



EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.
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1832

CITY ENGINEER'S OFFICE

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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

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Willow St. Oliphant to Newell 10-14

Cross Sec. Alley in Point Loma Center 15-22

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Cross section

Newell St.

Evergreen to Wabaska Dr.

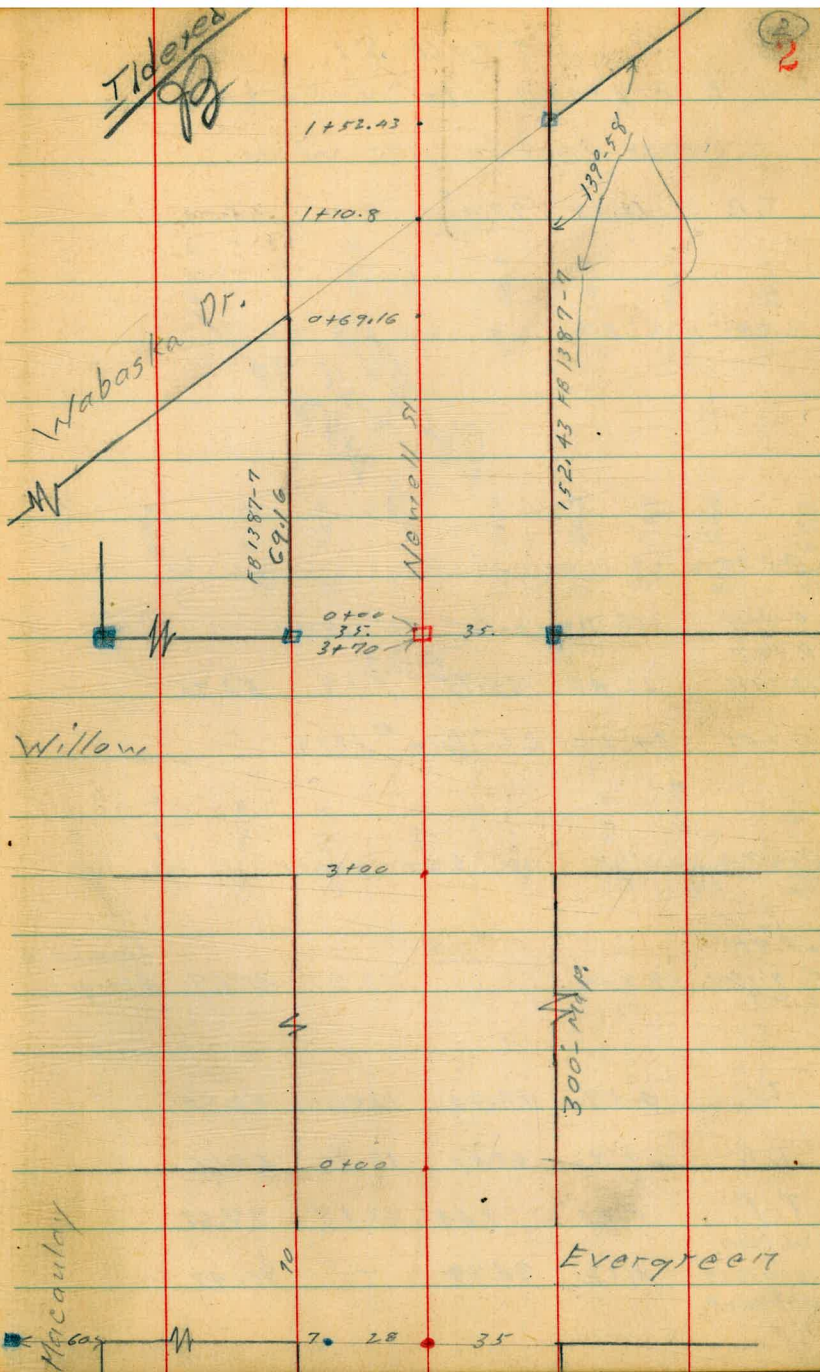
12-31-47

V.G. 25001

Sammerneyer

W. Moore

E. Sherman



Newell St.

Evergreen to Wabaska

Cross Section 70' Wide.

T.P. 12.38 77.42 0.11 65.04

0+60

0+30

0+17 25° Rt. = pole # 415519H

T.P. Pole # 415519H 12.40 65.15 0.19 52.75

0+01 34' Lt. = Ctr. Pole # 1798

0+00 = Wly. line Evergreen.

Set B.M. Newell +
S.E. 7' + Prop. - Evergreen 12.27 40.67 Evergreen
L. + T.

T.P. 0.39 52.94 13.02 52.55

T.P. 0.92 65.57 12.99 64.65

T.P. 0.03 77.64 13.18 77.61

N.W. Mon.
Evergreen + elephant 0.32 90.79 - 90.47

PHOTED
1-8-48
J. M. [unclear]

4

33
3

55.5
9.6
35
59.2
5.9
14
58.3
6.8
11
59.1
6.0
4.7
27
60.4
0.9
35
64.7
72.1
72.1
74.7
74.7
+9.6
50

45.1
20.0
60
49.1
16.0
35
52.8
12.3
76
52.0
13.1
12
52.1
13.0
52.0
13.1
9
54.3
10.8
31
56.8
8.3
35
65.6
40.5
40
69.1
4.0
60

65.15

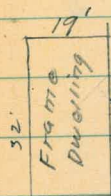
408
12.1
60
43.4
9.5
35
45.4
12.5
31
47.3
5.6
14
47.3
5.6
47.1
17
49.9
3.0
35
62.3
9.4
43
62.6
9.7
60

52.94

Newell St.

Newell.

35 Rt. = Int. S. edge walk + N line



54' → 17.45

1233 ← 40.7

1+305 ← 33.2

1+26 ← 30.8

1+18 ← 29.1

1+13 ← 24.7

1+00 ← 24.8 34.7

4' wide Flag stone + conc. steps

37.5 Rt. off

Conc. Topping on steps

3.2

3.2

Stucco

3.5

Bar. 13.5

1+00 34.7 Rt = start stucco Sing Bar.

0+75

77.42

52.1	62.6	67.7	67.9	71.6	72.9	79.8
20.3 60	14.8 35	9.7 13	9.5	5.8 14	4.5 35	+2.0 50
55.0	62.4 72.4?	61.8	62.6	62.9	73.6	74.0
22.4 35	15.0 16	15.6 10	14.8 77.42	14.6 5	3.8 35	3.9 50

Also 25² Rt. = Pole # 415518 H
 J.P. 3250 +
 4' wide Flag + conc. walk
 1+33 35' Rt. = Edge steps. 40.7 Rt. = Φ

83.2
 +5.8
 35
 83.7
 +6.3
 40.7

1+30^E 37^E Rt. = End Conc. slope cover

83.1
 +5.7
 37.5

Conc. slope covering
 1+26 32³ Rt. = Φ steps 33² Rt. = Start

80.2
 +2.8
 32.3
 80.2
 +2.8
 33.9
 83.0
 +5.6
 37.5
 Back of Conc.

35.5 Rt. = Δ in Ret. wall
 1+18 30^E Rt. = Φ steps. 32' Rt. = ^{END} Conc. Ret wall

75.7
 1.7
 30.5
 2.905
 72.7
 4.7
 32
 Base
 wall
 76.5
 0.9
 3.2
 Top
 wall
 81.0
 +3.6
 35
 Top wall

Conc. topping on slope
 34.9 Rt. = End Gar. Bldg. 38' Rt. = End of
 1+14 35^E Rt. = start 6" wide Ret. wall

72.63
 4.77
 24.9
 72.80
 1.62
 30.15
 73.00
 4.42
 34.9

30.5 Rt. = Φ 3' wide walk 34.9 Rt. = Gar. Floor
 1+13 24.9 Rt. = Edge apron

72.10
 5.72
 24.18
 73.03
 4.39
 34.7

34² Rt. = Gar. Floor
 1+01 24⁸ Rt. = Edge apron

77.42

77.42

Newell

T.P. 0.20 65.72 13,28 65.52

3+00 - Ely line Willow

50% Temp B.M

Nail in pole # 301352H 3.08 75.72

set. B.M.

2+80 27^c Lt. = Pole # 301352H

2+45

1+80

T.P. 3.55 78.80 2.17 75.251+48 25^z Lt. = Pole # 3251

1+45 54' Lt. = Frame dwelling

77.42

42.6	51.3	63.8	65.9	71.6	74.5
<u>362</u>	<u>27.5</u>	15.0	<u>12.9</u>	<u>7.2</u>	<u>4.3</u>
60	35		10	20	35

45.8	52.7	63.8	71.6	71.6	75.4
<u>390</u>	<u>26.1</u>	15.0	<u>7.2</u>	<u>7.2</u>	<u>3.4</u>
60	35		13	24	28

50.7	58.5	63.7	73.2	73.6	76.0	77.2	81.6	88.8
<u>18.1</u>	<u>20.3</u>	<u>15.1</u>	5.6	<u>5.2</u>	<u>2.8</u>	1.6	<u>+2.8</u>	<u>+10.0</u>
60	35	18		14	15	31	35	60

58.4	64.8	68.6	74.9	75.3	76.3	75.5	84.8	88.0
<u>20.4</u>	<u>1.2</u>	<u>10.2</u>	<u>3.9</u>	<u>3.5</u>	<u>2.5</u>	<u>0.3</u>	<u>+6.0</u>	<u>+9.2</u>
60	35	22	10		20	27	35	50

61.6	61.3	65.9	73.2	73.7	74.3	76.2	81.0	84.0
<u>15.8</u>	<u>15.9</u>	<u>14.5</u>	<u>4.2</u>	<u>3.7</u>	<u>3.1</u>	<u>1.2</u>	<u>+3.6</u>	<u>+6.6</u>
54	53	35	11		17	23	28	35

77.42

A

60

T.P.

0+69¹⁶ Cont 47' Lt. = Edge Wabaska

Dr. Pauling

0+69¹⁶ (see page 2)

0+35 35' Lt + 50' Lt are in wash

T.P. 0.60 53.60 12.72 53.00

also = 0+00 ahead.

3+70 = W'y. Live Willow

3+35 = ~~4~~ Willow

3+14

65.72

41.2
12.4
47
11.7
40

38.4
15.2
35
31.6
22.0
23
33.4
20.2
12
38.3
15.3
4
38.8
14.8

31.6
22.0
50
31.6
22.0
25
37.1
16.5
47
41.6
12.0
51.0
2.6
35

53.00

39.5
26.2
35

47.5
18.2

52.5
7.2
35
on d.

54.15
7.57
35
on Mon.

44.2
21.5
35

52.8
10.9

64.5
12
35

49.9
15.8
35

60.3
5.4

65.7
0.0
19

73.0
47.3
35

65.72

1+38 7' Rt. = Edge Pav
35' Rt. = Bottom of Wash.

1+30 = Edge Wabaska Pav.

1+21 7' Lt. = Edge Wabaska paving

1+10⁸ (See page 2)

0+95

0+79 46' Lt. = Edge Wabaska Pav

53.60

42.9
10.7
par
7
par
43.0
43.5
38.3
33.0
14.3
57

42.7
10.9

11.1
7
42.5
43.2
10.4
11.5
6
42.1
32.4
21.2
19
38.9
35
34.7
14.6
41
9.0
60
44.6

41.9
11.7
35
07 par
42.1
11.5
18
Edge
Pav
42.7
10.9
11
38.5
15.1
14
32.9
39.4
19.2
31
39.9
35
43.0
10.6
50

41.7
11.9
35
07 par
41.7
11.9
32
Edge
Pav
42.2
11.4
25
34.4
17.2
11
37.8
21.8
31.8
12.4
20
42.2
11.5
35
42.1

41.3
12.3
46
par
41.9
11.9
38
40.4
13.2
35
31.0
22.6
18
38.0
15.6
45.4
8.2
35
50.5
3.1
60

53.60

Newell St.

4

99

N.W. Cor. Newell
Elephant

2.08 58.15

T.P. 7.23 60.23 ✓ 0160 53.00

1+52⁴³ Cont.

40.8
12.8
29

44.6
9.0
85

N. Ely. line Wabaska.

1+52⁴³ 35' Rt. = Int. My line Newell 4

53.60

43.1
10.5
PAV

43.4
10.2
20.3
24.90
PAV

43.7
9.7
28

39.9
13.7
35

20.5
52

53.60

Willow St.

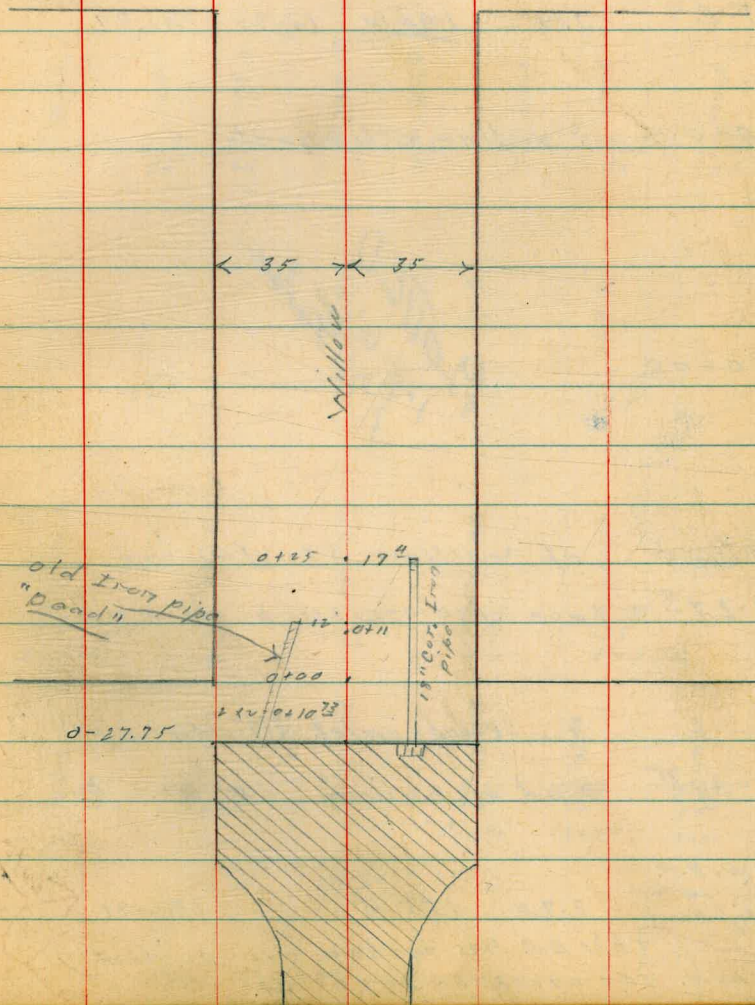
Oliphant to Newell

1-2-48
W.O. 25001

Sommermeier
VJ Moore
E Sherman

~~Indexed~~
[Signature]

10



Willow

EL

±

WL

130.8

121.5

11

17.3
35

22.6
60

0+15 Cont

0+15

145.1
+ 1.0
60

146.4
+ 2.3
35

135.1
9.0
13

135.2
8.9
12
144.10

137.2
6.9
12

130.8
13.3
17

132.3
11.8
17.5

132.4
11.7
24

INVERT
PIPE

T.P. 133 144.10 12.98 142.77

0+00 = Sly. line ofiphant

145.2
10.5
50

148.0
7.7
35

149.4
6.3
23

144.7
11.0
8

147.6
8.1
8

144.1
11.6
31

136.3
19.4
35

138.5
17.2
45

0-08

PROTIED
18'-4" x 8"
7.0 m x 2.0 m

148.7
7.0
35

150.95
4.8
25

150.6
5.1
25

148.35
7.4
35

of Willow St. Paving

0-27⁹ = Face of cross curb at end

151.65
4.10
35
End of

151.50
4.15
17
06.

151.21
4.54
06

151.06
4.69
17
06

150.71
5.04
35
END of

curb inlet (18" outlet pipe)

0-27⁷⁵ = End of paving 19' Rt. =

150.87
4.88
35
par

150.73
5.02
17
par

150.69
5.06
17
par

150.02
5.73
17
Grate

147.99
7.76
17
INVERT

150.30
5.05
35
par

N.W. B.P.
Willow &
otiphant

2.94

155.75

152.81

NOTE
↓

This B.P. Has sunken & is evidently
Low. see check on page 14.

W. Flow St.

T.P. in pole
J.P. 1825 0.60 108.67 0.64 108.07

0+90 Cont.

