

1843



ENGINEERS'
LEVEL BOOK

No. 410F

1843

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

CITY ENGINEER'S OFFICE

INDEXED
completely

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \times 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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Mission Valley Sewer profile 1-59

" " Fairmount 60

X-SEC + River road

INDEVED

WK

JUN 8 1949

INVERT
G.

Ar.O.Y. Exc.

/100: C.Y.

1

1+60 8.5 73.3 71.59

1+20 M.H.#69 33°07'-3044 10.3 71.5 71.05

0+90 7.6 74.2 70.57

0+84 End pav. 77

+65 pav. High crown on 59

0+60 7.0 74.8 70.07

+468 Edge pav 7.6

0+30 7.9 73.9 69.61

0+23 12.5

+15 9.7

0+00 M.H.#68 10.2 71.6 69.10

81.49 86.77 73.28

374.50 FROM F.B. 1809 - P. 75

BM: □ out west end south head wall Culvert under Camino Del Rio 1519 1203 20 43

Cut ArCut Dist /100: C.Y.

1.71

1.8 40 19.0 7.60

0.45

End of 15" Conc. Encaso.

2.04 30 27.6 8.28

3.63

4.17 25 50.0 12.50

4.71

4.50 30 53.8 16.14

4.29

3.40 30 42.5 12.75

7.5

57.27

Start of 15" Conc. Enc To 1+20

Dist	Rdg. Back 100	Rdg. Back 0.4
------	---------------------	---------------------

40	2.0	0.80
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30	3.79	0.99
----	------	------

25	25.0	6.25
----	------	------

30	28.8	8.64
----	------	------

30

30	17.5	5.75
----	------	------

21.93

5000

IN Vert.

4+40 4.0 77.8 75.34

4+00 4.6 77.2 74.80

3+60 5.5 76.3 74.27

3+20 6.2 75.6 73.73

2+80 7.1 74.7 73.19

2+40 7.8 74.0 72.56

2+00 7.8 74.0 72.12

81.77

1+60

Av. C.Y. Etc.

3

Cut Av. Cut Dist. /100' C.Y.

2.46

2.43 40 26.6 10.64

2.40

2.22 40 24.6 9.84

2.03

1.95 40 21.5 8.60

1.87

1.69 40 19.0 7.60

1.51

1.42 40 16.0 6.40

1.34

1.61 40 18.0 7.20

1.88

1.79 40 20.0 8.00

1.71

58.28

Dist.	Req. Back 100'	Req. Back C.V
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40	20.0	8.0
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40	17.0	6.8
----	------	-----

40	14.0	5.6
----	------	-----

40	14.0	4.8
----	------	-----

40	9.0	3.6
----	-----	-----

40	11.0	4.4
----	------	-----

40	13.0	5.2
----	------	-----

38.4

INVERT

7+00 4.9 85.0 72.08

6+60 5.5 84.4 78.38

F.P.
 10.06 Lt. of 5.08 89.88 5.08 84.80
 H.H. 470
 6+38⁵² 9'32" RT. 6.1 83.8 78.00

6+00 7.3 82.6 77.48

5+60 10.5 79.4 76.78

5+20 11.5 78.4 76.41

11.78 89.88 3.67 78.10

4+80 3.9 77.9 75.81

81.77

4+40

Avdy. Exc. 5
 Cut Ar. Out Dist 100' C.Y.

5.92

5.99 40 64.0 25.60

6.02

5.91 21.46 63.2 13.56

5.80

5.46 38.54 58.6 22.60

5.12

3.88 40 42.0 16.80

2.45

2.42 40 24.5 9.80

1.99

2.01 40 22.2 8.88

2.03

2.50 40 27.4 10.96

2.46

108.20

Dist	Ran, Back 100'	Ran, Back e.y.
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40	58.4	23.36
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21.46	56.8	12.19
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38.54	52.0	20.04
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40	35.6	14.24
----	------	-------

40	17.0	6.80
----	------	------

40	16.0	6.40
----	------	------

40	21.0	8.40
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		<hr/> 91.43
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						Cvt	Ar.Cvt	Dist	100'	C.Y.	Exc	7
9+80		9.1	90.1	84.01	6.09							
	9.66	<u>99.19</u>	0.35	89.53								
							6.14	40	65.4	26.16		
9+40		0.4	89.5	83.31	6.19							
							6.09	40	65.0	26.00		
9+00		1.3	88.6	82.60	6.00							
							6.05	40	64.5	25.80		
8+60		1.9	88.0	81.90	6.10							
							6.05	40	64.5	25.80		
8+20		2.7	87.2	81.19	6.01							
							5.61	40	60.0	24.00		
7+80		3.2	86.7	80.49	5.21							
								40	60.0	24.00		
							5.61					
7+40		4.1	85.8	79.79	6.01							
		<u>79.88</u>					5.96	40	63.6	25.44		
7+00					5.92					<u>177.20</u>		

Dist. Req. Back Req. Back
1100' 0.7

40 59.2 23.68

40 58.8 23.52

40 58.4 23.36

40 58.4 23.36

40 53.5 21.40

40 53.5 21.40

40 58.3 23.32

160.04

12+40		4.8	94.4	88.59
12+00		5.4	93.8	87.88
11+60		6.3	92.9	87.18
11+20		7.0	92.2	86.47
Nail 20' Lt. ↓		6.15	93.04	
10+80	P.O.T. M.H. 71	7.5	91.7	85.77
10+50		8.2	91.0	85.24
10+20		8.6	90.6	84.71
		<u>99.19</u>		
9+80				

Out	Ar. Out	Dist	Av. V. / 1000	Exc. C.V.
5.81				
5.86	40	62.5	25.00	
5.92				
5.82	40	62.2	24.88	
5.72				
5.72	40	61.2	24.48	
5.73				
5.83	40	62.3	24.92	
5.93				
5.84	30	62.4	18.72	
5.76				
5.83	30	62.3	18.69	
5.89				
5.99	40	64.0	25.60	
6.09				
			<u>162.29</u>	

Dist.	Req. Back	Req. Back
	1100'	C.Y.

40	56.0	vr. 40
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40	55.6	vr. 24
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40	54.8	21.92
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40	55.8	22.32
----	------	-------

30	56.2	16.86
----	------	-------

30	55.8	16.74
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40	57.6	23.04
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		<u>145.52</u>
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14+80 9.4 100.1 92.81

T.P. 10.68 109.47 0.40 98.79

14+40 0.1 99.1 92.11

14+00 1.1 98.1 91.40

13+60 1.9 97.3 90.70

13+20 3.0 96.2 89.99

12+80 4.0 95.2 89.29

12+40

99.19

Cut	Av. Cut	Dist.	Av. C.Y. / 100'	Exc. C.Y.	"
			7.29		
			7.14	40	76.2 30.48
			6.99		
			6.84	40	73.0 29.20
			6.70		
			6.65	40	71.0 28.40
			6.60		
			6.40	40	68.2 27.28
			6.21		
			6.06	40	64.8 25.92
			5.91		
			5.86	40	62.6 25.04
			5.81		<u>166.32</u>

Dist	Req. Back 100'	Req. Back e.v.
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40	69.6	27.84
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40	66.5	26.60
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40	64.5	25.80
----	------	-------

