

1852

1852

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

CITY ENGINEER'S OFFICE

INDEXED

*Completely
except page #5*

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \times 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
Copyright, 1914, by Eugene Dietzgen Co.

Violet
To

Snowdrop

Chicago

H

0
1
2
3
4
5
6
7
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9
10
11
12
13
14
15
16
17
18
19
20
21
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31
32
33
34
35
36
37
38
39
40

E
to be
of road
examp
30.6 =

Manzanita Drive

Sketches

43

Notes

52

final X-sect. of Opal St. - from
Cass to Dawes - 70' St. - 15' cbs
Orig. X-Sect in Book 1701-67 - Sections
on Pavé - to 0+00 are O.K. - use sketch
on P. 67 - see sketch for add Detail

#2347 5-17-48
W.O. 31533 7.0.

1+00 - 29.3 Rt. = Beg. Nly. of Hedge - 4' High
0+99 - 21.8 Rt. = end fence

0+50

0+20

INDEXED
MAY 18 1948

Rods on edge of Pavé + end of cb. Note sketch.
end of cb. on Rt. = 0+00.9 + on Lt. = 0+01.2

+34.5 Rt. = Beg. Lath fence:
0+00 = E.L. Cass - end of Walks

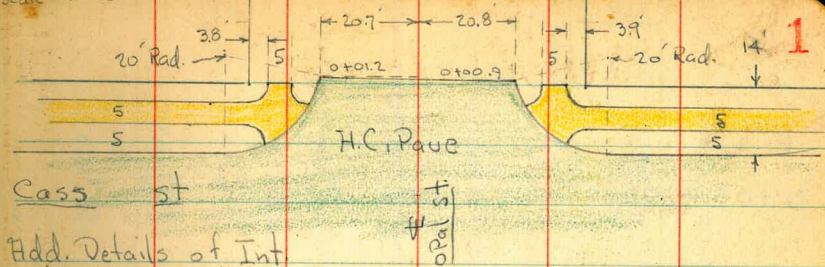
6.91

107.83

100.92

St. 7ct.
Opal + Cass
1701-P. 67

Scale = 1" = 40'



Add Details of Int
E. side Cass + Opal

Lt. = N.

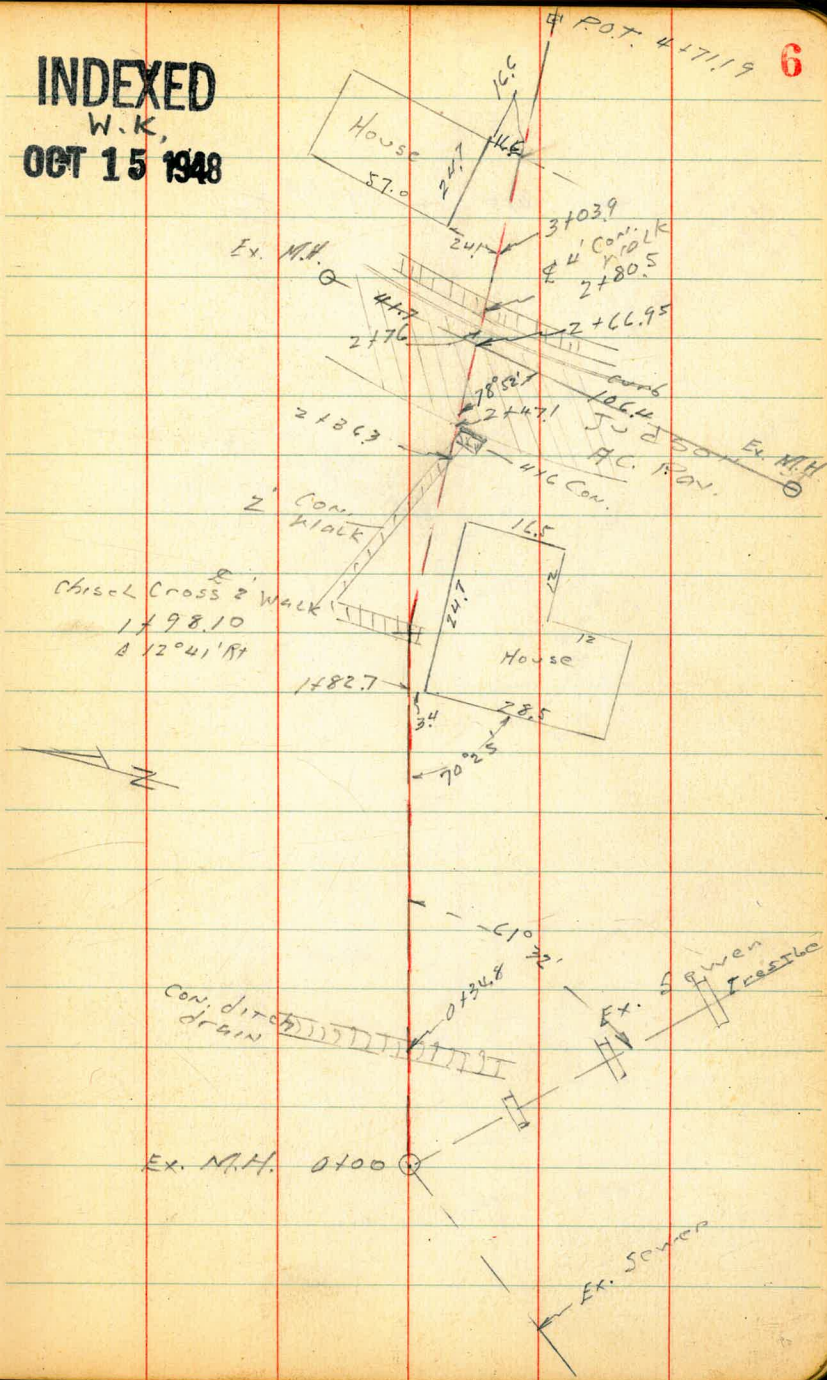
Rt. = S.

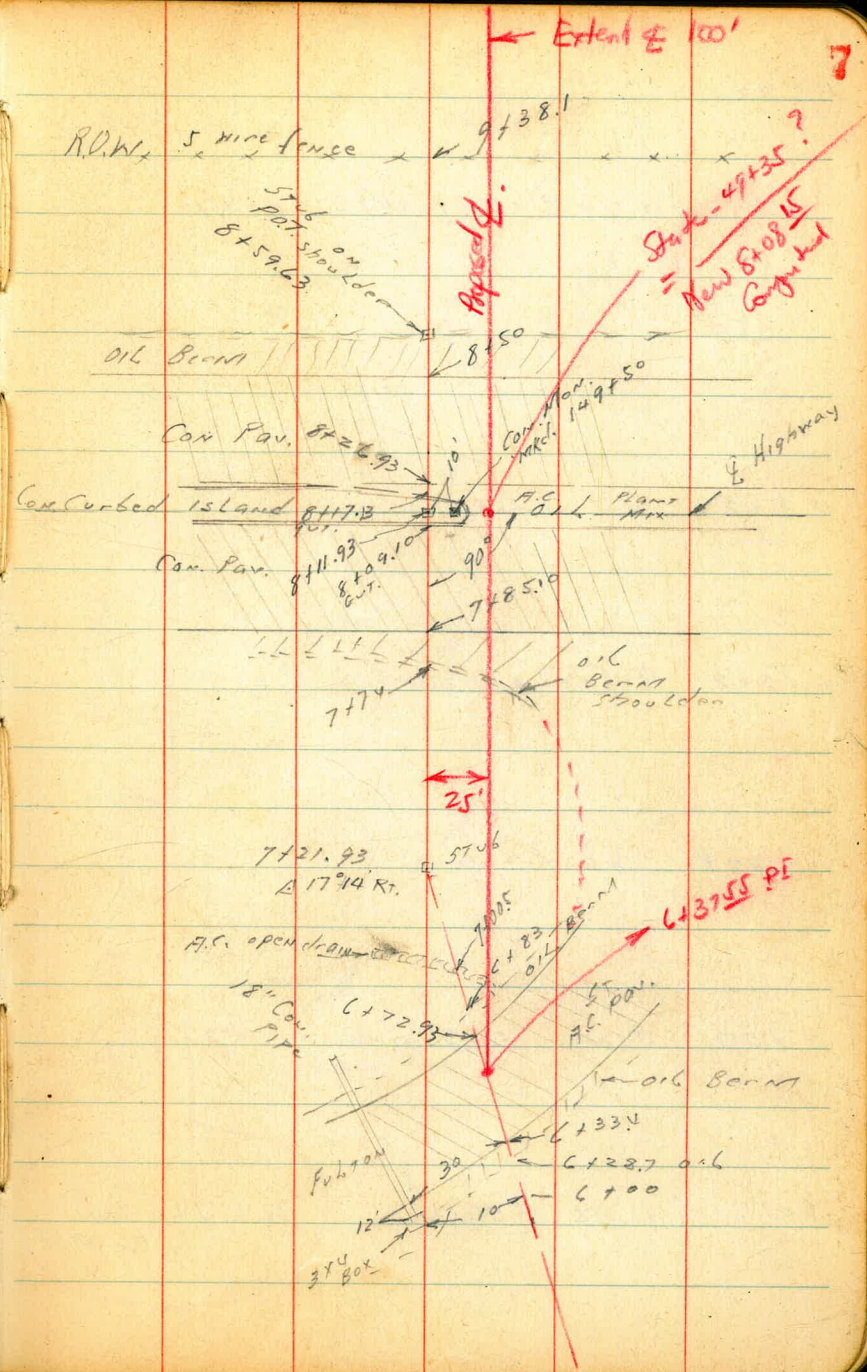
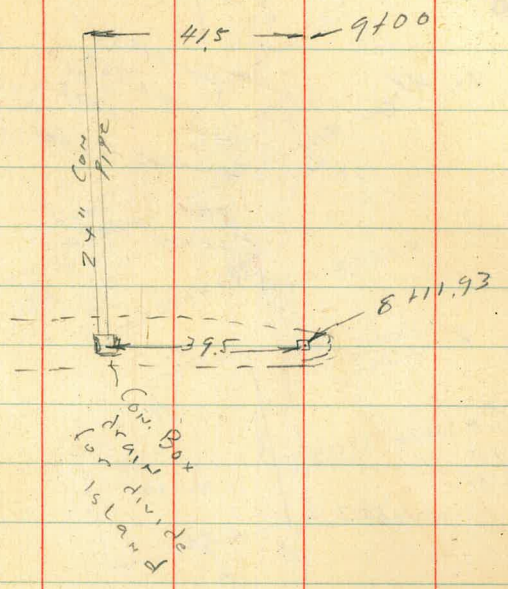
	4.2	4.4	4.7	5.3	5.7	5.8	5.9	5.9	6.2	6.3
	40	35	20	16	22	17	20	30	35	40
	5.10/03.3	5.10/03.1	5.10/02.9	5.10/01.9	5.10/02.0	6.10/01.2	6.10/01.8	6.10/01.3	6.10/01.0	7.10/00.8
	40	35	20	15	28	17	20	32	35	40
	5.10/03.5	5.10/03.0	5.10/02.6	5.10/01.8	5.10/01.9	6.10/01.7	6.10/01.4	5.10/01.1	7.10/00.8	
	35	20	15	10	10	17	20	35	40	
	5.10/02.45	5.10/01.83	6.10/01.73	6.10/01.45	6.10/01.02	7.10/00.67	6.10/01.9			
	20.7	20.7	10	23.8	10	20.8	20.8			
	Top	Top				Top	Top			
	5.10/02.81	5.10/02.59				6.10/01.4	6.10/01.1			
	31.2	26.2				26.1	21.1			
	end walk				107.83		end of walk			

Prop. Section to
 Veterans Hospital
 Linda Vista
 W.P. 90079

Moore
 BC99
 Sherman
 Bunch
 10-13-48

INDEXED
 W.K.
 OCT 15 1948





7

Stake-49+35?
New 8+08.15
Corner

6+37.55 PE

0.190

T.P 11.99 346.69 1.96 334.70

+50

0.738.8 E.C. ditch

0.734.8 E. Con open ditch

0.730.8 W.L. ditch

0.100 RIM East side

BM 11.92 336.66

324.74 Inv.
Ex. M.H

Tie into a City B.M.

338.6
8.1
1.5

338.5
8.2

338.5
8.2
1.5

R₁

8

346.69 ✓

334.6
2.1
1.5

331.8
4.9

330.5
4.2
1.5

329.8
4.9

331.7
11.5
1.5

328.2
8.5

326.0
11.7
1.5

329.3
7.4

328.0
8.6
ground RIM

329.9
7.4

336.66 ✓

Check Starting Elevation - ~~336.66~~

R.R.
T.P. spike
PP 279025 454 347.46 3.77 342.92

2 + 4710 Pav

2 + 4710 on walk

2 + 363 on 2' walk

1 + 9810 Δ 12° 41' R

1 + 50

1 + 20

346.69

L

E

R

9

4.1
15
Pav. 342.6

4.50
15
Pav. 342.2

5.10
15
Pav. 341.66

4.79
15
Pav. 342.3

3.77
15
Pav. 342.9

5.4
15
Pav. 343.3

5.83
15
Pav. 342.80

5.7
15
Pav. 343.0

5.0
15
Pav. 341.7

5.3
15
Pav. 341.4

5.4
15
Pav. 341.3

6.3
15
Pav. 340.4

7.1
15
Pav. 339.6

7.0
15
Pav. 339.1

346.69

Lr

Rr

±50

$\frac{4.7}{20} 342.9$ $\frac{4.5}{20} 343.1$ $\frac{4.3}{20} 343.1$

4/00

$\frac{4.6}{20} 343.0$ $\frac{4.4}{20} 343.2$ $\frac{4.4}{20} 343.2$

T.P. 4.22 347.61 4.07 343.39

347.61

±50

$\frac{4.1}{20} 343.4$ $\frac{4.1}{20} 343.4$ $\frac{4.2}{20} 343.5$

3/00

$\frac{4.5}{15} 343.0$ $\frac{4.2}{15} 343.3$ $\frac{4.0}{15} 343.5$

2+80.5 E WALK

$\frac{4.4}{15} 342.05$

2+76 gutter

$\frac{5.85}{907700} 341.61$ $\frac{5.58}{706200} 341.88$
TOP CURB

2+66.95 INT. Sewer Ex. 347.46

$\frac{11.14}{47.7} 342.32$ $\frac{5.35}{47.7} 342.11$ $\frac{5.7}{341.8}$ $\frac{6.54}{106.4} 340.92$ $\frac{18.32}{106.4} 329.14$
FL. RIM RIM F.L. MAIN of D.M.H.

(34.3)

1183

6472.93 E. edge Pav. FULTON

T.P. 4.64 333.83 12.91 329.19

133x W. edge Pav.

6400

T.P. 6.34 342.10 11.85 335.76

441

5400

347.61

11

341.8	327.6	328.4	327.7	327.87	328.3	327.8	333.8
$\frac{12.0}{36}$	$\frac{6.2}{21}$	$\frac{5.4}{7}$	$\frac{6.1}{5}$	5.95	$\frac{5.5}{32}$	$\frac{6.0}{36}$	0.0
		Bottom			S. edge pav		Top Cut

333.83 ✓

324.3	329.5	328.9	329.1	329.9	329.8	332.3	332.0	340.9	341.1
$\frac{17.8}{46}$	$\frac{12.6}{35}$	$\frac{13.2}{33}$	$\frac{13.0}{27}$	$\frac{12.2}{x}$	$\frac{12.3}{10}$	$\frac{9.8}{25}$	$\frac{6.1}{25}$	$\frac{1.2}{45}$	$\frac{1.0}{55}$

331.2	331.1	330.75	331.08	332.5	334.5	335.1	341.0	341.3
$\frac{10.9}{50}$	$\frac{11.0}{25}$	$\frac{21.35}{10}$	$\frac{11.02}{10}$	$\frac{9.6}{12}$	$\frac{7.0}{20}$	$\frac{6.0}{20}$	$\frac{1.341.0}{30}$	$\frac{0.8}{40}$
		FL. BOT. BOX	P.M. Box CULV. MILLER					

342.10 ✓

337.7	338.7	339.6
$\frac{9.9}{20}$	$\frac{8.9}{20}$	$\frac{8.0}{20}$

341.7	341.8	342.0
$\frac{6.4}{20}$	$\frac{5.8}{20}$	$\frac{7.0}{20}$

347.61 ✓

7+71

7+45

7+21.93 Δ 17° LR on SPLIT

7+01.5

7+01

7+00 open drain

6+99.5

333.83

\leftarrow 320.4
 3.4
 50
 SHOULDER
 ON
 HWY

329.6
 4.2
 25
 327.4
 327.5
 328.6
 4.9
 8
 328.9
 5.5
 12
 328.3
 6.3
 50
 327.5

12

315.1
 18.7
 45
 326.7
 7.1
 14
 327.4
 327.5
 328.0
 327.4
 327.4
 6.3
 22
 24
 27
 50
 BEND 90°
 PER FULTON

315.3
 18.5
 45
 320.8
 13.0
 28
 326.7
 7.1
 12
 326.7
 327.3
 328.7
 327.4
 327.5
 6.3
 18
 23
 25
 50
 PER
 FULTON

C x 327.4

326.6

7.3

326.5

7.3

327.48

6.5

333.83 ✓

116.4 Top Island curb

8+11.93 E Hwy

8+109.5 Top Island Curb

8+109.10 E.L. of W. Lane

+85.10 W. edge Cor. Pav. W. Lane Hwy

+75

7+738 Berth

333.83

331.26

2.57
50
curb

329.85
398
curb

329.56
4.27
9.6
curb

13

316.87

169C
39.5
F.L. Bot
Box

P.7

2.78
39.5
Top
Box

329.6
4.2
dirt

4.19
101

331.26
2.57
50

329.88
3.95
5.23
9.5

329.60

320.73

3.10
50

329.41
4.42

327.85
5.98
50

330.54
3.29
50

329.16
4.67

327.68
6.15
50

325.7
5.1

329.2
4.6

333.83

Check Bm to
City & State
BMS

STAT. ON
MCD 149+50
MCD 149+50

8778

8766

8759.53 Beam

758

8750 E.L. of E. Lane

8726.3 wedge of E. Lane

8717.13 G-5

33383

L	323.0	324.8	326.8	333.6	P
	10.8	9.0	7.0	0.2	
	50	9		30	

14

	329.8	328.8	328.3	328.9	330.7
	4.0	5.0	5.5	4.9	3.1
Fill	50	10	20	50	
Shoulder					

329.8
4.0

329.4
4.6

	320.57	329.30	327.93
	3.30	4.53	5.90
	50		50

	327.78	329.34	327.85
	3.05	4.49	5.98
	50		50

329.35
4.48

33383 ✓

check Back to 0100 M.H. 12.65 329.87 329.91
 $\frac{0.04}{0.04}$

T.P. 0.65 342.50 5.93 341.87

T.P. 5.03 347.80 1.11 342.77

T.P. 10.96 343.88 1.08 332.92

T.P. 11.94 334.00 0.47 322.06

LO 107

9167

9138.1 at fence

9100 P.7

8189

T.P. 0.41 322.53 11.91 321.92

33383

297.0
 $\frac{25.5}{50}$ 10 1 312.4 322.5
 $\frac{0.0}{44}$

291.4
 $\frac{31.1}{50}$ 20.5 302.0 313.0
 $\frac{9.5}{40}$

300.4 307.1 313.8 320.3 326.5
 $\frac{22.1}{50}$ $\frac{15.4}{25}$ 87 $\frac{2.2}{23}$ $\frac{+4.0}{50}$

307.3
 $\frac{14.8}{141.5}$
 FL. outlet
 24" PIPE
 10.4 322.9 324.9 326.5
 $\frac{+7.4}{25}$ $\frac{+12.5}{50}$

312.5 318.8 325.6 332.5 338.0
 $\frac{10.0}{33}$ $\frac{2.7}{77}$ +31 $\frac{+10.0}{28}$ $\frac{+15.5}{50}$

322.53 ✓

Laterals No. 1 & No. 2 Alley

Block 44, Hensley Subdivision.

