

1849

ENGINEERS

AND ARCHITECTS

NO. 1849

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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1849

440339
30051
100990
1367
10+2327

13.77
13.67
306.51
320.18
13.93 35
23 57

INDEXED

to page # 74.

Lat & Archer & LaJolla to 2 Drain Int.
(4+135)

Box drain 38" wide
15' throat 2' x 3' grate

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

30651

X-sec. + Bldg. Location	
Monroe Alaine to 48 th	1-22
Monroe + Euclid	28-38
Alley BIK. 2. Roseville Hgts	39
Island Court + Bayside Lane - Drain Extension	46-48
Beta St., Survey for proposed sewer	49-51
X- Sec. 20' Alley, BIK. 2, N. Shore Highlands	52-57
X- Sec. La Jolla Scenic Drive	58-64
Adams- Park Blvd. to Boundry	65-67
X- Sec. 15' Alley in BIK. 65, Resub. of BIKs. 39 + 56, Normal Heights	68-71

Additional Notes.
MONROE - Aldine Dr. East.
ALDINE Dr. Monroe North.

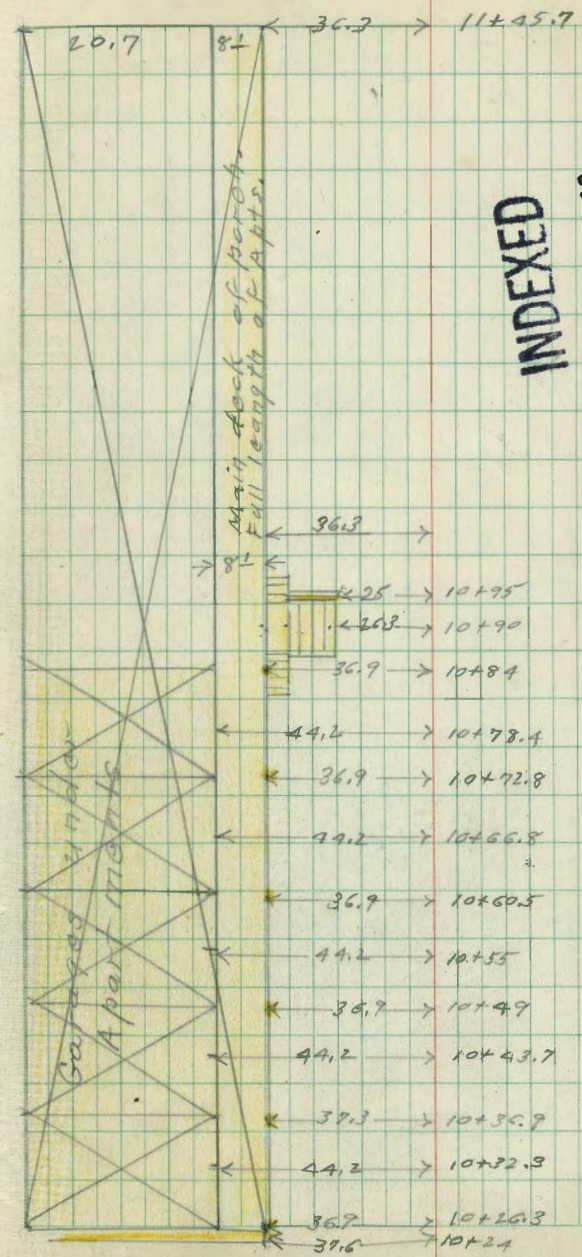
Sketches P. 10 F.B. 1585
Also P. 5 - FB 1849

Stationing same as original
notes. F.B. 1585

5-10-48
W.O. 21001

Sammermeyer
McCoy &
W. Moore
Sherman.

INDEXED
WK
DEC 20 1948



INDEXED
MAY 11 1948

10+49 36² Lt. = Ctr. 13" x 13" Conc. pier.

10+43² = \pm Gar. #2 - 44² Lt.

10+37³ 36² Lt. = Ctr. 13" x 13" Conc. pier.

10+32² 44² Lt. = \pm 8' wide garage

B.P. = Bottom (or base) of pier

T.P. = Top of pier

44² Lt. = start stucco apt. Bldg (5 unit.)

10+26³ 36² Lt. = Ctr. 13" x 13" conc. pier.

10+24 37⁵ Lt. = \pm 3' wide conc. walk

Stationing same as in $\frac{F.B. 1585}{10}$

T.P. 3.25 334.89 7.96 331.64

SE. B.P. 47' + Monroe 1.66 339.60 — 337.94

$\frac{1585}{23}$

332.09	330.4	331.5
2.80	4.5	3.4
36.9	36.9	36
T.P.	B.P.	Grid

331.81
3108
442
Conc. floor

332.05	330.5	331.4
2.84	4.4	3.5
36.9	36.9	36
T.P.	B.P.	Grid

331.81
3.08
442
Curt. floor

332.04	330.0	331.4
2.85	4.9	3.5
36.9	36.9	36
Top pier	Base pier	Grid

332.13	331.49
2.76	3.40
37.6	37.6
st. walk	= walk

334.89

Monroe

T.P. 6.74 341.41 0.22 334.67

10+84^o 36^o Lt. = Ctr. 13" x 13" Conc. pier.

10+78^o 44^o Lt. = Φ Gar. #5

10+72^o 36^o Lt. = Ctr. 13" x 13" Conc. pier.

10+66^o 44^o Lt. = Φ Gar. #4

10+60^o 36^o Lt. = Ctr. 13" x 13" Conc. pier.

10+55 44^o Lt. = Φ Gar. #3

334.89

SP. CP.
M. 10+41 3.66 3.700 - 3.111
1575

332.08	330.8	331.8
2.81	4.1	3.1
36.9	36.9	36
T.P.	B.P.	Ord.

331.79
3.10
44.2
Conc. floor

332.02	330.4	331.5
2.87	4.5	3.4
36.9	36.9	36
T.P.	B.P.	Ord.

331.80
3.09
44.2
Conc. floor

332.05	330.6	331.6
2.81	4.3	3.4
36.9	36.9	36
T.P.	B.P.	Ord.

331.79
3.10
44.2
Conc. floor

334.89

B.P.
N.E. 47th
Monroe

3.47 337.94

65² Lt. = N.W. Cor. Apts.

11+45² 36² Lt. = End. (S.W. Cor.) stucco Apts.

10+95² 25' Lt. = 6" wide N. + S. Conc. wall.

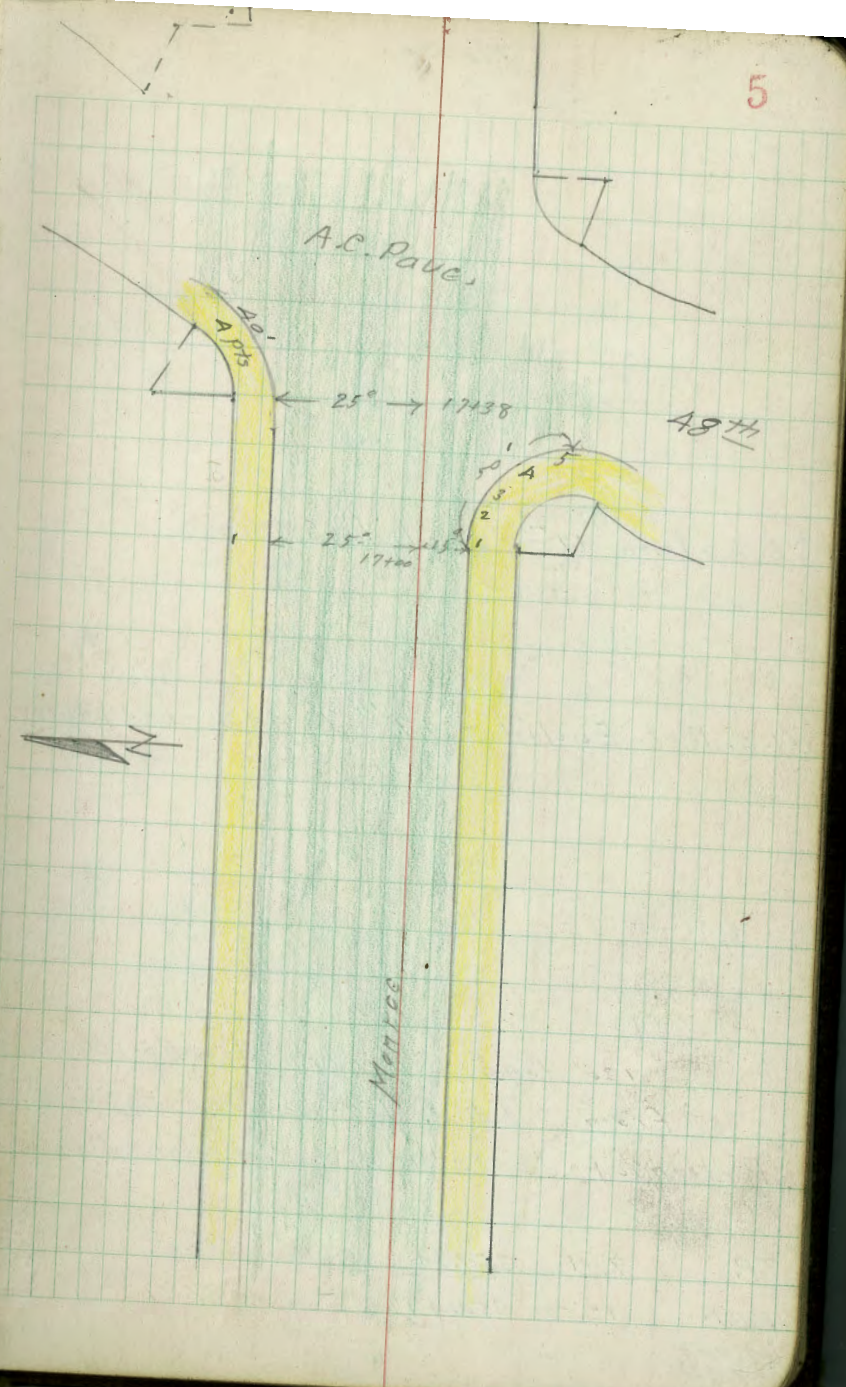
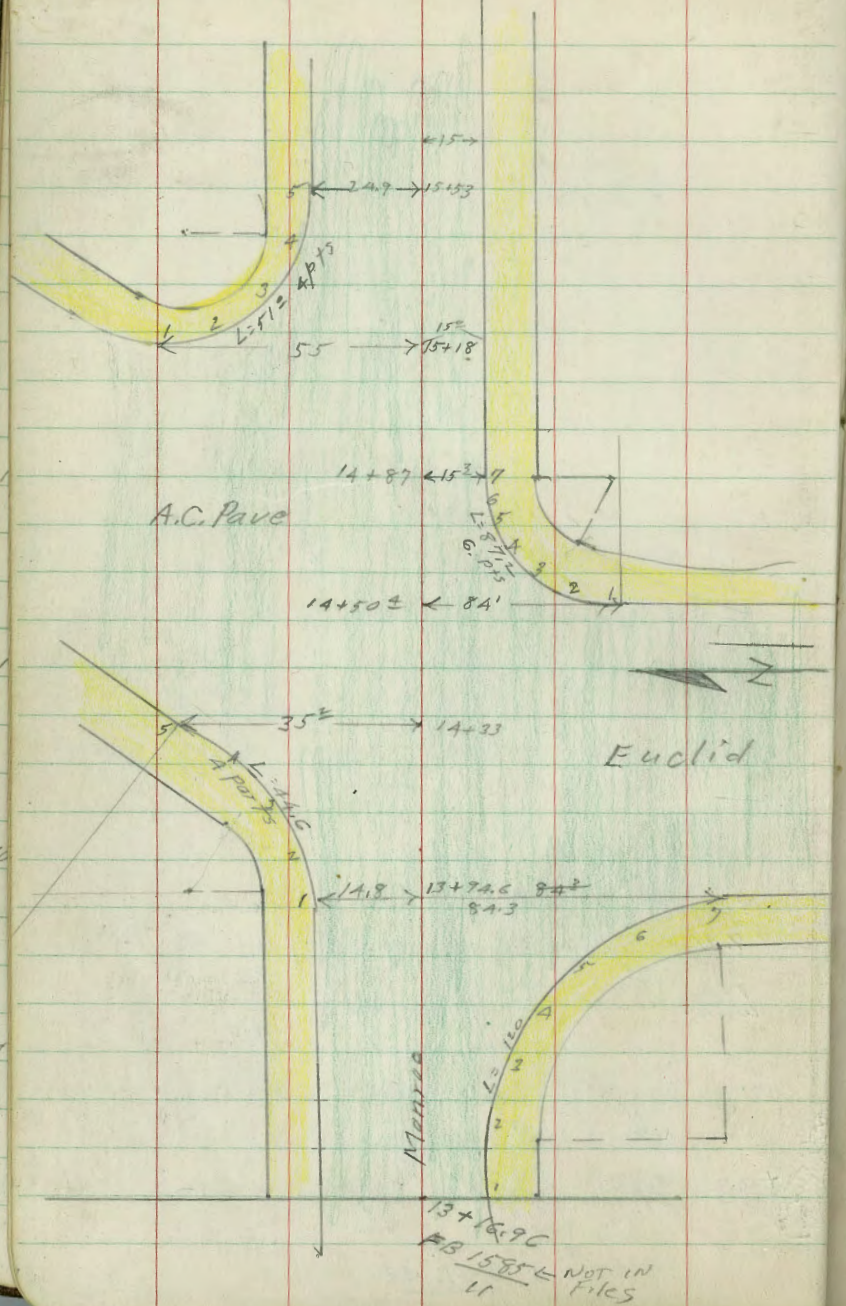
36² Lt. = Edge main porch deck
32² = landing to East + west steps

10+90 26² Lt. = 5" wide Conc. Steps

341.41

334.00	331.7	332.0
7.41	9.7	8.6
25	25	25
Top wall	Base wall	Ord

341.53	357.02	333.56
+0.12	4.39	7.85
36.3	32.3	26.3
Main deck	Landing	Top of Bottom step
		<u>341.41</u>



S.E. Return ^{Monroe} 47th + Euclid 6. pts.

N.W. Ret. Euclid + ^{Monroe} 47th L = 44.6 - in 4 parts

120' long 6 parts. G-gutter ob. curb
 from Sub. Div. line around to South.
 Portion of Cb. return, S.W. Euclid + Monroe

T.P.	9.01	<u>359.34</u>	0.11	350.33
S.E. B.P.	12.50	350.44	-	337.94
Monroe 47 th				

$\frac{4.85}{5}$ G	$\frac{4.75}{5}$ ob.	$\frac{4.55}{5}$ G	$\frac{4.00}{5}$ ob.	$\frac{4.41}{5}$ G	$\frac{3.91}{5}$ ob.
E.C. to east.					

5.61 G	^{5.45} Drive ob.	5.36 G	4.81 ob.	5.19 G	4.65 ob.	5.00 G	4.49 ob.
B.C. on 50							

$\frac{6.56}{5}$ G	$\frac{6.12}{5}$ ob.	$\frac{6.11}{5}$ G	$\frac{5.70}{5}$ ob.	$\frac{5.70}{5}$ G	$\frac{5.15}{5}$ ob.	$\frac{5.22}{5}$ G	$\frac{4.74}{5}$ ob.	$\frac{4.77}{5}$ G	$\frac{4.27}{5}$ ob.
E.C. to No									

$\frac{7.20}{5}$ G	$\frac{7.22}{5}$ ob.	$\frac{7.03}{5}$ G	$\frac{7.22}{5}$ ob.	$\frac{7.57}{5}$ G	$\frac{7.07}{5}$ ob.	$\frac{7.45}{5}$ G	$\frac{7.01}{5}$ ob.
Approx E.C.							

$\frac{11.41}{5}$ G	$\frac{10.80}{5}$ ob.	$\frac{9.44}{5}$ G	$\frac{8.89}{5}$ ob.	$\frac{8.25}{5}$ G	$\frac{7.70}{5}$ ob.	$\frac{7.95}{5}$ G	$\frac{7.41}{5}$ ob.
------------------------	--------------------------	-----------------------	-------------------------	-----------------------	-------------------------	-----------------------	-------------------------

359.34

14+33 35° Lt. = Cl. E.C.

+94° Cont.

13+94° 84.3 Rt. = Cl. E.C.
14.5 Lt. = Cl. B.C.

13+60

13+46

P.O.C. 90° to Sta. 15+18 ~~70~~
N.E. Ref 47 ^{Monroe} + Euclid 51' long from.

359.34

353.07. 4.27 35.2 00.	357.57. 4.77 35.2 0.	359.99. 4.95 25	353.99. 5.35	353.72. 5.62 15	358.69. 5.65 25	353.77. 5.57 50			
				351.89. 7.45 84.3 0.	352.33. 7.01. 84.3 0.				
353.22. 6.12 00.	353.70. 6.56 14.8 0.	352.89. 6.45 75	352.80. 6.52	352.62. 6.72 75	352.97. 6.87 75	352.97. 6.97 25	352.01. 7.33 50		
351.76. 7.58 00.	351.31. 8.03 15 0.	351.44. 7.90 75	351.46. 7.88	351.29. 8.05 11	351.18. 8.16 21.8 0.	351.74. 7.60 00.			
351.05. 8.29 00.	350.54. 8.80 15.1 0.	350.71. 8.63 75	350.75. 8.59	350.61. 8.73 85	350.58. 8.76 17 0.	351.06. 8.28 00.			
2.20 1 0.	1.67 1 0.	2.136 2 0.	1.83 2 0.	2.31 3 0.	1.87 3 0.	2.29 4 0.	0.00 4 0.	2.08 5 0.	1.55 5 0.
							E.C. to east.		

359.34

16450

16400

T.P. 6.44 365.15 0.63 358.71

15453 24.9 Lt. = Cl. E.C.

15418 55° Lt. = P.O.C.

14487 15° Rt. = Cl. E.C.

14150 ± 84 Rt. = Cl. D.C. on south.

359.34

B.L.

8

359.58.
5.57
Cl

359.09.
6.06
25
Q

359.15.
6.00
125

358.93.
6.22

359.65.
6.50
75

358.35.
6.80
15
Q

358.88.
6.27
Cl

358.65.
6.50
Cl

358.13.
7.02
25
Q

358.24.
6.91
125

358.00.
7.15

357.69.
7.46
75

357.33.
7.82
15
Q

357.82.
7.33
Cl

357.22.
1.56
Cl
P.C.

357.25.
2.09
24.9
Q

357.24.
2.10
125

357.01.
2.33

356.73.
2.61
75

356.34.
2.00
15
Q

356.85.
2.49
Cl

357.67.
1.67
55
Cl.
P.O.C.

357.14.
2.20
55
Q

357.49.
2.85
25

356.39.
2.95
125

356.15.
3.19

355.87.
3.47
75

355.57.
3.77
15
Q

356.07.
3.27
Cl

354.93.
7.44
153
Q

355.13.
3.91
Cl
E.C.

