  
 26.6  
 26.6

ON CON  
 CLAY  
 FL

228.04  
 225.64  
 225.69

12.55  
 15.2  
 TP  
 WALL

14.96  
 15.7  
 RT  
 GAR

14.9  
 15.7  
 BK  
 WALL

240.59





3+00

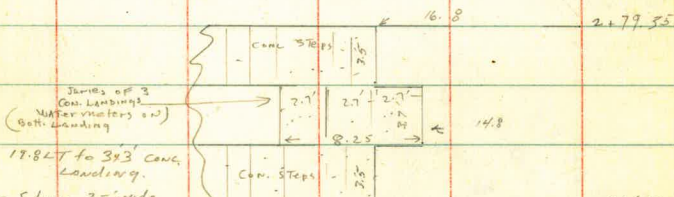
18' RT & 5" Leymon Tree

2+84

11' RT & 3" Pepper Tree

2+79.35 = NLY Line Conc. Steps

2+73.95 14.8 LT = ♀ Conc. 6 1/2' as:



2+68.6 = S. Line 7.5' wide  
Conc. Steps 16.8 LT

Note: See p. 23 - indicates steps once installed to apt. 14.8 Frame  
(Probing indicated steps are buried under present alkyl surface.)

2+50

2+25 11 RT to NLY END 5' Board Fence

2+24 23.5 LT. ELY END OF E-WEST CONC. BRK WALL

2+23 16.6 LT & Pole # PA 3467

2+19 26.6 LT END 3-CAR GAR.

LT

♀

RT

78

245.2 245.0 237.3 236.84 236.80 236.27 236.03 236.4 234.1 231.1 227.9 226.60 222.8

13.9 40 4.4 15 4.42 5.03 5.27 4.9 7.2 10.2 13.4 14.7 18.5

33 20 15 10 CL 2.5 7 10 15 21 43 55

Shoulder TP approx master c/c E side of fire

236.43 238.37 236.97 236.85

2.87 2.93 4.38 4.45

22.8 19.8 16.8 16.8

Bx landing TP step 9rd (cont)

238.31 237.75 237.36 236.70

2.77 3.55 3.94 4.60

20.2 17.5 14.8 14.8

3rd 2nd 1st 9rd (cont)

Landings landing

238.41 238.32 236.85 236.74

2.87 2.98 4.45 7.56

22.8 19.8 16.8 16.8

Bx landing on landing step 9rd (cont)

244.2 244.2 236.9 236.47 236.36 235.95 235.83 236.5 234.73 227.3 225.50 222.4

42.9 42.9 4.4 4.83 4.94 5.35 5.47 4.8 6.6 10.2 14.0 15.8 18.9

40 37 22 15 10 c.c. 2.5 7 10 15 25 43 50

1st surface c.c. c.c. 2.5 7 10 15 25 43 50

Approx. E side of fire

237.51

3.79 26.6 Fl.

241.30

4194.13 5.22 = 236.88 = 236.11 (see 13.11)

4194.13 Sect. 100' Nly to show grade  
EXIST. TAPS on Wbshire Pl.

3194.13 = N. LINE MYRTLE - SLY END EXIST. TAPS - (30.3' RT CA'S) - CON. PAV.; 5' CONC. WALKWAY TO CBS

3187.5 12.9' RT to sly end of CRB INLET. (15.5 RT to CRB SLY END INLET.)  
(24" Cast Iron pipe at 90° Ely extends 46' RT) } 4.5" x 2.6" Flush with Pav. at NLY END INLET

3164.13 S. MYRTLE

3163 0.22 RT & M.H.