Roberts
W. Moore
Clark
11-5-48

6986L

W.P. 31232

27th

Ed. Hub

St.

INDEXED

WK

NOV 12 1948

4+10

Sewer Lateral No. 2

3+82

Sewer Lateral No. 1

BLOCK

Alley

← 10' → ← 10' →

10' 0" 0+00

26th

St.

INDEXED
NOV 19 1907

CK 5.41 66.30 2.38 63.92 63.92
F.P. 5.09 60.89

4+10 Sewer Lateral No. 2 (0.07' Back Prop. Line)

3+82 Sewer Lateral No. 1 (Stub 10' Back Prop. Line)

4P 5.16 65.98 5.49 60.82

BM 2.39 66.31 63.92

Rd. Elev. Stub Elev. $\frac{2}{2}$ Elev. Prop. Line 17

N.W. B.P. 26th. & Imperial

5.57 60.41 57.51 C-290 57.71 C-270

65.98
N.W. B.P. 26th St. and Imperial Ave.

Staked for Construction
 Monroe Ave. (Texas to Arizona)

Roberts
 W. Moore
 Clark
 11-8-48

60952

WD 31323

[Large handwritten scribbles]

BM

338.96
 S.E. & P.
 Texas and
 Monroe

Arizona St.

18

352.99	352.91	352.83	352.21	351.60	0+00
351.02	351.00	350.98	350.44	349.70	0+20
	348.57		348.05		0+45
346.20	346.18	346.20	345.67	345.15	0+70
345.38	345.37	345.38	344.86	344.34	0+80
344.82	344.83	344.83	344.31	343.77	0+90
343.59	343.58	343.59	343.06	342.55	1+20
342.34	342.34	342.34	341.82	341.30	1+50
341.78	341.79	341.79	341.27	340.75	1+60
341.25	341.76	341.76	341.24	340.72	1+70
341.06	341.10	341.10	340.62	340.12	2+07
340.38	340.72	340.47	339.79	339.51	2+44
339.70	339.76	339.82	339.36	338.76	2+80
339.36	339.37	339.38	338.95	338.52	3+00

Texas Street

Alley in block 243 University Heights

Stake for Construction

F.B. 1776

6940L

Roberts
W. Moore
Clark
11-9-48

W.O. 31095

INDEXED

WK

NOV 12 1948

0+60

(2' Back) 293.85
4.79
4.68
C-0.11

293.69
4.35

294.13 (1' Back)
4.51
4.44
C-0.07

0+40

(2' Back) 293.65
4.99
4.65
C-0.34

293.46
4.56

293.87 (1' Back)
4.77
4.41
C-0.36

0+20

(2' back) 293.38
3.26
4.64
C-0.62

293.14
4.88

293.50 (1' Back)
5.14
4.39
C-0.75

0+00

Prop. Line at Brooks

8.89 298.02 For £ Grades (Add 0.25 for Subgrade)

9.51 298.64

BM S.E.P. Brooks Ave. & Herbert St 289.13

298.04
5.60
5.59 ✓

294.68
5.34 ✓

298.02

298.64

298.02
5.62
5.60 ✓

4

£

Rt

19

2+40

$$\begin{array}{r} \text{(2' Back)} \ 294.67 \\ 3.97 \\ \hline 3.92 \\ \text{C-0.05} \end{array}$$

$$\begin{array}{r} 294.52 \\ 3.50 \end{array}$$

$$\begin{array}{r} 294.96 \\ 3.68 \\ \hline 3.16 \\ \text{C-0.52} \end{array} \quad \text{2' Back}$$

2+20

$$\begin{array}{r} \text{(2' Back)} \ 294.62 \\ 4.02 \\ \hline 3.82 \\ \text{C-0.20} \end{array}$$

$$\begin{array}{r} 294.47 \\ 3.55 \end{array}$$

$$\begin{array}{r} 294.92 \\ 3.72 \\ \hline 3.23 \\ \text{C-0.49} \end{array} \quad \text{(2' Back)}$$

1+95

$$\begin{array}{r} \text{(2' Back)} \ 294.50 \\ 4.14 \\ \hline 3.86 \\ \text{C-0.18} \end{array}$$

$$\begin{array}{r} 294.35 \\ 3.67 \end{array}$$

$$\begin{array}{r} 294.80 \\ 3.84 \\ \hline 3.34 \\ \text{C-0.50} \end{array} \quad \text{(2' Back)}$$

1+70

N. Side of E.w. Alley

$$\begin{array}{r} \text{(2' Back)} \ 294.39 \\ 4.25 \\ \hline 4.04 \\ \text{C-0.21} \end{array}$$

$$\begin{array}{r} 294.24 \\ 3.78 \end{array}$$

$$\begin{array}{r} 294.69 \\ 3.95 \\ \hline 3.31 \\ \text{C-0.64} \end{array} \quad \text{(2' Back)}$$

1+50

s. side of E.w. Alley

$$\begin{array}{r} \text{(1.8' Back)} \ 294.30 \\ 4.34 \\ \hline 3.80 \\ \text{C-0.54} \end{array}$$

$$\begin{array}{r} 294.15 \\ 3.87 \end{array}$$

$$\begin{array}{r} 294.60 \\ 4.04 \\ \hline 3.77 \\ \text{C-0.27} \end{array} \quad \text{(1' Back)}$$

1+15

$$\begin{array}{r} \text{(2' Back)} \ 294.19 \\ 4.45 \\ \hline 4.18 \\ \text{C-0.27} \end{array}$$

$$\begin{array}{r} 293.99 \\ 4.03 \end{array}$$

$$\begin{array}{r} 294.44 \\ 4.20 \\ \hline 3.72 \\ \text{C-0.28} \end{array} \quad \text{(1' Back)}$$

D+80

$$\begin{array}{r} \text{(2' Back)} \ 293.98 \\ 4.66 \\ \hline 4.47 \\ \text{C-0.19} \end{array}$$

$$\begin{array}{r} 293.83 \\ 4.19 \end{array}$$

$$\begin{array}{r} 294.28 \\ 4.36 \\ \hline 4.36 \\ \text{Grade} \end{array} \quad \text{(2' Back)}$$

$$\begin{array}{r} \text{C} \\ 298.02 \end{array}$$

298.64

$$\begin{array}{r} \text{C} \\ 298.02 \end{array}$$

298.64

0+20

0+00 West Line of N. & S. Alley

T.P. 3.17 298.59 2.60 295.42T.P. 4.50 299.59 3.55 295.09

3+20 Prop. Line at Cypress

3+00

2+80

2+60

298.02298.64

Lt.

C

Rt

21

(Line)	294.60 4.99 4.89 C-0.10	294.32 4.27	294.60 4.99 5.18 F-0.19	(1' Back)
--------	----------------------------------	----------------	----------------------------------	-----------

(Line)	294.30	294.25 4.34	294.59	(1.6' Back)
--------	--------	----------------	--------	-------------

Set on other alley

For C Grades only - (add 298.59 for subgrade)

299.59

For.	293.94 4.70 4.70 ✓
------	--------------------------

293.69 4.35 ✓

For.	294.67 4.57 4.57 ✓
------	--------------------------

(1' Back)	294.23 4.41 3.38 C-1.03	293.99 4.65	294.41 4.23 2.70 C-1.53	(2' Back)
-----------	----------------------------------	----------------	----------------------------------	-----------

(2' Back)	294.47 4.17 3.21 C-0.96	294.29 3.73	294.71 3.93 2.45 C-1.48	(2' Back)
-----------	----------------------------------	----------------	----------------------------------	-----------

(2' Back)	294.61 3.05 3.92 C-0.31	294.45 3.57	294.88 3.76 3.85 C-0.91	(2' Back)
-----------	----------------------------------	----------------	----------------------------------	-----------

298.02298.64

1796

1764

1732

1700

0780

0760

0740

$$\begin{array}{c} \text{d} \\ 299.59 \end{array}$$

$$\underline{299.59}$$

H

$$\begin{array}{r} 293.10 \\ 6.49 \\ (1' \text{ Back}) \quad \underline{6.24} \\ C-0.25 \end{array}$$

$$\begin{array}{r} 293.53 \\ 6.06 \\ (2' \text{ Back}) \quad \underline{5.64} \\ C-0.42 \end{array}$$

$$\begin{array}{r} 293.96 \\ 5.63 \\ (2' \text{ Back}) \quad \underline{5.29} \\ C-0.54 \end{array}$$

$$\begin{array}{r} 294.38 \\ 5.21 \\ (2' \text{ Back}) \quad \underline{5.04} \\ C-0.17 \end{array}$$

$$\begin{array}{r} 294.56 \\ 5.03 \\ (0.19' \\ \text{ Inside}) \quad \underline{4.49} \\ C-0.54 \end{array}$$

$$\begin{array}{r} 294.67 \\ 4.92 \\ (0.04' \\ \text{ Inside}) \quad \underline{4.54} \\ C-0.38 \end{array}$$

$$\begin{array}{r} 294.69 \\ 4.90 \\ (\text{Line}) \quad \underline{4.77} \\ C-0.13 \end{array}$$

E

$$\begin{array}{r} 292.92 \\ 5.99 \end{array}$$

$$\begin{array}{r} 293.23 \\ 5.36 \end{array}$$

$$\begin{array}{r} 293.64 \\ 4.95 \end{array}$$

$$\begin{array}{r} 294.05 \\ 4.54 \end{array}$$

$$\begin{array}{r} 294.26 \\ 4.33 \end{array}$$

$$\begin{array}{r} 294.57 \\ 4.22 \end{array}$$

$$\begin{array}{r} 294.39 \\ 4.20 \end{array}$$

RE

22

$$\begin{array}{r} 293.10 \\ 6.49 \\ 6.05 \\ (2' \text{ Back}) \quad \underline{\hspace{1cm}} \\ C-0.44 \end{array}$$

$$\begin{array}{r} 293.52 \\ 6.07 \\ 5.25 \\ (2' \text{ Back}) \quad \underline{\hspace{1cm}} \\ C-0.82 \end{array}$$

$$\begin{array}{r} 293.94 \\ 5.65 \\ 5.49 \\ (2' \text{ Back}) \quad \underline{\hspace{1cm}} \\ C-0.16 \end{array}$$

$$\begin{array}{r} 294.55 \\ 5.24 \\ 4.65 \\ (0.4' \text{ Back}) \quad \underline{\hspace{1cm}} \\ C-0.59 \end{array}$$

$$\begin{array}{r} 294.56 \\ 5.03 \\ 4.78 \\ (0.5' \text{ Back}) \quad \underline{\hspace{1cm}} \\ C-0.25 \end{array}$$

$$\begin{array}{r} 294.67 \\ 4.92 \\ 4.83 \\ (2' \text{ Back}) \quad \underline{\hspace{1cm}} \\ C-0.09 \end{array}$$

$$\begin{array}{r} 294.69 \\ 4.90 \\ 5.00 \\ (2' \text{ Back}) \quad \underline{\hspace{1cm}} \\ F-0.10 \end{array}$$

$$\begin{array}{c} \text{d} \\ 298.59 \end{array}$$

$$\underline{299.59}$$

Lt.

¢

Rt.

23

0+01 Sewer Lateral Nal on N&S. Alley

298.64

2+06.56 East Line of Block 13 T.J. Higgins Sub.

298.59299.59

288.83

9.81

4.33

C-5.08

298.64

289.03

9.61

4.73

C-4.88

(5' Back
Prop. Line)

(2' Back)

293.10

6.49

6.52

F. 0.03

293.10

5.19

298.59299.59

293.10

6.49

6.04

C.045

(2' Back)

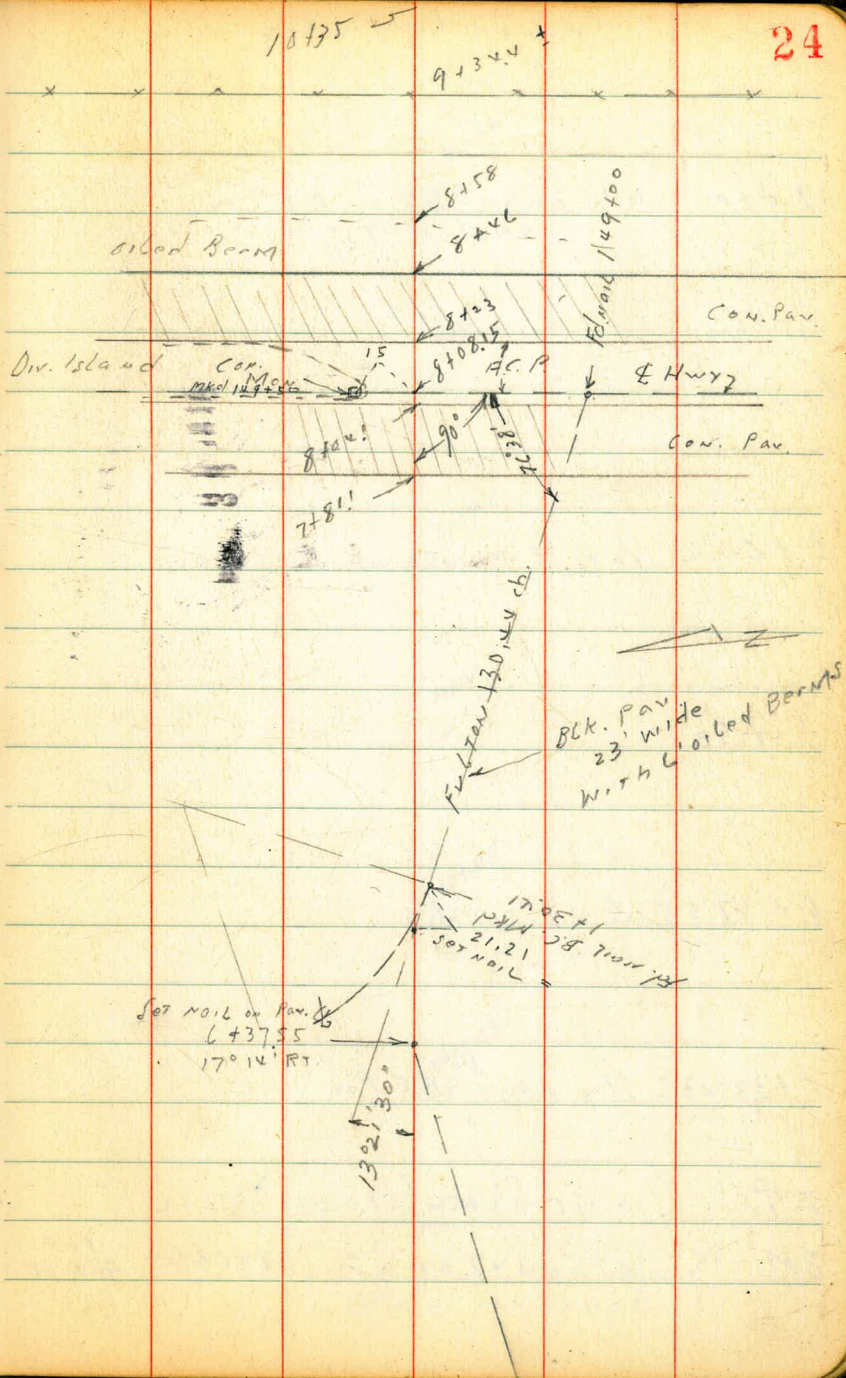
Proposed Align. change
to Vet. Hospital, Linda Vista
from P7.

Moore
3099
Stearns
Bunch
12-24-48.

No. 90079

INDEXED
WIK
DEC 27 1948

24



Sewer Levels

7+10 Nly edge End AC Pav
and Beg oil

327.66
986

7

327.75
977

6+60.6 Int. of Tang on FULTON

328.82
870

+50

329.21
831

6+37.55 Δ 17° x 1 ft

329.75
777

6+33.43⁺ Sly edge ^{Bog} AC Pav

329.93
759

T.P. 0.46 337.52 ✓ 10.03 337.06

337.52 ✓

B.M. 0.73 347.09 346.36 TOP
1/2" BOLT

CIR TOP F.H. S Ely Cor FULTON and
East Ingersol

Contd P, 25

8758

8746 Hedge Con Pav E Lane

8773 Hedge Con, E Lane

87815 E Hwy

8704.1 Hedge Con Pav W Lane

7811 end oil Hedge Con Pav

7750 oil

26

8

9.0 ^{328.5}

8.82 ^{328.70}

8.81 ^{328.66}

8.8 ^{328.7}

8.83 ^{328.69}

9.05 ^{328.97}

9.9 ^{327.6}

Easement Bk. 9 Marsene Park Sub.