355.84.
3.46
50

355.90.
4.04
35

355.02.
4.32
20

354.54.
4.80

354.18.
5.16
15

354.15.
5.19
25

354.20.
5.14
50

353.13.
5.61
84
Cl

353.88.
5.46
84
Cl

359.34

Drive

S.E.B.P
Euclid + Monroe

9.64 355.51 (355.48)

N.W. Ret. 48th + Monroe Ad' long Apts

see plans for Rad. P.R.C. etc.
S.W. Ret. 48th + Monroe 50' of Arc.

17+38 25' Lt. = cl. B.C.

17+00 15° Rt. = cl. B.C.

365.15

B.L.

9

4.38	3.94	4.14	3.68	3.77	3.85	3.37	2.95	3.00	2.59
1 G.	1 cl. B.C.	2 G	2 cl.	3 G	3 cl.	4 G	4 cl.	5 G	5 cl. E.C.

5.72	5.25	5.55	5.20	5.46	5.20	5.47	5.12	5.58	5.16
1 B.C. G.	1 B.C. cl.	2 G.	2 cl.	3 G	3 cl.	4 G	4 cl.	5 G	5 B.C. cl.

361.21	360.77	360.79	360.59						
3.94	4.38	4.36	4.56	4.74	4.83	4.99	5.38		
25 cl. B.C.	25 G	125		75	15	25	50		

360.53	360.00	360.07	359.92	359.64	359.48	359.90		
4.62	5.15	5.08	5.23	5.51	5.72	5.25		
cl.	25 G	125		75	15 G	cl. B.C.		

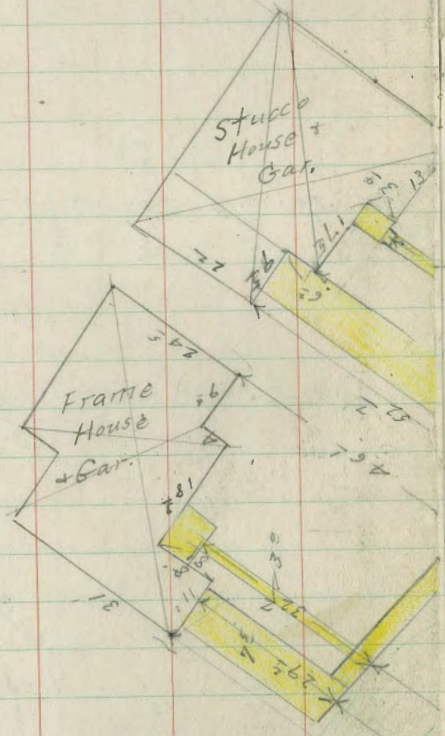
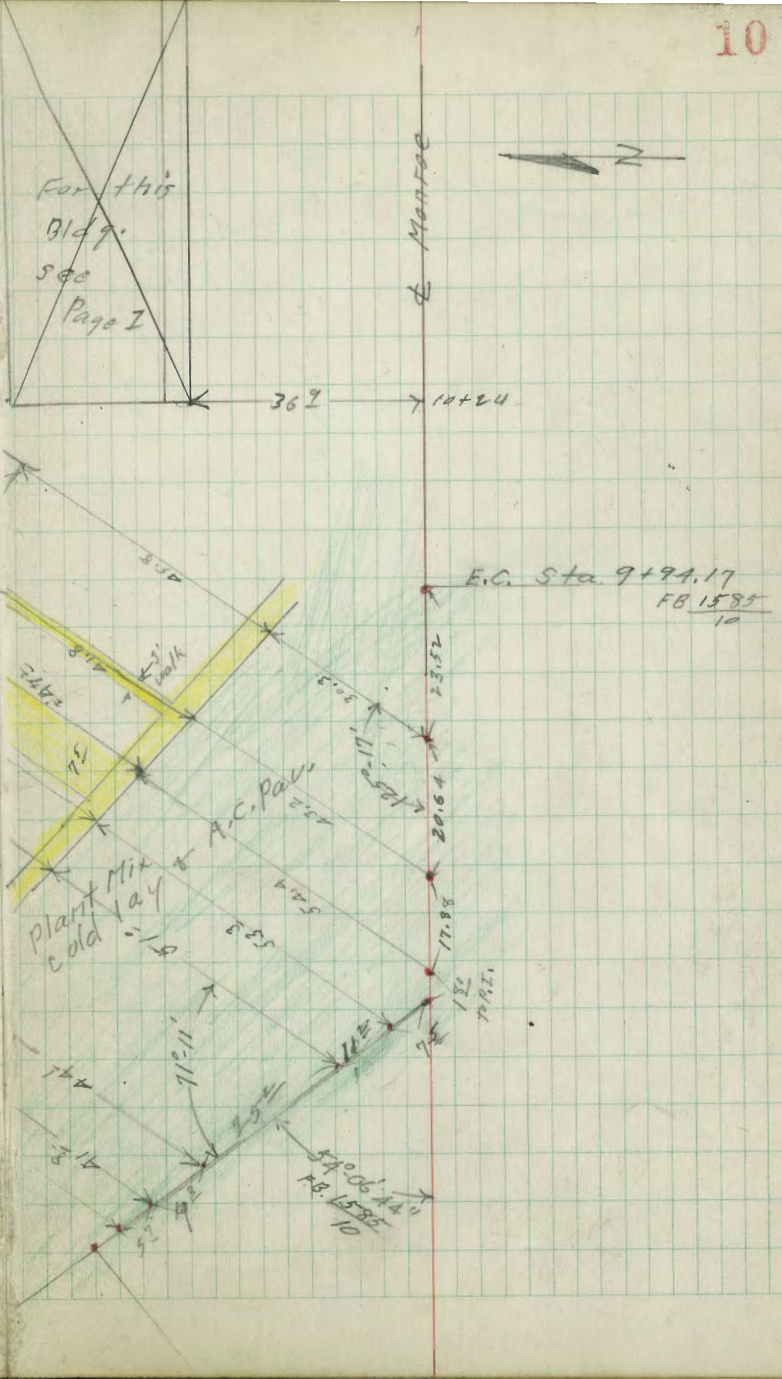
365.15

Location of Houses
Aldine Drive North of Monroe

Simmmermeyer
w/ Moore &
Sherman
5/12/48

W.O. # 21001

INDEXED
WK
'JAN 14 1949



for floor El. see $\frac{1585}{79}$ $\frac{1585}{27}$

$\frac{1585}{32}$

For this
Bldg.
see
Page 1



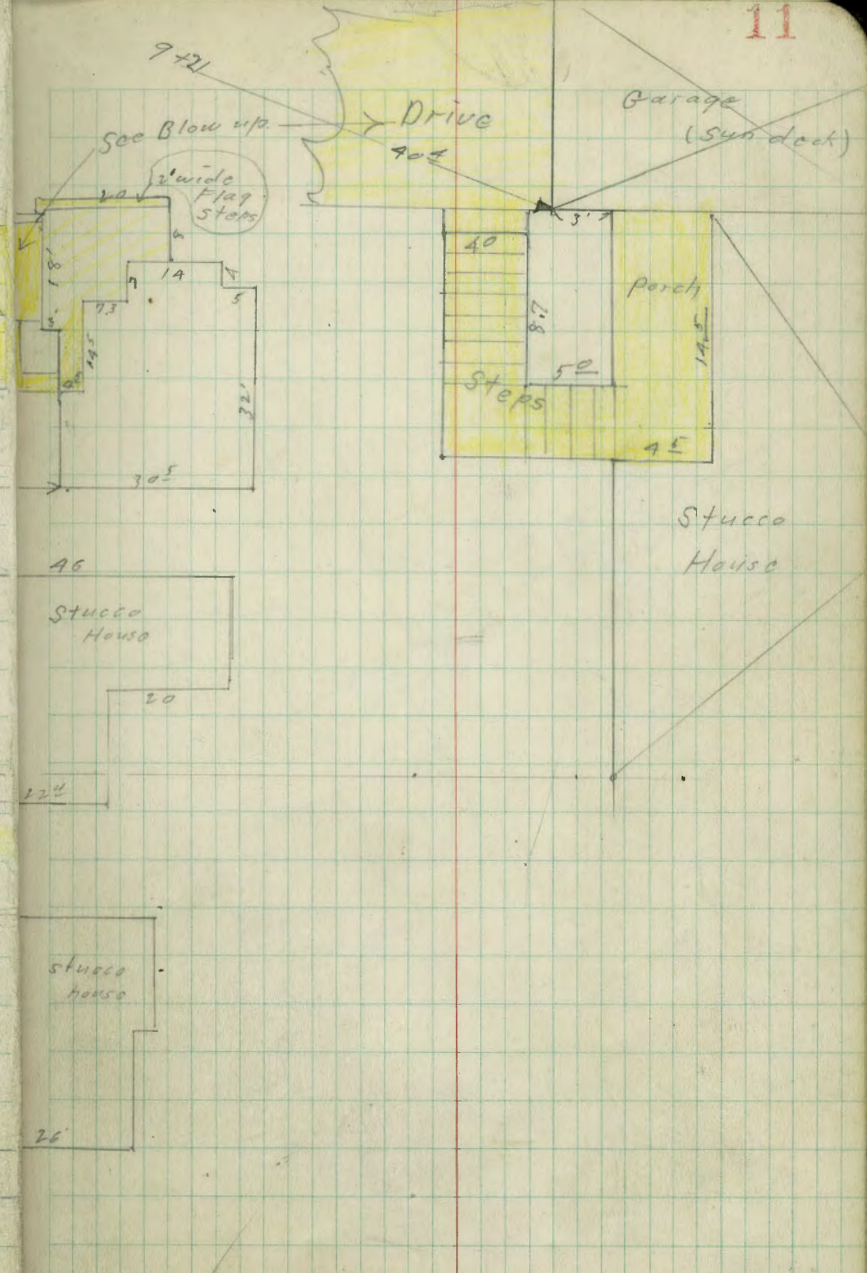
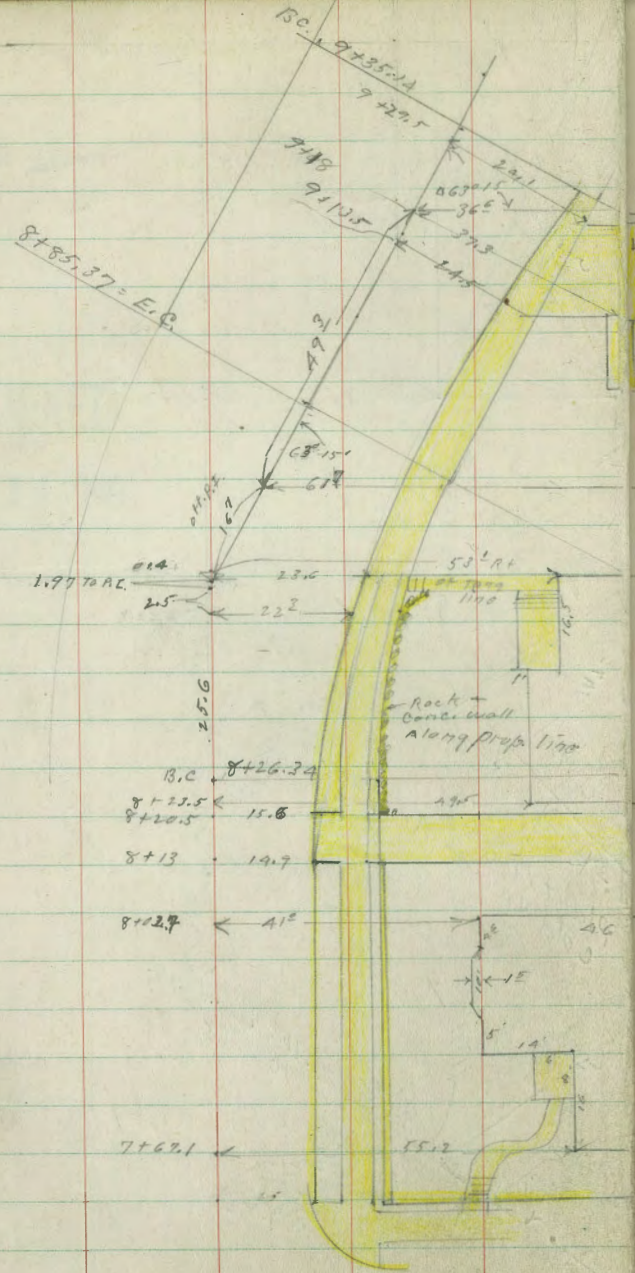
E. Monroe

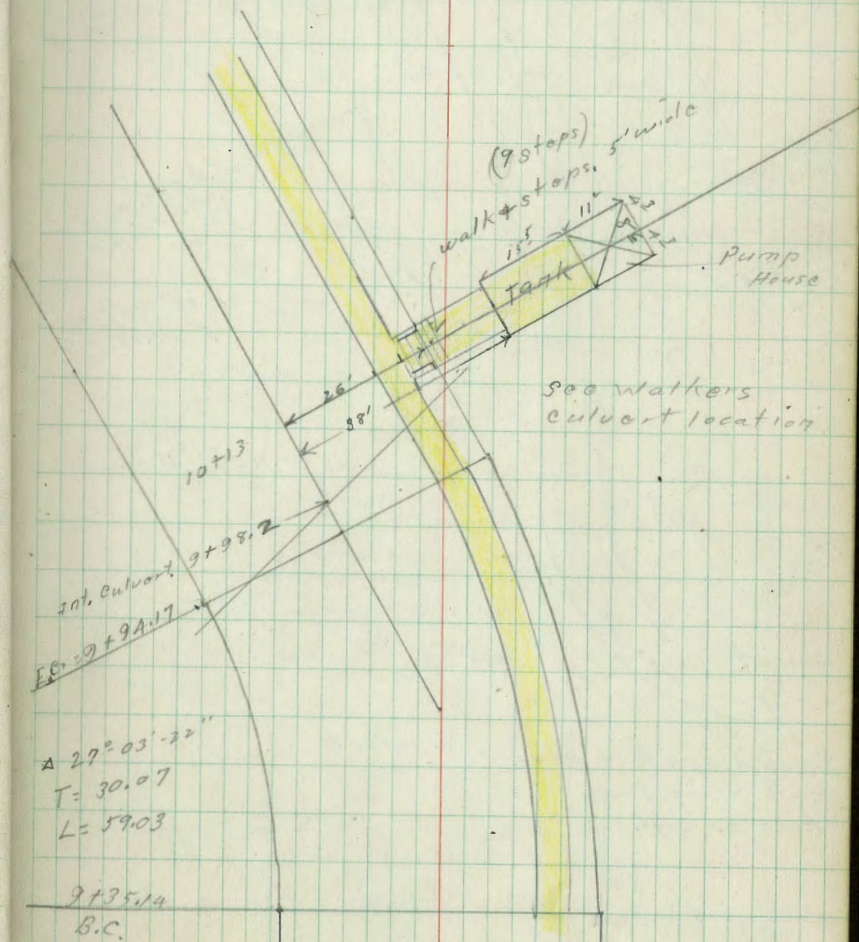
E.C. Sta. 9+94.17
FB 1585
10

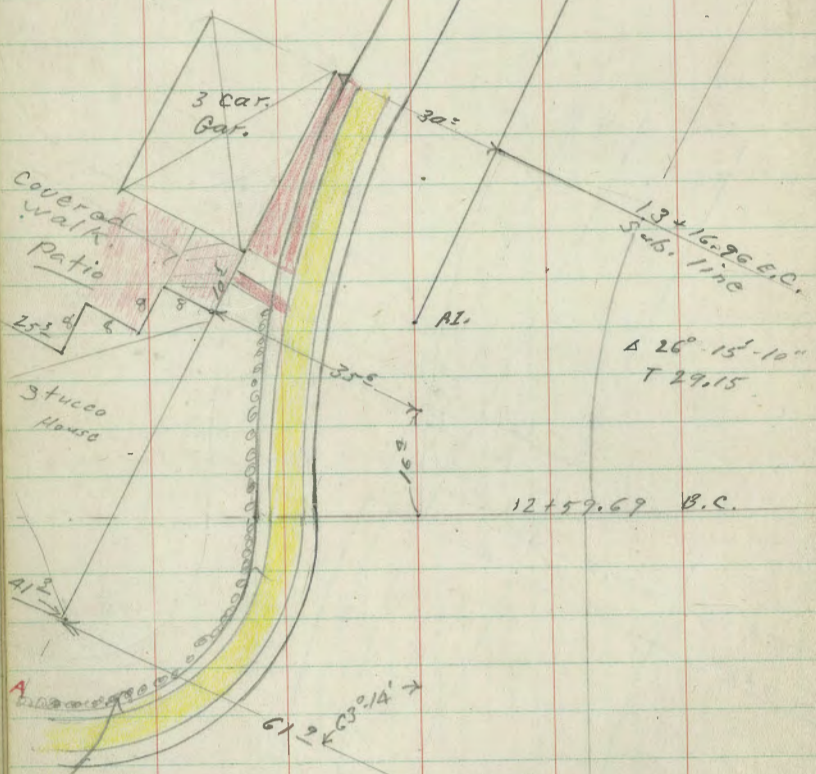
367 14+24

Plumb Mix
A.C. Power
11.91
11.2
11.1
11.0
10.9
10.8
10.7
10.6
10.5
10.4
10.3
10.2
10.1
10.0
9.9
9.8
9.7
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1.6
1.5
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1.2
1.1
1.0
0.9
0.8
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0.6
0.5
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0.2
0.1
0.0

5406 140
FB 1585
10

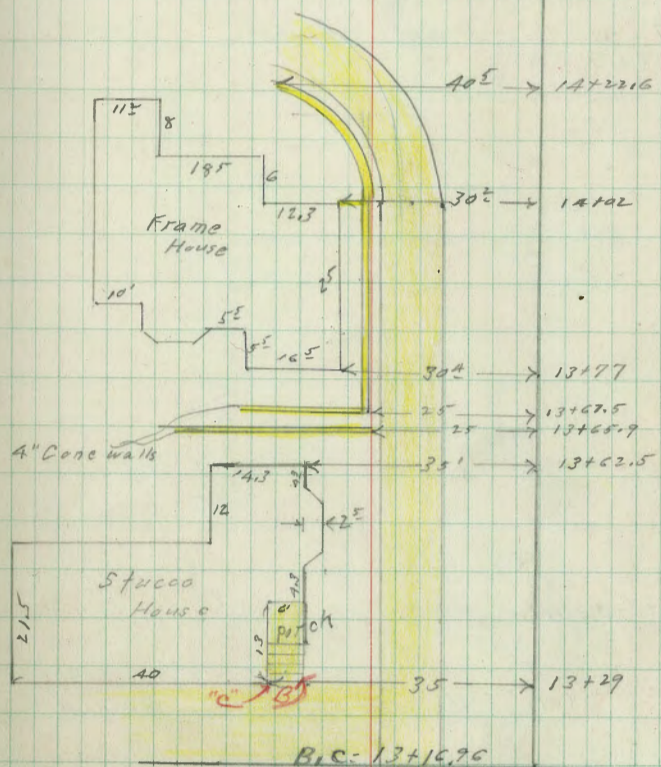






Faced rock + Conc
Wall along Prop. line
Average Hgt. = 2'

11+75.178 - 15.85
4 crosses in P.M.



