

W. H. BROWN
1850

W. H. BROWN
LEVEL BOOK

No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
Copyright, 1914, by Eugene Dietzgen Co.

1833

B.M. 2 x 2 Hub

7.17 = 0400 - 1821 - 9

Napier

INDEXED
Completely

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Sewers Bayside V.L.
 Main trunk sewer
 on Frankfort St
 (2' west of E) From
 Napier to Littlefield

Sketch F.B. 1821

+50

INDEXED
 MAR 11 1948

W O 3147X

0+83 S.E. Cor House This sewer lat.
 can drop to
 Napier
 Line

+50

0+00 2x2 Hub @ Napier St.

B.M.
 NW B.P. 585 (L1.01)
 Frankfort
 NAPIER

Rec.
 55.16 55.13

LT 2
 Moore
 899
 Green
 Roberts
 1-27-48

Sewer

177

1

65.6

+4.5

55
 F.L.E.L.

61.7

+0.7

55
 9nd.

56.0
 49

56.0

5.0

56.0 53.2 53.9 51.0

5.0

7.7 7.1 10.0

54 dirt 89 Back
 Line 89
 House
 F.L.E.L.

56.0

5.0

56.0

4.6

(L1.01)

+29 2 Gar. same house

3

+75 NW Cor house

+50

House to 2nd is high
+36 NW Cor house

2

1764 SW Cor gar. & House

6101

27th

56.6 ✓
4.4

56.7 ✓ 19th
4.6
53
FL. EL.

2

56.4 ✓
4.6

56.4 ✓ 59.0 ✓ 50.8 ✓
4.6 4.0 10.2
8.4 8.4
FL. EL. 9th

56.3 ✓
4.7

65.0 ✓ 61.0 ✓ 56.3 ✓ 59.0 ✓ 50.5 ✓ 48.8 ✓
+4.0 0.0 4.7 4.0 10.5 12.2
FL. EL. 55 91 91 120
W. House 9th FL. EL. Main 9th

56.2 ✓
4.8

56.1 ✓ 53.0 ✓ 51.3 ✓ 49.8 ✓
4.9 8.0 9.7 11.2
75 75 100
FL. EL. 9th 9th

6101 ✓

53.6
7.4
FL. EL.
House

L

E

R

4+60 E Gar. same house

+50

4+3015 = 20 or TEN ST to EAST

T.P. 650 <L3.27> 424 <5677>

4+24 NW Car house

3+50 House to LT 15 high



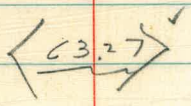
57.1^v
9.7

55.0^v
8.3
71
FL.EL. gar.

57.3^v
6.0

57.9^v
6.0
9rd
56.80^v
6.7

"2x2"
ON HUB

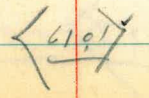


57.2^v 58.3^v 58.6^v
3.8 2.7 7.X
80 80
FL.EL. 9rd

57.1^v
3.9

56.6^v
4.4

60
FL.EL. 9rd



6 E gar + house $\begin{matrix} 58.1 \\ 5.2 \\ \hline \text{FL. CL. of house} \end{matrix}$

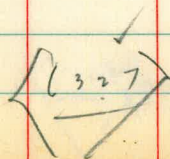
+73 NW Cor House

+69 SW Cor House + gar. in rear of house

+50

+16 SW Cor House

J
same
K + 80 E gar.



LT

$\begin{matrix} 63.8 \\ + 0.5 \\ \hline 58 \\ \text{FL. EL.} \end{matrix}$ $\begin{matrix} 61.1 \\ 2.7 \\ \hline 58 \\ \text{7rd} \end{matrix}$ $\begin{matrix} 57.6 \\ 57 \end{matrix}$

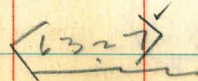
$\begin{matrix} 57.6 \\ 57 \end{matrix}$ $\begin{matrix} 58.0 \\ 5.3 \\ \hline 58 \\ \text{FL. EL.} \\ \text{House} \end{matrix}$ $\begin{matrix} 55.7 \\ 7.6 \\ \hline 58 \\ \text{8rd} \end{matrix}$ $\begin{matrix} 55.4 \\ 8.1 \\ \hline 110 \\ \text{FL.} \\ \text{gar} \end{matrix}$ $\begin{matrix} 53.9 \\ 9.2 \\ \hline 130 \\ \text{FL.} \\ \text{area} \\ \text{cesspool} \end{matrix}$
AND TANK + CESSPOOL
IN REAR OF GARAGE

$\begin{matrix} 57.6 \\ 5.7 \end{matrix}$

$\begin{matrix} 57.4 \\ 5.9 \end{matrix}$ $\begin{matrix} 51.8 \\ 5.5 \\ \hline 51 \\ \text{FL. EL.} \end{matrix}$ $\begin{matrix} 54.7 \\ 8.6 \\ \hline 51 \\ \text{8rd} \end{matrix}$

$\begin{matrix} 57.4 \\ 5.9 \end{matrix}$

$\begin{matrix} 57.3 \\ 6.0 \end{matrix}$ $\begin{matrix} 55.4 \\ 7.9 \\ \hline 60 \\ \text{FL. EL.} \\ \text{gar} \end{matrix}$



$\begin{matrix} 57.5 \\ 5.8 \end{matrix}$ $\begin{matrix} 56.5 \\ 6.8 \\ \hline 9.2 \\ \text{FL. CL.} \end{matrix}$ P. 541 ✓ 4
125
9rd

8

7+50 SW Cor + house gar in rear with Wash Trays

T.P. 413 <61.12> 628 <56.99>

+50 House on LT

7

6+90 SW Cor house and gar. in rear Wash Trays

+50

<63.27>

LT

R

R

5

56.5 ✓
4.6

56.7 ✓ 53.1 ✓ 57.4 ✓ 52.8 ✓
4.4 8.0 2.7 8.3
93 73 108
gar. house gar. floor FL.

<61.12>

62.5 ✓
0.8 56.7 ✓
50 66
F.L.E.L.
house

57.0 ✓
63

60.4 ✓ 57.0 ✓ 57.9 ✓ 55.3 ✓ 54.9 ✓
2.9 5.4 8.0 8.4
60 90 90 117
F.L.E.L. house gar. FL.
house at Tray

58.1
52

<63.27>

11 + 00

+50

10 Gar. S. side house

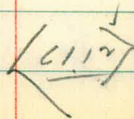


+67 NW Cor house

+50

9

8 + 50



L+

55.8 ✓
53

17

6

55.9 ✓
57

56.1 ✓
50

56.4 ✓
4.7
20
gar. FL.

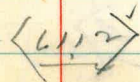
56.1 ✓ 57.4 ✓ 54.1 ✓
50 3.7 7.0
80 80
FL. FL. 9rd

56.1 ✓
50

56.3 ✓
4.8

49.1 ✓
12.0
130
9rd

56.3 ✓
4.8



12 + 62 Sep. Tank IN FRONT of house

+50

12 + 30 N.E. Cor house gar. in rear
and SL garage

T.P. 887 $\langle \underline{65.18} \rangle$ 481 $\langle \underline{56.31} \rangle$

14

11 + 50

check to N.W. B.P. BM Rec.
FRANKFORT + ASTON 546 55.26 $\underline{55.13}$
003

11 + 09.63 2 ASTON

$\langle \underline{61.12} \rangle$

Lt ✓
62.7
3.0
83
9rd.
TOP TANK

56.8 ✓
8.4

56.5 ✓
8.7

56.3 ✓ 58.4 ✓ 54.3 ✓
8.9 $\frac{6.8}{20}$ 10.9
FL. EL. House FL. EL. GAR.

$\underline{65.18}$ ✓

55.8 ✓
5.3

55.5 ✓
5.6

55.6 ✓
5.5
9rd.

$\langle \underline{61.12} \rangle$

Rt

17

15+30 gar. + Wash ROOM

15+00

Note! 5 houses in
this block on LT.
will show off alley as
Tanks are in rear and on
ctr. of houses

+50

+23 SE Cor house

14

+70 House on LT, will show
off alley sewer

+49 NE Cor house + S.L. gar.

13+00

<65.8>

LT

8
62.0 ✓
3.2

8
61.9 ✓
0.3
75
FL. EL.

8

61.6 ✓
3.1

60.8 ✓
4.4

60.4 ✓
4.8

61.9 ✓
3.3
5.5
House

60.1 ✓
5.1
6.9
gar. FL.

59.7 ✓
5.5

Tank ctr of house
in rear

58.4 ✓
6.8

60.8 ✓
4.4
5.7
FL. EL.
House

57.2 ✓
8.0
6.7
gar. FL.

57.5 ✓
2.7

<65.8>

193 E garage + house 8' 11" = House ^{SL}

150

125 CR house

16

15+90 E gar. wash room

T.P. 547 $\langle 68.58 \rangle$ 207 $\langle 63.11 \rangle$

15+50 CR house gar below
97, 15, 130

$\langle 65.18 \rangle$

LT

9
63.6[✓] 66.4[✓] 68.2[✓]
5.0 $\frac{2.2}{2.2}$ $\frac{0.4}{0.4}$
gar. FL. House FL.

63.6[✓]
5.0

63.5[✓] 69.3[✓]
5.1 + 0.7
 $\frac{5.1}{5.1}$
FL. EL.

63.3[✓]
5.3

63.2[✓] 66.6[✓]
5.4 2.0
 $\frac{6.2}{6.2}$
gar. FL.

$\langle 68.58 \rangle$

67.6[✓]
2.6

67.2[✓]
+ 2.0
 $\frac{5.5}{5.5}$
FL. EL.

$\langle 65.18 \rangle$

check to NWBP 4.30 6472

Frankfort + Gardena
19+24.94 Littlefield St
and House to LT.

rec.
64.12
0.10

19

+50

+08 House to Lyon W Cor

18

+50

17+19.15 = 2 Gardena Ave

17

(18.58)

LT 6.8 ✓
1.8
CS
FL. EL

65.8 ✓
2.8

64.8 ✓
3.8

63.9 ✓
4.7

60.9 ✓
7.7
54
FL. EL.

63.8 ✓
4.8

63.8 ✓
4.8

63.4 ✓
5.2

63.6 ✓
5.0

63.7 ✓
4.9

(18.58)

RH 10

Sewer Levels in Alley
Bet. Frankfort & Galveston
Beg. at N L Gardner

+88 9rd. over Tank Rear of house

+50

0441 septic Tank rear of house

0436 NW Cor house

0425 10' LT Tel # 450839 H

T.P. 7.70 <64.08> 12.20 <56.38>

0100 N L Gardner Ave

<68.58>
Fluid Pio

L

R

R

11

60.7 ✓

3.4

85

9rd

58.1 ✓

4.0

57.0 ✓

7.1

59.8 ✓

4.3

85

9rd

over Tank

56.7 ✓

7.4

56.6 ✓

7.5

55.5 ✓

54.6 ✓

8.0

9.2

FL. EL. 9rd.

<64.08> ✓

56.4 ✓

12.2

<68.58> ✓

T.P. 8.85 $\langle 70.7 \rangle$ 2.21 $\langle 41.87 \rangle$

2

+ 90 House to RT.

+ 85 grd. over Tank Cr. House

+ 55 10' Lt. 450840 H T.P.

+ 50

+ 44 grd. over Tank Cr. of house

+ 00

$\langle 64.08 \rangle$

Lt

R

RT

12

61.5 ✓
2.6

61.2 ✓
- .9

65.1 ✓
+ 1.0
100

61.1 ✓
30

59.1 ✓
5.0

63.1 ✓
1.0
100

59.0 ✓
5.1

58.4 ✓
5.7

$\langle 64.08 \rangle$

62.1 ✓
2.0
125
FL. EL.

59.7 ✓
4.4
125
grd

5

+50

+30 C.547. 4490 11 H TELP,

4

+50

3 Sep. Tank CTO house in Rear

+80 10 LT TELP. 449010 H

2+50

~~70.72~~

LT

69.0 ✓
1.7

R_T

13

69.0 ✓
1.7

66.5 ✓
2.2

67.4 ✓
3.3

64.1 ✓
L.C
95
grid
over T

65.8 ✓
4.9

70.2 ✓
0.5
100

House
Floor

63.9 ✓
6.8

~~70.72~~

81
0400 = 1714 at ^{Frankfort} Ashton See sketch
F. Dk. $\frac{1.821}{5}$

T.P. 169 $\langle 6896 \rangle$ 345 $\langle 6777 \rangle$ ^{2x2} Hub
Δ PT.