Map 7844 Sheet 2

Roberts
vs Moore
Clark
11-70-48

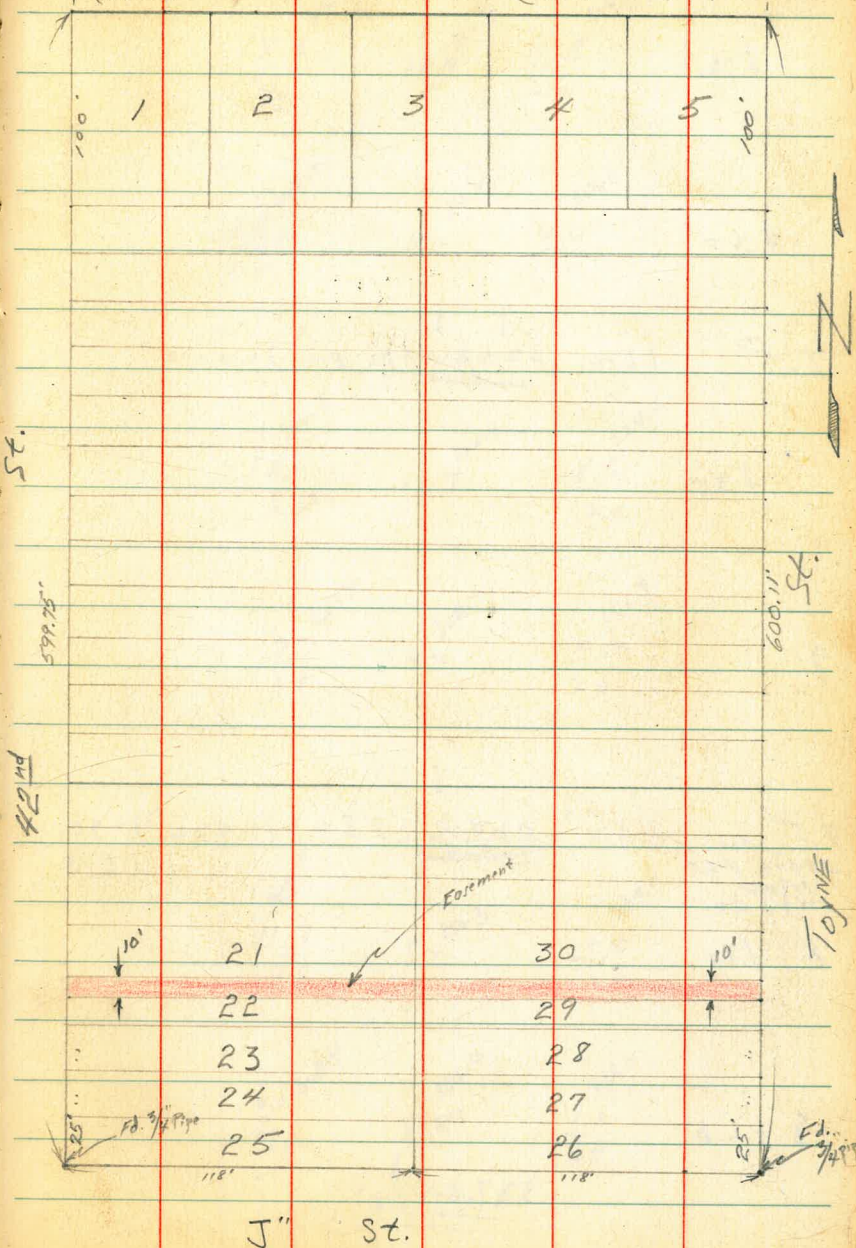
FB 1632, 1638

6916L - 3607B

INDEXED
WIK
NOV 12 1948

Market St.
(E.L.P. & Market W. Prop. Line 42nd)

(C.T. W. Prop. Line of Toyns
and 8' Line on N. Side
Market) 27



21 30
22 29
23 28
24 27
25 26
118' 118'

J St.

72

75

T.P. 1.62 321.84 12.84 320.22

735

9

T.P. on 334 333.06 780 329.72 329.62
STATE PAT. P.13
Mon
149750

8 780

8 + 68

337.52

Lt

Q

R

28

^{306.2}
15.6
25

^{310.9}
10.9
20

^{315.0}
5.8
20

^{314.4}
17.4
25

^{311.4}
10.4
20

^{317.8}
4.0
20

321.84

^{314.5}
18.6
25

^{320.4}
12.7
20

^{324.5}
8.6
20

^{323.4}
9.7
25

^{328.7}
4.4
20

^{332.9}
0.2
20

333.06

^{332.3}
11.7
25

^{337.0}
5.2
20

^{337.0}
0.5
25

^{328.4}
9.1
25

^{332.0}
5.5
20

^{336.2}
1.3
25

337.52

Check to State B.M., 3/4" Iron Bolt |
 8' RT of 151 + 84
 STATE STA 5.72 316.12 316.02

10435

195

321.84

$$\begin{array}{r} 30.6 \\ 3.7 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 325.3 \\ + 3.5 \\ \hline \end{array}$$

$$\begin{array}{r} 329.8 \\ + 8.0 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 322.3 \\ 9.5 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 318.5 \\ + 3 \\ \hline \end{array}$$

$$\begin{array}{r} 322.3 \\ + 0.5 \\ \hline 20 \end{array}$$

321.84

Notes Reduced. 12/27/40

X-Sect. Alley Block 179

Maunassee and Schiller

Roberts
W. Moore
Clark
2-7-49
WD, 31512

Beardsley to Sigsbee between

Logan and Kearny

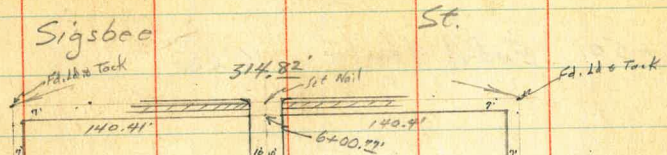
T.P. 359 Map 209

INDEXED

WIK

FEB 10 1949

30



Note: -

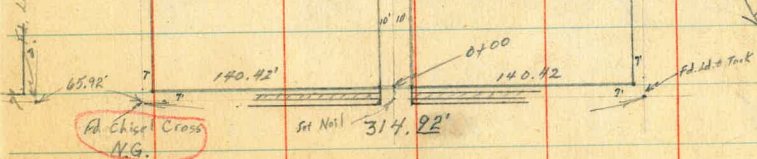
Improvements in oil
both Sigsbee and
Beardsley Sts. SIGSBEE:

- Cb. face to edge
sidewalk 2.5'. Side-
walk 5'. Cb. face
to property 10'.

BEARDSLEY: -

Cb. face to edge of
sidewalk 3'. Sidewalk
5'. Cb. face to
property 10'.
2' Cb. Rad.

Ed. 14 x 16 Tack across Logan
Logan



Beardsley

St.

Ave

Ave.

Block

Kearny

179

+ 41 - FI BM
Cont'd From Page 30

0+50 End of Theatre 10' Lt.

0+48.5 End Board Fence 10.2' Rt.

0+46 5' Fire exit of theatre 10.2' Lt

0+16 End Wire Fence Begin Board Fence 10' Rt.

0+10 Gas Meter 9.40' Lt. to Near Edge 8.70' Lt to Guard Posts ^{4" Pipe}

0+04 5' Fire exit of theatre 10.2' Lt. Rod = 4.72

0+00 Prop. Line on Beardsley

0-2 End. Curb on Left Rod = 4.70 Elev. = 43.78

0-10 Curb Line on Beardsley

0-30 5' Beardsley St.

BM 2.44 48.78

46.04 ^{SEBY}
Kearney +
Beardsley

Lt. 31 Rt.

42.58
5.9
70
42.85
5.6
70
42.94

43.72
4.76
10.2
Floor

Posts

43.64
4.80
10.05
5.145
43.52
4.96
Rim M.H.
4.40
9.30
Cb.
4.62
9.30
Gutt.
Begin
wire fence
10

42.21	4.99	42.00	42.06	43.52	43.92	43.07	43.52	43.89	43.79	44.43	44.58	45.22
6.27	6.94	5.48	6.22	4.96	5.36	5.41	5.16	4.59	4.69	4.05	3.90	3.26
100	100	50	50	12	12	50	12	12	50	50	100	100
Ch.	Gutt.	Ch.	Gutt.	Ch.	Gutt.		Gutt.	Ch.	Gutt.	Ch.	Gutt.	Ch.

42.07
6.41
100
42.65
6.93
50
43.44
5.04
44.20
4.28
50
44.98
3.60
100

48.48

Cont'd From Page 31

1720 NE. Cor. House 93' Lt

1707 4" Soil Pipe 9.0' Lt. to face

1704 End of Board Fence ^{9.1' Lt.} SE. Cor. House 96' Lt.

1700

0+97.5 Power Pole #A1790 8.6' Lt. to Center

0+76' Begin Board Fence 9.8' Lt.

0+74.5 ¹ Power Pole #12392H - 10.4' Rt. to Center of Pole
Begin Board Fence 8.6' Rt

0+68 ϕ of Double Garage 9.3' Lt.

0+63 ϕ of Double Garage 11.3' Rt

48.48

ft.

ϕ

Rt. 32

41.78
6.7
9.3
Dist. Elev.

41.68 41.64 42.16 42.38 42.48 42.48
6.8 6.8 6.3 6.1 6.0 6.0
20 12 10 70 70 15

42.18
6.3
9.9
Dist. Elev.

42.98
5.5
11.3
Dist. Elev.

48.48

Cont'd From Page 32

T.P. 4.21 45.70 6.99 41.49

1+69 £ Single Garage 112' Rt.

1+61 £ Double Garage 92' Lt

1+54 End of Board Fence 10' Rt.

1+50

1+45 £ Single Garage 9' Lt.

1+39 End Board Fence 92' Lt.

1+29 Begin Board Fence 92' Lt.

1+24 £ Single Garage 93' Lt.

48.48

Lt.

£

Rt.

33

41.58
6.9
11.9
Dirt Floor

41.58
6.9
9.2
Dirt Floor

41.68
6.8
9.2
41.98
6.5
41.78
6.7
10

41.78
6.7
9.1
Dirt Floor

41.98
6.5
9.3
Dirt Floor

48.48

Cont'd From Page 33

2+24 End Picket Fence begin shed 9 $\frac{3}{4}$ ' Lt.

2+15 $\frac{1}{2}$ 2' Sidewalk 9 $\frac{1}{2}$ ' Lt. Begin Picket Fence 9 $\frac{1}{2}$ ' Lt.

2+14 $\frac{1}{2}$ Double Garage 9 $\frac{1}{2}$ ' Rt.

2+0.7 $\frac{1}{2}$ Single Garage 11.6' Lt.

2+04 $\frac{5}{8}$ End Board Fence 10' Rt.

2+00 Power Pole #A1766 9.2' Lt to Center

1+95 End Shed 10 $\frac{5}{8}$ ' Rt. Begin Board Fence 10' Rt.

1+90 $\frac{1}{2}$ Double Garage 11.2' Lt.

1+75 Begin Shed 9 $\frac{3}{4}$ ' Rt.

45.70

Lt.

$\frac{1}{2}$

Rt.

34

41.20
4.50
9.9
conc.

41.20
4.5
9.8
Dirt Floor

41.20
4.5
11.6
Dirt Floor

41.30
4.4
10

41.40
4.3

41.40
4.4
10

41.20
4.5
11.7
Dirt Floor

45.70

Cont'd From Page 34

2+64 E of 3' WIDE DOOR 10' Rt

2+61 END BOARD FENCE & BEGIN SHED 8' Lt

2+56 S.W. Cor. Bldg. 9' Lt. BEGIN SHED AT 9' Rt.

2+52 E of single garage 9' Lt.

2+50

2+46 End of shed 8' Lt. Begin^{Bd.} Fence 8' Lt

2+33 E Double Garage 9' Lt.

2+26 S.E. Cor. Bldg. 9' Lt.

2+25 Telephone Pole # 305458H 8' Lt to Center

45.70

Lt.

E

Rt. 35

41.00
47
107
Dirt Floor

41.00
47
93
Dirt Floor

40.40
53
15

40.40
53
70

41.10
46
88

41.20
45

41.00
47
93

41.10
46
96
Dirt Floor

45.70

CONT. FROM Pg. 35

Lt.

£

Rt.

36

3+47 END OF PICKET FENCE - 10⁴ RT.

3+41 TELEPHONE POLE #4105604 8⁷ RT. TO CENTER

3+40 END OF DWELLING - 9⁴ LT.

3+27 END OF BOARD FENCE - BEGIN SHED - 8⁹ LT.
DWELLING

3+12 END OF BOARD FENCE - BEGIN PICKET FENCE - 10¹ RT.

3+02 POWER POLE #A1750 - 7⁶ LT. TO CENTER.

3+01 END OF SHED & BEGIN BOARD FENCE - 9¹ LT.

3+00

2+89 END OF SHED - 9² RT. & BEGIN BOARD FENCE - 9² RT.

2+81 £ of SINGLE GARAGE - APRON 9² RT. - GARAGE 10² RT.

45.70

40.80
~~49~~
91

40.70
50

40.90
~~48~~
10

41.00
~~47~~
15

41.07
~~161~~
97
CONC.

41.14
~~156~~
102
CONC.

45.70

Cont. From Pg. 36

4+13 E of 3 CAR GARAGE - 10° Rt. DIRT FLOOR

4+02 POWER POLE #A173A - 8° LT

4+00

3+90 BEGIN OF PATCHED IRON SHEET & BOARD FENCE - 8° LT

3+83 E of SINGLE GARAGE - 8° LT

3+73 E of SINGLE GARAGE - 14° Rt

3+66 E of DOUBLE GARAGE - 12° LT

3+57 END OF BOARD FENCE - 12° LT

3+53 JOG IN BOARD FENCE - 9° LT. & 12° LT.

3+50

15.70

LT.

E

39.40

Rt.

37

63
102
DIRT FLOOR

40.10
56
9
39.80
61
9
39.40
63
2
39.30
64
10
39.50
63
10
39.70
60
15

40.20
55
89
DIRT FLOOR

40.16
554
140
CONC. FLOOR

40.20
55
120
DIRT FLOOR

40.40
53
15
40.40
53
9
40.20
53
40.20
53
10
40.10
56
15

15.70

CONT. FROM PAGE 37

LEFT

±

RIGHT

38

TELEPHONE POLE # JPA 1719 & # A10559H - 93 Rt TO CTR.
BASIN BOARD FENCE - 102 Rt.

A+74 END OF SHED & BEGIN BOARD FENCE.

A+68⁵ E OF SINGLE GARAGE - 10⁵ Rt.

A+67 BEGIN OF SHED - 8⁹ Lt.

A+63 END OF BOARD FENCE - 11¹ Rt.

A+51 END OF SHED - 8⁵ Lt.

A+50 END OF DWELLING - 10⁷ Rt. & BEGIN BOARD FENCE - 11³ Rt.

A+45 2" SOIL PIPE - 10³ Rt.

A+38 END OF BOARD FENCE & BEGIN DWELLING - 10⁵ Rt.

A+27 E OF 2" WIDE CONC. WALK - 11⁰ Rt.

A+26 BEGIN BOARD FENCE - 10⁵ Rt.

A+23 END OF PATCHED IRON SHEET & BOARD FENCE & BEGIN SHED - 9¹ Lt.

45.70

3770	3710	3700	3700	3640
$\frac{80}{7}$	$\frac{86}{6}$	82	$\frac{85}{7}$	$\frac{93}{10}$
				DIRT FLOOR

3820	3760	3740	3760	3790	3690
$\frac{75}{85}$	$\frac{79}{7}$	$\frac{83}{7}$	81	$\frac{7}{10}$	$\frac{8}{12}$

35.60	35.24	37.64
$\frac{71}{110}$	$\frac{76}{110}$	$\frac{802}{210}$
DIRT	CONC.	

45.70

5+20

5+19 Begin Shed 10' RT

5+15 E Conc. Steps & Walk 3' Wide - 10' RT. 2 Steps 1' wide.

5+06 Power Pole # A1716 - 8' Lt.

5+05 Begin Board Fence 13' Lt.

T.P. 0.86 38.00 8.56 37.14 Mail in Telephone Pole

5+00

4+95 E of DOUBLE GARAGE - 9' Lt.

4+84.5 End of Board Fence - 9' Lt.

15.70

37.20	36.60	35.80	35.00	35.32	34.90
0.8	14	2.2	3.0	2.7	3.1
135	70	75		70	10.8

35.14	33.87
2.86	4.13
708	13
conc.	conc.

38.00

36.90	36.20	36.10	35.90	36.10	35.70	34.50
8.5	9.5	9.6	9.8	9.6	10.2	11.2

8.2 37.00
9.2
DIRTY ROAD

15.70

Cont'd From Page 39

Lt.

¢

Rt.

40

5+63 } Begin Conc. Retaining Wall on Angle 12¹ Rt
End Dwelling 12¹ Rt

32.72
5.28
12.7
conc.

5+57 End

29.60 29.70 32.50 32.60 31.90 32.50 32.90
8.4 8.3 5.5 5.4 6.1 5.3 5.1
20 13 12 10 6.1 7.0 13

5+52 Begin Dwelling 12⁶ Rt

5+50 End of Shed Begin Picket Fence 11¹ Rt.

29.80 29.80 31.10 32.60 33.10 32.80 33.20
8.2 8.2 6.9 5.4 4.9 5.2 4.8
25 15 14 11 10 5.2 7.6

5+34

30.20 30.60 32.30 35.00 34.10 34.60
7.8 7.4 5.7 3.0 3.9 3.4
25 18 16 10 3.9 7.0

5+33

33.00 33.00 35.20 34.10 34.60
5.0 4.7 2.8 3.9 3.4
20 16 10 3.9 7.0

5+28

35.60 35.70 35.60 34.60 34.80
2.2 2.3 2.4 3.4 3.2
20 16 10 3.4 7.0

5+26 Jog in Fence 10¹ Lt + 13⁵ Lt

38.00

38.00

Cont'd From Page 40

6+00.77 Prop. Line on Sigsbee

6+00.5 Begin Paving & Curbs End of Drive way

5+90 Driveway Angles to point at End

5+80 End Board Fence 13' Lt.

5+73 Telephone Pole (No Number) 10' Rt to Center

Bottom of Conc. Steps from Porch 12' Rt

5+67.5 Begin Conc Drive Parallel to Alley 11' Rt

5+66 End of Conc. Retaining Wall 9' Rt.