0+90

T.P. 0.63 108.71 13.25 108.08

0+89 27° Lt. = Pole # J.P. 1825

0+50

T.P. 0.19 121.33 10.21 121.14

T.P. 0.06 131.35 12.81 131.29

Hanging in the air.

pipe end on "sky hooks"

0+25 17⁵ Rt. = End 18" corr. Iron pipe

1AA.10

♀

12

93.5
15.2
29

98.6
10.1
35

89.3
19.4
60

113.61
+49
55

107.5
1.2
35

101.9
6.8
11

101.3
7.4
15

97.8
10.7
23

98.1
10.6
23

108.71

123.8
+2.5
50

121.2
0.1
35

116.8
4.5
121.33

110.7
10.6
35

102.2
19.1
70

128.8
15.3
17.5
INVERT

1AA.10

Willow St.

T.P. 0.50 71.52 13.07 71.02

2+00

1+92 27^E LI. = Pole # 30.1398 H

1+84

1+62

T.P. 0.69 84.09 13.16 83.40

1+35

T.P. 0.97 96.56 13.08 95.59

1+20 Cont.

1+20

108.67

4

13
13

75.9

8.2
35

76.2

7.9
9

79.9

13.2

64.2

17.9
35

90.2

16.1
60

84.7

10.6
35

82.1

2.0
22

79.7

1.4
19

80.9

3.2
84.09

75.7

8.4
11

72.6

11.5
35

68.2

15.9
60

92.8

3.8
35

89.6

7.0
11

84.7

7.9
9

85.3

11.3
96.56

86.9

7.7
20

83.5

13.1
29

81.9

14.7
35

75.3

21.3
60

86.2

22.5
35

82.5

26.2
60

101.7

7.0
50

99.4

7.3
35

97.5

11.2
27

97.4

11.3
16

95.4

13.3
108.67

91.3

17.4
3

91.7

17.0
8

88.6

20.1
10

89.5

17.2
28

Willow

N.W.B.P. Willow +
Oliphaat ory. B.M. 3.51 152.81 152.80

T.P. 12.35 156.31 0.27 143.96

T.P. 12.43 144.23 0.67 131.80

T.P. 12.70 132.47 0.38 119.77

T.P. 11.99 120.15 0.22 108.16

T.P. 12.81 108.38 0.17 95.57

N.W. Mont. ^{0.41 Diff}
Oliphaat +
Evergreen Page 3 4.86 90.47 90.88

T.P. 10.07 95.74 1.91 85.67

T.P. 10.71 87.58 1.28 76.87

T.P. 7.98 78.15 1.35 70.17

N.W. Mont. see note bottom of page 11
Newell + Willow 55 12.95 58.15 58.57 page 9

2+00 = Nly. line Newell

71.52

14

see note page 11

see note page 11.

INDEXED
JAN 18 1942

74.9
+3.4
35

73.3
+1.8
21

64.9
6.6

58.9
12.6
35

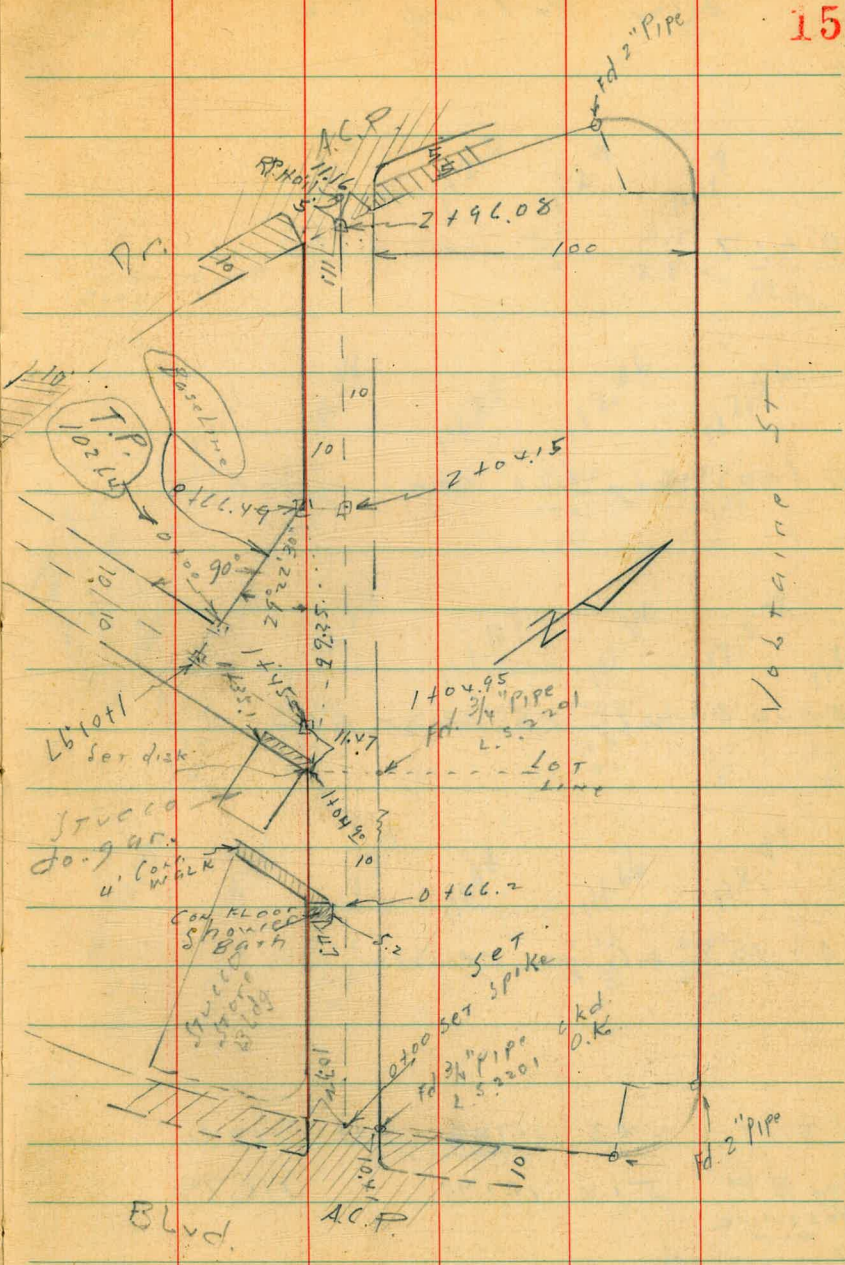
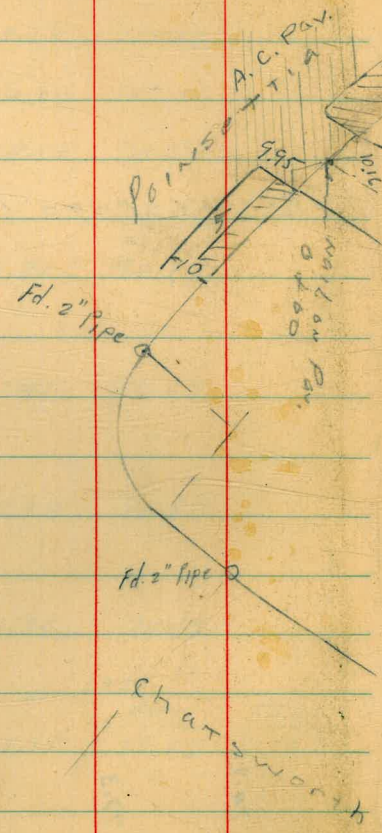
71.52

XSec 20' Alloys in
PT. LOMA CENTER Map 1862

Moore
Begg 1-14-49
Sheppard
Bunch W.O. 25001

Fl = 2" x 2" R.W. hubs

INDEXED
WK
JAN 18 1949



Voltaire St

Blyd.

A.C.P.

0 + 17

$$\begin{array}{r} 111.8 \\ 5.6 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 112.0 \\ 5.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 112.9 \\ 4.5 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 113.7 \\ 3.7 \\ \hline 28 \end{array}$$
 wly line
Blodg.

0 100 wly line chatsworth

$$\begin{array}{r} 111.11 \\ 6.32 \\ 10.32 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 110.78 \\ 6.65 \\ 10.32 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 111.23 \\ 6.20 \\ 10.41 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 112.06 \\ 5.37 \\ 10.41 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 112.56 \\ 4.87 \\ 10.41 \\ \hline 66 \end{array}$$

Produced
 J. Barrett
 1-20-49

0 - 10.4 wly cb. chat. Blod

$$\begin{array}{r} 109.80 \\ 7.63 \\ 30 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 110.73 \\ 6.70 \\ 13 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 111.01 \\ 6.42 \\ \hline \end{array}$$

$$\begin{array}{r} 111.80 \\ 5.63 \\ 12.5 \\ \hline 97 \end{array}$$

$$\begin{array}{r} 112.57 \\ 4.86 \\ 12.5 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 113.72 \\ 3.71 \\ 30 \\ \hline 66 \end{array}$$

0 - 10.5 wly gr. chatsworth

$$\begin{array}{r} 108.96 \\ 8.47 \\ 30 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 109.98 \\ 7.45 \\ 13 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 110.27 \\ 7.15 \\ 10.3 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 111.00 \\ 6.42 \\ \hline \end{array}$$

$$\begin{array}{r} 111.66 \\ 5.77 \\ 10.3 \\ \hline 66 \end{array}$$

$$\begin{array}{r} 112.91 \\ 4.52 \\ 30 \\ \hline 66 \end{array}$$

T.P. 483 117.43 9.33 112.60

117.43

Sw. BP 514 121.93 116.79
 Voltaire
 and
 chatsworth

1 + 04.90

0 + 85

0 + 66.7 N.E. Cor Bld. on 67.

T.P. 3.95 115.59 5.79 111.64

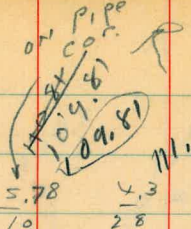
0 + 50

0 + 30

117.43
2

<

&



17

108.9
 $\frac{4.7}{10}$
 107

109.1
 65

109.81
 $\frac{5.78}{10}$

111.3
 $\frac{4.3}{28}$

114.58
 $\frac{1.01}{28}$
 TOP CON. FD.

S.W. Bldg. CON.

109.8
 $\frac{5.8}{20}$

110.1
 $\frac{5.5}{10}$

110.6
 $\frac{5.0}{10}$

110.9
 $\frac{5.7}{10}$

112.5
 $\frac{3.1}{28}$
 Bldg.

111.61
 $\frac{3.98}{10}$
 N. Cor. Bldg ON WALK

111.82
 $\frac{3.77}{5.3}$
 WALK

111.6
 4.0

111.9
 $\frac{3.7}{10}$

113.3
 $\frac{2.3}{28}$
 Bldg.

CUT OFF

115.59

112.0
 $\frac{5.4}{10}$
 Bldg.

112.3
 5.1

112.4
 $\frac{5.0}{10}$

113.6
 $\frac{3.8}{28}$
 Bldg.

112.1
 $\frac{5.3}{10}$
 Bldg.

112.4
 5.0

112.8
 $\frac{4.6}{10}$

113.6
 $\frac{3.8}{28}$
 Bldg.

117.43

1 + 80

T.P. Hub
P. 15 327 105.91 1295 10264

1 + 527

1 + 324

1 + 2785

1 + 16.37

115.59

102.8	103.2	104.3	104.8	105.9
$\frac{3.1}{15}$	$\frac{2.7}{15}$	$\frac{1.5}{10}$	$\frac{1.1}{10}$	$\frac{0.0}{20}$

103.8	104.3	105.91	109.6
$\frac{11.8}{15}$	$\frac{11.3}{10}$	$\frac{105.6}{10.0}$	$\frac{9.0}{38.8}$

106.3	107.2	107.6	110.05
$\frac{9.3}{10}$	8.4	$\frac{8.0}{10}$	$\frac{5.5x}{37.8}$

Com. slab
Rear platform
cleaner

106.7	107.6	108.1	109.6
$\frac{8.9}{10}$	8.0	$\frac{7.5}{10}$	$\frac{6.0}{28}$

107.5	108.3	109.1	110.5
$\frac{8.1}{10}$	7.3	$\frac{6.5}{10}$	$\frac{5.1}{28}$

alley →

115.59

check to SEBP 9.55 9636 9635
 Voltmeter Villa Dr.
 POINSETTIA Dr.

Ely curb Poinsettia $\frac{1158}{30}$ $\frac{1217}{30}$
 06 P 06 P

2 + 9608 = Ely Line Poinsettia Dr

2 + 87

2 + 82

2 + 65

2 + 35

2 + 04.5

10591

94.97 93.80 93.88 93.91 93.93 94.06 94.06 94.66 94.14 94.75
 $\frac{11.4}{19}$ $\frac{12.11}{19}$ $\frac{12.03}{17}$ $\frac{12.00}{10}$ $\frac{11.98}{10}$ $\frac{11.85}{10}$ $\frac{11.85}{123}$ $\frac{11.25}{123}$ $\frac{11.77}{30}$ $\frac{11.16}{30}$
 06 P 06 P 06 P 06 P 06 P 06 P 06 P 06 P 06 P
 94.65 94.49 94.21 94.69 94.90
 11.26 11.42 11.70 11.23 11.11
 11.12 11.12 11.10 11.12
 06 P 06 P 06 P 06 P 06 P
 95.1 96.3 96.3 94.6 94.5 94.5 96.6 97.2
 $\frac{10.4}{20}$ $\frac{9.6}{10}$ $\frac{9.6}{7}$ $\frac{11.3}{6}$ $\frac{11.4}{6}$ $\frac{11.4}{6}$ $\frac{9.3}{10}$ $\frac{8.7}{20}$
 95.9 96.9 97.1 97.4 97.7
 $\frac{10.0}{20}$ $\frac{9.0}{10}$ $\frac{8.8}{10}$ $\frac{8.5}{10}$ $\frac{8.2}{20}$
 96.9 97.6 98.1 98.5 100.2 100.2
 $\frac{9.0}{20}$ $\frac{8.3}{10}$ $\frac{7.8}{10}$ $\frac{7.4}{10}$ $\frac{5.7}{19}$ $\frac{5.7}{25}$
 98.7 100.1 101.1 101.3 102.2
 $\frac{7.2}{20}$ $\frac{5.8}{10}$ $\frac{4.8}{10}$ $\frac{4.6}{10}$ $\frac{3.7}{20}$
 100.9 101.8 102.9 103.3 104.6
 $\frac{5.0}{20}$ $\frac{4.1}{10}$ $\frac{3.0}{10}$ $\frac{2.6}{10}$ $\frac{1.3}{20}$
 5.6. 10591

0+60

100.0	100.1	99.8	100.2	100.6	100.6	100.9
$\frac{5.9}{20}$	$\frac{5.8}{14}$	$\frac{6.1}{10}$	5.7	$\frac{5.3}{8}$	$\frac{5.3}{10}$	$\frac{5.0}{20}$

0+30

98.5	99.0	98.1	98.3	98.2	99.1	99.5
$\frac{7.4}{20}$	$\frac{6.9}{10}$	$\frac{7.8}{9}$	7.6	$\frac{7.7}{7}$	$\frac{6.8}{10}$	$\frac{6.4}{20}$

0+05

97.1	97.1	96.3	96.3	96.4	97.2	98.0
$\frac{8.8}{15}$	$\frac{8.8}{10}$	$\frac{9.1}{9}$	9.5	$\frac{9.5}{6}$	$\frac{8.7}{10}$	$\frac{7.9}{20}$

0+00 N Ely POINSETTIA Dr

95.89	95.76	95.81	96.52	96.65
$\frac{10.07}{10.16}$	$\frac{10.15}{10.16}$	$\frac{10.10}{P}$	$\frac{9.39}{9.95}$	$\frac{9.26}{9.95}$
$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$

0-10

95.21	94.61	95.72	96.53	96.59	97.2
$\frac{10.70}{40}$	$\frac{11.30}{40}$	$\frac{10.19}{12}$	$\frac{9.38}{12}$	$\frac{9.37}{40}$	$\frac{8.70}{40}$
$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$

0-10 CURB NE LINE POINSETTIA Dr.

95.14	95.21	95.51	95.91	95.96
$\frac{10.77}{12}$	$\frac{10.70}{10}$	$\frac{10.40}{P}$	$\frac{10.00}{10}$	$\frac{9.95}{12}$
$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$	$\frac{06}{06}$

10591

10591

Top 3/4" Pipe 294 10980 10981
10 Rt of 1704,95
P. 15 and 17

17504

174500 Sec. on S.E. of E+W alley

17351

T.P. Hub 1012 112.76 327 10264

170197

10591

108.1 108.31 108.56
4.45 4.20
5.9 10 Gar
end Floor
Approx.