5+696 P Ashton = 1796.78

+59

+55

+49 11 LT P 4349 PP

5+50

5+14 9 LT 46900 H TELP

$\langle 7072 \rangle$

21

2

R

14

55.4
13.6

$\langle 6896 \rangle$

67.6
31

66.8
39

67.8
29

67.8
29

$\langle 7072 \rangle$

+15

+10

2 + 00 Now Nlyj via alley

1 + 96.78 $\Delta = 89^{\circ} 58' 27''$
= 5 + 69.64 on PIX

+50

1

0 + 50

East in Astoria

$\langle 68.96 \rangle$

$\langle 7 \rangle$

68.5 ✓
0.5

R

15 ✓

67.0 ✓

2.0

67.5 ✓

1.5

67.6 ✓

1.4

64.1 ✓

4.9

60.7 ✓

8.3

57.9 ✓

11.1

$\langle 68.96 \rangle$

+50

+36

9LT TELP 472415 H

H

+50

3+00

to Rt 15 High ground

+87

10LT 472414 H

2+70

House on Rt Tank in Rear

2+50

T.P

7.33

$\langle 75.65 \rangle$
68.96

0.64

$\langle 78.37 \rangle$

LT

E

Rt

16

70.4 ✓
5.7

70.8 ✓
2.8

71.0 ✓
4.6

61.6 ✓
14.0
125
9rd.

69.8 ✓
5.8

69.2 ✓
6.4

71.8 ✓

3.8

20

9rd. at
Tank

68.8 ✓
6.8

$\langle 75.65 \rangle$

+50

T.P. 4.99 $\langle 74.84 \rangle$ 5.80 $\langle 69.85 \rangle$

7 House to RT High

+87 9 LT 472417 H T-L P

+50

6

+87 9 LT 472416 H T-L P

+50

+100

$\langle 75.65 \rangle$

LT

E

RT - 17

68.0 ✓
6.8

$\langle 74.84 \rangle$ ✓

69.1 ✓
4.6

76.7 ✓	79.2 ✓
+ 1.0	+ 3.5
90	90
9rd	FL.

68.7 ✓
7.0

67.8 ✓
8.0

68.4 ✓
7.2

70.8 ✓
4.8

$\langle 75.65 \rangle$ ✓

P_r

Z

LT

68.4 ✓
6.6

68.2 ✓
6.6

67.8 ✓
7.0

67.6 ✓
7.2

67.9 ✓
6.9

63.5 ✓
11.3
7.6
9.0

67.6 ✓
7.2

5 rear of house

74.8 ✓

+50

9 cont nly to Napier ST.

8+76.71 9 Octen ST.

+50

8

+80 9 LT 472418 H.T.C.P.

7+64 SMALL DWELLING, NO SEPTIC TANK
HOUSE PLANNED IN FUTURE
TO FACE ON FRANKFURT

74.8 ✓

check to T.P.
△ Pr. alley to N.

Via alley
E of Frankford

6.25 71.81

12 + 66.7 SL

+ 50

12

+ 50

T.P. 11.80 78.06 1.58 73.26

11

+ 50

10 + 100

74.84

Please check
to F.B. 18.21

LT

19

75.0 ✓
3.1

75.4 ✓
2.7

74.8 ✓
3.3

74.7 ✓
3.4

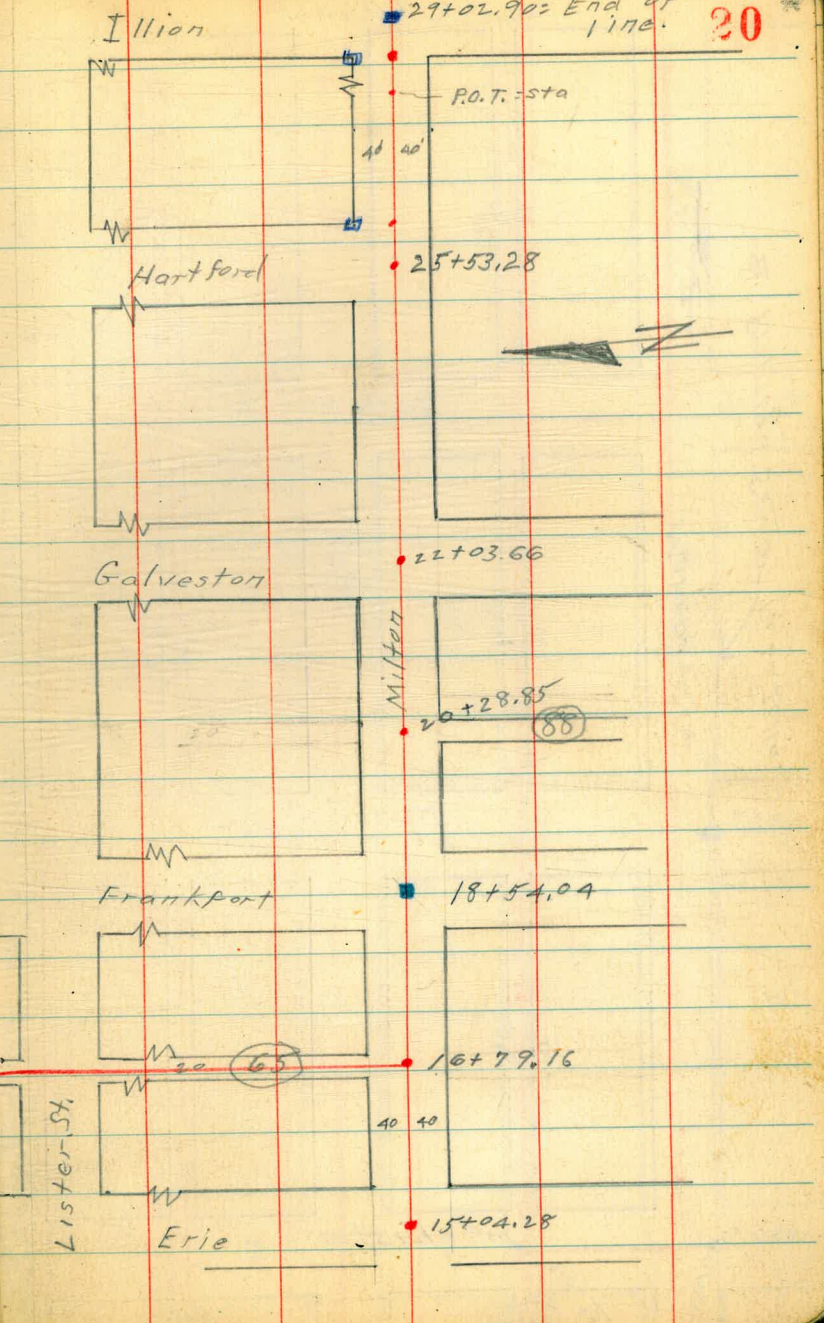
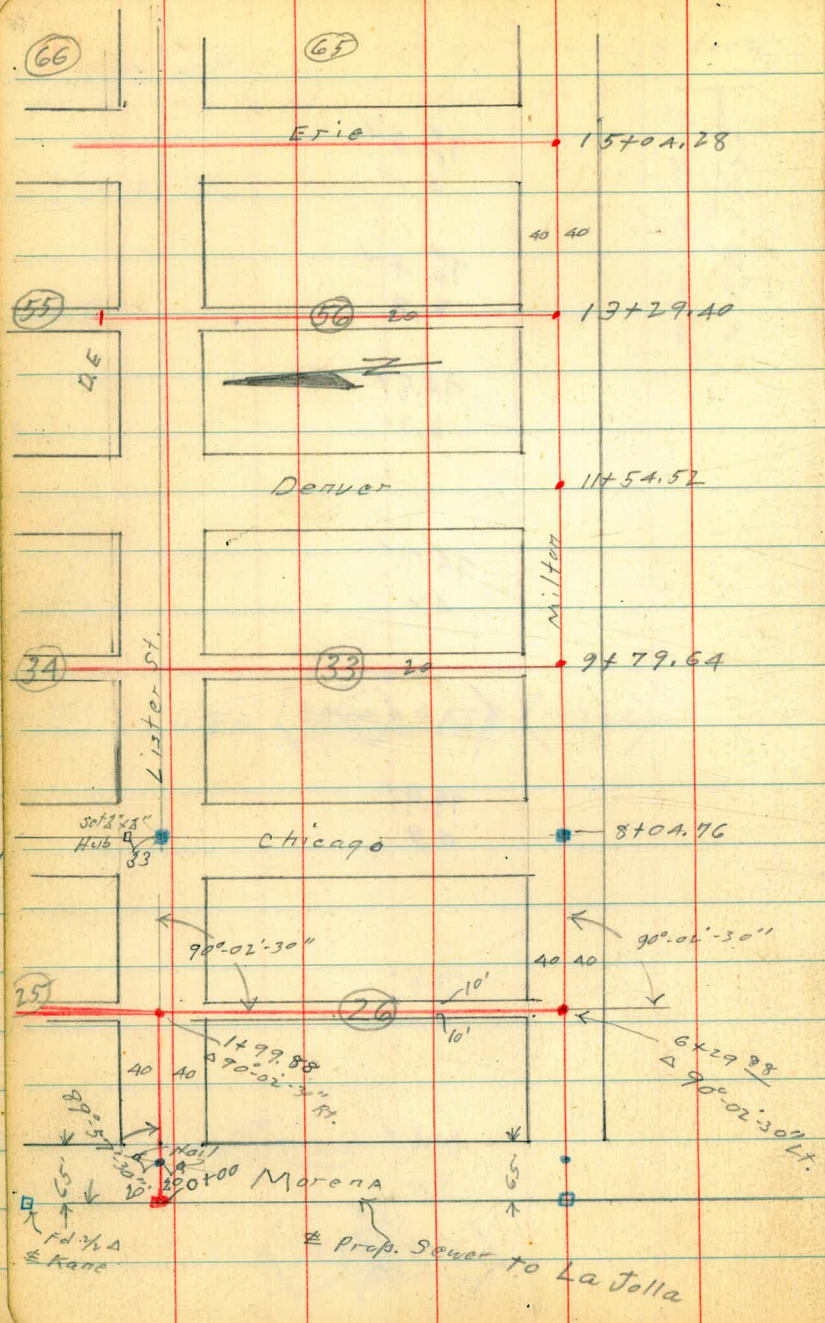
78.06 ✓

73.9 ✓
0.9

71.8 ✓
3.0

69.8 ✓
5.0

74.84 ✓



Ingulf

Ingulf

21



Proposed Sewer to La Jolla.

Morena

23

36

53

68

65b

Jellett

80'

40' 40'

Jellett

Chicago

Denver

Denver

Erie

Frankport

24

35

67

Kane

100'

100'

Kane

25

34

55

66

Lister

80'

Lister

100'

100'

38

33

54

65

Sewer Profile
 Lister St-Alley Bk 26 and

Milton St. Sommermeyer
 McCoy
 W Moore

0+40 = \pm paving

0+30 = west. edge Moreno paving

0+21 $\frac{1}{2}$ 1' Lt. = 8" diam. eucalyptus

0+19

~~Sketch~~

0+16

\pm Lister St. (Page 20-10ft).

0+00 = Intersection Prop. La Jolla sewer

2+2 Hub. Int. \pm Lister & La Jolla Sewer,	10.70	16.12	9.30	5.42	= 0+00 Page 20 left.
-------------------------------------------------------	-------	-------	------	------	----------------------------

T.P.	3.88	14.72	5.64	10.84
------	------	-------	------	-------

T.P.	4.90	16.48	1.44	11.58
------	------	-------	------	-------

FB 1821-9 0+00 Hub.	5.85	13.02	—	7.17
------------------------	------	-------	---	------

\pm Napier

4

9.81
6.31

9.62
6.50

9.01
7.1

5.1
10.4

5.1
10.4

16.12

Lister St. Alley BIK 26 and
Milton st. (Sketch Page 20)

2+25

↑
Deleg. Pl. 26

1+9988 = L 90° 02' 30" RT. Also = 0100 to North

1+50

Lister St.