Monroe.

T.P. 7.90 348.43 10.07 340.53

+02.7 Cont.

8+02.7 41° N.E. Cor. house

7+83

7+80

7+67^{1/2} Cont.

7+67^{1/2} (Page 11) 55² = N.W. Cor. House

7+60 = 2 9" wide N. & S. Corner wall
 24.2 R.N. - start 9" wide corner wall, also
 SE. B.R. Monro
 + Monroe 6.98 350.60 - 343.62

345.9
 4.7
 35
 346.9
 3.7
 41
 AT HOUSE

341.87
 8.73
 14.7
 06
 341.9
 8.7
 24.8
 Ord.
 341.1
 9.5
 24.8
 Base
 wall
 + Ord.
 342.9
 7.68
 24.9
 top
 wall
 + Ord.

342.91
 7.69
 06
 15
 343.0
 7.6
 24.5
 wall
 + Ord.
 343.78
 6.82
 24.7
 wall
 + Ord.
 346.5
 4.1
 34
 347.5
 3.1
 41
 AT
 House

350.14
 0.46
 55
 on porch
 350.34
 0.36
 55
 Floor
 level

343.48
 7.12
 15
 06
 343.9
 6.9
 24.6
 Ord.
 344.51
 6.09
 24.7
 wall
 + Ord.
 347.3
 3.3
 35
 348.5
 4.1
 55

343.74
 6.86
 06
 344.1
 6.5
 24.5
 Ord.
 343.7
 6.9
 24.6
 Bottom
 wall
 344.78
 5.82
 24.7
 top
 wall
 + Ord.
 345.55
 5.05
 40
 top
 wall
 + Ord.

350.60

Rock + Conc. walk

4^E Back of P.I. (Page 11) 28^E Rt. = End8+23^E 49^E Rt. N.W. Cor. house8+20^E Cont.8+20^E East edge Conc. Dr.

8+13 Cont.

west edge conc. Dr.

8+13 248 Rt. = End conc. wall, also =

348.43

337.92	340.07
10.51	8.36
28.9	2.7
walk +	top
Base wall	wall

341.8
0.6
49.5
Floor level

344.23	346.05	346.49
1.20	2.38	1.94
37	49.5	60
drive	drive	drive

340.57	340.56	340.82	342.13
7.72	7.87	7.61	6.30
15.6	24.8	24.8	25.5
ok	walk	edge	top
	+ Base	drive	wall
	wall		

344.46	344.93	346.03	346.45
5.97	3.50	2.40	1.98
24.8	70	49	60
Edge	drive	drive	drive
drive	end	end	

341.33	341.3	340.8	341.95
7.10	7.1	7.6	6.48
14.8	24.8	24.8	24.8
ok	end	Base	top
		wall	wall

348.43

9+29^E 24^L Rt. = N.E. Cor. drive

9+21 40^L Rt. = N.W. Cor. Ber.

9+18 = Bottom of steps on drive (P.11)

9+13^E Cont.

9+13.5 24^E Rt. = N.W. Cor. Conc. Dr.

T.P. 4.85 340.31 12.97 33546

8+85²⁷ E.C.

P.I. - 2^o = \neq 3' conc. walk + steps 31^o Rt.

348143

332.64

7.67
24.1
drive

335.21

5.10
40.4

335.06

5.25
37.3

340.1

0.1
39.3
on conc. steps

334.06

6.75
24.5
Drive

335.3

5.0
25

338.7

1.6
33

340.0

0.3
39

340.311

336.09

12.34
17.9
06

336.2

12.2
25
ord

340.0

8.4
32
ord

341.7

6.7
75

338.23

10.20
31.9
Bottom
stop

340.22

8.21
34.4
start
walk

342.63

5.80
49
N.E. Cor.
porch steps

T.P.N.E. Cor. Tank 10.48 333.96 10.50 323.48

± 8⁵ wide pump house

steps: 38⁵ = ± 8⁵ wide tank. 54² =

10+13 20' Rt. = ± 5' walk, 26 Rt. = start 5' wide

10+08

9+94¹⁷ E.C.

Sec. at P.I. on split of Δ

T.P. 3.90 333.98 10.23 330.08

Flag stone steps.

9+35¹⁴ B.C. 30⁵ Rt. = wedge 2' wide

9+33⁵ 33⁴ Rt. = N.E. Cor. Gate.

340.31

329.19
4.80
20
329.31
4.61
20
329.48
10.50
38.8
on tank
Bottom
steps
329.53
10.45
34.3
at pump
House

328.91
5.07
15
cc
329.12
4.86
20
329.3
4.7
25
329.4
11.1
40
329.5
11.0
41
329.6
14.5
160

328.95
5.03
15
cc
329.1
4.9
20
329.0
5.0
31
321.0
13.0
55
321.0
13.0
70

330.03
3.75
14.2
cc
330.78
3.70
17.2
walk
+ dirt
332.4
1.6
40
335.0
4.142
52.

332.17
8.14
18.8
cc
332.30
8.01
23.8
walk
and
334.4
5.9
30
335.0
5.3
30.5
on
1107
steps

335.17
5.14
33.4
Floor

at top

Wall follows property line 6" wide

12+33^e 60.8 Lt. = wall at 'A' Page 13 Lt.

343.6	343.6	341.1	341.6
6.0	6.0	8.5	8.0
Ord Back of wall 60.8	Top wall 60.8	Base wall 60.8	Ord. at walk 60.8

349.61

T.P. 11.69 349.61 2.77 337.92

11+47^z - W. Edge W. Walk 47th St. to south

335.87	337.03	332.80
4.82	3.66	1.89
24.3 00	41 walk + Ord.	60 walk + Ord.

14+24 15 Rt. = Approx. Cb. B.C.

334.04	334.3	335.1	338.8
6.61	6.4	5.5	1.7
15 00	20	47	60

11+00

332.70	333.1	334.3	338.3	340.3
7.24	7.6	6.4	2.4	0.4
15 00	20	35	45	60

10+60

330.20	331.1	336.7	336.0	336.7
2.88	2.6	4.0	4.7	1.0
15 00	20	28	40	55

T.P. 9.89 340.69 3.16 330.80

340.69

10+26

341.23	341.5	340.8	343.2	341.7
7.73	1.5	4.2	10.8	12.3
15 00	20	25	38	55

333.96

333.96

30 Lt. = S.W. Cor. Gar.
 walk + start brick ramp to 3 car. Gar.
 90° to P.I. (on Fwd. tang) 21 Lt. = inside

= 205 Lt. = 3' wide brick walk.
 3' ahead of P.I. on back tang. produced

90° to back tang.
 2' ahead of P.I. on back tang. produced
 = End of wall 21.7 Lt.

12 + 57^E 25² Lt. = line of wall

+ 44^E Cont

12 + 44^E Lt. at 90° = S.W. Cor. house

349.61

340.50
 1.11
 30
 Car.

346.95
 2.66
 21
 Walk +
 Ramp

347.87
 1.79
 IN
 Patio

347.54
 2.02
 2 walk
 at house

346.37
 3.24
 20.5
 2 end
 walk

346.6
 3.0
 22
 Ord

346.8
 2.8
 21.7
 TOP
 wall

345.6
 4.0
 21.7
 Base
 wall

346.2
 3.4
 21.7
 Ord.

344.7
 4.9
 26
 Ord

344.7
 7.9
 25.4
 TOP
 wall

342.7
 6.9
 25.3
 Base
 wall

343.2
 6.4
 25.3
 Ord

347.7
 1.9
 55.6
 Floor
 1348

344.8
 4.8
 53.6
 Ord
 at
 House

344.0
 5.6
 51
 Ord

344.0
 5.6
 30.3
 TOP
 wall

344.5
 8.1
 308
 Base
 wall

342.0
 7.6
 30
 Ord

342.3
 7.48
 29.2
 Back
 edge
 walk

342.35
 7.26
 18.7
 06

349.61

+65² Cont.

Mortgage

13+65² 25' Lt. = 4" wide N+S. Conc. wall.

13+40 40⁹ Lt. on porch + door sill.

drive

13+29 = East line drive, 25' Lt. = S.E. Cor

S.W. Cor Conc. Dr.

13+16.96 = E.C. 24.8 Lt. = Back edge walk &

wide N+S. Conc. wall. 26⁵ Lt. = start wall
0.3 west (on Tang) of E.C. (13+16.96) = 6"

T.P. 8.29 957.13 0.77 348.84

+ 3 car Gar.

1' west of E.C. (13+16.96) = End brick ramp

349.61

B.L.

20

	3.85	4.13		
	35	35		
	Base wall	top wall		
			352.12	
4.14	4.47	5.13	5.01	
35	25	25	25	
Grd	top wall	Base wall	Grd + walk	
	545.0		545.4.3	
	2.1	2.035		
	40.8	40.8		
	Floor level at house	porch		
	351.75			
	5.39	5.58	6.25	7.30
"0"	40.8	35	30	25
	P.13	"B" page	drive	drive
	35	13 ft.		
	352.10	351.72	350.88	349.83
	5.03	5.41	6.64	7.85
	55	31	30	24.8
	on drive	on drive	on drive	on drive
	350.91	350.91	348.65	
	6.24	6.24	8.58	
	top wall at Gar	top wall	Bottom wall on drive	
	30			
			<u>357.12</u>	
	1.10	1.14	0.44	
	30	28.5	28.9	
	End ramp		S.E. Cor Ramp	
	S.E. Cor Gar.			

14702 Cont.

3" wide N.T.S. Conc. wall.

cor. Jog in house. also = \pm

14702 25' Lt. = face wall, 30' Lt. = S.E.

13795 = B.C. Lt. of wall

13777 = S.W. Cor. house

+67^E Cont.

also = start E+W. wall.

13767^E 25' Lt. = \pm 4" wide Conc. N.+S. wall

357.13

354.46.
2.67
30.2
Top
wall

353.83.
3.5
30.2
Base
wall

354.33.
2.8
30.2
Grd

354.33.
2.8
25
Grd

354.88.
2.75
25
Top
wall

353.61.
3.52
25
wall

353.130
3.2
25.5
Grd

353.65.
4.1
25
Base
wall

354.11.
3.02
25
Top
wall

353.33.
3.80
25
wall

356.93.
0.7
30.4
Flwr
total

353.33.
3.8
30.
Grd

353.13.
4.0
25.3
Grd

353.26.
3.87
25
Top
wall

352.62.
4.51
25
wall

353.44.
3.67
35
Top
wall

352.63.
4.51
35
Base
wall

353.13.
4.0
35
Grd

352.83.
4.3
25.4
Grd

352.83.
4.30
25
Top
wall

351.93.
5.2
25
Base
wall

352.20.
4.23
25
wall +
Grd.

357.13

Monroe

B.L

22

S.E.B.P. Euclid + Monroe 1.65 355.48 (355.48)

40.5 ft = End wall.

1A+22E 2.45 = cl.

357.13

354.83. 2.3 40.5 Base wall	355.17. 1.96 40.5 End wall top wall ↓ Grd.	355.13. 2.00 40.5 or walk	357.45. 2.68 40.5 cl.
--	--	---------------------------------------	--------------------------------

357.13

Monrovia + Aldine Drive
Additional Levels
Sketch Page 23

F

E - Conc Walk

D

INDEXED
WK
JAN 14 1949

C

B

A

B.M.

0.63

329.57

327.94

S.F.B.P.
Monrovia 47-4

24

329.17

8.8
0.0

329.38

9.19

0.0 = 5 ft Conc
Walk

329.47

9.1
0.0

329.47

9.1
0.0

329.44

9.13
1.00 = 5 ft Conc
Slab

329.17

9.10
0.00 on Conc
Drive

B.M.

0.63

329.57

327.94

S.F.B.P.
Monrovia 47-4

329.57

8.8
1.0

329.27

8.30
1.00 on Conc
Walk

330.37

8.6
1.0

330.17

8.4
1.0

330.48

8.09
1.00 on Conc

330.20

8.37
1.00 on Conc
Drive

328.57

330.97

7.6
0.0

330.97

7.60
2.00 on Conc
Walk

330.87

7.7
0.0

330.97

7.6
0.0

331.22

7.35
1.75 = 5 ft Conc

331.39

7.18
18.5 = 5 ft Conc
Slab

331.57

7.0
0.0

331.57

7.60
2.00 on Conc
Walk

331.57

7.0
0.0

331.77

6.8
0.0

331.47

7.1
2.0

331.39

7.18
18.5 = 5 ft Conc
Slab

332.17

6.4
0.5 = 5 ft Stucco
House

331.58

6.99
2.00 = Conc Walk
Bottom Step

331.57

7.0
0.0 = 5 ft Stucco
House

332.37

6.2
1.0

332.02

6.55
2.00 on Conc
Walk

331.39

7.18
18.5 = 5 ft Conc
Slab

Reduced
2-16-49
C.J.K.

10+87.21 = EC Prepared

10+77.21

10+67.21

10+57.21

10+47.21

10+37.21

33857

H=H

332.57
6.0
7.5 = 5/4 Storage
Stop

332.78
5.79
0.79 = H.C.

331.77
6.80
19.2 = 5/4 Storage
Stop

331.65
6.99
7.0 = 0.79 on Con

332.27
6.30
6.0 = 5/4 Con + 5/4 S
H

331.71
6.86
19.1 = 5/4 Storage
Stop

331.59
6.98
7.0 = 0.79 on S

331.87
6.70
6.0 = 5/4 Con + 5/4 S
H.C.

331.66
6.91
19.2 = 5/4 Storage
Stop

331.59
6.98
7.0 = 0.79 on S

331.58
6.99
7.0 = 0.79 on S

331.91
7.70
7.0 = 5/4 Con + 5/4 S
H.C.

331.57
7.00
11.5 = 5/4 Storage
Stop

331.77
7.10
7.0 = 0.79 on S

330.82
7.75
7.0 = 5/4 Con + 5/4 S
H.C.

331.55
7.02
11.7 = 5/4 Storage
Stop

331.71
7.10
7.0 = 0.79 on Con

330.91
8.26
7.0 = 5/4 Con + 5/4 S
H.C.

33857

11+60.7 = W C6 of 17th St

11+47.21

TP 8.18 346.12 346.75 0.63 338.57 SEBP Monroe +47

11+37.21

11+27.21

11+17.21

11+07.21

10+97.21

338.57

339.60.
 340.23.
 339.01.
 337.64.
 338.51.
 339.74.
 337.58.
 338.71.
 337.28.
 337.91.
 6.5/40-Top Corn
 7.1/30-Top Field Corn
 7.6/20-Top Field Corn
 8.5/10-Top Pen
 8.8/00-Top Pen
 340.02.
 340.45.
 339.52.
 340.45.
 339.02.
 340.45.
 338.22.
 338.95.
 337.17.
 337.95.
 9.00
 10.00
 07 Cops
 07 Halls
346.75 346.12
 19.33
 66.67
 07 Larr
 337.77.
 0.8
 11.45
 1/8
 337.67.
 0.8
 1/8
 336.07
 2.5
 6.00
 07 Larr
 339.27.
 1.3
 11.4
 5/8
 337.17.
 1/8
 336.07
 336.47.
 1.1
 11.4
 5/8
 336.37.
 4.8
 1/8
 335.27.
 3.5
 07 Larr
 336.47.
 334.97.
 335.82.
 11.75
 5/8
 334.97.
 333.67.
 1.9
 10.00
 07 Larr
 334.97.
 333.67.
 1.9
 10.00
 07 Larr
 338.57

Euclid and Monroe
Levels on 10' grid plus
side shots on cb. B.C. etc.

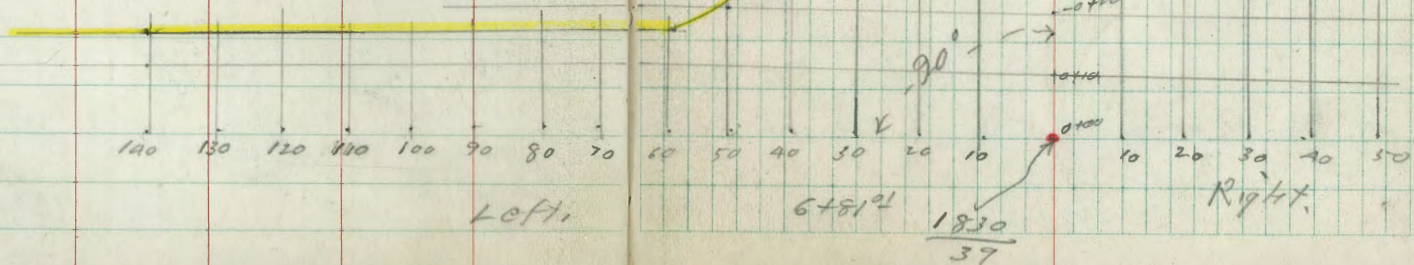
1-24-49
W.O. 60264

Sommermeier
McCoy
Jones

INDEXED
WK
JAN 26 1949

Levels P. 29-33

$$\begin{array}{r} \text{E } 0+00 = 6+81 \text{ 01} \\ \text{FB } 1830 \\ \hline 39 \end{array}$$



Sly from & Monroe

28

E. Euclid to South

1+25

1+20

1+10

1+05

1+00

0+90

0+80

0+70

0+60

0+50

0+40

0+30

0+20

0+10

0+00

90°

6+81 01

$$\begin{array}{r} 1830 \\ \hline 39 \end{array}$$

Right.

Sketch - Page 28

0 + 10 cont.

0 + 10 Cont.

0 + 10

0 + 00 Cont.

0 + 00 Cont.