107.3 107.6 108.24 108.50
5.5 5.2 4.52 4.26
11x7 5.9 11.47
Con. Approx 9 Gar. Floor

106.0 106.0 106.9 106.6 107.93 108.48
6.8 6.8 6.2 4.83 4.28
15 10 3 5.9 10
Beg. Con. 9 Gar. Floor
approx

102.3 102.61 112.76
3.6 3.7 2.7 2.0 1.4
20 10 10 20
Hub

10591

Alley Pt. Loma (7P)
see sketch

016649 = A alley

016633

012216

0100 = Wly line of Nly & Sly alley
see sketch

112.76

LT

Sline alley
= Baseline

R 22

100.5
12.3
10
101.8
11.0

100.6
12.2
10
101.0
10.8
102.0
9.8
10
104.2
8.5
20

101.4
11.4
10
102.3
10.5
102.9
9.9
10
103.9
8.9
20

101.8
11.0
10
102.7
10.1
103.5
9.3
10
104.4
8.4
20
10' S of Sline alley

112.76

Pershing Drive Alignment Change
 18th & H St North & East

4+58.88 P.O.T.

INDEXED

M.K.

JAN 18 1950

+60.78 E.C.	37° 49'	
+50	36° 26.63'	
3+40	30° 04.66'	Δ 75° 38'
+50	23° 42.89'	R 225'
2+40	17° 20.72'	T 174.63
+50	10° 58.75'	Δ 297.01
1+0	4° 36.78'	D. 763.94

0+63.77 B.C. Pt.

0+00 = North line H St

North line Change

Pershing Drive

Jan. 17. 50
 H.S. 1503
 D. Smith
 Porter
 Chavez

23

N.O. 20006

3+60.78 E.C.

2+38.40 P.I.

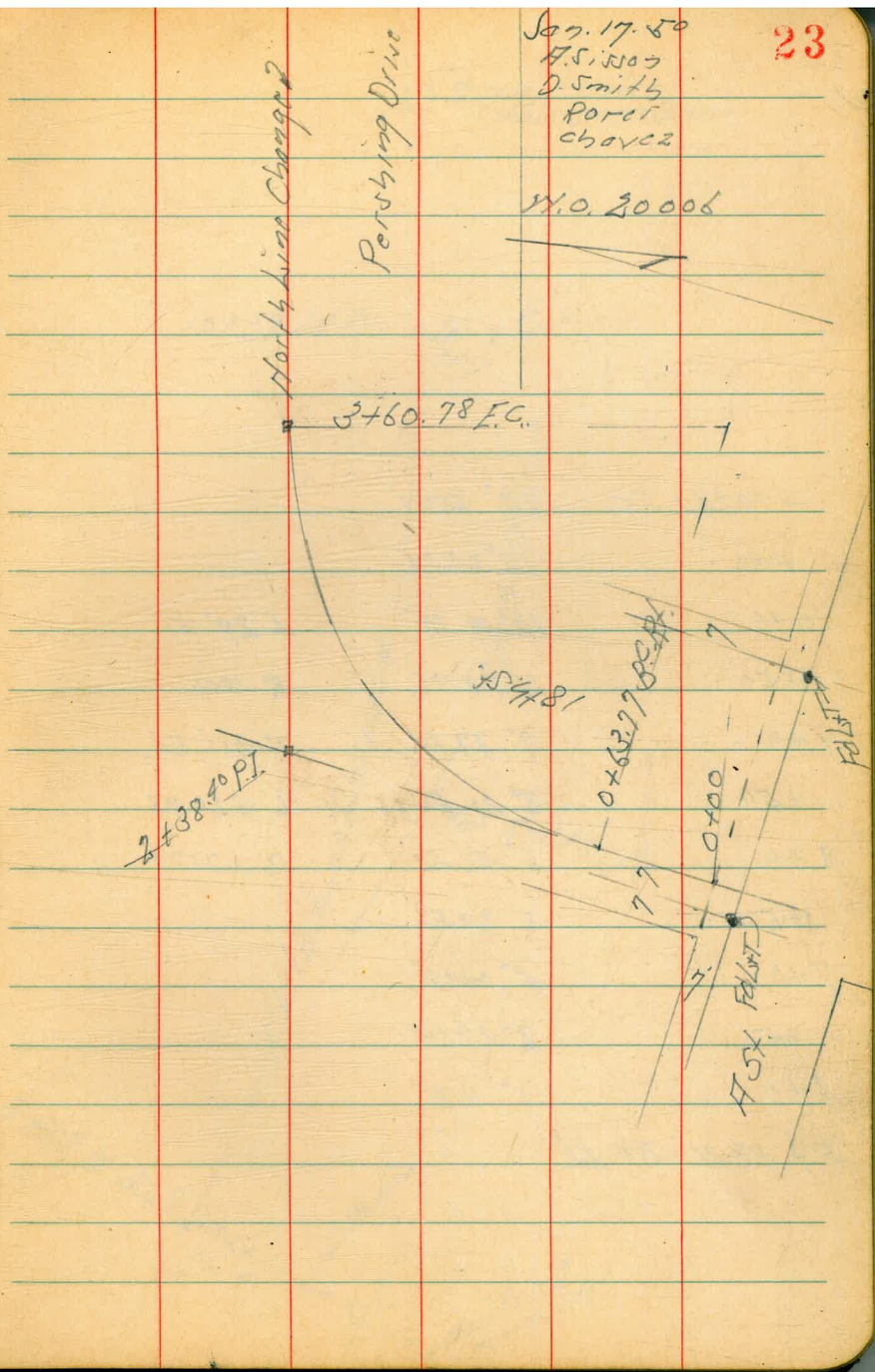
2+48.81

0+63.77 B.C. Pt.

0+00

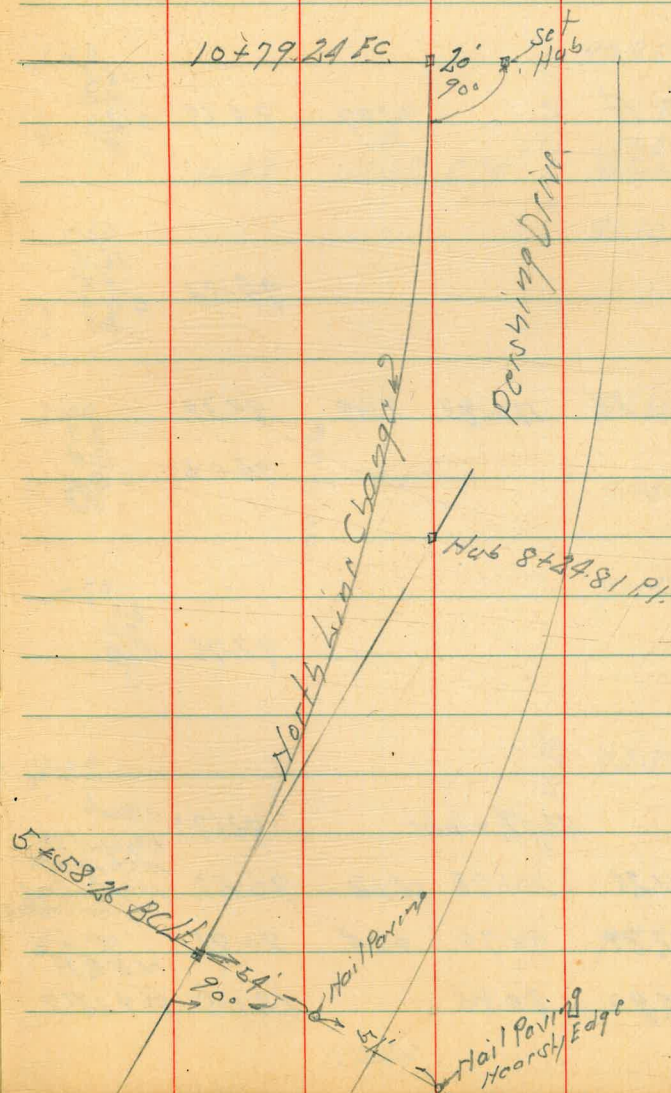
H St. PAVEMENT

PAVEMENT



14 NW. Pillar
Cobble Stone Bridge

+79.24 = F.C.	14° 55.50'	
+50	14° 05.24'	
10+0	12° 39.29'	L 29° 51'
+50	11° 12.85'	R 1000'
9+0	9° 47.41'	T 266.55'
+50	8° 21.46'	L 520.98'
8+0	6° 55.52'	D, 1.7189'
+50	5° 29.58'	
7+0	4° 03.64'	
+50	2° 37.69'	
6+0	1° 11.75'	
5+58.26 B.C. Lt.		



Northline Pershing Drive Grader

Sketch page 23

6+0 01628 93.99 $\frac{16.8}{41}$ $\frac{127}{64}$ $\frac{1}{4}$ "

+58.26 BC Lt 94.97 ^{16.2} 94.67 $\frac{12.2}{12.0}$ $\frac{7}{9}$ $\frac{3}{4}$ "
 Pav.

5+0 94.34 $\frac{16.5}{5.5}$ $\frac{11.0}{8.3}$ $\frac{3}{4}$ "

TP 11.44 110.83 2.39 99.39

+50 94.05 $\frac{7.7}{2.4}$ $\frac{5.3}{5.3}$ 11"
 .00578

4+0 93.76 $\frac{8.0}{7.0}$ $\frac{1.0}{1}$

3+85 R/W = 10' Lt 93.67 \rightarrow Grate
 Ch. 10' / 11'
 W/C 6' 18" St
 N/W 6' End
 S/W 8' 6" 1/2" 1/2"

11.26 101.78 3.18 90.52

12.89 93.70 0.14 80.81 NERP

B.M 12.90 80.95 68.05 B+18 1/2

9+0 90.95 $\frac{27.6}{13.4}$ $\frac{14.2}{10.7}$ $\frac{3}{4}$ "

10.48 118.52 2.79 $\frac{109.20 \text{ Corrected}}{108.04}$

+50 91.10 $\frac{12.7}{2.2}$ $\frac{17.4}{10.1}$ $\frac{3}{4}$ "
 .00312

8+0 91.26 $\frac{19.6}{2.0}$ $\frac{15.6}{11.7}$ $\frac{3}{4}$ "

+60 out 91.38 = inlet

+50 91.56 $\frac{19.3}{2.5}$ $\frac{16.8}{13.6}$ $\frac{3}{4}$ "

7+0 92.37 $\frac{18.5}{1.3}$ $\frac{17.2}{12.9}$ $\frac{3}{4}$ "
 .01628

6+50 90.18 $\frac{17.7}{1.6}$ $\frac{16.4}{8.3}$ $\frac{1}{2}$ "

110.83

			5.31	93.56	on cut of 6 4 to
	9.55	98.87	0.30	89.32	
BM	0.96	89.63	6.88	88.66	SFBP Pershing + Parr. Ho. Canyon Top of 106 Col 66/106 89.88
	0.85	95.54	12.45	94.69	
	0.35	107.14	12.34	106.79	
TP	2.38	119.13	1.77	116.75	
+80				90.38	90.62 Rev
+79.24 E.C.				90.39	

+50				90.48	28° out
-----	--	--	--	-------	------------

10+0			0.05/2	90.64	27.9 105 c 17.4 3.1 130
------	--	--	--------	-------	----------------------------------

9+50				90.79	27.7 12.7 c 15.0 3.1 11.3
------	--	--	--	-------	------------------------------------

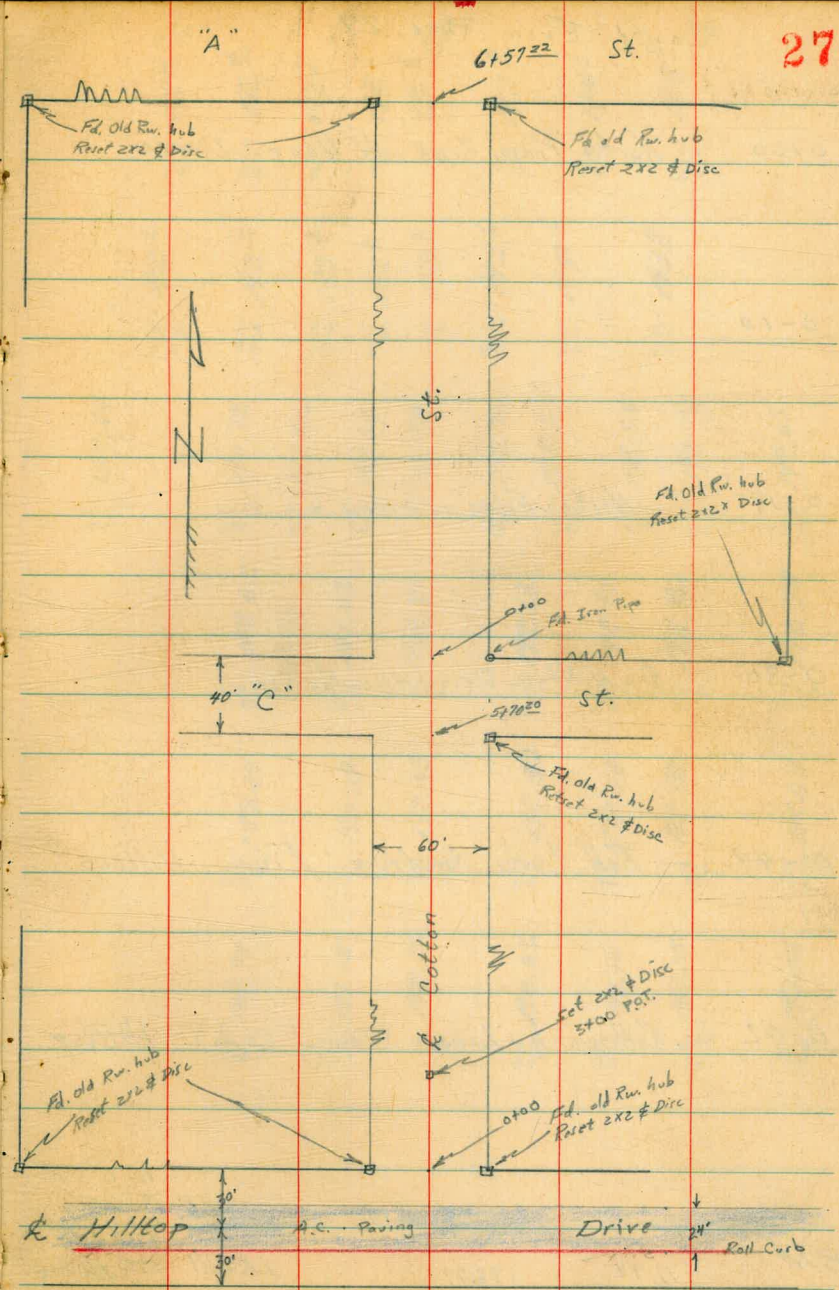
118.52

Roberts
Garber
Moore
Clark
2-6-50
H.D. 25020

X-Sect Cotton Street
(Hilltop to Northby End)

Map 1572

INDEXED
W.K.
FEB 9 1950



0+00 North Prop. Line Hilltop Drive

192 1/2	192 2/2	193 1/2	192 1/2	196 1/2	193 1/2	194 1/2	194 1/2
9.4	9.2	8.5	9.3	9.2	8.5	7.9	7.8
50	30	2	5	2	17	30	50

0-10 North Prop. Line Hilltop Drive

192 0	192 1/2	193 2	192 2	192 2	193 1	194 1	193 1/2
10.0	9.4	8.8	9.8	8.7	8.9	7.9	8.1
50	30	10	6	2	20	30	50

0-18 North Edge Paving

189.44	190.72	191.26	191.63	191.98	192.36	192.55	192.68	192.74	192.65
12.54	11.26	10.70	10.35	10.00	9.62	9.43	9.30	9.24	9.33
100	50	30	15	10	15	30	50	75	100

0-30 E Hilltop Dr. (Also Pav. Strip)

189.62	191.03	192.20	192.63	192.90	192.96	192.78	192.78
12.36	10.95	9.78	9.35	9.08	9.02	9.20	9.20
100	50	25	30	50	75	100	100

0-41 Roll Curb Gutter Line Hilltop

189.49	190.79	192.03	192.57	192.78	192.82	192.68
12.49	11.19	9.95	9.44	9.20	9.16	9.30
100	50	25	50	75	100	100

0-42 So. Roll curb Line (Top of Curb). Hilltop

189.79	191.12	192.36	192.86	193.10	193.15	193.02
12.19	10.86	9.62	9.12	8.88	8.83	8.96
100	50	25	50	75	100	100