1+00

0+90 27' RT. = ctr. 4' diam. eucalyptus

0+75

0+55

0+50 = East edge paving

{16.12}

23

♀

12.1 ✓
4.0

12.4 ✓
3.9

11.3 ✓
4.8

10.6 ✓
5.5

10.1 ✓
6.0

9.2 ✓
6.7

9.58 ✓
6.54 ✓
{16.12}

3+00 to 1821/58

T.P. 5.78 <20.19> 1.71 <14.41>

2+50

<16.12>

<20.19>

1.8

3.3

<16.12>

Sewer levels for Blk.
14 Bay Park Village Betw.
Monera Blvd

0+61 A to Pt. on Sky See Sketch
1821
52

0+50 Top curb

0+50

0+30 w. edge Pav. Cur Base

0+00 = on main line trunk sewer #

check to Napier 6.95 7.17 7.17

B.M.B.P. Top
w. hdwl 7.36 (14.12)
R.R. Culv.
150' S of Napier

6.76

12.3 ✓
1.8

12.56
1.56
curb

11.8 ✓
2.3

11.8 ✓
2.3

11.6 ✓
2.5

(14.12) ✓

3 + 22.5 = DE

3 + 03 4' Pt = Cir. 4' di. Eucal
tree

3

+50

2

+50

1400

14.10

26

11.6 ✓
2.5

12.10

2.02
11

Top
Curb

11.6 ✓
2.5

11.4 ✓
2.7

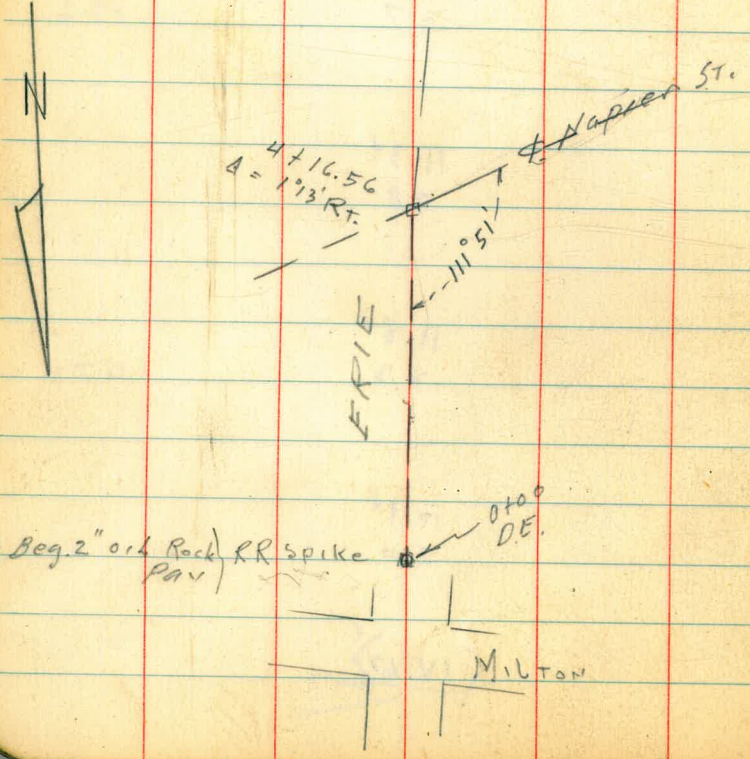
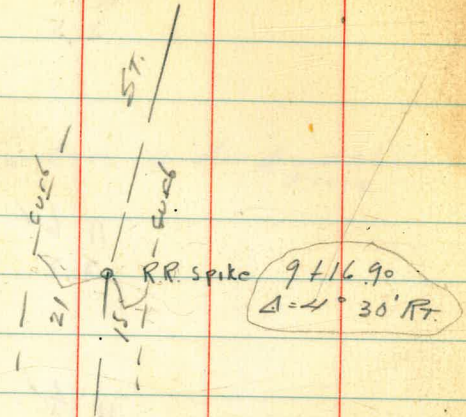
11.3 ✓
2.8

11.8 ✓
2.3

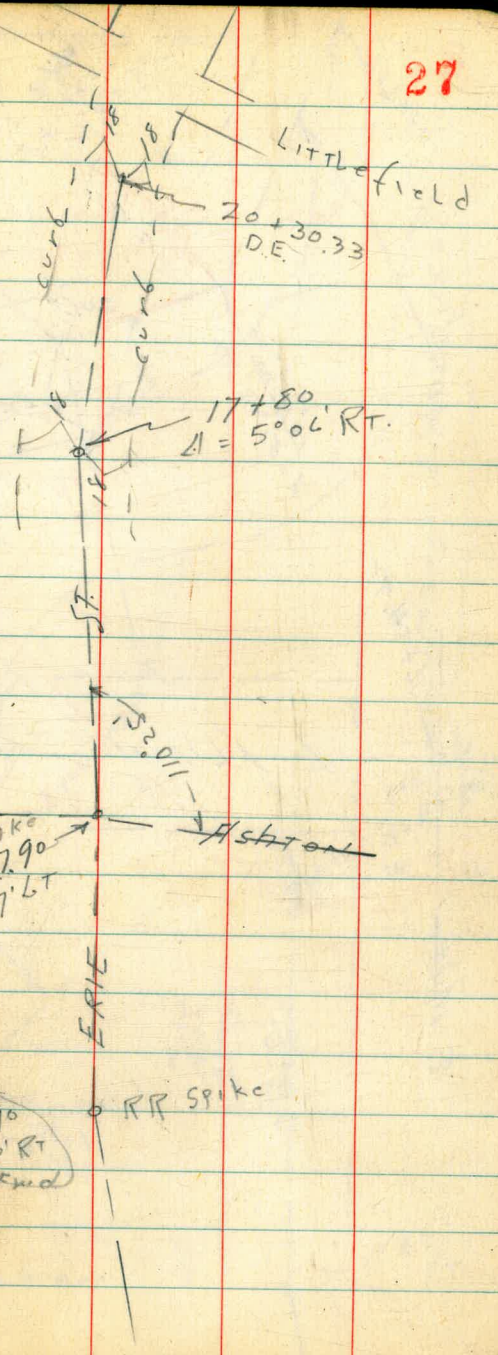
12.1 ✓
2.0

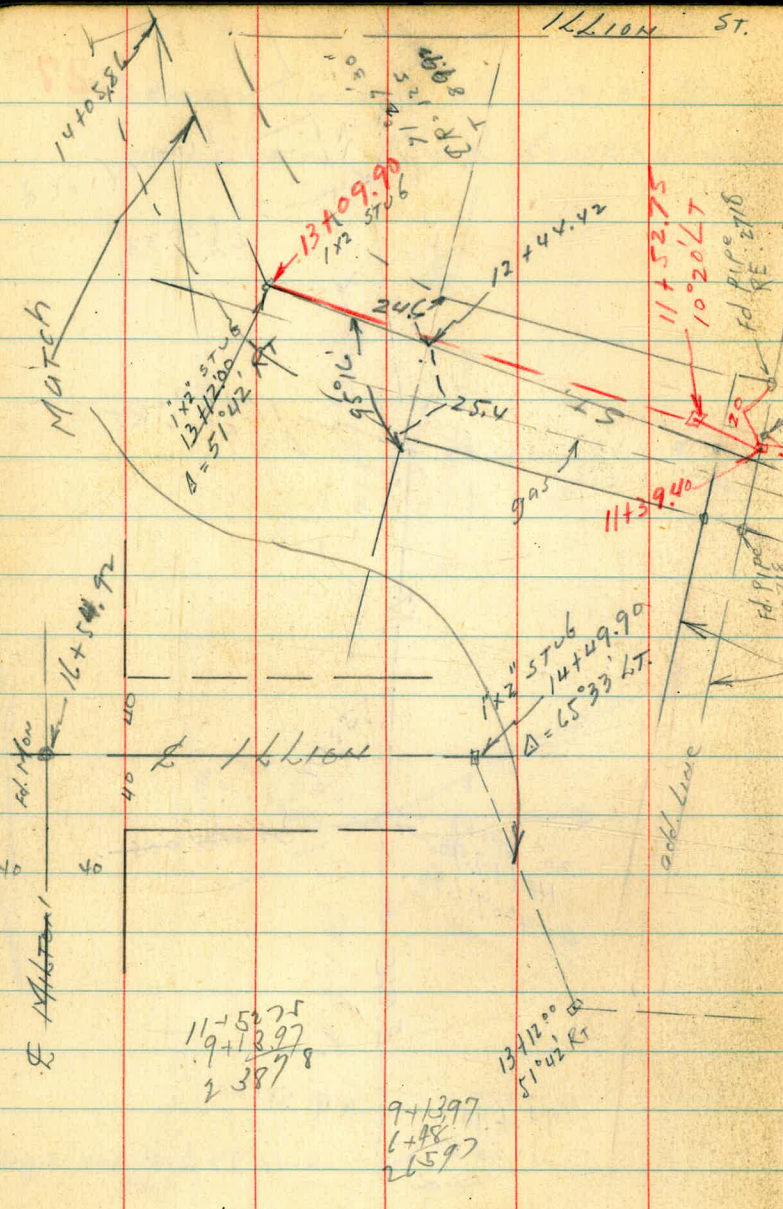
14.10

Sewer Levels on ERIE ST.
 MILTON Sky to Littlefield.



27





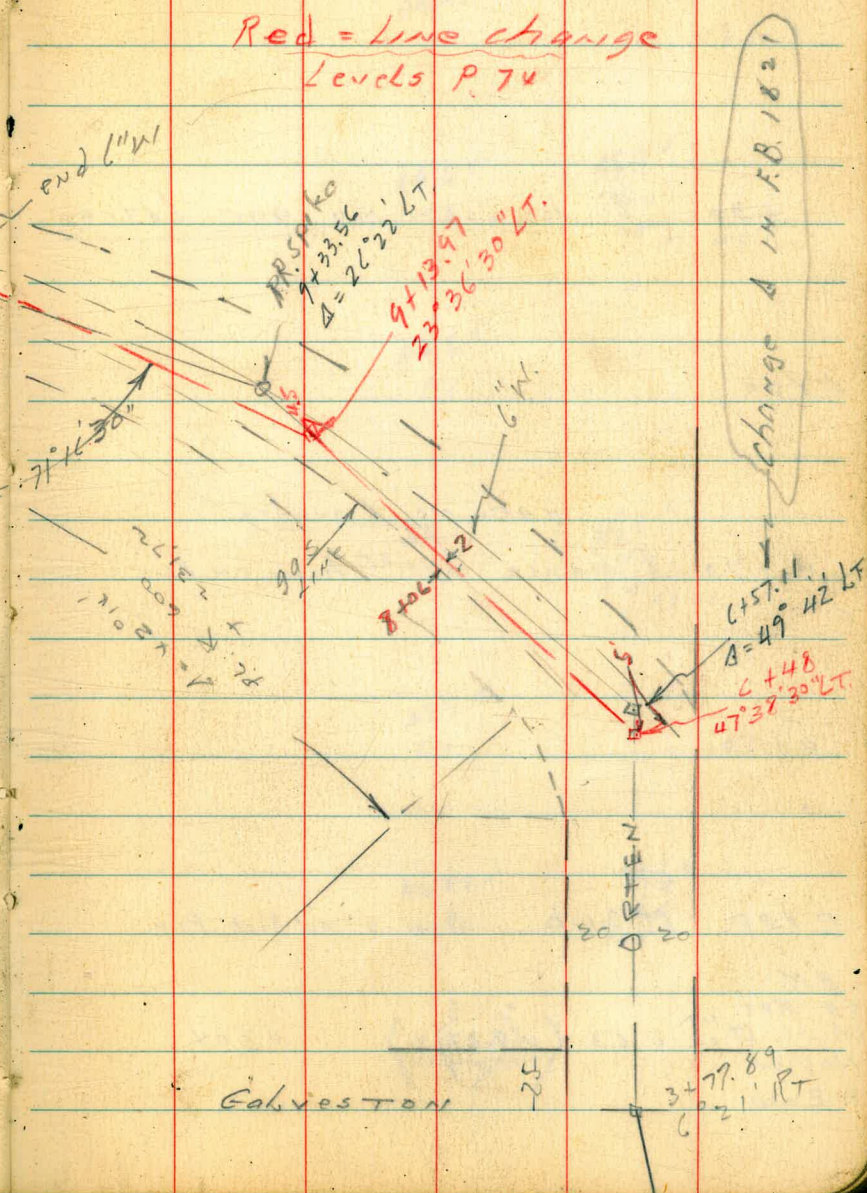
$$\begin{array}{r} 11+52.75 \\ 19+12.97 \\ \hline 2387 \end{array}$$

$$\begin{array}{r} 9+13.97 \\ 1+18 \\ \hline 6597 \end{array}$$

13+12.00
5'02" RT

Galveston to 16 Lion

Red = line change
Levels P. 74



Change Δ in F.B. 1821

$$\begin{array}{r} 1+57.11 \\ \Delta = 49^\circ 42' \text{ LT} \\ 6+48 \\ 47^\circ 39' 30'' \text{ LT} \end{array}$$

$$\begin{array}{r} 3+77.89 \\ 6+21' \text{ RT} \end{array}$$

Galveston

Sewer Levels on
Eric St. Milton to Littlefield

1 + 50

+ 30 E house NO gar. & tray

1 + 00

gar. no Laundry

0 + 70 E house (1st house on Rt.)

0 + 50

0 + 00 RR Spike Beg. 2" oil Rock Pav.

B.M.

S.E. Ret.

Chisel \square ^{top}

Napier

+ Eric

6.63

(49.67)

4304

Sketch P. 27

£

R+

29

44.9 ✓
4.8

44.8 ✓
4.9

44.6 ✓
5.1

44.1 ✓
5.0

43.7 ✓
6.0

42.81 ✓
6.80

(49.67) ✓
2

45.7 ✓
4.0

48 fl. el.

45.5 ✓
4.2

48 fl. el.

39.6 ✓
10.1

725

4

$$\begin{array}{r} 42.7 \checkmark \\ 7.0 \end{array}$$

P+

30

+50

$$\begin{array}{r} 43.3 \checkmark \\ C.4 \end{array}$$

3

$$\begin{array}{r} 43.8 \checkmark \\ 5.7 \end{array}$$

+80 E gar. with ldy. trays

$$\begin{array}{r} 44.1 \checkmark \\ 5.6 \end{array}$$
42.4[✓]

$$\begin{array}{r} 7.3 \\ 80 \text{ fl. cl.} \end{array}$$

some
↓
5 P.O.