5+65 Across Top Conc. Porch 11' Rt

38.00

Lt.

±

Rt. 41

26.45
26.19
25.85
26.05
26.12
26.93

$\frac{11.52}{9.8}$ Cb.	$\frac{11.81}{9.8}$ Gutt.	12.15	$\frac{11.95}{9.8}$ Gutt.	$\frac{11.88}{9.8}$ Cb.	$\frac{14.07}{10.8}$ conc.
----------------------------	------------------------------	-------	------------------------------	----------------------------	-------------------------------

27.40
27.50
27.20
27.90
27.92
28.17

$\frac{10.6}{20}$	$\frac{10.5}{10}$	10.8	$\frac{10.1}{10}$	$\frac{10.08}{11}$ conc.	$\frac{9.83}{20}$ conc.
-------------------	-------------------	------	-------------------	-----------------------------	----------------------------

28.80
28.60
29.60
29.50
28.90
29.50
28.60

$\frac{9.7}{30}$	$\frac{9.4}{20}$	$\frac{8.5}{13}$	$\frac{8.5}{10}$	9.1	$\frac{8.5}{10}$	$\frac{9.40}{11}$ conc.
------------------	------------------	------------------	------------------	-----	------------------	----------------------------

29.11
29.11

$\frac{8.89}{11}$ conc.	$\frac{8.89}{20}$ conc.
----------------------------	----------------------------

29.50
29.50
31.80
31.90
31.00
30.70
31.74
31.70
31.70
29.14
29.12

$\frac{8.5}{20}$	$\frac{8.5}{14}$	$\frac{6.2}{13}$	$\frac{6.1}{10}$	7.0	$\frac{7.3}{9}$ Ret. wall	$\frac{6.26}{9}$ conc.	$\frac{6.3}{9}$ dirt	$\frac{6.3}{10}$	$\frac{8.86}{11}$ conc.	$\frac{8.88}{18}$
------------------	------------------	------------------	------------------	-----	------------------------------	---------------------------	-------------------------	------------------	----------------------------	-------------------

31.60
29.15
31.50
29.18

$\frac{6.40}{11.3}$ conc.	$\frac{8.85}{11.3}$ conc.	$\frac{6.50}{17.2}$ conc.	$\frac{8.82}{17.2}$ conc.
------------------------------	------------------------------	------------------------------	------------------------------

38.00

Cont'd from Page 41

Check			2,35	46.04 = 46.64	Starting B/A
TP	691	48.39	4.46	41.48	
TP	8,80	45.94	1.15	37.14	
T.P.	12.00	38.29		26.29	

Check			4.87	23.40 = 23.50	NE BP Keorny and SIGSBEE ↓
T.P.	1.78	28.27	11.71	26.29	

6 + 30.77 $\text{\textcircled{L}}$ Sigbee

6 + 10.77 Curb Line on Sigbee

38.00

LE

$\text{\textcircled{L}}$

RE

42

Need New Ch. Rot. on the Right

27.48	28.21	26.48	27.19	26.34	25.71	25.22	25.45	25.43	25.20	26.28	25.84	24.50	25.10
10.52	9.77	11.50	12.81	11.64	12.27	12.28	12.55	12.57	12.50	11.72	12.19	13.50	12.96
100	100	50	50	72	12	10	10	10	10	12.8	12.8	50	50
Gutt	cb.	Gutt	cb.	cb.	Gutt.			Gutter		cb.	cb.	Gutt	cb.

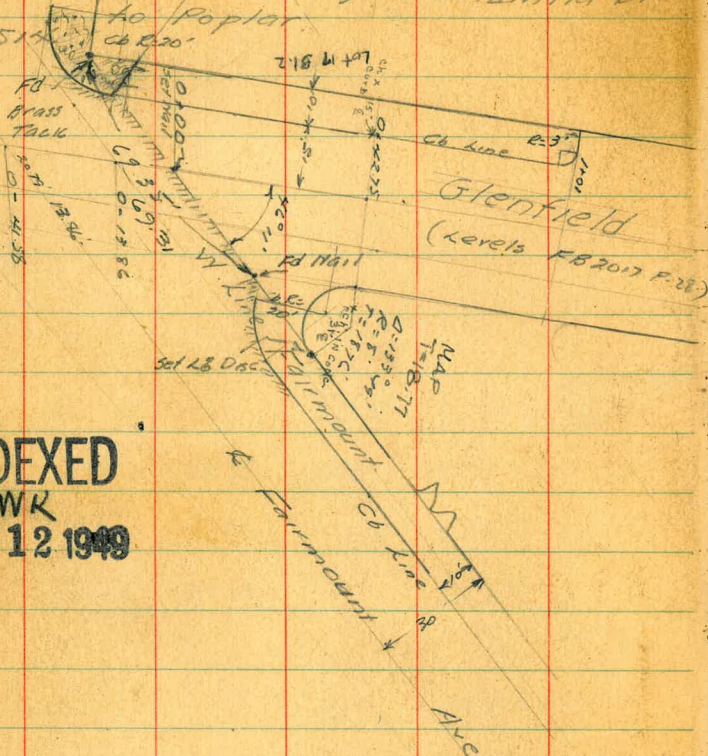
38.00

14.21
100
Gutt

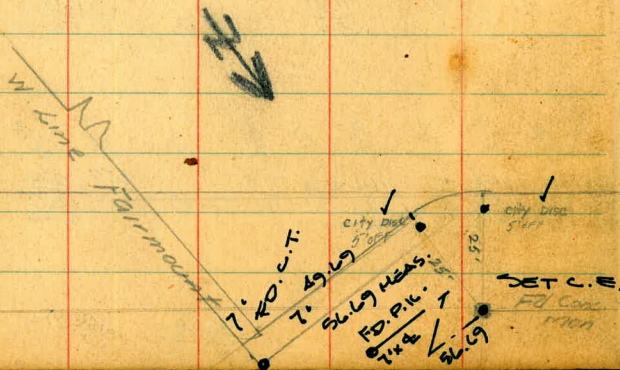
14.22
100
cb.

Mar 1949
Hendricks
Bramby
Greer
Rorer
No #31514

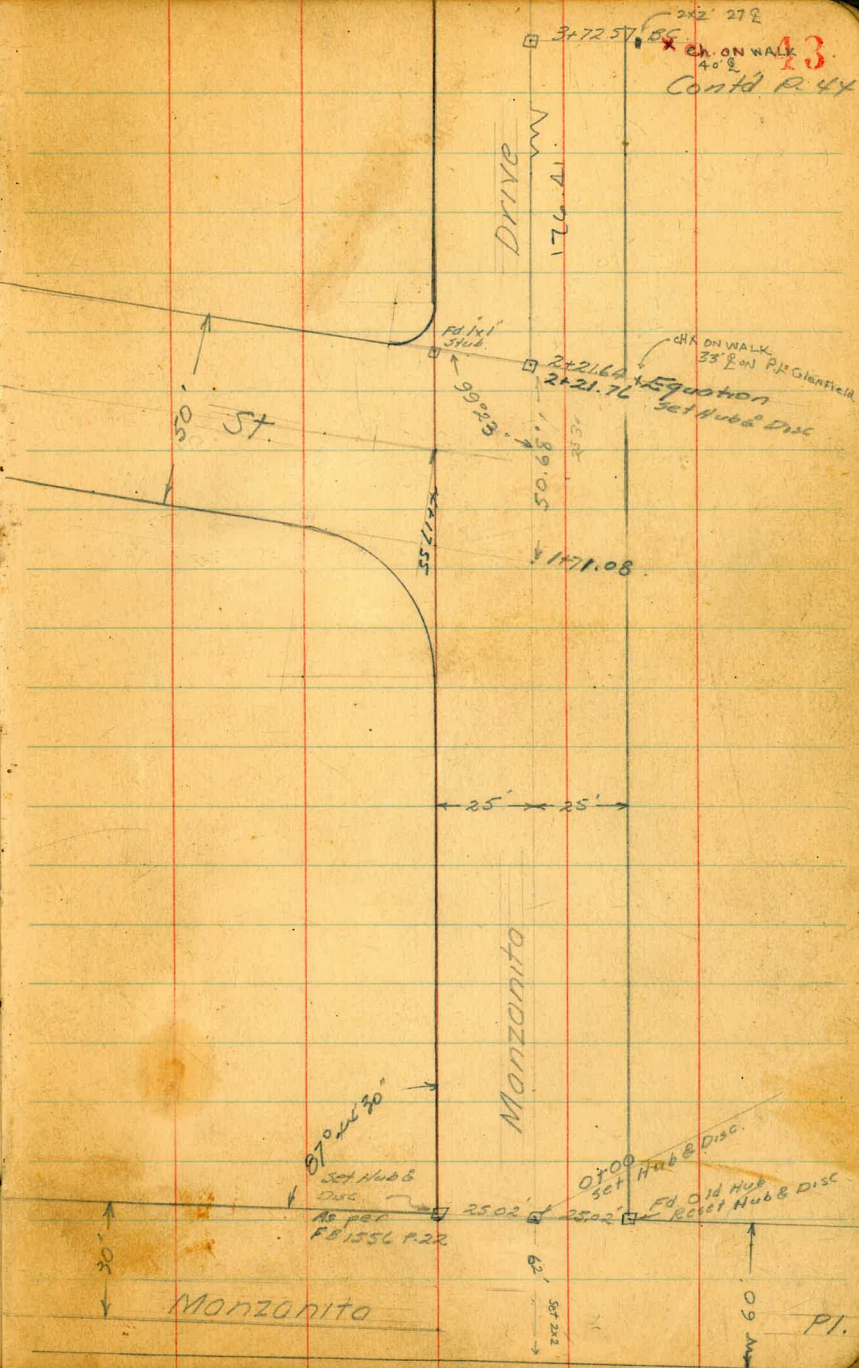
X Section Manzanita Dr.
Manzanita Pl. to Marlborough
& Marlborough Manzanita Dr.
to Poplar



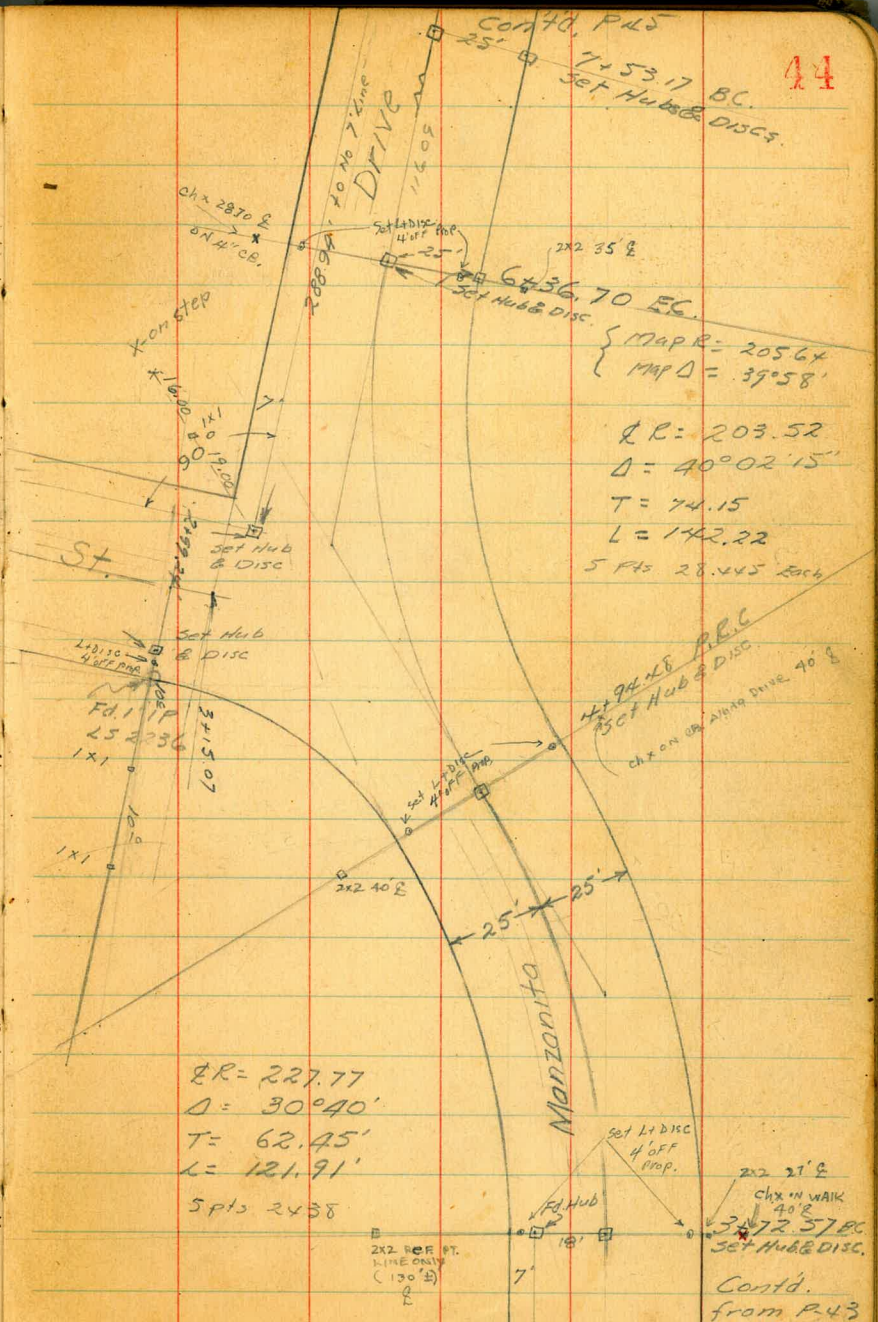
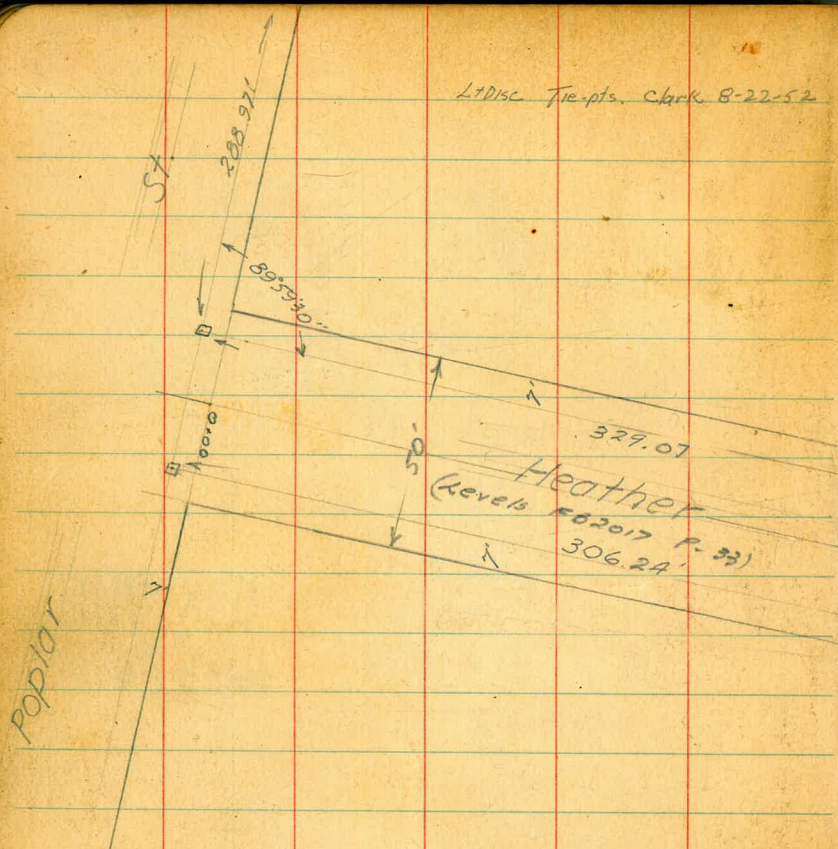
INDEXED
WK
APR 12 1949



242' 272'
3772 57.85
CH ON WALK
40' 2'
43
Cont'd P. 44



L1 Disc Tie pts. Clark 8-22-52



44

$\left\{ \begin{array}{l} MAP R = 205.64 \\ MAP \Delta = 39^{\circ}58' \end{array} \right.$

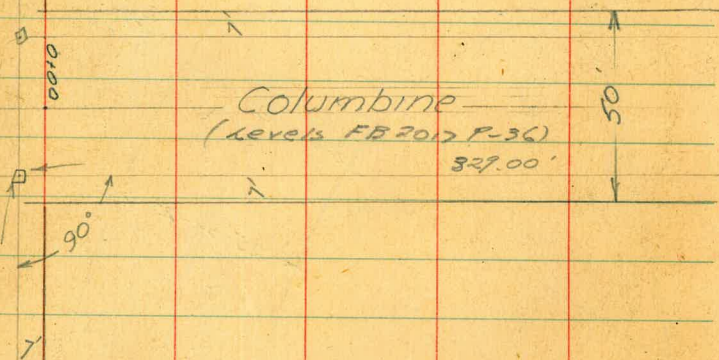
$R = 203.52$
 $\Delta = 40^{\circ}02'15''$
 $T = 74.15$
 $L = 142.22$
 5 pts 28.445 each

$R = 227.77$
 $\Delta = 30^{\circ}40'$
 $T = 62.45'$
 $L = 121.91'$
 5 pts 2438

$R = 227.37$
 $\Delta = 40^{\circ}R$
 $L = 121.91$
 Set Hub & Disc.
 Contd.
 from P. 43

11 758.57
 9766.98
 1491.57

ST.



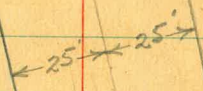
Poplar

288.97'

Cont'd. R 46

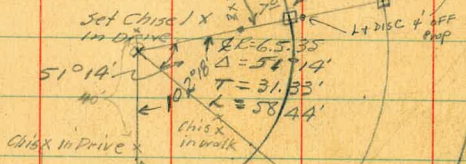
11758.55 BC
 Set Hub & Disc. 15

Fd. Hub Reset



DRIVE

Map R = 6525
 Changed to fit
 Pts. Fd.



Fd. old org
 Hubs re-
 placed with
 2x2 Pts
 2 Discs
 9766.98 BC
 Set Hub & Disc.

ST.



