

1834

1834

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

CITY ENGINEER'S OFFICE

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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6 + (20 - 16) * 2 or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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Rogers - Rosecrans west sewer Prelim	2-12
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Rogers St. Sewer profile

Rosecrans - west.

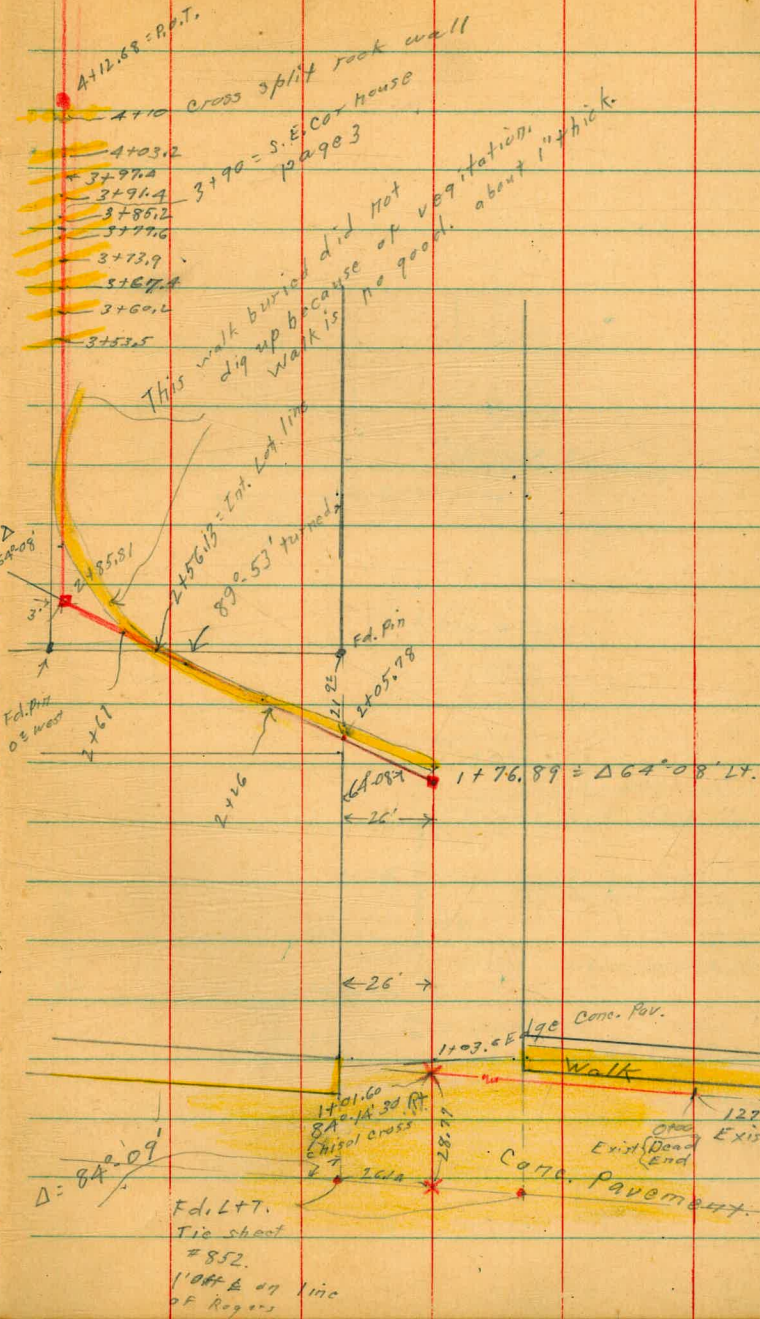
3-3-48

W.O.# 80087

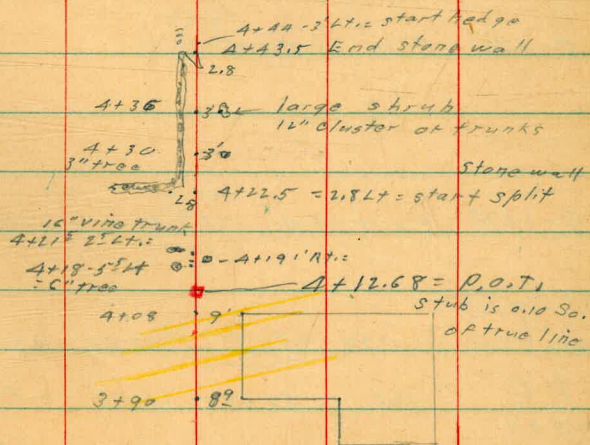
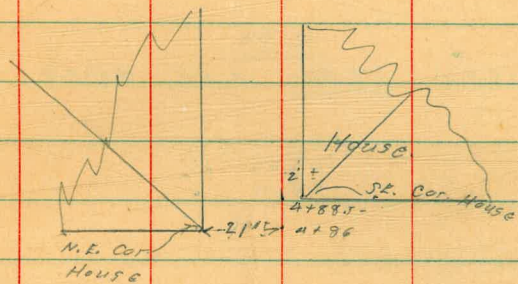
Sammermeyer
 McCoy X
 W. Moore
 E Sherman

INDEXED
MAR 8 1948

Fd. pin.
 Used
 as
 correct



Not to scale past station A+12.68



Rogers St. Rosecrans - west
Sewer profile

0+75[±] 1st Rt. = End. Exist curb

46.73
11.87

T.P. 12.52 57.60 0.54 45.08

57.60

0+50

44.75
0.87

0+00 = Existing D.E. as per plan.

42.75
2.87
par

0-126[±] Rim of Exist M.H.

37.72
7.90

0-127[±] Exist M.H. - 1st Rt. = Face Conc. Curb.

31.94
13.68
invert.

NE. Prop. pipe
L.S. 2341
Rogers + Rosecrans 0.54 45.62 11.80 45.08 B.M.#1

45.62

T.P. 165 56.88 13.07 55.23

NE.B.P.
Perry +
Rosecrans 4.15 68.30 → 64.15

T.P. 12.40 82.39 0.18 69.99

1+68 3° Lt. = End 2' wide E.W. hedge

1+40

T.P. 13.17 70.17 0.60 57.00

1+18

1+15 4° Lt. = Ctr. 2' wide E.W. hedge

1+12

1+04

1+03° = End paving

1+01⁶⁰ Δ 84°-14'-30° RT.

57.60

61.5

8.7

70.17

55.9

1.7

49.6

8.0

46.7

10.9

46.42

11.18

46.40

11.20

57.60

2+50 E of 2' wide N. Fly + S. Fly, conc. walk

86.8
8.0

T.P. 12.65 94.84 0.20 82.19

94.84

2+26 Int. East edge walk

82.1
0.3

2+15

80.0
2.4

2+00

76.9
5.5

This walk is about 1" "thin" & in ^{condition} poor sh.

1+76⁸⁹

2' RT. (off Fwd Tang) = E. Edge 2' wide conc. walk
Δ 64'-08" Lt. B.M. 02

71.54
10.85
on
Hub

1+70

70.5
11.9

82.39

82.39

±. Walls average 3 1/2" wide.

walls. These walls run approx. 60° Rt. to

3+53^E Start series of terrace retaining

T.P. 12.38 117.95 0.62 105.57

3+45

3+10

2+85⁸¹ Cont.

90° to Fwd. Tang.

2+85⁸¹ Δ 64°-08' Rt. Section taken at

T.P. Top of
3rd Marker 12.32 106.19 0.97 93.87

2+67 Ely. edge conc. walk.

94.84

±	107.8	109.7
107.9	102	8.3
10.1		
±	±	±
Grd	Base of wall	Top of wall

7

117.95

104.8
1.4

95.3
10.9

98.7	92.5	95.3
7.5	13.7	10.9
1.80	1.40	1.15

99.0	98.0	90.5	91.8
7.2	8.2	15.7	12.4
60	38	8	

106.19

89.2
5.6

94.84

3+74²

±

113.7

4.3

3+73²

cross wall

112.5

112.4

113.8

5.5

5.6

4.2

±

B

T

±

±

3+68

112.3

5.7

3+67⁴

cross wall

111.2

111.2

112.4

6.8

6.8

5.6

±

B

T

±

3+60⁵

111.0

7.0

±

3+60²

cross wall

109.7

109.9

110.0

8.3

8.1

7.0

±

B

T

±

±

3+55

17' Lt. = 5" trunk shrub.

± = ground

B = base of wall

T = top of wall

3+54

117.95

109.7

8.3

117.95

3+91²

3+91⁴

Cross wall

T.P. 9.73 126.47 1.21 116.74

3+90 8³ Rt. = S.E. Cor Frame house

3+85^E

3+85^W Cross wall.

3+80

3+79^E Cross wall

117.95

±

9

117.8
8.7
±

116.7 116.6 117.9
2.8 9.7 8.6
± ± ±
126.47

116.6 116.4 121.5 117.7
1.4 1.6 +3.5 0.3
8.2 8.2
± Floor of House
± Main soil
± Pipe below
dropping into
tank.

116.6
1.4

115.4 115.2 116.7
2.6 2.8 1.3
± ± ±
± ± ±

115.1
2.9

114.1 113.8 115.3
3.9 4.2 2.7
± ± ±
± ± ±

117.95

A+12⁶120.6
5.9

top of wall 06 wide.

A+12

Cross split rock wall.

120.6	120.6	122.4
5.9	5.9	4.1
G	B	T
	±	±

A+03^F120.5
6.0A+03^E cross last conc. wall

119.4	119.4	120.5
7.1	7.1	6.0
G	B	T
	±	±

3+97^Z119.3
7.23+97^A cross wall

117.8	117.8	119.4
8.7	8.7	7.1
G	B	T
	±	±

126.47126.47

4+54 1x1 P.O.T.

T.P. 10.56 144.76 1.46 134.20

4+44 3° Lt. = start 2' wide hedge.

4+43^E 2⁸ Lt. = End split rock wall.T.P. 9.90 135.66 0.71 125.76

4+36 3° Rt. = 12" diam. cluster of small tree trunks

4+30 3° Rt. = 3" diam. tree

4+22^E 2⁸ Lt. = start split rock wall.4+21^E 2' Lt. = 16" diam vine trunk.

4+19 1' Rt. = 4" diam (trunk) shrub

4+18^E 5^E Lt. = 6" diam tree

4+14

4+12⁶⁸ on stub of 1/2 of 4.126.47

4

136.96

7.80

0.7

5.46

144.76

133.2	132.7	132.7	132.6	124.9
2.5	3.0	3.0	3.1	7.8
3.2	2.8	2.9		<u>2.5</u>
Top of wall	Base of wall	0		
			<u>135.66</u>	

129.5	126.3	125.7
+3.0	0.2	0.8
4.0	2.8	
Top of wall	Base of wall	8 Brd.

122.4

4.1

121.5

5.0

2.5

122.30

4.17

0.1126.47

S.E. Quoltraugh
 + San Elijo Top. Hydt. 6.90 160.09 0.07 ^(160.02) Top. Hite Hydt.

T.P. 10.42 166.99 0.35 156.57

T.P. 12.47 156.92 0.31 144.15

grade.

These three houses well above

4+88E = 2' Rt. = S.E. Cor. house

also 106 Lt. = N.E. Cor. house

4+86 } 21' Lt. = N.E. Cor. house

rock wall. Do not go beyond ^{here}

4+66 = start flag stone terrace &
 3' Lt. = E.W. Hedge

144.76

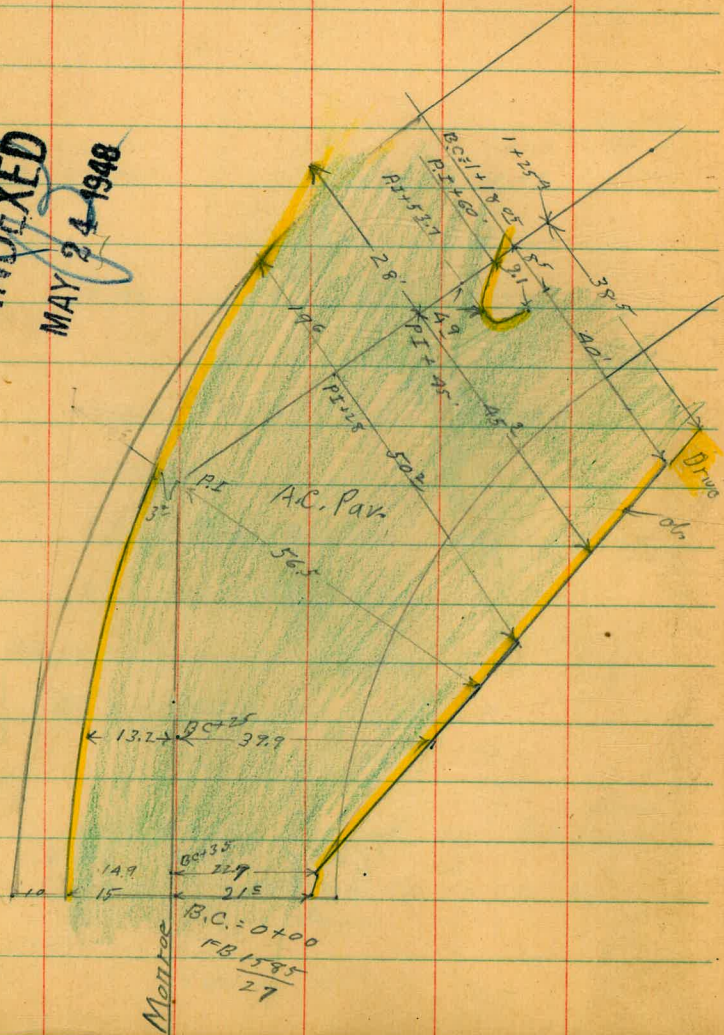
140.0	139.7	141.6
4.8	5.1	3.2
0.	±	±
	Base wall	on terrace

Aldine Drive. Pavement
 X-Sec. Monroe - 200' North

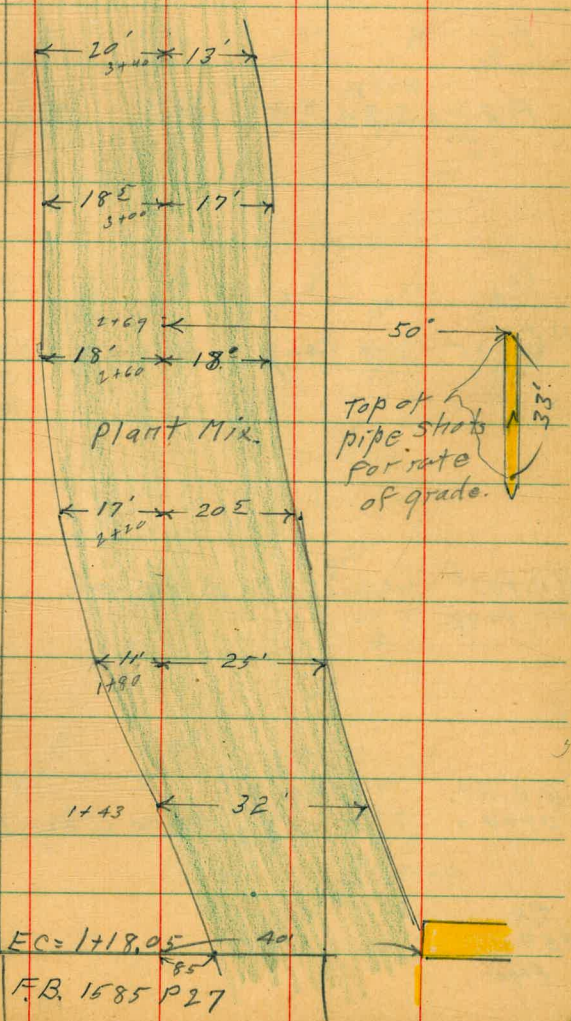
5-21-48
 W.O.# 21001

Sommermeier
 McCoy
 W Moore
 Sherman

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Tang. line
 Aldine Dr.