+55 E house

$$\begin{array}{r} 44.2 \checkmark \\ 5.5 \end{array}$$
45.7[✓]

$$\begin{array}{r} 4.0 \\ 50 \text{ fl. cl.} \end{array}$$

2+05 E house

$$\begin{array}{r} 44.7 \checkmark \\ 5.0 \end{array}$$
45.2[✓]

$$\begin{array}{r} 4.5 \\ 50 \text{ fl. cl.} \end{array}$$

1+87 E gar.

$$\begin{array}{r} 44.8 \checkmark \\ 4.9 \end{array}$$
43.6[✓]

$$\begin{array}{r} 6.1 \\ 27 \text{ gar. fl. cl.} \end{array}$$

$$\langle 49.67 \rangle$$

$$\langle 49.67 \rangle$$

6704 E 900, with 2 dy. trays

50
P.O.

+ 80 E house

+ 50

5

4 + 50

T.P.

4.97

$\left\langle \frac{48.01}{26} \right\rangle$

6.63

$\left\langle \frac{43.05}{26} \right\rangle$

4 + 16.50 Δ = 1° 13' RT E Napier St

$\left\langle \frac{49.67}{26} \right\rangle$

43.4 ✓
46

40.9 ✓
 $\frac{7.1}{85}$ Fl. cl.

43.1 ✓
49

43.9 ✓
 $\frac{4.1}{48}$ Fl. cl.

42.8 ✓
52

42.4 ✓
56

42.0 ✓
60

$\left\langle \frac{48.01}{26} \right\rangle$

42.7 ✓
70

$\left\langle \frac{49.67}{26} \right\rangle$

Erle St

7185 ♀ gar. Ldy trays

SAME
P.O.

7182 ♀ house

7150

7125 ♀ gar. with ldy. trays

SAME
P.O.

7100 ♀ house

6165 ♀ gar. with ldy. trays

SAME
P.O.

6140 ♀ house

4801

45.4 ✓
2.6

43.4 ✓
4.6
82 FL.OL. 32

46.4 ✓
2.8

46.4 ✓
1.6
46 FL.OL.

45.1 ✓
2.9

44.9 ✓
3.1

43.0 ✓
5.0
85 FL.OL.

44.7 ✓
3.3

45.8 ✓
2.2
40 FL.OL.

44.2 ✓
5.8

42.0 ✓
6.0
85 FL.

43.8 ✓
4.2

45.0 ✓
3.0
46 FL.OL.

4801

9+40 49R gar Ldy
Tray

9+16.90 Δ 4°30' Pt. E gar with
Ldy. Trays

+87 E House

+50 E gar with Ldy. Trays

↑
SAME P.O.
↓

+25 E House

8+00

TR 559 $\left\langle \begin{array}{l} 51.00 \\ \hline 48.01 \end{array} \right\rangle$ 260 $\left\langle \begin{array}{l} 45.41 \\ \hline \end{array} \right\rangle$

46.2 ✓
48

45.0 ✓
6.0
49

46.2 ✓
48

43.0 ✓
8.0
95 Fl. el.

46.0 ✓
50

46.1 ✓
4.9
45 Fl. el.

45.8 ✓
52

43.0 ✓
8.0
82 Fl. el.

45.1 ✓
53

46.5 ✓
4.5
47 Fl. el.

45.5 ✓
55

$\left\langle \begin{array}{l} 51.00 \\ \hline \end{array} \right\rangle$

11+20 49 R gar Tray

11+00

10+80 49 R House E

10+61 49 R gar Tray

10+20 48 R House E

10+00 48 R House E

+58 House 49 R

 $\left\langle \begin{array}{c} 51.00 \\ \rightarrow \end{array} \right\rangle$
45.4[✓]
5.644.0[✓]
7.0
4945.6[✓]
5.445.7[✓]
5.345.8[✓]
5.2
4945.8[✓]
5.244.5[✓]
6.5
4946.2[✓]
4.845.9[✓]
5.1
4846.2[✓]
4.844.8[✓]
6.2
4846.3[✓]
4.746.3[✓]
4.7 floor
49
 $\left\langle \begin{array}{c} 51.00 \\ \rightarrow \end{array} \right\rangle$

ERIC

+50

13

+61

♀ house

↑
SAME P.O.

+73

♀ gar. with ldy trays

R100

♀ house

+80

♀ gar. with ldy. trays

T.P.

5.79

<50.87>

5.92

<45.08>

11 +40

H9 R House

<51.00>

44.7 ✓
4.2

44.9 ✓
6.0

44.9 ✓
6.0

45.0 ✓
5.9

45.1 ✓
5.8

<50.87>

45.3 ✓
5.7

<51.00>

41.3 ✓
2.6
35 ✓
125 vac. Lot

45.6 ✓
5.3
50 Fl. cl.

44.2 ✓
6.7
50 Fl. cl.

45.5 ✓
5.4
44 Fl. cl.

43.3 ✓
7.0
25

45.4 ✓
5.6
49 Fl. cl.

+50

+40 E 400 with ldy. trays

+13 E House

15

+50

14 +17.90 @ 4°07'21" E Ashton

14

E

R.

36

46.3 ✓

4.4

46.2 ✓

4.7

47.1 ✓

3.2

43 fl. cl.

45.9 ✓

5.0

50.6 ✓

0.3

45 fl. cl.

45.8 ✓

5.1

45.2 ✓

5.7

45.2 ✓

5.7

44.6 ✓

6.3

Eric

4

Rt.

37

R.R.
SPIKE
T.P.
17+80

10.40 $\langle \underline{60.31} \rangle$ 0.96 $\langle \underline{49.91} \rangle$

17+80 Δ 5° 06' Rt

+50

17

+50

16

E gar. with Ldy. trays

~~SAME
PD.~~

15+73

E House

$\langle \underline{50.87} \rangle$

50.0 ✓
0.9

49.3 ✓
1.5

48.3 ✓
2.0

44.5 ✓
 $\frac{6.0}{125}$

47.6 ✓
3.3

47.0 ✓
3.9

45.7 ✓
 $\frac{5.2}{95 \text{ Fl. ol.}}$

46.6 ✓
4.3

48.6 ✓
 $\frac{2.3}{45 \text{ Fl. ol.}}$

$\langle \underline{50.87} \rangle$

20 + 100

57.4 ✓
2.9

+ 65 E house

56.2 ✓
4.1

58.5 ✓
1.8
54 FL. CL.

same po.

+ 40 E garage

55.2 ✓
5.1

54.9 ✓
5.4
75 FL. CL.

19

53.6 ✓
6.7

50.9 ✓
9.4
125

+ 50

51.9 ✓
8.4

18

50.3 ✓
10.0

47.6 ✓
12.7
125

60.31 ✓

60.31 ✓

64.22
P. 10

check to NWBP
Frankfort
and Gardens Ave

6.50 64.20 Rec. 64.12

T.P. 3.19 70.70 527 67.51

T.P. 0.35 59.96

20 + 30.33 DE opposite ^{North Line} last house on LT. which is on Higher ground.

58.6
1.7

20 + 15 E house last house on RT.

58.0
with 2.3
Ldy. trays
59.0
1.3
50 ft. 6. 100
53.8
6.5
90.

60.31

60.31

Sewer Levels on
Orton St.
Frankfort Aly
to Union St.

8

40

2+50

72.1 ✓
9.5

T.P 1278 $\left\langle \begin{array}{c} 81.64 \\ \hline \end{array} \right\rangle$ 0.52 $\left\langle \begin{array}{c} 68.86 \\ \hline \end{array} \right\rangle$

$\left\langle \begin{array}{c} 81.64 \\ \hline \end{array} \right\rangle$

1+96.9 Δ to Lt. see sketch 1821
5

67.1 ✓
1.7

+50

64.5 ✓
4.9

1

62.2 ✓
7.2

0+50

60.2 ✓
9.2

0+00
B.M. 2x4 Hb
4+30.15
Page 3

12.58

$\left\langle \begin{array}{c} 69.38 \\ \hline \end{array} \right\rangle$

56.80

56.80
 $\left\langle \begin{array}{c} 69.38 \\ \hline \end{array} \right\rangle$

5 + 50

5 + 00

4 + 50

Set B.M. on 2" Pipe Cor.
S.E. Cor. of Orton
and Galveston

8.48 84.21

4 + 00 Beq. of $\frac{1}{2}$ " oil Pav.

3 + 77.89" A Pt.

Sketch
FB. 182check
this

T.P.

12.37

~~92.69~~

1.32

~~80.32~~

+ 50

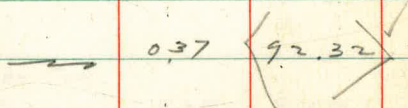
3 + 00

~~81.14~~90.8 ✓
1.9
$$\begin{array}{r} P.T. \checkmark \\ 85.1 \checkmark \\ \underline{7.0} \\ 80 \\ \text{Swale} \end{array}$$

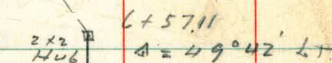
41

90.2 ✓
2.589.2 ✓
3.5
$$\begin{array}{r} 80.2 \checkmark \\ \underline{12.5} \\ 90 \\ \text{swale} \end{array}$$
85.3 ✓
7.483.5 ✓
9.2~~92.69~~80.6 ✓
1.076.6 ✓
5.0~~81.64~~

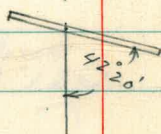
T.P.



6 + 57.91 $\Delta = 49^{\circ}42'LT.$
New angle

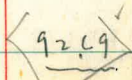


6 + 16.5 Cross 24" Iron Pipe
DRAIN



6 + 15

6 + 00



91.9 ✓
0.8

88.56 ✓
4.13
82
INV.

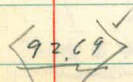
91.2 ✓
1.5

85.65 ✓
7.04
43.4
INV.

91.2 ✓
1.5

90.7 ✓
2.0

88.3 ✓
4.4
50



Sewer Levels & Alley

SA Betw. ERIE & Franfort.

MILTON only to Inghit

T.P. 1107 $\langle 64.96 \rangle$ 0.14 $\langle 53.89 \rangle$

1

+66

+50

+21

+16

+13

+7

0+00 & MILTON

B.M.B.P.

SW. curb
MILTON
and
ERIE

11.93

$\langle 54.03 \rangle$

$\langle 42.10 \rangle$

&

43

53.3 ✓
0.7

49.9 ✓
4.1

49.8 ✓
4.2

49.0 ✓
5.0

46.3 ✓
7.7

46.2 ✓
7.8

48.1 ✓
5.9

48.1 ✓
5.9

$\langle 54.03 \rangle$

4

3 + 60 Rear house (Septic Tank
IN FRONT)

3 + 50

T.P. 7.50 $\langle 71.09 \rangle$ 137 $\langle 63.59 \rangle$

3 + 00

+ 78 Large Orange tree on E

+ 72 5' RT E w. side 18' shed

+ 50

+ 20 house

2

1 + 50

$\langle 64.96 \rangle$

LT

$\langle 65.71 \rangle$

44

61.9
9.2
35
FL.OL.

63.7
7.4

63.6
7.5

$\langle 71.09 \rangle$

55.5
9.5
80

62.9
2.1

62.4
2.3

56.0
9.0
70
FL.OL.

61.4
3.3

61.4
3.9

58.3
6.7

$\langle 64.96 \rangle$

WILL
OWNER
SAYS
HE

T.P.

838 $\langle 79.40 \rangle$ 0.01 $\langle 71.08 \rangle$

7+00

House

+45

house

6

+91

house

+45

house

5

+80

house

+50

4+30

♀ Lister

 $\langle 71.09 \rangle$

L7

♀

67.4 ✓

8.7

40

70.3 ✓

0.8

61.9 ✓

9.2

76

FL. el.

69 0 ✓

2.1

69 2 ✓

1.9

67.6 ✓

8.5

90

FL. el.

69 3 ✓

1.8

61.3 ✓

9.8

90

FL. el.

69 0 ✓

2.1

67 6 ✓

3.5

58.1 ✓

12.4

90

FL. EL.

67.5 ✓

3.6

66.8 ✓

4.3

66 1 ✓

4.4

 $\langle 71.09 \rangle$

+ 50

11

+ 50

10

NO houses in this blk.

+ 50

9

8 + 70 E Kane

+ 50

8 + 100 house

7 + 50 house

Lt

$$\begin{array}{r} 77.7\checkmark \\ 1.8 \end{array}$$

$$\begin{array}{r} 67.5 \\ 12.0 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 75.3\checkmark \\ 4.2 \end{array}$$

$$\begin{array}{r} 75.0\checkmark \\ 4.5 \end{array}$$

$$\begin{array}{r} 65.0 \\ 14.5 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 74.1\checkmark \\ 5.4 \end{array}$$

$$\begin{array}{r} 73.6\checkmark \\ 5.9 \end{array}$$

$$\begin{array}{r} 73.1\checkmark \\ 4.4 \end{array}$$

$$\begin{array}{r} 73.0\checkmark \\ 6.5 \end{array}$$

$$\begin{array}{r} 72.5\checkmark \\ 7.0 \end{array}$$

$$\begin{array}{r} 68.5 \\ 16.0 \\ \hline 97 \\ \text{FL.EL.} \end{array}$$

$$\begin{array}{r} 72.4\checkmark \\ 7.1 \end{array}$$

$$\begin{array}{r} 62.3 \\ 17.2 \\ \hline 97 \\ \text{FL.EL.} \end{array}$$

$$\begin{array}{r} 71.5\checkmark \\ 8.0 \end{array}$$

150

15

150

14

150

110

g. dellott

13

T.P.