TBM	6.33	201.98	3.14	195.65	
BM	11.98	198.79	186.81		201.98

Pole on left # 77092
 @ 1.8 ft. ct.
 7.7 ft. Hilltop

Cont'd From Page 28

1+54

30[±] Rt & 8' Conc. Drive

1+50

1+17

30[±] Rt & 3' Conc. Walk

1+00

0+90

215' Rt to Center T. Pole # JP278618

0+68

215' Rt Deadman

0+50

0+47

231' Lt. P. Pole # 77092

0+28

23' Lt Deadman

201.98

Lt

Rt

196.7

196.61

29

197[±]

4.6
5.0

5.0

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5.0

5.0

5.18
Drive

5.37
Drive

196.45

196.54

5.33
30[±]
Walk

5.44
45[±]
Walk

195.5

196.1

5.9
22

5.6
30

194.8

195.1

7.6
17

6.9
50

194.8

195.1

7.2
30

6.9
50

194.8

195.1

7.2
30

6.9
50

194.8

195.1

7.2
30

6.9
50

194.8

195.1

7.2
30

6.9
50

194.8

195.1

7.2
30

6.9
50

201.98

2+94 23[±] Lt. Center 9" Acacia Tree

2+51 21[±] Rt. Center P.Pole # JP270749

2+50

2+48[±] 23[±] Lt. Center P.Pole # P77093

2+17 30' Rt & 2[±] Conc. Walk

2+06 31[±] Lt & 3[±] Conc. Walk

2+00

1+96[±] 22' Rt. Center P.Pole # P277637

1+78 30[±] Rt & 8' Conc. Drive

20,98
↑

Lt

Rt

Rt

30

199[±] 198[±] 198[±] 197[±] 197[±] 197[±] 196[±]
 2.7 3.2 3.9 4.2 4.4 4.8 5.3
 30 30 18 15 30 30 50

197.36
 4.62
 30
 Walk
 4.54
 48
 Walk

199.06
 198.91
 2.92 3.07
 50 31[±]
 Walk Walk

198[±] 198[±] 198[±] 197[±] 197[±] 197[±] 197[±]
 3.2 3.4 3.6 4.2 4.5 4.7 4.9
 50 30 29 15 30 30 50

197.05
 4.93
 30[±]
 Drive
 196.72
 5.26
 50
 Drive

20,98
 ↑

4+50

191 [±]	189 [±]	188 [±]	189 [±]	188 [±]	188 [±]	187 [±]	187 [±]	186 [±]
0.6	2.2	2.9	2.8	3.6	3.5	4.8	4.7	5.8
30	30	26	13	11		24	30	30

4+10 23' Lt Center P.Pole #77094

T.P. 2.07 $\frac{191.76}{\lambda}$ 12.29 189.69 $\frac{191.76}{\lambda}$

4+00

194 ⁻	193 [±]	193 [±]	191 [±]	192 [±]	191 [±]	191 [±]	191 [±]	190 [±]	190 [±]
7.9	8.4	8.4	10.1	9.2	10.4	10.2	10.4	11.0	11.6
50	30	23	17	13	11		15	25	30

3+71 21[±] Rt Center T.Pole #440327M

3+50

197 [±]	196 ⁻	195 [±]	194 [±]	195 [±]	194 [±]	194 [±]	193 [±]	193 [±]
4.8	5.9	6.2	7.4	6.6	7.7	7.2	8.3	9.0
50	30	25	20	17	11	14	30	50

3+05 29[±] Rt 8' Conc. Drive

195.91
6.07
29[±]
Drive

6.40
49.8
Floor

3+00

198 [±]	198 [±]	196 [±]	196 [±]	196 [±]	195 [±]	195 [±]	195 [±]
3.3	4.0	5.6	5.1	5.4	6.2	6.1	6.4
30	30	12		13	20	30	49

$\frac{201.98}{\lambda}$

$\frac{201.98}{\lambda}$

0 + 35 246 Rt End Hedge Begin Lath Fence

0 + 19 243 Rt Eugenia Hedge

0 + 00 North Prop. Line "C" St.

5 + 90²⁰ & "C" St.5 + 70²⁰ South Prop. Line "C" St.5 + 66 26³ Lt Center P. Pole # 171081

5 + 35

5 + 20 21' Rt. Center T. Pole # 414522 #

5 + 00

191.76
x

		181 ²	181 ²	182 ⁰	182 ⁰	182 ⁰	182 ⁰	182 ²	183 ²	183 ⁵
		10.1	9.7	9.7	9.0	9.0	8.9	8.9	8.6	8.3
		50	30	30	14	20	20	30	30	50
		181 ²	182 ¹	182 ⁵	182 ⁰	182 ⁶	183 ⁰	183 ²	183 ²	183 ²
		10.1	9.7	9.3	9.6	9.2	8.8	8.5	8.5	8.3
		50	30	20	12	20	30	30	30	50
			181 ⁵	182 ⁵	182 ²	182 ²	182 ⁵	183 ⁰	183 ⁹	183 ²
		10.2	9.4	9.1	9.3	8.8	8.8	7.9	7.9	7.9
		50	30	15	20	20	30	30	50	50
		183 ²	183 ⁵	183 ⁰	183 ¹	183 ⁶	183 ¹	184 ¹	184 ²	184 ²
		8.6	8.3	8.0	8.7	8.2	8.7	8.8	7.7	7.1
		50	30	23	20	13	13	10	20	30
		187 ⁵	187 ⁵	186 ⁹	184 ²	185 ²	184 ⁵	184 ²	184 ²	185 ²
		4.3	4.3	5.4	7.1	6.6	7.3	7.0	7.1	6.8
		50	40	30	20	15	12	25	30	50

191.76
x

2+50

2+47 22' Lt. Center P. Pole # 77640
21' Rt. Center T. Pole # 5P271#47

2+00

T.P. 12.58 200.11 4.23 187.53

1+50

1+00 23' Lt. Center P. Pole # 77095

0+73 20' Rt. Center T. Pole # 456645

0+58 24' Rt. End Lath Fence

0+50

191.76

188 [±]	189 [±]	189 [±]	190 [±]	190 [±]	190 [±]	190 [±]	191 [±]	192 [±]
11.9	11.4	10.4	9.4	9.9	9.6	9.6	9.8	8.3
50	30	15	9	8		15	20	30

187 [±]	187 [±]	188 [±]	189 [±]	188 [±]	188 [±]	188 [±]	189 [±]	190 [±]
13.1	12.2	12.0	11.2	11.7	11.5	11.2	11.6	10.2
50	30	16	11	9		16	20	30

200.11

186 [±]	186 [±]	186 [±]	187 [±]	187 [±]	187 [±]	187 [±]	188 [±]	188 [±]	189 [±]
5.8	5.3	5.1	4.4	4.5	4.4	4.3	4.5	3.5	3.3
50	30	20	10	8		15	18	26	30

184 [±]	185 [±]	186 [±]	185 [±]	186 [±]	186 [±]	185 [±]	186 [±]	187 [±]	187 [±]
7.4	6.6	5.7	6.1	5.8	5.5	6.0	5.1	4.8	4.3
50	30	10	8		14	17	25	30	50

183 [±]	183 [±]	184 [±]	184 [±]	184 [±]	184 [±]	184 [±]	184 [±]	184 [±]	185 [±]	185 [±]
8.3	7.9	7.4	7.8	7.4	7.8	7.4	7.6	7.0	6.2	6.0
50	30	15	10		10	12	24	25	30	50

191.76

4+31 22' Rt Deadman

4+26 22' Lt Deadman

4+06 22' Lt Center P. Pole #77641
22' Rt Center T. Pole #172284

4+00

3+50

3+25 213' Rt End Cobblestone Wall

3+03 28' Rt Center 8" Acacia Tree

3+00 22.4' Rt Begin 6" Cobble Stone Wall

200.11

Lt

E

Rt

34

1922	1942	1951	1948	1951	1955	1957	1958	1957	1967	1980
7.2	5.3	5.0	5.3	4.4	3.6	4.4	4.3	4.4	3.7	2.1
50	30	23	19	11	9	7		20	30	50

1902	1911	1935	1941	1935	1938	1938	1935	1953	1958	1955
7.4	8.4	6.5	6.0	6.6	6.3	6.3	6.6	4.8	4.3	4.6
50	30	12	10	8		5	8	28	30	50

1931	1943
7.0	5.2
23	20
23	11

1892	1903	1916	1925	1920	1923	1920	1925	1941	1935	1940	1941
10.9	9.8	8.5	7.5	8.1	7.8	8.1	7.6	6.0	6.5	6.1	6.0
50	30	13	10	8		18	22.4	22.4	23	30	40
							gra.	Top wall			

200.11

6+87²²

6+57²² South Prop. Line "A" St.

6+00

5+50

5+00

T.P. 12.87 212.44 0.54 199.57

4+50

200.11

197 ²	198 ²	199 ⁴	199 ^L	199 ^B	200 ³	200 ²	200 ^E	200 ^B	200 ^F	201 ⁹	202 ³
152	140	130	133	126	121	124	12.2	11.6	11.9	10.5	10.1
50	30	23	19	12	10	8	2	16	20	30	50
195 ³	196 ³	196 ²	197 ⁹	198 ⁶	198 ²	198 ¹	198 ³	198 ²	199 ³	199 ^B	
4.8	3.8	3.2	2.2	1.5	2.1	2.0	1.8	1.2	0.8	0.3	
50	30	19	11	8	6	20	17	23	30	50	
203 ⁰	204 ⁰	204 ¹	205 ⁴	206 ⁵	206 ¹	207 ¹	208 ²	208 ¹	208 ²	210 ¹	
9.4	8.0	7.7	7.0	5.9	5.7	4.7	4.4	3.7	3.7		
50	30	22	15	20	23	30	30	50	50		
201 ³	202 ²	203 ²	204 ¹	204 ¹	204 ⁴	204 ⁴	204 ⁵	204 ²	205 ²	205 ²	206 ²
11.1	10.2	8.5	7.7	8.3	8.0	7.8	8.0	7.2	6.5	6.4	
50	30	11	9	8	80	16	20	24	30	50	
199 ³	200 ⁶	201 ²	202 ¹	202 ⁰	202 ⁴	202 ⁸	202 ⁴	203 ⁶	204 ⁵		
13.1	11.8	10.5	9.6	10.4	10.0	9.7	10.0	8.8	7.8		
50	30	12	10	8	10.0	15	20	50	50		
204 ⁵	205 ²	205 ²	206 ⁵	206 ⁵	207 ¹	208 ²	208 ²	210 ¹			
7.8	7.0	7.0	5.0	5.0	5.0	5.0	5.0	5.0			
50	30	30	50	50	50	50	50	50			

200.11

check			6.76	210.61 = 210.64
T.P.	5.77	217.37	0.84	211.60

R 2d + C.T.
47th # "A"

7+17²²

212.44

2060
6.4
30

2070
5.4
30

2080
3.9

2090
2.5
30

2100
1.8
30

212.44

Roberts
Garber
Moore
Clark
4-7-50
H.O. 21560

X-Sect. Olivet Street
Ivanhoe Ave. to Cabrillo Ave.

T.P. 30, 32 T.P.
May 2171

INDEXED
Y.R.
APR 11 1950

← Ivanhoe Ave. East

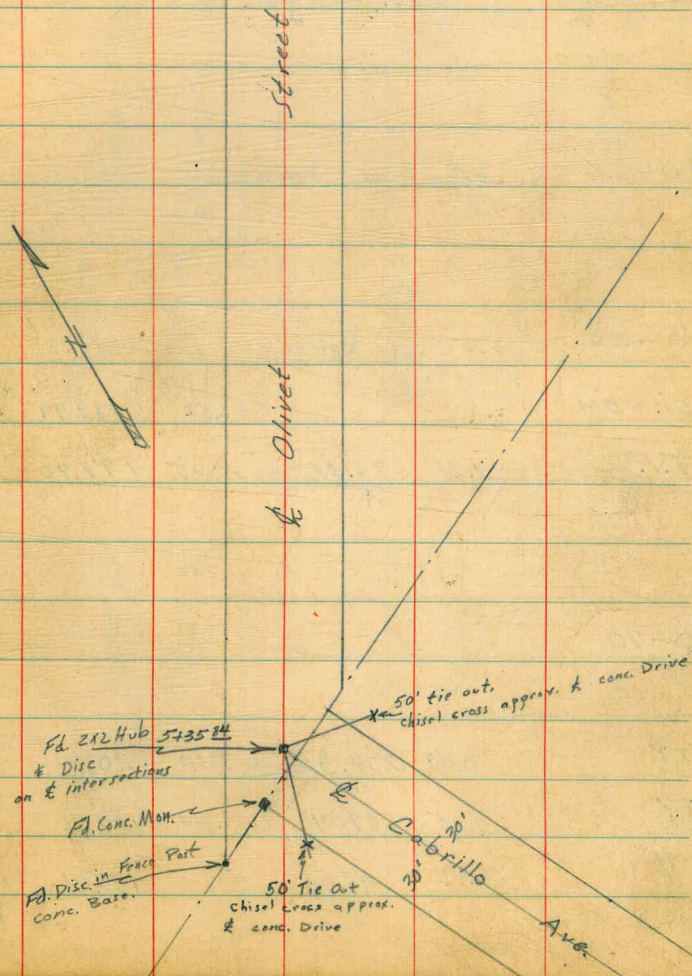
Set chisel CROSS 0-01

37

← 0+00

Ad. & C.T.
on E Ivanhoe Ave. E.
Westerly 10' Line
of Olivet

Olivet St.: —
60' Street
30' Roadway
5' 8" Comb. Cb. & Walk
3' Cb. Radius



0+08 21' Lt to Deadman

0+06 22' Rt. Begin Row of bushes.

0+00 sly. line Ivanhoe Firehydrant behind Exist cb. 4

0-00.4 Pav. Edge.

0-20 cb. line Ivanhoe

0-23 B.C. cb Ret.

Set TBM

T.P.

0-70

TP

TP

BM

197.9	190.98	190.95	190.13	190.41	190.44	190.03	189.74	188.4	184.7	181.7	180.4
+1.6 30	5.33 2067 Walk	5.36 15 cb	6.18 15 Gutt	5.80 11	5.87	6.28 15	6.57 203	7.7 208	11.6 30	14.6 40	15.9 50
			4.17 15 cb	5.56 18 Gutt	5.47	6.56 15 Gutt	6.73 18 Gutt	5.97 18 cb	6.87 21 Gutt	6.16 21 cb	1.5
			191.64	190.92	190.72	189.97	190.46				
			4.67 15 cb	5.39 15 Gutt	5.39	6.44 15 Gutt	5.85 15 cb				
	6.52	189.79									
	4.91	196.31	12.95	191.40	196.31						
			9.10 15 cb	9.82 15 Gutt	9.84	10.81 15 Gutt	10.27 15 cb				
	0.44	204.35	3.10	203.91	204.35						
	9.05	207.01	0.04	197.96							
	12.99	198.00		185.01							

North to Zinc Offcut
& Ivanhoe
Ld + Disc

250 ft
SWBP
Exchange &
Virginia Hwy

1736⁵ 30' Lt End Conc. Drive

1721 30' Lt. Begin Conc. Drive

1702 27' Rt End Row of Cypress

1700

0+91⁵ 167' Lt. to Center P.P. # P 1261

T.P. 1.66 186.08 11.89 184.42

0+86 27¹/₂' Rt to Row of Cypress

0+75

0+50 23¹/₂' Rt to 3" Tree
18¹/₂' Rt End Bushes

0+25 26' Rt 3" Acacia

196.31

Lt

Rt

Rt

39

0.0 186.1
47 Apron
2.59 183.49
30 Apron

90	186.1	1.76	184.38	3.4	182.7	4.4	181.7	4.6	181.1	4.8	181.3	9.5	176.6	9.9	176.2	11.0	175.1	12.6	173.5	12.6	173.5
43 ⁵		30		15		10		7		7		15		28		30		36 ²		37	
Apron		Apron																			

191.1	186.4	185.4	184.0	183.7	183.4	183.6	179.2	177.3	176.3	176.4	174.0	174.0
+50	+0.3	0.7	2.1	2.4	2.7	2.5	6.9	8.8	9.8	9.7	12.1	12.1
50	30	17	13	7	7	9	17	18	30	30 ⁵	31	32 ⁵

186.08

195.8	189.6	188.4	187.5	186.1	186.0	185.7	185.8	180.4	178.3	177.8	177.6	173.9	173.9
0.5	6.7	7.9	8.4	10.2	10.3	10.6	10.5	15.9	18.0	18.5	18.9	22.4	22.4
50	30	24	13	12	7	9	19	21	30	30 ⁵	30 ⁵	36 ²	36 ²