Aldine Monroe North.

P.I. +28° on Fwd. Tang.

tang =
P.I. - 63.84

B.G. +25 on Tang

B.C. +03 E 22° RT = Δ in cl.
on tang.

B.C. RT. 21° RT. } basin grate.
0+00 = 15' LT } = Face Cb. 21° RT. = catch

T.R.
FB# 12.06 335.54 - 323.48
page

B.L.

14

334.40

1.14
176
0

333.04

2.50

331.22

4.32
20

330.02

5.52
35

329.11

6.83
30 =
0

331.79

7.80
3.2
0

331.70

3.84

331.36

4.18
15

331.04

4.50
37

329.19

6.35
56.5
0

329.33

6.21
13.2
0

329.54

6.00

329.41

6.13
12

328.90

6.64
25

328.77

6.77
38.9
0

327.80

7.74
22.7
0

328.29

7.25
15
0

328.65

6.89
7

328.86

6.69

328.75

6.77
6

327.63

7.91
21.6
on grate

335.54

1+25⁴ 38⁵ RT. = End Conc. Drive

E.P. = Edge oil pav.

= Sta. 1+18.05 F.B. 15.85 P. 27 = E.C.
63.8A Ahead of Tang on Tang =

Tang + 63⁵ 40' RT. = End Exist cl.

P.I. + 60 9¹ RT. = End Cl.

P.I. + 53⁷ 4² RT. of Tang. = Nose cl. Rot

P.I. + 45⁹ on Fwd Tang

329.64
5.70
385
oil pav.
+ Drive

330.1 330.3 329.6
5.4 5.2 5.9
8.5 24 40
E.P.

329.81
5.72
40
cl

322.87 320.6
2.67 5.0
9.1 9.1
top cl oil pav.

333.23 332.81 333.76
2.31 2.73 1.78
4.9 4.9
pav top cl

335.85 335.21 333.22 331.32 330.53 329.44
+0.31 0.33 2.32 4.22 5.01 6.10
28 18 15 28 45.3
Q

335.54

B.L.

3+00

312.9	313.9	314.2	313.9
11.0	10.0	9.7	10.0
185		9	17
E.R.			E.R.

2+69

50' Rt. - outlet
24" Conc. Culvert

12.66 - Rod used
1.50 level
11.06 - Below X for
11.49 Best rod.
22.55 = Rod total

301.36	303.61	305.69
22.55	20.30	18.22
50	outlet	outlet
Invert		-331

2+60

316.3	317.3	317.6	317.3
7.6	6.6	6.3	6.6
18		9	18
E.R.			E.R.

shots on top of pipe for rate of fall.

2+20

320.3	321.1	321.3	320.6
3.6	2.8	2.6	3.3
17		7	20.5
E.R.	323.91		E.R.

T.P. 0.29 323.91 11.92 323.62

1+80

324.5	325.1	325.4	325.0
11.0	10.4	10.1	10.5
11		10	25
E.R.			E.R.

1+43

328.2	328.6	328.4
7.3	6.9	7.1
E.R.	16	32
		E.R.

335.54

Aldine Dr.

17

T.P. from P. 1A.

11.06

323.48

322.42

T.P.

10.92

334.54

0.29

323.62

3+40

323.91

309.6

14.3

20

E.R

310.8

13.1

311.5

12.4

13

EP

xsec Electric Ave.

6-15-48

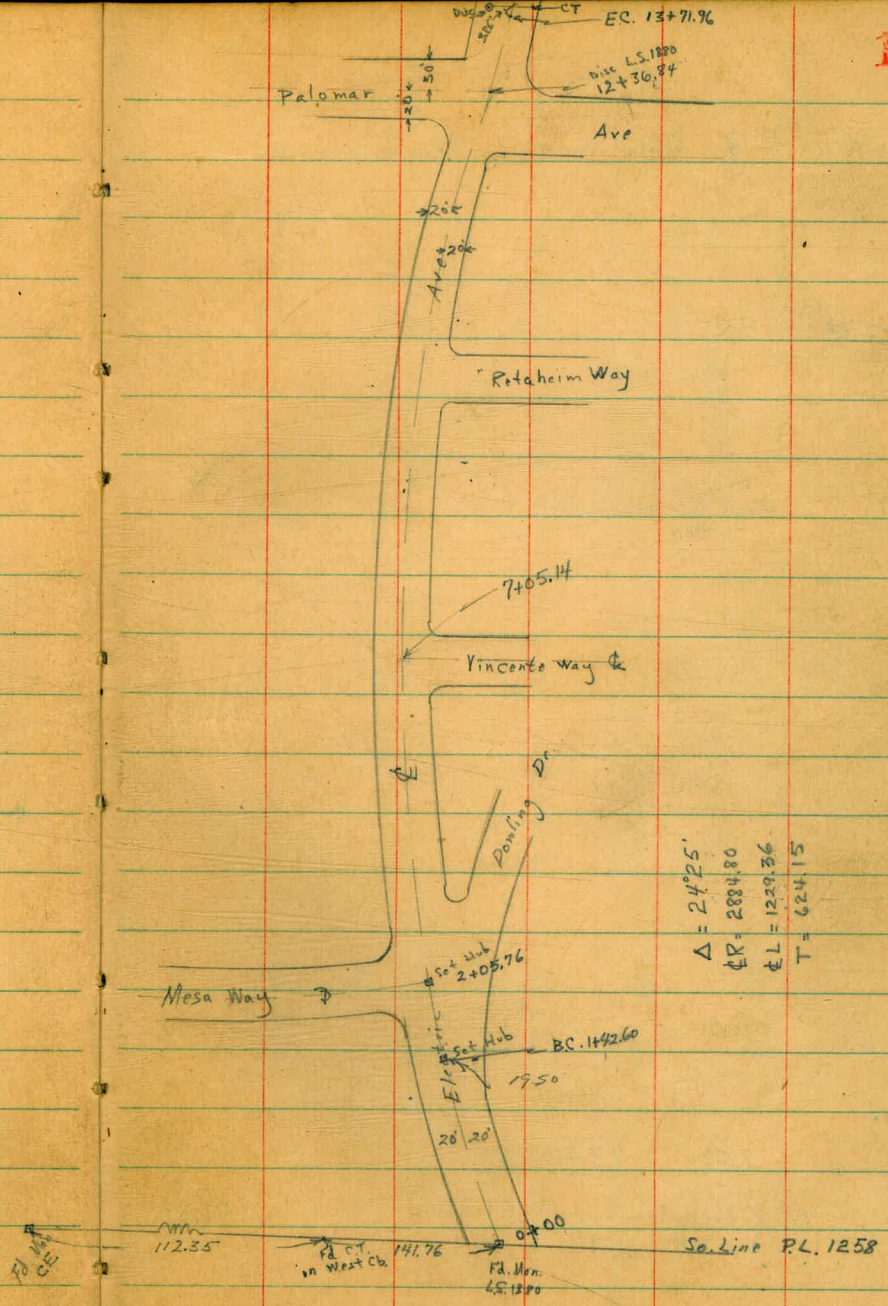
Dowling Dr. to Palomar Ave.

Roberts
Greer
Rorer

W.O. 31410

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18



Electric Ave

2+05.76 $\frac{1}{2}$ Mesa Way Taken on Line Mesa Way

1+42.60 B.C.

1+19 Beg. Cb. on right

1+00

0+50

0+00

1.53

93.42

B.P. E. Curb Dowling at Electric
See 1990 page 29

91.89

Lt. 88.3

$\frac{5.1}{40}$

88.6

$\frac{4.8}{40}$

88.6

$\frac{4.8}{40}$

89.1

$\frac{4.3}{40}$

89.3

$\frac{4.1}{40}$

89.5

$\frac{3.9}{40}$

89.0

$\frac{4.4}{40}$

90.0

$\frac{3.4}{40}$

89.8

$\frac{3.6}{40}$

90.2

$\frac{3.2}{40}$

90.5

$\frac{2.9}{40}$

91.0

$\frac{2.4}{40}$

90.5

29

91.2

2.2

91.4

2.0

91.5

1.9

92.0

1.4

92.1

1.3

91.8

$\frac{1.6}{21.7}$

92.0

$\frac{1.4}{18.9}$

92.0

$\frac{1.4}{18.8}$

92.1

$\frac{1.3}{16}$

92.8

$\frac{0.6}{16}$

93.2

$\frac{0.3}{20}$

92.7

$\frac{1.33}{21.7}$

92.19

$\frac{1.23}{18.9}$

92.27

$\frac{1.15}{18.5}$

92.6

$\frac{0.8}{20}$

94.8

$\frac{1.4}{30}$

90.9

$\frac{1.10}{30}$

5+00

Lt	88.5	87.1	87.0	89.54
	$\frac{4.5}{40}$	$\frac{4.3}{20}$	$\frac{4.0}{18.9}$	$\frac{3.43}{18.9}$
		3.9		0.6

4+50

Lt	87.9	88.5	89.2	90.03
	$\frac{5.1}{40}$	$\frac{4.5}{20}$	$\frac{3.8}{18.9}$	$\frac{2.94}{18.9}$
		3.7		0.6

T.P. 3.16 92.97 3.61 89.81

4+00

Lt	87.7	88.8	92.97	90.4
	$\frac{5.5}{40}$	$\frac{4.6}{20}$	$\frac{3.8}{19}$	$\frac{3.00}{19}$
		3.7		0.6

see 1790 page 32 for gutter and curb elevations on curb return Electric and Dowling

3+50

$\frac{5.5}{40}$

Lt	89.0	89.5	90.4	90.1	90.8	90.8
	$\frac{4.4}{20}$	$\frac{3.9}{13}$	$\frac{3.0}{11}$	$\frac{3.7}{9}$	$\frac{2.9}{20}$	$\frac{2.6}{30}$
				3.3		

3+00

Lt	87.8	89.0	90.9	91.2	91.9
	$\frac{5.6}{40}$	$\frac{4.4}{20}$	3.0	$\frac{2.0}{20}$	$\frac{1.0}{30}$

2+50

Lt	88.3	89.4	90.2	91.0	91.3	92.11
	$\frac{5.1}{40}$	$\frac{4.0}{20}$	3.2	$\frac{2.4}{20}$	$\frac{2.1}{20}$	$\frac{1.31}{35}$
						0.6

93.42

93.42

T.P. 3.70 91.99 4.68 88.29

7+05.14 ϕ Vincente Way (xsec. taken on Line of Vincente)

6+50

6+00

5+93 ϕ Conc. Drive 7' Opening

5+50

5+38 ϕ Conc. Drive 13' opening
92.97

Lt.

ϕ

Rt.

21

91.99

87.6
 $\frac{5.4}{40}$

88.3

$\frac{4.7}{40}$

88.5

$\frac{4.5}{40}$

88.3

$\frac{4.7}{40}$

88.1

$\frac{4.9}{20}$

88.5

$\frac{4.5}{20}$

88.5

$\frac{4.5}{20}$

88.5

$\frac{4.5}{20}$

88.1

4.9

88.4

4.6

88.8

4.2

89.1

3.9

87.7

$\frac{5.3}{20}$

87.8

$\frac{5.2}{18.8}$

88.3

$\frac{4.7}{18.8}$

$\frac{4.68}{18.8}$
Conc.

88.6

$\frac{4.4}{18.8}$

88.72

$\frac{4.25}{18.9}$
conc.

87.7

$\frac{5.3}{30}$

88.22

$\frac{4.15}{18.8}$

88.63

$\frac{4.34}{18.8}$

$\frac{4.11}{21.8}$
Conc.

89.10

$\frac{3.87}{18.8}$

89.34

$\frac{3.63}{22.9}$
conc.

92.97

12+00

11+50

11+00

10+935 ϕ Conc. Drive 16 $\frac{1}{2}$ ' Opening

10+50

10+42 ϕ Conc. Drive 12' Opening

10+00

88.58

Lt.