1054 <8900>

1.00 <7840>

150

12

<7940>

27

86.0 ✓
3.0

47

13.9 ✓

15.1

100

85.8 ✓
3.2

83.7 ✓
5.3

10.0 ✓

19.0

100

81.8 ✓
7.2

81.0 ✓
8.0

19.8 ✓
7.2

19.5 ✓
9.5

<89.00> ✓

19.1 ✓
2.4

68.4 ✓
11.1

78.3 ✓
1.2

<79.40> ✓

20 drops INTO CANON

+50

19

18+50

Set nail B.M. on
P.P. # J.P. 4252
10' Rt. of 17+00

822 $\langle 84.48 \rangle$

18+00

17+40 E Inguelt

17+40 E Inguelt 45° Rt. approx. SW. Cor.
of 2 1/2 story house

17

T.P. 10.73 $\langle 92.79 \rangle$ 7.03 $\langle 81.97 \rangle$

+50

16

$\langle 89.00 \rangle$

Lt

E

Rt.

48

75.7 ✓

17.0

81.4 ✓

11.3

82.4 ✓

10.3

83.4 ✓

9.3

83.0 ✓

9.7

71.1 ✓

21.6

100

15.6 ✓

17.1

50

80.8 ✓

11.9

80.8 ✓

11.9

Note
this

82.7 ✓

10.0

93.1 ✓
+ 0.4
11.2

Basement. Fl.
el.

$\langle 92.70 \rangle$

84.9

41

72.6

16.4

100

86.4

2.6

$\langle 89.00 \rangle$

Sewer Levels on
E Erie St.

Between MILTON + Ingholt.

3

+ 74 S.E. Cor of House

+ 50

2

+ 50

+ 100

+ 50

+ 100 E MILTON

B.M. SW BP
MILTON
and
ERIE

9.70

51.80

42.10

LT

E

49

46.1 ✓
3.7

46.1 ✓
5.4
70

47.1 ✓
4.7

46.0 ✓
5.8

44.1 ✓
7.7

39.3
12.5
100
90

43.5 ✓
8.3

43.4 ✓
8.4

42.8 ✓
9.0

42.7 ✓
9.1

51.80 ✓

7

+50

6

+50

5

T.P.

827

 $\langle 59.87 \rangle$

020

 $\langle 51.60 \rangle$

+50

+30

E Lister

4

3150

 $\langle 51.80 \rangle$

27

$$\begin{array}{r} 49.1 \\ 10.8 \\ \hline 100 \end{array}$$

←

$$\begin{array}{r} 55.0 \\ 4.9 \\ \hline \end{array}$$

$$\begin{array}{r} 54.8 \\ 5.1 \\ \hline \end{array}$$

$$\begin{array}{r} 54.3 \\ 5.6 \\ \hline \end{array}$$

$$\begin{array}{r} 53.4 \\ 6.5 \\ \hline \end{array}$$

$$\begin{array}{r} 45.8 \\ 14.1 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 52.5 \\ 7.4 \\ \hline \end{array}$$
 $\langle 59.87 \rangle$

$$\begin{array}{r} 51.0 \\ 0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 50.6 \\ 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 50.6 \\ 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 49.4 \\ 2.4 \\ \hline \end{array}$$
 $\langle 51.80 \rangle$

11

+50

T.P. 11.02 <70.39> 0.50 <59.37>

10

+50

9

+70 E Kane St.

+50

8

+50

<59.87>

27

56.2
14.2
100

28

62.1
8.3

60.1
9.7

<70.39>

53.6
6.3
100

59.5
0.4

58.0
1.9

57.0
2.9

56.7
3.2

56.5
3.4

55.7
4.2

55.3
4.6

<59.87>

51

+29 house

14

#4129

Set nail B.M. on R.P.

SW Cor of JELLETT
AND ERIE STS.

651 (63.88)

+71 house

+50

13 +10

♀ JELLETT

13

*50

12

11+50

(70.39)

LT

♀

52

65.0 ✓
5.4
69
FL.OL.

66.1 ✓
4.3

66.0 ✓
4.4

64.4 ✓
6.0
72
FL.OL.

65.1 ✓
4.7

65.5 ✓
4.9

66.0 ✓
4.4

65.9 ✓
4.5

64.9 ✓
5.5

64.1 ✓
6.3

63.2 ✓
7.2

(70.39)

+40 E Ingot

17

+50

16

+50

+20 house

15

+80 house

14+50

7039

LT

£

R+

53

Note!

1740
1310
430

64.7✓
5.7

68.8✓
1.6
50

65.4✓
5.0

65.3✓
5.1

65.5✓
4.9

65.6✓
4.8

63.4✓
7.0
69
Fl. cl.

65.8✓
4.6

66.1✓
4.3

65.0✓
5.2
69
Fl. cl.

66.2✓
4.2

66.2✓
4.2

7039

Scanner Levels on
E of Jellott St.
ERIE to Frankfort
thence Nly to Lugult

2+50

T.P. $\frac{13.01}{95.03} \left\langle \frac{95.03}{13.01} \right\rangle 0.82 \left\langle 82.02 \right\rangle$

2

+75 E Alley

- +50

1

T.P. $13.04 \left\langle 82.84 \right\rangle 0.59 \left\langle 69.80 \right\rangle$

0+50

0+00 = 13+10 P. 52 (E ERIE)

$\left\langle \frac{70.39}{22} \right\rangle$

54

86.5 ✓

8.5

$\left\langle \frac{95.03}{82.1} \right\rangle$ ✓

82.1 ✓

0.7

19.8 ✓

3.0

77.5 ✓

5.3

13.5 ✓

9.3

$\frac{82.84}{69.8}$ ✓

69.8 ✓

0.6

66.0 ✓

4.4

$\left\langle \frac{70.39}{22} \right\rangle$ ✓

T.P. 10.68 (116.67) 0.40 (105.99)

5+00

4+50

Frankfort

4+0

3+50 Δ Lt. Frankfort

T.P. 11.72 (106.39) 0.36 (94.67)

3+0

Jelle's

(95.03)

93.2 ✓
13.2
100

104.4 ✓
2.0

102.1 ✓
14.3

99.9 ✓
6.5

(98.4) ✓
8.0

(106.39) ✓

92.9 ✓
2.1

(95.03) ✓

see
P 48

		9.48	8447	84.48
	0.83	[93.95]	12.19	[97.12]
T.P	0.07	[105.31]	11.43	[105.24]

Rail on PP
425-2 on
Ingulf

7+50

94.7 ✓
22
100

113.5 ✓
3.2

7+0

6+75 68A House

97.0 ✓
19.7
68

112.4 ✓
4.3

6+50

Frankfort

111.5 ✓
5.2

6+00 House 130 ft

93.8 ✓
22.9
130

109.5 ✓
7.2

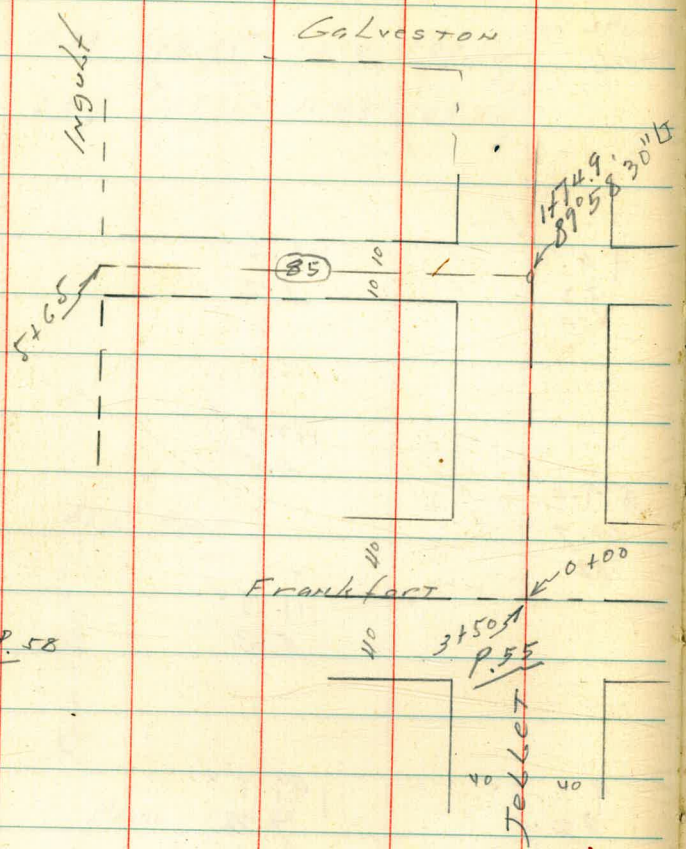
5+5

107.1 ✓
9.6

116.67

116.67

Sewer Levels in alley
Betw. Frankfort + Galveston
to INGOLF + JELLET



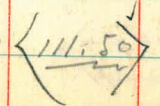
Cont'd. P. 58

1 + 00

0 + 50

0 + 00 = 3 + 50

Ground at
3 + 50 alt 13.10
P. 55

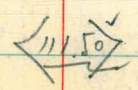


98.40

109.1 ✓
1.8

103.5 ✓
8.0

96.4 ✓
13.1



T.P. 536 $\langle 140.31 \rangle$ 0.58 $\langle 134.95 \rangle$

4 + 45

3 + 90

+ 45

3

T.P. 13.01 $\langle 135.53 \rangle$ 1.65 $\langle 122.52 \rangle$

+ 50

2

1774.9 89° 58' 30" (7)

1735

T.P. 12.82 $\langle 124.17 \rangle$ 0.15 111.35
 $\langle 111.50 \rangle$

L.T.

2

58

124.1 ✓
13.4 ✓
Fl. House $\frac{90}{135.0}$ ✓
0.5

114.5 ✓
16.0 ✓
Fl. House $\frac{90}{130.5}$ ✓
3.4

114.3 ✓
18.4 ✓
Fl. House $\frac{90}{129.6}$ ✓
5.9

113.1 ✓
22.4 ✓
90 ✓
Floor house $\frac{126.6}{8.9}$ ✓

$\langle 125.53 \rangle$ ✓

123.1 ✓
11

120.3 ✓
3.9

119.2 ✓
5.0

114.2 ✓
9.8

$\langle 124.17 \rangle$ ✓

J.P. # 4152

check to nail B.M. PP
P. 48 8.99 84.51 84.48

T.P. 0.34 93.50 12.49 93.16

T.P. 0.37 105.65 11.41 105.28

T.P. 0.26 116.69 12.19 116.43

T.P. 0.56 128.62 12.25 128.06

5+65 52 14 gulf

4+90

140.31

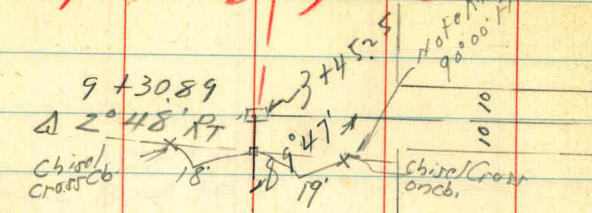
140.30

124.8 ✓
15.5
90
Fl. house

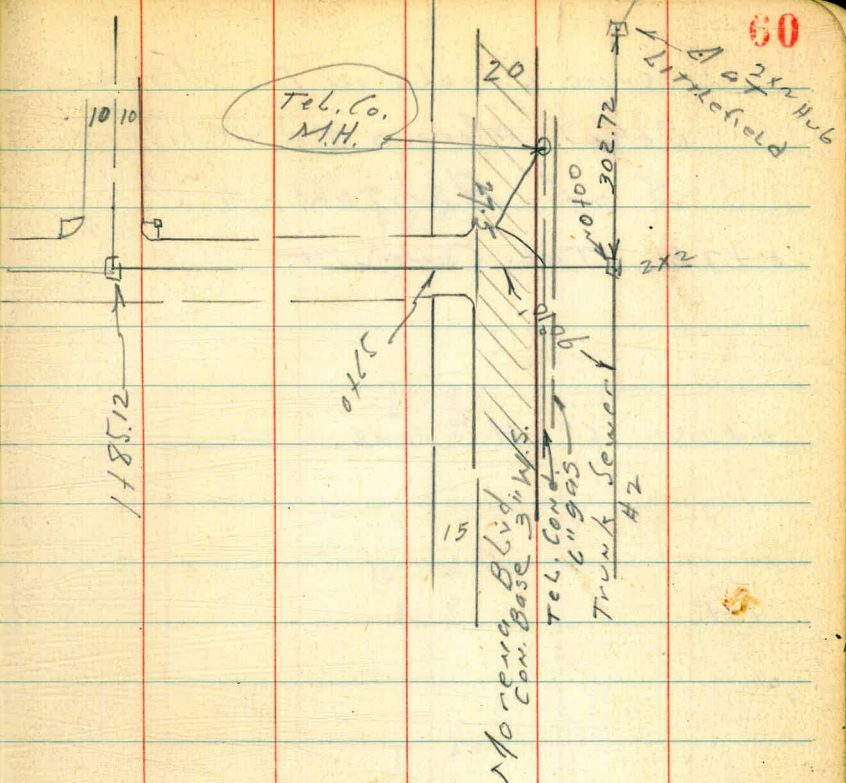
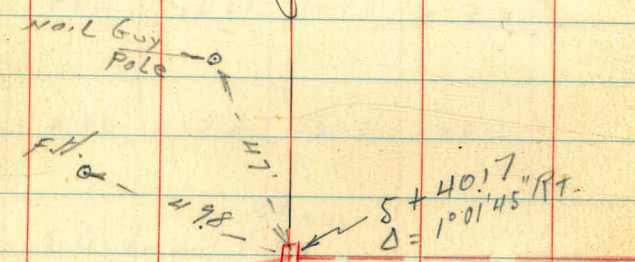
137.9 ✓
2.4

140.31

20 SPIKE
 DE
 Line change on
 Chicago ST
 Napier Sky to



Horton
 Chicago St.