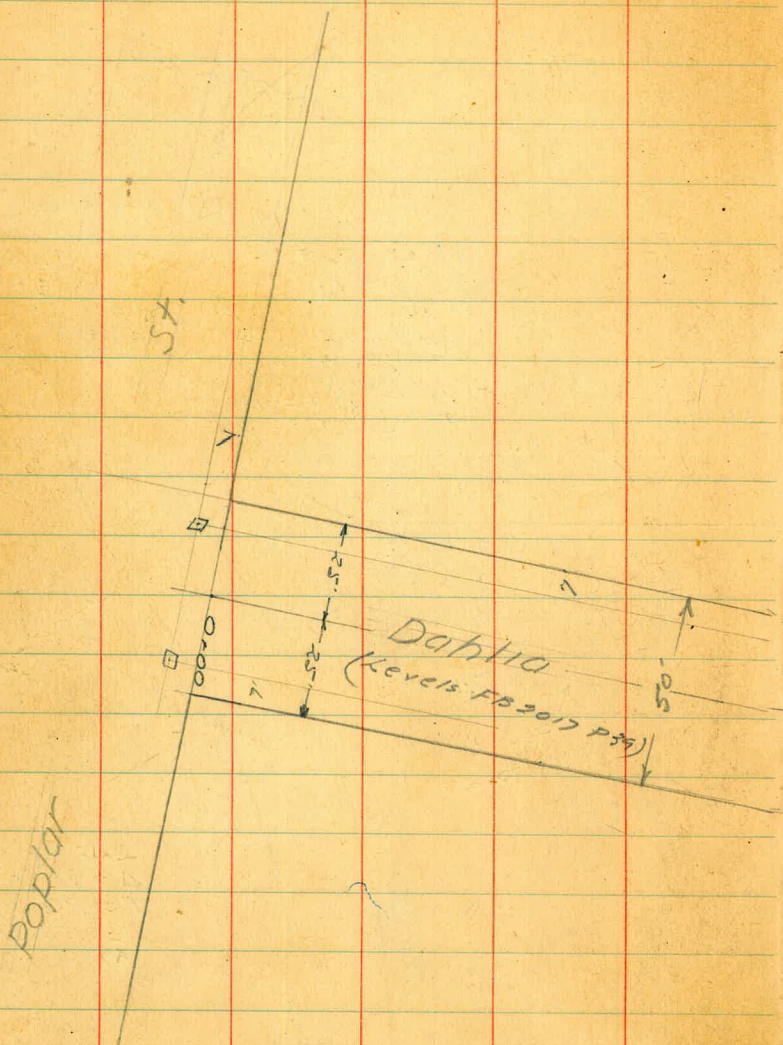
432
 Pts. 2x2
 Fence Cor

E.C. = 228.65'
 Delta = 38.56'
 T = 80.82'
 L = 155.37

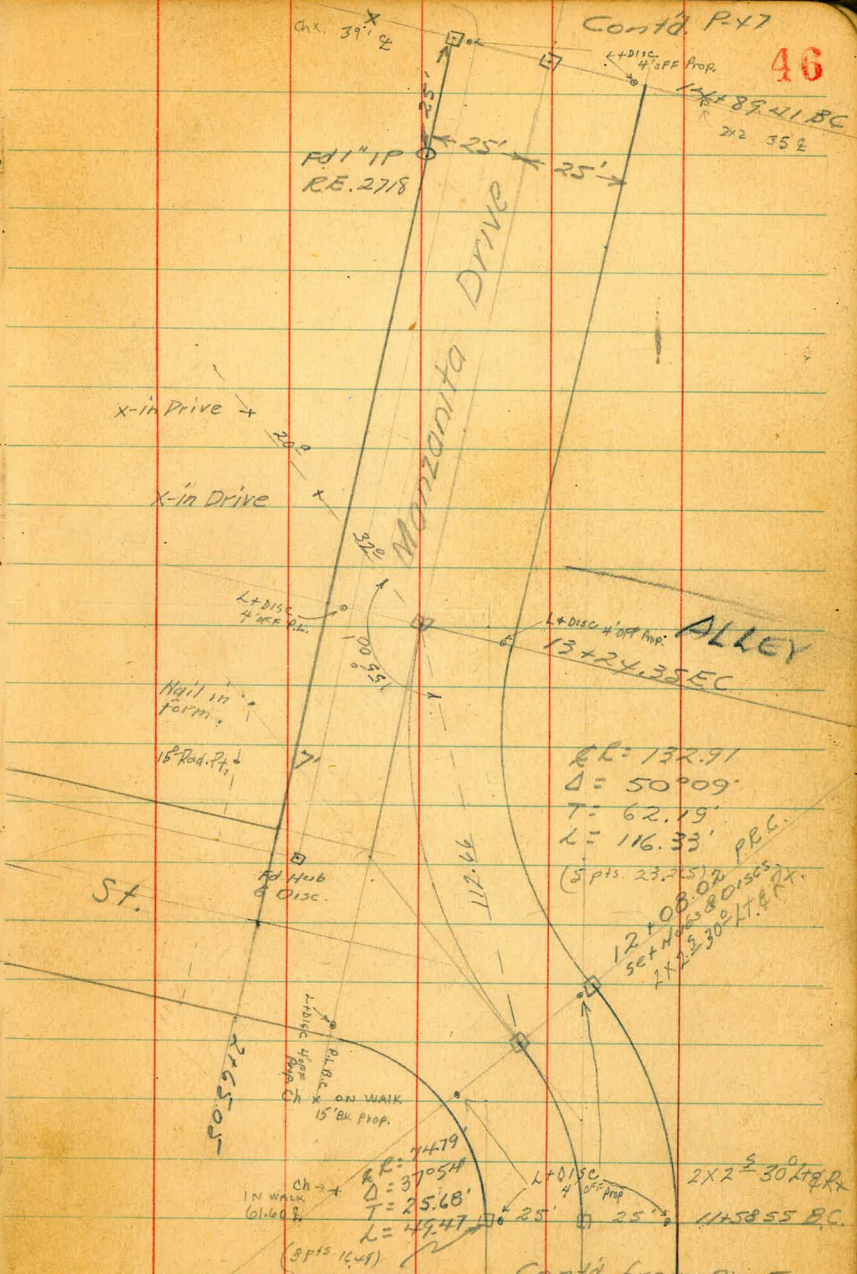
2 Pts 25.893 each
 Map R = 225.25
 Changed to fit
 Points Fd.

7153.17 BC
 Set Hubs & Discs.

Cont'd from P. 44



Cont'd. P. 47
 46
 13+89.41 BC
 2x2 35 E

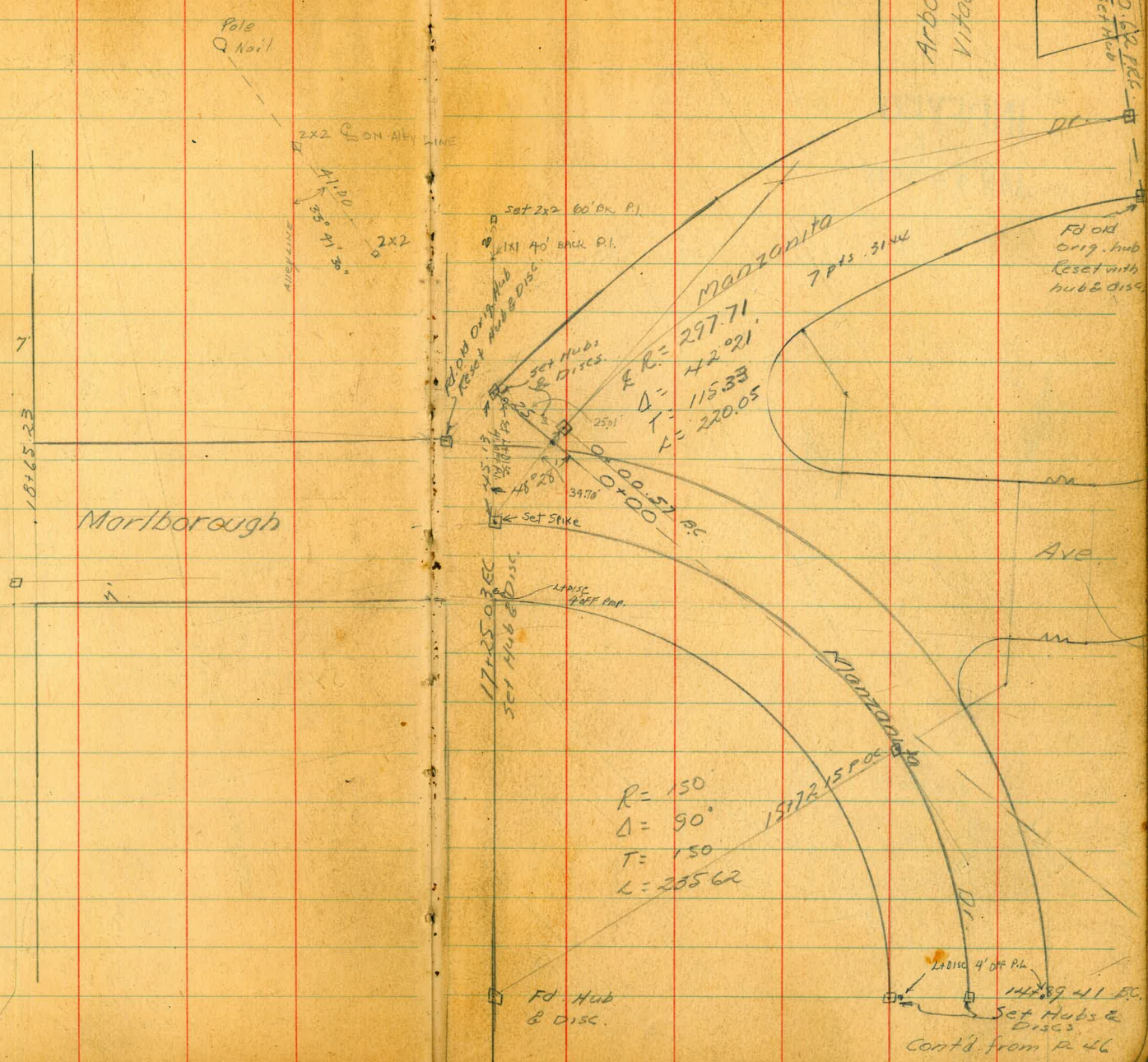


Ch →
 IN WALK
 01.603
 $R.C. = 114.79$
 $\Delta = 37^{\circ} 54'$
 $T = 25.68'$
 $L = 149.47'$
 (3 Pts. 1.49)

$R.C. = 132.91$
 $\Delta = 50^{\circ} 09'$
 $T = 62.15'$
 $L = 116.33'$
 P.C.
 (5 Pts. 23.25)

Cont'd. from P. 45

FD old orig
 Hub Rest
 WITH Hub
 & DISC



Cont'd. P. 48
 2x2.00 P.C.
 47
 ch Hub

Arbor Vitae

Pole Q Nail

2x2 G ON AVE LINE

41.20
 35° 21' 38"
 2x2

Set 2x2 60' BK P.I.

1x1 40' BACK P.I.

FD Old Orig. Hub
 Reset with hub & disc

Set Hubs & DISCS

$R = 297.71$
 $\Delta = 42.021$
 $T = 115.33$
 $L = 220.05$

7 Pts. 3144

FD old Orig. hub
 Reset with hub & disc

18165.23
 7

Marlborough

17125.07 EC
 Set Hub & Disc

Set Spike

LAISE 4' OFF C.P.

$R = 150$
 $\Delta = 90^\circ$
 $T = 150$
 $L = 235.62$

15772.15 P.O.C.

Ave.

Manzanita

FD Hub & Disc

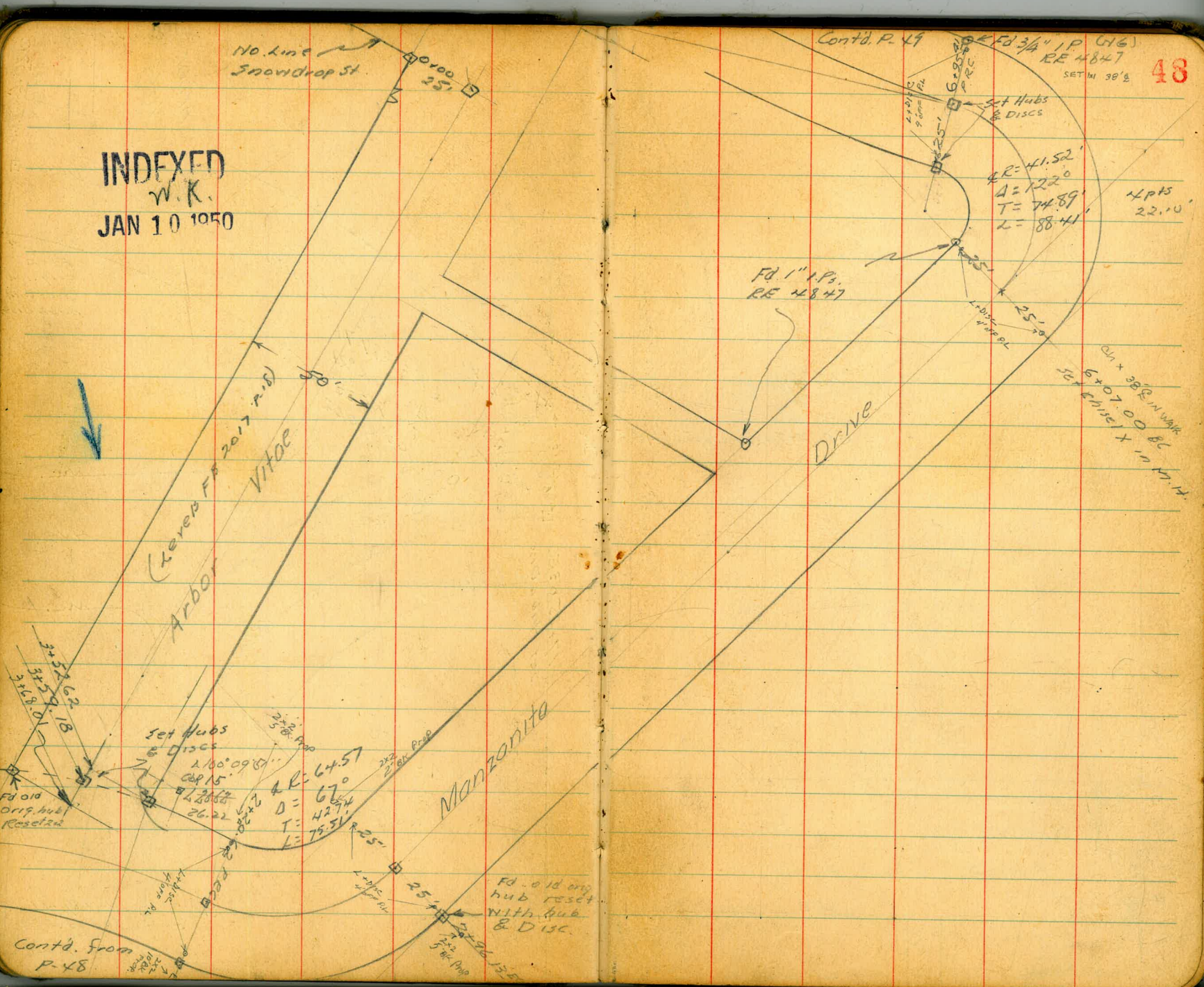
2 DISC 4' OFF P.L.

14289.41 EC
 Set Hubs & DISCS

Cont'd. from P. 46

INDEXED
W.K.
JAN 10 1950

No. Line
Snowdrop St.



Cont'd. P. 49
FD 3/4" I.P. (16)
RE 4847
SET IN 30' 8" **48**

Set Hubs
& DISCS
AR = 41.52'
A = 122°
T = 74.89'
L = 88.41'

HPIS
22.10

FD 1" I.P.
RE 4847

Drive

6" x 38" IN MARK
6 x 07.00 BC
SET HUBS x 10 IN MARK

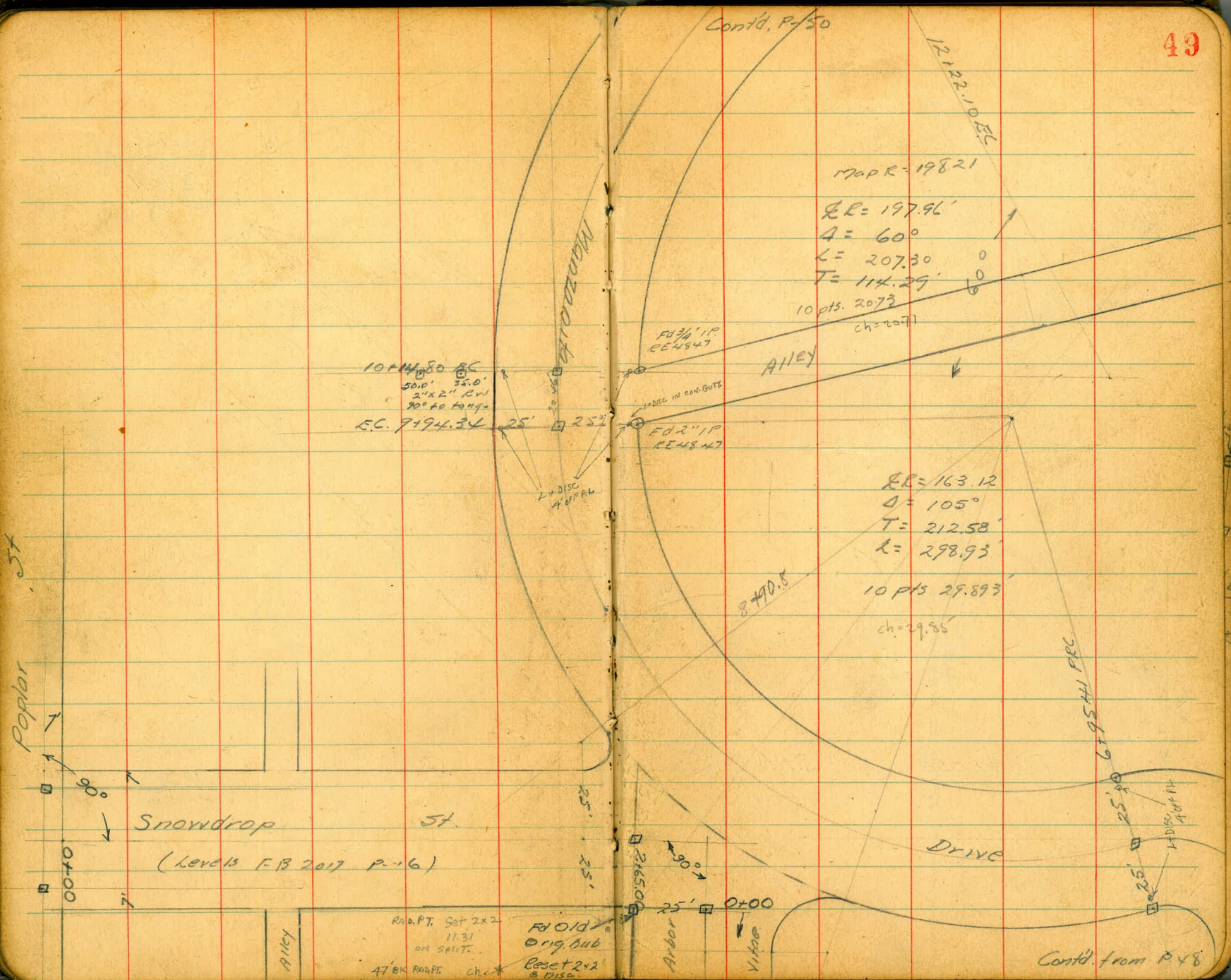
(Kerep Fb 2017 210)
Arbor
VITOE

MANZONITO

Set Hubs
& DISCS
110° 09' 15"
HPIS
26.22
AR = 64.57'
D = 67°
T = 42.94'
L = 75.31'

FD .010 and
hub reset
with hub
& DISC.