198.4	192.8	188.1	187.6	187.8	187.8	187.1	187.7	179.3	179.3	178.4	176.9	176.9
+2.1	3.5	8.2	8.7	8.5	8.5	8.2	16.6	17.0	17.0	17.9	19.4	19.4
50	30	13	12	8	8	10	24	30	31 ³	31 ³	40	40

200.9	195.0	189.8	189.0	189.2	189.5	190.0	184.9	182.7	180.9	180.3	177.9	177.9
+4.6	13	6.5	7.3	7.1	6.8	6.3	11.4	13.6	15.4	16.0	18.4	18.4
50	30	14	12	11	11	13	20	28	30	31 ³	31 ³	38 ²

196.31

Contd From Page 39

2400 30^E Lt Begin Brick Ret Wall

T.P. 226 175.25 13.09 17 2.99 Hour No. 1235 No. End

1792

1790 30^E Lt End Conc Drive

1777 30' Lt Begin Conc. Drive
30' Lt End Conc. Block Ret Wall

1750 29^E Lt to Conc. Block Ret Wall

1744 21^E Rt to 14" Eucalyptus

1740^E 18^E Rt to 5" Eucalyptus

1739 24^E Rt to 5" Eucalyptus

186.08

176.5	175.28	173.9	174.4	173.3	171.8	171.4	171.1	172.5	171.6	167.0	167.2	166.4	165.2
+1.2	+0.08	1.4	0.9	2.0	3.5	3.9	4.2	3.8	3.7	8.3	8.1	8.9	10.1
40	30 ^E Top	30 ^E Foot	30 ^E Dirt	20	8	9	9	11	15	25	30	33	40

Step 175.25

179.1	177.9	175.2	172.8	172.6	172.2	172.5	172.5	168.4	168.3	167.6
7.0	8.2	10.9	13.3	13.5	13.9	13.6	13.6	17.7	17.8	18.5
40	30	19	7	9	9	10	16	25	30	32

179.91
6.17
45
Apron

178.08
8.00
30
Apron

179.46	178.38	180.3	178.0	178.4	177.4	175.8	175.0	174.5	174.2	174.5	170.1	169.4	167.6
6.6	7.0	5.8	8.1	7.7	8.7	10.3	11.1	11.6	11.9	11.6	16.0	16.7	18.5
40	30	30	30	30	23	12	9	8	12	25	30	40	
Apron	Apron	Top	Foot	Dirt									

183.6	182.2	182.2	180.7	181.1	179.7	178.1	178.0	177.8	178.2	174.2	171.8	170.3
2.5	3.9	3.9	5.4	5.0	6.4	8.0	8.1	8.3	7.9	11.9	14.3	15.8
40	30	29 ^E Top	29 ^E Foot	29 ^E Dirt	17	10	8	8	10	20	30	40

186.08

3+16⁸

30' Lt \times 3' Walk

Lt. 163.1
143
25⁸
Walk

162.18
242
30⁸
Walk

\times

Rt.

41

3+03

Rt \times 3' Walk

157.41
7.19
30⁸
Top Stop

8.29
33
Walk

8.50
40
Walk

3+00

0.6
40

1.7
30

3.7
10

4.8
9

4.9
49

4.9
10

4.2
12

4.9
17

7.3
27

7.0
30

8.3
33

8.5
40

T.P.

1.84

164.60
 \times

12.97 162.76

164.60
 \times

2+50

4.4
40

7.0
30

9.3
16

10.5
9

10.3
33
Rim
Walk

10.8
9

10.3
11

13.5
28

13.7
30

16.1
36

T.P.

2.74

175.73
 \times

172.99

175.73
 \times

2+45

30' Lt End Brick Rt Wall

171.09
4.6
30⁵
Top

168.5
6.7
30⁵
Foot

169.4
5.9
30⁵
Dirt

2+29

218' Lt to Center P. Pole # P1231

175.25
 \times

175.25

Cont'd From Page 41

3+80 30' Rt End Conc. Block Wall

3+59 29' Lt & 10' Conc. Drive

3+50 22' Lt. Deadman

3+42 30' Rt Begin Conc. Block Wall

3+40

3+38 26' Rt & 8' Conc. Apron

3+30 22' Lt to Center P.P. # P1215

16460

9.1	155.5													
40		9.9	154.7											
		11.8	152.8											
		12.5	152.1											
		12.4	152.2											
		11	151.7											
		12.4	152.2											
		12.4	152.2											
		12.9	151.7											
		12.4	152.2											
		12.9	151.7											
		12.9	157.63											
		12.9	157.63											
		12.9	151.9											
		12.9	151.9											

7.05
40
Apron

7.75
29.8
Apron

7.2	157.4													
40		7.6	157.0											
		8.3	156.3											
		9.2	155.4											
		9.6	155.0											
		9.5	155.1											
		9.6	155.0											
		10.3	155.1											
		10.6	154.0											
		10.9	153.7											
		10.9	153.7											
		10.9	153.7											
		10.9	153.7											

140.7														
39	160.1													
40	157.8													
	156.8													
	156.0													
	156.1													
	155.8													
	156.2													
	155.4													
	154.3													
	153.8													
	153.8													
	153.8													
	153.8													

10.48
26.2
Apron

10.18
30.3
Flur

16460

Cont'd From Page 42

4+38 29' Rt & 2⁵ Walk

4+31 28' Lt to Deadman
22' Lt to Center P. Pole # P1205

4+30 29' Rt Board Fence Begins
28' Lt Center 12" Accia

4+26 29' Lt Begin Ornamental Fence

4+24 29' Lt & 2⁵ Conc. Walk

4+00

3+91 33' Rt & Single Garage

3+85

T.P. 2.16 154.03 12.73 151.87
164.60

148.1 Lt
53 6.2 7.0 8.0 146.4
40 30 16 8 76 8.0 9.5 84 9.3
292 292
Walk Walk

149.7
4.3 5.5 6.1 7.1 6.9 7.5 6.8 6.5 7.3 7.3
40 30 15 8 13 17 23 30 40

149.85
4.1 4.6
35 292
Walk Walk

153.1 152.2 150.7 149.9 150.0 149.4 150.4 148.5 148.34 149.20
0.9 1.8 3.3 4.1 4.0 4.6 3.6 5.5 5.6 5.83
40 30 15 8 40 12 17 30 33 40
Walk Walk

154.3 153.9 152.5 151.5 151.6 151.2 151.7 151.3 150.1 149.4 149.9
+0.3 0.1 1.7 2.5 2.4 2.8 2.3 2.7 3.9 4.6 5.1
40 30 9 7 11 14 20 30 33 40

154.03
149.67
436 334
Floor

5770

5768⁴ 6' Rt to Deadman

5759⁴ 55' Rt to Center P. Pole # P7598

5750

5737 11' Lt to MH

5735⁸⁴ Intersection of Es Cabrillo & Quiet

5730 196' Rt 6" Acacia

5715

5713 231' Rt to 10" Acacia

5707

144.55

136.4	136.1	136.2	136.6	135.9	135.6	135.5	136.0	138.8	45
9.2	9.5	9.4	9.0	9.7	9.9	10.1	9.6	8.8	
50	30	17	13	6		12	23	30	

8.2	8.0	7.9	8.0	7.8	7.2	8.1	8.1	8.1
50	30	15		2	5	13	13	30

7.25
17

142.34	141.10	139.88	139.9	139.8	140.1	139.6
3.21	4.45	6.67	6.0	5.7	5.8	5.5
38E	34E	23E	19	11	14	30
Edge Drive	Edge Drive	Edge Drive				
140.8	140.4	140.4	140.16	140.2	140.6	140.2
4.8	5.2	5.0	5.4	5.0	5.4	5.4
22	16		13	15	30	
Edge Drive	Edge Drive					

144.55

check 4.02 154.98 155.01 N.M. T' 22.8

T.P. 10.43 159.00 1.25 148.57

T.P. 13.03 150.42 7.16 137.39

set TBM 10.45 134.10 conc. Non wly. Line Cabrillo where it hits Olivet

5497 30' Rt End Wire Fence

5486 1357.6 135.7 136.0
10.0 9.9 9.6
50 33 32

5480 29' Rt End board Fence Begin Wire

5478

144.55

ct Pearl # Cabrillo

11.0	134.6	11.75	132.82	12.10	133.45	12.3	133.3	12.9	132.7	13.4	132.2	13.5	132.1
30		103		12		15		30		40			
		Edge Drive		Edge Drive									
9.6	136.0	10.23	135.32	10.96	134.59	11.7	133.9	12.0	132.6	12.1	133.5		
28		161		73		20		30		30			
		Edge Drive		Edge Drive									
9.8	135.8	10.9	134.7	10.8	134.8	10.9	134.7	9.9	135.7	9.7	135.9		
50		6		20		24		30					
		Edge Drive		Edge Drive									
		on Cabrillo											

144.55

Roberts
Cota
Moore
Pollen
6-15-51
W.O. 25020

X-Section Calle Quebrada
So. Subd. Line Tres Lomas to Cumberland
Map # 2160

T.P. 0.44 260.80T 12.83 260.36

1+39.16 BC Fd 3/4" Iron Pipes on E. & W. P.L.
Set Stub on E

1+00

0+50

0+00

South Line Tres Lomas Subdivision
Fd 3/4" Iron Pipes on East & West Prop. Lines
Fd 2x2 Rehub & CT on E

T.P. 5.21 273.19T 8.55 267.98 3/4" I. Pipe

T.P. 3.87 276.53 11.21 272.66

T.P. 0.53 283.87 12.85 283.34

T.P. 0.58 296.19 10.82 295.61 3/4" I. Pipe

BM 2.25 306.43 304.18 NW Cor.

44

E

FB

47

INDEXED

JUN 19 1951

253.7
17.5 13.7 9.8 9.7 9.9 7.6 5.4 2.7
50 25 5 12 17 25 50

259.2 263.3 265.1 266.7 266.9 267.4 269.8 270.9 273.0
14.0 9.9 8.1 6.5 6.3 5.8 3.4 2.3 0.2
50 25 10 4 11 17 25 50

261.5 265.3 268.6 268.8 270.2 270.8 273.4
11.7 7.7 4.6 4.4 3.0 2.4 10.2
30 25 11 16 25 50

254.0 260.0 263.75 266.32 268.57 272.9
19.2 13.2 8.44 6.87 3.62 0.3
100 30 25 on Pipe 25 on Hub 25 on Pipe 30

273.19T
P.C. Sta. 1+39.16 E. Prop. Line

S.E. Cor. Quebrada & Parana E.C. P.L. on Quebrada
Cumberland & Tres Lomas Chisel Square
See FB 2050 pg 48

3+00

2+70

T.P. 12.40 272.87A 0.33 260.47

2+43.88 EC Fd 3/4" Iron Pipes on EFW Pip.L.
Set Stub on R

2+25

2+10

2+00

1+75

260.80A

261.1 263.8 265.6 265.9 266.3 267.5 268.3 271.7 48
11.8 9.1 7.3 7.0 6.6 5.4 3.6 1.2
50 25 12 8 11 25 50

257.2 259.2 261.3 261.1 263.6 265.1 269.0
15.7 13.7 11.6 11.8 9.3 7.1 3.9
50 25 9 12 25 50

272.87A

248.8 250.4 252.0 253.7 256.2 258.2
12.0 10.4 8.8 7.1 4.6 2.6
50 25 13 25 50

245.6 243.9 246.5 247.0 251.3 251.7 248.5 250.1 254.2
15.2 16.9 14.3 9.8 9.5 9.1 12.3 10.7 6.6
50 25 13 7 11 18 25 50

241.2 244.0 244.1 251.4 251.6 252.6 254.4 258.4
19.6 16.1 16.7 9.4 9.2 8.2 6.4 2.4
50 25 22 7 15 25 50

247.6 252.8 254.9 257.4 257.6 258.2 260.4 262.3 266.2
13.2 8.0 5.9 3.4 3.2 2.6 0.4 1.5 1.5
50 25 12 5 12 16 25 50

260.80A

5+75

268.4	270.6	272.3	272.7	272.8	274.4	275.4	278.4
9.0	6.8	5.1	4.7	4.6	3.0	2.0	1.0
50	25	11	8	11	25	50	

5+50

268.2	270.5	272.9	273.0	274.4	276.1	279.6
9.2	6.9	4.5	4.4	3.0	1.3	+2.1
50	25	8	11	25	50	

5+00

260.0	267.1	269.9	272.3	272.6	273.9	275.5	278.7
17.4	10.3	7.5	5.1	4.8	3.5	1.9	+1.3
100	50	25	8	11	25	50	

4+50

267.5	269.9	272.5	273.0	274.0	275.7	278.7
9.9	7.5	4.9	4.4	3.4	1.7	+1.3
50	25	10	12	25	50	

T.P. 5.28 277.37X 0.78 272.09

277.87X

4+00

267.6	269.6	271.5	272.1	272.0	273.3	275.0	277.4
5.3	3.3	1.4	0.8	0.9	+0.4	+2.1	+1.9
50	25	12	7	9	25	50	

3+50

267.0	268.9	270.4	270.6	270.8	272.5	273.6	276.0
5.9	4.0	2.5	2.3	2.1	0.4	+0.7	+3.1
50	25	12	7	10	25	50	

272.87X

272.87X

7+77.67 EC. Fd. 3/4" I. Pipe on E & W P.L.
Set Stub on E

7+50

7+24

7+04.37 BC. Set Stub on E

6+75

T.P. 0.56 265.67 $\bar{\Delta}$ 12.26 265.11

6+35

6+00

277.37 $\bar{\Delta}$

248.2	252.7	254.2	253.5	254.5	255.9	257.9
17.5	13.0	11.5	12.2	11.2	9.8	7.8
50	25	7		8	25	50

242.9	244.7	245.5	251.7	252.5	252.4	246.3	246.8	249.2
22.8	21.0	20.2	14.0	13.2	13.3	19.4	18.9	16.5
50	25	18	8		5	17	25	60

242.1	248.3	254.4	253.9	254.9	256.9	260.3
23.6	17.4	11.3	11.8	13.8	8.4	5.4
50	25	6		11	25	50

257.9	259.8	262.8	260.3	260.4	264.5	266.3	268.1
7.8	5.9	2.9	5.4	5.3	1.2	0.6	12.4
50	25	8		10	15	25	50

265.67 $\bar{\Delta}$

267.2	269.8	268.7	266.1	265.9	266.9	271.6	272.2	274.4
10.2	9.6	8.7	11.3	11.5	10.5	5.8	5.2	3.0
50	25	11	3		9	13	25	50

265.2	268.4	270.1	271.4	271.1	271.4	273.6	275.5	278.6
12.2	9.0	7.3	6.0	6.3	6.0	3.7	1.8	1.2
100	50	25	10		8	12	25	50

277.37 $\bar{\Delta}$

10+00

13.5 50	271.0	9.6 25	274.9	5.5 3	279.0	5.4 5	279.1	5.5 9	279.0	4.0 11	280.5	1.7 25	282.8	+2.8 50	289.3
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9+35

18.3 100	266.2	10.9 50	273.6	5.6 25	278.9	4.6 22	279.9	4.3 10	280.2	4.4 10	280.1	3.3 14	281.2	2.8 25	281.7	+0.7 50	285.2
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9+00

11.9 50	272.6	7.7 25	276.8	6.8 6	277.7	6.7 10	277.8	6.1 13	278.4	5.3 25	279.2	2.8 50	281.7
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T.P.

7.23 284.487 0.57 277.25

284.487

8+50

10.5 50	267.3	9.5 25	268.3	7.5 5	270.3	7.7 10	270.1	6.2 14	271.6	4.9 25	272.9	2.9 50	274.9
------------	-------	-----------	-------	----------	-------	-----------	-------	-----------	-------	-----------	-------	-----------	-------

T.P.