81.8

$\frac{88}{40}$

81.6

$\frac{71}{40}$

82.2

$\frac{64}{40}$

82.9

82.7

$\frac{57}{40}$

84.0

84.0

$\frac{51}{40}$

82.5

$\frac{61}{20}$

82.6

$\frac{60}{20}$

82.8

$\frac{59}{20}$

85.3

85.3

$\frac{53}{20}$

85.2

85.2

$\frac{34}{11}$

ϕ

83.0

5.6

83.1

5.5

83.8

4.8

84.5

84.5

4.1

85.3

85.3

3.3

83.0

$\frac{56}{20}$

83.2

$\frac{54}{18.9}$

83.5

$\frac{51}{18.7}$

83.67

84.1

4.5

84.7

84.7

$\frac{3.9}{18.7}$

83.0

$\frac{56}{30}$

83.7

$\frac{4.71}{18.9}$

83.5

$\frac{4.93}{18.7}$

85.1

84.8

$\frac{3.80}{18.9}$

85.26

85.26

$\frac{3.32}{18.9}$

Rt

24

88.58

12+36.84

Palomar

88.58

82.58
6.00
40

83.93
5.65
20

83.22
5.36
conc.

88.58

83.34 ← CH. See 1790 Pg. 43 - 83.34

5.24
6.9
conc.

83.2
5.4
20

X Sec. Mesa Way

La Jolla Blvd to Electric Ave.

6-15-48

W.O. 80094

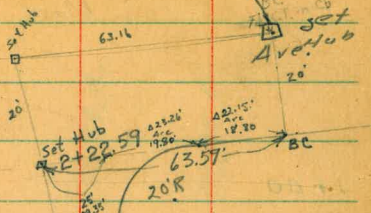
Roberts
Greer
Racer

INDEXED

JUN 17 1948

Electric

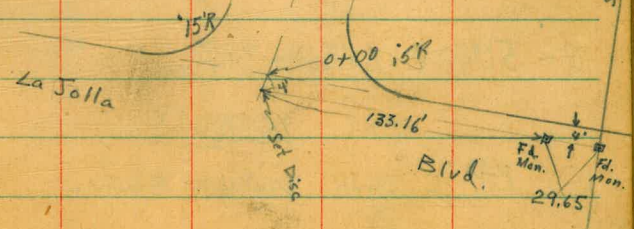
50R



50'

Mesa Way

$\Delta = 6^{\circ} 22' - 34''$
 $R = 2000$



Mesa Way

1+00

Lt.	84.4	84.1	84.6	84.4	84.5
	$\frac{7.7}{50}$	$\frac{7.4}{25}$	7.5	$\frac{7.7}{25}$	$\frac{7.6}{50}$

0+50

	83.2	83.4	83.2	83.0	82.9
	$\frac{8.9}{50}$	$\frac{8.7}{25}$	8.9	$\frac{9.1}{25}$	$\frac{9.2}{50}$

0+12

	82.5	82.4	82.4	82.5	82.1
	$\frac{9.6}{50}$	$\frac{9.7}{25}$	9.7	$\frac{9.6}{25}$	$\frac{10.0}{50}$

0+00

	82.0	81.8	81.6	81.4	81.3
	$\frac{10.1}{50}$	$\frac{10.3}{25}$	10.5	$\frac{10.7}{25}$	$\frac{10.8}{50}$

0-20 Curb line La Jolla Blvd.

81.93	81.37	81.64	81.10	80.73	81.25	80.46	80.92	80.15	
$\frac{10.16}{100}$ cb.	$\frac{10.72}{100}$	$\frac{10.45}{50}$ cb.	$\frac{10.99}{50}$	$\frac{11.36}{100}$ cb.	$\frac{10.88}{50}$ cb.	$\frac{11.63}{50}$	$\frac{11.17}{50}$ cb.	$\frac{11.26}{100}$	$\frac{11.44}{100}$ cb.

0-50 E La Jolla Blvd.

82.08	81.72	81.44	81.11
$\frac{10.01}{100}$	$\frac{10.37}{50}$	10.65	$\frac{10.98}{50}$
			$\frac{11.30}{100}$

0.20 92.09

92.09

B.P. E. Curb Dawling at Electric

91.89

2+22.59 Prop. line Electric

2.7
50 89.4

2.5
25 89.4

2.8
25 89.3

2.5
25 89.6

2.5
50 89.6

2+00

3.6
50 88.5

3.7
25 88.4

3.7
25 88.4

3.7
25 88.4

4.1
50 88.0

1+50

5.7
50 86.4

5.6
25 86.5

5.6
25 86.5

5.7
25 86.4

6.0
50 86.1

92.09

92.09

X Sec Vincente Way

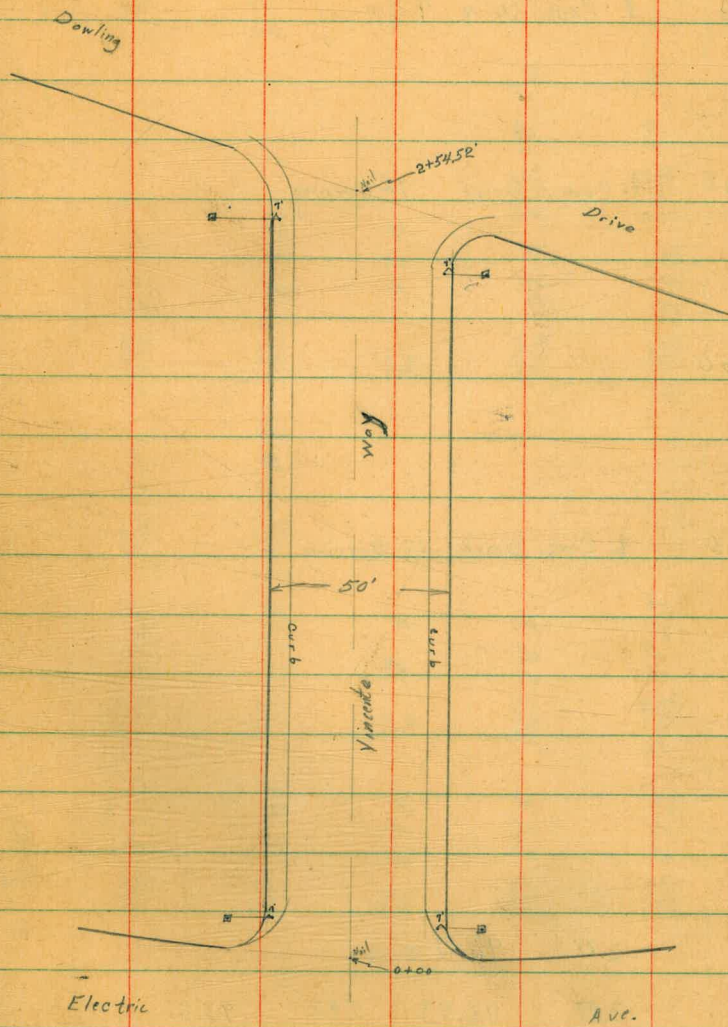
Electric Ave to Dowling Dr.

W.D. 31410

6-16-48

Roberts
Greer
Rorer

INDEXED
JUN 17 1948



Vincente Way

0+96 £ Conc. Drive 9' Opening

Lt.
87.54
6.65
18
conc.

£

Rt.

87.02
71.7
15
conc.

0+60[±] £ Conc. Drive 7[±] Opening

88.31

88.4

88.50
7.09
15
conc.

89.10
7.09
18
conc.

0+50

88.31
7.88
15
Cb.

7.8

7.9
15

88.82
7.37
15
Cb.

0+33 £ Conc. Drive 13' Opening

88.01
8.18
15
conc.

87.47
8.72
15
conc.

0+20

87.68
8.01
15
Cb.

87.4
8.19
15

8.4

8.8
8.4
15

88.17
8.02
15
Cb.

0+00

87.63
8.56
35
Cb.

87.0
8.10
15
Cb.

87.3
8.19
15

8.6

8.8
8.4
15

88.17
8.5
35.6

88.02
8.17
35.6
Cb.

2.88 96.19

T.P. 3.88 98.73 5.42 93.31

96.19

B.P. E. Curb Dowling Dr. at Retahaim 94.85

3.75 97.13 5.24 91.89 = 91.89
PA Electric Dowling

T.P. 2.81 93.38

2+54 ⁵² Prop. line Dowling (xsec taken on prop. line)

2+50

96.19

Lt.

4

Rt.

32

280 184	36 18.7	32	32 17	34 30.3	280 30.3 Cb.
93.31	92.5	92.8	93.1	93.2	93.34
93.39	92.6	93.0	93.0	92.8	
3.4					<u>96.19</u>

XSec Palomar Ave

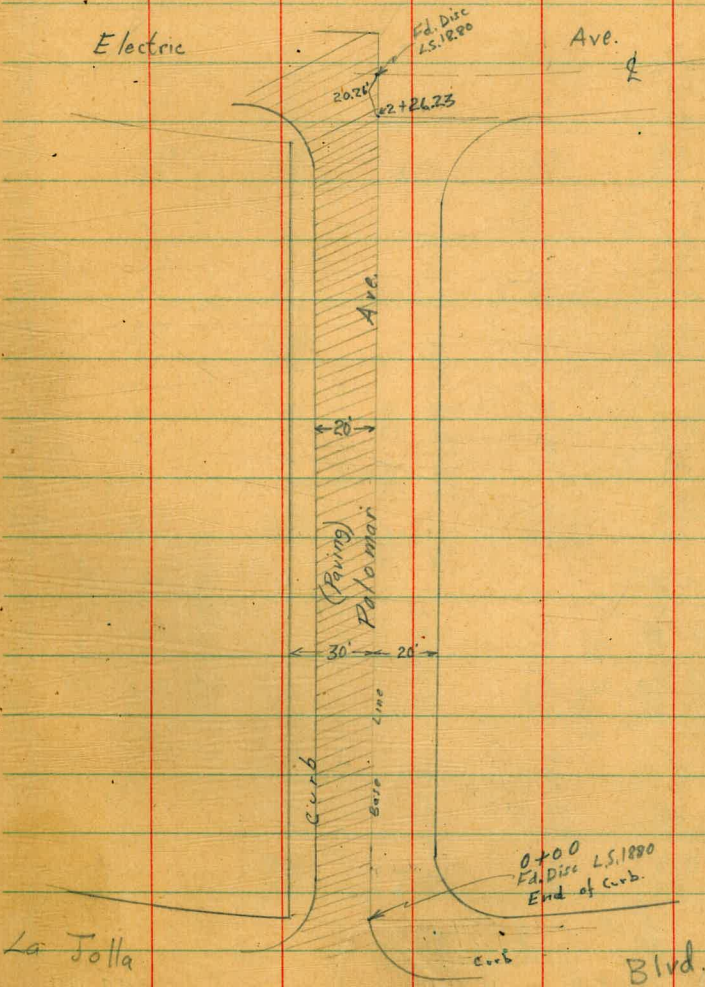
La Jolla Blvd. to Electric Ave.

W.O. 80094

6-16-48

Roberts
Greer
Rorer

INDEXED
APR 17 1948
JUN 17 1948



2+46.49 Electric

2+26.23 Prop. Line Electric

2+18

2+09

2+00

84.57

Lt.

Base Line

Rt.

35

1.58 30	82.99	1.75 20	82.82	1.48 10	83.22	1.5 20	83.1	1.5 40	83.1
2.10 30	82.97	2.11 20	82.46	1.81 10	82.76	2.0 20	82.57	2.0 40	82.57
2.24 20	82.33								
1.58 30	82.99	1.71 10	82.66	1.65	82.92	2.2 20	82.4	2.3 40	82.6
1.62 20	82.95	2.2 20	82.22	1.77	82.80	2.3 20	82.3	2.7 40	81.9
2.35 20	82.05	2.09 10	82.48	1.92	82.65	2.3 20	82.0	2.7 40	81.7
1.85 20	82.72	2.27 10	82.30	2.13	82.44	2.6 20	82.0	2.9 40	81.7

84.57

INDEXED

W.K.

SEP 3 1948

Acct. 02
Ed. Co.
Lot 30
Marston
Hills
151880

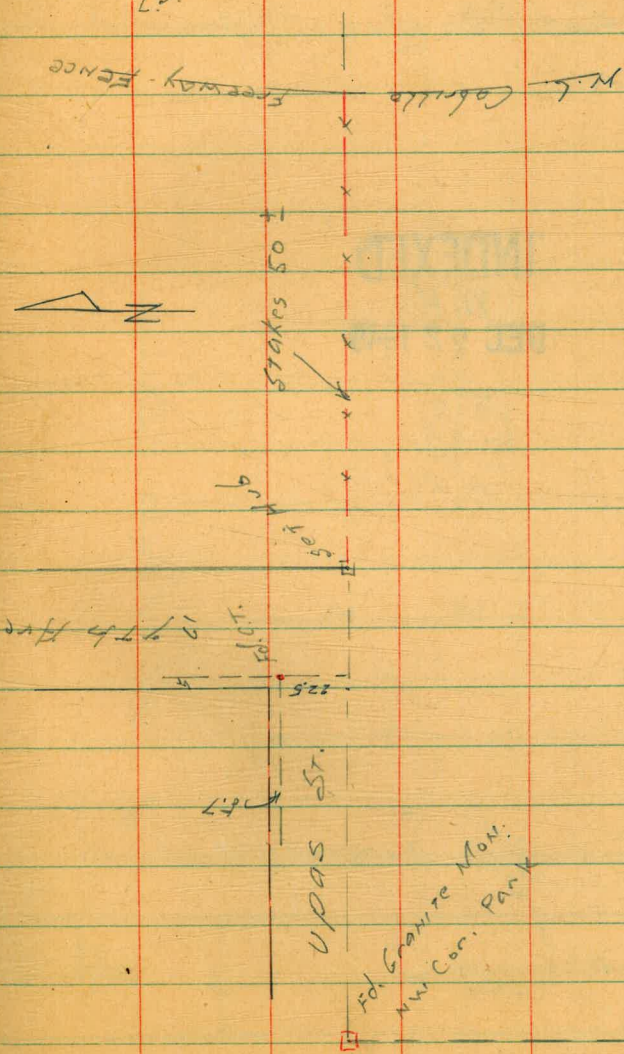
Set line stakes on
N.L. Babcock Part
7th to Cabrillo Freeway