0 + 00 = £ Monroe (P. 28)

SE.B.P.
 Monroe
 Euclid

4.50 359.98 ← - 355.48

Reduced 1-26-99
 C. Lawrence

356.66
 $\frac{8.32}{1405}$

356.46
 $\frac{3.52}{130}$

356.22
 $\frac{3.76}{120}$

356.02
 $\frac{3.96}{110}$

355.79
 $\frac{4.19}{100}$

355.55
 $\frac{4.43}{70}$

355.34
 $\frac{4.62}{79.82}$

355.09
 $\frac{4.89}{70}$

354.90
 $\frac{5.08}{60}$

354.65
 $\frac{5.33}{50}$

354.50
 $\frac{5.48}{70}$

354.27
 $\frac{5.71}{30}$

353.97
 $\frac{6.01}{20}$

353.69
 $\frac{6.29}{10}$

357.06
 $\frac{2.72}{1405}$

356.90
 $\frac{3.08}{130}$

356.65
 $\frac{3.33}{120}$

356.40
 $\frac{3.58}{110}$

356.20
 $\frac{3.78}{100}$

355.92
 $\frac{4.06}{90}$

355.64
 $\frac{4.34}{79.82}$

355.37
 $\frac{4.61}{70}$

355.15
 $\frac{4.83}{60}$

354.96
 $\frac{5.02}{50}$

354.79
 $\frac{5.19}{40}$

354.55
 $\frac{5.42}{30}$

354.20
 $\frac{5.78}{20}$

353.89
 $\frac{6.09}{10}$

359.98

0 + 14²0 + 14⁶0 + 14⁵0 + 14⁴0 + 14³0 + 14²0 + 14¹

$$\begin{array}{r} 355.94 \\ 4.54 \\ 70 \\ 06 \end{array}$$

$$\begin{array}{r} 354.92 \\ 5.06 \\ 70 \\ 06 \end{array}$$

$$\begin{array}{r} 355.14 \\ 4.84 \\ 7933 \\ 06 \end{array}$$

$$\begin{array}{r} 355.65 \\ 4.33 \\ 7933 \\ 70 \end{array}$$

$$\begin{array}{r} 356.08 \\ 3.90 \\ 100 \\ 06 \end{array}$$

$$\begin{array}{r} 355.58 \\ 4.20 \\ 100 \\ 06 \end{array}$$

$$\begin{array}{r} 355.80 \\ 4.10 \\ 90 \\ 06 \end{array}$$

$$\begin{array}{r} 355.34 \\ 4.64 \\ 90 \\ 06 \end{array}$$

356.33

$$\begin{array}{r} 3.65 \\ 110 \\ 06 \end{array}$$

355.83

$$\begin{array}{r} 4.15 \\ 110 \\ 06 \end{array}$$

356.54

$$\begin{array}{r} 3.44 \\ 120 \\ 06 \end{array}$$

356.02

$$\begin{array}{r} 3.96 \\ 120 \\ 06 \end{array}$$

356.74

$$\begin{array}{r} 3.24 \\ 130 \\ 06 \end{array}$$

356.24

$$\begin{array}{r} 3.74 \\ 130 \\ 06 \end{array}$$

356.99

$$\begin{array}{r} 3.99 \\ 1405 \\ 06 \end{array}$$

356.51

$$\begin{array}{r} 3.47 \\ 1405 \\ 06 \end{array}$$

359.98

0+40

0+30 Cont

0+30

0+20 Cont.

0+20

0+152

354.83.

$$\begin{array}{r} 5.25 \\ 352 \\ \hline 26 \end{array}$$

354.28.

$$\begin{array}{r} 5.70 \\ 352 \\ \hline 6 \end{array}$$

354.18.

$$\begin{array}{r} 5.80 \\ 30 \\ \hline 20 \end{array}$$

353.85.

$$\begin{array}{r} 6.03 \\ 20 \\ \hline 10 \end{array}$$

353.63.

$$\begin{array}{r} 6.32 \\ 10 \\ \hline 10 \end{array}$$

353.27.

$$\begin{array}{r} 6.71 \\ 10 \\ \hline 10 \end{array}$$

352.83.

$$\begin{array}{r} 7.15 \\ 20 \\ \hline 20 \end{array}$$

352.43.

$$\begin{array}{r} 7.55 \\ 20 \\ \hline 30 \end{array}$$

351.98.

$$\begin{array}{r} 8.00 \\ 30 \\ \hline 6 \end{array}$$

351.62.

$$\begin{array}{r} 8.36 \\ 398 \\ \hline 6 \end{array}$$

352.15.

$$\begin{array}{r} 7.83 \\ 398 \\ \hline 26 \end{array}$$

351.52.

$$\begin{array}{r} 8.46 \\ 49.1 \\ \hline 6 \end{array}$$

352.64.

$$\begin{array}{r} 7.94 \\ 49.1 \\ \hline 26 \end{array}$$

354.94.

$$\begin{array}{r} 5.04 \\ 40.3 \\ \hline 26 \end{array}$$

354.40.

$$\begin{array}{r} 5.58 \\ 40.3 \\ \hline 6 \end{array}$$

354.12.

$$\begin{array}{r} 5.86 \\ 30 \\ \hline 20 \end{array}$$

353.81.

$$\begin{array}{r} 6.11 \\ 20 \\ \hline 10 \end{array}$$

353.61.

$$\begin{array}{r} 6.37 \\ 10 \\ \hline 10 \end{array}$$

353.29.

$$\begin{array}{r} 6.69 \\ 10 \\ \hline 10 \end{array}$$

352.88.

$$\begin{array}{r} 7.18 \\ 20 \\ \hline 20 \end{array}$$

352.57.

$$\begin{array}{r} 7.41 \\ 20 \\ \hline 30 \end{array}$$

352.19.

$$\begin{array}{r} 7.27 \\ 30 \\ \hline 40 \end{array}$$

351.80.

$$\begin{array}{r} 8.18 \\ 40 \\ \hline 26 \end{array}$$

355.88.

$$\begin{array}{r} 4.75 \\ 50.6 \\ \hline 26 \end{array}$$

354.71.

$$\begin{array}{r} 5.27 \\ 50.6 \\ \hline 6 \end{array}$$

354.71.

$$\begin{array}{r} 5.27 \\ 50 \\ \hline 20 \end{array}$$

354.37.

$$\begin{array}{r} 5.61 \\ 40 \\ \hline 30 \end{array}$$

354.12.

$$\begin{array}{r} 5.86 \\ 30 \\ \hline 20 \end{array}$$

353.79.

$$\begin{array}{r} 6.19 \\ 20 \\ \hline 10 \end{array}$$

353.59.

$$\begin{array}{r} 6.39 \\ 10 \\ \hline 10 \end{array}$$

355.35.

$$\begin{array}{r} 4.63 \\ 60 \\ \hline 26 \end{array}$$

354.82.

$$\begin{array}{r} 5.16 \\ 60 \\ \hline 6 \end{array}$$

359.98

1+00

354.02.	353.51.	353.42.	353.28.	353.05.	352.64.	352.25.	351.98.	352.43.
$\frac{5.96}{302}$	$\frac{6.17}{302}$	$\frac{6.56}{20}$	$\frac{6.70}{10}$	6.93	$\frac{7.34}{10}$	$\frac{7.73}{20}$	$\frac{8.00}{2}$	$\frac{7.55}{257}$
cc	G						G	cc

0+90

353.59.	353.58.	353.40.	353.12.	352.65.	352.22.	351.88.	352.35.
$\frac{6.39}{302}$	$\frac{6.40}{20}$	$\frac{6.58}{24}$	6.86	$\frac{7.33}{10}$	$\frac{7.76}{20}$	$\frac{8.10}{20}$	$\frac{7.63}{20}$
cc	G					G	cc

0+80

354.27.	353.75.	353.71.	353.50.	353.13.	352.69.	352.18.	351.78.	352.33.
$\frac{7.71}{302}$	$\frac{6.23}{302}$	$\frac{6.27}{20}$	$\frac{6.48}{10}$	6.85	$\frac{7.29}{12}$	$\frac{7.80}{10}$	$\frac{8.20}{200}$	$\frac{7.65}{285}$
cc	G						G	cc

0+75³³

351.77	352.30
$\frac{8.21}{202}$	$\frac{7.68}{262}$
G	cc

0+70

351.46.	353.90.	353.90.	353.81.	353.52.	353.18.	352.72.	352.23.	351.80.	352.29.
$\frac{5.52}{302}$	$\frac{6.08}{302}$	$\frac{6.08}{30}$	$\frac{6.17}{20}$	$\frac{6.46}{10}$	6.80	$\frac{7.26}{10}$	$\frac{7.75}{20}$	$\frac{8.18}{202}$	$\frac{7.67}{262}$
cc	G							G	cc

0+60

354.59.	353.99.	353.99.	353.88.	353.57.	353.20.	352.73.	352.25.	351.71.	352.18.
$\frac{5.39}{318}$	$\frac{5.99}{318}$	$\frac{5.99}{30}$	$\frac{6.10}{20}$	$\frac{6.41}{10}$	6.78	$\frac{7.25}{10}$	$\frac{7.73}{20}$	$\frac{8.27}{292}$	$\frac{7.80}{292}$
cc	G							G	cc

0+50

354.71.	354.15.	354.14.	353.91.	353.61.	353.18.	352.74.	352.30.	351.78.	351.61.	352.12.
$\frac{5.27}{332}$	$\frac{5.83}{332}$	$\frac{5.84}{30}$	6.07	$\frac{6.37}{10}$	6.80	$\frac{7.24}{10}$	$\frac{7.45}{20}$	$\frac{8.20}{30}$	$\frac{8.37}{332}$	$\frac{7.86}{332}$
cc	G							G	G	cc

359.98

orig B.M.
P. 29

4.50 355.48

1+25 30° Lt. = start Next Sv. curb.

1+20

1+10

1+05 N. Alley Cl. to left.

353.87. 6.11 40 Pave.	353.64. 6.34 30° Cl.	353.38. 6.60 30° Cl.	353.42. 6.56 20	353.22. 6.76 10	353.00. 6.98	352.71. 7.27 10	352.30. 7.68 20	352.05. 7.93 25° Cl.	352.55. 7.43 25° Cl.
--------------------------------	-------------------------------	-------------------------------	-----------------------	-----------------------	-----------------	-----------------------	-----------------------	-------------------------------	-------------------------------

353.24. 6.24 40	353.37. 6.61 30	353.36. 6.62 20	353.15. 6.93 10	352.92. 7.06	352.61. 7.37 10	352.28. 7.70 20	352.08. 7.90 25° Cl.	352.54. 7.44 25° Cl.
-----------------------	-----------------------	-----------------------	-----------------------	-----------------	-----------------------	-----------------------	-------------------------------	-------------------------------

353.74. 6.24 10	353.45. 6.53 30	353.28. 6.70 20	353.15. 6.83 10	352.89. 7.09	352.60. 7.38 10	352.25. 7.73 20	352.06. 7.92 25° Cl.	352.50. 7.48 25° Cl.
-----------------------	-----------------------	-----------------------	-----------------------	-----------------	-----------------------	-----------------------	-------------------------------	-------------------------------

354.03. 5.95 40° End Cl.	353.88. 6.10 45° Cl.	353.99. 5.99 32° Cl.	353.65. 6.33 32° Cl.	353.99. 6.49 30° Pave. Cl. P.T. 2' Rad
--------------------------------------	-------------------------------	-------------------------------	-------------------------------	---

359.98

Sketch P. 38

0+50

0+40

0+30

0+20

0+10

0+00 = \perp Monroe 18³ East'y of \perp Euclid
 Δ off \perp Monroe to East = $50^{\circ} 32' 47''$

S. E. B. P.
 Euclid \pm
 Monroe

5.61 361.09

355.48

34

355.91.	355.72.	355.51.	355.67.	R.L.	355.77.	355.87.	355.83.	355.74.	355.75.	355.83.
5.18	5.67	5.58	5.42	5.30	5.22	5.16	5.35	5.34	5.20	5.20
249	249	20	10	10	20	20	30	40	40	50
00	0									

355.50.	35490.	355.12.	355.27.	355.40.	355.47.	355.45.	355.42.	355.45.
5.59	6.11	5.77	5.82	5.69	5.62	5.64	5.67	5.64
232	232	20	10	10	10	20	30	40
00	0							

355.12.	354.61.	354.66.	354.89.	355.03.	355.47.	355.09.
5.27	6.48	6.43	6.20	6.06	6.04	6.00
221	221	20	10	10	10	20
00	0					

354.73.	354.16.	354.22.	354.44.	354.63.	354.74.
6.36	6.73	6.87	6.60	6.46	6.35
210	210	20	10	10	10
00	0				

354.26.	353.88.	353.86.	354.08.	354.25.
6.83	7.21	7.23	7.01	6.84
222	222	20	10	
00	0			

353.80.	353.40.	353.57.	353.80.	353.82.
7.29	7.09	7.52	7.29	7.20
268	268	20	10	
00	0			

361.09

0+80 Cont.

0+80

0+76²⁸

curb if built thru drive.
in drive curb rod = top of

0+70 Cont.

0+70

0+60 Cont.

0+60

B. L.

35

	357.07	356.60	356.74	356.86	356.99	357.00	356.86	356.70	356.67	356.65
Drive	4.49	4.35	4.23	4.10	4.09	4.23	4.39	4.42	4.44	
CG	259	259	20	10	70	20	30	10	50	
		Q								

	356.91	356.44
(Curb should be)	4.18	4.65
	260	260
		Q

	356.64	356.16	356.91	356.44	356.61	356.56	356.48	356.36	356.34
	4.45	4.93	4.78	4.62	4.48	4.53	4.61	4.73	4.75
CG	259	259	20	10	10	20	30	10	10
		Q							

	356.15	356.24
Aver. dr. →	4.94	4.85
CG. fac. →	50	60

	355.74	355.88	356.09	356.19	356.17	356.15	356.07	356.05
	5.35	5.71	5.00	4.90	4.92	4.94	5.02	5.04
CG	255	20	10	10	20	30	10	

361.09

1+19.

358.73 ^a	358.17 ^a	358.41 ^a	358.94 ^a	358.39 ^a	358.22 ^a	357.92 ^a	357.69 ^a	358.29 ^a
2.37	2.92	2.68	2.45	2.70	2.87	3.17	3.40	2.86
29 ^o	29 ^o	20	10		10	20	23 ^o	23 ^o
cc	a						a	cc

1+10

358.32 ^a	357.87 ^a	357.97 ^a	358.01 ^a	358.01 ^a	357.92 ^a	357.65 ^a	357.94 ^a	358.04 ^a
2.77	3.22	3.12	3.02	3.02	3.17	3.44	3.65	3.05
27 ^o	27 ^o	20	10		10	20	25 ^o	25 ^o
cc	a						a	cc

1+00 Cont.

357.81 ^a	357.17 ^a
3.28	3.92
82 ^o	82 ^o
cc	a

82^o Rt = Nly. of Morocco.
 1+00 31^o Rt = Ely of Euclid

357.92 ^a	357.44 ^a	357.56 ^a	357.67 ^a	357.67 ^a	357.59 ^a	357.36 ^a	357.16 ^a	357.12 ^a	357.70 ^a
3.17	3.65	3.53	3.42	3.42	3.50	3.73	3.93	3.97	3.39
26 ^o	26 ^o	20	10		10	20	30	31 ^o	31 ^o
cc	a							a	cc

68^o ^{Rt} = Nly. of Morocco (in drive)
 0+90 Cont. 45^o Rt = Ely of Euclid

356.85 ^a	357.43 ^a	356.99 ^a	357.19 ^a
4.24	3.66	4.19	3.70
45 ^o	45 ^o	68 ^o	82 ^o
a	cc	a	

0+90

357.50 ^a	357.03 ^a	357.17 ^a	357.26 ^a	357.34 ^a	357.90 ^a	357.16 ^a	356.99 ^a	356.93 ^a
3.59	4.00	3.92	3.83	3.75	3.79	3.93	4.10	4.16
26 ^o	26 ^o	20	10		10	20	30	40
cc	a							

361.09

17 drive
curb if built thru would be →

1+40

	359.56	359.04	359.14	359.20	359.24	359.06	358.84	358.43	358.39	358.95
Drive	2.05	1.98	1.89	1.85	2.03	2.25	2.66	2.70	2.14	
322	322	30	20	10		10	20	20	20	20
	Q							Q	Q	Q

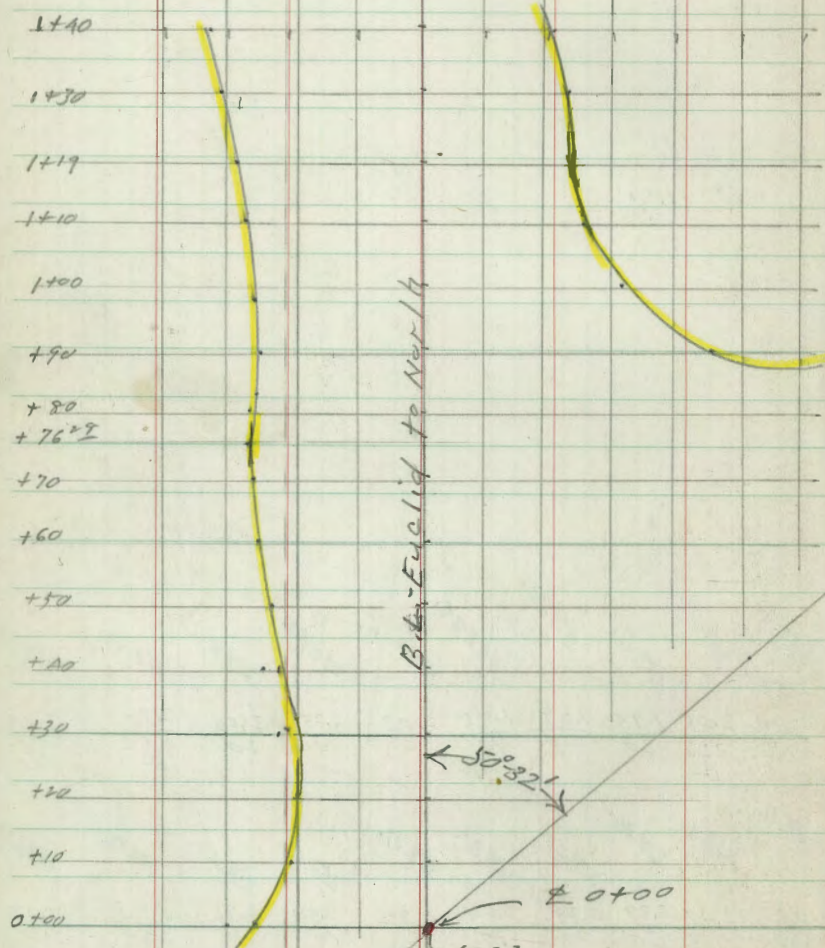
1+30

	359.16	358.62	358.70	358.81	358.86	358.77	358.59	358.23	358.06	358.22
Drive	1.93	2.47	2.39	2.28	2.14	2.32	2.50	2.86	2.03	2.47
308	308	30	20	10			10	20	20	20
Q	Q								Q	Q

361.09

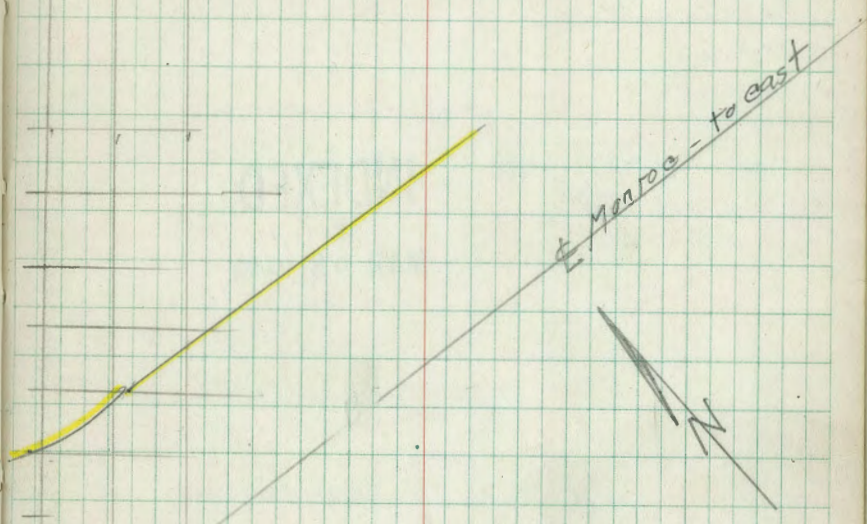
Euclid Nly. from E Monroe

40 ft
30 ft
20 ft
10 ft
B.L.
10 ft
20 ft
30 ft
40 ft
50 ft
60 ft



6+81.01 $\Delta 0^{\circ}04'$ South
 FB $\frac{1830}{39} + \frac{1849}{28}$

70 ft
80 ft
90 ft



Levels P34-37

Alley B1K. 2. Roseville Hqts.