12.35 277.827 0.20 265.47

277.827

8+00

5.6 50	260.1	4.2 25	261.5	3.5 8	262.2	3.8 10	261.9	3.0 10	262.7	4.8 14	263.9	1.3 25	264.4	+0.9 50	266.6
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265.677

265.677

Contd From Page 51

T.P. 959 305.71 ∇ 0.32 296.12

13+00 Set Stub on ϕ ^{So. Line} Pavana (E.C.P.L. At)

12+50

12+00

T.P. 12.19 296.44 ∇ 0.23 284.25

11+50

11+00

10+50

284.48 ∇

44

4

4

52

289.2 291.3 293.4 293.9 294.5 295.66 297.4
7.2 5.1 3.0 2.5 1.9 0.78 +1.0
50 25 10 13 25 50
on Pipe

286.7 288.8 290.7 291.0 291.9 292.9 294.5
9.7 7.6 5.7 5.4 4.5 3.5 1.9
50 25 12 16 25 50

285.5 287.2 287.8 287.5 287.7 288.5 289.5 290.5
10.9 9.2 8.6 8.9 8.7 7.7 6.9 5.9
50 25 5 12 14 25 50

296.44 ∇

274.2 279.8 282.5 284.1 282.9 283.9 285.3 285.9 287.7
10.3 7.7 2.0 0.4 0.6 0.6 +0.8 +1.4 +3.2
100 50 25 4 11 13 25 50

275.0 278.4 281.2 281.3 281.3 282.6 283.3 285.6
9.5 6.1 3.3 3.2 3.2 1.9 1.2 +1.1
50 25 7 10 13 25 50

274.2 276.3 279.1 279.5 279.5 280.5 282.1 285.9
10.3 8.2 5.4 5.0 5.0 4.0 2.3 +1.4
50 25 7 10 14 25 50

284.48 ∇

16+00.50 Fd. 3/4" Pipe 25' Rt on East P.L.
Set stub on R

15+50

T.P. 9.05 314.157 0.61 305.10

15+10 Fd 3/4" Pipe on West P.L.

15+00

14+50

14+00

± Fd 3/4" Pipe 25' R+E EC of No. line of Pavana on Quebrada

13+50

305.717

Lt

303.5 305.0 306.2 306.9 308.9 309.0 310.7
10.7 9.2 8.0 7.3 5.3 5.2 3.5
50 25 22 23 25 50

303.0 304.8 305.6 306.4 307.4 307.8 309.7
11.2 9.4 8.6 7.8 6.8 6.4 4.5
50 25 12 17 25 50

314.157

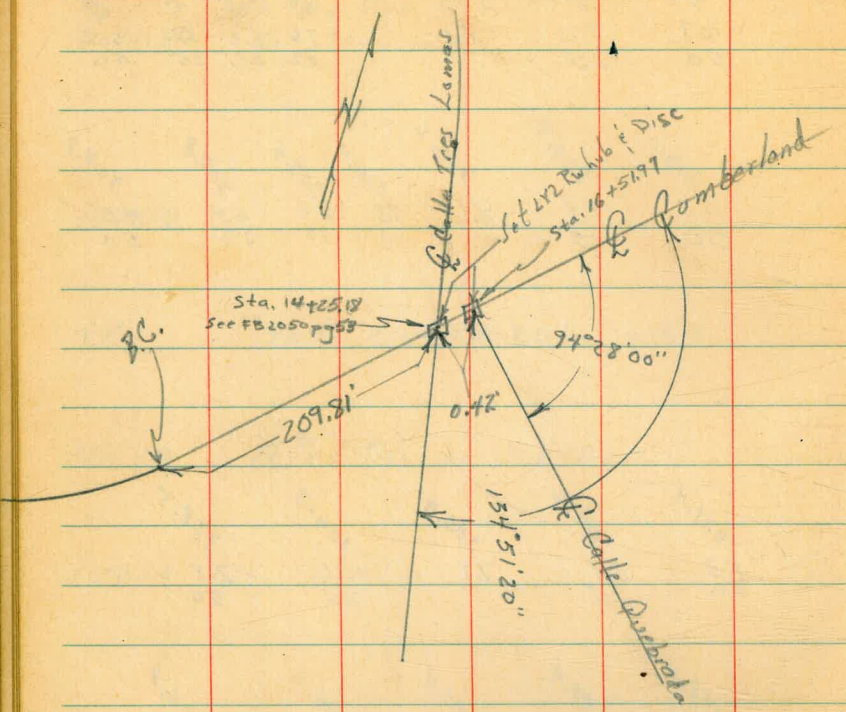
301.4 302.6 303.9 306.3 308.5
7.3 3.1 1.8 7.6 4.8
50 25 25 50

298.4 299.4 301.4 304.0 306.8
7.3 6.3 4.3 5.7 4.1
50 25 25 50

294.6 296.8 298.6 301.3 303.6
11.1 8.9 7.1 4.4 2.1
50 25 25 50

297.4 292.2 294.0 296.5 298.6 301.0
18.3 13.5 11.7 9.2 7.1 4.7
100 50 25 25 50

305.717



starting S.M.

check 9.94 304.21 = 304.18

Section 1 to 6 Quebrada

16+51.97 £ Cumberland Set Hub & Disc

16+27

314.15 7

303.5	304.2	305.0	305.4	305.9
10.7	10.0	9.2	8.8	8.3
50	25		25	50
303.5	304.3	305.0	305.7	306.4
10.7	9.9	9.2	8.5	7.8
50	25		25	40
				310.9
				46
				311.2
				50

314.15 7

Roberts
Cota
Shepard
6-21-51
No. 25020

X-Section Calle Tortuosa
From East Subd. Tres Lomas Line to
Calle Chanate (Full length) May 21 69

1796.58 EC $\frac{3}{4}$ " I.P. on West P.L. Set Stub on Q
Set 2XL Rwhub & City Disc on East P.L.

1750

INDEFINITE
JUN 22 1951

Reduced by
R. McLeod
6-22-51

1700

T.P. 1.35 334.19X 1.99 332.84

0+50

0+00 $\frac{3}{4}$ " I. Pipes on Both P.L. Set Stub on E
East Tres Lomas Subd. Line

T.P. 12.27 334.83X 0.11 322.56

T.P. 12.52 322.67 0.29 310.15

BM 10.61 310.44 299.83 $\frac{3}{4}$ " Iron

Lt

F

R

55

333.8
0.4
50
330.5
3.7
25
329.5
4.7
14
328.5
5.7
10
328.4
5.8
25
327.3
6.7
25
325.7
10.5
50

341.4
+7.2
50
336.9
+2.7
25
333.4
0.8
10
331.8
2.4
5
331.4
2.8
25
328.5
5.7
25
325.4
8.8
50

344.4
+10.2
50
340.5
+6.3
25
336.0
+1.8
9
334.3
0.1
6
334.5
0.3
25
331.0
3.2
25
327.0
7.2
50

334.19X

338.1
+3.3
50
336.7
+1.9
25
335.2
+0.4
8
333.0
1.8
5
332.9
1.9
25
331.3
3.5
25
326.9
7.9
50

336.0
+1.2
50
334.0
0.8
25
330.9
3.9
12
330.3
4.5
25
326.53
8.30
25
325.4
9.4
50
318.6
16.2
100

334.83X

El. P.L. on Tortuosa
Pipe S.W. Corner Tortuosa & Cumberland

Tortuosa
Cumberland
This is it!

4+50

T.P. 0.50 310.06 π 12.87 309.56

4+00

3+96.70 Fd 3/4" I. Pipes on Both RL. Knocked over Reset

3+50

3+00

T.P. 0.41 322.43 π 12.17 322.02

2+96.70 Fd 3/4" I. Pipes on Both RL. Knocked over Reset.

2+50

334.19 π

56

311.1	308.9	307.7	307.2	306.9	305.2	303.0	298.3
+1.0	1.2	2.3	2.9	5.2	4.9	7.1	11.8
50	25	15	11		25	50	100

310.06 π

315.6	314.3	312.0	310.9	311.3	308.3	307.0
6.8	8.1	10.4	11.5	11.1	14.1	15.4
50	25	12	10		25	50

318.2	314.6	312.6
7.2	7.8	9.8
25		25

323.9	322.2	321.7	319.8	319.7	317.3	314.3
+1.5	0.2	0.7	2.6	2.7	5.1	8.1
50	25	14	11		25	50

322.43 π

328.4	327.1	326.6	324.7	324.3	321.5	319.3
5.8	7.1	7.6	9.5	9.9	12.7	14.9
50	25	15	11		25	50

334.19 π

Cont'd From Page 56

7+06⁹⁵ BC Fd 3/4" I. Pipes on Both PL Set Stub on L

6+81

6+79

6+50

check

10.23 299.83 = 299.83

6+00

5+96.70 Fd 3/4" I. Pipes on Both PL.

5+50

5+00

310.067

305.1
5.0
50

303.4
6.7
25

301.7
8.4

299.8
10.3
25

297.6
12.5
50

57

302.2
7.9
50

301.1
9.0
25

299.7
10.4

297.5
12.6
25

296.1
14.0
50

298.9
11.2
50

297.6
12.5
25

297.0
13.1

296.1
14.0
25

295.2
14.9
50

295.9
11.2
50

297.9
12.2
25

297.1
13.0

296.3
13.8
25

295.9
14.2
50

301.5
8.6
50

299.5
10.6
25

299.1
11.0
14

295.3
11.8
10

295.3
11.8

296.9
13.2
25

295.9
14.2
50

305.6
4.5
50

304.4
5.7
25

303.0
7.1
13

301.4
8.3
9

301.4
8.7

299.5
10.6
25

298.7
11.4
50

307.6
2.5
50

305.6
4.5
25

305.1
5.0
15

303.9
6.2
10

303.9
6.2

301.9
8.2
25

299.6
10.5
50

310.067

10+00

9+50

9+00

8+26.84 EC

T.P.

8+00

7+50

T.P.

Fd 3/4" I Pipe on East Limb. Set Stub on E.
Fd 3/4" I. Pipe on west limb Knocked over. Reset.

6.06 318.75 ∇ 0.88 312.69

11.88 313.57 ∇ 8.37 301.69

310.06 ∇

LT E RT 58

319.3	315.5	313.1	311.1	310.3	307.6	302.4
+0.5	3.3	5.7	7.7	8.5	11.2	16.4
50	25	13	9		25	50

320.7	315.9	313.6	312.5	308.8	307.1
+1.9	2.9	5.2	6.3	10.0	11.7
50	25	10		25	50

321.1	317.5	314.5	313.7	310.7	306.7	299.4
+2.3	1.3	7.3	5.1	8.7	12.1	19.4
50	25	10		25	50	100

318.7	315.7	313.8	312.3	309.9	306.3
0.1	3.1	5.0	5.5	8.9	12.5
50	25	10		25	50

318.75 ∇

318.5	314.7	313.6	312.4	312.2	309.9	306.3
+4.9	+1.1	0.0	1.2	1.4	3.7	7.3
50	25	14	10		25	50

311.3	310.0	309.2	307.5	307.2	305.1	303.0
2.3	3.6	4.4	6.1	6.4	8.5	10.6
50	25	13	9		25	50

313.57 ∇

Contd From Page 58

T.P. 130 297.28 ∇ 10.90 295.78

13+00

12+50

12+00

11+50

11+00

T.P. 0.35 306.88 ∇ 12.22 306.53

10+50

318.75 ∇

24

25

26

59

305.4
1.5
50

300.7
6.2
25

298.9
8.0
15

296.5
10.4
10

296.2
10.7
10

293.0
13.9
25

287.4
18.5
50

304.3
2.6
50

301.0
5.9
25

299.5
7.4
15

297.3
9.6
10

296.3
10.6
10

292.9
14.0
25

289.3
17.6
50

305.5
1.4
50

302.1
4.8
25

300.7
6.2
15

298.9
8.0
10

298.2
8.7
10

294.5
12.4
25

292.2
14.7
50

283.3
23.5
100

307.8
+0.9
50

304.3
2.6
25

303.5
3.4
15

301.9
5.0
10

302.1
4.8
10

302.0
4.9
10

298.7
8.2
25

296.0
10.9
50

305.8
+6.4
50

306.7
+1.1
25

304.9
0.2
16

305.0
2.0
10

302.1
1.9
25

297.9
9.0
50

306.88 ∇

316.7
2.1
50

311.5
7.3
25

309.7
9.1
15

307.8
11.0
10

307.3
11.5
10

303.7
15.1
25

301.7
17.1
50

318.75 ∇

15+50

15+30

J.P. 6.11 296.99~~X~~ 6.40 290.88

15+00

14+50

14+00

13+57.52 BC Fd 3/4" I. Pipes on Both P.L.
Set Stub on R

29728~~X~~

LL

R

FR

60

298.6
+1.6 50
291.0
6.0 25
283.3
13.7
278.4
18.6 20
276.7
20.3 25
273.7
23.3 50

298.0
+1.0 50
294.5
2.5 43
292.7
1.3 25
289.1
7.9
277.4
19.6 25
275.0
22.0 31
272.3
23.7 50

296.99~~X~~

294.7
2.6 50
292.5
1.8 25
289.3
8.0
284.0
13.3 19
281.4
15.9 25
272.0
25.3 50

298.6
+1.3 50
292.3
5.0 25
286.0
11.3
282.5
14.8 25
276.6
20.7 50

300.6
+3.3 50
294.4
2.9 25
292.8
1.5 16
290.7
6.6 11
290.8
6.5
285.2
12.1 25
283.8
13.5 50

302.4
+5.1 50
297.9
+0.6 25
293.5
3.8 9
292.8
1.5
285.9
8.4 25
282.9
14.1 50

29728~~X~~

Check 7.04 299.79 = 299.83

T.P. 5.61 306.83 0.99 301.22

T.P. 12.55 302.19 7.35 289.64

16+22.58 Opposite PCC on Sly P.L. Ad 1/2 Pipe on Sly P.L.

296.99

301.3
+43
50

276.59
0.40
25
on
Pipe

284.5
12.5

282.2
14.8
25

275.0
22.0
50

296.99

R.R. Row.

2+07.37 = Nail
= POT. Fd.

IMPROVED
SEP 14 1954

± Culvert
Box - See
Notes

2+07.32 = Fd. Cop. Nail
POT.

14'
outlet Thru
cb
A.C. Drive

1+46 = P.R.C.

ASH

1+00

35' Dr.
0+65

7'

0+93

35' Drive

0+08

0+20 = Cross

0+20 = Fd. 1st
0+2 North

20' Rad.

See Plan
1937-L
for Improvements
Here

Pacific Hwy.

Kettner

Fd. 1st. See R

63
33

4+82.19
33'
Set P.K.

Blud.
Fd. 7ct

02

14'

26'

26'

14'

Drive

ASH

7'

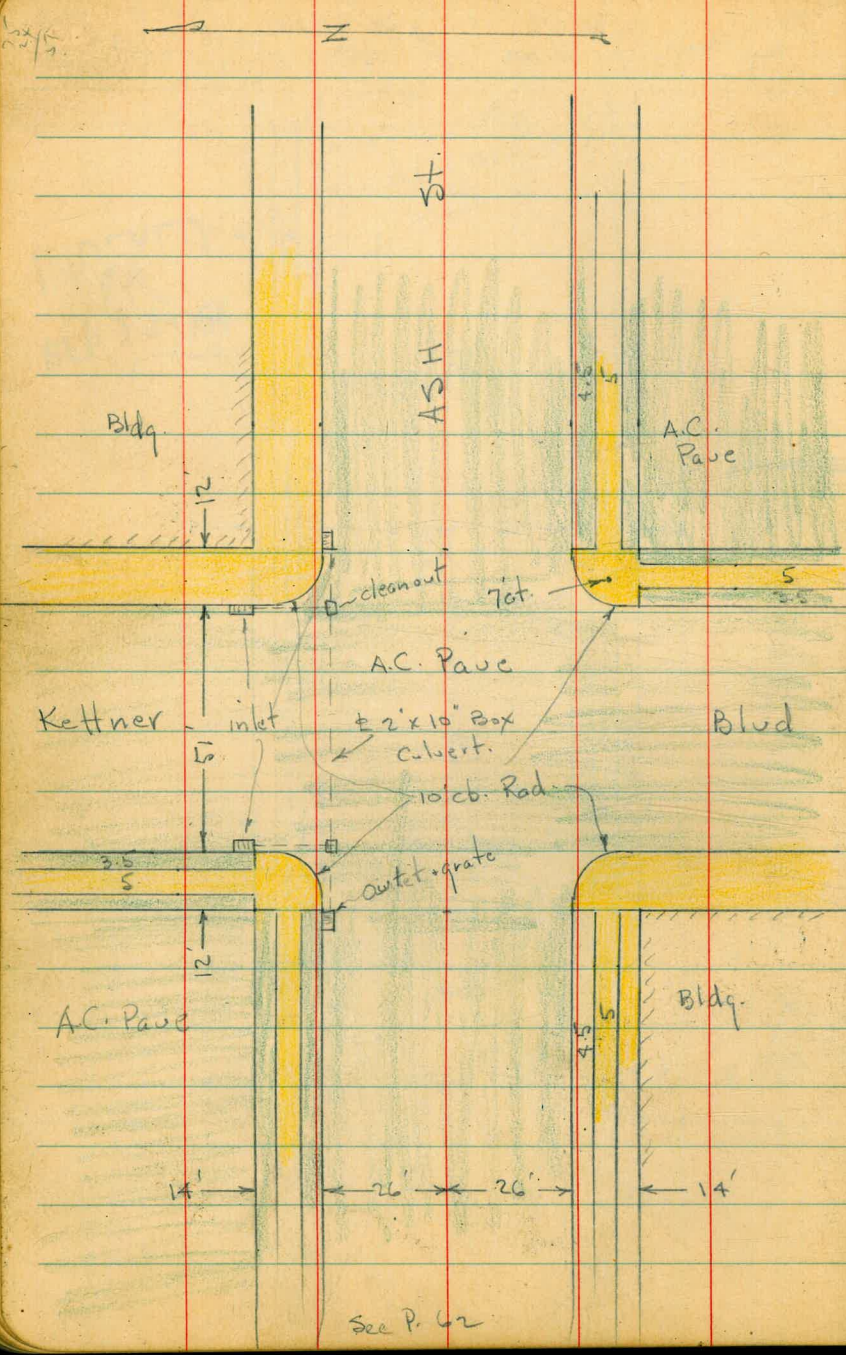
inlet in cb.