Moore
Begg

Shoeman W.D. 60257

Bunch

8-2-48



Hendricks
Johnson
Greer
Rorer
Cota
12-20-49
W.O. #25020

X-section "C" Street
47th St to Cotton St

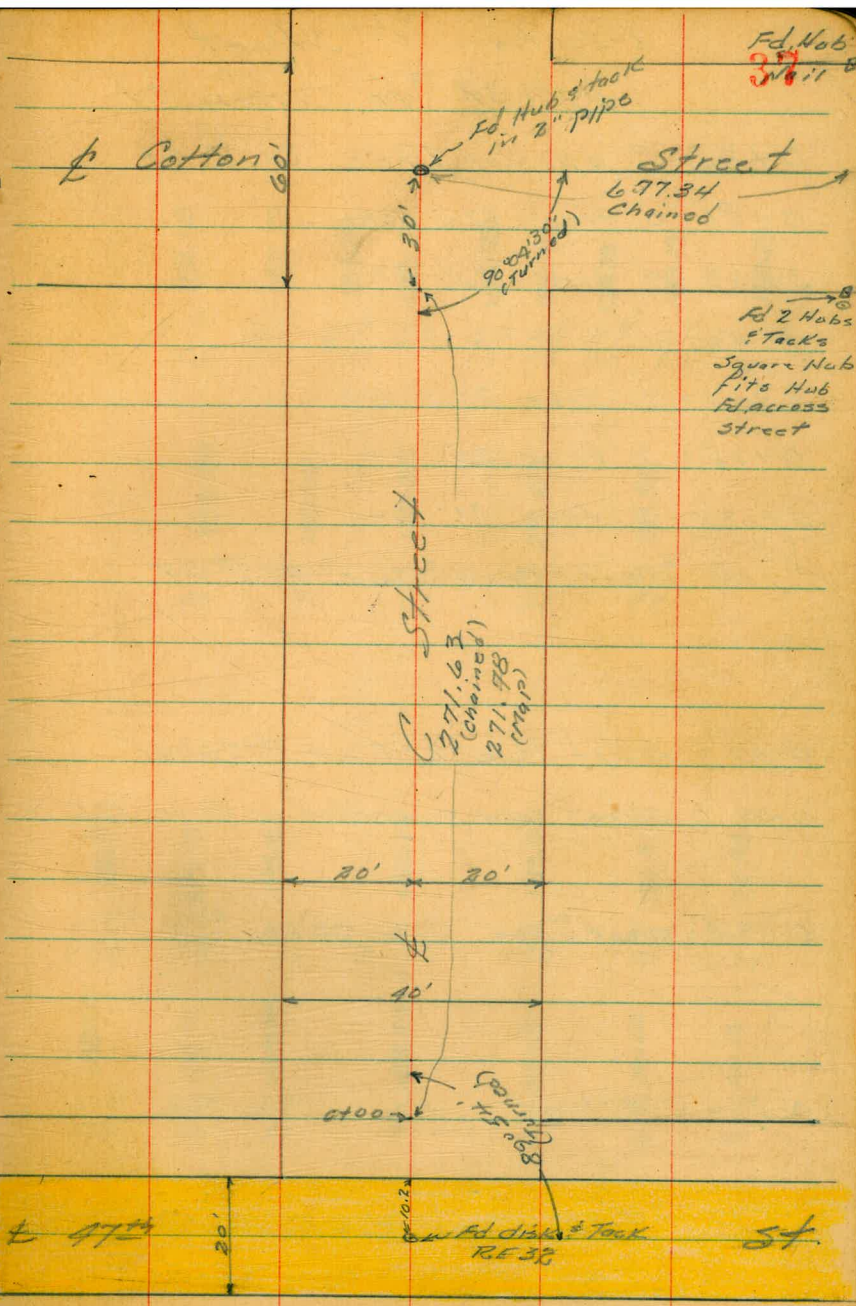
3+01.63 = E "C" St. & Cotton St

2+71.63 = East Prop. Line Cotton St

INDEXED
W.K.
DEC 22 1949

Hilltop Drive

0+00 = West Prop. Line 47th St



Fd. Hub
3711

Rd 2 Hubs
& Tack's
Square Hub
fits Hub
Rd. access
street

C Street
2+71.63
(Chained)
2+71.98
(Map)

X-section "C" Street

47th St to Cotton St

0+95 = 3" apricot Tree 21.5' Rt

0+81 = 6" tree 22.5' Rt

0+69 = 7" tree 22.5' Rt

0+50

0+42 = 7" tree 20.5' Rt

0+25 = 7" tree 22.5' Rt

0+17 = 4" tree 22' Rt

0+00 = West Prop line 47th St

0-07 = Power Pole 22.3' Lt #176841

0-08 = Street sign embedded in Conc. 17.5' Lt

0-19.8 = West edge of pave.

0-30 = E 47th St

T.P. 4.20 ^π 194.29 3.42 190.09

6.70 193.51 186.81

Left

±

Right

38

189.69	188.59	188.39	188.29	187.99	188.49	188.99	189.19	189.29
4 ⁶	5 ⁷	5 ⁹	6 ⁰	6 ¹⁰	5 ⁸	5 ¹⁰	5 ¹¹	5 ¹⁰
40	20	12		10	13	20	33	40

188.99	189.09	189.29	189.69	189.89
5 ¹⁰	5 ¹²	5 ⁰	4 ⁶	4 ⁹
40	20		20	40

188.57	188.73	188.93	189.19	189.42	191.01	192.46
5 ⁷²	5 ⁵⁶	5 ³⁶	5 ¹⁰	4 ⁸⁷	3 ²⁸	1 ⁸¹
120	70	20		20	70	120

188.68	188.79	189.08	189.29	189.53	191.00	192.56
5 ⁶¹	5 ⁵⁰	5 ²¹	5 ⁰⁰	4 ⁷⁶	3 ²⁹	1 ²³
120	70	20	017 0124	20	70	120

T.B.M. Spike in pole #176841

B.M. 1st E 47th & Hilltop Drive

X-section "e" Street
(Cont.)

2+50

2+34

2+12

2+00

1+50

1+35 = Pole 12' Lt #17/1083

T.P. 0.30 190.39 4.20 190.09

1+00

	Left					#	Right		
184.39	183.89	183.09	183.69	183.19	183.29	183.29	183.69	184.79	
6 ⁰	6 ⁵	7 ³	6 ³	7 ²	7 ¹	7 ⁶	6 ⁷	5 ³	
40	20	16	7	5	7	18	20	33	

182.49	183.09	183.99	183.49	183.59	183.59	183.79	184.59	
7 ²	7 ³	6 ⁴	6 ⁹	6 ⁸	6 ⁸	6 ⁶	5 ⁸	
40	20	7	4	6	17	20	37	

184.09	185.09	183.69	184.19	183.89	183.99	183.89	183.99	183.99	184.29
7 ⁵	5 ³	6 ⁷	6 ²	6 ⁵	6 ⁴	6 ⁵	6 ⁴	6 ⁴	6 ¹
46	34	20	15	9	5	16	17	20	40

183.79	184.39	183.89	184.39	184.09	184.19	184.19	184.39	184.39	184.89
6 ⁶	6 ⁰	6 ⁵	6 ⁰	6 ¹⁰	6 ²	6 ²	6 ⁰	6 ⁰	5 ¹⁵
40	20	15	7	5	6	15	16	20	40

185.29	185.29	184.89	185.29	185.19	185.29	185.19	185.59	185.69	186.09
5 ¹	5 ¹	5 ⁵	5 ¹	5 ²	5 ¹	5 ²	4 ⁸	4 ⁷	4 ¹⁰
40	20	17	9	6	8	13	14	20	40

186.99	187.09	187.09	190.39	186.79	187.09	187.69
7 ³	7 ²	7 ²	7 ³	7 ⁵	7 ²	6 ⁵
40	20	8	7	12	20	40

194.29

X-section "C" Street
"Cent"

7.20 186.52 186.81 = L.O.T. E 47th St & Hilltop Drive

T.P. 5.35 194.02 1.72 188.67

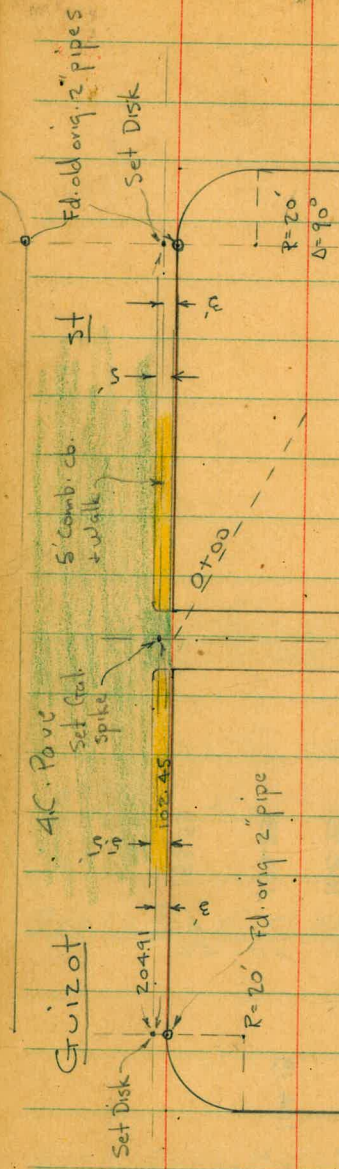
3+01.62 = E Cotton St

185.49	184.29	182.89	182.69	182.59	182.79	183.29	183.59
49	61	75	77	78	76	71	68
100	80	50	20		20	40	50

2+71.62 = East Prop. Line Cotton St.

184.19	183.79	182.69	183.19	182.89	182.89	183.19	184.19
62	64	72	73	75	75	72	62
40	20	15	11	8		20	40

190.39
X



Alhambra

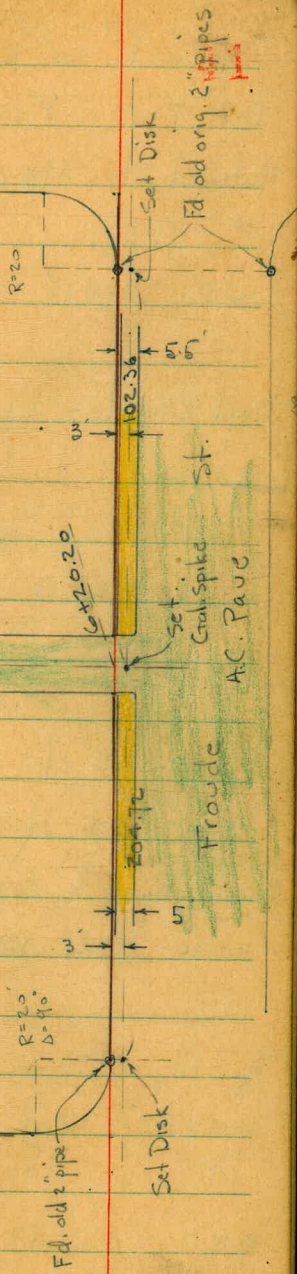
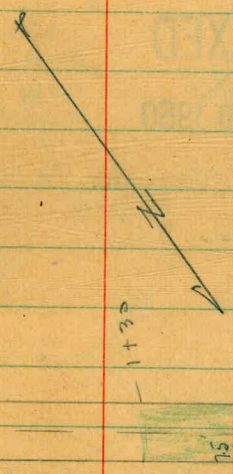
Block 16
Sunset Cliffs

15'

Osprey

Please Note on Tie sheets.

st.



st.

X-Sect. 20' Alley in Block 16 - Sunset Cliffs

Set Ties - Please Note on Sheets.

Matched Sta. Shown in Book 1657 - P. 63

4387

W.O. 31875

INDEXED
MAY 10 1950

5-9-50

Osborne
Hardin
Hatch
Shepard.

Soil Sample - 3+00

REDUCED - 5-22-50
P.V.S.

0+60

0+48 - 8.2 Lt. - end Gar. + Beg. Stucco Wall - 7' High

0+20 - 8.2 Lt. - end Dr. + Beg. Stucco Gar. opens

0+00 - 8.2 Lt. - Beg. Nly of Conc. Drive

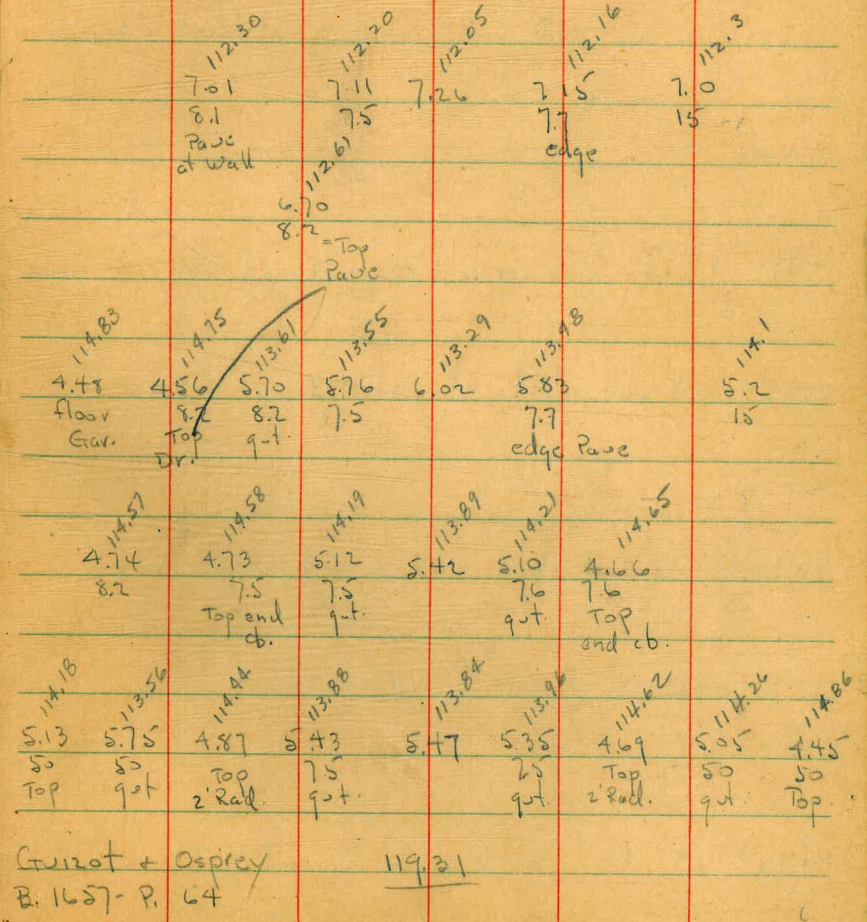
Pave - Beg. Rough A.C. Pave in alley

0+00 = w.l. Guizot - 0.2 E. - end obs. + Reg. A.C.