40	62.0	24.80
----	------	-------

40	58.4	23.36
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40	56.0	22.40
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150.80

Cut	Ai.Cut	Dist.	C.Y.	Exc	C.Y.
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17+20	5.7	103.8	97.30		
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6.50					
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16+80	6.4	103.1	96.54		
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6.56					
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6.53	40	70.0	28.00		
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16+40	7.5	102.0	95.78		
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6.39					
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6.39	40	68.2	27.28		
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16+00	7.6	101.9	95.02		
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6.55					
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6.55	40	70.0	28.00		
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15+60	7.8	101.7	94.26		
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6.88					
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7.16	40	76.2	30.48		
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20' Lt. Nail
 Δ 4" 01'-30 Rt.
 MH # 72

15+26 ⁷⁹	7.64	101.83			
	8.4	101.1	93.63		

7.46					
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7.46	33.21	79.5	26.40		
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14+80
 109.47

7.47					
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7.38	46.79	78.8	36.84		
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177.00					
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Dist	Req. Back 100'	Req. Back C.Y.
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40	63.7	25.28
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40	61.8	24.72
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40	63.4	25.36
----	------	-------

40	69.6	27.84
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33.21	73.0	24.24
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46.79	73.0	33.69
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	161.13	
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19+20 10.1 106.3 101.16

T.P. Nail 9.25 117.39 1.33 108.14
20¹ L⁴ of

18+98⁴⁸ A 110 32 RT. M.H.# 73 2.3 107.2 100.69

18+80 2.6 106.9 100.34

18+40 3.4 106.1 99.58

18+00 4.2 105.3 98.82

17+60 4.9 104.6 98.06

17+20 109.47

15
Av. Av. @ Y. Exc.
Cut Cut Dist. 100. C.Y.

5.14

5.32 21.52 57.0 12.26

6.51

6.53 18.48 69.8 13.10

6.56

6.54 40 69.8 27.92

6.52

6.50 40 69.5 27.80

6.48

6.51 40 69.6 27.84

6.54

6.52 40 69.7 27.88

6.50

136.80

Req. Req.
Back Back
Dist 100' C.Y

21.52 50.4 10.85

18.48 63.3 11.70

40 63.4 25.36

40 63.0 25.20

40 63.1 25.24

40 63.7 25.28

123.63

Req. Req.
Back Back
Dist 1100' e.y.

40 57.4 22.96

40 57.7 23.08

40 54.6 21.84

40 53.7 21.28

40 54.0 21.60

40 52.0 20.80

131.56

Alt. 20' Lt
of

7.32 118.35

Δ 1°-17'-30" Rt.
M.H. 4 7A

24+00 7.7 117.8 116.72

23+60 8.4 117.3 110.84

23+20 9.0 116.7 109.96

T.P. 9.50 125.67 1.22 116.17

22+80 2.0 115.4 109.08

22+40 3.7 113.7 108.20

22+00 4.5 112.9 107.32

21+60 117.37

Av. C.Y. Exc.

17

Cut. Av. Cut Dist. /100' C.Y.

6.08

6.27 40 67.0 26.80

6.46

6.60 40 70.5 28.20

6.74

6.53 40 68.6 27.44

6.32

5.91 40 63.2 25.28

5.50

5.54 40 59.0 23.60

5.58

5.67 40 60.7 24.28

5.76

155.60

Dist	Req. Back 1100'	Req. Back C.Y
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40	60.5	24.20
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40	64.0	25.60
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40	63.4	25.36
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40	57.8	23.12
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40	53.0	21.20
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40	54.0	21.60
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141.08

Invert

Av. Q.Y. Exc.

21

Cut Av. Cut Dist 100. C.Y.

26+40 3.1 122.6 115.80

6.80

6.84 40 72.8 29.12

26+00 3.7 122.0 115.12

6.88

6.87 40 73.2 29.28

25+60 4.4 121.3 114.44

6.86

6.55 40 70.0 28.00

25+20 5.7 120.0 113.76

6.24

6.38 40 68.0 27.20

24+80 6.1 119.6 113.08

6.52

6.31 40 67.2 26.88

24+40 7.2 118.5 112.40

6.10

6.09 40 65.0 26.00

24+00 125.67

6.08

166.48

	Req. Back	Req. Back
Dist	1100'	@.Y.

40	66.4	26.56
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40	66.7	26.68
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40	63.5	25.40
----	------	-------

40	61.6	24.64
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40	61.0	24.40
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40	58.8	23.52
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		151.20
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28+60 7.4 129.8 119.48

Take off B.M.

As shown. 8.21 137.20

Chisel

N. W. wing wall culvert.

Measurement

Fair mount

128.99

8.21 129.07 (128.99)

= 28+41.91 $\Delta 51^\circ - 15' 30''$ Lt.

28+39.02 M.H. #75 8.0 129.3 119.18

Cut Ar.Cut Dist. 100' C.Y. Exc C.Y.

23

10.32

10.22 18.09 101.0 18.27

Start of 12" ETC.

10.12

End of 15"

28+00 9.7 127.6 118.52

9.08 9.60 39.02 102.0 39.80

27+60 11.1 126.2 117.84

8.36 8.72 40 93.0 37.20

8.45 40 90.0 36.00

27+20 11.6 125.7 117.16

8.52 1

T.P. 12.62 137.28 1.01 124.66

8.53 40 90.8 36.32

26+80 1.7 124.0 116.48

8.52

7.66 40 81.6 32.64

26+40 125.67

6.80

200.23

Req. Req.
Back Back
Dist 1100' 0.7

18.09 82.0 14.83

Start of 12" Encl

End. of 15"

39.07 96.4 37.58

40 86.4 34.56

40 83.5 33.40

40 84.5 33.80

40 75.0 30.00

184.17

31+00	9.9	127.3	125.98 123.50
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30+60	9.6	127.6	125.38 122.93
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30+20	6.0	131.2	124.78 121.76
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29+80	7.1	130.1	124.18 121.99
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29+40	5.7	131.5	123.58 120.32
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29+05			123.05
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29+00	6.4	130.8	120.15
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28+60	137.20		
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25

Cvt.	Ar.Cvt	Dist	Ar.C.Y.	Exc	C.Y.
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1.32

1.77	40	17.4	6.96
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2.22

4.32	40	41.0	16.40
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6.42

6.17	40	58.6	23.44
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5.92

6.92	40	65.2	26.08
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7.92

Start of 12" No. Encas.

End of 12" Enc.