W.O. 25001

3-25-49

Sommermayor
Allen
Jones

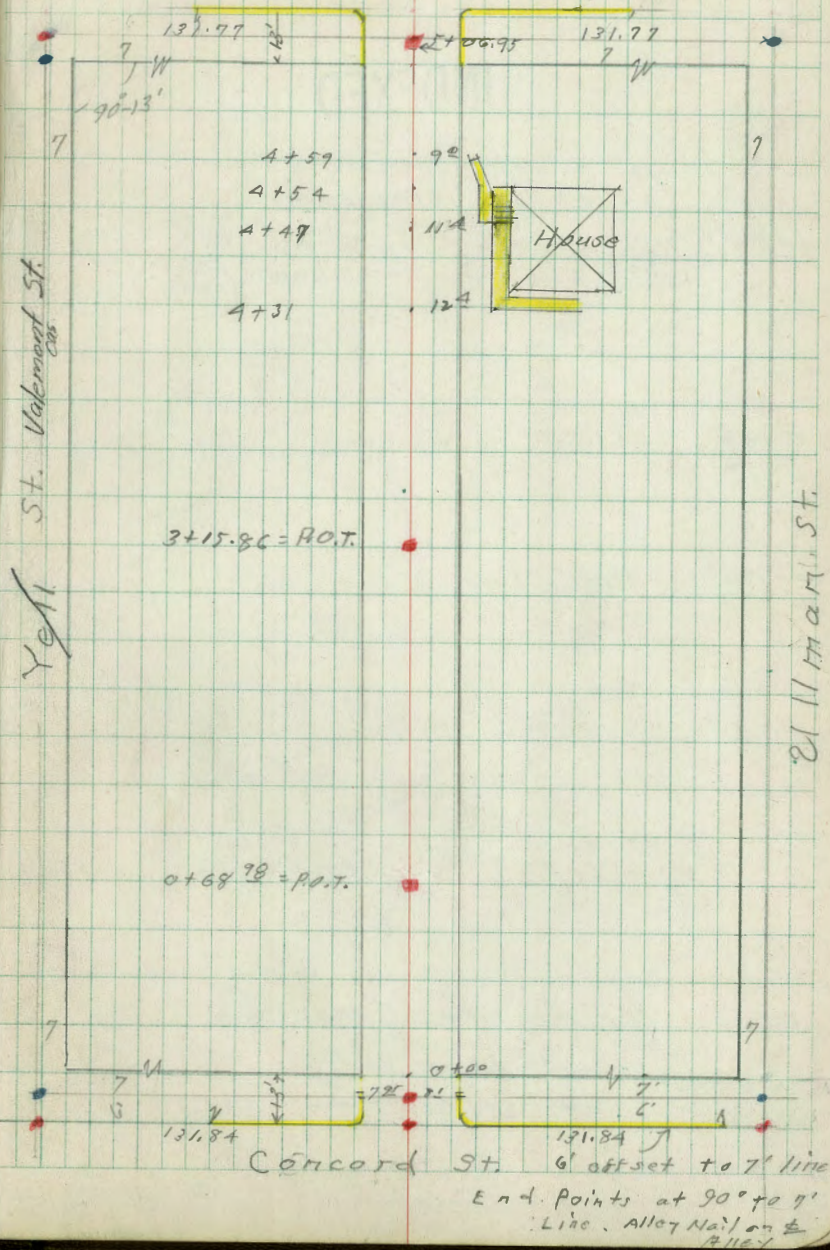
- = Fd. L+T
- = Set Hub
- = Set. Nail

INDEXED
W.K.
MAR 28 1949

Platted 3/30/49, N.F.D.

Bangor St.

39



Alley Bk. 2 Roseville Hqts.

16' wide.

INDEXED

23rd Rt. = start. Gar. Conc. floor.

20th Rt. " Conc. Apron.

0+09 25th Lt. = start Conc. Apron.
28th " " " Gar. Conc. floor.

0+00 = Ely. line Concord

0-06² = 8th Rt. = End Exist Cb.

0-07 = 7th Lt. = End Exist Cb.
End A.C. Pave.

0-10 8th Lt. } = Curb B.C. (Approx. 3' cl. Rad)
8th Lt. }

0-13 Ely cl. line Concord

S.F.B.A. ~~YALL~~ changed to Valemont St.

+ Concord 3.49 238.76 — 235.27

23 6.42	236.12	235.7	234.3	233.5	232.3	231.33	230.57
<u>2.34</u>	<u>2.64</u>	<u>3.1</u>	<u>4.5</u>	<u>4.5</u>	<u>3.5</u>	<u>3.43</u>	<u>3.19</u>
282	252	15	8		8	20 th Apron	23 rd Part Floor
Gar Floor	Apron						

234.8	234.8	233.4	233.4	233.5	234.8	234.8
<u>4.0</u>	<u>4.0</u>	<u>5.4</u>	<u>5.4</u>	<u>5.3</u>	<u>4.0</u>	<u>4.0</u>
10	8	7		4	7	8

232.14
6.62
8th
End. Cb.

232.60	232.28	231.99	231.75	232.13
<u>6.16</u>	<u>6.48</u>	<u>6.77</u>	<u>7.01</u>	<u>6.63</u>
7 th End cl.	7 th G	Pave	8 th G	7 th cl.

232.54	232.18	231.94	231.74	232.10
<u>6.22</u>	<u>6.58</u>	<u>6.82</u>	<u>7.02</u>	<u>6.66</u>
8 th	8 th G	Pave	8 th G	8 th cl. B.C.

232.62	232.16	231.90	231.60	232.05
<u>6.14</u>	<u>6.60</u>	<u>6.86</u>	<u>7.16</u>	<u>6.71</u>
11 th Cb. B.C.	11 th G	Pave	11 th G	11 th cl. B.C.

238.76

1+15 - 55' Rt. = \neq double Gar. Conc. floor.

231.4
5.6
55
Gar. floor.

1+00

231.5 231.2 231.5 232.1 232.2
5.5 5.8 5.5 4.6 4.8
8 8 5 6 8

8' Lt. = End Cold lay apron
24⁰ Lt. = End Gar. - Conc. floor.
9⁵ Rt. = End Conc. Apron.
232 Rt. = End Gar. Conc. floor.

0+69

234.69 233.9 234.06 234.08
2.35 3.1 2.98 2.2
244 8 95 232
Gar. floor Apron Apron Gar. floor

8' Lt. = start Cold lay apron.
24² Lt. = " double Gar. Conc. Floor
92 Rt. = start Conc. Apron.
232 Rt. = " double Gar. Conc. floor.

0+54

234.72 234.6 234.2 234.1 234.5 234.49 234.96
2.32 2.4 2.8 2.9 2.5 2.55 2.18
244 15 8 8 92 92 232
Gar floor Apron Apron Apron Apron Gar. floor

T.P. 2.78 237.04 4.50 234.26

237.04

0+51 9⁵ Rt. = End Conc. block wall

234.8 234.1 240.1
4.0 4.7 +1.3
95 95 95
End. Base of wall

0+30 9⁵ Rt. = start. Conc. block wall.

235.7 234.5 240.1
3.1 4.3 +1.3
95 95 95
End. Base of footing Top of wall.

0+25 282 Lt. = End Gar.
252 Lt. = " Conc. Apron.
20⁵ Rt. = End Conc. Apron
23' " " " Gar.

238.76

236.41 236.12 235.2 235.0 235.7 235.38 235.56
2.35 2.64 3.6 3.8 3.1 3.38 3.20
282 252 8 8 8 201 23
Gar floor Apron Apron Apron Gar. floor

238.76

INDEXED

3+11 15² Rt. = \pm Sing. Gar. Conc. floor. Apron.
12² Rt. = \pm 7² wide Apron. level Conc.

3+00

2+71 13² Lt. = End Car port.

2+53 13² Lt. = start. Conc. Car. port

2+50

2+00

T.P. 1.09 225.70 12.43 224.61

1+50

1+36 40' Lt. = \pm Double Gar. Conc. floor.

237.04

214.22
11.48
12²
Apron

214.66
11.24
15²
Gar. Floor

214.3
11.4
8

214.0
11.7

213.9
11.8
6

214.7
11.0
8

216.10
9.60
13²
Conc.

215.8
9.7
13
End.

216.00
9.70
13²
Conc.

216.4
9.3
13
End.

216.8
8.7
15

217.3
8.4
8

217.4
8.3

217.3
8.4
5

218.4
7.3
8

218.7
7.0
15

220.7
5.0
15

221.4
4.3
8

221.4
4.3
225.70

221.5
4.2
6

222.0
3.7
8

222.5
3.2
15

227.4
9.6
8

227.3
9.7
5

226.7
14.3
4

227.1
9.9

227.4
9.6
6

228.6
8.4
8

229.0
8.0
15

227.89
9.15
40
Conc. Floor.

237.04

3+70 Also = start Conc. block wall.
9th Rt. = End car port (Conc. floor)

3+69⁵ 8th Lt. = \pm 3' wide loose brick walk

3+68 8th Lt. = End brick patio

3+54 8th Lt. = start loose laid brick patio

3+52 8th Lt. = \pm south face of 4' x 4' brick fire place.

3+50 Also = start Conc. Car port
9th Rt. = End Conc. block wall.

3+16 8th Rt. = start Conc. block wall.

3+15.80
T.P. = Rot 0.95 213.60 13.05 212.65

225.70

208.9	209-18	208.9	215.5
4.7	4.42	4.7	+1.9
9.4	9.4	9.4	9.4
Ord.	Conc.	Base	Top
	car	wall	wall
	port.		

208.5
5.1
8.2
2 walk

209.4
4.2
8.2
on patio

209.3
4.3
8.2
patio

209.4	210.3
4.2	3.3
8.4	8.4
Base of	Ord
Fire place	

210.4	210.3	210.4	210.4	210.3	214.5	210.00
3.2	3.3	3.2	3.2	3.3	+0.9	3.52
8		8	8.2	9.2	9.2	9.2
			Ord.	Base	top	Conc.
				wall	wall	car
						port.

213.4	213.0	217.5
0.2	0.6	+3.9
8.4	8.4	8.4
Ord	Base	Top
	wall	wall

213.60

12² Rt. = End. E.+w. walk.
4+54 11³ Rt. = Δ in wall footing

198.8	198.0	198.28
<u>2.0</u>	<u>2.8</u>	<u>2.48</u>
71	114	124
Grnd	Top Footing	End of walk

4+50 3 - 12³ Rt. = End steps + start^(E+w) walk

199.5	198.0	198.31
<u>1.3</u>	<u>2.8</u>	<u>2.45</u>
71	114	124
Grnd	top Footing	End of steps on walk

(Footing is 0.7' deep)

12³ Rt. = start E.+w. steps.
12³ Rt. = End. E.+w. Conc. walk.
4+47 11³ Rt. = start 1' wide wall footing

200.1	200.0	197.6	197.6	200.0	197.88	200.58
<u>0.7</u>	<u>0.8</u>	<u>1.2</u>	<u>1.2</u>	<u>0.8</u>	<u>2.78</u>	<u>0.18</u>
8	4	8	8	114	114	124
				Grnd	Top Footing	End E+w walk

200.76

T.P. 0.27 200.76 13.11 200.49

4+34 12³ Rt. = start 3' wide E.+w. walk.^{Conc.}

202.63
<u>10.97</u>
124
Start E+w walk

4+32^E 12⁴ Rt. = ± N.+S. Conc. walk.

201.4	201.4	201.7	202.5	202.64
<u>12.2</u>	<u>12.2</u>	<u>11.9</u>	<u>11.1</u>	<u>10.96</u>
8	8	8	12	124
			Grnd.	± walk

4+00 9⁰ Rt. = End Conc. block wall.

204.8	205.4	205.4	205.9	206.2	206.2	212.0
<u>8.8</u>	<u>8.2</u>	<u>8.2</u>	<u>7.7</u>	<u>7.4</u>	<u>7.4</u>	<u>1.6</u>
25	8	8	8	9	9	9
				Grnd	Base wall	Top wall

3+79 8² Rt. = Δ in wall

208.0	208.0	213.6
<u>5.6</u>	<u>5.6</u>	<u>0.0</u>
8E	8E	8E
Grnd	Base of wall	Top of wall

213.60

213.60

Orig B.M.
P. 40

1.80 235.32 235.27

T.P. 8.19 237.12 4.34 228.93

T.P. 12.31 233.27 0.22 220.96

T.P. 12.29 221.18 4.76 208.89

T.P. N.W. 11.70 209.67 2.99 197.77
7 1/2 ft. Bangor
+ allment

5+13 = Wily. cl. line Bangor.

5+10 $\left. \begin{matrix} 8' Lt. \\ 8' Rt. \end{matrix} \right\} = \text{cb. Ret. B.C. (3' Rad.)}$

5+07 $\left. \begin{matrix} 8' Lt. = \text{start cl.} \\ 8' Rt. = \text{start cl.} \end{matrix} \right\}$
start A.C. Pavc.

4+99 $\frac{95}{95}$ $\left. \begin{matrix} 8' Rt. = \text{End Conc. Drive} \\ = \text{wily line Bangor} \end{matrix} \right\}$

4+85 $8' Rt. = \text{start conc. Dr.}$

4+59 $9' Rt. = \text{End of 1' wide 0.7' deep}$
conc. footing

200.76

187.78	187.38	188.46	188.06	188.74	189.47	189.89	190.10	190.51
12.98	13.38	12.30	12.70	12.02	11.29	10.87	10.66	10.25
21	21	11	11	11	11	21	21	21
cl	G	cl.	G	G	G	cl.	G	cl.
		E.C.				E.C.		

189.63	188.33	189.37	189.76
12.13	12.43	11.37	11.00
8	8	8	8
cl.	G	G	cl.

188.74	189.37	188.9	189.86	189.7	189.30	189.75
12.02	12.37	11.9	11.90	11.1	11.46	11.01
8	8	8	8	8	8	8
cl	G	Ord.	pav.	Ord	G	cl.

191.6	190.6	190.6	191.6	191.62
7.2	10.2	10.2	7.2	7.14
8	G		8	8.5
				End of Drive

195.2	195.2	193.4	193.5	194.1	194.25
5.6	5.6	7.4	7.3	6.7	6.51
8	4	3		8	8.5
					Drive

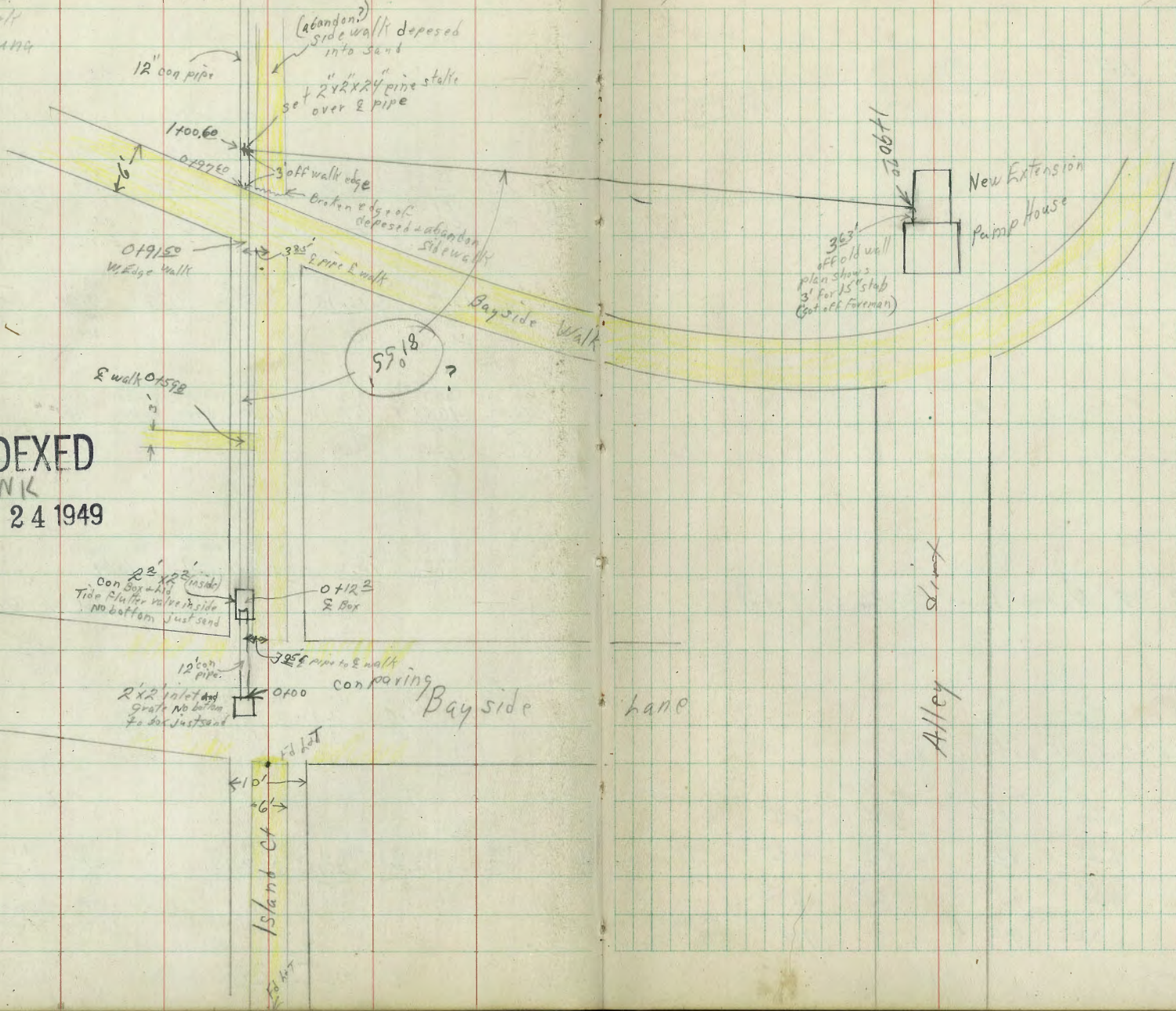
198.8	198.8	198.1	197.9	198.3	198.3	198.0	198.3
2.0	2.0	2.7	2.9	2.5	2.5	2.8	3.5
8	4	3		8	9	9	9
					Ord.	Top Footing	Base Footing

200.76

D. Smith
W. Moore
J. Clark
K. Acuna

Drain Extension Island Ct + Bay side lane

WO# 90086
June 23, 1946



INDEXED

WK

JUN 24 1949

Levels for Drain extension

1+00[±] L

0+97[±]

0+91[±]

0+50

0+12[±] E valve box (flutter for tide)

0+00 East side of 2x2 inlet box

513	464	500	-0.47
634	401	591	-1.83
453	408	820	-0.45
BM	022	785	703

BP Sea wall +
Santa Barbara

Island Ct + Bayside Lane

W0#90086

47

3.47
1.17 (1.2")
4.64 FL

3.47
811
58
Top 12" con pipe

516
-0.52

515
-0.51

60
-1.86

4.14
828
FL
642
Top box

4.27
821
FL
707
Top pipe

464

cont

BM

50

-0.46

↓
-0.48
Brought down
from Santa
Barbara + sawmill
By Planning Com
party

1790²⁰

1775

1750

1725

1707²⁰

1701²⁰ North edge of G' abandon walk.