0-05.5 = w.cb. Guizot

B.M. 2.97 119.31 116.34 = S.F.B.P.

Lt = S ♀ Rt = N. 42



T.P. 0.60 107.41 12.50 106.81

2+25

2+00

1+90- 7.8' Lt. = end wall - footing - at least 1' Below ground.

1+65

1+57- 7.7' Lt. = end apron + Beg. Stucco wall - 5' High

1+35 = end wall on Lt. at Doub. Gar. - Conc. floor

1+30- 7.7' Lt. = end Wall + end Alley Pave. + Beg Conc apron

1+20- 6.7' Lt. = P. pole # P.A. 4526

1+00

0+98- 7.7' Lt. = 2' Gate in wall

43

106.7
12.6
7.5

106.9
12.4
7.5

105.8
13.5

105.6
13.7
7.5

102.1
12.2
15

109.2
10.1
15

108.7
10.6
15

108.0
11.3

108.2
11.1
7.5

108.8
10.5
15

109.2
10.1
7.8
ground

110.3
9.0
7.9
along wall

110.3
9.0
7.5

109.9
9.4

110.2
9.1
7.5

110.8
8.5
15

110.40
8.9
7.7

apron at wall

110.66
8.65
11.7
floor
Gar.

110.46
8.85
7.7
apron

110.46
8.85
7.7
Beg. apron

110.56
8.75
7.7
at wall

110.36
8.95

110.63
8.68
7.5
Cor Pave

111.1
8.2
15

111.08
8.23
7.4
Pave at wall

110.84
8.47

111.00
8.31
7.6
edge

111.5
7.8
15

111.10
8.21
7.7
Pave in Gate

119.31

3+48-8.1' Lt. - Req. Conc. apron to Dwb. Crav.

3+44-8.2 Lt. - end wall

3+11-8.1 Lt. = Req. 6" Conc. wall

3+10-10.6 Rt. - end of footing to wall

3+00

2+89-10.7' Rt. = Conc. footing at \pm of 8' gate in wall

2+75

2+61-8.2 Lt. = \pm 8' apron to Sing. Crav.

+ 11' Rt. = Req. 8" Conc. Block wall

2+50-7' Lt. = \pm P. pole \rightarrow P.A. 4546

Lt.

\pm

Rt.

44

94.51
12.90
17.6
floor
Crav.

94.27
13.14
8.1 = apron.

94.4
13.0
9.3
inside
wall

98.76
5.65
8.2
Top
wall

94.9
12.5
8.2
ground

94.5
12.9
9.3
ground
inside
wall

98.79
8.62
8.1
Top
wall

95.5
8.9
8.1
ground.

97.6
9.8
10.6
ground

99.04
8.37
10.6
Top
footing

104.84
2.57
Top
Wall

99.6
7.8
15

99.3
8.1
7.5

98.6
8.8
7.5

99.0
8.4
7.5

99.4
8.0
10.6
along
footing

100.3
7.1
10.7
ground

100.98
6.45
10.7
Top
Conc.

101.2
6.2
15

101.3
6.1
7.5

101.2
6.2
7.5

101.3
6.1
7.5

101.4
6.0
11
along
wall

102.27
5.14
18.1
floor
Crav.

102.28
5.13
8.2
apron

102.7
4.7
15

103.0
4.4
7.5

103.0
4.4
7.5

103.3
4.1
7.5

103.6
3.8
11
ground

104.75
2.66
11
Top
wall

100.99
6.42
11
Top of
footing

107.41

4+50

4+30 - 7.9' Lt. = Beg. 6" Conc. Block wall

4+23 - 7.6' Lt. = end apron

4+04 - 8.2' Lt. = end wall and Beg. Conc. apron to

Doub. Star.

4+00

3+70 - 8.2' Lt. = Beg. 6" Conc. Block wall

3+70 - 6.4' Lt. = P. pole = # PA 4566

3+64 - 8.2' Lt. = end apron

T.P. 0.16 94.29 13.28 94.13

3+50

Lt. R Rt

85.9	85.9	85.6	85.8	85.9
8.4	8.4	8.7	8.5	8.4
7.9	7.5		7.5	15
wall				

84.8	90.96	88.0		
8.5	3.33	6.3		
8.4	7.9	7.9 = ground		
ground	Top			
inside	wall			
90.12		88.85		
4.17		5.44		
17.5		7.6		
floor		apron		
90.16	93.95	89.83		
4.13	0.54	4.46		
18	8.2	8.2		
Conc.	Top	apron		
	wall			

90.3	90.3	90.0	90.1	90.6
4.0	4.0	4.3	4.2	3.7
8.2	7.5		7.5	15
along				
wall				

90.69	93.88	93.2		
3.60	0.41	1.1		
8.7 =	8.2	8.2		
Conc.	Top	ground		
floating	wall			
inside				
	93.79			
	0.80			
	8.2			
	apron			

94.29

94.16	94.11	94.5	94.5	93.6
13.25	13.0	12.9	12.9	13.8
8.1	7.5		7.5	15
apron.				
		107.41		

See next page

T.P. 13.00 81.74 1.57 68.74

6+25.7 = E. cb.

Miss elev. of cbs. shown in B. 1657-P-70 - Turn back ^{To BM.}

AC. Pauc is 1' w. - Rods on edge

6+20.20 = E.L. Froude = end of cbs. - edge of

6+10

T.P. 1.57 70.31 12.97 68.74

5+81 - 8.9' Lt. - end Conc. Slab

5+75

5+67 - 8.8' Lt. - Ply. of Conc. wall + Req. Conc. Slab

Gar. To be Built on Lt.

5+50 - 8.5' Lt. - end wall + 7.7 Rt. - end wall

Lt.	±	Rt.
62.73 7.58 25 Top	62.03 8.29 25 Cut	62.51 7.80 Top 2 Rad.
61.81 8.50 7.5 Cut	61.60 8.71 7.5 Cut	61.45 8.86 7.5 Cut
61.92 8.39 Top 2 Rad.	59.83 10.48 3.5 Cut	60.43 9.88 3.5 Top

62.62 7.69 7.3 Top end cb.	62.19 8.12 7.3 Cut 3 w.	61.71 8.60 7.5 Cut 3 w.	61.11 8.60 7.5 Top	62.04 8.27 7.5 Top
68.9 1.4 20	68.8 1.3 13	66.0 4.3 7.5	64.4 5.9 6	63.9 6.4 6
			66.41 6.2 6	65.2 5.1 7.5
				66.2 4.1 15

70.31

20.66 11.05 15.4 Conc.	71.09 10.62 8.9 Conc.
---------------------------------	--------------------------------

71.49 10.22 8.9 Conc slab.	71.4 10.1 7.5	71.4 10.3 7.5	71.6 10.1 7.5	72.8 8.9 15
--	---------------------	---------------------	---------------------	-------------------

71.26 10.45 15.4 Slab. To W.	73.86 17.85 15.4 floor to E.	82.01 9.70 8.8 Conc slab.	73.86 7.85 Top wall
--	--	---------------------------------------	------------------------------

73.86 7.85 15.4 floor of Prop. Gar.	74.2 7.5 footing	75.3 6.4 8.5	75.6 6.1 7.5	75.3 6.4 81.71	75.8 5.9 7.7	74.1 7.0 Bottom of footing
---	------------------------	--------------------	--------------------	----------------------	--------------------	-------------------------------------

11.82	118.64	2.32	126.32	-116.34	= Starting B.M.
13.35	107.49	0.67	106.82		
13.29	94.57	0.43	94.14		
	81.74	0.46	81.28		

Sketch - Showing \pm - Base Lines for
Sections - Pave not shown - See notes
for Loc.

Data from R.O.W. Plan - 4826-L

4974

5-18-50

w.o. 20668

7.0.

INDEXED
MAY 19 1950

Notes Reduced -
6-5-50 Remington

1°	26'
2°	52'
4°	18'
5°	44'
7°	07' 45"
8°	35' 45"
10°	01' 30"
11°	27' 30"
12°	53' 30"
14°	19' 30"
15°	45' 30"
17°	11' 30"
18°	37' 15"
20°	03' 15"
2+19.37	20' 36' 30"

ch = 50'

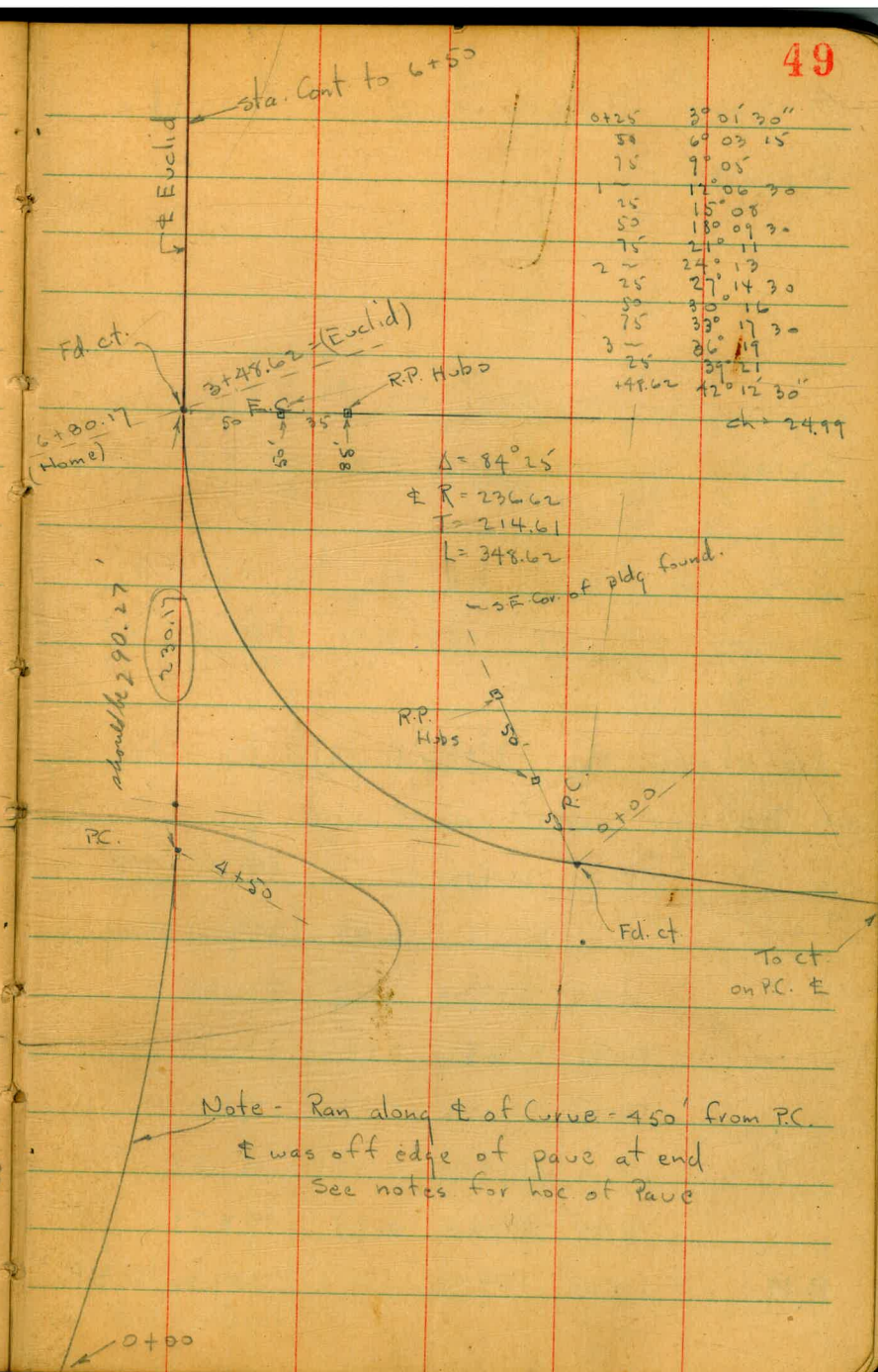
$$\Delta = 41^\circ 13'$$

$$\pm R = 1000'$$

$$T = 376.04$$

$$L = 719.37$$

For corrected \pm
see opening plat 4-13
Curve data o.k. for
corrected \pm but P.C. is
off.



0+25	2° 01' 30"
50	6° 03' 15"
75	9° 05'
1	11° 06' 30"
25	15° 08'
50	18° 09' 30"
75	21° 11'
2	24° 13'
25	27° 14' 30"
50	30° 16'
75	33° 17' 30"
3	36° 19'
25	39° 21'
48.62	42° 12' 30"

ch = 24.99

X-Sect. Exist. Pavc on Euclid r

Home.

0-100'

0-150'

edge of Conc. Pavc has roll gutter

0-200' = 200'S. of P.C. on Euclid.

2.30 224.15 221.85 = T.P.

6.08 227.01 = spike

11.24 233.09 1.67 221.85

12.81 223.52 0.12 210.71

12.51 210.83 0.47 198.37

11.26 198.79 0.31 187.53

9.45 187.84 0.91 178.39

B.M. 1000 179.30 169.30 = B.P.

Lt.