9.28	40	92.0	36.80
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10.65

10.48	40	103.2	41.28
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10.32

150.96

	Req. Back	Req. Back
Dist	1100'	C.Y

40	13.0	5.20
----	------	------

40	37.0	14.80
----	------	-------

40	54.0	21.60
----	------	-------

40	61.2	24.48
----	------	-------

Start of 12" Encas

End. of 12" Encas

40	73.0	29.20
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40	84.0	33.60
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128.88

INVERT

33+40		7.3	138.7	132.18 130.85
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33+00		9.3	136.7	130.89 129.29
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32+60		13.3	132.7	129.57 127.93
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T.P.	11.28	<u>145.97</u>	2.51	134.67
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32+20		8.3	128.9	128.29 126.17
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31+90	P.O.T. M.H. #76	8.8	128.4	127.32 125.60
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31+45		9.6	127.6	126.65 124.15
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31+00				137.20
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Cont	Av. Cont	Dist	Ar. C.Y. / 100'	Exc. C.Y.	29
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6.52

6.16 40 58.2 23.28

5.81

4.47 40 42.7 17.08

3.13

2.37 40 23.0 9.20

0.61

0.85 30 8.5 2.55

1.08

1.02 45 10.2 4.58

0.95

1.13 45 11.3 5.09

1.32

61.78

Req. Req.
Back Back
Dist 100' C.Y.

28

40 54.2 25.68

40 38.4 15.36

40 18.0 7.20

30 4.0 1.20

45 6.0 2.70

45 7.0 3.10

~~55.24~~

T.P.
4054104
M.H. 77
97 Nail

6.72 154.56 3.75 148.34

35+60 5.0 149.1 139.11

35+44.56 Δ 11" 42 Rt.
M.H. 77 5.2 148.9 138.83

T.P. 8.62 154.09 0.50 145.17

35+00 0.7 145.3 137.38
137.09

34+60 5.3 140.7 136.07
135.53

34+20 4.4 141.6 134.78
133.97

33+80 4.7 141.3 133.48
132.41

33+40
145.97

Ar.C.Y. Exc. 49

Cvt Ar.Cvt Dist /100' C.Y.

9.99

10.03 15.44 94.4 14.58

10.07

9.00 44.56 84.8 37.79

7.92

6.48 40 59.4 23.76

4.63

5.73 40 54.3 21.72

6.82

7.32 40 69.2 27.68

7.82

7.17 40 67.7 27.08

6.52

152.61

Dist	Req. Back 100'	Req. Back @.Y.
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15.44	90.2	13.93
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44.56	89.2	39.75
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40	55.4	22.16
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40	50.0	20.00
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40	65.0	26.00
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40	63.7	25.48
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147.32

INVERT.

38+00 5.4 149.2 143.43

5.77

37+60 5.3 149.3 142.71

6.59

6.18 40 58.6 23.44

37+20 5.0 149.6 141.99

7.61

7.10 40 67.2 26.88

36+80 6.4 148.2 141.27

6.93

7.27 40 68.7 27.48

36+40 7.6 147.0 140.55

6.45

6.69 40 63.2 25.28

36+00 4.2 150.4 139.93

10.57

10.28 40 97.0 38.80

35+60 154.56

9.99

173.96

Req. Back Req. Back
Dist 1100' @ Y.

40 53.6 21.44

40 63.0 25.20

40 64.6 25.84

40 59.7 23.68

40 76.7 30.48

40 93.0 37.20

163.84

40+40	6.7	154.0	149.58
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4.42

40+00	6.6	154.1	148.50
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5.60

5.01 40 47.6 19.04

39+60	7.8	152.9	147.42
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5.48

5.54 40 52.4 20.96

39+20	9.7	151.0	146.34
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4.66

5.07 40 48.0 19.20

T.P.	12.04	160.70	5.90	148.66
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4.60 40 43.8 17.52

38+80	4.8	149.8	145.26
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4.54

20 th Rt. of M.H.	6.29	148.27	
20.1 + 38.19 Rt. of 110. 42 Rt			
38+36.80 M.H. 78	5.9	148.7	144.09

4.61

4.57 43.2 43.5 18.79

38+00	154.56		
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5.77

5.19 36.8 49.2 17.10

 112.61

Dist	Req. Back 100'	Req. Back C.Y.
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40	43.6	17.44
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40	48.4	19.36
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40	44.0	17.60
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40	39.8	15.92
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43.2	39.5	17.06
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36.8	45.2	16.83
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104.21

Cut Ar. Cut Dist. 100' C.Y.

42+80 12.5 160.9 156.06

4.84

T.P. 13.25 173.42 0.53 160.17

4.98 40 47.2 16.88

42+40 0.6 160.1 154.98

5.12

5.14 40 49.0 19.60

42+00 1.6 159.1 153.90

5.20

4.99 40 47.4 18.96

41+60 3.1 157.6 152.82

4.78

4.87 40 45.4 18.16

41+20 4.0 156.7 151.74

4.96

5.10 40 48.4 19.36

40+80 4.8 155.9 150.66

5.24

4.83 40 46.0 18.40

40+40

160.70

4.42

111.36

Dist	Req. Back 100'	Req. Back @.Y
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36

40	43.3	17.32
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40	45.0	18.00
----	------	-------

40	43.5	17.40
----	------	-------

40	41.4	16.64
----	------	-------

40	44.4	17.76
----	------	-------

40	41.8	16.72
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		103.84
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T.P.	3.10	176.01	0.51	172.91
A5+20			1.8	171.6 161.70
A4+80			5.0	168.4 160.90
A4+40			7.5	165.9 160.10
55-20 RT G	End C.B. 231 Start C.B. 238 Δ 4°-04' LT		9.21	164.21
A4+00	M.H. #79		9.4	164.0 159.30
A3+60			10.2	163.12 158.22
A3+20			11.8	161.6 157.14
A2+80				

173.42

Cvt	Av. Cvt	Dist	100' C.Y
	9.90		
	8.70	40	82.0 32.80
	7.50		
	6.55	40	62.0 24.80
	5.80		
	5.25	40	50.0 20.00
	4.70		
	4.84	40	46.0 18.40
	4.98		
	4.72	40	45.0 18.20
	4.46		
	4.65	40	44.0 17.68
	4.84		
			<u>131.88</u>

Req. Req.
Back Back
Dist. 100' C.Y.

40 78.0 31.20

40 57.8 23.12

40 46.0 18.40

40 42.0 16.80

40 41.0 16.40

40 40.4 16.16

122.08

Cut	Av. Cut	Dist	Av. C.Y. / 100'	Exc. C.Y.
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47+60	3.9	172.1	166.50	5.60
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47+20	5.8	170.2	165.70	4.50
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46+80	4.6	171.4	164.90	6.50
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46+40	5.4	170.6	164.10	6.50
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46+00	3.5	172.5	163.30	9.40
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45+60	2.4	173.6	162.50	11.10
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176.01

45+20

9.90

10.50	40	98.8	39.52
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171.68

	Req. Back	Req. Back
Dist	100'	C.Y.

40	44.0	17.60
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40	48.2	19.28
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40	61.8	24.72
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40	74.0	29.60
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40	87.0	34.80
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40	94.6	37.84
		<hr/>
		163.84

21+20 7.2 178.4 171.91

20+80 8.5 177.1 170.90

20+40 9.5 176.1 167.88

- 20+00 Δ 19° 56' 21" 168.86
48+77.57 M.H.# 80 10.4 175.2 168.85

T.P. 10.15 185.61 0.55 175.46
48+40 1.6 174.4 168.10

48+00 2.5 173.5 167.30

47+60
176.01

Cut Ar. Cut Dist / 1000 Cy

6.49

6.35 40 60.0 24.0

6.70

6.22

6.28 40 59.5 23.80

6.34

6.32 37.57 59.8 23.92

6.30

6.25 40 59.5 23.80 95.52

6.20 ~~End of Period 3/31/48~~

5.90 40 56.0 20.40

5.60

20.40

Dist	Req. Back 100'	Req. Back C.V.
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40	56.00	22.40
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40	55.5	22.70
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37.57	56.00	21.04
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40	59.4	23.76	89.40
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End. of Period 3/31/48.