60
 Littlefield

Sewer Levels in E. Valley
Betw. Morena Blvd + Chicago
S of Ashton St.

0+28 Tel. Conduit

12.0 ✓
9.2

0+25 6" H.P. Gas

11.9 ✓
9.3

+14

12.4 ✓
8.8

+10

13.5 ✓
7.7

0+00 at Trunk Sewer #2

12.76 ✓
8.44

8.44 { 21.20 } 25.8 { 12.76 }
BM. B.P. W. hdwl. 8.58 { 15.34 }
of P.R.C. U.L. 676
150' S of Napier
or 900' N of
Kennedy's
Rd. House

{ 21.20 }
15.34

2 + 00

1 + 85.12

+ 50

1 + 00

0 + 65

0 + 50 Edge Pav.

MORENO BLVD.

0 + 30 wedge Pav. 6" Con. Base
3" W.S.

21.20

8

17.8 ✓
34

17.6 ✓
34

16.7 ✓
45

14.8 ✓
67

12.6 ✓
86

12.15 ✓
905

~~905~~

12.07 ✓
913

21.20 ✓

62

check to
old hub A Pt. 0.38 20.82 20.81
10' N Ly

3 + 45.25 = 9 Chicago

+ 15

3

2 + 50

2120

20.9 ✓
0.3

20.1 ✓
0.8

19.9 ✓
1.3

18.7 ✓
2.5

2120 ✓

Sewer Levels
ON ASHTON ST.

Denver to alley
East of Franfort.

+44 cross HP gas line

2

+50

1

0+50

0+07 = cross 6" waterline

0+00 = { 30d SPIKE & DENVER
and ASHTON
10+91.34

30^d BM.
SPIKE
1821-23

11.34

49.14

37.80

44.7 ✓
4.4

43.7 ✓
5.4

42.2 ✓
6.7

40.9 ✓
8.2

39.4 ✓
9.7

37.8 ✓
11.3
Beg. of 2" pav.

