



1838

104
25084
28248

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

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Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

CITY ENGINEER'S OFFICE

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This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

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Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6 + (20-16) * 2 or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.

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Cross Section Santa Clara Point Mission Beach 1-9

Prop Sewer Catalina Wilcox to Pascegraf 10-22

" " Arthur Sub (also PAA) 23-26

" " Silvergate Wilcox + Jennings 27-35

Cross Sec. South Crest Park playground 36-43

" " Wabaska Dr. at Capistrano 45-49

Proposed drain, ^{E. of} Monmouth Foothill 51

Parker Place ^{2-sec. for grade} Everts to Emanuel 65

Mendocino ^{Yoltaire} to Green 70-77

Cross Section Santa Clara Point

Mission Beach

Sketch Page 1

0+93 $\frac{1}{2}$ = $\frac{1}{2}$ 30" Palm Tree

0+75

INDEXED

0+50

0+25

30' Lt of BL = $\frac{1}{2}$ 30" Palm
26' Rt of BL = $\frac{1}{2}$ 30" Palm

0+10

0+00 = M.L. Bayside Walk

TP 7.86 6.90 10.32 -0.96

07 LINDA
S. Santa Clara
+ M.L. Bayside
Walk

TP 8.17 9.36 2.26 7.19

S.M.B.P.
Santa Clara
+ Seawall

B.M. 8.37 9.45 7.08

S.M.B.P.
San Jose +
Seawall

Lt. - 11

Rt. - 8

Rt. = 5

2

-0.2	-0.4	0.0	+0.6	+1.1	+0.9	+1.0	0.0	-0.4	-0.7
$\frac{71}{100}$	$\frac{73}{75}$	$\frac{69}{50}$	$\frac{61}{25}$	58	$\frac{60}{25}$	$\frac{59}{24}$	$\frac{69}{50}$	$\frac{73}{35}$	$\frac{76}{100}$

-0.2	0.0	+0.3	+0.3	+0.5	+0.5	+0.1	-0.2	-0.5
$\frac{71}{100}$	$\frac{69}{75}$	$\frac{66}{50}$	$\frac{66}{25}$	64	$\frac{64}{25}$	$\frac{68}{50}$	$\frac{71}{25}$	$\frac{74}{100}$

-0.3	-0.1	0.0	0.0	-0.2	+0.1	-0.2	-0.2	-0.3
$\frac{72}{100}$	$\frac{70}{75}$	$\frac{69}{75}$	$\frac{69}{25}$	71	$\frac{68}{20}$	$\frac{71}{50}$	$\frac{71}{25}$	$\frac{72}{100}$

-0.61	-0.6	-0.4	-0.5	-0.3	-0.4	-0.2	-0.4
$\frac{75.7}{77}$	$\frac{75}{50}$	$\frac{75.5}{25}$	74	$\frac{72}{25}$	$\frac{73}{50}$	$\frac{71}{25}$	$\frac{73}{100}$

S.M.B.P.
Santa Clara
+ Seawall

-0.4	-0.5	-0.44	-0.51	-0.43	-0.45	-0.6
$\frac{74.6}{67.6}$	$\frac{74}{25}$	$\frac{73.4}{25}$	74	$\frac{74.3}{25}$	$\frac{73.5}{25}$	$\frac{75}{10}$

S.M.B.P.
Santa Clara
+ Seawall

690

2+25

+5.4	-2.1	+1.1	+2.6	+2.8	+2.6	+2.3	+2.0	+0.9	+1.0	-4.5
128	90	58	73	41	13	45	49	66	87	114
100	75	50	25	25	25	25	25	50	75	100

2+0

-4.2	+1.1	+1.7	+2.5	+2.8	+2.1	+1.9	+0.1	-1.8	-4.3
111	80	52	44	41	48	50	68	87	112
100	75	50	25	25	25	25	50	75	100

+75

-3.8	-1.2	+1.5	+2.3	+2.4	+1.8	+1.4	+0.2	-1.1	-3.6
107	81	54	46	45	51	55	67	86	107
100	75	50	25	25	25	25	50	75	100

+50

-3.3	-1.1	+1.7	+1.9	+1.8	+1.5	+1.3	+0.4	-1.3	-3.1
102	80	58	50	51	54	56	65	82	100
100	75	50	25	25	25	25	50	75	100

+25

+2.3	-0.5	+0.9	+1.7	+1.8	+1.3	+1.2	+0.3	-0.9	-2.3
92	74	50	52	51	56	57	66	78	92
100	75	50	25	25	25	25	50	75	100

1+0

-1.1	-0.2	+0.6	+1.2	+1.5	+1.0	0.0	-0.5	-1.8
80	71	50	53	54	59	59	77	87
100	75	50	25	25	25	25	50	75

6.90

6.00

+75

$\frac{86}{100} \times 1.1$ $\frac{61}{75} \times 1.08$ $\frac{37}{80} \times 1.16$ $\frac{33}{50} \times 1.18$ $\frac{31}{25} \times 1.18$ 27×1.2 $\frac{30}{25} \times 1.1$ $\frac{35}{50} \times 1.1$ $\frac{17}{50} \times 1.1$ $\frac{10}{75} \times 0.9$ $\frac{80}{100} \times 1.1$

+50

$\frac{98}{100} \times 1.1$ $\frac{66}{75} \times 1.05$ $\frac{43}{50} \times 1.1$ $\frac{31}{25} \times 1.1$ 50×1.1 $\frac{31}{25} \times 1.1$ $\frac{36}{50} \times 1.1$ $\frac{17}{50} \times 1.1$ $\frac{20}{75} \times 1.1$ $\frac{75}{100} \times 1.1$

+25

$\frac{100}{100} \times 1.1$ $\frac{72}{75} \times 1.05$ $\frac{36}{50} \times 1.1$ $\frac{35}{25} \times 1.1$ 51×1.1 $\frac{57}{25} \times 1.1$ $\frac{37}{50} \times 1.1$ $\frac{45}{50} \times 1.1$ $\frac{75}{75} \times 1.1$ $\frac{98}{100} \times 1.1$

310

$\frac{108}{100} \times 1.1$ $\frac{75}{75} \times 1.05$ $\frac{40}{50} \times 1.1$ $\frac{36}{25} \times 1.1$ 51×1.1 $\frac{40}{25} \times 1.1$ $\frac{41}{50} \times 1.1$ $\frac{57}{50} \times 1.1$ $\frac{80}{75} \times 1.1$ $\frac{105}{100} \times 1.1$

2+75

$\frac{112}{100} \times 1.1$ $\frac{80}{75} \times 1.1$ $\frac{36}{50} \times 1.1$ $\frac{37}{25} \times 1.1$ 51×1.1 $\frac{47}{25} \times 1.1$ $\frac{46}{50} \times 1.1$ $\frac{58}{50} \times 1.1$ $\frac{80}{75} \times 1.1$ $\frac{110}{100} \times 1.1$

+74

1st of 2 = 2.30 Palm Tr. cc

2+50

$\frac{111}{100} \times 1.1$ $\frac{81}{75} \times 1.1$ $\frac{38}{50} \times 1.1$ $\frac{48}{25} \times 1.1$ 51×1.1 $\frac{45}{25} \times 1.1$ $\frac{42}{50} \times 1.1$ $\frac{65}{50} \times 1.1$ $\frac{81}{75} \times 1.1$ $\frac{118}{100} \times 1.1$

6.90

6.90

TP 5.55 8.05 140 2.50

4+70 $\begin{matrix} \times 3.5 \\ 194 \\ 175 \end{matrix}$ $\begin{matrix} \times 1.3 \\ 82 \\ 150 \end{matrix}$

4+50 $\begin{matrix} \times 2.2 \\ 191 \\ 160 \end{matrix}$ $\begin{matrix} \times 0.1 \\ 20 \\ 25 \end{matrix}$

4+75

4+25

4+0

4+0

6.90

Lt.

B

Rt.

5

$\begin{matrix} \times 0.9 \\ 80 \\ 125 \end{matrix}$ $\begin{matrix} \times 3.1 \\ 38 \\ 100 \end{matrix}$ $\begin{matrix} \times 3.4 \\ 25 \\ 75 \end{matrix}$ $\begin{matrix} \times 4.0 \\ 99 \\ 50 \end{matrix}$ $\begin{matrix} \times 4.2 \\ 27 \\ 35 \end{matrix}$ $\begin{matrix} \times 4.5 \\ 21 \\ 25 \end{matrix}$ $\begin{matrix} \times 4.5 \\ 21 \\ 25 \end{matrix}$ $\begin{matrix} \times 4.3 \\ 26 \\ 50 \end{matrix}$ $\begin{matrix} \times 4.0 \\ 29 \\ 75 \end{matrix}$ $\begin{matrix} \times 3.40 \\ 107 \\ 100 \end{matrix}$

$\begin{matrix} \times 2.3 \\ 44 \\ 100 \end{matrix}$ $\begin{matrix} \times 3.4 \\ 25 \\ 84 \end{matrix}$ $\begin{matrix} \times 3.7 \\ 22 \\ 50 \end{matrix}$ $\begin{matrix} \times 3.7 \\ 22 \\ 50 \end{matrix}$ $\begin{matrix} \times 4.2 \\ 27 \\ 35 \end{matrix}$ $\begin{matrix} \times 4.2 \\ 27 \\ 35 \end{matrix}$ $\begin{matrix} \times 4.3 \\ 26 \\ 25 \end{matrix}$ $\begin{matrix} \times 3.9 \\ 30 \\ 50 \end{matrix}$ $\begin{matrix} \times 3.7 \\ 27 \\ 75 \end{matrix}$ $\begin{matrix} \times 3.2 \\ 27 \\ 75 \end{matrix}$ $\begin{matrix} \times 2.1 \\ 18 \\ 100 \end{matrix}$ $\begin{matrix} \times 0.05 \\ 195 \\ 125 \end{matrix}$

$\begin{matrix} -1.5 \\ 84 \\ 135 \end{matrix}$ $\begin{matrix} -2.9 \\ 98 \\ 150 \end{matrix}$ $\begin{matrix} -3.15 \\ 10.05 \\ 137 \end{matrix}$

$\begin{matrix} \times 0.5 \\ 64 \\ 100 \end{matrix}$ $\begin{matrix} \times 2.0 \\ 19 \\ 85 \end{matrix}$ $\begin{matrix} \times 2.8 \\ 21 \\ 75 \end{matrix}$ $\begin{matrix} \times 3.8 \\ 31 \\ 50 \end{matrix}$ $\begin{matrix} \times 4.0 \\ 29 \\ 25 \end{matrix}$ $\begin{matrix} \times 4.6 \\ 23 \\ 35 \end{matrix}$ $\begin{matrix} \times 4.1 \\ 28 \\ 35 \end{matrix}$ $\begin{matrix} \times 3.9 \\ 30 \\ 50 \end{matrix}$ $\begin{matrix} \times 3.2 \\ 27 \\ 50 \end{matrix}$ $\begin{matrix} \times 2.7 \\ 12 \\ 75 \end{matrix}$ $\begin{matrix} \times 0.6 \\ 63 \\ 100 \end{matrix}$

$\begin{matrix} -2.7 \\ 84 \\ 125 \end{matrix}$ $\begin{matrix} -4.8 \\ 112 \\ 150 \end{matrix}$ $\begin{matrix} -6.6 \\ 125 \\ 125 \end{matrix}$ $\begin{matrix} -7.1 \\ 110 \\ 185 \end{matrix}$

$\begin{matrix} -1.1 \\ 81 \\ 100 \end{matrix}$ $\begin{matrix} \times 1.6 \\ 25 \\ 35 \end{matrix}$ $\begin{matrix} \times 4.0 \\ 29 \\ 50 \end{matrix}$ $\begin{matrix} \times 3.9 \\ 30 \\ 50 \end{matrix}$ $\begin{matrix} \times 4.2 \\ 27 \\ 25 \end{matrix}$ $\begin{matrix} \times 4.4 \\ 25 \\ 35 \end{matrix}$ $\begin{matrix} \times 4.0 \\ 29 \\ 25 \end{matrix}$ $\begin{matrix} \times 3.7 \\ 33 \\ 50 \end{matrix}$ $\begin{matrix} \times 3.2 \\ 27 \\ 50 \end{matrix}$ $\begin{matrix} \times 1.9 \\ 19 \\ 75 \end{matrix}$ $\begin{matrix} \times 0.7 \\ 70 \\ 100 \end{matrix}$

6.90

6+22

6+0

+3.85
1.20
1.35
1.50
1.65
1.80
1.95
2.10
2.25
2.40
2.55
2.70
2.85
3.00
3.15
3.30
3.45
3.60
3.75
3.90
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4.35
4.50
4.65
4.80
4.95
5.10
5.25
5.40
5.55
5.70
5.85
6.00
6.15
6.30
6.45
6.60
6.75
6.90
7.05
7.20
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7.50
7.65
7.80
7.95
8.10
8.25
8.40
8.55
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8.85
9.00
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10.50
10.65
10.80
10.95
11.10
11.25
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11.55
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11.85
12.00
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13.65
13.80
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14.25
14.40
14.55
14.70
14.85
15.00
15.15
15.30
15.45
15.60
15.75
15.90
16.05
16.20
16.35
16.50
16.65
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17.10
17.25
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20.70
20.85
21.00
21.15
21.30
21.45
21.60
21.75
21.90
22.05
22.20
22.35
22.50
22.65
22.80
22.95
23.10
23.25
23.40
23.55
23.70
23.85
24.00
24.15
24.30
24.45
24.60
24.75
24.90
25.05
25.20
25.35
25.50
25.65
25.80
25.95
26.10
26.25
26.40
26.55
26.70
26.85
27.00
27.15
27.30
27.45
27.60
27.75
27.90
28.05
28.20
28.35
28.50
28.65
28.80
28.95
29.10
29.25
29.40
29.55
29.70
29.85
30.00

5+75

+3.0
5.0
200
+3.1
4.9
175
+4.2
3.8
150
+4.5
3.5
125
+4.4
3.6
100
+4.1
3.9
75
+4.3
3.7
50
+4.3
3.7
25
+4.5
3.5
0.0

5+50

+2.5
5.5
200
+2.6
5.1
175
+3.7
4.3
150
+4.1
3.9
125
+4.2
3.8
100
+4.4
3.6
75
+4.3
3.7
50
+4.6
3.4
25
+4.5
3.5
0.0

5+41

5+38

21.6 Lt of P = 2 Firch Hd

5+25

+0.7
1.3
200
+0.1
0.9
175
+3.1
1.9
150
+3.3
1.7
125
+3.9
1.1
100
+4.1
0.9
75
+4.1
0.9
50
+4.4
0.6
25
+4.6
0.4
0.0

5+0

-1.6
0.6
200
+0.4
0.6
175
+2.0
1.0
150
+2.9
1.9
125
+3.6
2.6
100
+4.1
3.1
75
+4.1
3.1
50
+4.2
3.2
25
+4.6
3.7
0.0

8.05

8.05

+4.2
3.8
25

+4.1
3.9
50

+4.0
4.0
75

+4.0
4.0
100

+4.4
3.6
125

+4.4
3.6
150

+4.2
3.8
175

+3.9
4.1
200

+3.7
4.2
225

+3.6
4.3
250

+3.45
4.4
275

+3.60
1.15
3.00
5.15
7.30
9.45
11.60
13.75
15.90
18.05
20.20
22.35
24.50
26.65
28.80
30.95
33.10
35.25
37.40
39.55
41.70
43.85
46.00
48.15
50.30
52.45
54.60
56.75
58.90
61.05
63.20
65.35
67.50
69.65
71.80
73.95
76.10
78.25
80.40
82.55
84.70
86.85
89.00
91.15
93.30
95.45
97.60
99.75
101.90
104.05
106.20
108.35
110.50
112.65
114.80
116.95
119.10
121.25
123.40
125.55
127.70
129.85
132.00
134.15
136.30
138.45
140.60
142.75
144.90
147.05
149.20
151.35
153.50
155.65
157.80
159.95
162.10
164.25
166.40
168.55
170.70
172.85
175.00
177.15
179.30
181.45
183.60
185.75
187.90
190.05
192.20
194.35
196.50
198.65
200.80
202.95
205.10
207.25
209.40
211.55
213.70
215.85
218.00
220.15
222.30
224.45
226.60
228.75
230.90
233.05
235.20
237.35
239.50
241.65
243.80
245.95
248.10
250.25
252.40
254.55
256.70
258.85
261.00
263.15
265.30
267.45
269.60
271.75
273.90
276.05
278.20
280.35
282.50
284.65
286.80
288.95
291.10
293.25
295.40
297.55
299.70
301.85
304.00
306.15
308.30
310.45
312.60
314.75
316.90
319.05
321.20
323.35
325.50
327.65
329.80
331.95
334.10
336.25
338.40
340.55
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721.10
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725.40
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729.70
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740.45
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744.75
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749.05
751.20
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761.95
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768.40
770.55
772.70
774.85
777.00
779.15
781.30
783.45
785.60
787.75
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792.05
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811.40
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125.70
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126.10
126.30
126.5

Lt.