40	52.0	20.80
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20.80

23+60 2.2 183.3 178.01

5.29

5.5 40 52.2 70.88

23+20 2.9 182.7 177.00

5.70

5.51 40 52.3 20.97

22+80 4.3 181.3 175.98

5.32

5.58 40 53.0 71.70

22+40 4.8 180.8 174.96

5.84

6.35 40 60.0 24.00

22+00 4.8 180.8 173.95

6.85

6.76 40 64.0 25.60

21+60 6.0 179.6 172.93

6.67

6.58 40 67.2 24.88

21+20

6.49

~~24.88~~
137.48

185.61

Av. C.Y. Exc
Cut Cut Dist /100' C.Y.

Req. Req.
Back. Back.
Dist. 100' C.Y.

40 48.2 19.28

40 48.3 19.32

40 48.0 19.20

40 56.0 22.40

40 60.0 24.00

40 58.2 23.28

127.48

26+00			6.3	190.1	184.02
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6.08

6.18	40	58.5	23.40
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25+60			7.1	189.3	183.02
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6.28

T.P.	8.82	<u>196.41</u>	2.21	187.59	
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5.88	40	55.8	27.37
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25+20			2.3	187.5	181.02
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5.48

6.13	40	58.0	23.70
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24+80			2.0	187.8	181.02
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6.78

6.28

24+40			3.0	186.8	180.02
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5.78

40	59.4	23.76
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st. 6. 20.24
M.H. #81

5.77	184.03
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5.98	44.04	56.8	25.00
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Δ 170-3524
M.H. #81

23+95.96			4.7	185.1	178.92
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6.18

5.73	35.96	54.3	19.53
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23+60	6.23	<u>189.80</u>	2.04	183.57	
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5.29

<u>185.61</u>

<u>137.21</u>

Dist.	Req. Back.	Req. Back.
	100	0.0
	54.4	25.76
	51.6	20.64
	54.0	21.60
	55.4	22.16
	44.04	23.34
	35.96	18.32
		<hr/> 131.72

28+10			7.4	196.8	190.02
T.P.	8.56	<u>204.20</u>	0.77	195.64	

28+00			1.0	195.4	189.02
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27+60			2.5	193.9	188.02
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27+20			2.7	193.7	187.02
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26+80			5.2	191.2	186.02
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26+40			5.3	191.1	185.02
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26+00					
		<u>196.41</u>			

Cvt Av.Cvt Dist. 100. C.Y.

6.78					
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6.58	40	62.2	24.88		
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6.38					
------	--	--	--	--	--

6.13	40	58.0	23.20		
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5.88					
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6.28	40	59.4	23.76		
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6.68					
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5.93	40	56.3	21.92		
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5.18					
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5.63	40	53.3	21.32		
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6.08					
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6.08	40	57.6	22.98		
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6.08					
			<u>138.06</u>		

	Req. Back.	Req. Back.
Dist.	100.	C.Y

40	58.1	23.24
----	------	-------

40	54.0	21.60
----	------	-------

40	55.3	22.12
----	------	-------

40	52.3	20.92
----	------	-------

40	49.3	19.72
----	------	-------

40	53.6	21.40
----	------	-------

129.00

30+80 5.2 202.3 196.25

6.05

30+40 5.9 201.6 195.17

6.43

30+00 7.0 200.5 194.09

6.41

T.P. 121 446

2085 Lt of 7.20 207.49 3.91 200.29

6.30 36.04 59.6 21.48

29+63.76 Δ 332.00 RT. M.H. 82 4.9 199.3 193.12

6.18

5.94 43.96 56.4 24.79

29+20 6.5 197.7 192.02

5.68

6.03 40 57.0 24.80

28+80 6.8 197.4

6.38

191.02

6.58 40 62.2 24.88

28+40

6.78

141.95

204.20

Ar.Cy Exc.

49

Cut Ar.Cut Dist 1.00 C.Y

	Req. Back	Req. Back
Dist	100	0.7

40	55.0	24.00
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40	57.0	24.80
----	------	-------

36.00	55.5	20.00
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43.96	57.7	22.95
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40	53.0	21.20
----	------	-------

40	58.0	23.20
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132.15

33+20 5.8 208.5 202.73

32+80 7.4 206.9 201.65

32+40 8.4 205.9 200.57

T.P. 8.52 214.25 1.76 205.73

32+00 2.9 204.6 199.49

31+60 3.2 204.3 198.41

31+20 4.0 203.5 197.33

30+80 207.49

51

Out	Av. Crt	Dist.	Av. C. / 100'	Exc. C. /
	5.77			
	5.51	40	52.3	20.92
	5.25			
	5.29	40	50.0	20.00
	5.33			
	5.22	40	49.5	19.80
	5.11			
	5.50	40	52.0	20.80
	5.89			
	6.03	40	57.0	22.80
	6.17			
	6.11	40	58.0	23.20
	6.05			<u>127.52</u>

Dist	Req. Back	Req. Back
	100	@.7

40	48.2	19.28
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40	46.2	18.48
----	------	-------

40	45.5	18.20
----	------	-------

40	48.0	19.20
----	------	-------

40	53.0	21.20
----	------	-------

40	54.0	21.60
----	------	-------

117.96

35+60 8.2 215.6 208.89

6.71

6.76 40 63.5 25.40

35+20 9.1 214.7 207.89

6.81

T.P. 10.65 223.72 6.18 213.07

6.51 40 61.5 24.60

34+80 1.2 213.1 206.89

6.71

5.31 40 50.4 20.16

34+40 4.0 210.3 205.89

4.41

4.71 40 40.0 16.00

34+00 P.O.T.
M.H. # 83 5.4 208.9 204.89

4.01

4.80 40 45.6 18.34

33+60 4.9 209.4 203.81

5.59

5.88 40 55.8 22.32

33+40

5.77

214.25

126.82

Ar.C.Y. Etc.

53

Cut Ar.Cut Dist 1100' C.Y.

	Req. Back	Req. Back
Dist	100	0.4

40	59.5	23.80
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40	57.4	22.86
----	------	-------

40	46.5	18.60
----	------	-------

40	36.0	14.40
----	------	-------

40	41.6	16.64
----	------	-------

40	51.8	20.72
----	------	-------

117.02

1x1710 20'
R+MH 84

SS

1.83 225.38

Δ 410 16' LT

38+00

M.H. #84

5.4 221.9 214.89

T.P.

6.27

227.21

2.78 220.94

37+60

3.2 220.6 213.89

37+20

4.1 219.7 212.89

36+80

4.9 218.9 211.89

36+40

6.0 217.8 210.89

36+00

7.1 216.7 209.89

35+60

223.72

Cut

Ar.Cut.

Dist

Ar.C.Y.

Exc.

1000'

C.Y.