49.14 ✓

E

54.0^v
6652.0^v
8650.0^v
106[60.61]^v48.0^v
1146.1^v
3045.1^v
40[49.14]^v

5

+50

4

T.P. 11.60 [60.61]^v 0.13 [49.01]^v

+50

3

2+72 cross 6" water line

2+63.36 Δ 9°58' Lt ⊥ ERIC ST.

~~~~~



714325 2x2 Hub 3.68 67.24 67.27  
Galley 0.03

7

6+50

T.P. 10.68 70.92 0.37 60.24

6+00

5+53 = Cross 6" Water Line

5+46.2  $\Delta$  3° 07' LT. = 2' W of E of Frankfort

5+41 end of 2" Blk Pav.

5+21

$\langle 60.61 \rangle$  ✓

8

66

67.5 ✓  
3.4 ← ground

64.3 ✓  
6.6

see 1833  
15

60.8 ✓  
10.1

70.92

58.0 ✓  
2.6

55.7 ✓  
4.9

54.8 ✓  
5.8

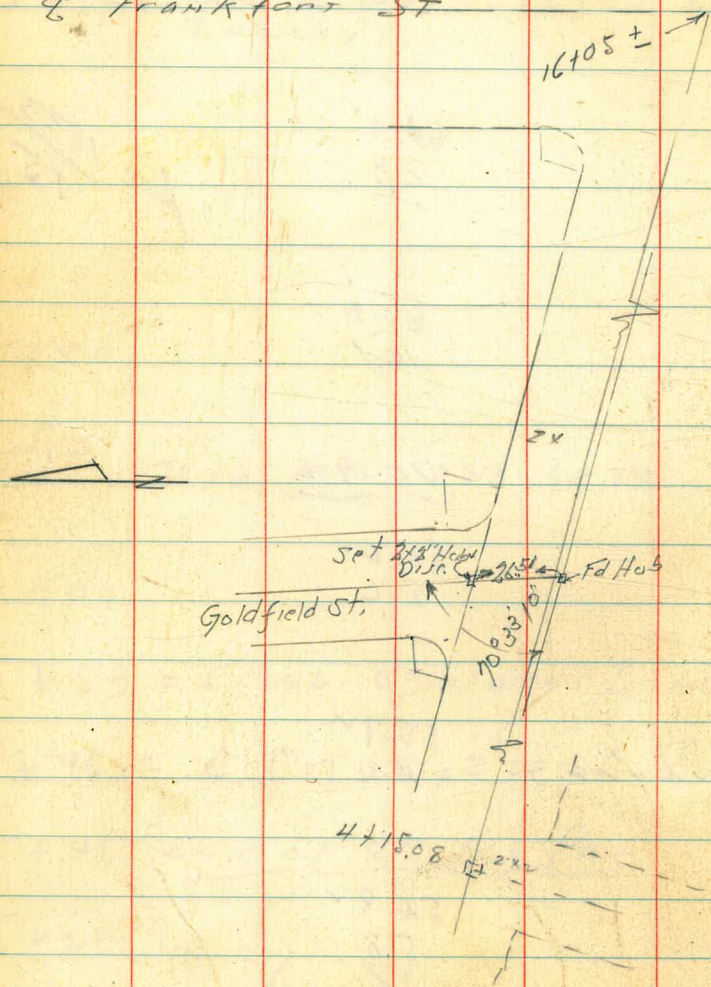
$\langle 60.61 \rangle$  ✓



39

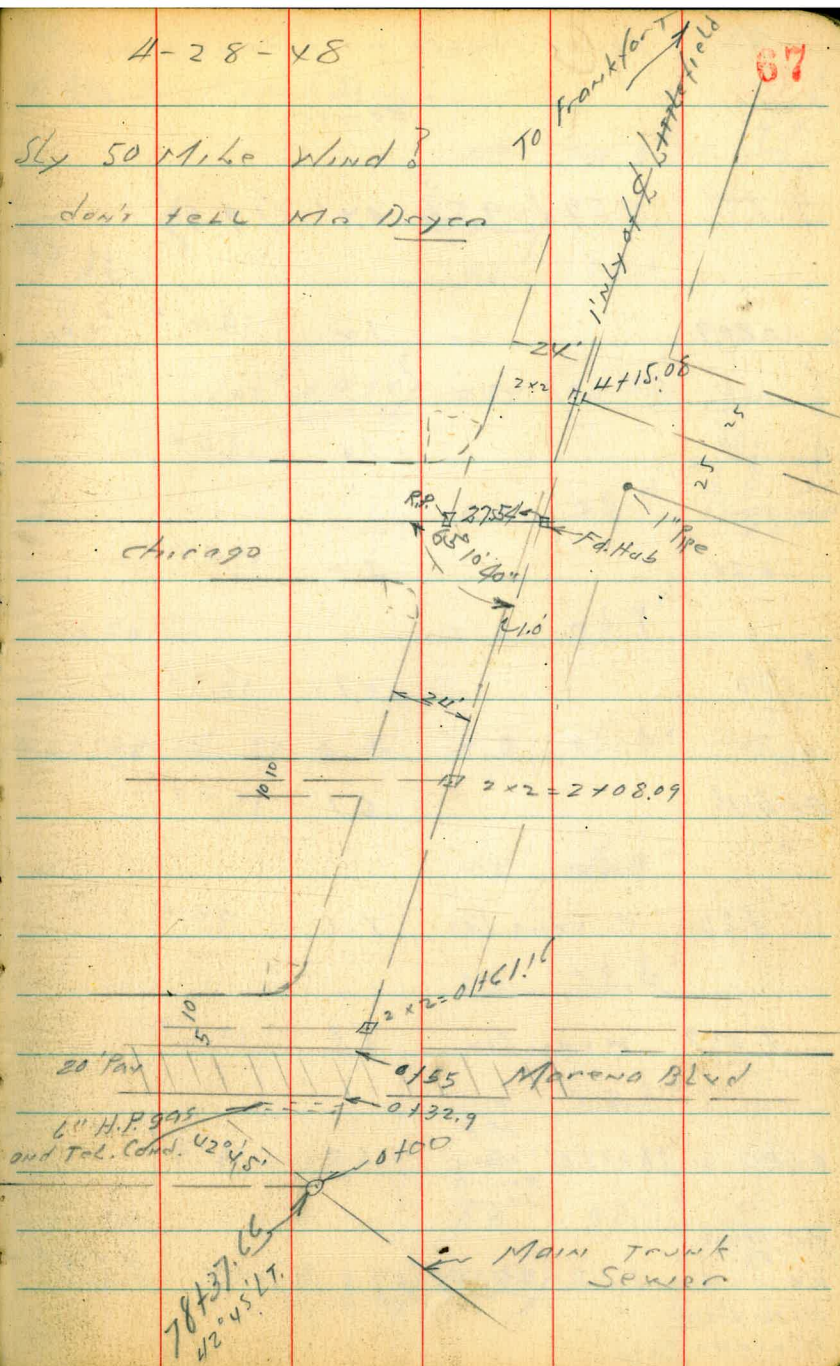
Sewer Levels on Littlefield  
1' nly of E ST.  
Old Sketch 1821-67

E Frankfort ST



4-28-48

Sly 50 Mile Wind?  
don't tell Ma Deyca



67



Sewer Levels on Littlefield

|                             | ℄<br>Sewer                                            | Rt                                                 |
|-----------------------------|-------------------------------------------------------|----------------------------------------------------|
| T.P.                        | 9.59 $\left\langle \frac{29.53}{17} \right\rangle$    | 0.46 $\left\langle \frac{19.94}{17} \right\rangle$ |
| 2 + 0809                    | 1.2                                                   | 19.2 ✓<br>2.9<br>17.5 ✓<br>17.5                    |
| 2                           | 1.4                                                   | 19.0 ✓                                             |
| + 50                        | 3.0                                                   | 17.4 ✓                                             |
| 1 + 100                     | 4.7                                                   | 15.7 ✓                                             |
| 0 + 6116                    | 6.7                                                   | 13.7 ✓                                             |
| + 55 E. edge Pav            | 6.6                                                   | 13.8 ✓                                             |
| + 329 W edge Pav            | 6.8                                                   | 13.6 ✓                                             |
| 0 + 00 = 78 + 37.66         | M.H. Main Trunk Sewer<br>6.5                          | 13.9 ✓                                             |
| BM. Chisel 56.<br>N.E. curb | 5.65 $\left\langle \frac{20.40}{14.75} \right\rangle$ | 14.75                                              |
| Littlefield<br>Morena Blvd  |                                                       | 10' sly from<br>℄ Return                           |

Morena Blvd  
Ely to Frankfort

|           | ℄                                                  | Rt                                                            |
|-----------|----------------------------------------------------|---------------------------------------------------------------|
| 6         | 7.9                                                | 34.0 ✓<br>30.0<br>9.9<br>150                                  |
| + 50      | 9.8                                                | 30.1 ✓                                                        |
| T.P. 1100 | 0.59 $\left\langle \frac{39.94}{11} \right\rangle$ | 28.94 ✓                                                       |
| 5         | 0.8                                                | 28.7 ✓<br>Floor<br>House<br>2.9<br>26.6<br>26.1<br>3.1<br>120 |
| + 50      | 2.6                                                | 26.9 ✓                                                        |
| 4 + 1508  | ℄ ST to Rt<br>3.9                                  | 25.6 ✓<br>22.3 ✓<br>7.2<br>150                                |
| 4         | 4.5                                                | 25.0 ✓                                                        |
| + 50      | 5.9                                                | 23.6 ✓                                                        |
| 3         | 7.2                                                | 22.3 ✓                                                        |
| 2 + 50    | 8.8                                                | 20.7 ✓                                                        |
|           |                                                    | $\left\langle \frac{29.53}{1} \right\rangle$                  |



|       |       | F<br>sewer | Rt                                                                  |
|-------|-------|------------|---------------------------------------------------------------------|
|       | +50   | 2.8        | 49.0 ✓                                                              |
| 10    |       | 4.0        | 47.4 ✓<br>$\begin{array}{r} 47.8 \\ 3.6 \\ \hline 750 \end{array}$  |
|       | +50   | 5.3        | 46.1 ✓                                                              |
| 9     |       | 6.6        | 44.8 ✓                                                              |
|       | +50   | 7.9        | 43.5 ✓                                                              |
| 8     |       | 9.2        | 42.0 ✓<br>$\begin{array}{r} 20.0 \\ 11.4 \\ \hline 750 \end{array}$ |
| T.P.  | 11.90 | 0.45       | 39.49 ✓                                                             |
|       | +50   | 0.0        | 39.9 ✓                                                              |
| 7     |       | 3.1        | 36.8 ✓                                                              |
| (+50) |       | 5.5        | 34.4 ✓                                                              |

$\langle 39.94 \rangle$

|      |       | F<br>sewer | Rt                                                               |
|------|-------|------------|------------------------------------------------------------------|
|      | +75   | 2.9        | 68.1 ✓                                                           |
|      | +50   | 4.6        | 66.4 ✓                                                           |
|      | +25   | 6.9        | 64.1 ✓                                                           |
| T.P. | 8.77  | 0.17       | 62.21 ✓                                                          |
|      |       |            | $\langle 70.98 \rangle$                                          |
| 13   |       | 0.4        | 62.0 ✓                                                           |
|      |       |            | $\langle 62.0 \rangle$                                           |
|      |       |            | $\times 88$                                                      |
|      |       |            | $\times 750$                                                     |
|      |       |            | de Morenci St per Ba 79 <sup>4</sup><br>cross Erie St water line |
|      |       | 3.4        | 59.0 ✓                                                           |
| 12   |       | 7.1        | 55.3 ✓                                                           |
|      |       |            | $\begin{array}{r} 54.0 \\ 8.4 \\ \hline 750 \end{array}$         |
|      | +150  | 9.9        | 52.5 ✓                                                           |
| T.P. | 11.65 | 0.66       | 50.73 ✓                                                          |
|      |       |            | $\langle 62.38 \rangle$                                          |
|      | +100  | 0.9        | 50.5 ✓                                                           |
|      |       |            | $\langle 51.39 \rangle$                                          |



Check to NW BP BM  
Frankfort + Gardena

$\begin{array}{r} \text{P. 10} \\ \text{Record} \\ 6.85 \quad \langle 64.13 \rangle \quad 64.12 \end{array}$

16+05 ± approx  
Frankfort

4.8 66.2 ✓

56.6 ✓

$\frac{14.4}{150}$

$\left\{ \begin{array}{l} 50' \text{ E.} = 66.2' + 2' \text{ South thence} \\ \text{to point opposite hence} \\ 100' \text{ to E.} \end{array} \right.$

9/16

4.9 66.1 ✓

+50

6.8 64.2 ✓

15

6.7 64.3 ✓

+75

5.9 65.1 ✓

+50

4.4 66.6 ✓

+25

3.2 67.8 ✓

14+00

2.4 68.6 ✓

62.8 ✓

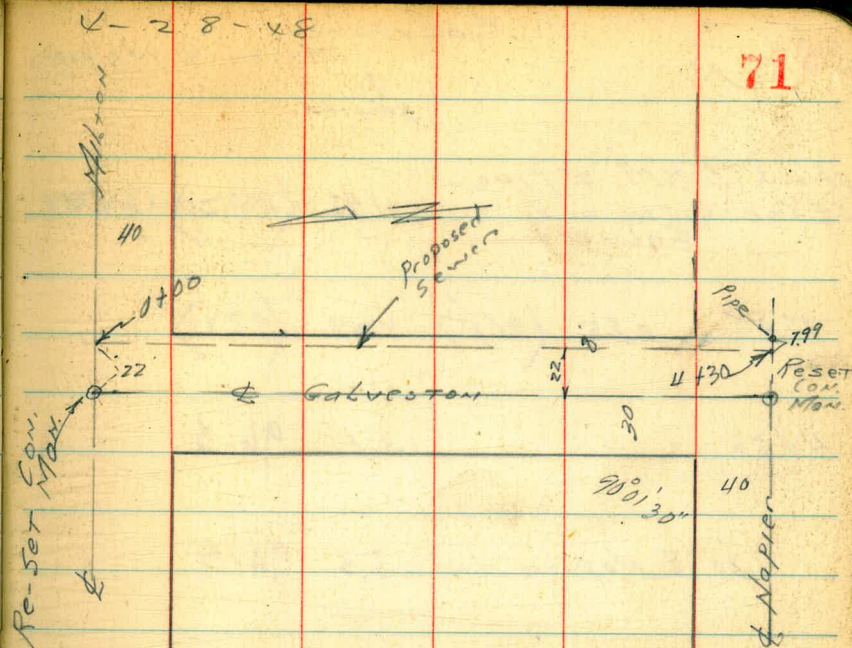
$\frac{8.2}{150}$

40.98 ✓



Sewer Levels on Galveston  
Milton to Napier St  
&  
Sewer

|                    |          |         |      |         |
|--------------------|----------|---------|------|---------|
| 2                  |          | 1.0     | 88.1 | ✓       |
| +50                |          | 4.5     | 84.6 | ✓       |
| 1100               |          | 8.6     | 80.5 | ✓       |
| T.P.               | 11.49    | <89.09> | 0.60 | <77.60> |
| +50                |          | 1.2     | 77.0 | ✓       |
| 0100               | & Milton | 1.8     | 76.4 | ✓       |
| T.P.               | 13.02    | <78.20> | 0.93 | <65.18> |
| T.P.               | 11.85    | <66.11> | 0.50 | <54.26> |
| BM B.P.<br>SW Ret. | 12.67    | <54.76> |      | <42.09> |



Milton + Erie Sts FB 1821-62



Galveston  
Milton to Napier

♀  
Sewer

12

check to BM 2" Pipe  
SE Con Driven and  
Galveston

11.95

~~84.20~~

84.21

FB. 1821-57

T.P.

0.85

~~96.15~~

4.29

~~95.30~~

47.50

3.1

96.5

130 E Napier

5.3

94.3

4

6.7

92.9

7.50

6.5

93.1

3

7.6

92.0

27.50

9.3

90.3

T.P.

10.68

~~99.59~~

0.18

~~88.91~~

~~99.09~~