B

Pt.

7

TP 2.29 9.26 1.08 6.97

Top F. H. V. d.
21.64 of
5438

64.75

64.75

64.50

64.50

64.25

64.25

$\times 2.82$
 $\frac{122}{172.5} = \frac{5.1}{\text{Porch}}$
 $\times 2.7$
 $\frac{33}{150}$
 $\times 2.6$
 $\frac{35}{125}$
 $\times 2.3$
 $\frac{37}{100}$
 $\times 2.7$
 $\frac{43}{75}$
 $\times 2.8$
 $\frac{42}{50}$
 $\times 2.6$
 $\frac{41}{25}$
 $\times 2.5$
 $\frac{45}{100}$

$\times 3.19$
 $\frac{126}{190} = \frac{5.1}{\text{Porch}}$
 $\times 2.7$
 $\frac{32}{150}$
 $\times 2.3$
 $\frac{37}{100}$
 $\times 2.8$
 $\frac{42}{75}$
 $\times 2.7$
 $\frac{43}{50}$
 $\times 2.8$
 $\frac{42}{25}$
 $\times 2.8$
 $\frac{46}{100}$

$\times 2.87$
 $\frac{118}{168.5}$
 $\times 2.6$
 $\frac{35}{150}$
 $\times 2.5$
 $\frac{35}{125}$
 $\times 2.4$
 $\frac{36}{100}$
 $\times 2.8$
 $\frac{43}{75}$
 $\times 2.7$
 $\frac{42}{50}$
 $\times 2.6$
 $\frac{41}{25}$
 $\times 2.3$
 $\frac{42}{100}$

8.05

8.05

$\times 2.4$
 $\frac{16}{325}$
 $\times 2.9$
 $\frac{11}{350}$
 $\times 2.8$
 $\frac{13}{375}$
 $\times 2.5$
 $\frac{15}{400}$
 $\times 2.8$
 $\frac{52}{125}$
 $\times 2.6$
 $\frac{51}{150}$
 $\times 2.5$
 $\frac{55}{175}$
 $\times 2.5$
 $\frac{55}{200}$

$\times 2.4$
 $\frac{15}{25}$
 $\times 2.6$
 $\frac{11}{50}$
 $\times 2.6$
 $\frac{11}{75}$
 $\times 2.6$
 $\frac{11}{100}$
 $\times 2.6$
 $\frac{11}{125}$
 $\times 2.6$
 $\frac{11}{150}$
 $\times 2.7$
 $\frac{11}{175}$
 $\times 2.3$
 $\frac{17}{200}$
 $\times 2.3$
 $\frac{17}{225}$
 $\times 2.2$
 $\frac{18}{250}$
 $\times 2.1$
 $\frac{19}{275}$
 $\times 2.2$
 $\frac{18}{300}$

$\times 2.1$
 $\frac{19}{300}$
 $\times 2.1$
 $\frac{19}{325}$
 $\times 2.3$
 $\frac{22}{350}$
 $\times 2.7$
 $\frac{23}{375}$
 $\times 2.4$
 $\frac{26}{400}$
 $\times 2.7$
 $\frac{53}{125}$
 $\times 2.5$
 $\frac{55}{150}$
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 $\frac{11}{75}$
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 $\frac{11}{100}$
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 $\frac{16}{125}$
 $\times 2.3$
 $\frac{19}{150}$
 $\times 2.3$
 $\frac{19}{175}$
 $\times 2.6$
 $\frac{21}{200}$
 $\times 2.3$
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$\times 2.5$
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 $\frac{56}{175}$
 $\times 2.4$
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$\times 2.7$
 $\frac{15}{25}$
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 $\frac{13}{75}$
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 $\frac{17}{125}$
 $\times 2.6$
 $\frac{17}{150}$
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 $\frac{17}{175}$
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 $\frac{17}{200}$
 $\times 2.8$
 $\frac{17}{225}$
 $\times 2.7$
 $\frac{19}{250}$
 $\times 2.7$
 $\frac{19}{275}$
 $\times 2.6$
 $\frac{22}{300}$

Lt: North

8

7+50

+3.76
5.30
102 = 51 Conc
Porch

+3.4
5.9
100

+3.5
5.8
75

+3.5
5.8
50

+3.5
5.8
25

+3.4
5.9

7+25

+3.96
5.30
110 = 55 Conc
Porch

+3.81
5.45
100 = 51 Conc
Porch

+3.6
6.1
88

+4.2
5.1
75

+4.2
5.1
50

+4.2
5.1
25

+4.2
5.1
0.0

7+25

+4.2
5.1
25

+4.3
5.0
50

+4.3
5.0
75

+4.3
5.0
100

+4.2
5.1
125

+4.3
5.0
150

+4.3
5.0
175

+4.3
5.0
200

+4.2
5.1
225

+4.1
5.2
250

7+0

+3.5
5.8
275

+3.4
5.9
300

+3.5
5.8
325

+4.0
5.2
350

+3.9
5.1
375

+3.1
5.6
400

+3.1
5.2
425

+2.8
5.5
450

+2.7
5.6
475

+2.6
5.7
500

7+0

+3.83
5.13
110 = 51 Conc
Porch

+4.0
5.3
100

+4.3
5.0
75

+4.2
5.1
50

+4.2
5.1
25

+4.1
5.2
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+3.9
5.4
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+3.8
5.5
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+3.8
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+3.3
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+2.9
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+3.6
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+3.6
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BM
 TP = 7.89 10.33 4.94 2.44
 TP 4.01 7.38 5.89 3.27
 8+25

Δt = 11 or 13

SXRP
 2220 Clarap.
 4300 11
 1.19

8+25
 126 120 116 110 108 109 109 107 10.6
 200 175 150 125 100 75 50 25 0.0

8+0
 -1.7 -1.1 -0.4 0.0 +0.1 0.0 +0.3 +0.7 +0.9
 110 104 97 93 92 93 90 8.6 8.4
 200 175 150 125 100 75 50 25 0.0

7+75
 +0.2 +0.7 +1.5 +1.9 +2.3 +2.4 +2.6 +2.9 +2.7
 91 86 78 74 70 69 67 64 66
 200 175 150 125 100 75 50 25 0.0

9.26

9.26

Pt. South

9

+1.1 +0.9 +1.1 +1.3 +1.2 +1.4 +1.1 +0.5 -0.4 +2.3
 83 84 82 80 81 79 82 84 87 118
 275 300 325 350 375 400 425 450 475 500

-1.2 -1.0 -0.7 -0.3 -0.0 +0.2 +0.4 +0.9 +1.0 +1.0
 10.5 10.5 10.0 9.6 9.2 9.1 8.9 8.4 8.2 8.0
 25 50 75 100 125 150 175 200 225 250

+2.9 +2.9 +2.8 +2.9 +2.7 +2.5 +2.3 +2.1 +1.7 +0.5
 84 84 85 84 86 88 90 92 96 98
 275 300 325 350 375 400 425 450 475 500

+0.9 +1.2 +1.3 +1.5 +1.9 +1.9 +2.0 +2.5 +2.6 +2.7
 84 86 88 90 94 94 97 100 107 106
 25 50 75 100 125 150 175 200 225 250

+3.3 +3.2 +3.2 +3.3 +3.4 +3.2 +2.7 +2.6 +2.5 +2.2
 60 61 61 60 59 61 66 67 68 71
 275 300 325 350 375 400 425 450 475 500

+2.7 +2.8 +2.9 +2.9 +2.9 +3.0 +3.2 +3.2 +3.2 +3.2
 66 65 64 64 64 63 61 61 61 61
 25 50 75 100 125 150 175 200 225 250

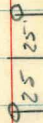
5-19-48 Proposed Sewer along Catalina
Hendricks Blvd Wilcox St to Rosecroft Lane
Walker
Becker
Williams

10

Levels P. 13

~~Indexed~~

INDEXED



Dudley St

6279.81, Fd Spk

Charles St

3228.78, Fd Spk



Wilcox St

0100, Fd Disc



Proposed Line of Sewer

Blvd Parking

20 AC

Catalina

Dupont St.

1917976 Fd Spk

← 15' → 25' → 40' →

Warner St.

1012978 Fd Spk

Proposed Line of Sewer

Catalina Blvd. Paving 20' AC

Dudley St.

617981 Fd Spk

Rosecroft Lane

23+61.03 Fd Spr

Proposed Line Arthur Sub

21+88.09

Int. Proposed Line to East Set Nail

Arbe Lane

Proposed Line of Sewer

← 15' 25' 40' →

Catalina

20' AC

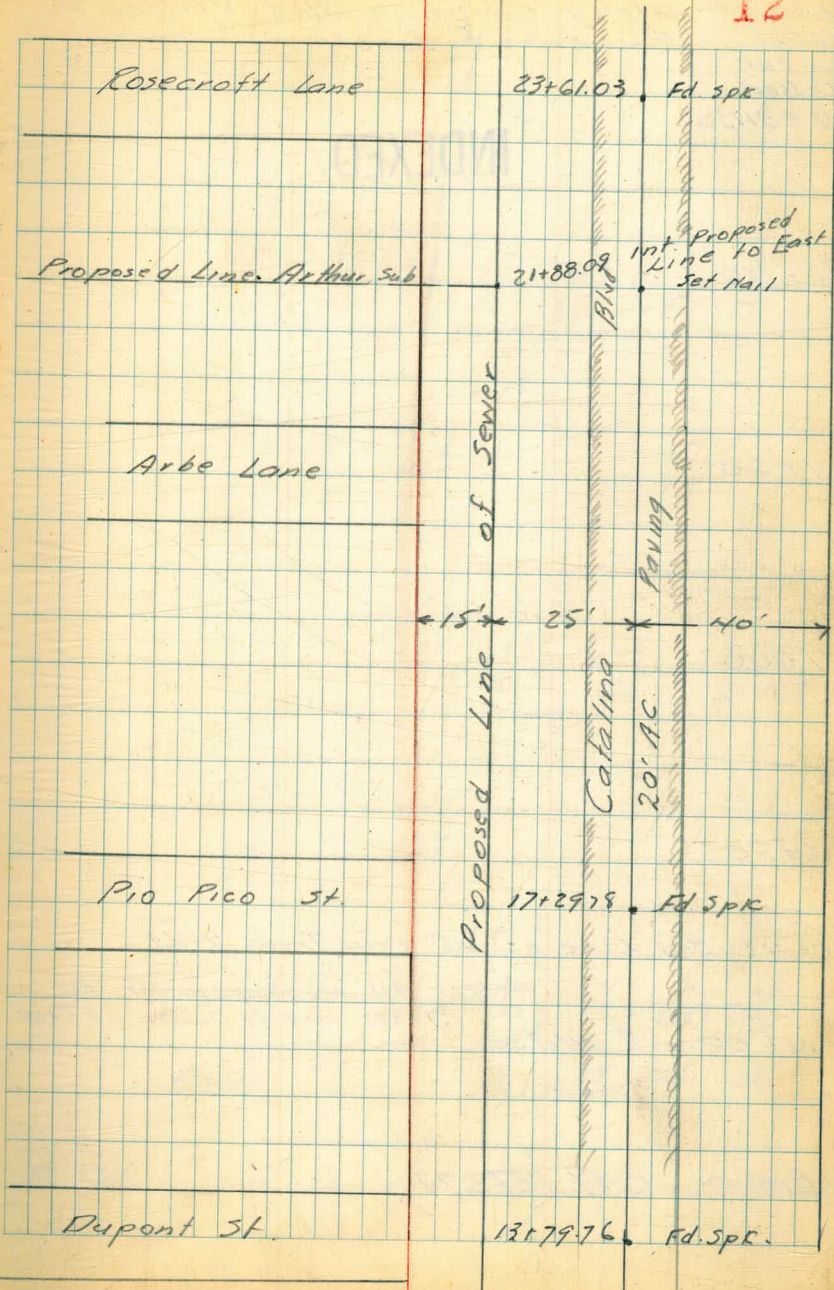
Paving

Pio Pico St

17+29.78 Fd Spr

Dupont St

13+79.76 Fd Spr



5-19-48 Levels Proposed Sewer
 Hendricks along Catalina Blvd. Wilcox to
 Walker Rosecroft Lane
 Becker
 Wilson
 HO # 31130

INDEXED

2+00

1+50

1+00

0+50

0+42 Beg Line of 48" Palm Trees 7' Lt.

Note: All measurements to
 Trees are to Center of Tree.

0+00 E Wilcox

B.M.

0.39 (272.77)

272.38

13

263.2

9⁶ 9⁸ 10⁸ 12¹ 12³ 10³
 15 65 105 150 275
 Paving

262.3

10⁵

260.7

12¹ 11⁵ 12⁵ 12³ 13⁰
 15 65 115 165
 Paving

259.2

13⁶

258.4

258.0

258.0

258.1

258.2

14⁴

14²

14²

14²

15⁵

15

35

65

155

Edge Paving

higher

E 5 ft. in par. Dudley & Catalina (from FB 1751-FT)

4+00

3+758 18" CMP H.W. on line

3+60.5 Fire Hydr. 55 Lt.

3+28.78 @ Charles St.

3+00

2+99 End of Palm Trees 7' Lt.

2+50

272.77

✓
2668

55	60	60	56	56	59	77	93	89	87
10	4		(15	35)	45	52	100	150	200

(Paving)

✓	✓
264.22	266.45
855	632
FL. H.W.	FL. H.W.
inlet	outlet

✓	✓
266.1	609
55	25
50	@ 5pt.

✓
265.3
75

✓
264.0
88

(177.77)

75
250

6+270 8" Euc 0.7 Rt.

6+13.0 10" Euc on Line

6+00

5+91.2 18" Euc 0.6 Rt.

5+89.1 15" Euc 0.7 Lt.

5+77.7 36" Euc 0.5 Lt.

5+50

5+04.76 & Alley

5+00

4+50

272.77

✓
270.6

22	22'	25	22	26	38	5	4
15	25	35	45	51	100	150	

Paving

✓
269.6

32

✓
268.7

24	4	4	387	377	389
50	15		15	25	35

Pav. Spk. Pav.

✓
268.5

43

✓
267.3

55

← 272.77 →

8+50

8+00

7+50

7+00

B.M 1234 $\left\langle \begin{array}{l} 284.72 \\ 0.39 \end{array} \right\rangle \left\langle \begin{array}{l} 272.38 \\ 272.38 \end{array} \right\rangle$

6+798 £ Dudley

6+42.6 10" Euc 0.9 RT

6+34.4 10" Euc 0.7 RT

272.77

278.0[✓]
62276.4[✓]

8 ⁵	8 ⁶	8 ⁵	8 ⁶	8 ⁷	10 ³	11 ⁸	12 ³
15	25	35	47	54	110	150	

N⁴

200

274.5[✓]
10³274.9[✓]
11⁸ $\left\langle \begin{array}{l} 274.74 \\ 274.74 \end{array} \right\rangle$

£ Spc. Dudley & Catalina

274.0[✓]

13 ⁵	0 ⁶	0 ⁸	0 ⁵	0 ³⁹	0 ⁴⁵
50	6		15	25	35
	Deq. Rev		Par	Spc	Par

 $\left\langle \begin{array}{l} 274.77 \\ 274.77 \end{array} \right\rangle$

12+50

12+15.5 End 10" pipe 0.8 Lt

12+06.5 ± & Alley

11+94.7 Beg 10" Metal Pipe across Alley
208

11+50

11+00

10+99.5 & 3' Board walk 3.3 RL

296.43

299.8
32

291.02
541
05

299.8 ✓

8' 12'
220 195

13	21	36	349	339	351	40	42	84	102	440
50	28		15	25	35	47	52	115	145	175
			PAV		PAV					

290.49 ✓
594
12

290.2 ✓
63

287.5 ✓
89

296.43 ✓

15+00 30" cyp 8' LH.