±

Rt

50

216.2	215.7	215.59	215.36	215.47	215.33	215.52	215.5	216.2
8.0	8.5	8.56	8.79	8.68	8.82	8.63	8.7	8.0
17	15	10.9	10		10	10.8	15	18
						Top	sh	Top

214.6	214.3	214.24	213.96	214.18	214.16	214.42	214.4	215.1
9.4	9.9	9.91	10.19	9.97	9.99	9.73	9.8	9.1
17	15	10.8	10		10	10.9	15	18
						Top	sh	Top

214.1	213.7	213.68	213.43	213.55	213.49	213.73	213.7	214.3
10.1	10.5	10.47	10.72	10.60	10.66	10.42	10.5	9.9
17	15	10.8	10		10	10.8	15	17
Top	edge	Top	Roll			Top	sh.	Top
bank	shoulder			224.15		Top		bank
						(Conc.)		

in pole - w. side Home + Euclid

on NW. Cor. 46± + Home
on Box Culvert.

5.97 232.98 227.01 = B.M

1+25

1+00

0+75

0+50 - Conc. is entirely covered from here

0+25 end fill Sect. on Lt

Sect. Radiad

0+00 = P.C. ± Curve - end fill Sect. on Rt.

0-50

Lt ± Rt

223.6	222.78	222.36	221.78	220.94	221.9
0.6	1.37	1.79	2.37	3.21	2.3
20	9	10	10	20	30
	edge				

222.7	222.6	221.96	221.55	220.88	220.12	220.9	221.3
1.5	1.6	2.19	2.60	3.27	4.03	3.3	2.9
40	20	9	10	10	19	25	50
		edge			edge		

221.85	221.22	220.75	219.67	219.7
2.3	2.93	3.40	4.48	4.5
20	10	10	16	25
	edge		edge	

221.9	221.7	220.64	220.1	219.03	219.5
2.3	2.5	3.51	4.10	5.12	4.7
25	16	11		14.5	20
		edge		edge	

220.5	220.0	219.81	219.71	219.21	218.39	218.9
3.7	4.2	4.34	4.44	4.94	5.76	5.3
19	14	10.7	10.3		12	20
		Top	conc. edge			

219.7	219.1	218.97	218.78	218.39	217.74	217.98	217.8	218.7
4.5	5.1	5.18	5.37	5.76	6.41	6.17	6.4	5.8
17	14	10.7	9.5		10.1	11	17	20
Top		Top				Top	Sh.	

218.0	217.4	217.22	217.02	216.93	216.61	216.74	216.7
6.2	6.8	6.93	7.13	7.22	7.54	7.41	7.5
16	17	10.9	10		10	10.9	17 = Top
				224.15			± sh.

3+00

228.5	228.5	228.24	227.50	226.85	225.89	227.7	227.7
4.5	4.5	4.74	5.48	6.13	7.09	5.3	5.3
27	23	15		10	25	29	50
Top	sh	edge			edge		

2+75 - fill sect. on Lt.

227.4	227.67	227.44	226.78	226.10	225.14	226.8	227.2
5.6	5.31	5.54	6.20	6.88	7.84	6.2	5.8
34	32	24	12	10	24	28	35
Top	sh.	edge			edge		
bank							

2+50

226.64	226.05	225.34	224.28	226.1	226.3
6.34	6.93	7.64	8.60	6.9	6.7
10		10	23	26	35
			edge		

2+25

226.20	225.82	225.32	224.62	223.75	225.2	225.5
6.78	7.16	7.67	8.36	9.23	7.8	7.5
20	10		10	23	26	35
				edge		

2+00

225.42	225.03	224.57	223.88	222.06	224.2	224.3
7.56	7.95	8.41	9.10	9.92	8.8	8.7
25	10		10	23	26	50
				edge		

1+75

224.22	224.30	223.82	223.15	222.30	223.3	223.2
8.76	8.68	9.16	9.83	10.68	9.7	9.8
27	10		10	22	26	35
				edge		
S.N. of Nty. of 20 Rad. Pavc Curve						

1+53 - 17' Lt. - P.C. of 20' Rad. of edge of Pavc.

1+50

224.3	223.59	223.52	223.11	222.41	221.75	222.7	222.6
8.7	9.39	9.46	9.87	10.57	11.23	10.3	10.4
25	16	9		10.	21	24	30
	edge				edge		
		232.98					

5+50
T.P. 13.31 257.45 0.77 244.14

5+00
25.4
75

4+60
27.4 29.7
70 58
± wash

4+20
T.P. 12.09 244.91 0.16 232.82

3+80
14.9
70

3+48.62 = E.C.
18.9
70

3+25 - add outs Cont. from 6+50 - P. 57

219.9	229.1	245.8	245.05	245.26	245.43	245.26	245.20	246.1
37.6	28.4	11.7	12.4	12.19	12.02	12.19	12.25	11.4
75	40	18	13	9.7		10	17	25
	Toe	Top	sh.	edge	257.45		edge	

216.9	220.8	241.1	240.2	240.21	240.33	240.21	239.85	240.7
28.0	24.1	3.8	4.7	4.70	4.58	4.70	5.06	4.2
63	47	16	13	9.8		10	19	30
± wash	Toe	Top	sh.	edge			edge	

217.7	220.7	236.5	236.1	236.26	236.42	236.35	235.87	236.1
27.2	24.2	8.4	8.8	8.65	8.49	8.56	9.04	8.8
53	40	18	14	9.7		10	22	30
	Toe	Top	sh.	edge			edge	

214.5	216.7	233.3	232.6	232.70	232.82	232.68	232.20	232.1
30.4	26.2	11.6	12.3	12.21	12.09	12.23	12.71	12.8
67	40	18	14	10		10	23	35
± wash	Toe	Top	sh.	edge			edge	

244.91

213.4	218.2	231.2	230.6	230.50	230.22	229.75	229.17	229.8	229.9
19.6	14.8	1.8	2.4	2.48	2.76	3.23	3.81	3.2	3.1
8	38	19	13	10		10	25	28	40
± wash	Toe		sh.	edge			edge		

214.1	215.6	218.4	219.5	219.38	219.94	218.34	217.56	218.6	218.6
17.4	14.6	2.6	3.5	3.60	4.04	4.64	5.42	4.4	4.4
55	36	19	14	9.6	on Ct.	10	26	29	40
	Toe	Top	Sh	edge			edge		

219.6	219.2	228.74	228.16	227.55	226.65	226.2	226.2		
19.1	15.7	3.4	3.8	4.24	4.82	5.43	6.33	4.8	4.8
70	39	22	17	11		10	26	30	40
	Toe	Top	sh.	edge	232.98		edge		

Lt.

←

Rt.

54

T.P.

0.22 257.23

Rt. 6+75

spike in pace

6+50

255.9	255.2	255.31	255.43	255.25	254.97	255.7
1.6	2.3	2.14	2.02	2.20	2.48	1.8
17	14	9.7		10	17	25
Top	sh.	edge			edge	Toe

219.9

227.7	236.0	250.8	250.2	250.31	250.47	250.39	250.03	251.7
29.8	21.5	6.7	7.3	7.14	6.98	7.06	7.42	5.8
62	40	17	14	9.7		10	17	25
Toe	Top	sh.		edge	257.45		edge	Toe bank

6+00 - Fill Sect. Cont. on Lt.
end add. outs on Lt.

X-Sect. Home Ave Pavc - S. + W.
of Euclid.

T.P. 12.53 221.79 0.93 209.26

2+00

1+50

1+00

0+50

Fill Sect. - Both sides

0+00 - 450' S.W. of P.C. of 1000' Rad.

± Curve - on curve.

11.87 210.19

198.32 = T.P. - P. 50'

Lt.

±

Rt.

55

221.79

206.5	206.1	206.98	208.22	208.93	209.4	209.8
3.7	4.1	3.21	1.77	1.26	0.8	0.4
10	6	1	14	26	33	37
Top	sh	edge	±	edge	sh	Top

201.0	203.6	204.42	205.58	206.28	206.6	206.9
6.2	6.6	5.77	4.61	3.91	3.6	3.3
7	4	4	16	27	36	41
Top	sh.	edge	±	edge	sh.	Top

203.1	201.7	202.04	203.19	203.72	204.0	204.0
7.1	8.5	8.15	7.00	6.47	6.2	6.2
7	sh	7	19	30	40	45
Top		edge	±	edge	sh.	Top.

200.8	200.7	199.7	199.98	200.94	201.57	201.5	201.5
9.4	9.5	10.5	10.21	9.25	8.72	8.7	8.7
2		4	10	23	35	42	46
Top		sh.	edge	±	edge	sh.	Top

198.1	197.6	98.12	99.04	99.46	99.6	99.8
12.1	12.6	12.07	11.15	10.73	10.6	10.4
Top	7	13	25	37	45	48
slope	sh	edge	±	edge	sh	Top
	(shoulder)					slope

210.19

5+00

4+77.5 - 30' Rt. = P.C. of 20' Rad. Curve in Pavc.

4+50 = P.C.

T.P. 10.90 231.76 0.93 220.86

4+00 - Beg. Extended X-Sept.

Use Same H.I.

3+50

3+00 - end of fill sect. on Rt.

2+50

210.3	208.7	203.8	203.5	204.18	221.54	224.62	224.51	224.13
21.5	23.1	8.0	8.3	7.58	7.22	7.14	7.25	7.63
20	40	20	16	9		9	20	40
	Toe	Top	sh	edge				

223.13
8.63
30 - edge

207.5	208.6	220.8	220.3	221.30	221.87	222.05	221.83	221.71	223.0	222.7
24.3	23.2	11.0	11.5	10.46	9.89	9.71	9.93	10.05	8.8	9.1
70	36	21	17	9		7	20	29	32	50
	Toe	Top	sh	edge				edge		

231.76

207.4	210.3	218.0	217.4	218.07	218.78	219.19	219.13	218.95	220.1
14.4	11.5	3.8	4.4	3.72	3.01	2.60	2.66	2.84	1.7
60	37	23	18	9		11	22	31	60
	Toe	Top	sh	edge				edge	

215.3	214.3	215.05	215.73	216.19	216.54	216.43	216.6
6.5	7.5	6.74	6.06	5.60	5.25	5.36	5.2
21	16	8		8	18	28	40
	Top	sh	edge			edge	

212.2	211.2	212.08	212.73	212.45	214.15	214.5
9.6	10.6	9.71	9.06	8.34	7.64	7.3
20	14	5		10	26	35
	Top	sh	edge		edge	

210.5	208.9	209.47	210.0	211.49	211.8
11.3	12.9	12.32	110.8	10.30	10.10
16	9	3	11	26	34
	Top	sh	edge	edge	

check BM - spike in Pole 4.75 227.01 - P. 50

Go to 3+25 Sect. on P. 53 for add outs

6+00 - end.

5+75

5+50

5+25

5+20 - 39.5 Lt. = ± old Found. wall

212.9	215.3	222.5	227.5	227.70	227.46	226.79
18.9	16.5	4.3	4.3	4.06	4.30	4.97
70	41	21	19	10		10
	Toe	Top	sh.	edge		

227.1	226.8	227.11	227.11	226.86	226.10
4.7	5.0	4.65	4.65	4.90	5.66
21	18	10		8	20
Top	sh.	edge			

211.6	212.4	226.1	226.0	226.38	226.49	226.40	225.93
20.2	19.4	5.7	5.8	5.38	5.27	5.36	5.83
70	43	20	16	9		8	20
	Toe	Top	sh.	edge			

210.5	211.4	225.0	224.9	225.39	225.61	225.62	225.45
21.3	20.4	6.8	6.9	6.37	6.15	6.14	6.31
70	43	19	15	9		8	21
	Toe	Top	sh.	edge	231.76		

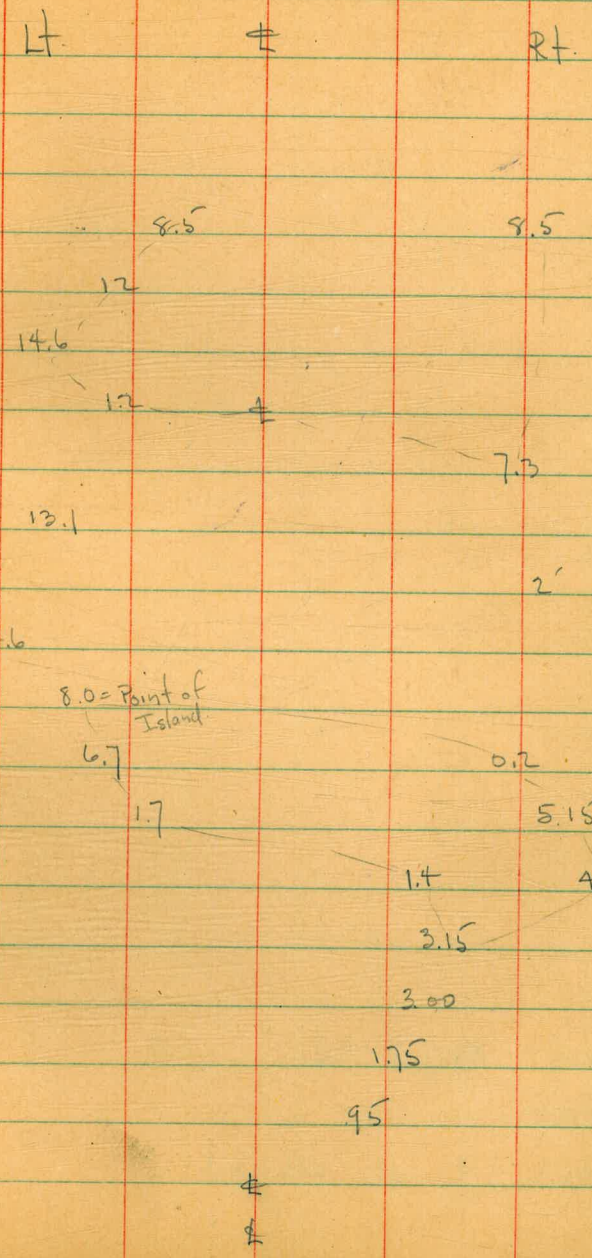
477.31

$\frac{14.45}{39.5}$ Top

Location of Stripes + Islands - painted.
along Euclid - 0+00 = P.C. - See sketch P. 49
W.O. 20668 - 8-11-50 - 7.0.