7.01

6.86 40 64.6 25.84

6.71

6.76 40 64.0 25.60

6.81

6.91 40 65.2 26.08

7.01

6.96 40 65.6 26.24

6.91

6.86 40 64.6 25.84

6.81

6.76 40 64.0 25.60

6.71

~~155.20~~

	Req. Back.	Req. Back.
Dist	100'	0.4

56

40 60.5 24.20

40 60.0 24.00

40 61.2 24.48

40 61.5 24.60

40 60.5 24.20

40 60.0 24.00

~~145.48~~

40+40 4.4 226.8 221.13

40+00 5.7 225.5 220.09

T.P. 6.90 234.17 2.94 224.27

39+60 2.8 224.5 219.05

39+20 5.4 224.9 218.01

38+80 5.3 222.0 216.97

38+40 4.8 222.5 215.93

38+00 227.21

57

Cut	Av. Cut	Dist.	Av. O.Y. /100'	Exc. C.Y.
	5.67			
	5.54	40	57.2	24.88
	5.41			
	5.43	40	56.3	22.52
	5.45			
	4.67	40	49.0	19.60
	3.89			
	4.46	40	47.2	18.88
	5.03			
	5.80	40	59.9	23.92
	6.57	38+60	Conc. Encasement Starts	
	6.79	40	64.0	25.60
	7.01			
				<hr/> 133.40

	Req. Back.	Req. Back.
Dist	100'	2.7

40	38.0	15.70
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40	37.3	14.92
----	------	-------

40	30.0	12.00
----	------	-------

40	28.0	11.20
----	------	-------

40	40.4	16.16
----	------	-------

End. Eggs. Starts

40	60.0	24.00
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93.18

X. on. M. H. Ritt.

F.B. 3.70 231.69

X on. M. H. Ritt over out lot 231.71
- 0.03

Invert of
EXIST. M.H.

229.61

End. of job.

41+86^{ce} Connect to
Exist. 10" sewer 3.9 231.15 224.9A

41+60 4.8 230.6 224.25

T.P. 5.67 235.38 1.46 229.71

41+20 2.0 229.2 223.21

40+80 4.9 226.3 222.17

40+40
231.17

Back fill

41+86^b

Req. Back 100' C.Y.

26.6 57.0 15.16

41+60

40. 54.4 21.76

41+30

10 44.0 17.60

40+80

10. 37.8 13.12 67.64

40+40

End. of Con. Encase.

Cut Av. Cut

Dist. Av. C.Y. Exc. C.Y.

6.56

6.45 26.6 61.0 16.23

6.35

6.17 10 58.4 23.36

5.99

5.06 40 48.0 19.20

4.13

4.90 40 52.6 25.04

5.67

End. of Conc. Encasement
40+60

83.83

X. Sec. M.V. Sewer.

⊕

60

0+95 to M.H. # 70

2+25

$\frac{4.3}{60}$	$\frac{6.2}{40}$	$\frac{7.2}{30}$	7.6	$\frac{8.2}{25}$
T.B.				

2+00

$\frac{4.5}{67}$	$\frac{6.0}{58}$	$\frac{6.3}{11}$	$\frac{7.8}{8}$	7.8	$\frac{8.4}{25}$
T.B.					

1+75

$\frac{5.2}{60}$	$\frac{6.3}{50}$	$\frac{7.1}{72}$	$\frac{7.7}{8}$	7.7	$\frac{8.8}{25}$
T.B.					

1+50

$\frac{5.6}{50}$	$\frac{8.7}{12}$	8.4	$\frac{8.9}{25}$
T.B.			

1+20 90° to Fwd. Tang

$\frac{6.2}{28}$	$\frac{7.9}{22}$	8.8	$\frac{7.6}{20}$
T.B.			

T.B. = ^{Edge} ~~Foot~~ of berm

0+95 on berm of Camino del Rio

$\frac{6.2}{25}$	7.1	$\frac{7.7}{25}$
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0+00

M.H. #68

(⊕ = Sewer Line)

B.M. Chisol
D. Hardwall

7.88

81.16

-

73.28

FB1809

P. 75

81.16

5+00

6.4	7.7	9.2	9.7	9.0
17	8	5		25
T.B.				

4+50

7.1	9.2	9.5	9.4
29	15		25
T.B.			

4+00

7.8	9.9	10.3	10.2	9.6
32	26	15		25
T.B.				

T.R 7.12 87.27 1.02 80.14

87.27

3+50

2.3	4.8	5.1	5.1
38	30		25
T.B.			

3+00

3.2	4.7	5.8	5.9	6.1
50	44	30		25
T.B.				

2+50

3.6	6.6	7.1	7.1
60	30		25
T.B.			

81.16

81.16

20' Lt. M.H. #70

Page 5

2.50 84.77 84.80

6439.54 M.H. #70 (Page 5)

6+00

5+50

87.27

62

$\frac{3.0}{5}$

3.2

$\frac{3.4}{6}$

$\frac{10.3}{25}$

T.B
APPROX

$\frac{3.8}{9}$
T.B

$\frac{4.8}{7}$

4.7

$\frac{5.7}{12}$

$\frac{9.1}{20}$

$\frac{9.5}{25}$

$\frac{5.3}{11}$
T.B

$\frac{7.6}{7}$

7.5

$\frac{7.9}{17}$

10.0

$\frac{10.2}{35}$

87.27

Varona

St.

Fd. Hub

0+00

Fd 3/4" Iron Pipe
RE 2317

St

Savoy

Block

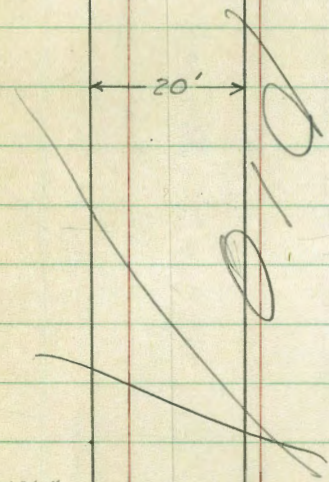
20'

Fd 3/4" Iron Pipe
RE 469

10'