14+50

14+00

13+79.76 & Dupont St.

13+50

TP 7.25 $\left\langle \begin{array}{c} 302.90 \\ \hline \end{array} \right\rangle$ 0.78 $\left\langle \begin{array}{c} 295.65 \\ \hline \end{array} \right\rangle$

13+00

296.43

297.9 ✓
50

297.3 ✓
50

297.0 ✓
50 55 112 125 72
70 105 160 200

296.6 ✓
24 47 63 610 598 606
50 30 15 25 35
FeV SPC FeV

296.2 ✓
67
 $\left\langle \begin{array}{c} 299.30 \\ \hline 302.90 \\ \hline \end{array} \right\rangle$
295.2 ✓
15 295.39
104
15

B.17. 6.97 $\langle 306.58 \rangle$ 3.29 $\langle 299.61 \rangle$ 299.63

17+29.78 £ Pio Pico

17+00

16+58 36" Cyp. 8' Lt.

16+50

16+36.3 Power Pole H 450601H 37 Lt.

16+00

15+56 ± £ Alley

15+36.4 10" Euc. 8.0 Lt.

15+16.3 24" Euc. 9.5 Lt.

$\langle 302.90 \rangle$

£ Spike Catalina & Pio Pico P9 FB 1751 39

299.2 ✓
 25 3² 35 34 329 344 37 50 8! 74
 50 27 15 25 35 45 70 100 125

299.2 ✓

37

298.8 ✓

41

298.2 ✓

42 53 10² 6² 4²
 70 97 135 160

298.1 ✓

25 28 31 4⁸ 464 447 455
 50 30 15 15 25 35

$\langle 302.90 \rangle$

20+50

20+39 Power Pole # 95850 H 4' 3" Lt.

20+00

19+50

19+00

18+52 Power Pole # 95900 H 4' Lt.

18+50

18+29 24" Cyp 8' Lt.

18+14 30" Euc 6' Lt.

18+10.5 30" Euc 7' Lt.

18+00

17+91.5 36" Cyp 8.5' Lt.

306.58 ✓

21

300.1 ✓

C₅

300.3 ✓

C₇ C₇

20

299.9 ✓

C ₄	C ₇	5 ₅	5 ₅	5 ₄	5 ₅	5 ₂	7 ₁	8 ₂	C ₄
30		8	15	25	25	45	70	85	130
			Per						

299.8 ✓

C₈

299.5 ✓

7₄

299.2 ✓

7₄

306.58 ✓

BM

6.74 299.60 299.63

Spk & Catalina & Pio Pico (FB1757 - p.9)

TP 474 306.34 10.17 301.60

306.1

22

23+6103 & Rosecroft Lane End

6 ³	5 ⁷	5 ⁵²	5 ³⁹	5 ⁵²
60		15	25	35
		SPK	SPK	

23100

304. A
7²

22150

303.5
8²

21+88.09 Int of Line Through Arthur's Sub.

302.5 ✓
9²

21+50

10.17 311.77
 TP On PIPE w Line Arthur Sub
 Bet lots 889 498 301.60

301.6
10²

311.77 21

21+00

301.0 ✓
5²

?
20+82+ & Arbe Lane

300.8 ✓

6¹ 58
50

306.58

306.58 ✓

5-19-48
Hendricks
Walker
Becker
Williams

Proposed Sewer in Arthur Sub
East of Catalina Blvd Between
Arbe Lane & Rosecroft Lane

Levels Next Page

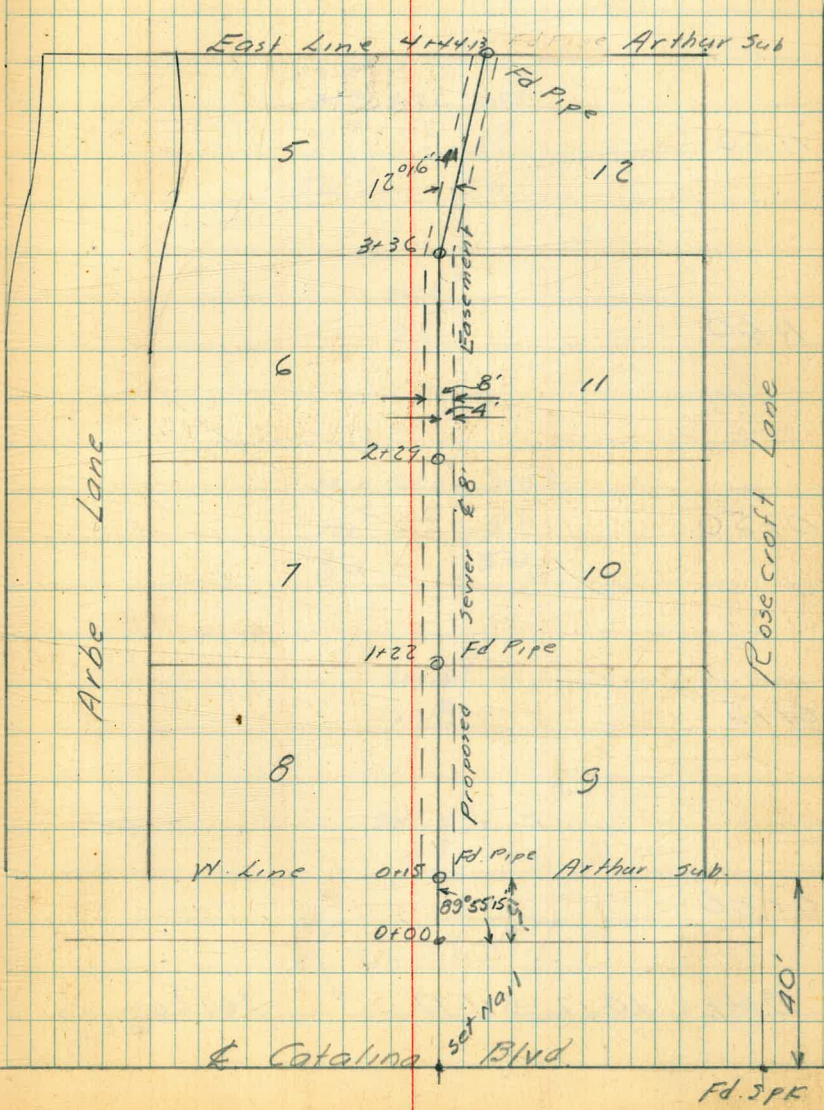
INDEXED
WK
APR 25 1949



Pio Pico St

Fd Spc

See page 44



5-19-58
 Hendricks
 Walker
 Becker
 Williams

Levels Proposed Sewer
 in Easement Arthur's Sub

7+82

1+50

1+00

0+50

0+15

0+00

B17 10.17 311.77 301.60

✓ 302.5	✓ 301.9	✓ 302.4
9 ³ -	9 ⁹ -	9 ⁴ -
50		50

✓ 301.9	✓ 302.2	✓ 302.7
9 ⁹ -	9 ⁶ -	8 ⁹ -
50		50

302.0 ✓
9⁸

✓ 301.0	✓ 302.0	✓ 302.2
10 ⁸ -	9 ⁸ -	9 ⁶ -
50		50

301.6 ✓
10²

302.5 ✓
9³

311.77

On Pipe W. Line Arthur's Sub Lots 8 & 9

4+00

see page

3+36

3+00

2+50

2+25 30" Cyp. 25 ft.

2+00

311.77

AA

310.0 ✓

18

307.77 ✓

400

PIPE

307.0 ✓

48

50

306.7 ✓

51

100

306.4 ✓

54

304.6 ✓

72

304.4 ✓

74

50

303.2 ✓

82

311.77

1317 6.74 299.60 299.63
 TP 474 306.34 10.17 301.60

4195

4+46 30" CYP 25 RT

4+44.13 50 Line Sub Division

4+41.5 36" CYP 10.5 LH

311.77

See

Spk & Catolima & Pio Pico

Page 4A

315.2
+ 34
$$\begin{array}{r} 312.8 \\ + 10 \\ \hline 322.8 \\ \hline 50 \\ \hline 311.5 \end{array}$$

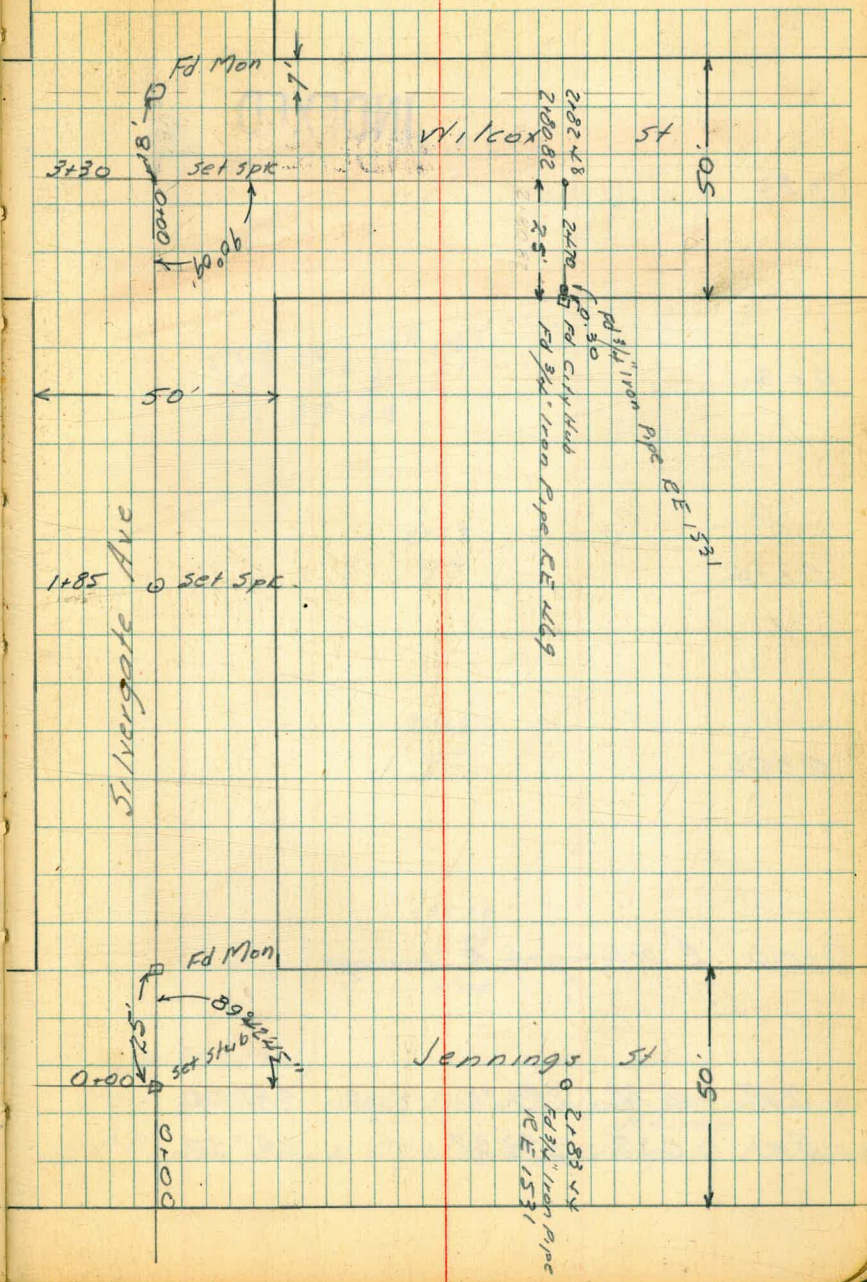
311.77

5-19-48
Hendricks
Walker
Becker
Nelson

Proposed Sewer Silvergate, Wilcox
& Jennings Sts

27

INDEXED



INDEXED

0+50

276.3
75

0+30

272.9 274.2 275.7 276.7
10.9 9.8 8.1 8.1
50 39 13

0+15

274.8
90

0+05

274.8
90

0+00 $\frac{1}{2}$ Silvergate & Jennings

275.80
7.98
Hub

T.P. 278 283.78 12.37 281.00

B.M. 0.85 293.37 292.52

(# 92267H)

Mail in Pole East Side Silvergate Bet Wilcox & Jennings

SE BP End E Curb Charles & Silvergate FB1751-21

3+00

2+50

2+29 S. Edge of House

2+00

1+53 S. Edge of House

1+00

282.78

277.2	280.0	280.7	281.9
6 5	7 8	5 1	1 9
100	50	20	

280.6
3 1

278.93	276.7	278.7	280.0
4 8 5	7 1	5 1	3 8
Floor	8 3	20	
	Back		
	edge		
	House		

279.5
3 1
4 1

276.98	276.2	276.6	278.2
6 8 0	7 6	7 2	5 4
Floor	8 0	20	
	Back of		
	House		

277.3
6 1

T.P. 10.62 293.51 0.89 28289

3+30 £ Wilcox St.

28378

278.1	280.8	281.6	282.7
52	30	22	15
100	50	21	

Levels Proposed Sewer on
Wilcox St. & Silvergate to West.

INDEXED

1+00

287.7
5
1

0+92

287.6
6
1

0+74

284.9
8
6

0+39

282.7
10
2

0+18

282.2
11
3

0+00 & Silvergate

282.6
10
2

293.51 from P30
π

2+50

288.6	289.4	286.1	279.4
<u>49</u>	<u>41</u>	<u>74</u>	<u>141</u>
	17	50	100

2+25

289.6
<u>39</u>

2+00

290.0	289.7	289.3	288.1	288.5
<u>35</u>	<u>38</u>	<u>42</u>	<u>54</u>	<u>100</u>
	13	29	50	100

1+75

290.1
<u>34</u>

1+50

289.6
<u>39</u>

1+30

288.8
<u>42</u>

293.51

TP			11.61	25809
TP	0.70	26970	12.84	26900
TP	0.62	28184	12.29	28122

3*75

3+00

293.51

on 2" pipe 2+8344 & Jennings St.

280.5	279.9	270.7	278.0	273.6
130	125	125	155	195
	17	23	50	100

285.6	285.6	286.3	282.7	278.8
75	79	75	105	142
	11	15	50	100

5-20-58 Levels Proposed Sewer
 Hendricks on Jennings St Silvergate
 Walker to West
 Becker
 Williams

1+75

1+76 Power Pole # P 3625 21' Lt.