Σ

48

-1.11
575

Floor level of old Bld

-0.86
550

-0.88
550

-0.96
550

-1.22
550

-1.33
597

HI - 4.64

42nd

st

49

Survey for Prop. Sewer in Beta St
41st to 42nd

3720

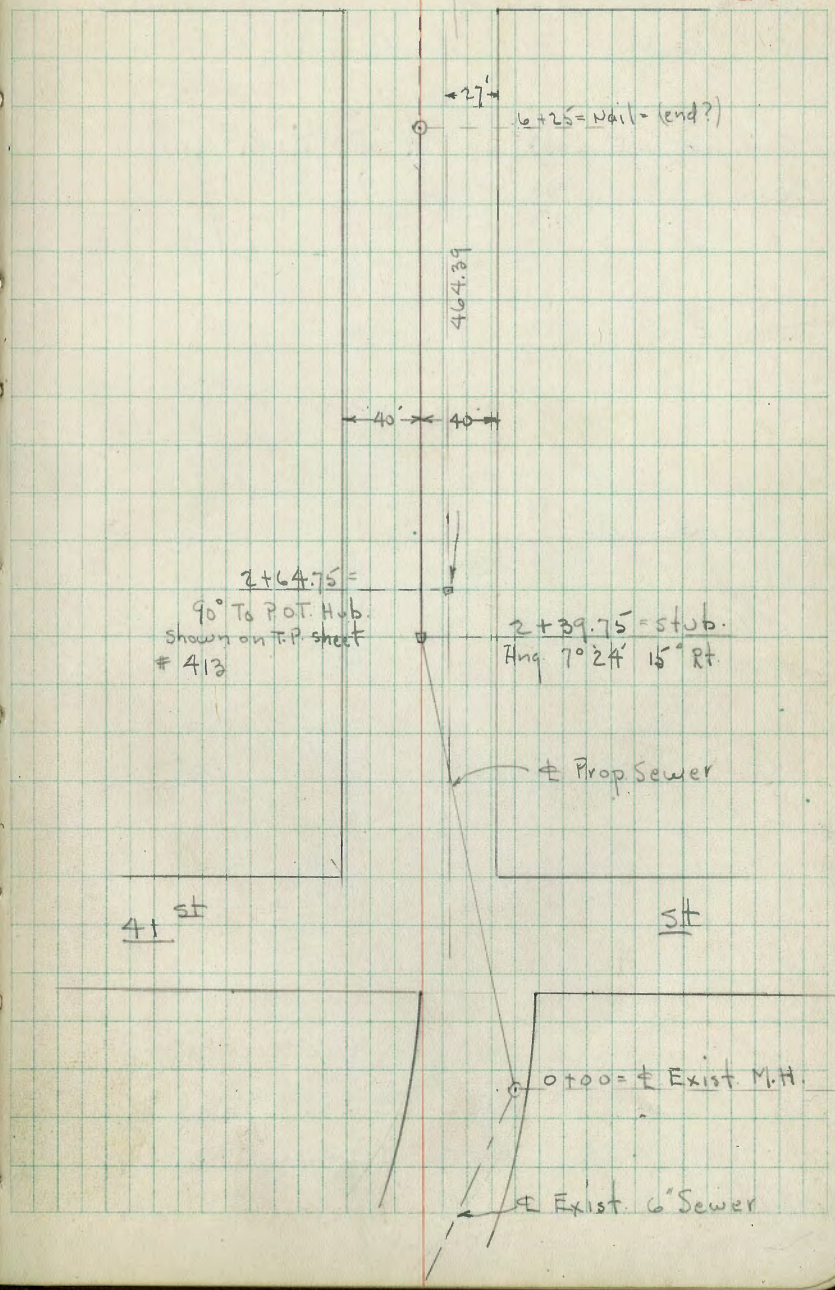
INDEXED

6-29-49

w.o. 31724

JUL 1 1949

7.0. 135"



Begin levels along \pm of Prop. Sewer
in Beta St. - see sketch - P-49

Ground \pm Houses on Lt. are High
3+00

2+39.75 = Ang. $7^{\circ} 24' 15''$ Rt.

2+00

1+50

T.P. 12.53 75.54 0.62 63.01

1+00

0+50

0+00 = \pm Exist. M.H.

0.62 63.62 12.34 63.01

1.71 75.35 12.38 73.64

1.49 86.02 7.27 84.53

B.M. 3.66 91.80 88.14

Nail in Pole
Nail in Pole
S.W. 43rd
 \pm Beta.

Lt.

\pm

Rt.

50

15.5
0.0
100
Var. Lat.

13.6
1.9
10

13.9
2.1

12.8
2.7
40

68.0
7.5
105
 \pm Wash

11.37
4.17
on Stub.

6.87
6.8
10

6.2
7.3

6.9
7.6
15

62.9
12.6
80
 \pm Wash =
low - goes up to 5.

6.39
11.6

75.54

63.6
0.0
25

60.9
3.2
9

60.4
3.2

59.9
3.7
10

58.2
5.4
36

58.0
5.6
10

51.6
6.0

57.0
6.6
10

55.41

50.24

8.22
on Rim

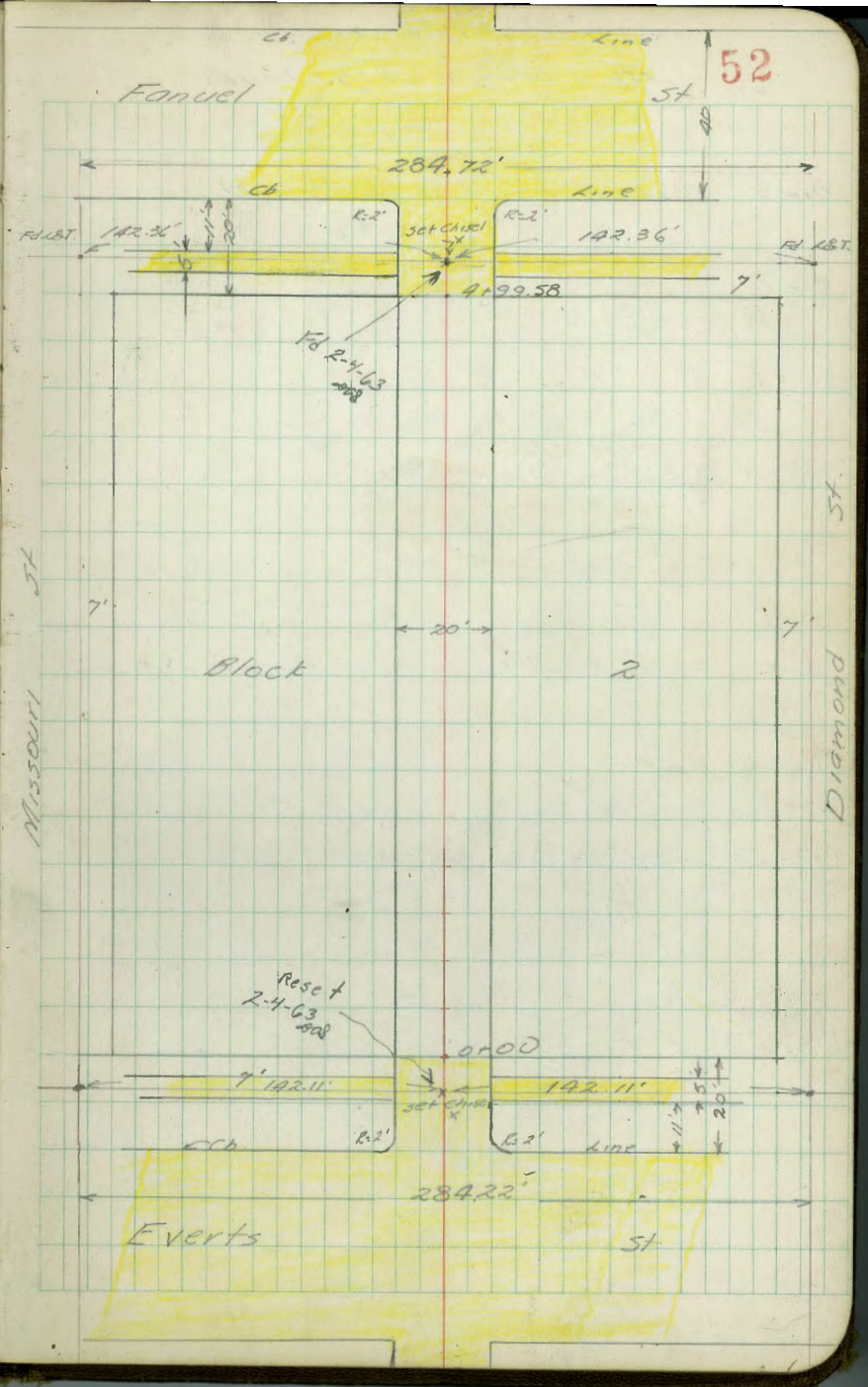
13.39
on Flow line

63.63

41st \pm Beta
S.W. Cor.

7-28-49 X Sect 20' Alley
 Hendricks Block 2 No Shore Highlands
 Roberts
 Greer
 Bunch
 NO# 25020

INDEXED
 W.K.
 AUG 1 1949



Levels Alley Block 2
No Shore Highlands

0+18 Power Pole # A1209 8.6' Lt

0+27

0+00 Edge Conc. Pav.
E Line Everts

0+18 EC Cb Ret.

0-20 East Cb Line Everts

0-40 E Everts

B.M. 269 \downarrow
6970
7

6701

53

66.2 65.2 65.0 65.0 64.7 64.6
35 45 47 47 50 51
11 6 10 13 23

64.93 64.40 64.05 64.31 64.50
477 530 565 539 520
10 10 99 99
G G Cb

64.80 64.33 63.94 64.43
490 537 526 527
10 10 10 10
Cb G G Cb

65.49 64.88 64.86 64.26 64.20 63.99 63.83 63.80 64.42 63.01 63.59
421 482 484 544 550 571 557 590 528 669 611
50 50 12 12 10 10 12 12 25 55
Cb G Cb G G 10 6 Cb G Cb

64.20 64.58 64.34 64.22 63.41
440 512 536 548 629
50 10 10 50

6970
7

SW 7' LBT MISSOURI 8 Everts

TP 5.99 ~~74.21~~ 1.48 68.22

2100 Power Pole # 505768 H 9' Lt

1157 & Single Gar 10.4

1450

1432 Power Pole # A 1220 9' Rt

1700

0485 & Single Garage Conc Drive

0450

69.70
/

(Nail in Power Pole # 505768 H 9' Lt 2100)

67.1 67.3 67.0 66.8 66.5
25 24 27 29 33
15 10 10 20

67.16 66.82
254 288
18.4 10.4
Fl Ramp

66.4 66.4 66.1 66.1 65.9
33 33 35 35 38
20 10 10 20

66.6 66.3 65.6 65.3 65.3
31 34 41 44 44
20 10 10 20

65.48 65.37
42 43
9 17
Drive Drive

66.1 65.9 65.3 65.0 65.0 65.0
35 38 44 47 47 47
20 11 6 10 20

69.70
/

3+91.5 End Conc Ramp Double Gar. 11 Rt

69.41
 $\frac{480}{11} = 43.64$
 19.2

3+78 Beg Conc Ramp Double Gar. 10.8 Rt

69.27
 $\frac{494}{10.8} = 45.74$
 19.3
 Camp

3+67 Beg Board Fence 9.9 Lt

3+51 Power Pole # 505767 H. 9.2 Lt

3+50

69.4
 $\frac{480}{20} = 24$
 10
 69.2
 $\frac{510}{10} = 51$
 69.8
 $\frac{514}{10} = 51.4$
 69.8
 $\frac{514}{20} = 25.7$

3+36 9' Conc Apron (formerly Gar.)
 Now Residence

69.37
 $\frac{424}{12.1} = 35.04$
 10
 69.62
 $\frac{424}{11.5} = 36.87$
 Camp

3+13 Power Pole # A1260 9' Rt

68.6
 $\frac{550}{20} = 27.5$
 10
 68.6
 $\frac{550}{10} = 55$
 68.4
 $\frac{550}{10} = 55$
 68.3
 $\frac{550}{10} = 55$
 68.3
 $\frac{550}{20} = 27.5$

3+00 End Board Fence 10' Lt

2+50 Beg Board Fence 9.9 Lt

67.9
 $\frac{630}{20} = 31.5$
 10
 68.0
 $\frac{630}{10} = 63$
 67.8
 $\frac{630}{10} = 63$
 67.8
 $\frac{630}{10} = 63$
 67.7
 $\frac{630}{20} = 31.5$

74.21
 7

74.21
 7

5117.58 BL. cb Rets.

Edge Conc. Paving
4199.58 W. Line Fance

T.P. 3.57 $\frac{75.30}{1}$ 2.48 $\frac{71.73}{1}$

4496 Power Pole # 505766 H. 9.2' Lt.

4475

4450

4412 Power Pole # A1280 8' Lt.

4400 End Board Fence 10' Lt.

74.21

70.72	70.16	69.66	70.19
2.58	5.14	5.64	5.1
10.1	10.1	9.8	9.8
cb	G	G	cb.

71.01	70.40	70.02	70.11	70.39
4.29	4.90	5.28	5.3	4.21
10.1	10.1	9.8	9.8	9.8
cb	G	G	G	cb.

$\frac{75.30}{1}$

71.6	71.3	71.3	70.7	70.7	70.7
2.5	2.9	2.9	2.5	2.5	2.5
20	10	5	10	12	

71.3	70.8	70.2	70.2	69.8
2.9	2.4	4.0	4.0	2.4
20	10		10	20

70.2	69.7	69.5	69.6	69.1
4.0	4.5	4.2	4.6	5.1
20	10		10	20

B.P.			9.07	58.21	58.26
T.P.	1.72	67.28	9.75	65.55	

5139.58 E Fanuel

5119.58 West Cb Line Fanuel 51

75.30
↑

JEBP Emerald & Fanuel

71.90	70.88	70.56	71.34	69.28
540	422	424	496	602
50	10		10	50

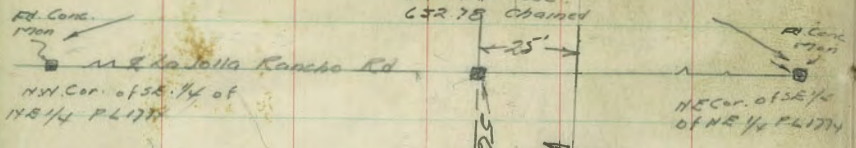
71.71	71.18	70.75	70.26	70.15	69.87	69.66	69.60	70.17	68.59	69.17
359	412	455	504	515	543	564	570	513	671	613
50	50	12	12	10		10	12	12	50	50
		Cb	G				G	Cb	G	Cb

75.30
↑

10-31-49
Hendricks
Smith
Greer
W 0425020

X Sect La Jolla Scenic Dr (Ret- RofS No. 771) (FB-1779)

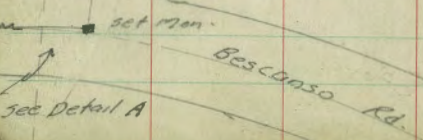
653.44' Rec.
632.75' Chained



(Detail "B")



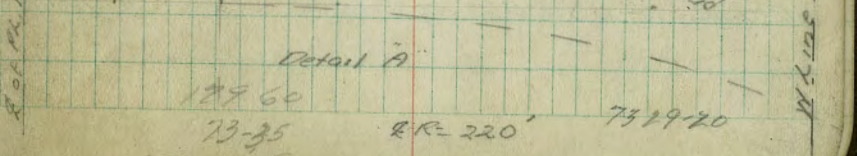
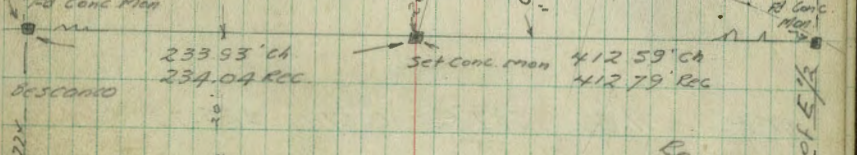
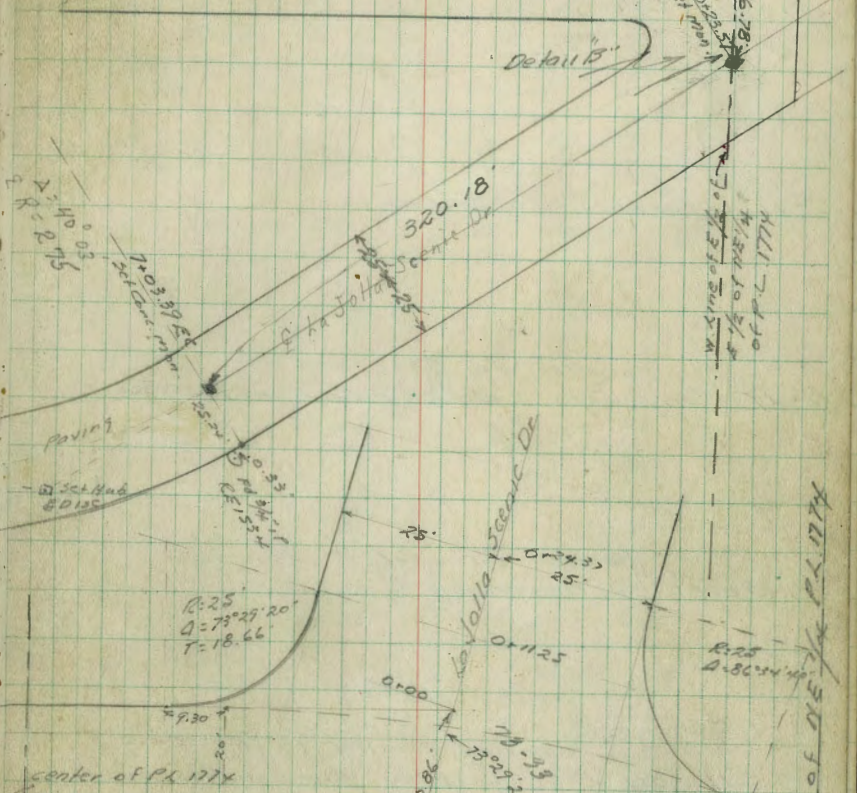
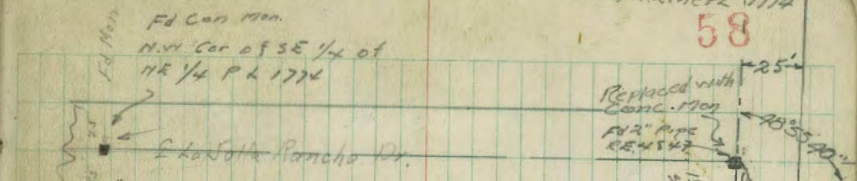
INDEXED
W.K.
NOV 2 1949



see Detail A

to Conc. Man
on N. Line PL 1774

58



see Detail A

0+00 Rt L3

7.9	530.6
8.2	527.4
9.5	528.1
11.1	526.5
11.1	526.4
11.7	525.9
12.1	525.3
11.9	526.6
7.1	530.3