La Poloma

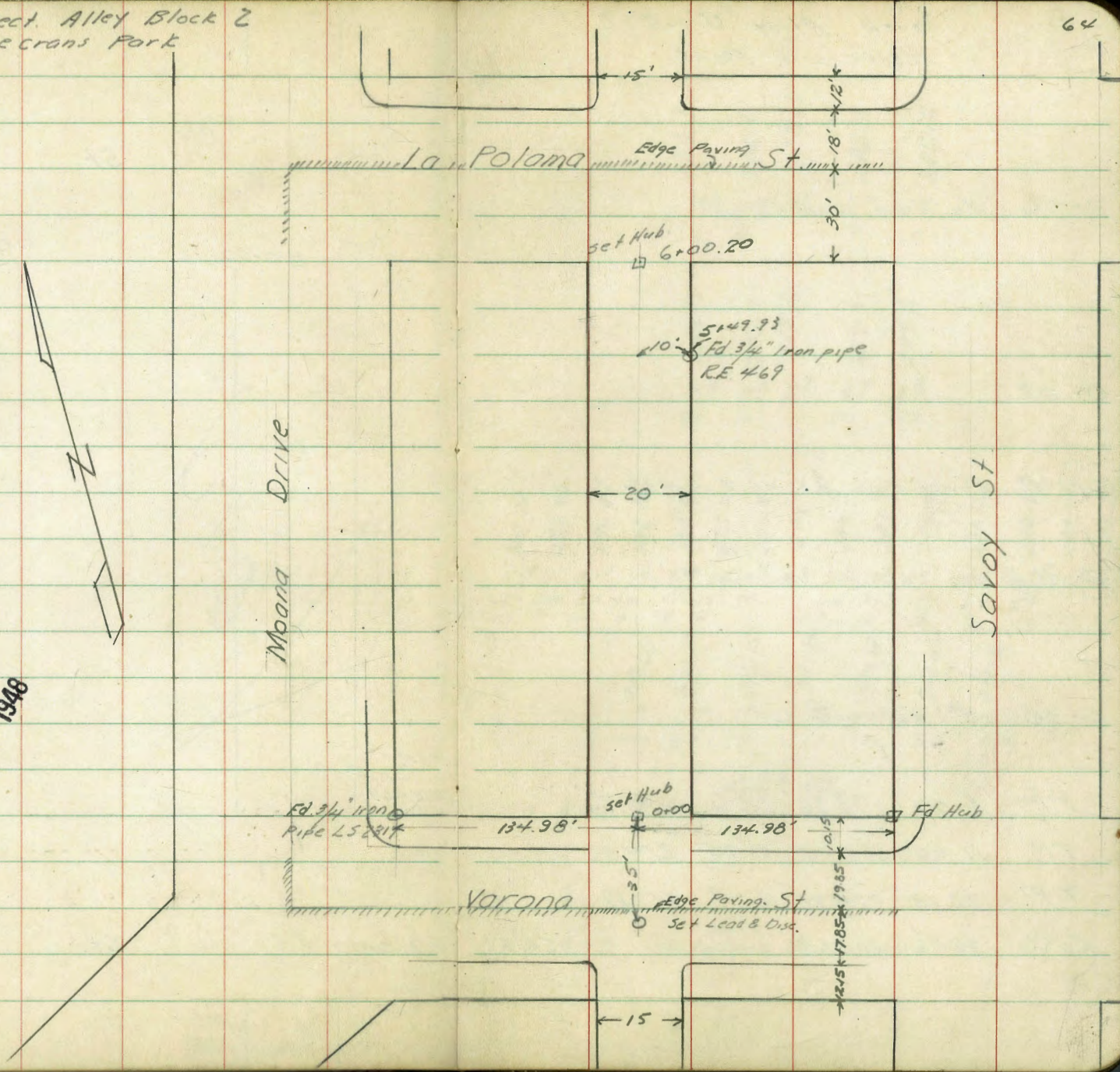
St.



6-2-48
Hendricks
Becker
Oatley

X Sect. Alley Block 2
Rosecrans Park

64



INDEXED
JUN 3 1948

Levels Alley Block 2
Rosecrans Park

0+00 No. Line Varona St.

0-02.

0-7.7 Power Pole 84 Lt. & #4250

0-10.15 No. Cb Line Varona St

0-30 E Varona St

TP 8.00 293.36 1.06 285.36

TP 11.60 286.42 0.15 274.82

TP 12.78 274.97 0.49 262.19

B.M. 11.86 262.68 250.82

286.0
7th 7th 8^o
20 10 10 20

285.9
7th 7th 8^o
20 10 10 20

287.5A
287.46
286.81
286.16
285.16
285.0
284.9
284.6
284.2
283.9
284.19
281.66
242.43
240.06
240.32

5th 5th 5th 7th 8^o 8th 8th 8th 9th 9th 9th 11th 10th 13th 13th 13th
100 100 50 50 13th 13th 10 10 12th 12th 50 50 100 100
Cb G. Cb G. Cb G Cb G Cb G Cb G Cb G Cb

247.65
246.81
245.15
244.80
244.28
242.61
240.38
5th 6th 8th 9th 10th 13th
100 50 10 10 50 100

293.36

on Hub & Alley 0+00

S.V.B.P. Catalina & Varona FB 1671-68

1+00

0+80

0+50

0+30

0+04

293.36

π

289.8	289.3	287.2	286.3	285.9	286.2	288.5	288.4	287.9
3 ^h	4 ^h	6 ^h	7 ^h	7 ^h	7 ^h	4 ^h	5 ^h	5 ^h
20	16	10	6	6	6 ^h	8	10	20

289.4	289.8	288.0	287.9	287.7	288.1	287.8
4 ^h	4 ^h	5 ^h	5 ^h	5 ^h	5 ^h	5 ^h
20	10	7	5	7	10	20

287.4	288.8	288.0	287.9	287.8	288.2	288.8
4 ^h	4 ^h	5 ^h	5 ^h	5 ^h	5 ^h	5 ^h
20	10	7	5	10	21	20

287.4	287.1	287.1	286.4	286.3	286.1	285.6
6 ^h	6 ^h	6 ^h	7 ^h	7 ^h	7 ^h	7 ^h
20	10	8	6	10	20	20

286.0	285.8	285.5	284.7	284.3
7 ^h	7 ^h	7 ^h	8 ^h	9 ^h
20	10	10	10	20

2+56 Single Garage 28' RT

2+50

2+31 Double Garage 20' RT.

T.P. 232 283.00 1268 280.68

2+00

1+99 Power Pole C.G. LL # A1137

1+50

293.36

280.89
4"
28
Floor

281.6
28
20
279.9
31
10
279.6
34
10
279.0
40
10
278.8
43
20

280.13
287
20
Floor

281.8
16
20
281.3
12
10
281.6
11
10
283.00
129
10
280.5
129
10
280.4
13
20

284.0
94
20
283.5
99
10
283.3
101
10
282.7
101
10
282.3
111
20

293.36

3+50

3+49.5 Power Pole 9' LL & # PA 1159

3+22.5 Dead Man to Pole 9' LL &

3+19.7 & Sewer M.H. 0.5 LL

3+00

2+74.8 End Conc Drive 10.5 LL &

2+63 Beg. Conc Drive 10.5 LL &

283.00

277.3

57
20

277.0

60
10

277.0

60
10

276.5

65
10

276.4

60
20

277.41

59
Rim

278.9

41
20

278.7

42
10

278.3

41
10

277.8

52
10

277.4

56
20

279.06

374
10.5

279.36

364
21

279.21

379
10.5

243.00

5+34.9 £ Double Garage 57 3 RT £

5100

4+64 Power pole 10.2 RT £ # 447 099 H

4+60.5 £ Garage

4+50

4+00

3+58 £ Single Garage 22.3 RT.