Cont'd. from
P. 48



MAP R-19821

RL = 197.96'

A = 60°

L = 207.30

T = 114.29'

10 pts. 2073
ch = 2071

RL = 163.12

A = 105°

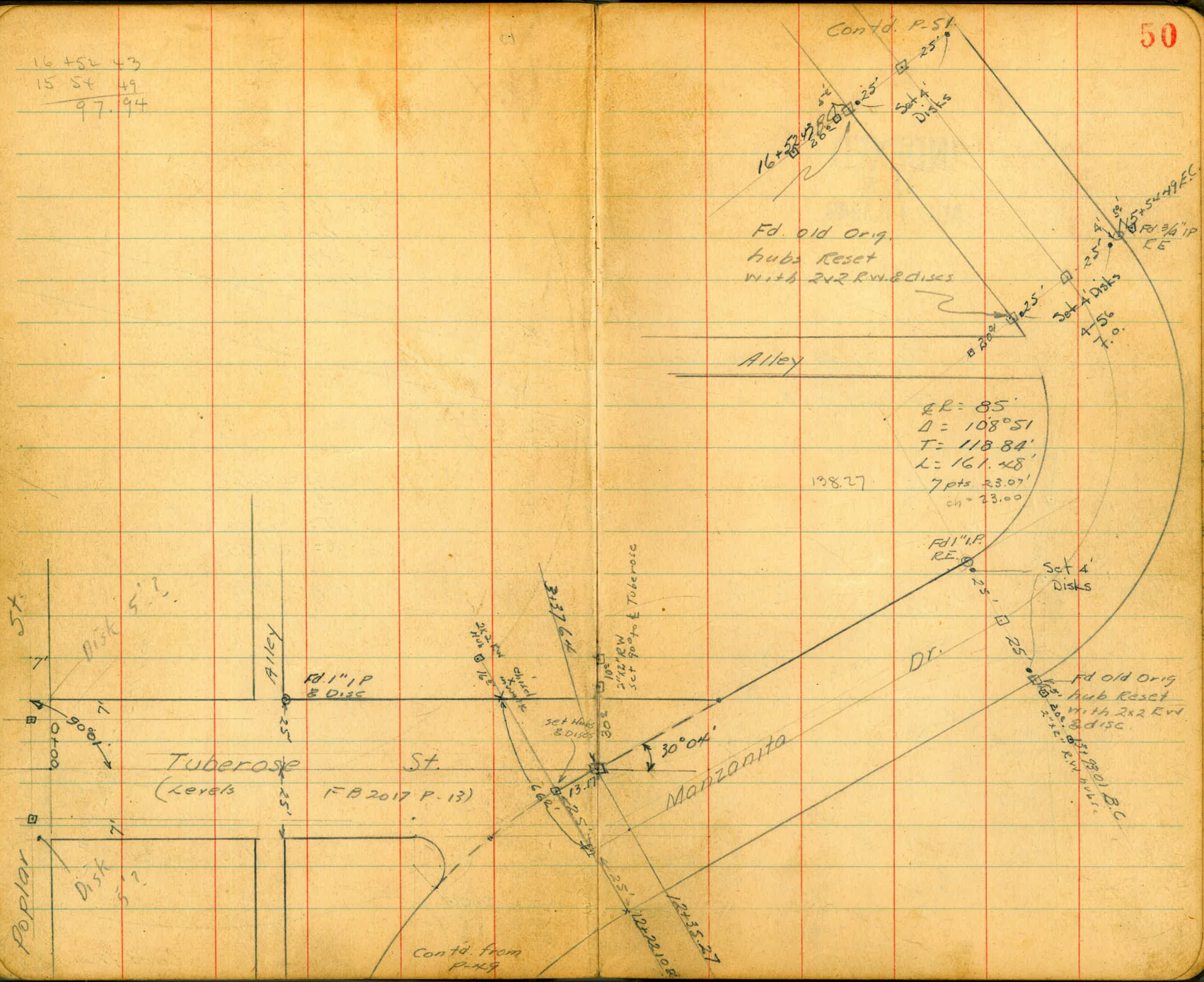
T = 212.58'

L = 298.93'

10 pts 29.893'
ch = 29.85

Cont'd. from P. 48

16 + 52 = 68
 15 54 49
 97.94



Fd. old Orig.
 hubs Reset
 with 2x2 RW & discs

Alley

QR = 85'
 D = 108°51'
 T = 118°84'
 L = 161.48'
 7 pts 23.07'
 ch = 23.00

138.27

Fd 1" IP
 RE

Set A
 Disks

Fd old Orig
 hub Reset
 with 2x2 RW
 & disc

5x
 Disk 5'?

900'
 900'

Poplar
 Disk 5'?

Alley

Fd 1" IP
 & Disc

Tuberose St.
 (Levels FB 2017 P. 13)

2" RW
 set 90° & Tuberose

337.64

Manzanita

30° 04'

Contd. from
 P-19

12035.27
 12022.10

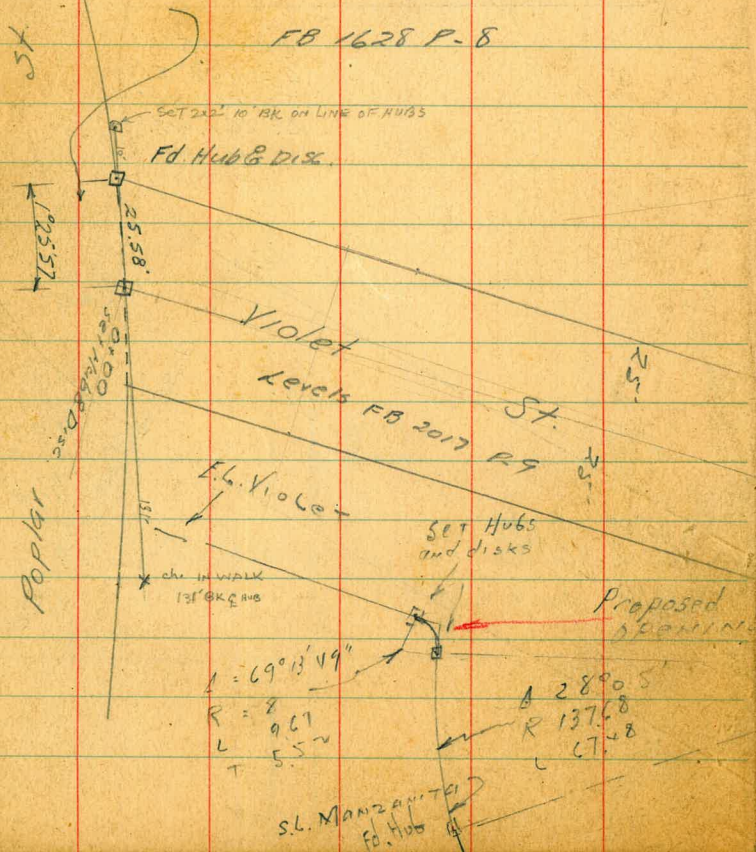
INDEXED

M.R.

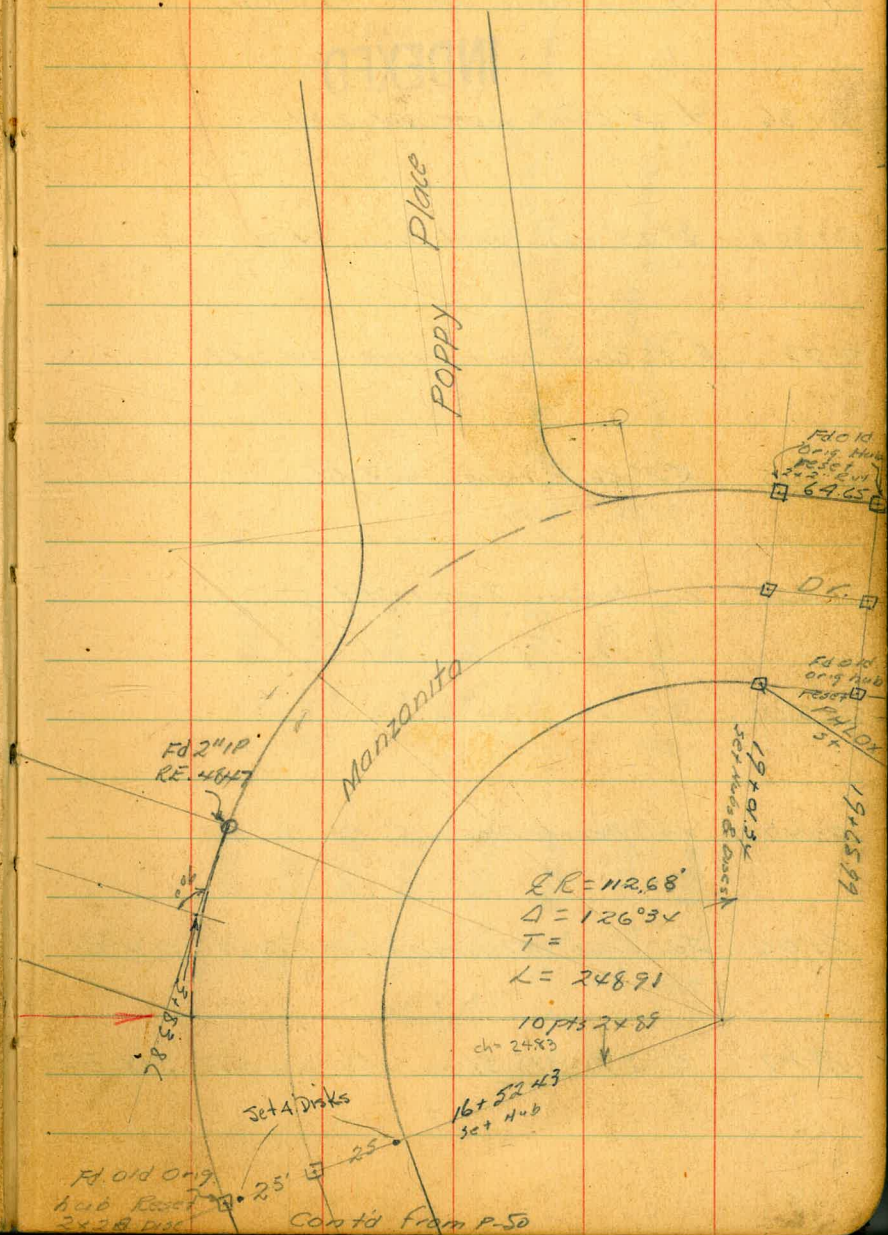
AUG. 19 1949

Note: This data taken from

FB 1628 P-8



51



Levels Manzanita Dr

Manzanita Pl. to Marlborough

Sketch P. 43-47

0+91 E 3.5 Conc Walk 25.6 Lt

INDEXED

0+86 E 3' Conc. Walk 24.2 Et

0+80.5 E 2.5' Conc split Drive 24.2

0+73 E 2.5 Conc split Drive 24.2 Et

0+68.5 E 2' Conc Walk 22.5 Et

0+65 12" Pepper Tree 17' Et

0+50

0+47 12" Pepper Tree 16' Et

0+00 So. line Manzanita Place (P. 43)

B.M. 0.29 318.31

318.02

311.21
7.10
35
310.83
7.40
25.6

310.40
7.21
24.2
310.46
7.85
24.2
310.76
7.55
24.2
310.85
7.16
22.5
310.40
7.21
24.2
310.23
7.35
310.18
7.13
310.18
7.35
310.19
7.80
310.87
7.44
22.5

311.9
6.4
35
312.0
6.13
25
311.5
6.10
11
311.8
6.10
13
311.3
7.0
25
311.1
7.0
25
310.9
7.4
40

313.9
4.4
33
313.8
4.1
25
313.8
4.5
20
313.2
5.1
18
313.6
4.7
8
313.5
4.8
25
313.0
5.13
40
312.4
5.9
40

318.31

SE. BP Thorn & Fairmount

1159 10" Acacia Tree 15.3 Rt

11525 8' Conc Drive 14' Rt.

1150

1145 8' 3' Conc Walk 21' Lt

1130 8' Conc Drive 16' Lt

1124 Power Pole # JP 4323 17' Lt

1118 6" Pepper Tree 24.7 Lt

1100

0192 10" Acacia Tree 17.2 Lt.

318.31

308.65

308.13

9' 16"
14

10' 18"
28

309.8

309.4

309.2

308.3

308.7

308.1

308.68

308.18

307.94

8.5
35

8.9
25

9.1
22

10.0
14

9.6
11

10.12
11

9.16"
14

10.12"
25

10.27
35

309.35
8.27
+10'
up Drive

310.06
8.25
+14'
up Drive

309.35
8.96
21

309.74
8.27
16'

311.0

310.7

310.4

309.7

310.3

309.5

310.2

310.1

310.0

7.3
35

7.6
25

7.9
16

8.6
11

8.0
13

8.8
15

8.1
25

8.2
35

8.2
35

318.31

xsect. Manzanita Dr. Cont'd

2150

2138 Power Pole # 4249 16.5 ft.

2131 R 8' Conc Drive 24.8 ft.

2116 R 3' Conc Walk 24.7 ft.

2100 Ho. Edge 2' Conc Walk 24.6 ft.

T.P. 1.55 $\frac{307.96}{\hline}$ 11.90 306.41 306.38

1180 10" Acacia Tree 15' ft.

$\frac{318.31}{\hline}$

306.1
305.7
305.5
305.0
305.0
305.5
305.1
304.4
305.0
304.8
304.8

19 21 25 30 30 25
24 25 14 12 7 25
2.9 3.6 3.0 2.5 2.5
6 11 13 25 25

305.72
22.4
24.8 30.8
36

306.19
18.2 21.3
24.7 35

307.5
307.3
307.1
306.5
307.1
306.79
306.19

0.5 0.7 0.9 1.5 0.9 1.7 1.7
25 6 10 14 24.6 35

$\frac{307.96}{\hline}$
(On SE RT Stub FB (624 P. 43)
(Glenfield & Manzanita Dr)

$\frac{318.31}{\hline}$

2+11 8' Conc Drive 25' Rt.

302.10
 302.12
 4.86
 25 36

3+00

304.1
 304.1
 303.6
 303.6
 303.8
 303.5
 303.0
 303.4
 303.1
 302.7

3.9
 3.9
 4.4
 4.4
 4.2
 4.5
 5.0
 4.6
 4.8
 5.2

35 25 13 6 6 6 11 14 25 25

2+96 3' Conc. Walk 25' Rt.

303.48
 303.09
 4.4
 25 25

2+70.5 8' Conc Drive 25' Rt.

304.28
 303.34
 36.8
 25 36

2+55 3' Conc. Walk 24.8 Rt.

304.91
 304.60
 30.5
 24.8 35

307.96

307.96
 1

4+14 Production of 3' Conc. Walk 25' Rt.

4+21.33

6.9	7.0	7.0	7.2	7.5	7.4	8.1	7.6	7.7	7.8
35	25	16	14	6	7	8	12	25	30
301.1	301.0	301.0	300.3	300.5	300.6	300.64	300.4	300.3	300.31

3+96.95

6.5	6.6	6.6	7.3	6.8	7.3	7.0	7.2	7.4
35	25	15	13	9	9	12	25	30
301.5	301.5	301.4	300.7	301.2	300.7	301.0	300.8	300.6

(Curve divided into 5 parts)

3+72.57 BC

5.8	5.9	6.2	6.7	6.8	6.8	6.8	6.5	6.4	6.4
35	25	14	12	6	3	9	12	25	30
302.2	302.1	301.8	301.3	301.8	301.8	301.2	301.5	301.5	301.5

3+55 Power Pole # P4281 16' Lt.

3+50

5.1	5.1	5.4	5.8	5.5	5.7	6.0	5.8	5.7	5.8
30	25	15	10	4	11	15	25	30	30
302.9	302.9	302.6	302.2	302.9	302.3	301.7	302.2	302.3	302.2

3+49 Anchor Pole 16.5 Rt.

3+42 & 4.5' Conc. Walk 25.2 Rt.

5.5	5.5
25.2	35
302.45	302.46

30796

30796

* Sect. Manzanita Dr. Cont'd.

5104 Power Pole #P4264 17.7 RT

4194.48 P.R.C. (Curve in 5 pts)

4180 & 3' Conc. Walk Produced 24.6 RT

4170.09

4149.90 & 8' Conc. Drive Produced (on Lt) ^{24'}

4145.71

4134 Prod. 8' Conc. Drive 25.8 RT

30796

	299.9	299.7	299.3	298.8	298.5	298.4	297.8	
	8 ^L	8 ^W	8 ^L	9 ^W	9 ^W	9 ^L	10 ^W	
35?	25	25	14		12	25	35	
					298.63		298.39	
					9 ^W	9 ^W		
					24.6	25		
	300.5	300.1	299.8	299.5	299.5	298.8	298.6	298.5
	7 ^L	7 ^L	8 ^W	8 ^W	8 ^W	9 ^W	9 ^L	9 ^L
	24	25	16	14	8	11	25	35
		300.79	300.50					
		7 ^L	7 ^L					
		24	24					
	300.7	300.4	299.8	300.0	299.2	299.4	298.9	298.6
	7 ^W	7 ^L	8 ^W	8 ^W	8 ^W	8 ^L	9 ^L	9 ^L
	24	25	15		10	11	25	35
					300.21		300.05	
					7 ^L	7 ^L		
					25.8	35		

30796

57

5+85 & Produced of a 3' Conc. Walk 14.2 RT

5+61 & Produced of a 6'5 Split Drive

5+51.97

5+22.92

5+10 & 8' Conc Drive Produced 27 RT.