1+25

INDEXED

1+00

0+80

0+40

0+00 & Jennings & Silvergate

B.M. 0.78 276.58 275.80

265.2
 11' 13' 14' 16'
 7 50 100

267.5
 10' 28' 45' 79'
 139 95 60 21 7

262.8 268.3 262.3
 +29' 38' 52' 83' 83'
 135 100 50 23 50 100

272.6 278.5 268.0 266.6 262.7
 +34' 40' 68' 81' 84' 67' 75' 86'
 138 100 77 50 26 21 16 50 100

271.0 266.2
 +14' 22' 43' 53' 55'
 100 50 29 15 26 76 111 111
 Back of Garage Floor

275.80 275.2 274.6 270.1 266.3
 0.78 14' 29' 65' 10'
 Sub 10 26 75 106

On hub & Jennings & Silvergate P.28

T.P. 653 258.07 258.09

3+75

3+00

2+8344

2+77 48" Cyp. 7' Lt. & to Center of tree

2+50

2+41 36" Cyp. 2' Lt. to & Tree

2+01 36" Cyp. 2' Lt. to & Tree

T.P. 0.63 264.60 12.61 26397

27658

R-33

256.0

8 [±]	8 [±]	8 [±]	12 [±]
23	41	100	

258.0

6 [±]	7 [±]	9 [±]	12 [±]
37	44	100	

258.07

653

R.P.E

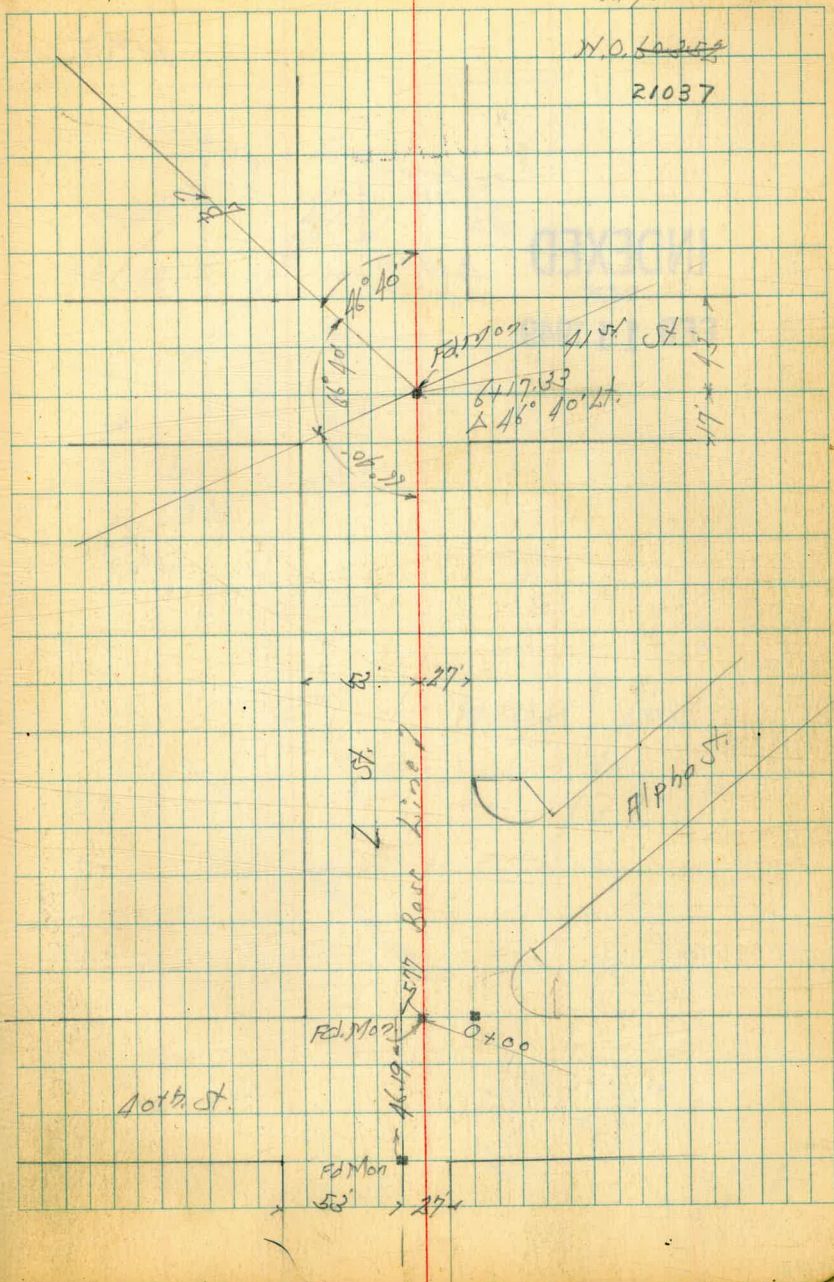
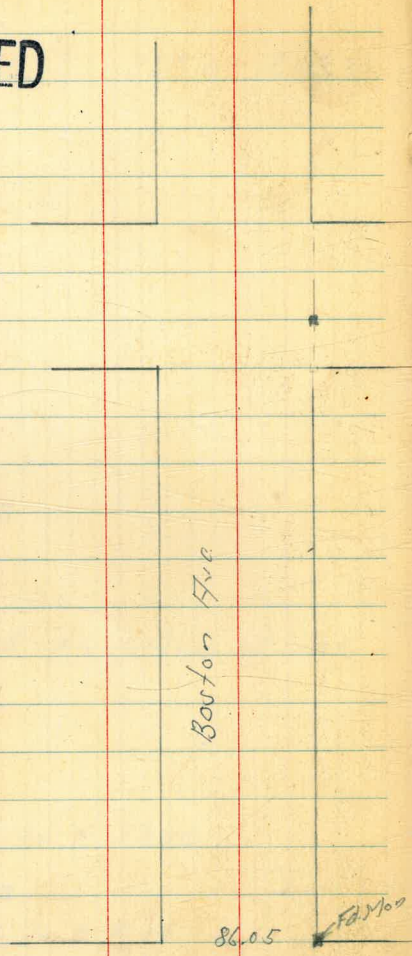
259.9

47	7 [±]	9 [±]
50	100	

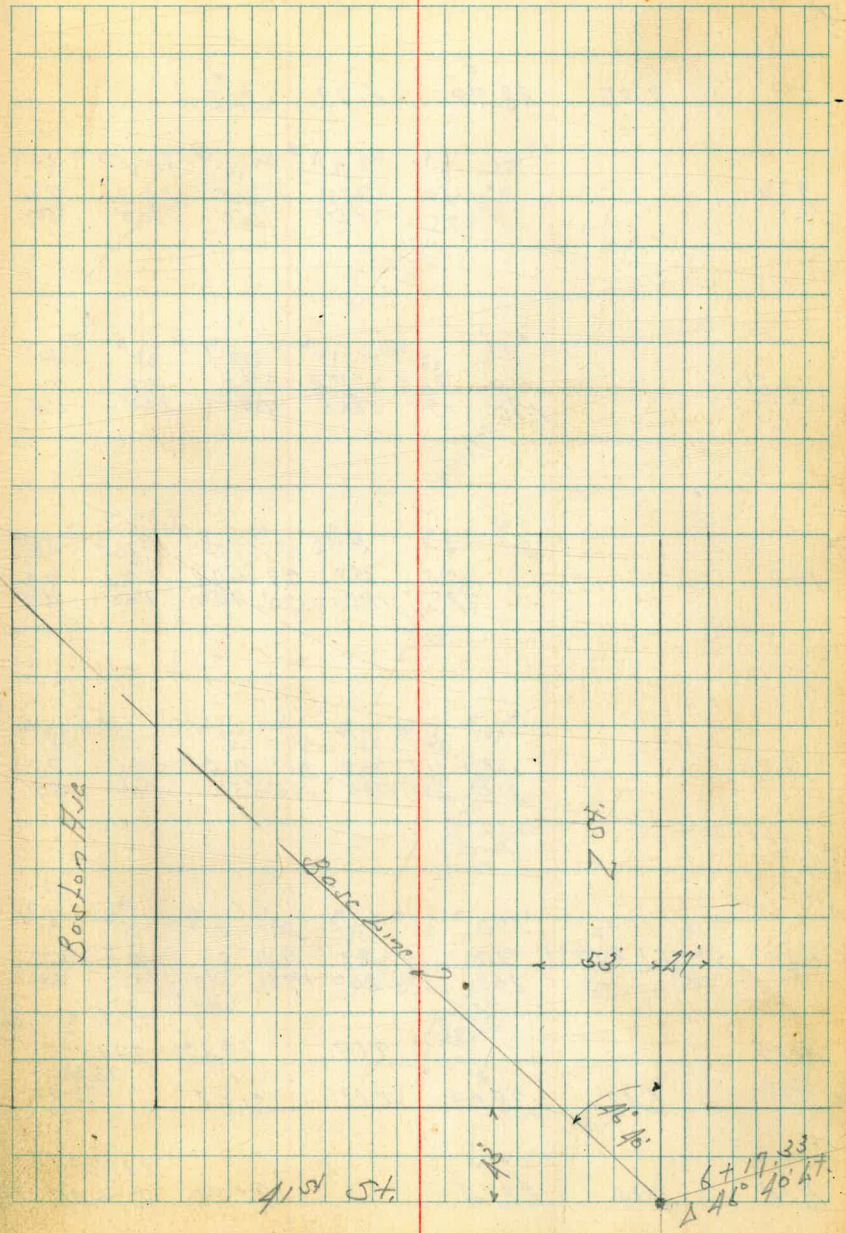
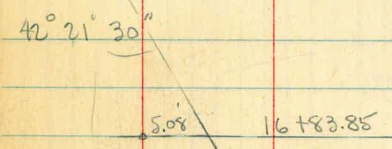
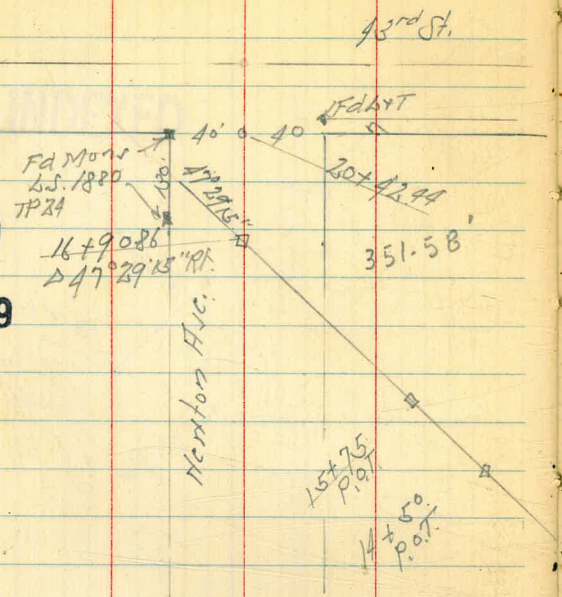
263.3

1 [±]	3 [±]	4 [±]	5 [±]
21	50	100	

INDEXED



INDEXED
WK
FEB 11 1949



Cross Section South Coast Park Playground

	+	H ¹	-	Et				
			Lt=North					
TP	7.55	28.79	6.77	21.24				
±10		11.1 169 175'	12.1 159 150'	16.5 115 140'	20.7 73 100'	20.9 71 50'		
		Sly Wash Water Line						
+50		11.1 169 175'	12.4 151 170'	18.6 94 165'	20.5 75 150'	21.0 70 100'	20.9 71 50'	
		Sly Wash						
+10		11.5 165 190'	13.7 143 185'	20.3 77 170'	20.7 73 150'	20.6 74 100'	20.9 71 50'	
		Sly Wash						
+50		11.3 167 215'	16.6 144 200'	17.2 108 185'	20.0 80 175'	20.5 75 150'	20.4 76 100'	19.8 82 50'
		Sly Wash Water Line						
0+0	FL 90 th St	12.0 160 250'	16.3 117 230'	16.3 117 200'	18.6 94 190'	19.8 82 150'	19.6 84 100'	19.5 85 50'
BM				9.69	18.32	21.40 th		
TP	648	28.01	5.61	21.53	18.32	16.25-29		
BM	2.34	27.14		24.80	18.140 th	21.41 th		

81-50

	22.2 58 0.0	22.0 60 50'	22.8 58 100'	24.4 36 150'	25.0 30 190'				
	21.3 67 0.0	22.0 60 50'	22.5 55 100'	23.6 44 150'	24.0 40 190'				
	21.1 69 0.0	21.4 66 50'	22.0 60 100'	21.9 61 150'	22.6 54 195'				
	20.3 77 0.0	20.6 74 50'	20.7 73 100'	20.7 73 150'	20.9 71 190'				
	18.2 82 100'	18.18 80 50'	19.5 86 100'	19.3 87 50'	19.8 82 100'	20.1 79 130'	20.1 79 160'	19.8 82 190'	
	Ground								
	180'								

81-South

Lt-North

5+0
 12.6 14.7 22.5 23.3 22.6 23.1 23.1
 211 190 112 104 111 106 106
 270=St/100 250 235 200 150 100 50

TP 9.52 33.66 465 24.14

+50
 12.4 16.0 22.7 22.8 22.3 23.6
 164 128 61 60 65 52
 240=St/100 230 190 150 100 50

4+0
 12.2 15.8 18.3 22.0 22.4 21.2 22.5
 166 130 105 68 64 66 63
 230=St/100 200 180 170 150 100 50

+50
 12.3 14.5 16.8 21.7 22.1 22.5
 165 143 120 71 67 63
 200=St/100 190 150 135 100 50

3+0
 11.8 15.1 21.0 21.8 21.6
 170 137 78 70 72
 180=St/100 150 135 100 50

2+50
 11.8 11.7 19.7 21.0 21.2
 170 171 91 78 76
 175=St/100 150 130 100 50

28.79

39

Rt-South

22.8 24.2 28.0 33.7 38.7 42.7
 109 95 57 20 150 190
 0.0 50 100 150 180 185

33.66 X

22.8 23.4 26.4 34.1 41.3
 60 54 34 150 185
 0.0 50 100 150 185

22.8 22.8 25.0 28.8 31.2
 60 60 38 0.0 84
 0.0 50 100 125 170

22.5 22.2 23.0 25.8 32.4
 63 66 58 50 36
 0.0 50 100 130 145

22.1 22.2 23.4 26.1
 67 66 54 27
 0.0 50 100 135

22.3 22.4 23.0 24.1 26.1
 65 64 53 47 27
 0.0 50 100 130 145

28.79

LT=11

8x0
 13.1 15.1 22.7 23.5 23.6 23.9 24.1
 236 216 140 135 151 138 126
 252 235 225 200 150 100 50
 152=51 2054

+50
 23.1 23.2 23.2 23.6 24.5
 136 135 135 131 122
 200 200 150 100 50

7x0
 22.9 23.7 24.6 25.3 25.3 24.7
 138 130 141 114 114 120
 130 100 76 76 50 50
 Ground Floor
 114 Blk
 09/02
 09/02

6x50
 24.4 28.3 29.8 34.2 41.4 45.7 46.3 48.5 53.4
 123 84 69 25 44 90 96 118 167
 00 50 100 110 160 200 250 270 300

Taken on Sept
 6x17.33 146'40" Lt.
 23.2 23.0 23.6 23.1
 135 137 131 126
 200 150 100 50

IP 11.90 36.70 8.86 24.80 25.4 41.4 St
 09/13/2000

5x50
 13.0 16.0 23.4 23.2 22.7 22.9 23.5
 207 177 103 105 110 108 102
 295 275 255 200 150 100 50
 114
 23.66

40

PT=5

24.5 25.2 26.9 29.2 34.7 42.0 48.4 72.5 77.6 91.3
 122 115 98 75 20 152 117 259 409 416
 00 50 100 150 200 240 290 370 428 488

24.1 25.4 27.9 28.9 32.2 35.9 42.2 57.8 70.4 77.9
 126 112 88 78 45 08 55 211 339 413
 00 50 100 130 150 200 235 314 334 413

23.9 25.8 28.4 29.5 33.3 36.5 40.7 48.7 57.7 71.5
 128 109 82 72 24 02 40 120 210 318
 00 50 100 117 135 178 225 275 310 386

24.4 28.3 29.8 34.2 41.4 45.7 46.3 48.5 53.4
 123 84 69 25 44 90 96 118 167
 00 50 100 110 160 200 250 270 300

24.8 26.3 29.0 29.9 38.7 48.9 59.2 72.5
 149 104 77 68 20 122 225 358
 00 15 20 30 90 135 175 205

36.70 St

23.6 26.9 29.8 36.7 40.9 49.2
 101 68 39 20 72 155
 00 50 95 125 150 190

33.66

South Crest Park Playground

40

11+0
 14.3 16.3 24.6 26.0 27.1
 252 232 149 135 124
 153 145 133 100 80

Sty Wars

+50
 13.8 17.5 24.5 25.9 26.5
 257 220 150 126 120
 178 157 145 100 50

Sty Wars

10+10
 13.8 16.3 23.5 25.3 25.8
 257 227 160 142 137
 186 170 155 108 50

Sty Wars

TP 10.99 39.48 8.21 28.49

+50
 13.0 15.5 16.6 23.3 24.8 24.7 25.1
 227 212 201 184 119 120 116
 212 205 180 165 145 120 50

Sty Wars

9+0
 13.0 16.6 23.8 24.3 24.1 24.7
 227 201 129 124 116 120
 225 195 180 150 100 50