0-11 Parallel to Bescanso

6.8	530.8
8.1	529.1
11.7	525.9
11.1	526.0
12.2	525.4
12.1	525.1
11.1	526.5
7.9	529.7

0-17 Parallel to Bescanso
N.W. Edge Cold Lay Pav. on Bescanso

11.7	525.9
11.8	525.8
11.1	525.8
12.2	525.3
12.1	524.8
11.1	526.0
8.7	528.9

0-20.86 Section Parallel to Bescanso
& Bescanso

11.1	526.0
11.7	525.9
11.9	525.7
12.2	525.4
12.1	525.0
9.1	528.3

0-41 Section Parallel to Bescanso
S.W. Edge Cold Lay Pav. on Bescanso

12.1	525.5
12.1	525.5
12.1	525.3
12.1	524.8
13.1	524.0
15.2	522.4

537.62

T.P. 11.89 537.62 6.67 525.73

BM 4.89 532.40 527.51

BM Mon LaJolla Mesa Dr. & Bescanso Road

2450

2425

2404.18 BC.

1150

1100

0450

537.62
K

50	533.8	533.1	533.0	531.5	531.5	535.5
25	533.0	531.9	530.7	531.2	531.0	535.0
17	532.6	531.4	530.0	530.4	529.4	534.2
16	532.0	530.4	529.3	531.2	528.9	533.7
10	532.8	531.2	529.9	530.0	528.4	534.4
Pay	533.0	531.5	530.0	528.4	528.4	534.2
9	533.0	531.0	529.4	528.1	528.1	533.9
Pay	532.5	530.6	528.9	527.5	527.5	533.5
11	532.6	530.6	528.9	527.5	528.9	534.2
12	533.5	531.6	529.6	528.9	528.9	534.5
13	533.5	532.3	530.5	529.6	529.6	534.5
25	533.9	533.0	530.5	530.5	529.6	534.5
Pay	533.7	533.6	532.6	532.6	532.7	534.1
50	533.7	533.0	532.6	533.0	532.7	534.1
Pay						

537.62
K

5+75

5+50

5+25

5+11.16 BC. LI.

4+77 TOL or Pole # 425829H 18' RT

4+40

542.23

50	IN	537.2	50	IN	538.8	50	IN	538.5	50	IN	538.8	50	IN	538.8	50	IN	538.8
25	IN	537.0	25	IN	538.0	25	IN	538.5	25	IN	538.8	25	IN	538.8	25	IN	538.8
18	IN	536.4	18	IN	537.2	18	IN	537.5	18	IN	537.8	18	IN	537.8	18	IN	537.8
16	IN	535.8	16	IN	536.1	16	IN	536.8	16	IN	536.8	16	IN	536.8	16	IN	536.8
13	IN	536.1	13	IN	536.2	13	IN	536.2	13	IN	536.2	13	IN	536.2	13	IN	536.2
10	IN	536.2	10	IN	536.4	10	IN	536.4	10	IN	536.4	10	IN	536.4	10	IN	536.4
Pay			Pay			Pay			Pay		Pay		Pay		Pay		Pay
10	IN	535.7	10	IN	536.3	10	IN	536.3	10	IN	536.3	10	IN	536.3	10	IN	536.3
7	IN	535.4	7	IN	535.8	7	IN	535.8	7	IN	535.8	7	IN	535.8	7	IN	535.8
12	IN	535.7	12	IN	535.6	12	IN	535.6	12	IN	535.6	12	IN	535.6	12	IN	535.6
25	IN	535.0	25	IN	535.5	25	IN	535.5	25	IN	535.5	25	IN	535.5	25	IN	535.5
50	IN	534.7	50	IN	536.1	50	IN	536.1	50	IN	536.1	50	IN	536.1	50	IN	536.1
Pay			Pay			Pay			Pay		Pay		Pay		Pay		Pay
50	IN	533.9	50	IN	534.9	50	IN	534.9	50	IN	534.9	50	IN	534.9	50	IN	534.9
29	IN	534.8	29	IN	533.9	29	IN	533.9	29	IN	533.9	29	IN	533.9	29	IN	533.9
10	IN	535.1	10	IN	533.9	10	IN	533.9	10	IN	533.9	10	IN	533.9	10	IN	533.9
Pay			Pay			Pay			Pay		Pay		Pay		Pay		Pay
10	IN	535.4	10	IN	533.9	10	IN	533.9	10	IN	533.9	10	IN	533.9	10	IN	533.9
12	IN	535.7	12	IN	533.9	12	IN	533.9	12	IN	533.9	12	IN	533.9	12	IN	533.9
25	IN	535.0	25	IN	533.9	25	IN	533.9	25	IN	533.9	25	IN	533.9	25	IN	533.9
50	IN	534.7	50	IN	533.9	50	IN	533.9	50	IN	533.9	50	IN	533.9	50	IN	533.9
Pay			Pay			Pay			Pay		Pay		Pay		Pay		Pay
10	IN	535.7	10	IN	533.9	10	IN	533.9	10	IN	533.9	10	IN	533.9	10	IN	533.9
12	IN	535.4	12	IN	533.9	12	IN	533.9	12	IN	533.9	12	IN	533.9	12	IN	533.9
25	IN	535.0	25	IN	533.9	25	IN	533.9	25	IN	533.9	25	IN	533.9	25	IN	533.9
50	IN	534.7	50	IN	533.9	50	IN	533.9	50	IN	533.9	50	IN	533.9	50	IN	533.9
Pay			Pay			Pay			Pay		Pay		Pay		Pay		Pay

7+50

7+03.39 EC.

6+75

6+50

6+25

T.P. 5.83 542.41 3.85 538.58

6+00

542.43
^

63

50	541.3	50	540.3	50	539.2	50	538.4	50	537.4	50	536.9	50	536.2
10	540.3	10	539.4	10	538.2	10	537.4	10	536.8	10	536.4	10	536.4
20	540.4	20	539.5	20	538.3	20	537.3	20	536.9	20	536.6	20	536.4
30	538.7	30	537.6	30	537.0	30	537.7	30	536.4	30	536.4	30	536.3
40	539.0	40	538.1	40	537.3	40	536.9	40	537.7	40	536.6	40	536.3
50	539.4	50	538.5	50	537.8	50	537.3	50	536.9	50	536.6	50	536.4
60	539.5	60	538.3	60	537.5	60	537.0	60	536.6	60	536.6	60	536.4
70	539.2	70	537.8	70	537.1	70	536.6	70	536.6	70	536.4	70	536.3
80	538.7	80	538.2	80	537.4	80	537.1	80	537.1	80	537.7	80	537.1
90	539.3	90	538.0	90	537.6	90	537.2	90	537.2	90	537.1	90	536.3
100	539.0	100	538.9	100	538.6	100	538.3	100	538.3	100	537.1	100	536.3
110	538.9	110	538.9	110	538.6	110	538.3	110	538.3	110	537.1	110	536.3

(BM set)

6.33 5.38.08

2 Pipe Ranch
Road

BM

0.03 544.38

SUTOP N.27

Rancho
E. Scenic Rd.
FB 1741

544.39

10+09.90 RT to A on RT

9+80

9+50

9+00

8+50

8+00

544.41
K

50	539.1	540.4	541.8	541.5	539.9	539.5	539.1	539.1	539.5	538.8	539.1	538.9	538.3
25	537.4	539.4	540.5	540.9	539.9	539.5	538.5	538.5	538.9	538.8	538.9	538.8	538.3
16	537.0	538.4	537.2	540.9	537.8	539.8	537.2	539.4	539.9	538.9	539.4	538.9	538.3
13	536.3	537.9	538.1	539.1	538.8	538.8	537.2	539.1	539.5	538.9	539.1	538.9	538.3
10	536.5	537.4	537.4	538.5	539.2	539.2	537.2	539.5	539.5	538.8	539.1	538.9	538.3
7.9	536.5	537.7	539.1	539.1	539.8	539.8	539.8	539.8	539.8	538.8	539.1	538.9	538.3
7.9	536.5	537.7	539.1	539.1	539.8	539.8	539.8	539.8	539.8	538.8	539.1	538.9	538.3
8.1	536.3	537.5	538.8	538.8	539.5	539.5	539.5	539.5	539.5	538.8	539.1	538.9	538.3
8.1	536.1	537.0	538.0	538.0	538.9	538.9	538.9	538.9	538.9	538.8	538.9	538.9	538.3
10.1	535.6	537.4	538.4	538.4	539.4	539.4	539.4	539.4	539.4	538.8	539.1	538.9	538.3
9.1	535.1	537.2	537.9	537.9	538.7	538.7	538.7	538.7	538.7	538.8	538.9	538.9	538.3
9.1	534.6	536.5	537.1	537.1	537.5	537.5	537.5	537.5	537.5	538.8	538.9	538.9	538.3
9.1	534.6	536.5	537.1	537.1	537.5	537.5	537.5	537.5	537.5	538.8	538.9	538.9	538.3

64

544.41
K

Typical Sections along Adams - from
Park Blvd. to Boundary

w.o. 20623

1-16-50

7.0

Rdwy in
This Column

w.L. Louisiana - to S.

INDEXED

M.K.

MAR 9 1950

E.L. Mississippi

52

100' E. of E.L. Panorama Dr. (to N.)

52

80' W. of W.L. Alabama - To S.

52

w.L. Florida

52 R

w.L. Georgia

- 52 R

50' E. of E.L. Park Blvd. - 52' Rdwy. - R

N. Side

#

S. side 65

3.98	4.39	3.61	3.61	3.65	4.26	3.80
T	9	1/4		1/4	9	T

0.33	0.83	0.30	0.21	0.28	0.70	0.21
T	9	1/4		1/4	9	T

8.02	8.64	8.17	8.26	8.28	9.08	8.56
T	9	1/4		1/4	9	T

6.32	6.78	6.43	6.20	6.22	6.66	6.36
T	9	1/4		1/4	9	T

4.10	4.63	3.90	3.95	4.02	4.80	4.81
T	9	1/4		1/4	9	T

6.10	6.60	5.03	5.41	5.50	5.76	5.07
T	9	1/4		1/4	9	Top

5.70	6.43	5.41	5.65	5.20	5.43	4.85
Top	9	1/4		1/4	9	Top

20' w. of w.l. Kansas

Rdwy.

w.l. Utah

25' w. of w.l. Idaho

w.l. Oregon

E.L. Hamilton

50' E of E.L. Arizona to N.

E.L. Arizona to S.

160' w. of w.l. of Arizona to S.

100' E. of E.L. Louisiana to S.

- N. side

E

- S. side 66

2.92	4.42	4.30	4.45	4.45	5.31	4.91
T	9	1/4		1/4	9	T

5.08	5.72	5.51	5.50	5.64	6.41	5.98
T	9	1/4		1/4	9	T

4.20	4.71	4.48	4.61	4.61	5.58	5.15
T	9	1/4		1/4	9	T

5.26	5.88	5.66	5.62	5.84	6.63	6.25
T	9	1/4		1/4	9	T

1.67	2.26	1.79	1.63	1.71	2.33	1.84
T	9	1/4		1/4	9	T

4.55	5.20	4.59	4.41	4.46	4.96	4.39
T	9	1/4		1/4	9	T

12.62	13.31	12.67	12.61	12.76	13.49	12.98
T	9	1/4		1/4	9	T

11.36	12.04	11.51	11.47	11.50	12.23	11.66
T	9	1/4		1/4	9	T

4.71	5.38	4.34	4.24	4.24	5.08	4.49
T	9	1/4		1/4	9	T

Rdwy

N. side

#

S. side 67

w.l. Boundary to N. + w.l. of Alley to S.

5.02	5.53	5.18	5.15	4.99	5.22	4.67
T	9	1/4		1/4	9	T

w.l. Ohio to S

52'

5.75	6.29	5.74	5.75	5.63	5.90	5.33
T	9	1/4		1/4	9	T

25' w. of w.l. 30th

52'

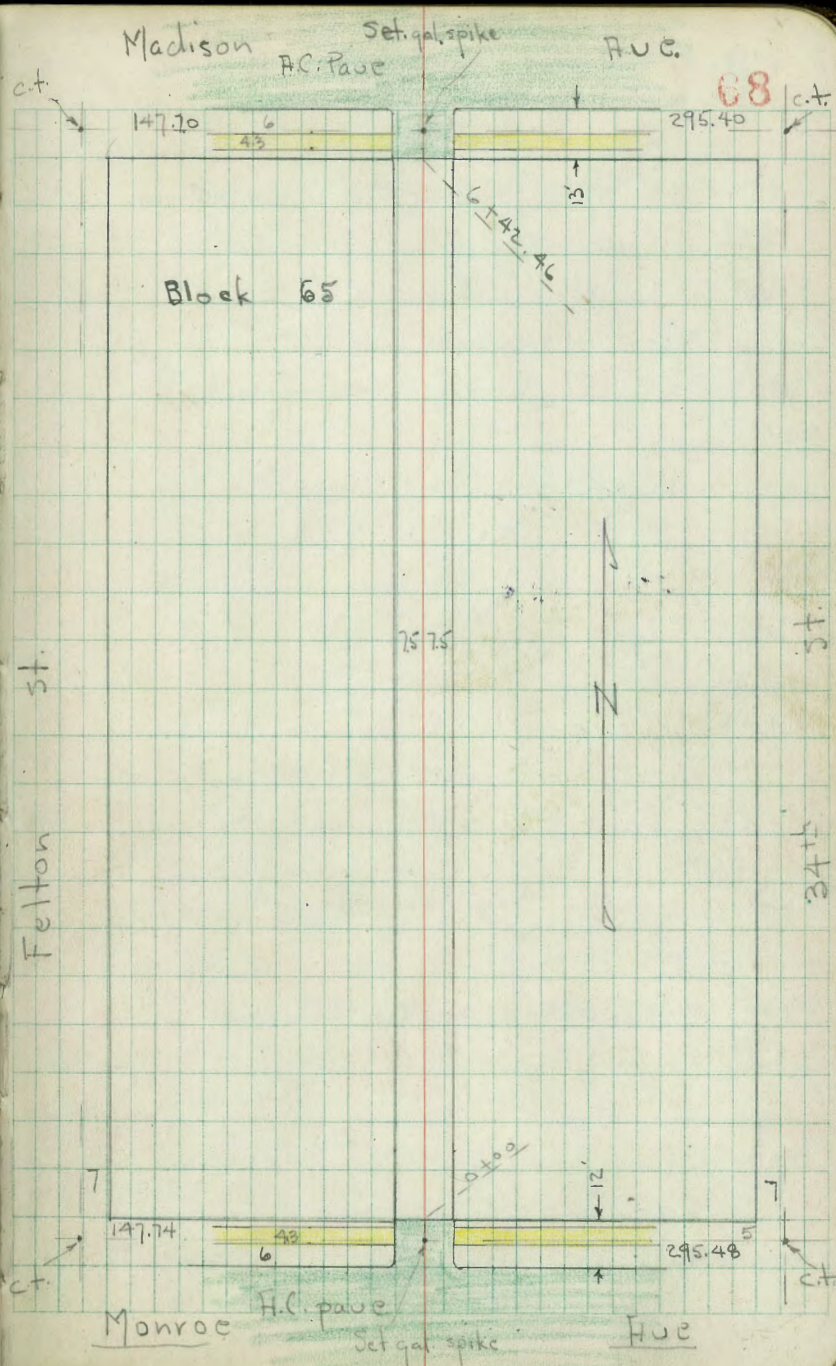
5.40	5.99	5.79	5.89	6.09	6.09	6.75	6.27
T	9	5' N.	1/4		1/4	9	T

7- Sect. 15 Alley in Block 65, Resub.
of Blks. 39 + 56, Normal Hts. - Map 1048

4237
W.O. 31816

3-8-50
Osborne
Hardin
Hatch
Shepard

INDEXED
MAR 9 1950



7-Sect. Alley - Blk. 65

- 1+50 - 9.9' Rt. = ± Sing Gar. - dirt floor
- 1+43 - 6.3' Lt. = ± P. pole # -
- 1+42 - 7.5' Rt. = end fence
- 1+17 - 7.5' Rt. = Beg. board fence
- 1+09 - 5.9' Rt. = ± of 11' Conc. apron to Sing. Gar.
- 1+02 - 7.5' Rt. = end Board fence
- 1+00
- 0+50
- 0+42 - 5.9' Lt. = ± P. pole # P.A. 4507
- 0+41 - 7.5' Rt. = end picket + Beg. board fence
- 0+38 - 7.7' Lt. = ± - end Hedge
- 0+15
- 0+01 - 7.5' Rt. = Beg. Picket fence
- 0+01 - 7.7' Lt. = ± of 1' Hedge - 4' High
- 0+00 = N.L. Monroe - + edge A.G. pave
- 0-01 - 0.5' Rt. = ± Sewer M.H. 5.70 on Rim
- 0-12 = N. cb.

check B.M. 0.26 388.76 388.71
 B.M. 8.73 389.02 380.29 S.E. B.P.

Lt. = w.

±

Rt. = E. 69

385.4	385.2	385.0	385.3	385.3
2.6	3.8	4.0	3.7	3.7
10.6	7.5	7.5	7.5	7.9
along shed				floor
				385.02
				385.40
				4.00
				3.56
				5.9
				apron
				11
				floor
385.1	385.0	384.4	384.8	385.4
2.9	4.0	4.6	4.2	3.8
15	7.5	7.5	7.5	15
384.4	384.6	384.7	384.7	385.0
4.6	4.4	4.3	4.3	4.0
15	7.5	7.5	7.5	15
384.5	384.5	384.3	384.5	384.7
4.5	4.5	4.7	4.5	4.3
10.6	7.5	7.5	7.5	11.5
along House				along House
383.67	383.32	383.22	383.48	383.80
5.35	5.70	5.70	5.54	5.22
7	7	on Rim	7.6	7.6
	9.4		9.4	7.6
				Top-end
				cb.
383.85	383.48	383.13	383.26	383.75
6.17	6.62	5.89	5.76	5.57
5.9	5.04	7.5	7.5	5.10
Top	Top-2	9.4	9.4	Top
	Rad			2' Rad
				9.4
				9.4
				Top
				4.0
				4.0
				BP
				383.84
				384.58
				389.02
				389.02
				34' + Monroe - S.E. B.P.
				33' + Monroe

L E Rt.