Sewer levels on Ingulf St.  
 Erie St. Ely to Alley  
 See p. 48 and 53

1175 Alley 3.9 80.8 ✓

1130 8.8 75.9 ✓

T.P. 12.55 ~~184.73~~ 1.85 ~~72.18~~

1100 0.9 73.1 ✓

+65 3.8 70.2 ✓

+35 6.5 67.5 ✓

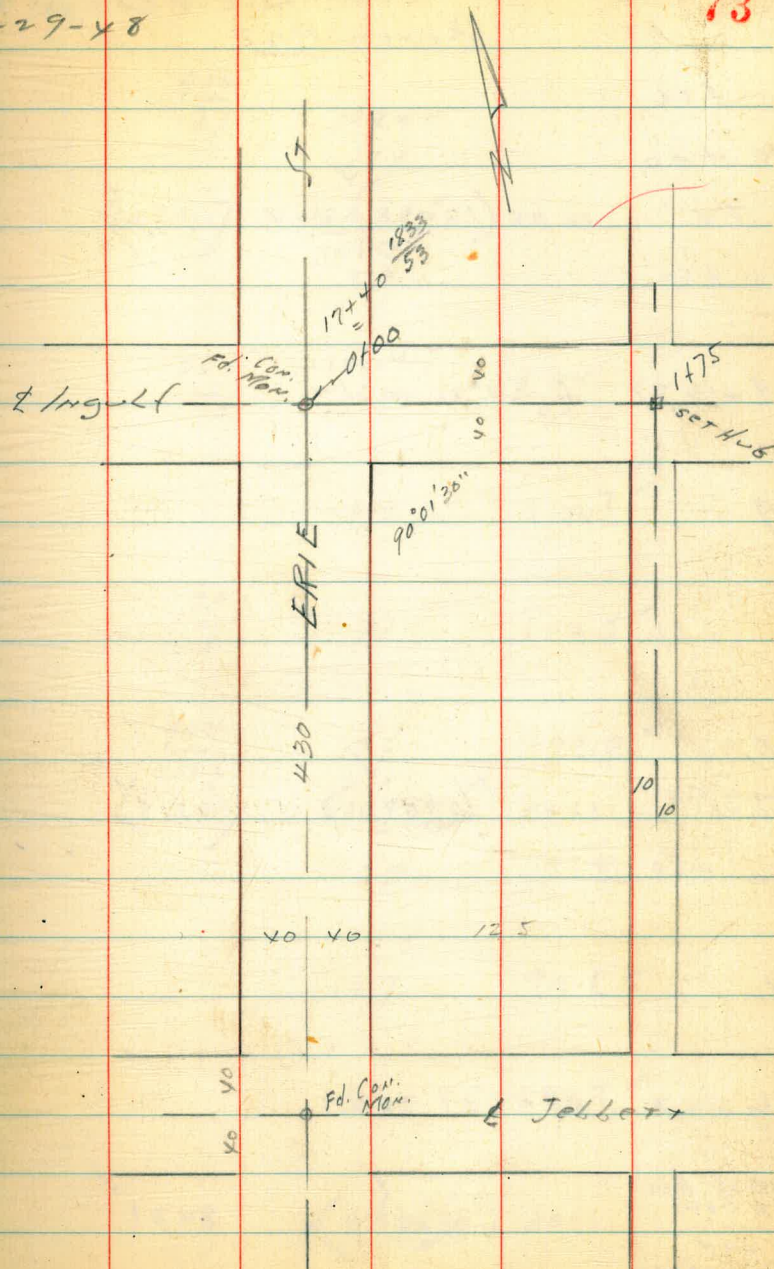
+10 7.8 66.2 ✓

0100 9.3 64.7 ✓

BM. Nail  
 SW. PP. 4149 10.15 ~~7403~~ 63.88  
 Jellert  
 and  
 Eric  
 P. 52

4-29-48

73





Levels on Sewer line change on Orten ST. <sup>LT</sup>  $\frac{\$}{R}$

+06  
 10 +00  
 T.P. 12.85 (120.28) 2.14 <107.43>  
 +50

9 +13.97  $\Delta$  23°36'30" LT

9

+50

8  
 T.P. 12.42 (109.57) 0.11 <97.15>  
 +50

7

L +48  $\Delta$  47°38'30" LT

BM. 12" Pipe  
 SE Cor.  
 Orten  
 and  
 Galveston  
 P. 41  
 13.05 (97.26) 84.21 <97.26>

99.5  
 $\frac{2.3}{109.9}$  ✓  
 104  
 $\frac{120.28}{107.25}$  ✓  
 $\frac{2.3}{105.4}$  ✓

90.5  
 $\frac{7.3}{105.4}$  ✓  
 4.2  $\frac{6'' W.}{7.5}$

4.9 104.7 ✓

94.5  
 $\frac{3}{71}$  102.5 ✓

99.5  
 $\frac{2.3}{96}$  100.0 ✓  
 <109.57>  
 0.9 97.3

2.7 94.6 ✓

5.6 91.7 ✓

<97.26>



$$13 + 099 = 13 + 12 \text{ P } 28$$

13

+79

12 + 50

T.P. 1245 (13205) 0.68  $\leftarrow$  (11960)  $\checkmark$

12

$$11 + 5275 \Delta 10^{\circ} 20' \text{ LT.}$$

11 + 39x

11

10 + 49

10 + 29

$$\leftarrow (12028) \checkmark$$

$$\begin{array}{r} 121.9 \checkmark \\ 41 \end{array}$$

$$\begin{array}{r} 132.05 \\ \times 1.5 \\ \hline 197.9 \\ 1821-55 \\ \hline 127.9 \checkmark \end{array}$$

$$\begin{array}{r} 129.5 \checkmark \\ 55 \end{array}$$

$$\begin{array}{r} 995 \\ \hline 13 \end{array} \quad \begin{array}{r} 124.0 \checkmark \\ 80 \end{array}$$

$$\begin{array}{r} 121.5 \checkmark \\ 10.5 \end{array}$$

$$\leftarrow \begin{array}{r} 132.05 \checkmark \\ 118.3 \checkmark \\ 20 \end{array}$$

$$\begin{array}{r} 116.1 \checkmark \\ 42 \end{array}$$

$$\begin{array}{r} 995 \\ \hline 13 \end{array} \quad \begin{array}{r} 115.1 \checkmark \\ 52 \end{array}$$

END 6" W.  
5

$$\begin{array}{r} 113.4 \checkmark \\ 69 \end{array}$$

$$\begin{array}{r} 995 \\ \hline 34 \end{array} \quad \begin{array}{r} 111.5 \checkmark \\ 88 \end{array}$$

$$\begin{array}{r} 995 \\ \hline 37 \end{array} \quad \begin{array}{r} 111.0 \checkmark \\ 93 \end{array}$$

$$\leftarrow \begin{array}{r} 12028 \checkmark \end{array}$$



Sewer Levels, Gardena Ave + Galveston

Galveston St

Fd. Pipe

Galveston

Ex. M.H. Berry St. 76

Linda Vista Sewer

Empire

Fd. Iron Pipe

House

Gardena Ave

Frankfort

Fd. Pipe

FANON

Hub

Setchler  
ET 0 15  
on curb

2463.5  
58°50' RT

21  
50  
5.5  
P.V.  
NAIL

Ed. nail  
set hub

1590 P.2  
no map?  
1606

1196.8  
35°40' P.

229.0

6177

6138.0  
78°37' LT

10/10

40

22

ST.

38



Sewer Levels on Gardena Ave  
Frankfort to Galveston  
via Empire St. to Linda Vista MA

X 1944 NW Cor house

3 + 40

T.P. 679 (6023) 1241 (53.44)

2 + 65.4 Lot Cor.  
75° RT to NW Cor house

1 + 96.8  $\Delta$  35° 40' R. to Cor. Lot  
& alley and Gardena

+ 65

+ 50

1

0 + 42 = 0 + 00 AB. 159-2 E.L. Frankfort

0 + 00

NW BP  
Frankfort 173 (6585) 6412  
and  
Gardena Ave

LT R 777

60.5 59.9 ✓  
+ 0.3 23 = ground NW Cor house  
Fl. elev.

55.7 ✓  
4.5

60.23 ✓

59.8 ✓  
13.0

54.4 ✓ ✓  
11.4

56.1 ✓ 59.0 ✓  
9.7 6.9  
703 fl.  
House

57.0 ✓  
8.8

58.5 ✓  
7.3

60.6 ✓  
5.2

63.3 ✓  
2.5

65.85 ✓



Series levels  
 on Frankfort St  
 Listen to Kane X10.31x74  
 Moore  
 Begg  
 Sherman  
 Bunch  
 1.11.49

1750

1700

T.P.

12.52

$\langle 87.23 \rangle$

0.78

$\langle 75.21 \rangle$

0750

0700

T.P.

12.65

$\langle 75.99 \rangle$

0.35

$\langle 63.34 \rangle$

T.P.

12.90

$\langle 63.69 \rangle$

0.79

$\langle 50.79 \rangle$

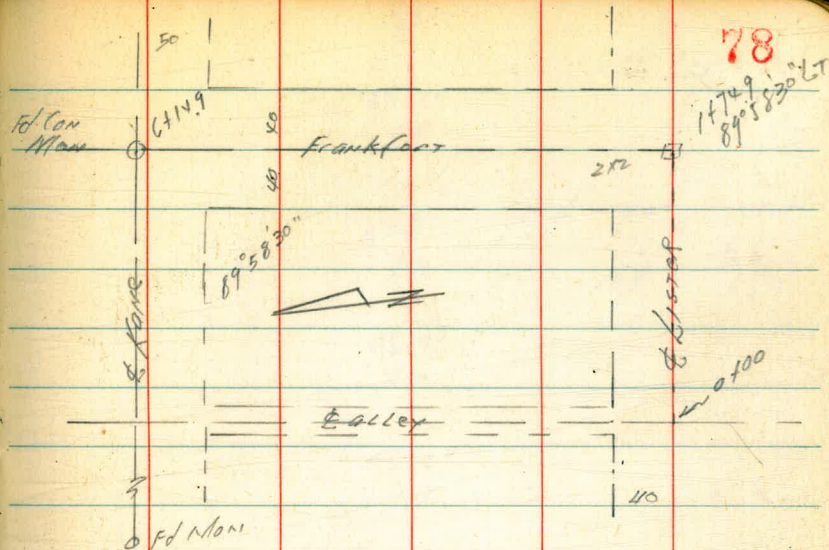
SW B.P.  
MILTON  
ERIC

9.48

$\langle 51.58 \rangle$

42.10

P.49



5 men  
 4.4  
 83.3 ✓

9.2 ✓  
 78.5 ✓  
 87.23 ✓

2.8  
 73.2 ✓

9.3  
 66.7 ✓

$\langle 75.99 \rangle$



5

+50

4

+50

2/00

T.P.

+50

2

+90

1/74.9

89° 58' 30" Lt.

T.P. RP spike  
on RP  
station  
listen &  
Franklin

1122

95.59

336

94.37

87.73

8

FLY 79

93.11  
88

92.71  
92

107.4  
+5.5  
75

114.9  
+13.0  
105

114.4  
+12.5  
750

95.71  
62

95.01  
69

91.71  
102

105.7  
+3.8  
75

109.1  
+0.2  
750

91.71  
102  
94.31  
63

86.81  
82

84.91  
107

85.81  
98

90.91  
4.7  
75

89.21  
6.4  
125

87.71  
7.8  
750

95.59

on station



79 1/2

at Littlefield  
and Erie

St. worn

P.T.

Sta 12483.8 = E Marconi St

Sta 12488 cross water line  
at Erie St 1/4 N



ground check

8470 E Kane & alley  
to west  
PVC 17.3 73° 73.0

T.P 027 <90.31> 1184 <90.04>

1149 E Kane St 94.0  
7.9

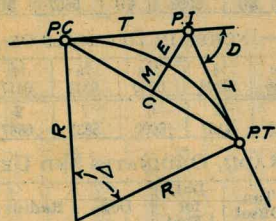
C 93.4  
8.5

5750 93.4 102.1 1167  
8.5 +2.7 +14.8  
75 75

<101.88>

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

- Radius  $= R = \frac{50}{\sin. \frac{D}{2}}$  (1) Degree of Curve  $= D$  and  $\sin. \frac{D}{2} = \frac{50}{R}$  (2)
- Tangent  $= T = R \tan \frac{\Delta}{2}$  (3) Length of Curve  $= L = 100 \frac{\Delta}{D}$  (4)
- Middle ordinate  $= M = R(1 - \cos. \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)
- External  $= E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos. \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)
- Long Chord  $= C = 2 R \sin. \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I. = Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8 \frac{1}{2} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I. -  $T = 157. + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 - Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8 \frac{1}{2} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8 \frac{1}{2} = 115.27$  and from Table V correction = .10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .



DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.2  | 8.3  | 8.5  | 8.6  | 8.8  | 8.9  | 9.1  | 9.2  | 9.4  | 0  |
| 1  | 9.5  | 9.7  | 9.8  | 10.0 | 10.1 | 10.3 | 10.4 | 10.6 | 10.7 | 10.9 | 1  |
| 2  | 11.0 | 11.2 | 11.3 | 11.5 | 11.6 | 11.8 | 11.9 | 12.1 | 12.2 | 12.4 | 2  |
| 3  | 12.5 | 12.7 | 12.8 | 13.0 | 13.1 | 13.3 | 13.4 | 13.6 | 13.7 | 13.9 | 3  |
| 4  | 14.0 | 14.2 | 14.3 | 14.5 | 14.6 | 14.8 | 14.9 | 15.1 | 15.2 | 15.4 | 4  |
| 5  | 15.5 | 15.7 | 15.8 | 16.0 | 16.1 | 16.3 | 16.4 | 16.6 | 16.7 | 16.9 | 5  |
| 6  | 17.0 | 17.2 | 17.3 | 17.5 | 17.6 | 17.8 | 17.9 | 18.1 | 18.2 | 18.4 | 6  |
| 7  | 18.5 | 18.7 | 18.8 | 19.0 | 19.1 | 19.3 | 19.4 | 19.6 | 19.7 | 19.9 | 7  |
| 8  | 20.0 | 20.2 | 20.3 | 20.5 | 20.6 | 20.8 | 20.9 | 21.1 | 21.2 | 21.4 | 8  |
| 9  | 21.5 | 21.7 | 21.8 | 22.0 | 22.1 | 22.3 | 22.4 | 22.6 | 22.7 | 22.9 | 9  |
| 10 | 23.0 | 23.2 | 23.3 | 23.5 | 23.6 | 23.8 | 23.9 | 24.1 | 24.2 | 24.4 | 10 |
| 11 | 24.5 | 24.7 | 24.8 | 25.0 | 25.1 | 25.3 | 25.4 | 25.6 | 25.7 | 25.9 | 11 |
| 12 | 26.0 | 26.2 | 26.3 | 26.5 | 26.6 | 26.8 | 26.9 | 27.1 | 27.2 | 27.4 | 12 |
| 13 | 27.5 | 27.7 | 27.8 | 28.0 | 28.1 | 28.3 | 28.4 | 28.6 | 28.7 | 28.9 | 13 |
| 14 | 29.0 | 29.2 | 29.3 | 29.5 | 29.6 | 29.8 | 29.9 | 30.1 | 30.2 | 30.4 | 14 |
| 15 | 30.5 | 30.7 | 30.8 | 31.0 | 31.1 | 31.3 | 31.4 | 31.6 | 31.7 | 31.9 | 15 |
| 16 | 32.0 | 32.2 | 32.3 | 32.5 | 32.6 | 32.8 | 32.9 | 33.1 | 33.2 | 33.4 | 16 |
| 17 | 33.5 | 33.7 | 33.8 | 34.0 | 34.1 | 34.3 | 34.4 | 34.6 | 34.7 | 34.9 | 17 |
| 18 | 35.0 | 35.2 | 35.3 | 35.5 | 35.6 | 35.8 | 35.9 | 36.1 | 36.2 | 36.4 | 18 |
| 19 | 36.5 | 36.7 | 36.8 | 37.0 | 37.1 | 37.3 | 37.4 | 37.6 | 37.7 | 37.9 | 19 |
| 20 | 38.0 | 38.2 | 38.3 | 38.5 | 38.6 | 38.8 | 38.9 | 39.1 | 39.2 | 39.4 | 20 |
| 21 | 39.5 | 39.7 | 39.8 | 40.0 | 40.1 | 40.3 | 40.4 | 40.6 | 40.7 | 40.9 | 21 |
| 22 | 41.0 | 41.2 | 41.3 | 41.5 | 41.6 | 41.8 | 41.9 | 42.1 | 42.2 | 42.4 | 22 |
| 23 | 42.5 | 42.7 | 42.8 | 43.0 | 43.1 | 43.3 | 43.4 | 43.6 | 43.7 | 43.9 | 23 |
| 24 | 44.0 | 44.2 | 44.3 | 44.5 | 44.6 | 44.8 | 44.9 | 45.1 | 45.2 | 45.4 | 24 |
| 25 | 45.5 | 45.7 | 45.8 | 46.0 | 46.1 | 46.3 | 46.4 | 46.6 | 46.7 | 46.9 | 25 |
| 26 | 47.0 | 47.2 | 47.3 | 47.5 | 47.6 | 47.8 | 47.9 | 48.1 | 48.2 | 48.4 | 26 |
| 27 | 48.5 | 48.7 | 48.8 | 49.0 | 49.1 | 49.3 | 49.4 | 49.6 | 49.7 | 49.9 | 27 |
| 28 | 50.0 | 50.2 | 50.3 | 50.5 | 50.6 | 50.8 | 50.9 | 51.1 | 51.2 | 51.4 | 28 |
| 29 | 51.5 | 51.7 | 51.8 | 52.0 | 52.1 | 52.3 | 52.4 | 52.6 | 52.7 | 52.9 | 29 |
| 30 | 53.0 | 53.2 | 53.3 | 53.5 | 53.6 | 53.8 | 53.9 | 54.1 | 54.2 | 54.4 | 30 |
| 31 | 54.5 | 54.7 | 54.8 | 55.0 | 55.1 | 55.3 | 55.4 | 55.6 | 55.7 | 55.9 | 31 |
| 32 | 56.0 | 56.2 | 56.3 | 56.5 | 56.6 | 56.8 | 56.9 | 57.1 | 57.2 | 57.4 | 32 |
| 33 | 57.5 | 57.7 | 57.8 | 58.0 | 58.1 | 58.3 | 58.4 | 58.6 | 58.7 | 58.9 | 33 |
| 34 | 59.0 | 59.2 | 59.3 | 59.5 | 59.6 | 59.8 | 59.9 | 60.1 | 60.2 | 60.4 | 34 |
| 35 | 60.5 | 60.7 | 60.8 | 61.0 | 61.1 | 61.3 | 61.4 | 61.6 | 61.7 | 61.9 | 35 |
| 36 | 62.0 | 62.2 | 62.3 | 62.5 | 62.6 | 62.8 | 62.9 | 63.1 | 63.2 | 63.4 | 36 |
| 37 | 63.5 | 63.7 | 63.8 | 64.0 | 64.1 | 64.3 | 64.4 | 64.6 | 64.7 | 64.9 | 37 |
| 38 | 65.0 | 65.2 | 65.3 | 65.5 | 65.6 | 65.8 | 65.9 | 66.1 | 66.2 | 66.4 | 38 |
| 39 | 66.5 | 66.7 | 66.8 | 67.0 | 67.1 | 67.3 | 67.4 | 67.6 | 67.7 | 67.9 | 39 |
| 40 | 68.0 | 68.2 | 68.3 | 68.5 | 68.6 | 68.8 | 68.9 | 69.1 | 69.2 | 69.4 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For some slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \div 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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