Sty Wars

8+50
 12.8 16.3 23.8 24.0 23.7 24.0
 229 204 129 127 120 127
 210 225 200 150 100 50

Sty Wars

36.70

40

41

27.8 29.4 31.2 33.0 33.8 37.0 44.1 58.9 63.1
 147 9.9 8.3 65 57 35 46 194 236
 0.0 50 100 150 180 200 250 292 318

27.2 28.7 30.1 32.0 32.5 35.8 43.5 70.2 71.3
 123 108 94 75 79 27 40 30.7 31.8
 0.0 50 100 150 180 200 250 319 328

27.2 27.8 29.3 31.1 31.4 34.7 40.4 69.2 69.4
 123 117 102 84 81 48 0.9 29.7 29.9
 0.0 50 100 150 180 200 270 320 370

39.48

25.9 26.7 28.1 29.7 33.2 35.3 49.0 62.2 64.2 71.8
 108 100 86 70 35 14 123 155 175 135
 0.0 50 100 150 200 240 283 326 392 442

25.3 26.2 27.2 28.8 33.4 40.0 51.3 56.2 64.2 73.3
 114 105 95 79 32 23 46 195 275 316
 0.0 50 100 150 200 253 298 347 386 450

24.7 25.9 26.8 28.8 33.8 39.5 48.1 59.2 72.4 78.1
 120 108 99 79 39 28 14 22.5 35.7 41.1
 0.0 50 100 150 200 250 302 367 407 460

36.70

Prop. sewer in Arthur Sub.
Cont. from page 23

A/22/49
W.O. 31130

El. Ord.
on Φ

INDEXED
NK
APR 25 1949

4+44 312.4

3+98 309.6

3+82 309.4

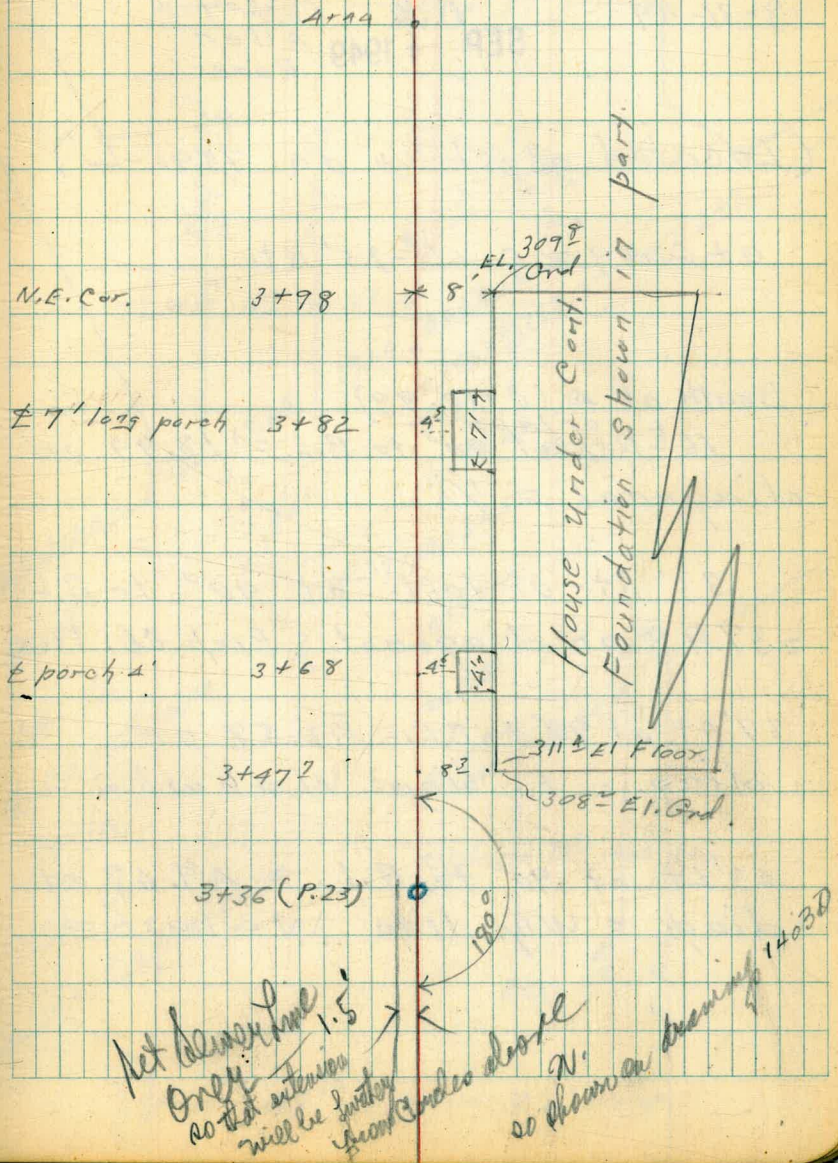
+68 309.0

+171 308.2

3+36 (P.25) 307.8

Sommer mayer
McCoy
Allen
Jones

44



Wabaska Dr
Capistrano to Poe

B.L. = $\frac{1}{4}$ prop. Imp. as per

NOTE $\begin{cases} 33' \text{ Rt. (or Lt.) at } 90^\circ = \text{cb.} \\ 16\frac{1}{2}' \text{ Rt. (or Lt.) at } 90^\circ = \frac{1}{4} \end{cases}$

Also $31\frac{1}{2}' \text{ Rt.} = \text{face cb. to come out}$
taken parallel to Capistrano.
0+00 Sec. from here on arc

P. = prop. line Wabaska Dr.

0+00 Sec. at 90° to B.L.

0-10

Also 25' Rt. = outlet exist 3' culvert.

(To come out)

0-39^e 33' Lt. = B.C. cb. half constructed

0-50

E.P. = edge of paving

N.W.B.P.
Capistrano & Poe
1.95 73.57 — 71.62

FB 1822
41
+ 64

B.L.

46

72.2	69.9	68.5	68.6	68.5	68.0	68.2	68.5	68.11	69.06	69.1	69.2
1.4	3.7	5.1	5.0	5.1	5.6	5.4	5.1	5.46	4.51	4.5	4.4
P.	23'	EP	1/4	1/4	0.5	EP	1/4	3	Top Ch.	0.5	prep
									to come out.		
70.4	68.9	68.6	68.0	68.2	69.3	64.0	64.0				
3.2	4.7	5.0	5.6	5.4	4.3	9.6	9.6				
43	21	13	0.5	EP	14	32	37				
70.4	69.1	68.5	68.4	67.9	68.0	70.0	61.0	62.1			
3.2	4.5	5.1	5.2	5.7	5.6	3.6	12.6	11.5			
43	32	20	12	0.5	EP	10	31	37			
		EP		EP							
									58.75		
									14.72		
									25.111111		
73.0	71.5	67.6	67.6	67.2	67.9	64.1	64.8	64.3	64.8	64.8	64.8
0.6	2.1	6.0	6.0	6.4	5.7	4.5	8.8	14.3	13.8	13.8	13.8
43	26	21	12	22	EP	12	20	28	37	37	37
		EP		EP							

73.57

$\Delta 1^{\circ}-25'$ RT.
 0+60⁹⁹ = Nly. 7' line Capistrano.

0+57⁵⁴ = Nly. Cl. line Capistrano

0+46⁰³ = Nly. 1/4 Capistrano.

0+34⁵² = $\frac{1}{4}$ Capistrano

0+23⁰² sly. 1/4 Capistrano

0+11⁵¹ Cont.

0+11⁵¹ sly. cl. Capistrano

68.6	68.6	68.8	68.9	68.9	68.7	68.3	68.0	67.9
5.0	5.0	4.8	4.6	4.6	4.9	5.3	5.6	5.7
P.	Cl.	25'E E.P.	1/4	15	E.P.	1/4	Cl.	P.

69.7	69.1	68.9	69.1	69.0	68.6	68.3	68.3	68.4
3.9	4.5	4.7	4.5	4.6	5.0	5.3	5.3	5.2
P.	Cl.	25'E E.P.	1/4	16	E.P.	1/4	Cl.	P.

70.2	69.5	69.1	69.0	68.9	68.5	68.3	68.3	68.3
3.4	4.1	4.5	4.6	4.7	5.1	5.3	5.3	5.3
P.	Cl.	27 E.P.	Cl.	15	E.P.	1/4	Cl.	P.

70.3	69.6	69.1	68.8	68.8	68.4	68.2	68.1	68.1
3.3	4.0	4.5	4.8	4.8	5.2	5.4	5.5	5.5
P.	Cl.	25 E.P.	1/4	15	E.P.	1/4	Cl.	P.

70.5	69.27	69.57
3.1	4.30	4.00
P.	50 Top.	100 Top.

69.2	68.9	68.7	68.7	68.3	68.4	68.2	68.2	69.23
4.4	4.7	4.9	4.9	5.3	5.2	5.4	5.4	4.34
Cl.	24 E.P.	1/4	15	E.P.	1/4	Cl.	P.	45'E Top. Expt Cl. E.C.

73.57

T.P. 5.89 75.22 4.24 69.33

1+50

Come out.

1+07 28th Rt. = End Exist. cl. - To

from here on.

0+69th Sec. at 90° to Wabaska Dr.

42nd Lt. = End Exist. cl.

0+56 at 90° to Wabaska Dr.

Cont.

0+69th Sec. Parallel to Capistrano
= Nly. line Capistrano.

72.5	70.7	69.4	69.5	69.6	69.4	69.3	69.2	69.8	69.7
1.1	2.9	4.2	4.1	4.0	4.2	4.3	4.4	3.8	3.9
43	33	26	16 ²	11		25	165	33	37
		E.P.				E.P.			

73.6	70.7	69.1	69.3	69.3	69.0	68.9	69.1	68.43	68.4	68.5
0.0	2.9	4.5	4.3	4.3	4.6	4.7	4.5	5.14	5.2	5.1
43	33	26 ²	16 ²	11		25	165	28 ²	33	37
		E.P.				E.P.		Top Exist. cl.		

72.3	70.8	68.7	69.1	69.1	68.7	68.5	68.2	68.2	68.3
1.3	2.8	4.9	4.5	4.5	4.9	5.1	5.4	5.4	5.3
43	33	27	16 ²	11		25	165	33	37
		E.P.				E.P.			

68.92
4.65
42nd
Top. End of cl.

69.09 68.2
4.48 5.4
45² 45²
Top. Exist. cl.

68.4	68.8	69.0	69.0	68.7	68.6	68.1	67.7	68.43
5.2	4.8	4.6	4.6	4.9	5.0	5.5	5.9	5.14
cl	26	14	14		25	14	cl	43 ² Top
	E.P.				E.P.			Exist. cl.
								(To come out.)

73.57

orig. B.M. P. 46

3.61

71.61

71.62

3+00

2+59^E 15^E Rt. = End. Exist. Wly. cl. on pcc

2+50 Cont.

cl. line pcc. st.

2+50 20^E Rt. = face exist. cl. on wly

2+00

B.L.

49

70.0	69.8	69.8	70.1	70.2	70.3	70.3	70.3	70.5
5.2	5.4	5.4	5.1	5.0	4.9	4.9	4.9	4.7
4.3	3.3	2.5	1.6	1.1		4	1.6	3.3
		E.R.				E.R.		

70.25
4.97
1.5
70.25
cl.

71.8	70.7
3.4	4.5
4.3	3.3

71.0	69.6	70.0	70.1	70.1	69.9	70.3	70.27	69.5	70.5	70.7
4.2	5.6	5.2	5.1	5.1	5.3	4.9	4.95	5.7	4.7	4.5
3.0	2.5	1.6	1.1		4	1.6	2.0	2.1	3.3	3.7
	E.R.				E.R.		Exist	on		

72.0	71.1	69.5	69.7	69.8	69.7	69.7	69.7	70.2	70.3
3.2	4.1	5.7	5.5	5.4	5.5	5.5	5.5	5.0	4.9
4.3	3.3	2.6	1.6	1.1	2.5	1.6	1.6	3.3	3.7
		E.R.			E.R.				

75.2.2

9/7/49 Wabaska. WO 20536
 Beggs at Capistrano extended
 Sherman
 Sisson south 200 feet see map p45
 see -10 2 -50 p 46

- 200 72.1 69.0
 1.1 4.2
 40 38

- 150 74.2
 + 1.0
 40

- 100 75.0 72.33
 + 1.1 0.9
 45 35

- 50 see p 46

- 10 see p 46

N.W. BP 1.61 73.23

Capistrano + Pee

71.62
 p 46

50

64.93 65.15 64.81 65.1 66.0 60.2 59.2 57.6 56.6
 8.30 8.08 8.42 8.1 7.2 13.0 14.0 15.6 16.6
 20.7 11.7 7 5 15 25 40 43
 PAN

69.9 66.08 66.27 65.90 66.2 66.9 62.7 60.4 58.4 57.6
 3.3 7.15 6.96 7.39 7.0 6.3 10.5 12.8 14.8 15.6
 27 20.8 11.4 1 8 16 30 40 43
 PAN

69.7 66.89 67.04 66.6 67.1 68.2 64.8 62.9 60.1
 3.5 6.34 6.19 6.6 6.1 5.0 8.4 10.3 13.1
 24 20 12 2 9 17 25 40
 PAN

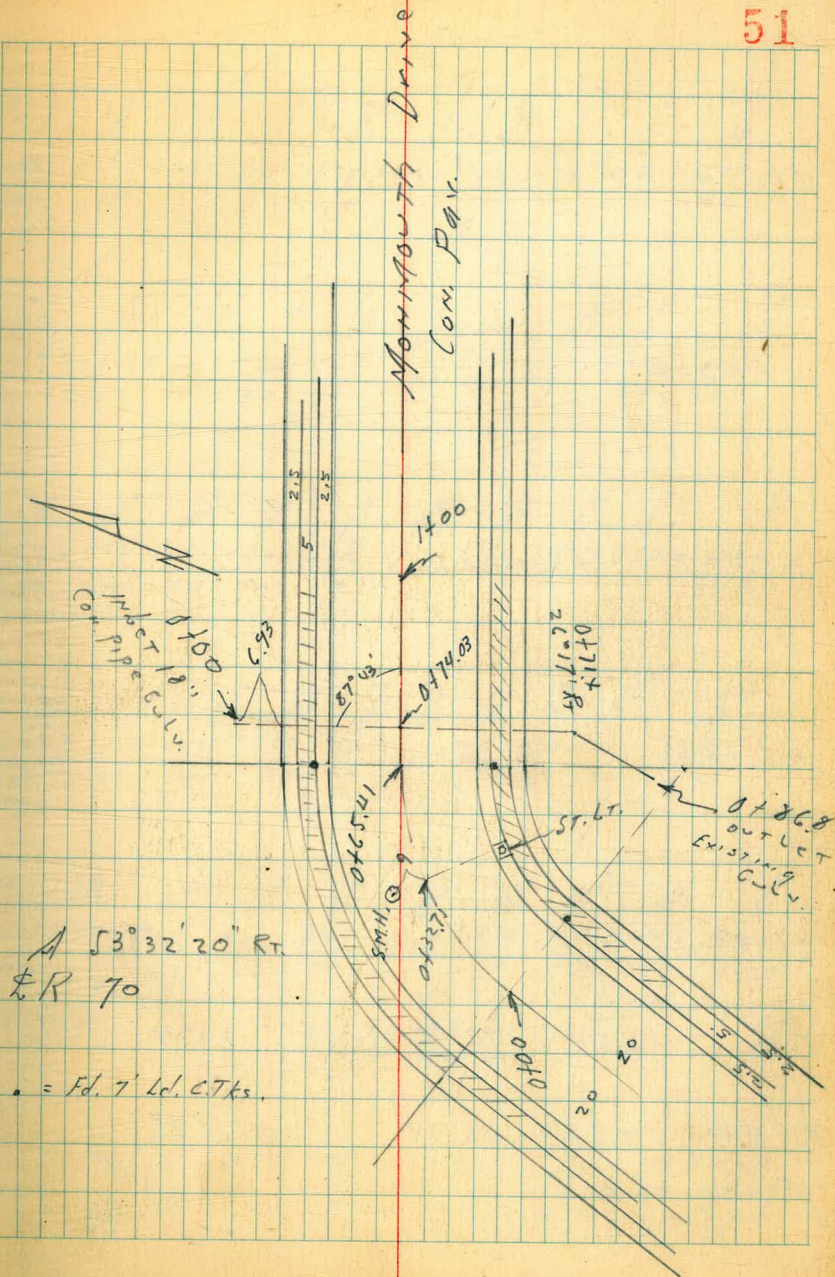
Levels for Proposed drain and
N. curb outlet on
Monmouth Dr. Eastly of
Foot Hill Blvd

10-25-49

Moon
Hardin
D. Sisson

NO 20585

INDEXED
W. K.
OCT 26 1949



016541 E.C.

174.6
2.0
30
3x
3x

0 + x 9.06

172.0
0.0
3x

0 + 32.71 F.L. Sewer M.H.