Box
± Culvert

15+20.1
2+00.76 = Disk
= POT.

R.R. Row.

See Notes for tracks.



51
21
75

See P. 62

X- Sect. ASH St. - from Pacific Hwy
to Kettner - Sketch - P. 62+63
W.O. 21270 - 9-10-54 - 7.0

- 0-05.8' - 36.8' Lt. = ± Clean out - Sec 7937-L
- 0-05.5' - 41.8' Rt. = ± F.H.
- 0-05.8' - 45.2' Rt. = ± Pull box (w.M. Box size)
- 0-06.1' - 60' Rt. = ± Light std.
- 0-06.1' - 53.5' Rt. = ± 2.8x1.6 Conc. base - for Cont. Box - (Traffic)
- 0-06.1' - 50.8' Rt. = ± 3' st. sign
- 0-06.5' - 47.1' Rt. = ± P. pole # P-1399
- 0-07.9' - 0.4' Lt. = ± of Nose of Island - 2' Rad.

0-08 - Conto

0-08 = F. cb. Line of Pac Hwy.

4.43
Top

3.90	3.70	3.66	3.67	3.74	3.74	3.66	3.52	3.43	3.50	3.99
90	58	40	33	15		15	33	40	46	Top
gut	PC in Dr.								gut	PCI

0-18

4.38	4.29	4.14	4.16	4.12	4.08	4.00	3.97	3.95	3.93	3.90
90	60	40	33	15		15	33	40	60	90

Set B.M. on 0+20 ct. on S. 7 line 4.61

B.M. = S.W.B.P. - Ash + India 22.97

Lt.

#

Rt.

64

364

36.8 = Rim - west
Mt.

3.42	3.97	3.22	3.80
60	Top	90	Top
gut.		gut	

Actual Elev. Shown.

0+52 - 27.5' Rt. = \pm Deadman

0+45.1 - 34.6' Lt. = \pm Tel. pole

0+40 - Conts

0+40 - 39.7 Rt. = Beg. ^{Behind walk} County Bldg. + end Conc.

0+17 = P.C. of 25' Rad. on N.

0+12 = P.C. of 20' Ret. on S.

0+07.5 - 34' Lt. = \pm St. sign

0+06 - 28.7 Rt. = \pm Signal Post (flush Base)

0+05 - 21' Rt. = \pm Sewer M.H.
 -2.66 = I.F.
 4.20 = S. Rim

0+00 Cont

0+00 = E.L. Pacific Hwy

0-00.4 - 10.1 Rt. = \pm Water gate Cap.

0-02.2 - 18.4 Lt. = \pm Light + Traffic signal Post.

0-05.3 - 0.4' Lt. = \pm Signal Post.

Lt. \pm Rt. 05

5.48	4.74	5.37	5.46	5.92	5.46	5.21	4.62	5.01	5.12
40.4	33.3	15	1.5		0.6	15	25.9	Top	33
	gut. in Dr.		Toe	island	Toe		gut.		walk

8.29
40 =
Conc. at
Cor. of Bldg.
4.56
33
walk
4.74
40 = Conc.

4.86	4.03	4.69	4.90	5.32	4.80	4.45	3.95	4.43
40.4	33.3	15	2			15	25.9	Top
edge walk	in W		Toe	island	Toe		gut.	

4.37
Top
3.86
gut.
25.9

4.72	4.63	4.37	3.44	4.28	4.34	4.31	4.17
90	60	Top	40	29.5	40	60	90
		cb.	on Grate	Top cb.			

3.50	3.60	3.90	4.09	4.60	3.96	3.84	3.71	3.72
27.5	33	15	2.3	0.45 of \pm	1.5	15	26	29.5
edge of Inlet Box			Toe of island	of Island	Toe of Island			gut.

Lt.

±

Rt.

16

1+69- 29' Rt. = ± Pullbox

1+68.9- 35.4' Rt. = ± 8.4' Conc. Slab - was to door
Not - Needed now

1+61.5- 31.4 Lt. = ± 4x4 Sign Post.

1+56- 28.5 Rt. = ± 3x4 Sign Post.

1+46 = P.R.C. of cb. on N. - 37' Lt. = ± W.M.

1+42- 56.7' Lt. = Beg. Bldg. (Note: front Moved back)

1+32- 27.5' Rt. = ± W.M.

1+37- end Dr. on Lt.

1+14- 40.3' Lt. = end Conc wall & fence

1+12.3- 27.5' Rt. = ± 4x4 Auto Club sign

1+12 = Beg. Dr. on Lt

1+09 = B.C. of cb. on N.

1+00- 40.3' Lt. = Cor. of 8' Conc wall & 7' Cyclone fence

0+85- 35.4' Rt. = ± 8.3' Conc. Ramp to Door in Bldg.

0+75

0+73- 27.9' Rt. = ± P. pole # 865

0+64.5- 27.5' Rt. = ± 4x4 R.R. Sign Post.
(Ditch Shows line across str.)

0+61.1- 36.1' Rt. = ± 33x18 Bell Syst M.H.

0+55.8- 28.5' Rt. = ± 4x4 Sign Post.

0+52.2- 0.5' Lt. = ± Nose of island - 0.8' Rad.

8.8	8.54	8.78	8.09	8.52	8.64	8.33	7.85	8.31	8.50	8.80
40	35.6	Top	29.8	15		15	25.9	Top	33	39.9
	edge of walk		gut.				gut.			A.C. by Bldg.

7.77	7.56	6.86	7.43	7.51	7.19	6.71	7.16	7.36	7.09
39	Top	33.2	15		15	25.8	Top	33	39.8
edge of walk	= PC	gut.				gut.		walk	A.C. by Bldg.

6.73	6.98
35.4	39.8 = at Bldg.
Conc.	

6.53	5.80	6.43	6.55	6.17	5.68	6.12	6.23	6.64
40.3	33.2	15		15	28.9	Top	33	39.7
edge of walk	gut. in Dr.				gut. =			A.C. by Bldg.
					I.E. of 3" CI. Root Drain			

5.86	6.22
Top	0.8
	Top
	end Island

9.11 - T.P.
 Ang. Pt. in \pm of Culvert - 2.7 x 0.7' to E.
 2+14.8 - 24.1 Rt. = \pm of Std. M.H. Cleanout to
 2+05.8 - 25.2 Lt. = ^{Approx.} Ang. Pt. in \pm of Culvert.
 2+02.2 - 0.6 Rt. = \pm Sewer M.H. 10.53 = S. Rim
 - 40' Rt. end bldg. + 56.5' Lt. = end bldg.
 Note: Part of Ret. on N. side
 2+00.4 = end of cbs. + face of Ret. to prop
 2+00.2 - 32.4 Rt. = approx. Ang. in \pm of Culvert.
 1+98.5 - 27.8 Rt. = \pm P. pole # P 801 - B.M. = 10.61
 1+97.8 = 27.2 Lt. = \pm Tel. pole
 1+97.6 - 30.6 Lt. = ^{approx.} Ang. in \pm of Culvert - 2.7 x 0.7' High
 - 2.03 = I.E.
 1+97.2 - 0.6 Rt. = \pm Sewer M.H. 10.37 = S. Rim
 1+94.2 - 28.2 Rt. = \pm 2.5 x 2.5 Conc. base for R.R.
 = Box - 2.7 x 0.6 High -
 1+92.3 - 32.4 Rt. = approx. Ang. Pt. in \pm of Culvert.
 1+86.7 - 26.1 Lt. = \pm cb. outlet 7.5' long - 5' High
 1+83.5 = B.C. of cb. on N.
 25.9 Rt. 0.5' High - 7.5' Long.
 1+78.7 = \pm of 7.5' opening = outlet Thru cb.
 1+76.5 - 36.8 Lt. = \pm Bell M.H. 9.77 = S. Rim
 1+74 - 28 Rt. = \pm W.M.
 1+69.5 = 2.2 Lt. + 12 Lt. = \pm of Traffic Detectors

87
 Lt. \pm Rt.
 10.78
 24.1 = Rim
 8.78 = I.E. of Culvert.
 10.8 10.60 10.51 10.55 10.54 10.50 10.24 10.04 9.98 10.14 10.22
 40 33 26.1 25 15 15 22.8 26 33 = cb. 40 =
 on A.C. end of cb. + end of cb. end of cb. + AC. + AC. end
 cb. + walk AC. cb. cb. got. cb. at Cor. of
 bldg.
 9.16 10.06
 Int. = Top cb.
 I.E.
 10.1 9.99 9.90 9.16 9.75 9.88 9.49 8.70 9.47 9.68 9.98
 40 33 Top 26.1 15 15 25.9 Top 33 39.9 =
 got. got. AC. out
 bldg.
 8.58 9.36
 Int. = Top cb.
 I.E.

2+82.7 - 28.4' Lt. = ± of 2.5' x 2.5' RR. signal
 base for
 2+79.9 - 27.5' Lt. = ± RR. Rail iron Signal Guard.
 2+78.8 - 27.2' Lt. = ± 8" x 8" post - 4' High
 2+73.1 }
 2+68.4 } = spur Track
 2+67.1 = E. Rail
 2+62.3 = W. Rail = Main track
 2+53 = E. Rail
 2+48.3 = W. Rail - Main Track
 +24.6' Rt. = 2.7' x 0.7' Box Culverts
 2+41.1 - 24.7' Lt. = ± of 1.8' x 1.8' Clean out to ± of
 2+38 = E. Rail
 2+33.3 = ^{w.} Rail - spur track
 2+20

Lt.	±	Rt.	
11.98 40			
11.92 40	11.95 40	11.83 = spur	
	2+69.2	11.83	11.53 40
11.93 40	2+64.5	11.85 = spur	
		11.82	11.55 40
11.94 40		11.80	11.52 40
11.93 40		11.82	11.55 40
9.37 I.E.	11.85 = Rim 24.7	11.59 24.6 Rim	9.06 I.E.
11.89 40		11.68 on Rail	11.43 40
11.87 40		11.70 on Rail	11.46 40
11.44 40	11.46 33	11.44 15	11.35 15
edge A.C.		11.20 15	11.13 33
			11.12 40 = edge A.C.

3+342 - 277' Lt. = ± P. pole # 780

3+33 - 30' Rt. = approx. Ang. in ± of culvert.

3+30 - 27.5' Rt. = ± P. pole # 735

3+25.7 - 40' Lt. = Beg. Bldg.

3+21.5 = Beg. cb. on S.

3+20.6 - 30' Rt. = approx. Ang. in ± of culvert

3+20.6 = Beg. walk on S.

3+15 - 24.6' Rt. = approx. Ang. in ± of culvert.

3+14.5 - 26' Rt. = end. cb.

3+11.5 - 26' Lt. = ± of 8' x 0.6' inlet thru cb. = culvert

3+04 - 27.6' Lt. = approx Ang. in ± of Culvert.

3+00.2 = beg. obs. & walk on N. - 3+00.76 - ^{Row.} edge of

Culvert, 30" x 9" - Joins reg. Culvert.

2+98.5 - 40.1' Lt. = ± of inlet of Cor. Iron Arch

2+98 - 24.7' Lt. = approx. Ang. in ± of Culvert.

2+96 - 27.2' Lt. = ± 6" x 8" post.

2+92.5 - 27.2' Lt. = ± 6" x 8" post. 4 High

2+88.5 - 27.2' Lt. = ± 6" x 8" post.

2+85.5 - 27.3' Lt. = ± RR iron guard

2+85

Lt.

±

Rt.

69

12.81 40 on A.C.	12.75 33	12.60 Top	12.05 26.1 gut.	12.49 15	12.58	12.22 15	11.85 26 gut.	12.00 Top	12.22 33	12.28 40 on A.C. RR parking
------------------------	-------------	--------------	-----------------------	-------------	-------	-------------	---------------------	--------------	-------------	--------------------------------------

12.36 Top cb.	11.33 26 = I.E. gut.
---------------------	-------------------------

11.90
26 = Top + A.C.

12.39 40.2 end cb. + A.C.	12.27 33 cb. + A.C.	12.16 26 cb.	12.17 15	12.16	11.91 15	11.66 25.9 = Cor. cb. + A.C.	11.67 33 cb. + A.C.	11.77 40 = end cb. + A.C.
---------------------------------	---------------------------	--------------------	-------------	-------	-------------	------------------------------------	---------------------------	------------------------------

11.22
40.1
I.E. of
inlet

12.09 40 edge A.C.	12.02 33	12.02 15	11.94	11.81 15	11.65 33	11.53 40 edge A.C.
--------------------------	-------------	-------------	-------	-------------	-------------	--------------------------

4+25.5 = end Dr. on S.

4+21.2 - 28.8' Rt. = \pm W.M.

4+16.5 - 28.1 Lt. = \pm 4x4 Traffic sign

4+04 - Beg. Conc. Dr. on S.

4+01.8 - 28.6' Rt. = \pm 2" Tank inlet - Gasoline?

4+00

3+97 } planting - shrubs - along Bldg. on S.
3+84 }

3+84 = end Dr.

3+83.5 - 26.1' Lt. = \pm 4" UC Drain thru cb.

3+76.8 - 26' Rt. = \pm 6" Iron Drain Thru cb.

3+75.3 - 40' Rt. = Beg. Bldg.

3+71 - 27.6 Rt. = \pm Gas Valve Cap

3+63 - 28.1 Rt. = \pm Dead man \rightarrow 3+75 = Sect.

3+58.8 - 40' Lt. = end Bldg.

3+58.5 - 27.7 Rt. = \pm 14x4 Traffic Post.
Drive

3+52 - 26.1 Lt. = \pm 4" UC pipe Drain + Beg. Conc.

3+50 = wly. of 3.3 Conc. walk from back of
Req. walk

3+48.7 - 27.6 Rt. = \pm W.M.

3+46.3 - 27.7 Lt. = \pm 3"x4" Traffic sign

3+43.7 - 27.1 Lt. = \pm 3/4" Cappel Vert. pipe
Inlet in cb.

3+38 - 26' Rt. = \pm of 4' Long 0.5' High opening

Lt.

\pm

Rt.

70

14.75	14.68	14.50	13.75	14.33	14.39	14.00	13.25	13.70	14.01	14.2
40	33	Top	26.1	15	15	15	25.9	Top	33	40
A.C.			gut.				gut.			

13.46
26.1' =
I.E. of
Drain

12.55 = I.E. of
Drain

14.18	14.14	13.90	13.32	13.77	13.82	13.37	12.65	13.12	13.46	13.4
40	35.5	33	26	15	15	15	25.9	Top	33	40
Conc.	Bk.		gut-in	Dr.			gut.			

12.72
26.1' = I.E.
of Drain

13.72	13.47	13.35	12.74	13.19	13.26	12.74	12.11	12.64	12.86	12.91
40	33	Top	26.1	15	15	15	25.9	Top	33	40
on A.C.			gut.				gut.			walk

11.60
26' I.E.
= gut. Top cb.

5+12.5 - 38.7' Rt. = \pm Sewer M.H. Top Covered.

5+12

4+98.5 - 17' Rt. = \pm 4" Gas Co. M.H. 16.44 = \pm

4+95

16.97
80

4+85.2 - 40.6' Lt. = \pm 3" St. sign

4+85.5 - 39.9' Rt. = \pm Signal Post

4+85 - 43' Rt. = \pm P. pole # 1398

4+87.2 - Cont.