3161.5 16.0 RT E 16" Pepper Tree

3140 13.8 LT & Rb #P - 1949

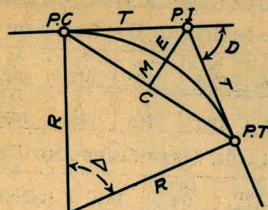
3134.13 = S. LINE MYRTLE

238.22  
237.70  
237.69  
236.73  
237.31  
3.08 3.60 3.61 4.57 3.99  
14.8 14.8  
TO C  
CA  
15.5 15.5  
TO C  
CA  
245.11  
244.3  
236.74  
236.6  
236.02  
236.2  
236.0  
235.9  
234.95  
235.64  
235.67  
235.1  
234.8  
219.5  
13.8 +3.0 4.56 4.89 5.28 5.1 5.30 5.4 6.35 5.66 5.63 6.1 6.5 21.8  
50 30 17.8 14.8 14.8 14.8  
TO C TO C TO C TO C TO C TO C TO C TO C TO C TO C  
17.8 14.8 14.8 14.8  
TO C TO C TO C TO C  
5.34  
0.2  
Rim  
M.H.  
247.1  
240.6  
236.5  
236.14  
235.96  
235.12  
234.89  
235.54  
232.10  
220.66  
6.12 6.41 5.76 9.20 20.64  
13.9 15.5 15.5  
90° TR CA  
FL. LINE  
CA. INLET  
9.6  
9.6  
FL  
PIPE  
5.71 5.7 5.3 11.9 17.9  
5 7 10 38 50  
5  
E. Edge  
C.L.  
241.30

245.8  
246.2  
237.13  
236.2  
95.40  
236.2  
236.0  
235.30  
235.30  
228.0  
227.2  
224.1  
4.5 4.9 4.17 4.25 4.70 5.22 5.0 6.0 9.8 13.3 14.1 14.2  
40 27 13 10 C.L. 4 7 10 15 22 41 50  
upper  
to edge  
C.L.  
to  
241.30

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

Radius  $= R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve  $= D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent  $= T = R \tan \frac{\Delta}{2}$  (3) Length of Curve  $= L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate  $= M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$  (6)

External  $= E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)

Long Chord  $= C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I.  $- T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C.  $+ L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 — Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$  and from Table V correction = .10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

TABLE VI.—CORRECTIONS FOR SUB-CHORDS AND LONG CHORDS.