T.P. 330 30203 9.23 298.73

30796

297.66
4.37
14.2
297.63
4.40
25.

297.84
4.9
13
No strip
297.76
4.27
25
(North?)

298.7
298.9
298.1
297.4
297.7
297.5
297.1
4.12
4.1
4.9
25
13
25
34

299.5
299.3
298.8
298.6
297.7
298.2
298.0
297.7
4.12
3.8
4.0
35
25
7
12
14
25
35

298.28
3.72
278
297.86
4.9
38

30203

On & Hub 4+94.48

30796

X Sect. 17000000000 Dr.

6+84 R 2' Conc. Wall 13.1 Rt.

6+70

6+42 Power Pole # P4254 16.6 Rt

6+3670 EC

6+0826

5+7981

302.03

4

295.27

295.04

59

676
13.1

699
25

296.8

296.6

296.3

295.7

296.0

296.0

294.9

295.4

295.1

294.9

5.0
35

5.4
25

5.7
15

6.0
12

6.0
4

6.0
11

7.0
14

6.0
25

6.0
25

7.0
30

297.8

297.7

297.3

296.6

296.9

295.7

296.7

296.2

295.6

4.0
30

4.0
25

4.7
17

5.4
12

5.1
12

6.0
16

5.0
25

5.0
25

6.0
35

298.6

297.9

297.7

297.3

297.5

296.6

296.9

296.6

296.1

3.0
35

4.1
25

4.3
17

4.7
13

4.5
12

5.4
15

5.1
15

5.4
25

5.0
25

298.6

298.3

297.9

298.1

297.9

297.2

297.5

297.6

297.2

3.4
35

3.7
25

4.1
19

3.9
9

4.1
11

4.8
14

4.5
25

4.4
25

4.0
35

302.03
1

8+18 & Produced of a 1.5' Conc. Walk 19.5 RT.

294.16
7.87
19.5
294.07
7.96
27

8+04.94

295.6
295.1
295.0
294.6
294.4
294.3
293.6
293.7
293.7

6.4
6.9
7.0
7.4
7.6
7.7
8.4
8.11
8.11

35
25
23
19
11
7
12
25
25

7+95 & Produced of a 10' Conc. Drive 25.7 RT

293.4
295.1
294.4
294.1
293.9
293.6
292.5
291.9

6.6
6.9
7.6
7.9
8.1
8.4
9.5
10.0

35
25
16
12
8
11
25
35

7+79.05

(Curve in 6pts)

295.4
295.3
294.9
294.2
294.1
293.8
293.5
292.6
291.8

6.6
6.7
7.1
7.8
7.9
8.2
8.5
9.4
10.11

35
25
15
10
7
10
18
25
30

7+53.17 BC.

296.6
296.4
295.8
295.0
295.2
294.5
294.9
294.6
294.5

5.4
5.6
6.2
7.0
6.8
7.5
7.6
7.4
7.5

35
25
16
11
10
9
13
25
30

7+00

302.03
↑

302.03
↑

x Sect Manzanita Dr. Cont'd.

9+28.02

(Curve in 3 pts)

9+0854 P.R.C. Gay Pole 18' Pt.

T.P. 2.61 297.59 708 294.98

8+82.59

8+56.71

8+30.82

302.03

295.0	295.0	294.9	294.1	294.6	294.0	293.3	292.9
25	25	27	25	20	26	25	27
35	25	16	13	10	10	25	35

295.4	295.4	295.4	294.5	295.1	294.6	294.2	294.4	294.3	293.8
22	22	22	31	25	20	34	20	25	20
35	25	17	11	9	13	18	25	35	

297.59
On a Hub 910854 P.R.C.

6 ¹⁰ 295.7	6 ¹⁰ 295.5	6 ¹⁰ 295.4	7 ¹ 294.9	6 ¹ 295.3	6 ¹⁰ 295.5	7 ¹⁰ 294.8	6 ¹⁰ 295.8	6 ⁸ 295.2	7 ⁰ 295.0
40	25	21	19	10	13	20	20	25	35

295.6	295.7	295.7	295.4	294.9	295.3	295.1	294.7
6 ⁴	6 ¹⁰	6 ¹⁰	6 ¹⁰	7 ¹	6 ¹⁰	6 ⁹	7 ¹⁰
45	25	20	13	17	25	35	

295.3	295.1	295.0	294.3	294.4	294.7	294.4	294.0
6 ²	6 ⁹	7 ⁰	7 ¹	7 ⁶	7 ³	7 ⁶	8 ⁰
35	25	18	13	17	25	35	

302.03

61

X Sect. Manzanita Dr. Cont'd.

11+00

56	61	65	74	73	78	86	94
35	25	15	10	13	12	25	25

293.2	293.0	292.6	291.5	292.0	291.4	291.7	290.5	289.5
4.4	4.6	5.0	6.1	5.6	6.2	5.9	7.1	8.1
25	25	14	10	11	11	16	25	35

10+50

10+48 Power Pole # P4275 21.8kt.

10+00

293.7	293.5	293.2	292.5	292.9	292.5	291.1	290.3
3.9	4.1	4.4	5.1	4.7	5.1	6.5	7.3
35	25	17	12	10	25	25	35

294.5	294.3	294.1	293.3	293.6	292.8	291.7	290.7
3.1	3.3	3.5	4.3	4.0	4.8	5.9	6.9
35	25	15	13	11	25	25	35

9+66.98 EC

294.6	294.6	294.4	293.7	294.1	293.4	292.4	291.6
3.0	3.0	3.3	3.9	3.5	4.3	5.2	6.0
35	25	16	14	9	25	25	35

9+47.50

297.59

297.59

X Sect. Manzanita Dr. Cont'd.

12+50 Anchor Pole 13' Rt # 4260

12+31.28

Curve in 5 pts.

T.P. 2.91 290.23 10.27 287.32

12+08.02 P.C.

11+91.53

11+75.04

Curve in 3 pts.

11+58.55 B.C.

297.59
A

289.4	289.2	289.0	287.3	286.7	285.8	286.0	285.6	284.7	282.7
0.8	1.0	1.3	2.9	3.5	4.4	4.3	4.5	5.5	7.5
35	25	20	16		9	11	19	25	35

290.23

on Hub 12+08.02 P.C.

289.8	289.5	289.3	287.4	287.4	287.0	287.4	286.2	284.7
7.5	8.1	8.3	10.2	10.2	10.6	10.2	11.4	12.9
35	25	16	11		9	16	25	35

290.1	289.6	289.4	287.5	287.8	287.7	287.8	287.1	285.9
7.5	8.0	8.2	10.1	9.8	9.9	9.8	10.5	11.7
35	25	16	12		9	15	25	35

290.3	289.7	289.4	287.7	288.1	288.0	287.4	286.3
7.3	7.9	8.2	9.9	9.5	9.6	10.2	11.4
35	25	16	12		12	25	35

290.6	290.0	289.3	288.0	288.5	288.3	287.0	287.0	286.6
7.0	7.5	8.3	9.5	9.1	9.3	10.6	10.6	11.0
35	25	15	11		10	20	25	35

297.59

X Sect Manzanita Or. Could

13+38

13+2435 EC

(ALLEY)

13+01.08

12+77.81

12+54.55

290.23

✓	8.0	10.1	10.4	10.2	12.2	17.2	21.2	23.4	25.1	251.4	250.1	279.5	280.0	278.0	273.0	269.0	267.1	265.1	64
	35	20	2		9	17	23	30	40										
18' X 1/2" / 75'	282.4	281.1	280.2	279.9	280.4	280.4	277.1	274.3	266.9	264.4									
✓	7.5	9.1	10.1	10.3	9.8	9.8	12.1	15.2	23.3	25.8									
	35	25	19	2		5	18	25	34	40									
	287.2	278.6	281.7	281.1	281.5	279.5	274.9	266.3											
	6.0	11.6	8.5	9.1	8.7	10.7	15.4	23.9											
	47	25	18	2		25	25	50											
	287.3	285.5	284.2		282.9	283.2	281.9	280.1	277.9										
	2.9	4.7	6.0		7.2	7.0	8.4	10.1	12.3										
	50	31	19			2	16	25	35										
	287.5	287.4	286.9	284.9	284.3	284.8	282.8	281.4											
	2.7	2.8	2.3	5.3	5.9	5.4	7.4	8.8											
	50	40	22		7	8	25	35											

290.23

X Section Manzanita Dr Contd.

14+23 R 8' Conc Drive 25.1 Rt.

14+05 R 3.5' Conc Walk 25.1 Rt.

14+00

13+84 Power Pole # 4226 23' Rt

13+60

13+52 R 20' Conc Drive 20' Lt

290.23

R

65

279.13
11.0
25.1

278.28
11.95
25.1

278.62
11.61
35

278.09
12.14
35

283.9	282.8	280.7	279.8	279.5	279.2	278.7	278.3	278.1
6 ^m	7.4	9.5	10.4	10.7	11.0	11.5	11.8	12.1
35	25	19	12		10	12	25	35

281.99	280.47	279.8	279.5	279.6	277.8	277.9	277.1	275.5
8.24	9.6	10.4	10.7	10.6	12.2	12.3	13.1	14.1
35	20	16		4	16	22	30	45

282.03	280.36
8.20	9.87
35	20

290.23

X Section Manzanita Dr. Cont'd.

15+00

T.P. 10.19 290.60 9.82 280.41

14+89.41 B.C.

14+64 & 3.5' Conc. Walk 25.2 ft.

14+50

14+46 & 8' Conc. Drive 25.1' ft.

290.23

285.9	285.4	285.5	281.4	280.3	280.8	280.8	280.0	279.8
4.1	5.2	5.4	9.2	10.2	9.8	9.8	10.6	10.8
35	25	22	7	2	5	5	25	35

286.1	285.5	285.4	280.8	280.3	280.5	279.8	279.6
4.1	4.7	4.8	9.4	9.9	9.7	10.4	10.6
35	25	22	7	2	25	35	35

279.80	279.42
10.43	10.81
25	35

285.7	284.9	284.8	281.0	280.0	280.0	280.3	279.9	279.4	279.1
4.1	5.2	5.4	9.2	10.2	10.2	9.9	10.2	10.8	11.1
35	25	22	4	6	5	5	17	25	35

279.34	279.10
10.89	11.2
25	35

290.23

X Sect. Manzanita Dr.

15+50 Dead Man to Pole 23' Rt.

15+35 Power Pole #4202 24.5 Rt.

15+25 & Produced of a 35' Conc Walk 126 Lt.

15+25

15+24 & Produced of a 8' Conc Drive 29' Rt.

15+03 & Produced of a 35' Conc Walk 256 Rt.

290.60

286.1	285.6	284.3	281.5	281.7	281.5	281.1	280.5	277.3
4 ⁵	5 ⁰	6 ¹³	9 ¹	8 ⁹	9 ¹	9 ⁵	10 ¹	13 ²
34	25	18	8		9	25	32	40

			282.53					
			8 ⁰					
			126					

286.0	285.0	284.0	282.0	281.1	281.3	281.0	280.5	280.3
4 ⁶	5 ⁶	6 ⁶	8 ⁶	9 ⁵	9 ³	9 ⁵	10 ¹	10 ³
35	25	21	12	2		13	25	35

						280.26		280.02
						10 ³⁴		10 ⁵¹
						29		39

						279.92		279.82
						10 ⁶⁸		10 ⁷⁸
						25.6		35

290.60

67

16+75

286.1
4¹¹
35

285.7
4⁹
25

285.5
5¹
20

284.9
5⁷
9

285.5
5¹
13

285.1
5⁵
18

285.9
4⁷
25

285.8
4⁸
50

286.4
4¹⁰
50

16+50

286.0
4⁰
40

285.1
5⁵
25

284.1
6⁵
16

284.6
6⁰
10

284.2
6⁴
1

284.5
6¹
6

283.9
6⁷
5

282.0
8⁶
13

283.1
7⁰
19

283.3
7¹⁰
25

284.7
5⁹
50

16+25

285.2
5⁴
40

284.8
5⁸
28

283.5
7¹
22

283.8
6⁸
14

283.1
7⁵
3

282.5
8¹
8

274.7
15⁹
15

273.8
16⁸
24

281.8
8⁸
40

283.0
7⁶
50

16+00

284.8
5⁸
40

283.9
6⁷
27

282.7
7⁹
21

283.0
7⁶
14

282.5
8¹
8

270.1
20⁵
23

269.5
21¹
22

273.1
17⁵
45

15+75

284.7
5⁹
35

283.9
6²
25

283.8
6⁸
23

282.4
8²
17

282.0
8⁶
8

281.2
9⁴
16

276.6
14⁰
25

265.4
25²
47

290.60

290.60

X Sect Manzanita Dr

18+00

TP 3.28 291.63 2.25 288.35

17+50

17+42 Power Pole # P-2924 16' Et.

17+32 & Sewer M.H

17+25.03 E.C.

17+00

290.60

287.0	287.0	286.9	286.9	287.0	288.0	287.9	288.1
4.5	4.6	4.7	4.7	4.6	3.6	3.7	3.5
35	25	13		10	12	25	35

291.63

Set Spk. in Power Pole # P-2924 16' Et. 17+42

287.1	287.0	286.9	286.7	286.9	287.0	287.9	287.8	287.9
2.5	3.6	3.7	3.9	3.7	3.6	2.7	2.8	2.7
22	25	14	9		12	13	25	25

286.71

3.89
Km

286.8	286.7	286.5	286.7	286.9	287.4	288.2
3.8	3.9	4.1	3.9	3.7	3.3	2.5
40	25	14		16	25	45

286.4	286.1	285.8	286.0	287.1
4.2	4.5	4.8	4.6	3.5
40	25	10		25

290.60

59

X Section Manzanita Dr.

4

70

B.M. 3.78 287.85 287.89

2.E Top E. Hyd. Poplar & Hollywood Park EB1628

18165 23 W. Line Poplar

286.5	286.7	286.8	286.3	286.6	286.9	288.0	287.5	287.5
5'	4.9'	4.1'	5.1'	5.0'	4.7'	3.6'	4.1'	4.1'
35	25	13	10		10	14	25	35

18164 Power Pole # 2902 17.2 RL

29163

29163

X Section Manzanita Dr.
 Marlborough to Violet
 (See P. 47 to 51 for sketch)

1+26.33

0194.89
 31.04

0163.45

0132.01

(Curve in 7 parts)

0100

B17 585 294.20

288.35

71

292.8	292.6	292.3	291.3	291.3	290.8	290.2	289.5
14	16	19	21	21	20	20	21
25	25	14	11	19	13	25	24
2916	2911	290.7	289.9	290.0	289.1	289.5	288.7
21	21	21	21	21	21	21	21
25	25	13	10	10	15	17	25
2903	289.9	289.3	288.6	288.8	288.0	288.6	288.2
21	21	21	21	21	21	21	21
25	25	10	9	5	8	20	25
289.4	288.8	288.3	287.6	287.6	287.5	286.7	287.1
8	5	5	6	6	6	7	7
35	25	7	1	1	11	25	26
288.3	287.9	287.3	287.1	287.1	286.4		
5	6	6	7	7	7		
25	7	6		13	25		
				294.20			

See in Pole # P2924 P. 69 this Book

X Sect. Manzanita Dr

2+92 Anchor Pole 18' Lt.

2+70.96

2+45.79

(Curve in parts)

2+20.62 PRC

1+89.21

TP 7.18 300.41 0.97 293.23

1+57.77
31.44

1+42.08 = opp E'ly corner Arbor Vitae
(End of Est. Grade, Profile sheet #2457
294.20

295.7	295.3	294.8	294.3	294.6	294.7	294.8	293.2	292.2
4.9	5.1	5.5	6.1	5.8	5.7	5.5	7.2	8.2
35	25	15	13	5	7	10	25	35

295.2	294.9	294.7	294.3	293.8	294.0	293.8	292.6	291.8
5.2	5.5	5.7	6.1	6.6	6.4	6.5	7.8	8.5
38	25	22	14	12	8	25	25	

295.1	295.0	294.6	294.0	293.4	293.5	293.1	292.5	291.9
5.3	5.4	5.8	6.4	7.0	6.9	7.2	7.9	8.5
35	25	19	13	9	13	25	35	

294.1	293.6	293.0	292.9	292.4	292.7	291.9	291.2
6.3	6.8	7.4	7.5	8.0	7.7	8.5	9.2
25	14	8		15	18	25	25

300.41
Hub 2+20.62 PRC

292.7	292.8	292.5	291.7	292.0	291.3	290.6
1.5	1.4	1.7	2.6	2.3	2.9	3.6
25	13	12	15	25	25	35

294.20

X Sect Marzanita Dr.

6+29.10 & 9' Conc. Drive 25.3 Rt.

Curve in 4 parts.

(Begin Profile #3269)

6+07.00 B.C. Jener MH.

6+05 Dead Man to Pole 17' Lt.

6+01 & 8' Conc. Drive 16.2 Rt.

5+86 Power Pole # P4161 17 Lt.

5+54 & 15.5' Conc. Drive 25.3 Rt.

5+30 & 3' Conc. Walk 17.3' Rt.

5+00 Power Pole # P4175 17' Lt.

4+58 & 2.6' Conc. Walk 19' Rt.