5+43 6.1' Lt = E P. Pole # P.A 4587

5+00

4+91 9.1' Rt. = end WIRE FENCE

4+50

4+43 7.0' Rt begin WIRE FENCE

4+43 6.3' Lt = E P. Pole # P.A. 45674 end fence 7.3 Lt.

4+00

3+90 7.1' Lt = end shed & begin board fence

3+84 7' Lt. = shed

3+50

3+42- 6' Lt. = E P. pole # P.A. 4551

3+41- 7.1' Lt. = Beg. board fence

3+00

2+50

2+43- 6.1' Lt. = E P. pole # P.A. 4537

2+42- 7.6' Rt. = end fence

T.P. 702 392.73 331 385.71

2+00

1+62- 8.4' Lt. = E 4' Conc. walk

1+59- 7.5' Rt. = Beg. board fence

387.5	387.5	387.5	387.4	387.9
5.2	5.2	5.2	5.3	4.8
15	7.5		7.5	15
387.2	387.6	387.6	387.8	387.7
5.5	5.1	5.1	4.9	5.0
15	7.5		7.5	15
387.5	387.5	387.5	387.7	387.6
5.2	5.2	5.2	5.0	5.1
15	7.5		7.5	15

386.9	387.2	386.8	386.8	386.7
5.8	5.5	5.9	5.9	6.0
15	7.5		7.5	15
385.6	386.6	386.6	386.6	386.5
7.1	6.1	6.1	6.1	6.2
35	7.5		7.5	15
385.8	386.0	385.8	385.9	386.6
6.9	6.7	6.9	6.8	6.1
15	7.5		7.5	50

385.1	385.9	385.7	385.5	385.6
3.9	3.1	3.3	3.5	3.4
30	7.5		7.5	15

385.59 385.45
3.43 3.57
15 8.4
walk

389.02

SOIL SAMPLE 1700

check B.M. 7.24 380.29

T.P. 3.52 387.53 7.28 384.01

6+55.46 = 5TH. CURB

T.P. 4.36 391.29 5.80 386.93

6+42.46 5TH. L of MADISON edge A.C. PAVE

6+25

6+16 9.0' Rt = E of House

6+00

5+50 1' 5TH Q. 12' LT = 10' CONC APRON TO
single garage

Lt. E Rt.

71

386.657	386.39	386.90	386.69	386.79	386.88	387.29	387.19	387.70
4.64	4.90	4.39	4.60	4.50	4.41	4.00	4.10	3.59
SO	SO	Top	Top	Top	Top	Top	Top	Top
Top	Gut.	Rad.	Rad.	Rad.	Gut	Rad.	Gut	Top

391.29

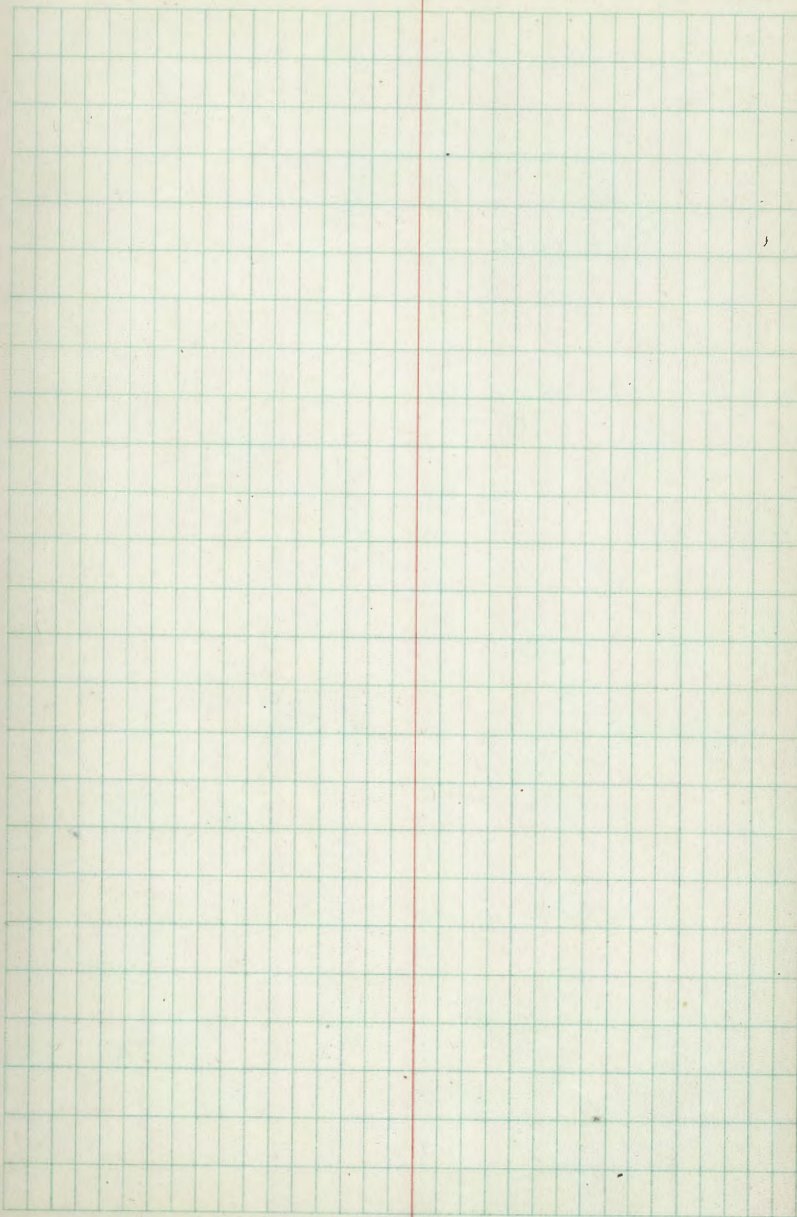
387.35	387.29	387.26	387.50
Top CURB	GUT	Gutter	Top CURB
5.38	5.44	5.45	5.23
	7.0	7.3	

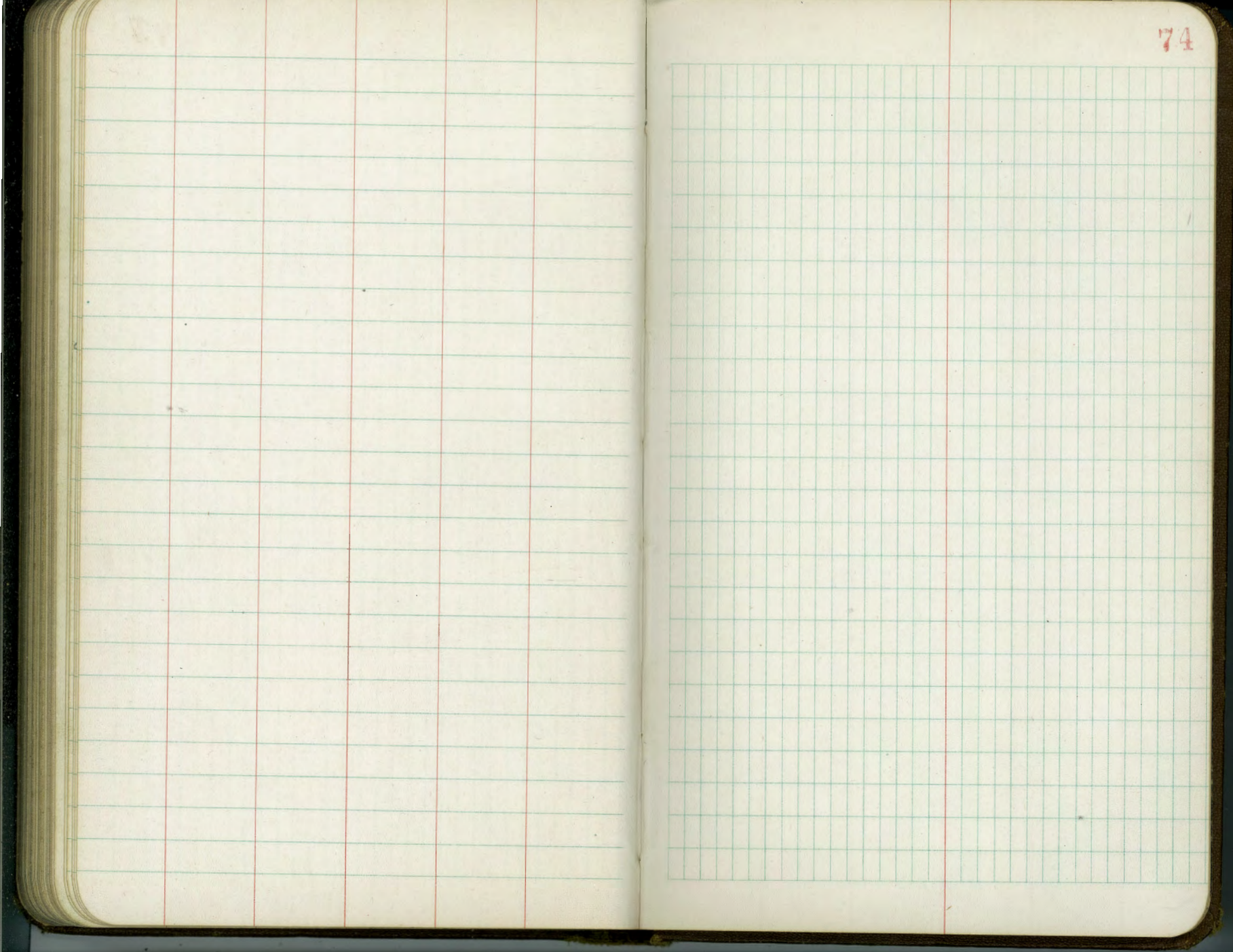
388.2	388.2	388.3	388.3	388.5
4.5	4.5	4.4	4.4	4.2
garage 8.8	7.5		7.5	15
			7.5	15
			4.3	3.17
			ground floor	

389.0	388.7	388.7	388.9	389.0
3.7	4.0	4.0	3.8	3.7
15	7.5		7.5	15

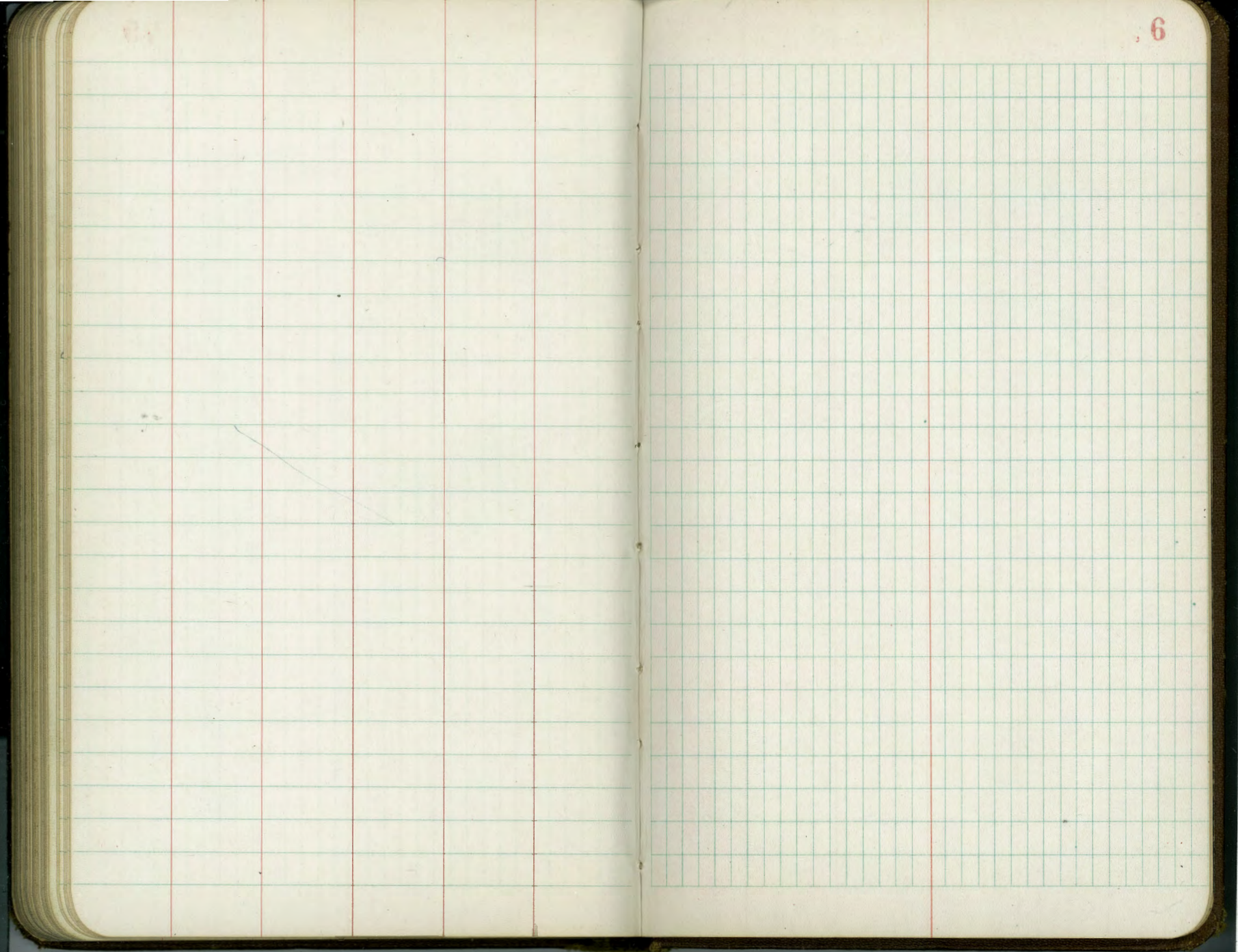
388.21	388.25	388.3	388.2	388.2
4.52	4.48	4.4	4.5	4.5
16.7	12.0	7.5	7.5	15
floor	APRON			

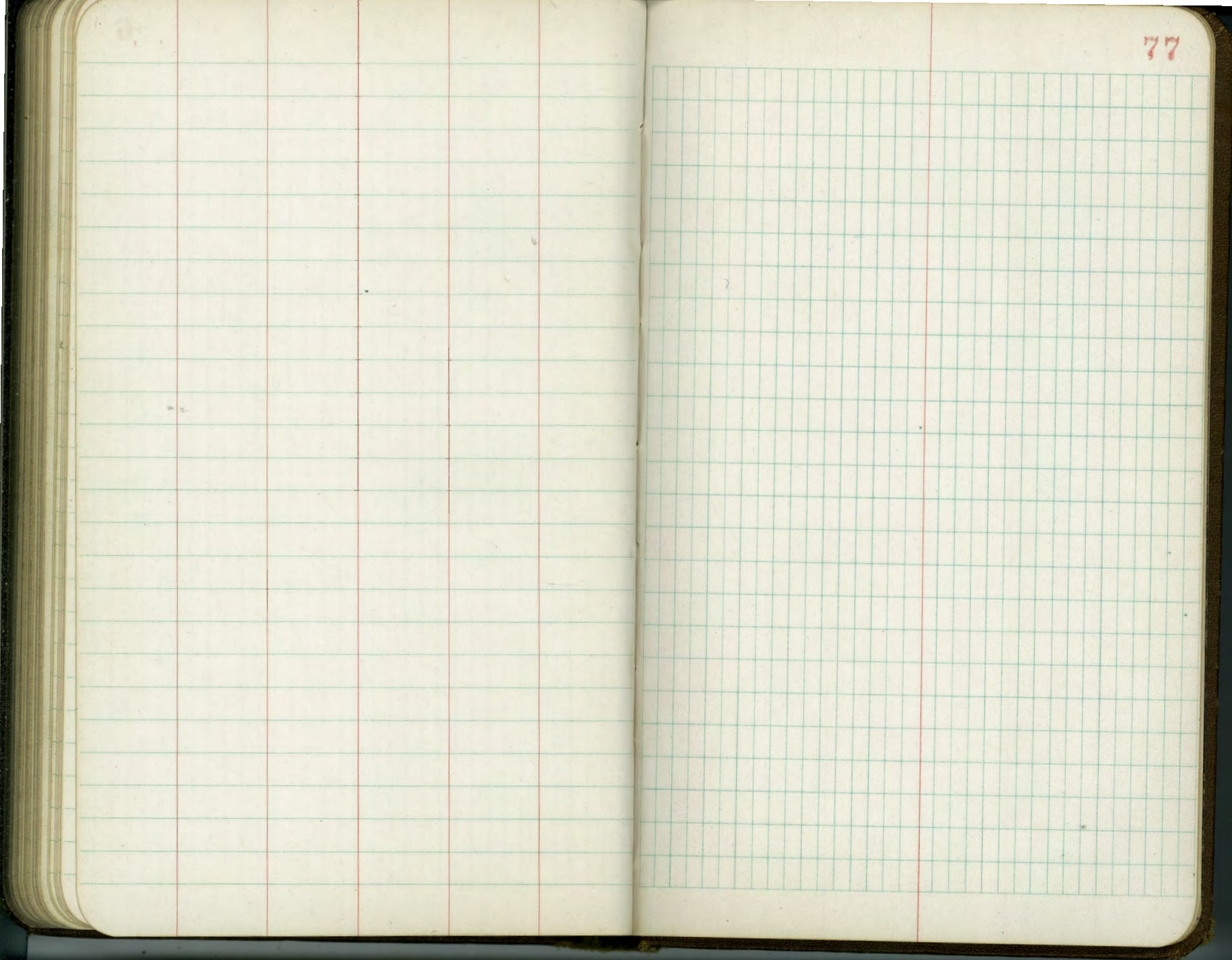
392.73





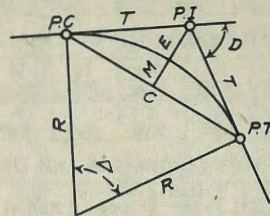






DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
 Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
 Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$ (5) (6)
 External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (7) (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
 Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction $= .36$ or $T = 414.85$ ft. P. C.—Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. $= 7.27$ ft. Distance $= 158 -$ Sta. P. C. $= 54.50$, hence offset $= 7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle $= \frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. $=$ (in minutes) $.3 \times C \times D^\circ$ or $=$ defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve $= .3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle $= 2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction $= .10$ or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

4942 Polk - Helsh

8537
281

11347

SE 1/4 58.26

SW 1/4 35 Top Hydt. Rancho Rd.

Adams W.O. 20623 - Park to Bndy.

24⁺ S.E. 388.71

20.85
11.25

92.11

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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