FOR SUB-CHORDS ADD										Excess of arc per 100 ft.	LONG CHORDS				
D	10	20	30	40	50	60	70	80	90		D	200	300	400	500
4°	.00	.00	.01	.01	.01	.01	.01	.01	.00	.02	1	199.99	299.97	399.92	499.85
6	.00	.01	.01	.02	.02	.02	.02	.01	.01	.05	2	199.97	299.88	399.70	499.39
8	.01	.02	.02	.03	.03	.03	.03	.02	.01	.08	3	199.93	299.73	399.32	498.63
10	.01	.02	.03	.04	.05	.05	.05	.04	.02	.13	4	199.88	299.51	398.78	497.57
12	.02	.04	.05	.06	.07	.07	.07	.05	.03	.18	5	199.81	299.24	398.10	496.20
14	.02	.05	.07	.08	.09	.10	.09	.07	.04	.25	6	199.73	298.90	397.26	494.53
16	.03	.06	.09	.11	.12	.12	.12	.09	.05	.33	7	199.63	298.51	396.28	492.57
18	.04	.08	.11	.14	.15	.16	.15	.12	.07	.41	8	199.51	298.05	395.14	490.31
20	.05	.10	.14	.17	.19	.20	.18	.15	.09	.51	9	199.38	297.54	393.86	487.75
22	.06	.12	.17	.21	.23	.24	.22	.18	.10	.62	10	199.24	296.96	392.42	484.90
24	.07	.14	.20	.25	.28	.28	.26	.21	.12	.74	12	198.90	295.63	389.12	478.34
26	.09	.17	.24	.29	.32	.33	.31	.25	.15	.86	14	198.51	294.06	385.22	470.65
28	.10	.19	.27	.34	.37	.38	.36	.29	.17	1.00	16	198.05	292.25	380.76	461.86
30	.11	.21	.31	.39	.43	.44	.41	.33	.19	1.15	18	197.54	290.21	375.74	452.02
32	.13	.25	.36	.44	.49	.50	.47	.38	.22	1.31	20	196.90	287.94	370.17	441.15
34	.15	.28	.40	.50	.55	.57	.53	.43	.25	1.48	22	196.32	285.44	364.06	429.30
36	.17	.32	.45	.56	.62	.64	.59	.48	.28	1.66	24	195.63	282.71	357.43	416.53
38	.18	.36	.51	.62	.70	.71	.66	.53	.31	1.86	26	194.87	279.76	350.30	402.89
40	.21	.40	.56	.69	.77	.79	.73	.59	.35	2.06	28	194.06	276.59	342.69	388.42
42	.23	.44	.62	.76	.85	.87	.81	.65	.38	2.28	30	193.18	273.20	334.61	373.20
44	.25	.48	.68	.84	.94	.96	.89	.72	.42	2.50	32	192.25	269.61	326.08	357.28
46	.27	.52	.75	.92	1.02	1.05	.98	.78	.46	2.74	34	191.26	265.81	317.12	340.73
48	.30	.57	.81	1.00	1.12	1.14	1.06	.86	.50	2.99	36	190.21	261.80	307.77	323.61
50	.32	.62	.89	1.09	1.21	1.24	1.15	.93	.55	3.24	38	189.10	257.60	298.03	305.99
52	.35	.67	.96	1.18	1.31	1.35	1.25	1.01	.59	3.52	40	187.94	253.21	287.94	287.94
54	.38	.73	1.04	1.28	1.42	1.46	1.35	1.09	.64	3.80	42	186.72	248.63	277.51	269.54
56	.41	.78	1.12	1.38	1.53	1.57	1.46	1.17	.69	4.09	44	185.44	243.87	266.78	250.85
58	.44	.84	1.20	1.48	1.65	1.69	1.57	1.20	.74	4.40	46	184.10	239.93	255.78	231.95
60	.47	.91	1.29	1.59	1.76	1.81	1.68	1.35	.80	4.72	48	182.71	233.83	244.51	212.92

NOTE.—When a chord of less than 100 ft. is used the corrections given in the above table should be added to the nominal length of chord to get the length which should be used in order that the 100 ft. points will check with those obtained by using the standard 100 ft. chord. Thus in locating a 14° curve by 25 ft. chords measure 25' 08" for each chord. Long chords are useful in passing obstacles.

TABLE VII.—MIDDLE ORDINATES FOR RAILS IN FEET.

Deg. of Curve	LENGTH OF RAILS							Deg. of Curve	LENGTH OF RAILS						
	32	30	28	26	24	22	20		32	30	28	26	24	22	20
1°	.022	.020	.016	.013	.011	.009	.008	16°	.356	.313	.273	.236	.200	.170	.139
2	.045	.038	.034	.029	.025	.021	.017	17	.378	.333	.290	.252	.213	.180	.148
3	.067	.058	.051	.044	.037	.031	.026	18	.400	.351	.306	.265	.225	.190	.156
4	.089	.079	.069	.060	.050	.042	.035	19	.423	.371	.324	.280	.238	.201	.165
5	.112	.099	.086	.074	.063	.053	.044	20	.445	.392	.341	.296	.250	.212	.174
6	.134	.117	.102	.088	.076	.064	.052	21	.466	.410	.357	.309	.262	.222	.182
7	.156	.137	.120	.104	.088	.074	.061	22	.487	.430	.375	.325	.275	.233	.191
8	.179	.158	.137	.119	.100	.085	.070	23	.509	.450	.390	.338	.287	.243	.199
9	.201	.175	.153	.133	.112	.095	.078	24	.531	.469	.408	.354	.299	.253	.208
10	.223	.196	.171	.148	.125	.106	.087	25	.552	.486	.424	.367	.311	.263	.216
11	.245	.216	.188	.163	.139	.117	.096	26	.573	.506	.441	.382	.323	.274	.225
12	.268	.236	.206	.179	.151	.128	.105	27	.594	.524	.457	.396	.335	.284	.233
13	.290	.254	.222	.192	.163	.138	.113	28	.618	.545	.475	.411	.348	.294	.242
14	.312	.275	.239	.207	.175	.148	.122	29	.638	.564	.491	.424	.361	.303	.250
15	.334	.295	.257	.223	.188	.159	.131	30	.660	.583	.508	.438	.374	.313	.259

SLOPE REDUCTIONS.