164.22
12.73

170.6
+ 3.7
3x

0 + 16.35

180.0
+ 3.0
3x

0100 B.C.R.

179.0
+ 2.0
3x
171.4
5.5
30

T.P. 2.58 176.95 12.57 174.37

Top Lot

BMBP 0.58 186.94

186.36

M. Corbett
Mandawish Dr.
at W.G. Congress Hrs.

No Record

174.0 173.79 173.50 172.94 173.23 173.21 172.89 172.23 172.77 172.91
2.9 3.1 3.5 4.0 3.7 3.7 4.0 4.7 4.8 4.0
30 27.5 20 20 10 10 10 20 20 27.5

174.0 174.52 174.42 171.72 171.90 171.94 171.71 171.14 171.75 171.72
3.0 4.8 4.5 5.3 5.05 5.01 5.24 5.81 5.20 5.23
30 27.5 20 20 10 10 10 20 20 27.5

174.6 171.42 171.32 170.65 170.83 170.85 170.55 170.00 170.60 170.59
2.3 5.53 5.63 6.30 6.12 6.10 6.40 6.95 6.35 6.36
30 27.5 20 20 10 10 10 20 20 27.5
M.H.
R.M.

174.0 170.32 170.20 169.50 169.65 169.60 169.30 168.69 169.34 169.43
2.9 6.63 6.75 7.45 7.30 7.35 7.65 8.26 7.63 7.52
30 27.5 20 20 10 10 10 20 20 27.5

168.75 168.69 167.90 168.09 167.65 167.23 167.84 167.91
8.20 8.26 9.05 8.93 8.86 9.30 9.72 9.13 9.04
27.5 20 20 10 10 10 20 20 27.5
Nudge
WALK
176.95 ✓
Sedge
WALK

check to orig. BM 024 186.38 186.38 ✓

TP 1026 186.64 0.59 176.30 ✓

Level on Existing Con. Pipe dn

0+00 F.b. ^{EXISTING} inlet 5.51 171.29

0+86.8 " outlet 14.26 162.69

1+00

175.6
1.2
30

0+78 Sec at 90°

3.7 173.9
4.0 173.0
4.1 172.8
56 46 36

176.95

66

Notes Reduced. 1-12-50

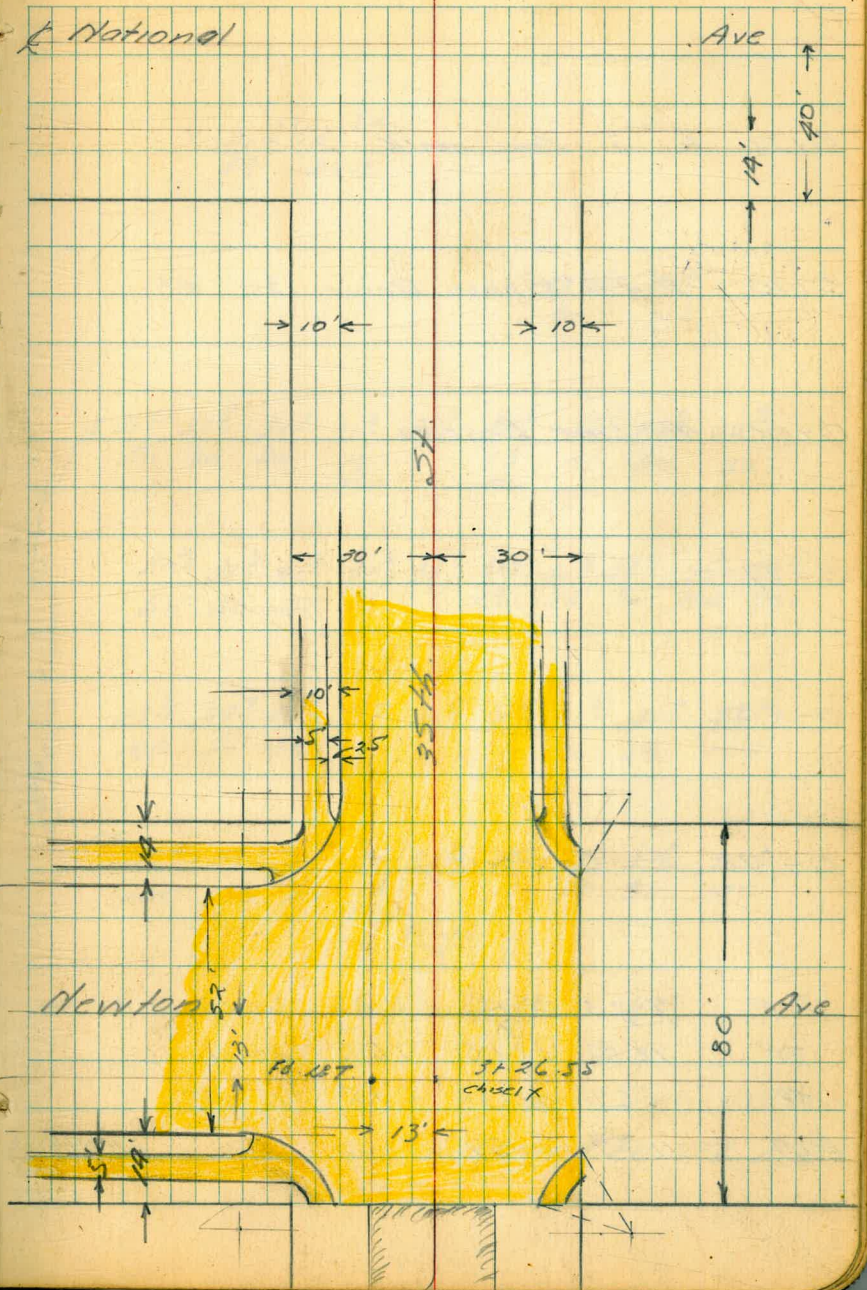
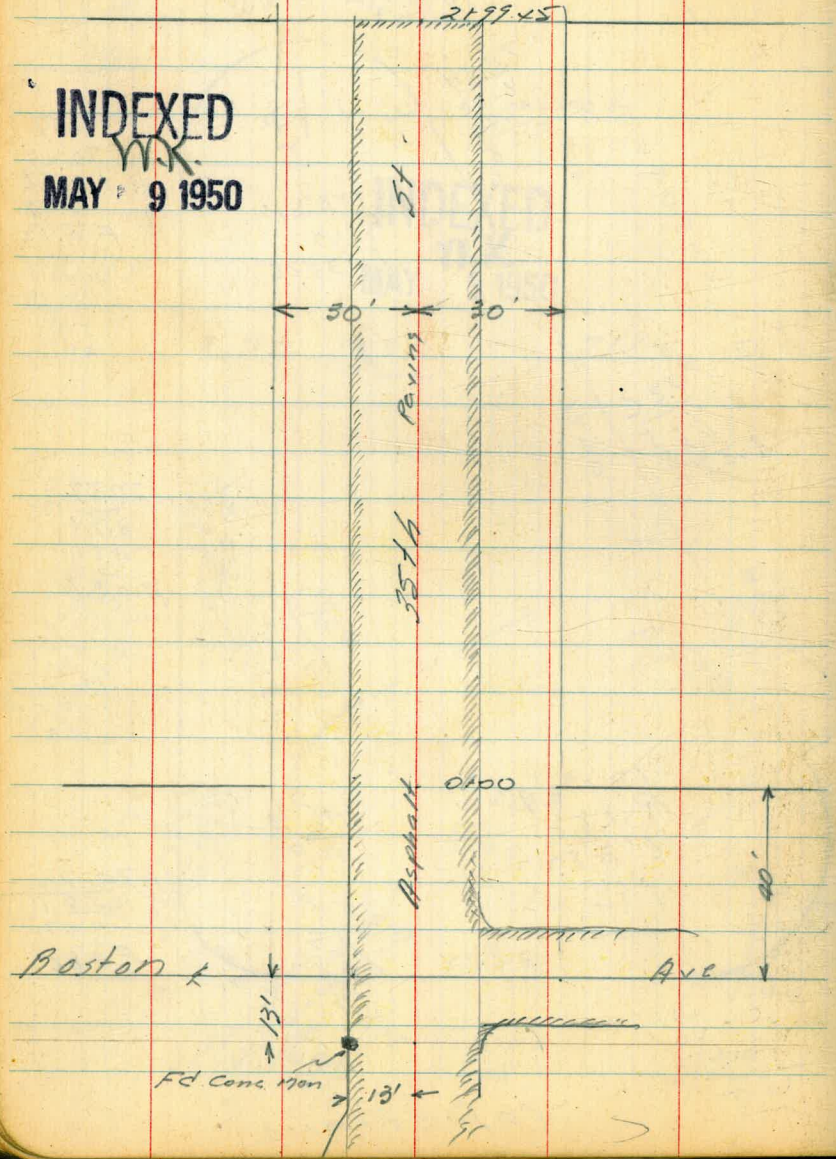
0.7 174.2
30
0.6 174.4
27.5
0.5 176.44
20
1.12 175.83
20
0.76 176.15
10
0.77 176.18
10
0.97 175.99
10
1.53 175.42
20
0.96 174.99
20
0.75 176.20
27.5

2.1 174.6
30
2.36 174.59
27.5
2.45 174.50
20
3.09 173.86
20
2.75 174.20
10
2.81 174.14
10
3.00 173.95
10
3.28 173.27
20
3.50 173.93
20
3.58 173.97
27.5

176.95 ✓

5-5-50 X Sect 35th St Boston to
 National Ave
 Hendricks
 Johnson
 Greer
 McCoy
 W0*
 25020 Newton

INDEXED
 MAY 9 1950



0+21 L 3' Conc Walk 28.3' Lt.

31.79 31.84
33 28.3

0+10 L 2' Ribbon Drive 30' Rt.

33.62 33.81
30 25

0+00 No. Line Boston

31.4 31.5 31.7 31.2 31.7 31.6 32.2 32.9 33.5
50 30 20 13 13 13 21 30 50
Pav Pav

0-17

31.2 31.3 30.8 31.0 31.5 31.4 31.8 32.5 33.2 33.5
50 30 22 13 13 25 30 42 50
Pav Pav

0-23

28.7 29.9 30.3 31.0 31.5 31.4 31.5 31.9 32.7
100 50 30 13 13 30 50 100
Pav Pav

0-40 L Boston

28.7 29.9 30.3 30.9 31.2 31.2 31.5 31.9 32.7
100 50 30 13 13 30 50 100
Pav Pav

38.48

SW 13' Conc Man. Boston & 35th St.

SW 13' Conc Man Sing & Birch (FB 1177 P54)

Elevations

T.P.	7.73	38.48	2.08	30.75
TP	12.22	32.83	1.62	20.61
TP	6.61	22.23	6.95	15.62
B.M.	11.59	22.57		1098

113972 So. Line Alley

1135 & 8' Conc. Drive on Rt. 16.5

1121 & 2' Conc. Walk on Lt. 30'

1114 & 3' Conc. Walk on Rt. 30.2'

T.P. 8.34 $\frac{42.23}{\text{A}}$ 4.59 33.89

1100

0162 & 2x2' Ribbon Drive 30.0' Lt.

0152 & 2' Conc. Walk 29.3' Lt.

0150

38.48

&

57

33 ⁹	33 ⁵	33 ⁵	33 ³	33 ⁷	33 ⁴	34 ⁴	34 ⁸	35 ⁴
50	30	21	13		13	22	30	50
			Pay		Pay			

33 ^{7.5}	34 ^{9.5}	35 ^{1.5}
16.5	30	50

33 ^{8.0}	33 ^{7.3}
39	30

42.23	33 ^{7.6}	38
	30.2	

S.W. 13' Lot Newton & 35th St.

32 ⁷	33 ⁵	32 ⁸	33 ¹	32 ⁸	33 ⁵	34 ³	34 ⁶
50	30	13		13	21	30	42
		Pay		Pay			

33 ^{6.6}	34 ^{0.9}
30	39

32 ^{3.5}	32 ^{5.2}
41	29.3

32 ²	32 ²	32 ³	32 ⁰	32 ⁴	32 ¹	33 ¹	33 ⁵	33 ⁸
40	30	17	13		13	18	30	39
			Pay		Pay			

38.48

2199.48 So. Line Newton

2+54 R 5' Conc. Walk 31.4 L

2150

2+31 R 1.5' Conc. Walk on Lt. 32.5

2+08 R 3' Conc. Walk on Lt. 34.4'

2+00

1+86 R 4' Conc. Stairway on Lt. 288'

1+59.72 No Line Alley

4223
1

33 ⁶⁸	33 ⁵⁰	33 ¹⁰	33 ⁸⁸	34 ⁰⁶	34 ²⁰	34 ⁸⁰
277	208	208		210	210	208
Sw.	Cl	G		G	Cl	Sw.

35²² 35²²
30' 31.4

35 ²¹	35 ²¹	35 ⁵	35 ⁷	34 ³	34 ⁵	34 ⁷	36 ⁸	36 ⁸	37 ¹
36	32	20	15	13		12	22	20	50
				Pay		Pay			

35⁴⁷ 35⁶²
37 31.9

35⁰¹ 35⁰¹
43 34.4

34 ⁹	34 ⁸	34 ⁷	33 ⁹	34 ⁴	34 ⁴	35 ⁶	36 ²	36 ⁰
35	30	18	13		13	19	30	50
			Pay		Pay			

35⁰⁵
288
Top 1st Riser

34 ²	34 ¹	32 ⁴	33 ⁹	33 ⁷	34 ¹	34 ⁸	35 ⁸
50	30	13		13	27	30	50
		Pay		Pay			

4223
1

55th Cont'd) 13.30 37.12 36.98
 TP 4.83 50.42 0.45 45.59
 BMT 1.24 44.80 44.19
 T.P. 7.29 46.04 3.48 38.75

SE Cb Ret. Newton E 35th. L = 148' 2 parts
 BC on 35th

SW Cb Ret Newton G 35th. L = 26' 2 parts
 BC on 35th

3+85.45

2+85.45 EC Cb Ret

2+72

2+65.45 No Cb. Line Newton

2+39.45 E Newton

3+13.45 So. Cb. Line Newton

42.23

(SE BP Nat'l E 36th)
 SE Top F. Hydt National E 35th

59

34⁰⁶ 34⁷⁰ 34²¹ 34⁷⁶ 34³¹ 34⁹⁸
 G Cb G Cb G Cb
 BC (C) EC

33⁵⁶ 33¹⁹ 33⁰³ 33⁶⁴ 32⁹³ 33⁴⁷ 32⁶⁷ 33²⁸
 G Cb G Cb G Cb G Cb
 BC (C) (C) EC

36⁴¹ 35⁹⁷ 37¹⁹ 37⁰⁶ 37⁶⁰
 20 20 20 20
 Cb G G Cb

34²⁵ 33⁷⁰ 34²⁷ 34⁶⁸ 35²⁹
 20 20 20 20
 Cb G G Cb

33⁶⁸ 34³¹ 34⁵⁸
 20 20

32²¹ 32¹⁹
 33⁷³ 33¹⁵ 33⁷⁴ 34³⁵ 34⁶⁴ 34²² 35⁵ 38²
 Cb. G 40 40 20 20 30 50 100
 G Cb G