28300

274.1	273.6	273.5	279.35
8 ⁹	9 ⁴	9 ⁵	3 ⁶⁵
20	10	10	27.3
			Floor
			273.1
			272.8
			10 ⁰
			20

272.91	273.00
10.09	10.00
45.7	48.7
Apron	Floor

275.1	274.9	274.5	274.3	273.9
7 ⁹	8 ¹	8 ⁵	8 ⁷	9 ¹
20	10	10	10	20

276.4	275.8	276.2	275.7	275.5	275.4
6 ⁵	7 ²	6 ⁰⁰	7 ²	7 ⁵	7 ⁶
20	10	20	10	20	20

276.33	276.57
6.7	6.43
19.3	22.3
Apron	Floor

243.00

6+10.20 So. Cb Line La Paloma (Cb in very poor condition)

269.16	268.7	267.50	267.2	267.3	266.8	266.1	266.35	264.2	264.29
54	59	70	74	73	78	85	822	104	1028
50	50	112	115	10		104	104	50	50
Cb	E. Cb	Cb	Cb			E	Cb	G.	Cb

6+08 Power Pole N. 8 LLE # PA 1199

6+00.20 So. Line La Paloma

268.5	268.4	268.16	267.7	267.4
61	62	621	69	72
20	10	Hub	10	20

5+92

272.0	271.6	270.2	270.2	269.7	270.2	271.1	270.8
26	30	44	44	49	44	35	38
20	16	10	4		10	15	20

5+76

273.6	273.6	272.8	272.2	272.0	272.1	272.2
10	16	18	24	26	25	24
20	10	4	2		10	20

274.57

TP. 1.80 274.57 10.23 272.77

on Pipe 10' RL 514993 (RE 469)

5+50

273.9	273.6	272.1	272.8	272.4
91	94	99	102	106
20	10		10	20

283.00
T

283.00

⊕

				250.81
B.M		4.03	250.79	250.82
			254.84	244.25
T.P.	10.59	254.86	1.67	244.23
			245.92	236.88
T.P.	9.04	245.90	12.46	236.86
T.P.	-0.04	249.34	12.94	249.38
T.P.	0.89	262.32	13.14	261.43

6 + 30.20 & La Paloma St.

274.57
↑

J.W.B.P Catalina & Yerong

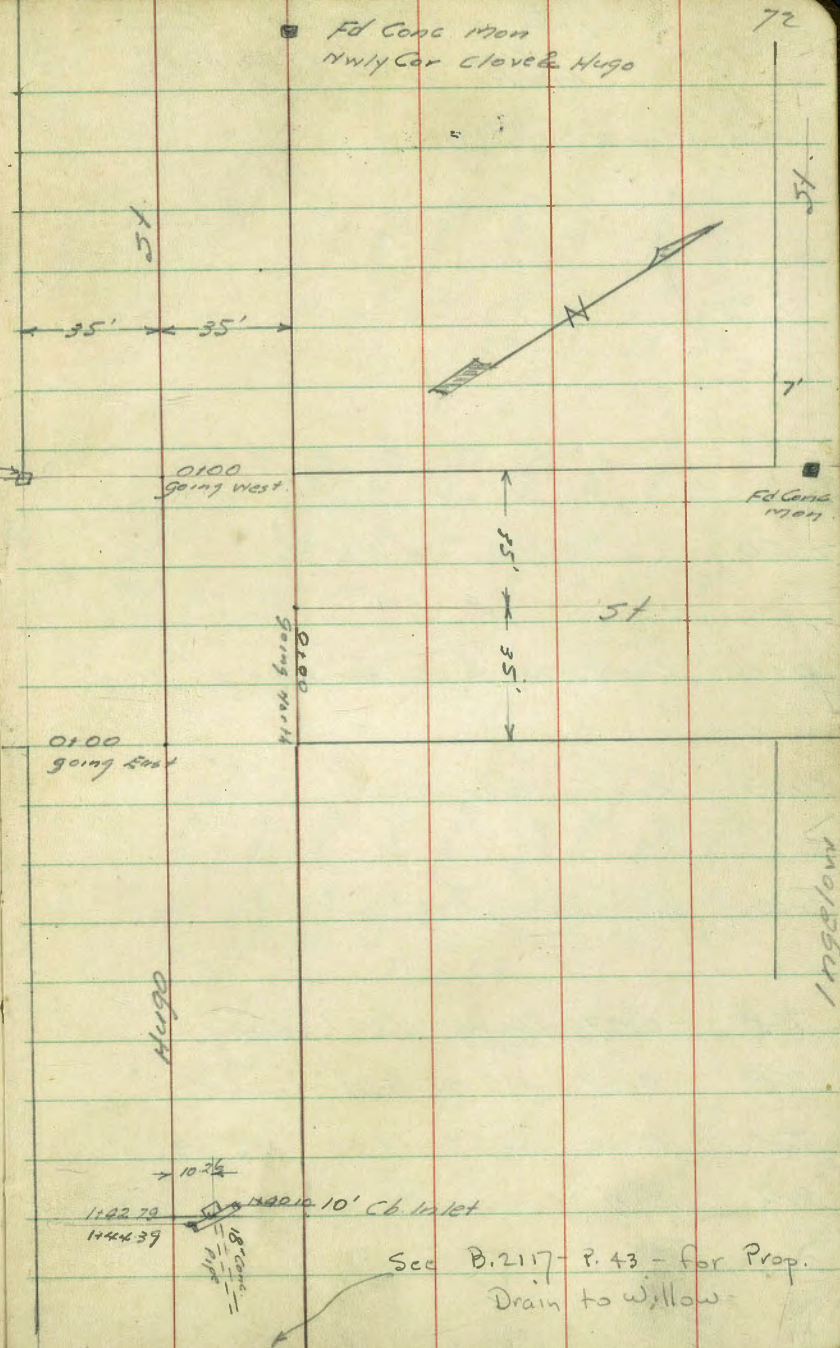
263.53	265.31	265.66	265.95	266.83
11.04	9.26	8.91	8.62	7.74
50	10	10	50	

274.57

6-6-49 X Sect. Plum & Hugo St.
Hendricks
Roberts
Greer
Korer
W.O.# 25001

INDEXED
WK
JUN 8 1949

148.61



72

F.d. Conc. 17011
NW 1/4 Cor. Clover & Hugo

F.d. Hub

0100
going West

F.d. Conc.
17011

Plum

0100
going North

0100
going East

Hugo

1 ng & low

10' x 10'
1402 79
1444 39
18' Conc.
10' x 10' Cb. Inlet

See B.2117 - P. 43 - for Prop.
Drain to Willow

X Section Plum St. from
 114 line Hugo to 150' 114. towards
 Ingelen St.

New Drive - P. 78.

0175

110.8	110.5	110.3	109.7	109.2	108.9	108.7	108.3	107.9
38	41	43	49	54	60	59	63	70
50	35	25	17		27	28	35	50

0150

111.9	111.7	110.8	109.1	108.9	108.2	108.7	108.4	107.9
27	29	38	55	57	64	59	62	67
44	35	22	15		18	19	35	50

0110 Dead Man to Anchor Pole 25' H.

0103 Anchor Pole 25' H.

0100 114. Line Hugo St.