4+50

300.67

294.1	294.0	294.1	293.7	293.6	293.4	292.4	292.49	291.90
6 ⁶	6 ⁷	6 ⁸	7 ⁰	7 ¹	7 ²	8 ³	8 ⁴	8 ⁷
35	25	17	15		9	22	25	37

294.2	294.1	294.3	293.9	294.17	293.4	293.4	292.9
6 ⁵	6 ⁶	6 ⁴	6 ⁰⁸	6 ⁵⁰	7 ¹¹	7 ¹²	7 ⁸
35	25	16	12	Rim	294.19	25	25

294.2	293.4	293.4	292.9
6 ⁰⁴	7 ⁰⁰	7 ⁰⁰	7 ⁰⁰
16.2	30	293.67	292.9

295.8	295.7	296.3	295.7	295.9	295.3	295.46	295.10
4 ⁹	5 ⁰	4 ⁵⁰	4 ¹⁸	5 ⁴	5 ²¹	5 ²¹	5 ²⁷
35	25	12	11	19	25.3	40	

297.0	297.0	297.0	296.6	296.5	296.2	296.4	296.2	295.7
3 ¹	3 ⁷	3 ⁷	4 ¹	4 ¹⁰	4 ¹⁵	4 ¹⁵	4 ¹⁵	5 ¹⁰
35	25	11	9		13	16	25	35

298.2	298.0	297.7	297.3	297.0	296.5	296.3	296.0
2 ¹⁵	2 ⁷	3 ⁰	3 ⁴	3 ⁷	4 ²	4 ⁴	4 ⁷
35	25	11	9	27	13	25	35

300.67

X Sect Manzanita Dr.

7+55.19 & 7' Conc Drive on Lt

294.55	294.45	293.5	293.1	292.6	292.6
5.6 ^W	3.1 ^W	4.7	5.1	5.1 ^W	5.6
25	228	10	.	25	35

7+27 & Produced of a 3' Conc Walk 2244

294.3	293.9	293.8	293.5	293.2	292.6	292.5
3.7	4.1 ^W	4.4	4.7	5.0	5.1 ^W	5.1
35	25	21	7	25	27	

7+25.30

T.P. 487 298.18 7.36 293.31

293.9	293.8	293.6	293.4	298.18	292.8	292.5	292.3
6.8	6.9	7.1	7.3	7.6	7.9	8.2	8.4
35	25	14	12	15	25	35	

6+95.41 PRC.

6+79 Power Pole # P4148-17' Rt.

294.1	293.9	293.7	293.4	293.5	292.9	292.5	292.2
6.6	6.8	7.0	7.2	7.3	7.8	8.2	8.5
35	25	18	16	12	25	35	

6+73.30

6+64 Dead Man to Pole 18' Rt.

292.3	292.4	292.7	293.6	293.5	294.0	294.1	294.1
8.4	8.3	8.0	7.1	7.2	6.7	6.6	6.6
35	25	18	17	19	25	35	

6+51.20

300.67

300.67

X Sect. Manzanita Dr.

9+0466

8+79.76

8+4487

8+1498

7198 Power pole ? # 15' RL

7+85.08

298.18

292.1	291.8	291.6	291.1	291.2	291.1	290.6	291.0	290.6	290.2
61	64	66	71	70	71	76	72	76	80
35	25	16	14	6		7	9	25	35

292.3	291.5	291.7	291.4	291.7	291.8	291.6	290.9	290.7	290.5
59	67	65	68	65	64	66	73	75	72
33	25	11	2	1		11	18	25	35

293.0	292.7	292.4	292.2	291.4	291.1	290.6
52	55	58	60	68	71	75
46	25	15		6	25	35

293.2	292.9	292.9	292.5	292.3	291.3	291.2
50	53	53	57	59	65	70
35	25	20		10	25	35

294.2	293.9	293.2	292.9	292.4	291.8	291.6	291.2
40	43	50	53	58	64	66	70
30	25	14	13	15	21	25	35

298.18
7

X Sect. Manzanita Dr.

10+35.83 Conc Drive on Lt. Dead man to pole 185 Rt.

10+17 Power Pole # P. 4098 17.5 Rt.

(Curve in 10 feet.)

10+14.80 BC

TP 5.80 295.13
5.40 ~~294.73~~ 8.85 289.33

9+94.34 EC.

9+64.44.

9+34.55

298.18

289.80
289.50
289.0
289.2
288.5
288.9
288.3
287.7

5²⁴ 5¹³ 6¹ 5⁹ 6⁶ 6² 6¹⁸ 7⁴
35 229 10 12 14 25 35

Disc Drive

290.6
290.3
289.8
289.8
289.1
289.5
288.6
289.2
288.5
287.7

4²⁵ 4²⁸ 5¹³ 5¹¹ 6⁰ 5¹ 6⁵ 5⁹ 6¹⁶ 7⁴
35 25 24 12 10 12 14 25 35

295.13
~~294.73~~

Hub 10+14.80 BC

290.8
290.1
289.9
289.5
289.7
289.9
288.8
289.4
289.0
288.5

7⁴ 8¹ 8¹¹ 8¹ 8⁵ 8¹ 9¹ 8⁸ 9² 9¹
35 25 14 11 6 11 13 25 25

291.2
291.0
290.1
290.3
290.3
289.6
290.0
289.9
289.8

7² 7² 8¹ 7² 7² 8⁶ 8² 8¹¹ 8⁴
35 25 11 6 11 12 25 25

291.9
291.8
291.0
290.5
290.8
290.8
290.3
290.6
290.7
290.6

6¹¹ 6⁴ 7² 7² 7⁴ 7⁴ 7⁹ 7⁶ 7¹¹ 7¹¹
35 25 13 12 5 9 11 25 35

298.18
✓

77

X Sect. Manzanita Dr.

11+39.18 \$ 2.5 Conc. Walk 19.7 ft.

11+18.45

10+977.2

10+76.99

10+56.26

295.13
294.73

295.13
294.73

78

289.9	289.7	289.1	288.8	289.1	288.6	288.86	288.97
25	25	12	11	10	13	19.7	29
6.1	6.1	6.1	6.1	6.1	6.1	Walk	Walk
289.2	289.2	289.0	288.8	288.8	288.4	288.6	288.7
25	25	15	11	10	16	25	22
5.9	5.9	6.1	6.1	6.1	6.1	6.1	6.1
289.3	289.2	289.1	288.9	288.7	288.5	288.7	288.3
25	25	12	11	10	11	15	25
6.1	6.1	6.1	6.1	6.1	6.1	6.1	6.1
289.5	289.5	289.2	289.1	288.9	288.8	288.2	288.6
25	25	23	12	11	10	11	25
5.6	5.6	5.9	6.0	6.1	6.1	6.1	6.1
289.7	289.6	289.3	289.1	288.8	289.0	288.4	288.6
25	25	22	11	10	12	14	25
5.4	5.5	5.8	6.0	6.1	6.1	6.1	6.1
289.7	289.9	288.9	288.8	288.8	288.4	288.6	288.3
25	25	11	10	10	12	14	25
5.4	5.5	5.8	6.0	6.1	6.1	6.1	6.1

X Sect. Manzanita Dr

Cont'd. in FB 2017 P. 2

TP (K Hub 12+22.10) 3.52 ^{291.61} ~~291.21~~

12+22.10 EL 10" Tree 17' Rt.

12+21.50g Rock & Conc Wall 14' Rt.

12+01.37

11+80.64

11+77 8" Tree 17.5 Rt.

11+69 Power Pole # P4091 17' Lt.

11+62 Dead Man to Pole 17.5' Lt

11+59.91

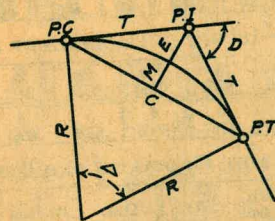
~~295.12~~
~~294.72~~

293.0	292.0	292.3	292.4	292.2	291.7	290.7	290.9	291.9	291.8	291.9
21	21	28	27	29	24	24	42	32	32	32
50	43	35	25	15		12	14	14	25	29
		292.1	291.9	291.3	291.0	291.9	291.79			
		30	32	30	41	32	32	25		16.82
		35	25	11		13	16	25	35	35
		291.1	291.1	290.8	289.9	290.1	289.2	289.4	289.3	289.1
		40	40	43	50	50	59	57	50	60
		35	25	13	10		13	15	25	35
		290.1	290.0	289.9	289.2	289.5	288.8	289.0	288.9	288.4
		50	51	52	59	56	63	61	62	61
		35	25	15	9		14	16	25	35

295.13
294.73

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External— $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ —Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction—.36 or $T = 414.85$ ft. P. C.—Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance—158—Sta. P. C.—54.50, hence offset— $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle— $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.—(in minutes) $.3 \times C \times D^\circ$ or—defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve— $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or— $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction—.10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

Manzanita Drive
 Notes reduced by
 Paul Tornheim
 May 10, 1949

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.	Angle	Sine.	Tan.	Cotg.	Cosin.		
0	0	0	∞	1	90	1	∞	0	0		
10	.0029	.0029	343.8	.9998	50	.7660	1.1918	.8391	.6428		
20	.0058	.0058	171.9	.9996	40	.6428	.7660	1.1918	.3572		
30	.0087	.0087	111.6	.9994	30	.5000	.5000	1.0000	.8660		
40	.0116	.0116	85.94	.9993	20	.3420	.3420	1.4618	.9397		
50	.0145	.0145	68.75	.9992	10	.1736	.1736	2.0904	.9848		
1	.0175	.0175	57.29	.9991	89	.9848	2.0904	.1736	.1736		
10	.0204	.0204	49.10	.9990	80	.9659	2.2522	.1564	.1564		
20	.0233	.0233	42.96	.9989	70	.9397	2.4618	.1311	.1311		
30	.0262	.0262	38.19	.9988	60	.8660	2.7500	.9397	.8660		
40	.0291	.0291	34.37	.9987	50	.7660	3.1072	.6428	.6428		
50	.0320	.0320	31.24	.9986	40	.6428	3.5264	.3572	.3572		
2	.0349	.0349	28.64	.9985	88	.3572	3.5264	.6428	.6428		
10	.0378	.0378	26.43	.9984	80	.3111	3.8568	.5000	.5000		
20	.0407	.0407	24.54	.9983	70	.2475	4.3314	.3420	.3420		
30	.0436	.0437	22.90	.9982	60	.1736	4.9616	.1736	.1736		
40	.0465	.0466	21.47	.9981	50	.1000	5.7682	.1000	.1000		
50	.0494	.0495	20.21	.9980	40	.0320	6.7552	.0320	.0320		
3	.0523	.0524	19.08	.9979	87	.0698	7.9674	.0698	.0698		
10	.0552	.0553	18.07	.9978	80	.0698	9.4138	.0698	.0698		
20	.0581	.0582	17.17	.9977	70	.0698	11.1061	.0698	.0698		
30	.0610	.0612	16.35	.9976	60	.0698	13.0903	.0698	.0698		
40	.0640	.0641	15.60	.9975	50	.0698	15.4090	.0698	.0698		
50	.0669	.0670	14.92	.9974	40	.0698	18.0000	.0698	.0698		
4	.0698	.0699	14.30	.9973	86	.1000	20.9057	.1000	.1000		
10	.0727	.0729	13.73	.9972	80	.1000	24.1421	.1000	.1000		
20	.0756	.0758	13.20	.9971	70	.1000	27.8390	.1000	.1000		
30	.0785	.0787	12.71	.9970	60	.1000	32.0000	.1000	.1000		
40	.0814	.0816	12.25	.9969	50	.1000	36.7554	.1000	.1000		
50	.0843	.0846	11.83	.9968	40	.1000	42.1569	.1000	.1000		
5	.0872	.0875	11.43	.9967	85	.1000	48.1569	.1000	.1000		
10	.0901	.0904	11.06	.9966	80	.1000	54.8344	.1000	.1000		
20	.0929	.0934	10.71	.9965	70	.1000	62.1569	.1000	.1000		
30	.0958	.0963	10.39	.9964	60	.1000	70.1569	.1000	.1000		
40	.0987	.0992	10.08	.9963	50	.1000	78.8344	.1000	.1000		
50	.1016	.1022	9.788	.9962	40	.1000	88.1569	.1000	.1000		
6	.1045	.1051	9.514	.9961	84	.1000	98.1569	.1000	.1000		
10	.1074	.1080	9.255	.9960	80	.1000	108.8344	.1000	.1000		
20	.1103	.1110	9.010	.9959	70	.1000	120.1569	.1000	.1000		
30	.1132	.1139	8.777	.9958	60	.1000	132.1569	.1000	.1000		
40	.1161	.1169	8.556	.9957	50	.1000	144.8344	.1000	.1000		
50	.1190	.1198	8.345	.9956	40	.1000	158.1569	.1000	.1000		
7	.1219	.1228	8.144	.9955	83	.1000	172.1569	.1000	.1000		
10	.1248	.1257	7.953	.9954	80	.1000	186.8344	.1000	.1000		
20	.1276	.1287	7.770	.9953	70	.1000	202.1569	.1000	.1000		
30	.1305	.1317	7.596	.9952	60	.1000	218.1569	.1000	.1000		
40	.1334	.1346	7.429	.9951	50	.1000	234.8344	.1000	.1000		
50	.1363	.1376	7.269	.9950	40	.1000	252.1569	.1000	.1000		
					82						
	Cosin.	Cotg.	Tan.	Sine.	Angle		Cosin.	Cotg.	Tan.	Sine.	Angle

TABLE VIII.—NATURAL TRIGONOMETRICAL FUNCTIONS.

Angle	Sine.	Tan.	Cotg.	Cosin.	Angle	Sine.	Tan.	Cotg.	Cosin.		
16	.2756	.2867	3.487	.96126	74	.4607	.4452	2.246	.91355		
10	.2784	.2899	3.450	.96046	50	.4094	.4487	2.229	.91236		
20	.2812	.2931	3.412	.95964	40	.4120	.4522	2.211	.91116		
30	.2840	.2962	3.376	.95882	30	.4147	.4557	2.194	.90996		
40	.2868	.2994	3.340	.95799	20	.4173	.4592	2.177	.90875		
50	.2896	.3026	3.305	.95715	10	.4200	.4628	2.161	.90753		
17	.2924	.3057	3.271	.95615	73	.4226	.4663	2.145	.90631		
10	.2952	.3089	3.237	.95545	50	.4253	.4699	2.128	.90507		
20	.2979	.3121	3.204	.95459	40	.4279	.4734	2.112	.90383		
30	.3007	.3153	3.172	.95372	30	.4305	.4770	2.097	.90259		
40	.3035	.3185	3.140	.95284	20	.4331	.4806	2.081	.90133		
50	.3062	.3217	3.108	.95195	10	.4358	.4841	2.066	.90007		
18	.3090	.3249	3.078	.95106	72	.4384	.4877	2.050	.89879		
10	.3118	.3281	3.048	.95015	50	.4410	.4913	2.035	.89752		
20	.3145	.3314	3.018	.94924	40	.4436	.4950	2.020	.89623		
30	.3173	.3346	2.989	.94832	30	.4462	.4986	2.006	.89493		
40	.3201	.3378	2.960	.94740	20	.4488	.5022	1.991	.89363		
50	.3228	.3411	2.932	.94646	10	.4514	.5059	1.977	.89232		
19	.3256	.3443	2.904	.94552	71	.4540	.5095	1.963	.89101		
10	.3283	.3476	2.877	.94457	50	.4566	.5132	1.949	.88968		
20	.3311	.3508	2.850	.94361	40	.4592	.5169	1.935	.88835		
30	.3338	.3541	2.824	.94264	30	.4617	.5206	1.921	.88701		
40	.3365	.3574	2.798	.94167	20	.4643	.5243	1.907	.88566		
50	.3393	.3607	2.773	.94068	10	.4669	.5280	1.894	.88431		
20	.3420	.3640	2.747	.93969	70	.4695	.5317	1.881	.88295		
10	.3448	.3673	2.723	.93869	50	.4720	.5354	1.868	.88158		
20	.3475	.3706	2.699	.93769	40	.4746	.5392	1.855	.88020		
30	.3502	.3739	2.675	.93667	30	.4772	.5430	1.842	.87882		
40	.3529	.3772	2.651	.93565	20	.4797	.5467	1.829	.87743		
50	.3557	.3805	2.628	.93462	10	.4823	.5505	1.816	.87603		
21	.3584	.3839	2.605	.93358	69	.4848	.5543	1.804	.87462		
10	.3611	.3872	2.583	.93253	50	.4874	.5581	1.792	.87321		
20	.3638	.3906	2.560	.93148	40	.4899	.5619	1.780	.87178		
30	.3665	.3939	2.539	.93042	30	.4924	.5658	1.767	.87036		
40	.3692	.3973	2.517	.92935	20	.4950	.5696	1.756	.86892		
50	.3719	.4006	2.496	.92827	10	.4975	.5735	1.744	.86748		
22	.3746	.4040	2.475	.92718	68	.4900	.5774	1.732	.86603		
10	.3773	.4074	2.455	.92609	50	.4925	.5812	1.720	.86457		
20	.3800	.4108	2.434	.92499	40	.4950	.5851	1.709	.86310		
30	.3827	.4142	2.414	.92388	30	.4975	.5890	1.698	.86163		
40	.3854	.4176	2.394	.92276	20	.4950	.5930	1.686	.86015		
50	.3881	.4210	2.375	.92164	10	.4925	.5969	1.675	.85866		
23	.3907	.4245	2.356	.92050	67	.4900	.6009	1.664	.85717		
10	.3934	.4279	2.337	.91936	50	.4925	.6048	1.653	.85567		
20	.3961	.4314	2.318	.91822	40	.4950	.6088	1.643	.85416		
30	.3987	.4348	2.300	.91706	30	.4975	.6128	1.632	.85264		
40	.4014	.4383	2.282	.91590	20	.4950	.6168	1.621	.85112		
50	.4041	.4417	2.264	.91472	10	.4925	.6208	1.611	.84959		
					66						
	Cosin.	Cotg.	Tan.	Sine.	Angle		Cosin.	Cotg.	Tan.	Sine.	Angle

13.69
4.00

11.7
2.0

8.62
1.01

117.52
97.83
9.69

117.52
13.67
103.85

15.7
6.0

NEBP 2350. Light Rainy

306.32
222.83

347.07

329.15

27.83

38-52-15

32.22x

77-57-30

38-55-45

38-56-1

51.10

39.
90.10

51.10

27.445

100.92

6.91

107.83

206

105.77

11.75

117.52

4.57

112.95

167.22.03

157.54.49

0.97.94

102.10.10

102.15

5500 8.00
5.00 1.5

102.10 + 51.10 = 102.80 x

15.53

22'0.02

31.44

57

01

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.

29977

6237
18
6249

11-56.64

34
20
65
62

64071
6009
18512