40.3' Lt. = sly. of 4' x 2.6' Inlet + grate
Box Culverts

4+87.2 = w. cb. + 24.9' Lt. = \pm 1.8' x 1.8' cleanout to 2' x 10'

Set B.M. = SW 7' ct. ✓

15.55

check B.M. = NW B.P. ✓

16.21

16.15

-45' Rt. - end Bldg. + grate

4+75.19 = w.l. of Kettner Blvd. + Fly of 4' x 22" outlet

4+74.5 - 27.8' Lt. = \pm Light Std. - Signell

4+65

4+60 - 27.7' Lt. = \pm 4' x 4' R.R. sign

4+55.5 - 28' Lt. = \pm Pipe pole # J.P. 702

3.2 Long x 1.8 wide

4+45 - 38.5' Lt. = \pm Bell M.H. 15.79 sly. Rim

4+35

4+30.5 - 27.9' Lt. = \pm Deadman

4+30 - 27.5' Rt. = \pm 4' x 4' Traffic sign

Lt. \pm

Rt

71

17.96 17.60 17.40 17.31 17.23 17.08 16.87 16.64 16.51 16.45 16.39 16.30 16.17
80 53 40 33 26 15 15 26 33 40 53 80

16.71 16.74 16.74 16.70 16.72 16.58 16.30 15.92 15.74 15.62 15.47 15.29
53 40 33 26 15 15 26 33 40 53 80

16.78 16.37 16.50 16.00 15.96 15.44 14.87 15.26
Top gut Top gut gut Top 80 gut Top

15.15 16.31 16.30 14.92 16.34 16.51 16.43 15.98 15.36 15.14 15.48 15.10 15.53
IE. 40.3 33 IE. 24.9 15 15 26 33 Top 40
gut Top cb. Top of outRet. gut Top
+ Inlet cleanout

Book

Rim - 16.05
IE - 10.19

16.58 16.43 16.25 14.94 16.15 16.13 15.87 14.92 15.49 15.65 15.80
40 33 Top 26.1 15 on Sewer 15 gut 25.9 33 40
cb. + Inlet gut = IE. on Sewer M.H. Top Conc

16.30 16.20 15.97 14.97 15.29 15.91 15.90 15.33 14.78 15.30 15.43 15.64
40 33 26 gut. 24 10 15 25.9 Top 33 40
A.C. Top Conc

15.61 15.52 15.32 14.63 15.12 15.20 14.72 14.17 14.63 14.80 15.00
40 33 Top 26 15 15 25.9 Top 33 40
on Alc. gut Conc

6+15.2 = \pm of 24.5' Conc. Dr. on Lt.

6+11 = \pm of 17' Conc Dr. on Rt.

5+99.7 - 27.3 Lt. = \pm 4x4 Traffic Post.

5+90 = end

5+68.7 = E. end of inlet

5+63.7 - 26 Lt. = W. & N. of 5'x2' Inlet + grate

5+51.2 - 27.6 Rt. = \pm Signal Post.

5+50.5 = 35.4 Lt. = \pm Bell Co. MH

5+50.19 = E.L. Kettner

5+50 - 27.4 Lt. = \pm Tel. Pole # 93781H

5+40.4 - 47.4 Rt. = \pm F.H.

5+40 - 40.8 = \pm Signal Post

5+38.2 - Cont.

Inlet + grate

5+38.2 = E. cb - 40.1 Lt. = Sly. & Fly. of 5'x2'

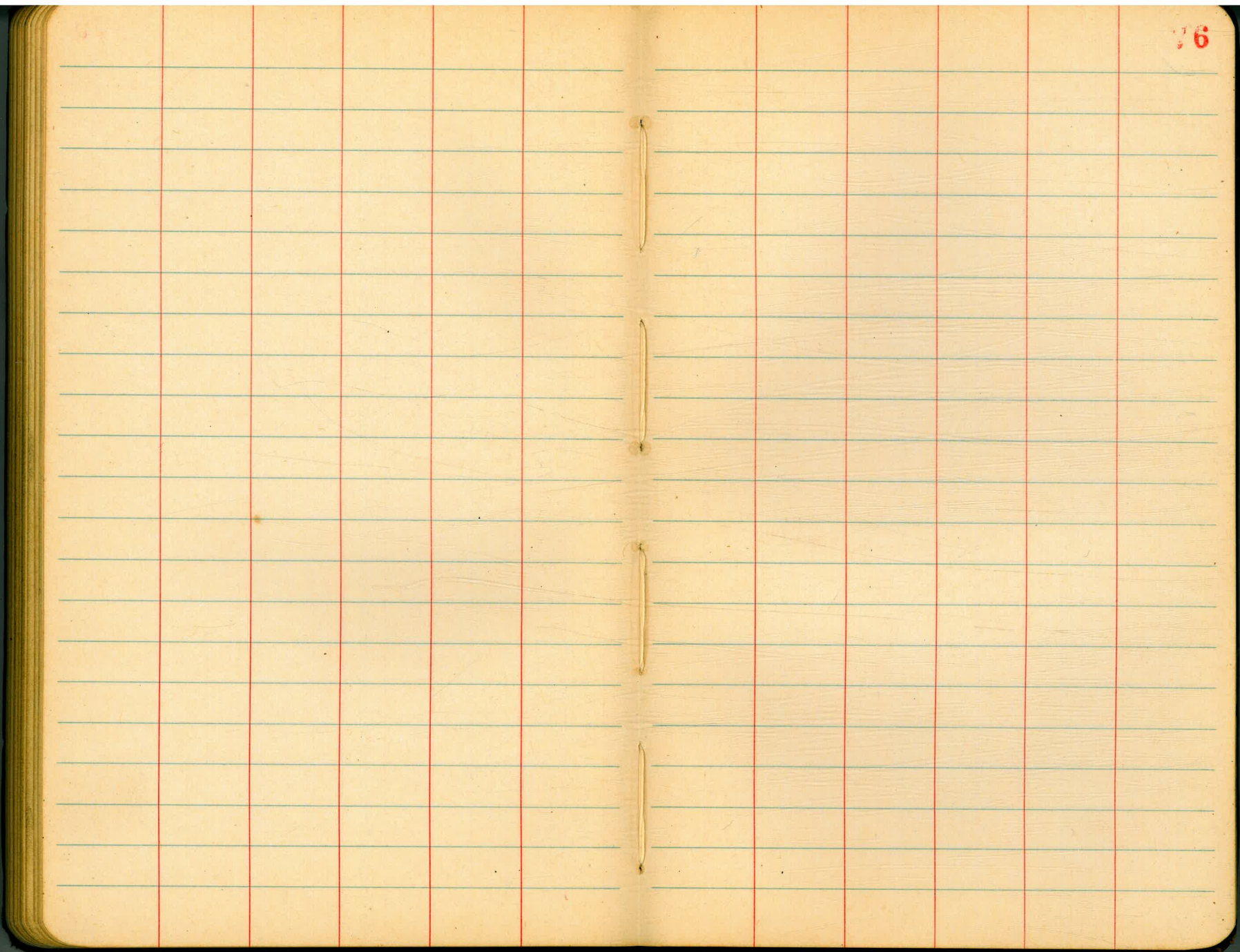
Colvert

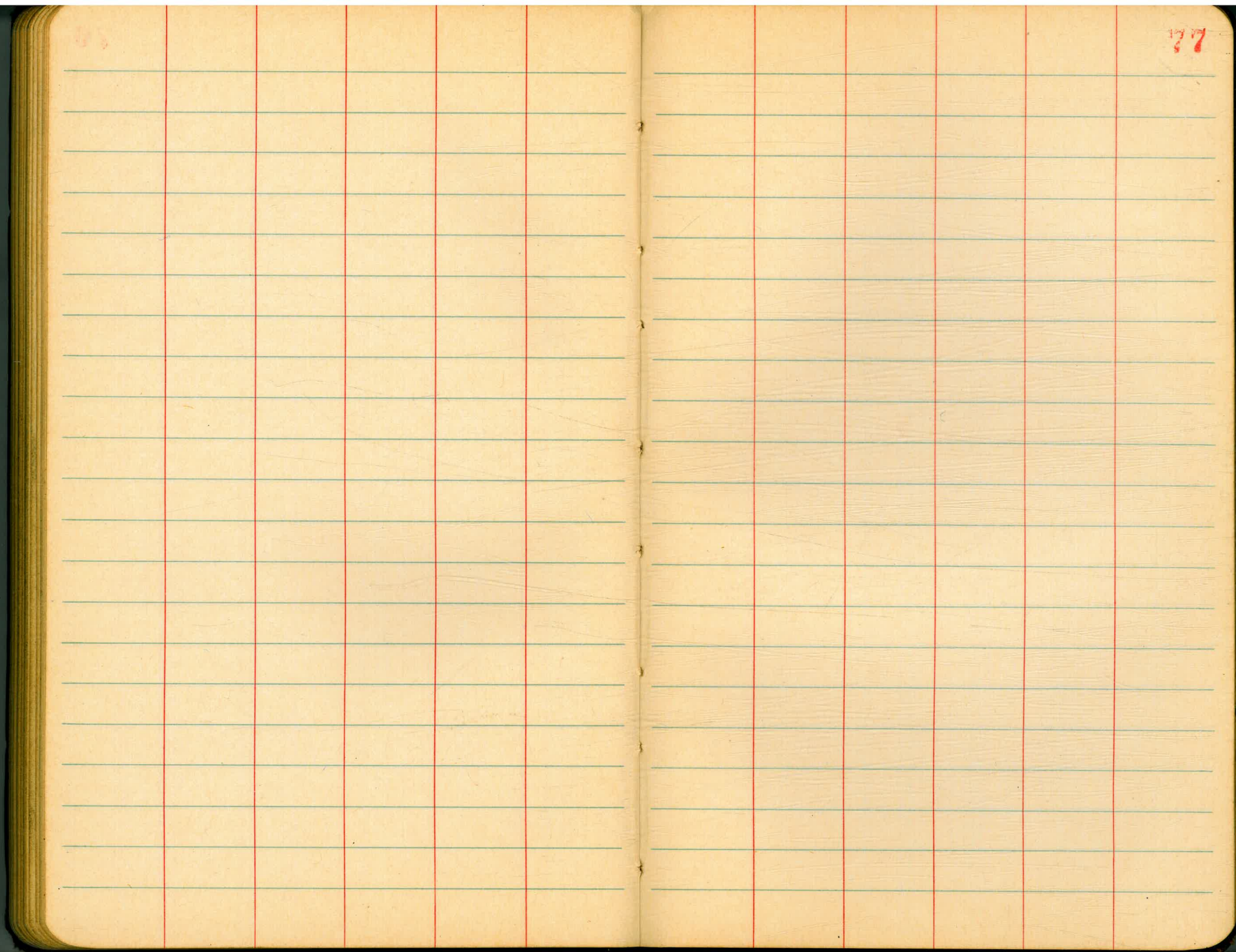
5+37.2 - 24.6 Lt. = \pm 1.8' x 1.8' cleanout = \pm 2' x 10' Box

5+27

18.05
80

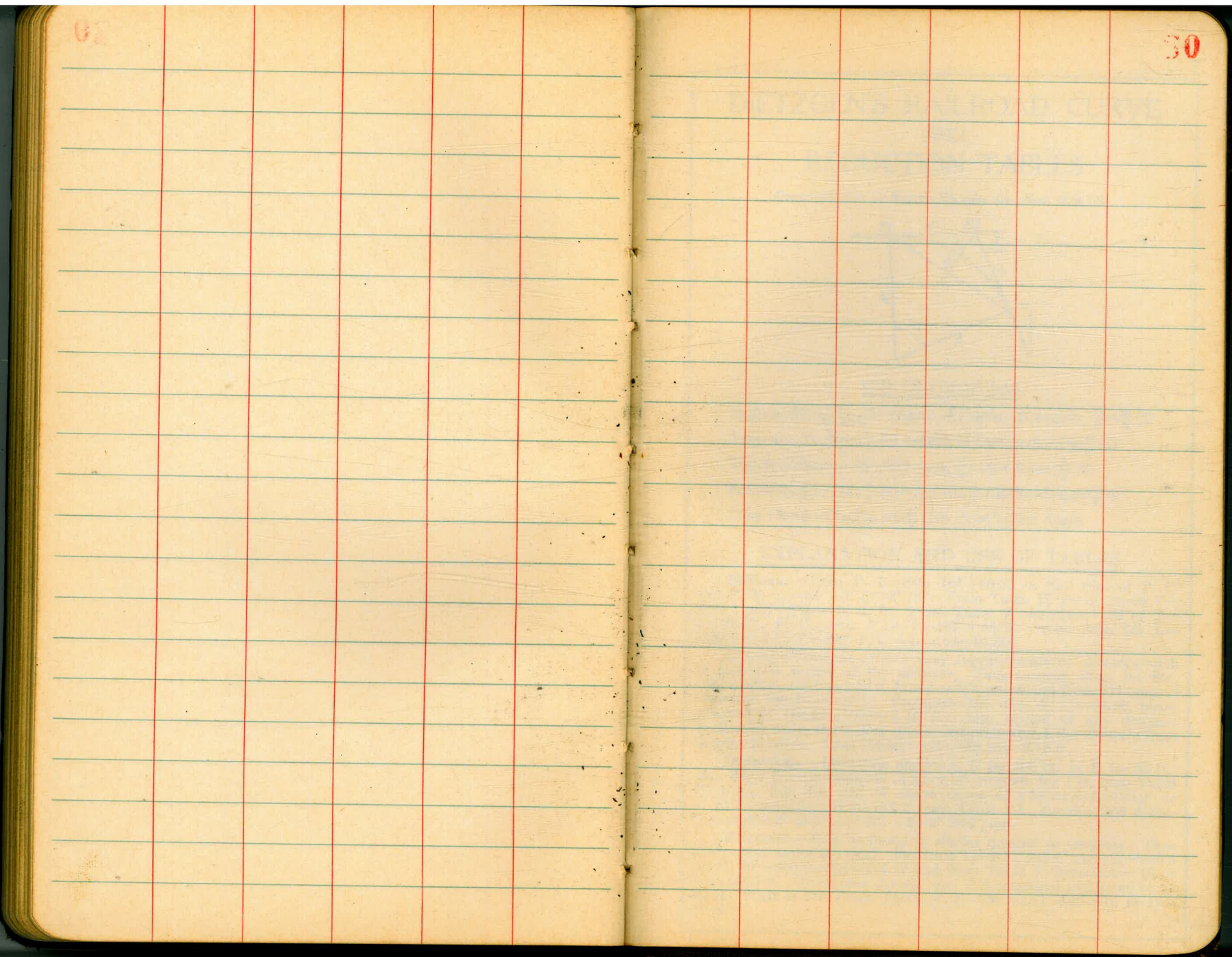
	Lt.	\pm	Rt.	72
20.62 40 Conc.	19.84 33	19.17 26 gut. in Dr	18.37 26 gut. in Dr.	18.96 30.5 walk
19.02 33 walk	18.99 40 AC			
19.49 40 Conc.	19.17 33 walk	19.00 Top	18.40 26 gut	18.71 15
18.65 15	18.33 15	17.74 26 gut	18.19 Top	18.42 33 on AC
18.52 40 AC				
18.26 Top	17.71 26 gut.	17.96 20		
	16.72 I.E.	18.12 26 Top cb inlet	17.97 15	17.96 15
			17.53 15	16.95 26 gut.
				17.40 Top
18.33 40 Conc.	17.92 Top	17.86 26 gut	17.66 15	17.56 15
			17.13 15	16.59 25.9 gut.
				17.04 Top
				17.37 40
		18.48 Top	17.73 80 gut.	16.22 53 gut.
				16.92 Top
				16.0 80 gut.
				16.79 Top
18.14 Top	17.45 53 gut	16.80 I.E. gut.	17.96 40.1 Top Inlet.	17.55 26 15
				17.45 15
				17.24 15
				16.87 15
				16.54 26 gut
				16.37 40 Top
				17.01
		17.50 Top	16.15 24.6 = I.E.	
	17.73 53	17.66 40	17.39 26	17.29 15
				17.04
				16.76 15
				16.62 26
				16.44 40
				16.37 53
				16.27 80





77

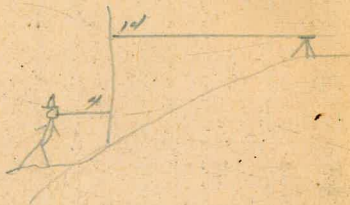
The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Vertical red lines create margins on both pages. The right page has the number '78' printed in red in its upper right corner. The notebook is bound in the center, and the pages are otherwise blank.



walks

196.3
53.7

4



DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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