INDEXED
SMA
AUG 18 1950

- 2+25
- 2+19.7 - Ang. on W.L.
- 2+07.7 - Ang. on W.L.
+ \pm of end. 1' Bar.
- 2+01.1 = \pm on \pm of Doub. Lines
- +96.7 = Pt. of Isl.
- +91 - Wly \pm of 1' Bar.
- +91 -
- +87 - } To edge of \pm of 8' High slow
- +83.9
- +75
- +50
- +25
- 1+00 - Beg. Island - Doub. Lines
- +75
- +50
- +25
- 0+00 = P.C.
- 0-10 = Beg. Doub. Line - offsets are to \pm of Doub. Line



Lt.

E

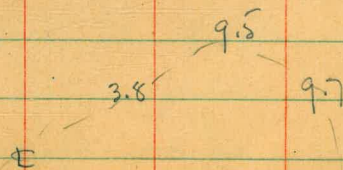
Rt.

59

2 + 61.5 - Pt. of Isl.

2 + 50

2 + 41.3 = E at W.L. Isl.



Beq. loc. of Stripes from \pm of Home
shown on P. 49

6+50

6+06.4 = opp. \pm of 8' slow Beq. stripes

+93 - \pm of 1' Bar to E. to Beq. of Doub. Str.

+63.5 = end of E.L. Doub. \pm of st. w.L.

+50

+42 - E.L. on Curve

+34.3 - Ang. in E.L.

+26 = Ang. in E.L.

+17 - E.L. on Curve

5+00

+95 = Beq. Isl.

+83 - end Doub. on Rt.

+50

+35 = Beq. another Doub. Stripe

4+00

3+93 = Beq. \pm of Doub. Stripe

+50 - Sing

3+00 = on Sing. Stripe

60

Lt.

\pm

Rt.

0.8

10.6

1.4 \pm 9.3

0.5

11.2 = end
Bar &
Beq. Dab

0.5

0.4

6.6

11.1

11

5.3

\pm 0.7

\pm

11.2 - end

0.1

11.2

0.3

11.6

11.8

12.1

12.5

6 + 44.4 = end. ^(Broken) Doub. - Sing. on up ±

6 + 00

+ 50

5 + 00

+ 75

+ 50

+ 20

4 + 00

3 + 83 - end of W. stripes + ± of 8's low

6 + 80.17 = E.C. of Euclid = 3 + 86.2 use these
sta. for Rest. of Loc.

0.2 = end

0.3

0.3

0.4

2.4

4.9

7.7

9.1

end 12

0.4 ± slow 8.4

10.1

9.4

± EL

Req. add. outs on Rt. to Top of bank
from Sta. 5+50 - P. 53

8+00

T.P. 13.26 283.27 913 270.01

7+50

7+00

12.91 270.14 257.23 = spike - P. 54.

6+50

6+00

5+50

± Rt.

62

270.13 270.1
12.84 13.2 271.3 279.0 286.4
10 18 25 32 +3.1
60
edge Toe Top

283.27

265.41 265.2 265.9 277.4 282.6
4.73 4.9 4.2 +7.3 +12.5
10 18 26 31 60
edge Toe Top

260.39 260.0 261.0 273.5 277.8
9.75 10.1 9.1 +3.4 +7.7
10 17 27 33 60
edge Toe Top

270.14

255.7 271.5 274.9
1.8 +14.0 +17.4
25 31 60
Top

251.7 261.8 276.5
5.8 +4.3 +19.0
25 33 60
Top

246.6 252.2 261.4
10.9 5.5 +3.9
30 37 60
Top

257.45 = from P. 53

on Inlet. at end cb.
 Set B.M. = Chisel □ in cb. 5.72 277.55

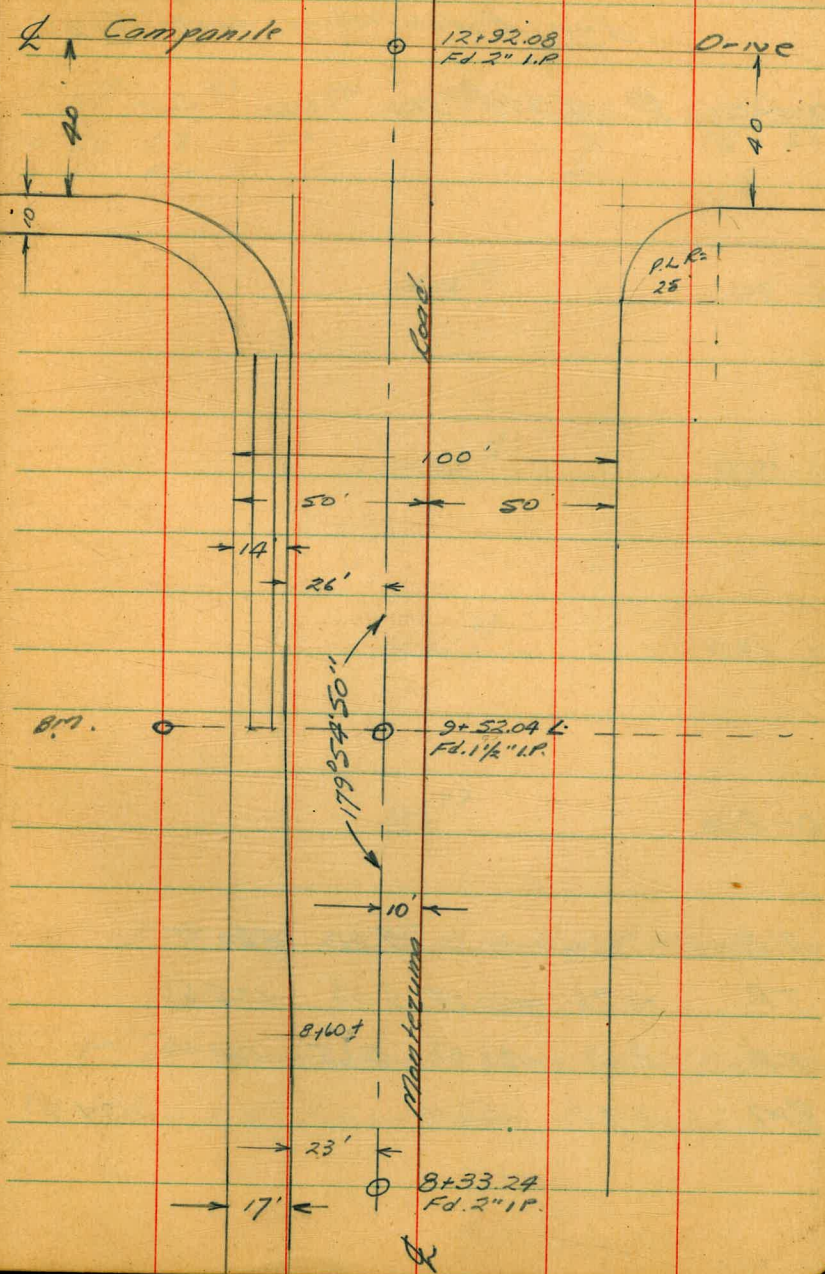
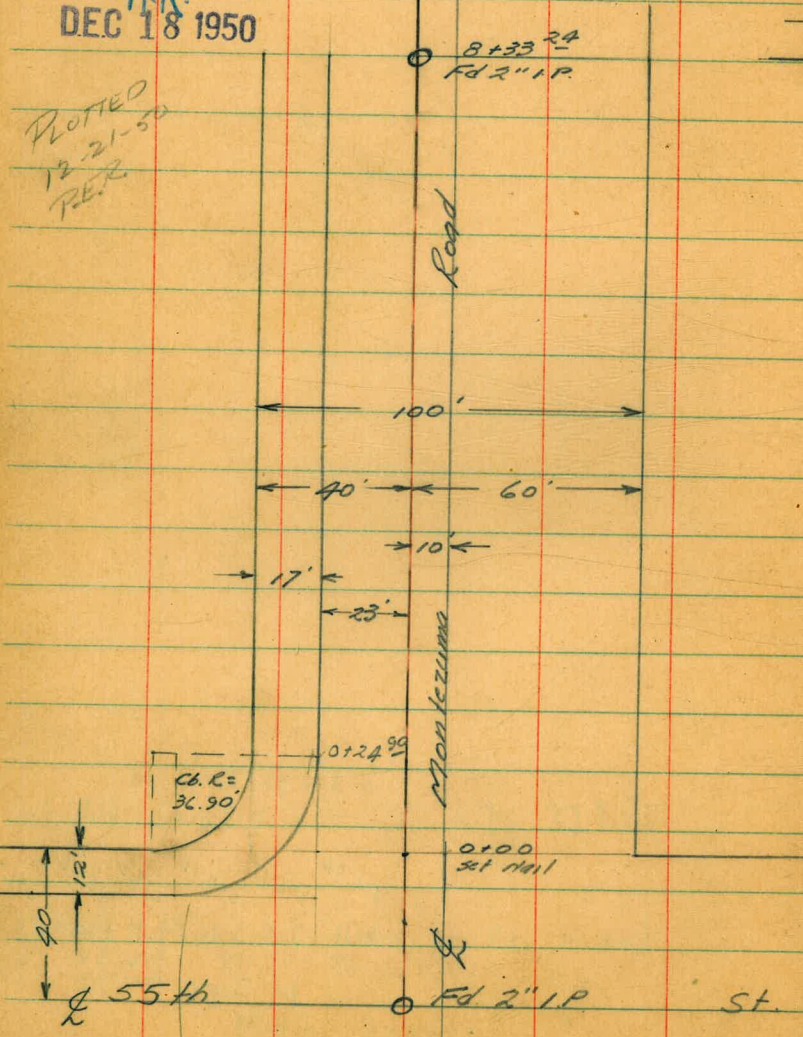
8+57 = Beg. cb. + walk on Rt = end.

276.56 276.15 277.12 279.2 287.6 291.3
 6.71 7.12 6.15 4.1 4.3 + 8.0
 10 18 19 32 38 60
 4th Topcb. 1st Top Top
 283.27 on Grate of Inlet

12-14-50 X Sect Montezuma Road
 Hendricks
 Shepard 55th St to Companie Dr
 Crawford
 N.O.# 25020

INDEXED
 MK
 DEC 18 1950

PLOTTED
 12-21-50
 PER



Levels Monteruma Road
 55th. St to Campanile
 for Establishing grade only

£

0-40 £ 55th. St.

452.5
 451.7 450.88 450.94 450.88 450.61 455.7 456.5
 100 50 28 10 9 16 50
 par par

0-90

448.20

0-140

445.11

0-190

441.99

0-240

338.97

TP		9.31	450.94	
TP	4.78	460.25	3.08	455.50
TP	8.13	458.58	5.65	450.45
BM	1.72	456.10		454.38

2" I.P. £ 55th. St. & 10' North of £ Monteruma

2" I.P. £ Campanile & 10' No. of £ Monteruma

S.V. top F.H. Linda Paseo & Campanile

0+77

454 ⁵²	455 ¹⁹	454 ³²	454 ^{82/87}	454 ⁴⁹	457 ¹	455 ²
33	33	24.5	10	10	18	60
cb.	G	Pay.				

0+57

454 ⁶⁵	453 ⁹⁸	453 ⁸⁵	454 ⁴⁴	454 ⁴²	454 ³⁵
33	33	25	10		9
cb.	G	Pay.			Pay.

0+40

454 ¹⁷	453 ⁵⁰	453 ⁴⁷	454 ⁰⁴	454 ¹⁴	453 ⁷⁸
33	33	26	10		9
cb.	G	Pay.			Pay.

0+2490 EC. Cb Ret. on Lt.

453 ⁷¹	453 ⁰⁴	453 ⁰²	453 ⁶⁴	453 ⁷²	453 ⁴³
33	33	26.5	10		7
cb.	G	Pay.			Pay.

0+00 E Line 55th St.

452 ⁴¹	452 ⁵⁰	452 ⁵⁰	452 ⁵⁰	456 ⁵	456 ⁰
29	10		9	17	30
Pay.			Pay.		

0-12 Ely. Cb Line 55th St.

452 ²⁴	451 ⁷	452 ⁰⁵	451 ⁷	451 ⁹⁹	452 ²⁵	452 ²⁴	451 ⁹⁰	456 ²	455 ⁹	455 ⁵
100	100	69.9	69.9	30	10		8	17	25	65
cb.	cb.			Pay.			Pay.			

1+97

456 ⁶³	455 ⁹⁸	455 ⁵¹	456 ²⁰	456 ⁰⁹	455 ⁷⁴
33	33	25	10		10
Cb	G	Pay			Pay

1+77

456 ⁵⁹	455 ⁷³	455 ³⁹	456 ⁰⁹	455 ⁹⁶	455 ⁵⁸
33	33	25	10		95
Cb	G	Pay			Pay

1+57

456 ⁴⁶	455 ⁷⁹	455 ³²	455 ⁹³	455 ⁸¹	455 ⁵³	457 ⁶	455 ⁹
33	33	25	10		10	19	60
Cb	G	Pay			Pay		

1+37

456 ²⁶	455 ⁵⁶	455 ³⁰	455 ⁷⁴	455 ⁶²	455 ⁴³
33	33	24	10		10
Cb	G	Pay			Pay

1+17

456 ⁹⁸	455 ³¹	455 ⁰⁷	455 ²⁰	455 ⁴⁰	455 ¹²
33	33	24.5	10		10
Cb	G	Pay			Pay

0+97

455 ⁵⁹	454 ⁹²	454 ⁶⁷	455 ⁵	455 ¹⁰	454 ⁷⁴
33	33	24.5	10		10
Cb	G	Pay			Pay

4+10

455⁹⁷ 455³⁰ 455⁰⁴ 455⁶¹ 455⁵³ 455²⁹
 33 33 24 10 10
 Cb. G Pay.