32⁵⁰ 33⁴⁷ 33⁹⁸ 34³⁷ 34⁷⁴ 34⁹⁶ 35⁶ 38⁰
 73 40 20 20 30 50 100

32⁴⁶ 32⁷⁶ 33²⁸ 32⁴⁷ 33³⁸ 33⁹² 34²⁴ 34³⁴ 35⁹ 38³
 G 40 40 20 20 30 50 100
 Cb. G Cb G

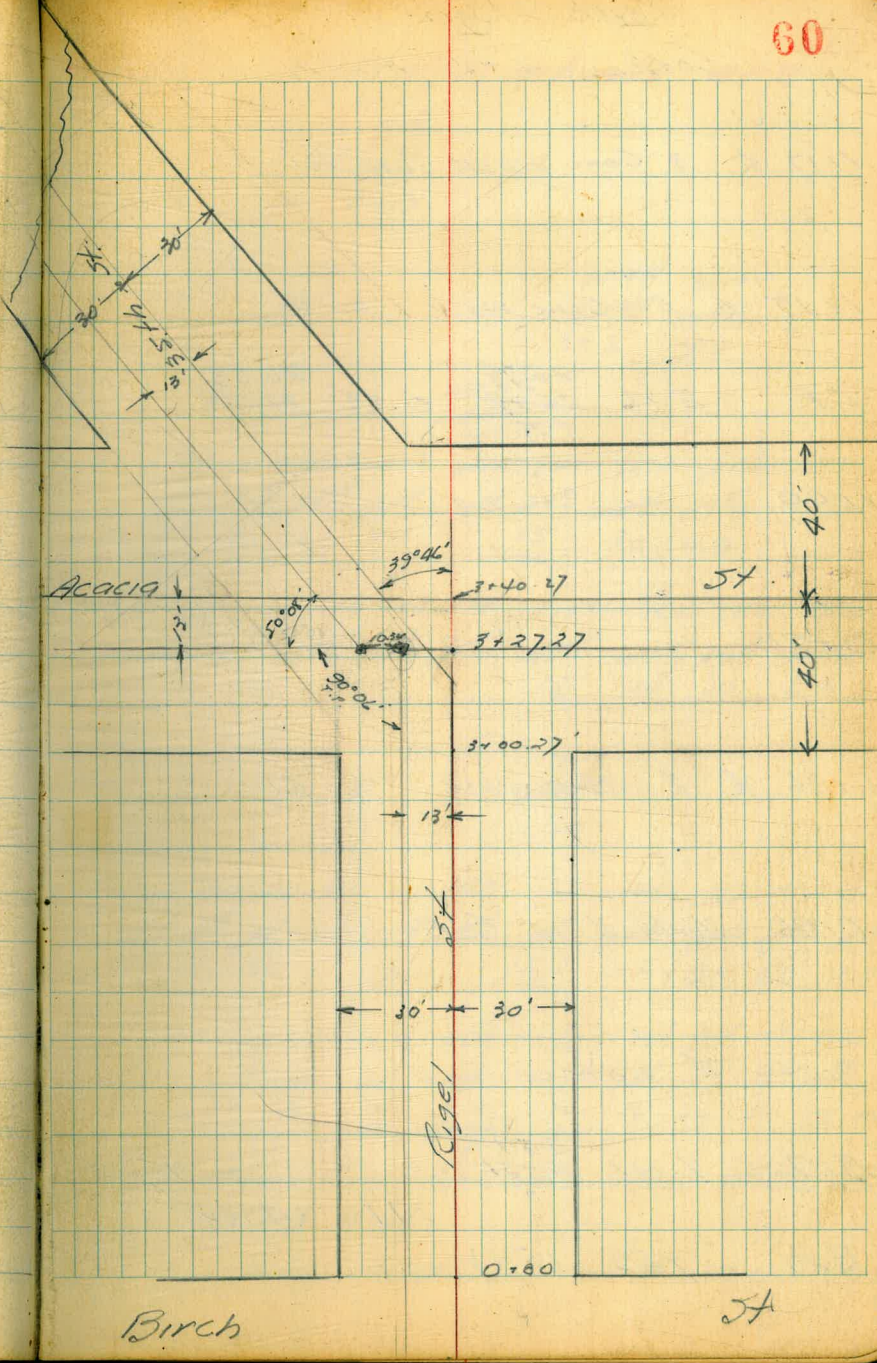
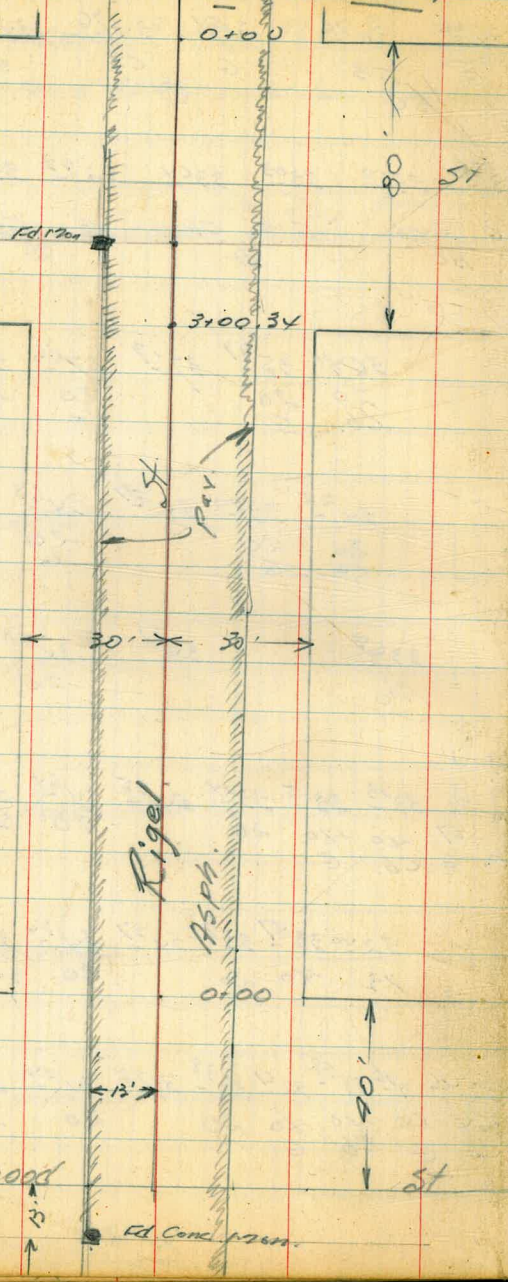
42.23

S.S. 50
Hendricks
Johnson
Greer
McCoy
W.O.P. 5020

X Sect. Rigel
Cotton wood to Acacia

Birch

INDEXED
MAY 9 1950



Levels Rigel St
Cottonwood to Beach

1417 & 3' Conc Walk on Lt

1415 & 3' Conc Walk on Lt

T.P. 5.16 $\frac{28.79}{\cancel{26.79}}$ 0.88 $\frac{20.63}{\cancel{21.63}}$

1100

0+50

0+26 & 2' Conc Walk 30' Lt

0+00 North Line Cottonwood

0+20 & Cottonwood

B.M. 7.41 $\frac{21.51}{\cancel{22.21}}$ 1.71 14.10 \swarrow 15.10 \nwarrow

B.M. 9.53 15.81 6.28

Note: All Elevations are
1' too high.

$\frac{22.34}{\cancel{22.21}}$
X0 20.3

$\frac{20.44}{\cancel{21.44}}$ 20.44
30.5 X3

$\frac{25.79}{\cancel{26.79}}$

21.9 20.9 20.8 20.4 20.4 20.0 20.4 20.2
~~21.9~~ ~~21.9~~ ~~21.9~~ ~~21.9~~ ~~21.9~~ ~~21.9~~ ~~21.9~~ ~~21.9~~
50 30 17 14 15 30 40
Pav

19.6 19.6 19.6 18.8 19.2 18.9 19.6 19.6 19.4
~~20.6~~ ~~20.6~~ ~~20.6~~ ~~20.6~~ ~~20.6~~ ~~20.6~~ ~~20.6~~ ~~20.6~~
50 30 16 13 15 22 30 50
Pav

$\frac{19.20}{\cancel{20.20}}$
30

14.9 16.7 17.1 17.3 16.7 17.4 17.2 18.4 18.6 18.2 15.2
~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~ ~~15.9~~
82 50 30 17 13 15.5 21 30 50 100
Pav Pav

14.2 13.4 14.4 15.2 15.9 15.6 15.5 16.8 17.1 16.2 14.4
~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~ ~~12.2~~
100 50 30 14 16 16 18 30 50 75 100
Pav Pav

SW 13' 170m Rigel & Cottonwood (FB 1182-6)
(Bench is 1' High)

(Chisel 1/2 inch 50.00 line 170m St. Vt. line Rigel)

Levels Rigel St. Cont'd.

1+60.13 No line Alley

1+40.13 50 line Alley

T.P. 11.09 $\frac{32.89}{}$ 3.39 21.80
1+00

0+75 & 13' Conc. Drive 16 on Lt.

0+50

0+00
3+80.34 = No. line Birch

3+65

3+57

~~26.19~~
25.19

24.2	23.7	23.3	24.1	24.0	23.8	23.3
25.2	25.2	24.3	25.1	25.0	24.8	24.3
50	30	15		17	30	50
		Pay.		Pay.		

24.0	23.7	23.6	22.6	23.4	23.2	22.9	22.6
25.0	24.7	24.6	23.6	24.4	24.2	23.9	23.6
50	30	23	15		16	30	50
		Pay.		Pay.			

22.9	22.3	21.7	20.7	21.8	32.89		
23.9	23.3	22.7	21.7	20.8	21.8	21.0	21.0
50	30	19	15		16	30	50
		Pay.		Pay.			

22.30	21.53	20.35
23.30	22.53	21.35
50	22	16
		Pay.

20.3	21.1	20.7	19.5	20.2	19.8	20.4	20.2
21.3	22.1	21.7	20.5	21.2	20.8	21.4	21.2
50	30	22	15		16	30	50
		Pay.		Pay.			

22.1	21.3	20.7	20.3	19.2	18.7	19.0	18.2	19.0	20.1	18.7
23.1	22.3	21.7	21.3	20.2	19.7	20.0	19.2	20.0	21.1	19.7
100	80	50	30	20	14		15	30	50	100
				Pay.		Pay.				

21.2	22.2	20.8	20.1	18.6	18.7		18.0	16.9	16.8	16.9
22.2	23.2	21.8	21.1	19.6	19.7		19.0	17.9	17.8	17.9
100	80	50	30	14			16	30	50	100
				Pay.			Pay.			

20.4	20.3	19.4	18.8	18.6	18.6	18.0	17.2	16.2	15.2
21.4	21.3	20.4	19.8	19.6	19.6	19.0	18.2	17.2	16.2
100	80	50	30	14		14	30	50	100
				Pay.		Pay.			

~~26.19~~
25.19

B.M. 2.09 ^{30.80}
~~31.80~~ 30.75

3+40.27 & Acacia

3+00.27 So. Line Acacia

2+72 & 2.5' Conc. Walk on Rf.

2+50

2+00

3289
~~3389~~
^

SW 1/2 Mon Boston & 35th (P. 56)

27.8	28.2	28.4	29.0	29.0	28.3	27.8	27.8
28.8	29.2	29.2	30.0	30.0	29.2	28.8	28.8
100	50	37	17		30	50	100
			fav				

27.8	28.2	28.2	28.3	27.0	28.0	28.0	27.8	26.7	26.3
28.8	29.2	29.2	29.2	28.0	29.0	29.0	28.8	27.2	27.2
100	50	30	21	16		16	30	50	100
				fav		fav			

27.90	27.96
28.90	28.96
29.8	38

26.7	29.0	27.2	26.1	26.6	27.2	27.3	26.7
27.7	28.0	28.2	27.1	27.6	28.2	28.0	27.7
50	30	17	12		17	30	50
			fav		fav		

25.4	25.8	26.0	25.4	25.4	25.8	26.0	25.0
26.0	26.0	26.0	26.0	26.0	26.0	26.0	26.0
50	30	17	14		17	23	30
			fav		fav		

3289
~~3389~~
^

PARKER Place

Events to Farnel.

2-sec. for grade

W.D.
25020

Sommermeier

Begg
Allet

6-30-50

■ = Fd. Conc. Mon

● = Fd. L+T.

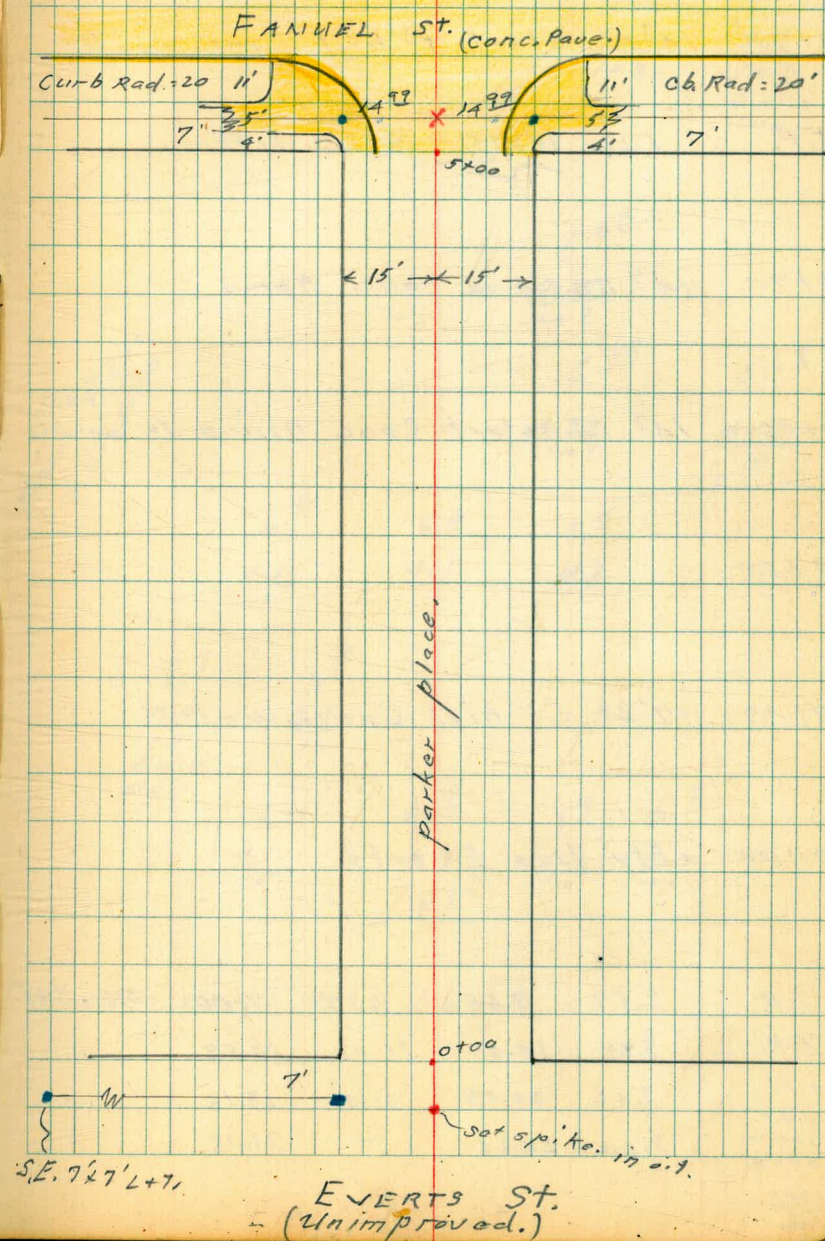
✕ = cut cross in conc.

• = set Nail

Parker Place has remains of
a thin oil coat. Now is no good so
is not noted in level notes or sketch.

INDEXED

VIX
JUL 3 1950



Parker Place

0+70^L 14² Rt. = start 5' high Conc. wall

T.P. 5.12 10.95 3.82 5.83

0+70 14² Rt. = end Conc. Apron

0+56 1A² Mt. = start Conc. Drive to double Gar.

0+50

0+49 17' Lt. = 5' high Conc. wall.

0+00 = Ely. Nine Everts.