111.6	111.3	110.8	108.5	108.3	107.6	108.0	107.8	107.5
30	33	38	61	62	70	65	68	71
50	35	25	15		18	19	35	50
114.62								

T.P. -0.07 114.62 12.86 114.69

TP 0.59 127.55 5.71 126.96

TP 0.44 132.67 13.22 132.23

BM 12.71 145.45 ✓ 132.74

Nail in Power Pole # 1448 Plum & Hugo
 (6' High on Pole)

N.E.P.P. Clove & Fenelon

1404 Rim of Canyon

111.0	110.3	109.6	108.7	107.4
5 16	2 1/2	5 0	5 9	7 1/2
50	25	35	50	

0198 End Conc Ramp to Garage

110.52	110.38
4 0	4 3/4
43.5	41.5
Fl	Ramp

0181 Beg Conc Ramp to Garage

110.66	110.59
3 9/16	4 0 3/4
43.5	41.5
Fl	Ramp

114.62

114.62

X Sect. Hugo St ~ Plum towards
Clove St.

0-09 Power Pole # 1448 35' Lt

0-11

0-23

0-27 Dead man to Pole 34' Lt

0-35 E Plum sewer MH 1.1 Rt

0-70 E. Line Plum

114.62 (From p 74)

107.4	107.5	108.3	108.0	108.2	108.7	110.6
7.3	7.1	6.3	6.5	6.7	5.9	4.0
50	41	35	25		15	35

107.0	107.8	108.1	108.6
7.5	6.8	6.5	6.0
50	35		35

109.6	109.3	108.0	108.0	108.5
5.0	5.2	6.5	6.5	6.1
50	39	25		35

110.1	107.8	108.4	108.0	107.4	107.4	107.9	108.3
4.5	4.8	6.2	6.5	7.0	6.7	6.8	6.3
50	40	35	32	17		11	35

109.8	109.1	107.0	106.5	106.9	106.4	106.8	107.8	107.9
4.8	5.5	7.5	8.1	7.7	8.2	7.8	6.8	6.2
50	35	17	15		19	21	35	50

114.62

X Sect. Hugo St. Contd.

1400

110.6	110.11	110.4	110.1	110.0	110.2	110.1	110.7	110.1
40	40	42	45	45	42	39	39	39
50	25	28	26	3		15	35	50

0465

109.6	109.1	109.3	109.0	109.7	110.1	110.7	110.1
51	50	53	55	53	45	39	40
50	35	25	9		15	35	50

0430

110.1	110.1	110.7	108.7	108.4	109.0	110.5	111.3	112.1
32	32	37	57	62	55	41	33	25
50	35	33	25	12		23	35	50

0410 3.5' Conc. Walk 24.1 RL.

110.99	111.45
36.3	37
24.6	35

0400 W Line Plum St.

111.7	111.4	108.2	108.1	109.0	110.1	111.3
28	32	64	61	56	32	33
50	35	25		11	27	35

114.62

114.62

X Set Hago St. Line Plum
to East.

0+47

105.9
82
50

105.7
82
35

104.6
100
27

103.8
100
18

103.2
114
15

103.6
110
15

103.4
112
15

108.1
65
35

108.9
52
43

108.5
61
50

0+25

107.2
74
50

107.1
75
35

105.6
90
25

105.4
92
17

105.0
95
15

105.4
92
14

104.8
98
14

106.1
85
22

109.8
108
35

109.6
50
50

0+23 End Conc. Drive on Rt. 20.5'

106.37
82
20.5

108.29
63
30.5

109.03
55
38.5

0+05 Beg. Conc. Drive on Rt. 20.5'

106.81
78
20.5

108.35
63
31

109.15
55
38.2

0+00 = 0-70 P. 75

114.62 from P. 76

114.62

1127

Note: New Drive

1104

T.P. 0 22 102.37 12.47 102.15

0 + 94 - 32.3 ft. end Dr.

0191

102.05
32.3
Cor.
Dr.

Actual Elev.
Shown

0 + 77 - 32.5 ft. = Rec. Corr. Dr.

0168

102.45
32.5
Rt. = Cor.
Dr.

102.95
50.7 = floor
Gar.

0150

114.62

98.9	98.2	97.6	97.4	97.4	98.0	96.4	94.8
25	20	20	5.0	5.0	25	6.0	7.5
50	35	27		18	25	35	50

101.3	100.6	98.9	98.7	99.0	98.8	99.6	99.6	98.0
15	18	25	37	37	36	25	20	25
50	35	24	19		17	24	35	50

102.0	101.8	99.7	99.8	99.7	104.8	105.2
12.5	12.8	15.2	14.8	14.9	9.5	9.5
50	35	16		16	35	50

104.0	103.9	103.2	102.0	101.6	101.8	101.6	103.8	104.2	104.5
10.5	10.7	11.2	12.5	13.0	12.5	12.0	10.5	10.5	10.5
50	35	31	17	15		12	28	35	50

105.5	105.3	104.2	103.5	102.9	103.4	103.0	105.0	105.0
9.5	9.3	10.1	11.1	11.7	11.2	11.6	9.5	9.5
50	35	27	18	15		13	35	50

114.62

B17 3.49 51.46 51.45

TP 4.43 54.95 94.2 50.52

TP 0.29 59.94 12.39 59.65

TP 0.36 72.04 13.15 71.68

TP 0.19 84.83 13.20 84.64

11.67 End 18" Conc Pipe 13.5 LL

TP 1.50 97.84 6.03 96.34

1144.39 End 10' Cb Inlet 55 LL

1142.79 R 10' Cb Inlet 10.26 LL

1140.10 Beg 10' Cb Inlet 14.5 LL

1139

102.37

✓

SW 8P Garrison & Willow

83.0	86.5	85.9	84.2	86.7	87.5	89.4	89.5
14 ⁸	11 ⁵	11 ⁷	13 ⁵⁷	11 ¹	10 ³	8 ⁴	8 ³
29	20	15	13.5	11		25	50
			FL				

HELY Cor 70' Cb Inlet

96.20	97.84
6.7	7.1
55	55
Cb	Gut

90.4	92.2	94.2	92.40	94.26	95.28	95.4	97.0	94.3	97.9	95.0	94.4	92.6
12 ¹⁰	8 ²	9 ²⁷	6 ¹¹	7 ⁹	7 ⁰	5 ⁴	4 ¹	4 ⁵	7 ⁴	4 ⁰	9 ⁸	
50	35	22	10.26	10.26	10.26	5		3	9	20	35	50
			FL	Cb	Gut							
			96.24	96.24	95.37							
			6.03	7.00								
			14.5	14.5								
			Cb	Gut								

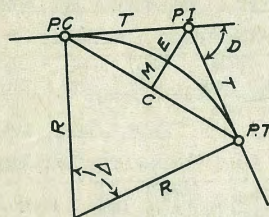
93.2	93.8	94.8	97.0	95.5	95.9	97.4	98.5	96.1	94.9	93.2
9 ¹	8 ⁶	7 ⁵	5 ⁴	6 ⁹	6 ⁵	5 ⁰	3 ⁹	6 ²³	7 ⁵	9 ³
50	35	27	18	14		3	17	26	35	50

102.37

✓

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
 Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
 Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers } \frac{\Delta}{2}$ (6)
 External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec } \frac{\Delta}{2}$ (9)
 Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction=.36 or $T = 414.85$ ft. P. C.=Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.=Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance= $158 - \text{Sta. P. C.} = 54.50$, hence offset= $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=def. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve= $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction=.10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

12 7 97

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

102 37
97 54
4 73

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.