3+60

456¹² 455⁵⁰ 455²⁷ 455⁷⁵ 455⁶⁵ 455³³ 455¹ 455³¹
 33 33 25 10 10 18 10
 Cb. G Pay. Pay.

3+10

456³³ 455⁸ 455³⁷ 455⁹⁸ 455⁸² 455¹³
 33 33 25 10 10
 Cb. G Pay. Pay.

2+60

456⁵³ 455⁸⁵ 455⁶⁰ 456²⁷ 456¹² 455⁷²
 33 33 25 10 10
 Cb. G Pay.

T.P.

456.0V

2+37

456⁵⁸ 455⁹⁰ 455⁶⁷ 456³³ 456¹⁷ 455⁷³ 455⁷ 456⁴
 33 33 24 10 10 19 10
 Cb. G Pay. Pay.

2+17

456⁶² 455⁹³ 455⁶⁰ 456²⁸ 456¹⁸ 455⁸²
 33 33 25 10 10
 Cb. G Pay.

7+10

454 ⁷¹	454 ⁷²	454 ⁷³	454 ⁷⁴	454 ⁷⁵	454 ⁷⁶
33	33	25	10		9
cb.	G	Pay.	Pay.		Pay.

6+60

455 ¹¹	454 ⁴⁰	454 ⁷⁷	454 ⁷⁸	454 ⁷⁹	454 ⁸⁴	457 ⁹	456 ²
33	33	26	10			9	50
cb.	G	Pay.				Pay.	

6+10

455 ²⁷	454 ⁵⁸	454 ⁶⁶	454 ⁹⁸	454 ⁸³	454 ⁵³
33	33	26	10		10
cb.	G	Pay.			Pay.

5+60

455 ⁴³	454 ⁷⁶	454 ⁹²	455 ²²	455 ⁴⁷	454 ⁸⁷	457 ⁹	456 ⁰
33	33	25	10		10	19	50
cb.	G	Pay.			Pay.		

T.P.

457.87

Top Flydt. Rt. Sta 4190

5+10

455 ⁶⁰	454 ⁹⁴	454 ⁸⁶	455 ⁴²	455 ³⁹	455 ⁷⁶
33	33	24	10		10
cb.	SW.				

4+60

455 ⁷⁶	455 ¹¹	454 ⁹⁸	455 ⁴⁷	455 ⁴⁴	455 ¹²	458 ¹	455 ⁴
33	33	24	10		10	20	60
cb.	G	Pay.			Pay.		

9.35

453⁷⁶ 453¹² 453³² - 453⁷² 453⁵¹ 453²⁹
 35.4 35.4 21 10 10
 Cb. C Pay Pay

9+10

453⁹³ 453³² 453⁷² 453⁹⁰ 453⁵²
 34.4 34.4 30 10 9
 Cb. C Pay Pay

8+85

454⁵ 453⁴⁹ 453⁹³ 454¹⁸ 453⁹⁶ 453⁷⁵
 33.3 33.3 29 10 8
 Cb C Pay Pay

5 0460 BC Cb on Lt.

454³³ 453⁶⁷ 454⁰⁷ 454²⁶ 454⁰³ 453⁸⁸ 457⁷ 457⁻
 33 33 26 10 8 18 40
 Cb C Pay Pay Pay

T.P.

454.36 1/2" 10" Lt. 8+33.24

8+10

453⁵⁷ 453²⁶ 454¹⁸ 454⁴⁴ 454³² 454⁰⁵
 33 33 26 10 8
 Cb. C Pay Pay

7+60

454²⁴ 454⁰³ 454⁴⁸ 454²² 454⁵³ 454³² 451⁸ 456⁸
 33 33 24 10 8 17 50
 Cb. C Pay Pay

11+54.6 RC Cb. Rd on Lt.

T.P

451.85-

11+50

10+95

10+50

10+00

9+52.04 L. Proj sidewalk on Lt.

451⁶⁴ - 451¹⁰
36 36
Cb G

451¹⁴ - 451¹² 451¹¹ - 451¹⁹ 451¹⁵
36 36 10 16
Cb G

452³¹ - 452¹⁵ 452³¹ - 452²⁷ 452⁶⁷
36 36 10 16
Cb G

452⁷⁴ - 452²⁴ 452⁸⁵ - 452⁷⁶ 452¹⁸
36 36 10 17
Cb G

453¹² - 452⁶¹ 453²⁶ - 453¹⁷ 452⁷²
36 36 10 16
Cb G Pav

453⁶⁰ - 453³³ 453⁶⁰ 453⁴¹ - 452⁹⁹ 453⁶⁰
36 36 10 1 1/2" IP 16 16
Cb G Pav Cb

13+65

13+40

12+9208 & Campanile

12+5208 w. cb line Campanile

12+00

11 w. cb. Ret. L=146' 6 parts BC on Monteruma Rd.
6 Campanile

449⁴⁷
10 449³⁴

449⁸²
10 449⁸³

449⁸⁴ 449⁷⁹ 450⁴⁴ 450³² 449⁶⁹
60 50 10 17

450³⁸ 449⁸⁵ 450⁰⁸ 450²¹ 450⁸⁰ 450⁶⁷ 450⁰⁹
115 115 50 36 10 17
cb G

450⁷³ 451⁷⁰ 451²⁰ 450⁶¹
36 10 165

451¹⁰ 451⁶⁴ 450⁸⁷ 451⁴¹ 450⁶⁰ 451¹¹ 450³⁸ 450²⁵ 450¹³ 450⁸⁴ 450⁰² 450²⁸ 449⁸⁹ 450²⁶
G cb G cb G cb G cb G cb G cb G cb G cb G cb G cb G cb
BC (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (12) (13) (14) (15)

15+18

452⁴⁸
10 452⁴³

14+90

453⁵³
10 453⁵²

T.P.

452³⁴

14+65

455⁰⁵
10 455⁰⁹

14+40

446⁵¹ 446⁵⁷

14+15

447⁸⁶
10 447⁸⁰

13+90

448⁸¹
10 448⁶⁹

Set BM

454.84

BM.

455.65 455.69

457.95 (no good)

15+65

15+40

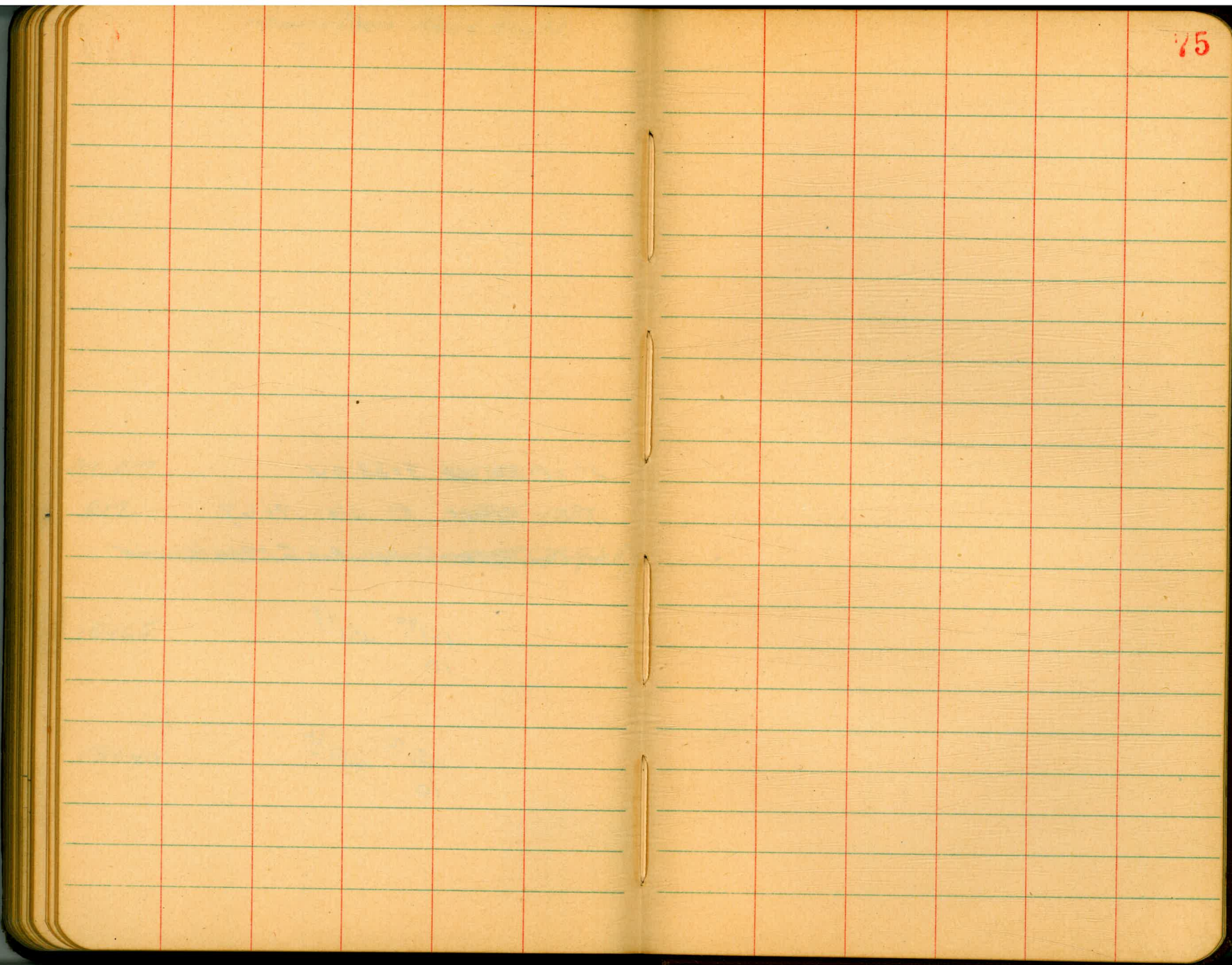
2" I.P. 50' Lt 9+52.0V

TOP FHdt Rt. Sta. 9+67

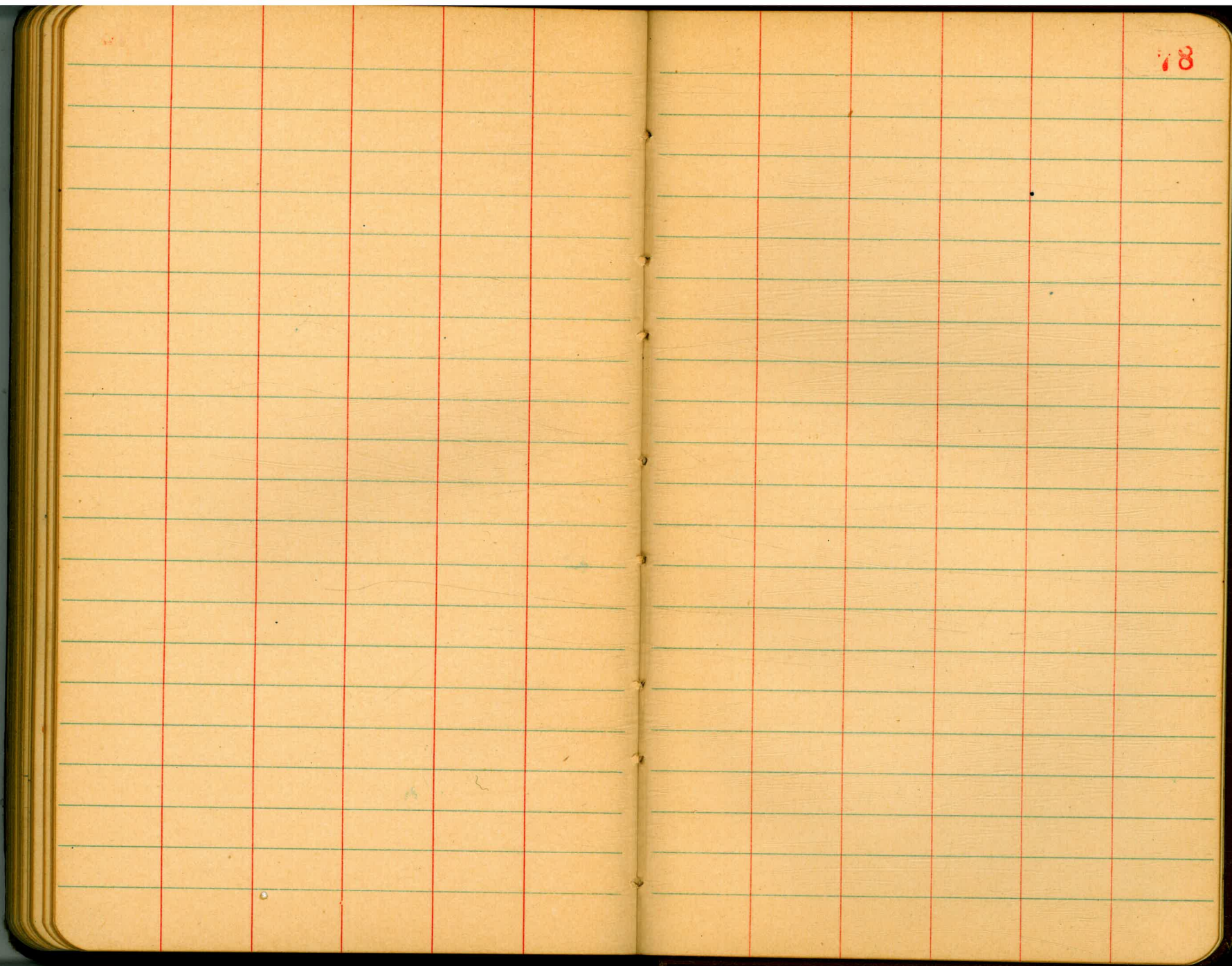
~~SE Top Hyd Gauge Ave La Monteruma~~

451.90 451.77
10

451.96 451.86
10



77



350
250
600

33554
1192
355.62

457.07

449.79

216
451.95

441.97
3
8

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.