When distances are measured on a slope that may be reduced to the equivalent horizontal distance by the following approximate rule:—subtract from the slope distance the square of the rise divided by twice the slope distance. Thus for a slope distance of 250.3 ft. and a rise of 15 ft. correction=15<sup>2</sup>÷2×250.3=.45 (by slide rule) or horizontal distance=250.3—.45=249.85. When vertical angle=V. A. is measured horizontal distance=slope distance—slope distance (1—Cos. V. A.). Thus for slope distance of 248.7 ft. and V. A. of 4° 20' from Table VIII Cos=.99714 and correction=1—.99714=.00286 per foot or total of .286×2½ (near enough)=.57 and horizontal distance=248.7—.57=248.13 ft.

See fig. (a). TRIGONOMETRICAL FORMULAS.

sin.  $A = \frac{a}{c}$   
 cos.  $A = \frac{b}{c}$   
 tan.  $A = \frac{a}{b}$   
 cot.  $A = \frac{b}{a}$   
 sec.  $A = \frac{c}{b}$   
 cosec.  $A = \frac{c}{a}$

FORMULA FOR SOLVING TRIANGLES.

Given Sought. Right triangles. See fig. (a).  
 a, c A, B, b sin.  $A = \frac{a}{c}$ , cos.  $B = \frac{a}{c}$ ,  $b = \sqrt{(c+a)(c-a)}$   
 a, b A, B, c tan.  $A = \frac{a}{b}$ , cot.  $B = \frac{a}{b}$ ,  $c = \sqrt{a^2 + b^2}$   
 A, a B, b, c  $B = 90^\circ - A$ ,  $b = a \cot. A$ ,  $c = \frac{a}{\sin. A}$   
 A, b B, a, c  $B = 90^\circ - A$ ,  $a = b \tan. A$ ,  $c = \frac{b}{\cos. A}$   
 A, c B, a, b  $B = 90^\circ - A$ ,  $a = c \sin. A$ ,  $b = c \cos. A$   
 Given Sought. Oblique triangles. See fig. (b).  
 A, B, a b  $b = \frac{a \sin. B}{\sin. A}$   
 A, a, b B sin.  $B = \frac{b \sin. A}{a}$   
 a, b, C A - B tan.  $\frac{1}{2}(A - B) = \frac{a - b \tan. \frac{1}{2}(A + B)}{a + b}$   
 c, b, c A  $\left\{ \begin{array}{l} \text{If } s = \frac{1}{2}(a + b + c), \text{ sin. } \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{bc}} \\ \text{cos. } \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}, \text{ tan. } \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} \\ \text{sin. } A = \frac{2 \sqrt{(s-a)(s-b)(s-c)s}}{bc} \end{array} \right.$   
 A, B, C, a area area =  $\frac{a^2 \sin. B \sin. C}{2 \sin. A}$   
 A, b, c area area =  $\frac{1}{2} b c \sin. A$   
 a, b, c area  $s = \frac{1}{2}(a + b + c)$ , area =  $\sqrt{s(s-a)(s-b)(s-c)}$

11 11

22° 42' 44"

2 37 48  
 3 43  
 346 88  
 3 50

4 35 34 50

48.2  
 46.6  
 71.6

242.6

242.4

254.35

14  
 840.2

583

46 30  
 16 30

DISTANCES FROM CENTER OF ROADWAY FOR  
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.