T.P. 2.59 9.65 7.37 7.06 S.E. Lt.

T.P. 3.85 14.43 10.00 10.58

T.P. 2.42 20.58 6.10 18.16

N.W. B.P. Oliver & Farnel 3.24 24.26 — 21.02

1803
42

4

66

5.7
5.3
14.8
5.1
5.9
14.9
Base of wall

10.95

5.40
4.25
14.2
5.33 5.13

4.32
14.9
4.52
30
Gar. floor

6.4 5.4 5.5
3.3 4.3 4.2
15 15

5.7 6.4
4.0 3.3
17.5 17
Base wall

5.2 4.8 3.7 5.3
4.5 4.9 6.0 4.4
15 10 15

Reduced 7/3/60
S. Barnett

Pacific Beach Dr. + Everts

T.P. 5.78 13.45 3.28 7.67

2+00 15' Rt. end 6' high conc wall

1+50

1+24 16' Lt. = 2' wide conc. walk
14' Lt. = 3' wide conc. step

1+22 15' Rt. = start 6' high conc. wall.

1+14 65' Rt. = double bar.

1+07 14³ Rt. = end wall

also = start 6' high conc. wall
14² Lt. = end 5' high conc. wall
17² Lt. = end conc. wall

1+00

67

7.6	7.4	7.2	6.3
<u>3.4</u>	3.6	<u>3.8</u>	<u>4.7</u>
15		15	15
			Base of wall

7.0	6.7	6.7
<u>4.0</u>	4.3	<u>4.3</u>
15		15

7.11	6.91	6.6
<u>3.84</u>	<u>4.04</u>	<u>4.4</u>
16	14	14
walk	top of	end
	step	

6.1	5.4
<u>4.9</u>	<u>5.6</u>
15	15
	Base of wall

5.0
<u>6.0</u>
65
Bar Floor

6.2	5.6
<u>4.8</u>	<u>5.4</u>
14 ²	14 ²
	Base wall

6.1	7.0	6.8	6.2	6.1	5.2
<u>4.9</u>	<u>4.0</u>	<u>4.2</u>	4.8	<u>4.9</u>	<u>5.8</u>
17 ²	17	15		14 ²	14 ²
Base of wall					Base of walls

10.95

£
Nail 4+50

T.P. 4.74 16.55 1.64 11.81

4+00

3+50

3+00

2+75 15' RT. = end Conc. apron

40' RT. = Gar.

2+59 15' RT. = start Conc. Apron

2+50 15' RT. = end Conc.

2+46 15' RT. = 2' wide Conc. drive ribbon

65' RT. = Gar.

2+41.5 15' RT. = 2' wide Conc. Dr. ribbon

£

08

11.5

10.7

10.7

2.0
15

2.8

2.8
15

10.3

9.8

9.7

3.2
15

3.7

3.8
15

9.4

8.9

8.9

4.1
15

4.6

4.6
15

8.32

5.13
152
Apron

8.09

8.13

5.36
154
Apron

5.32
40

Gar. floor

9.0

8.3

8.3

4.5
15

5.2

5.2
15

8.34

5.11
15
drive

8.8

7.61

5.27
15
Drive

5.84
65

Gar. floor

13.45

N.W. B.R. Pac. B. Dr
 + Fannuel 3.28 21.19 (21.19)
 T.P. 6.18 24.47 4.68 18.29
 T.P. 7.98 22.97 0.60 14.99 S.E. Lt.
 Fannuel +
 Pac. B. Dr.
 5+40 = ~~4~~ Fannuel

5+20 Cont

5+20 = Wly. cl. line Fannuel

5+13² - $\left. \begin{matrix} 15' AB \\ 15' LT \end{matrix} \right\} = \text{Face of cl. (on Return)}$

T.P. 4.72 15.59 5.68 10.87 = N.W. 7¹/₄ Prop. Lt. Fannuel + Parker

$\left. \begin{matrix} 10' Lt. \\ 9' Rt. \end{matrix} \right\} = \text{B.C. 20' Rad. Curb Ret. start Conc. curb + 5' walk.}$

5+00 = Wly. line Fannuel = start Conc. Pavc

4+50 40' Lt. = S.Wly. Cor. Sing Car. Conc. floor

12.57 11.37 10.64 9.92 8.69
 $\frac{3.02}{80}$ $\frac{4.22}{30}$ 4.95 $\frac{5.67}{30}$ $\frac{6.90}{80}$

12.39 11.54 9.88 8.12 8.74
 $\frac{2.20}{80}$ $\frac{3.75}{80}$ $\frac{5.71}{30}$ $\frac{7.47}{80}$ $\frac{6.85}{80}$
 cl. G cl. G cl.

11.19 10.57 10.21 10.11 9.86 9.63 9.50 9.24
 $\frac{4.40}{30}$ $\frac{5.02}{30}$ $\frac{5.38}{15}$ $\frac{5.48}{10}$ 5.73 $\frac{5.90}{10}$ $\frac{6.09}{15}$ $\frac{6.35}{30}$
 cl. G cl. G cl.

10.86 10.32 9.61 10.14
 $\frac{4.73}{15}$ $\frac{5.27}{15}$ $\frac{5.98}{15}$ $\frac{5.45}{15}$
 cl. G cl. G cl.

10.78 10.71 10.18 10.09 9.70
 10.20 10.22
 $\frac{5.77}{15}$ $\frac{5.84}{10}$ $\frac{6.37}{10}$ 6.46 $\frac{6.85}{9}$ $\frac{6.35}{9}$ $\frac{6.33}{15}$
 Back edge of walk cl. G cl. G cl. Back edge walk

14.15 12.6 11.9 11.4
 $\frac{2.50}{40}$ $\frac{4.0}{15}$ 4.7 $\frac{5.2}{15}$
 Cor. Floor.

16.35

Mendocino

11-July 1951
W.P. 25020

Sommermeier
Begg
R Sissell
Oltman

FB 1862 - P43
T.P. 13 - P. 40

F.B. $\frac{2235}{2}$ for Alley, Bk. 12

(W) = Water meter box. rods on top
of meter. Service pipe is 0.9' lower.

240

70

INDEXED

JUL 16 1951

1469.72

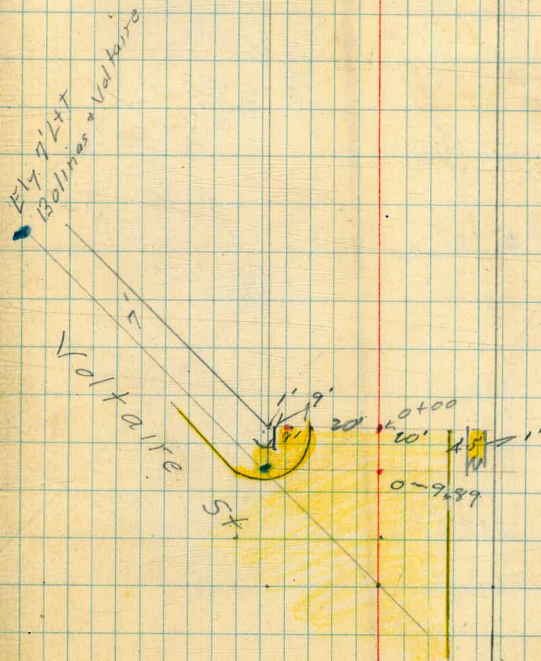
1459.12

1448.51

Alley Bk 12
Lotta Alley

KEY POINT
Bellmer + Voltaire

Voltaire St.



0+78 30⁸ Rt. = ϕ 2⁵ wide Conc. walk

0+75. 31³ Rt. = 10" Diam Cypress

0+50

0+44 30⁵ Rt. = end picket fence.
also start rail fence.

0+40 - 30⁶ Rt. = ϕ 3' wide conc. steps.

0+17 29' Rt. = start picket fence

0+3

0+2 } 22' Rt. = \textcircled{W}

0+1

0+00 Cont.

0+00 = End. existing c/c + pave

1.22 79.25 11.60 78.03 B.M.#1
3.13 89.63 - 86.50

2.2	3.5	4.3	7.9	8.5	8.4	7.5	7.7	12.7
40	30	21	20	15	23	30	50	
79.74	75.8	75.0	71.4	70.8	69.24	69.24	69.24	69.24
					9.53	9.53	9.53	9.53
					30.5	30.5	30.5	30.5

Reduced & Plotted

7.20	11.93
30.5	40
on steps	

4.0	3.9	1.0	3.9
30.5	30.5	30.5	30.5

1.0	1.22	3.95	3.9	3.9	15.9
30	29	N.E. cor	30	39	42
N.W. cor. Conc. walk					

1.94	2.40	2.53	2.90	3.50	4.45	3.98	3.98
20	20	10	10	10	20	20	24
26	6				0	0	N.W. cor
79.25							
Conc. walk							

L+T. 23' Lt of Sta 0 - 989 P. 70

N.W. R.P. Valtaira & Bolinas

Mendocino

	3.59	68.19	3.59	64.60	T.P.#3 P73
	1.79	68.19	13.07	66.40	T.P.#2 P73
	1.145	79.47	11.12	78.02	78.03 B.M. P 72
Check levels	2.64	89.14		86.50	Correct Elev. orig. B.M.
Orig. B.M.			3.74	86.32	} (86.50)
T.P.	10.38	90.06	1.55	79.68	
T.P.	9.92	81.23	0.55	71.41	

30' Rt. = Monument
= Pline to east.

5+95 99 = \pm Green to west

5+92 26 Rt. = Ctr. leadman

5+74 25 Rt. = Ctr pole # 2275

5+65 99 30' Lt. = end Conc. wall.
Sly line Green to west

5+62 299 Lt. = start Conc. wall.

5+62 299 Lt. = end Gar.
279 Lt. = end Conc. apart + Gar.

5+59 30' Lt. = \pm 3rd Gar. door.
365 Rt. = end double Gar.

(64.60)

(66.41) on rock

\pm Elev. shown in previous notes are o.k.
0.19 off correct Elev. See check above.

546	549	576	559	554	575	606
2.6	4.3	4.6	6.3	6.8	4.76	11.6
80	30		20	30	30	80
					Mon.	

210	5.6	4.5	5.8	5.8	6.7	7.4	7.9
30	30	30	11		27	30	40
T.W.	B.W.						

1.79	5.5	4.7
299	299	299
T.W.	B.W.	

4.76	4.81	5.7	5.9	6.5	7.2	8.3
299	273	12		24	30	40

4.80
30
Gar. pole

72.15

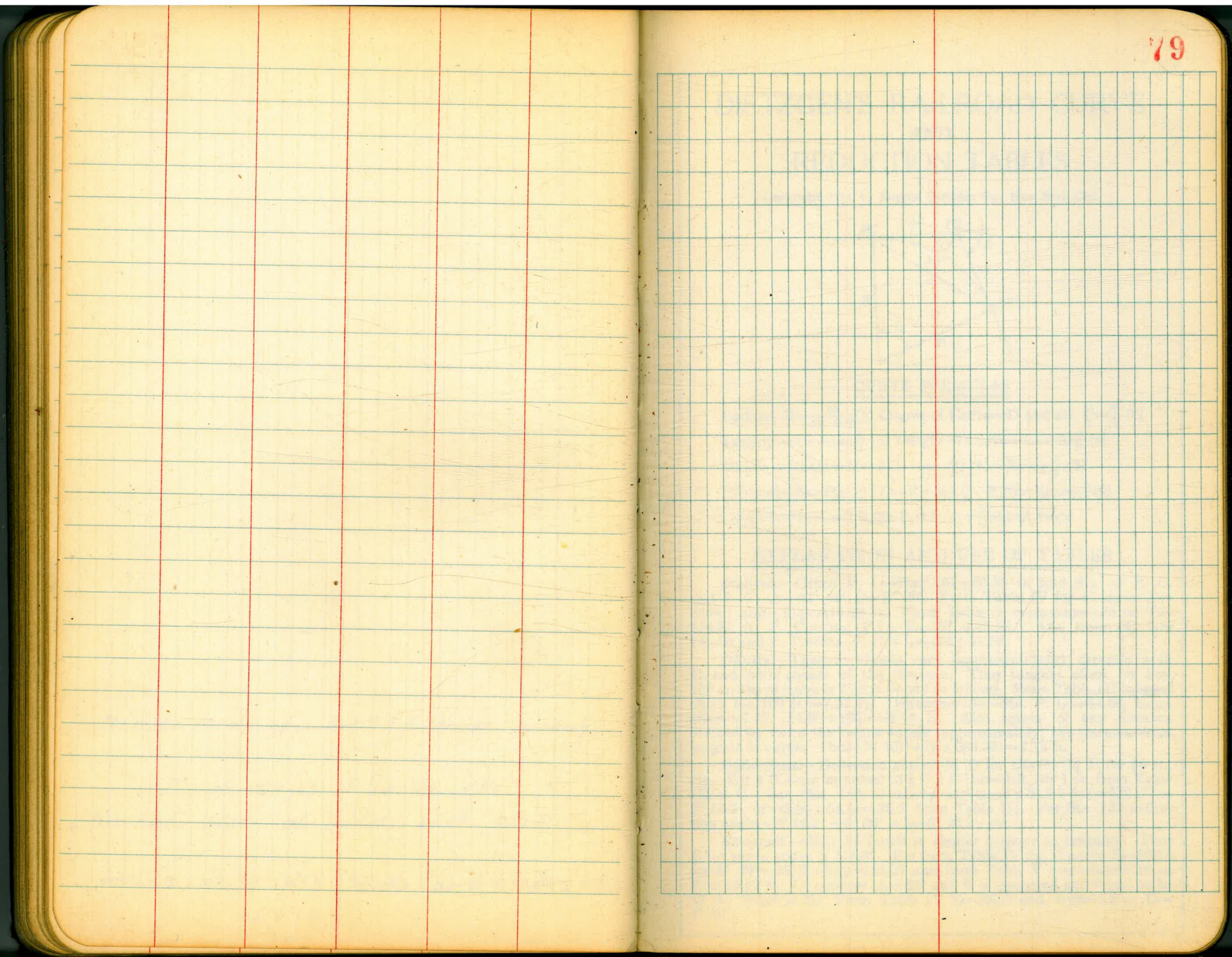
Mirius rod of 6.65 (P.7A) is wrong

π of 69.43 P7A is a.k.

Checked circ. cl. inlet 2+1A P.7A

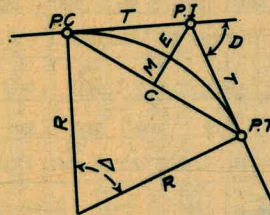
5122 62.97 T.P. #1 P7A
68.19

cl
orig R47 shows 62.78 this is in error



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve— D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve— $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$ (6)
- External— $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ —Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given $P. I. = \text{Sta. } 161 + 60.35$ to find $\text{Sta. of } P. C.$ and $P. T.$ $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8 \frac{1}{2} = 414.49$ ft. From Table V correction $= .36$ or $T = 414.85$ ft. $P. C. = \text{Sta. } P. I. - T = 157 + 45.50$. Also from (4) $L = 746.00$ and $P. T. = \text{Sta. } P. C. + L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for $\text{Sta. } 158$ on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. $= 7.27$ ft. Distance $= 158 - \text{Sta. } P. C. = 54.50$, hence offset $= 7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle $= \frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. $= (\text{in minutes}) .3 \times C \times D^\circ$ or $= \text{defl. for } 1 \text{ ft. from Table III} \times C$. For $\text{Sta. } 158$ of above curve $= .3 \times 54.5 \times 8 \frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For $\text{Sta. } 159$ deflection angle $= 2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37 . For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8 \frac{1}{2} = 115.27$ and from Table V correction $= .10$ or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

65 H-10

60
00
- 06

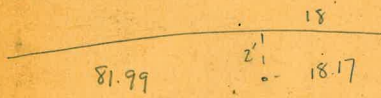
$\frac{2+99 \times 5}{1+9972 \text{ LANCY}}$

48

85.6 = Pole

56
283

9.2
2+8344
130
1390
10-23
283-8
769
1880



8+32 = POT Hub

13+00 = POT Hub

15+76.22 = POT Hub - Top of Hill

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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