



EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/4 see inside of back cover.

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1857

INDEXED

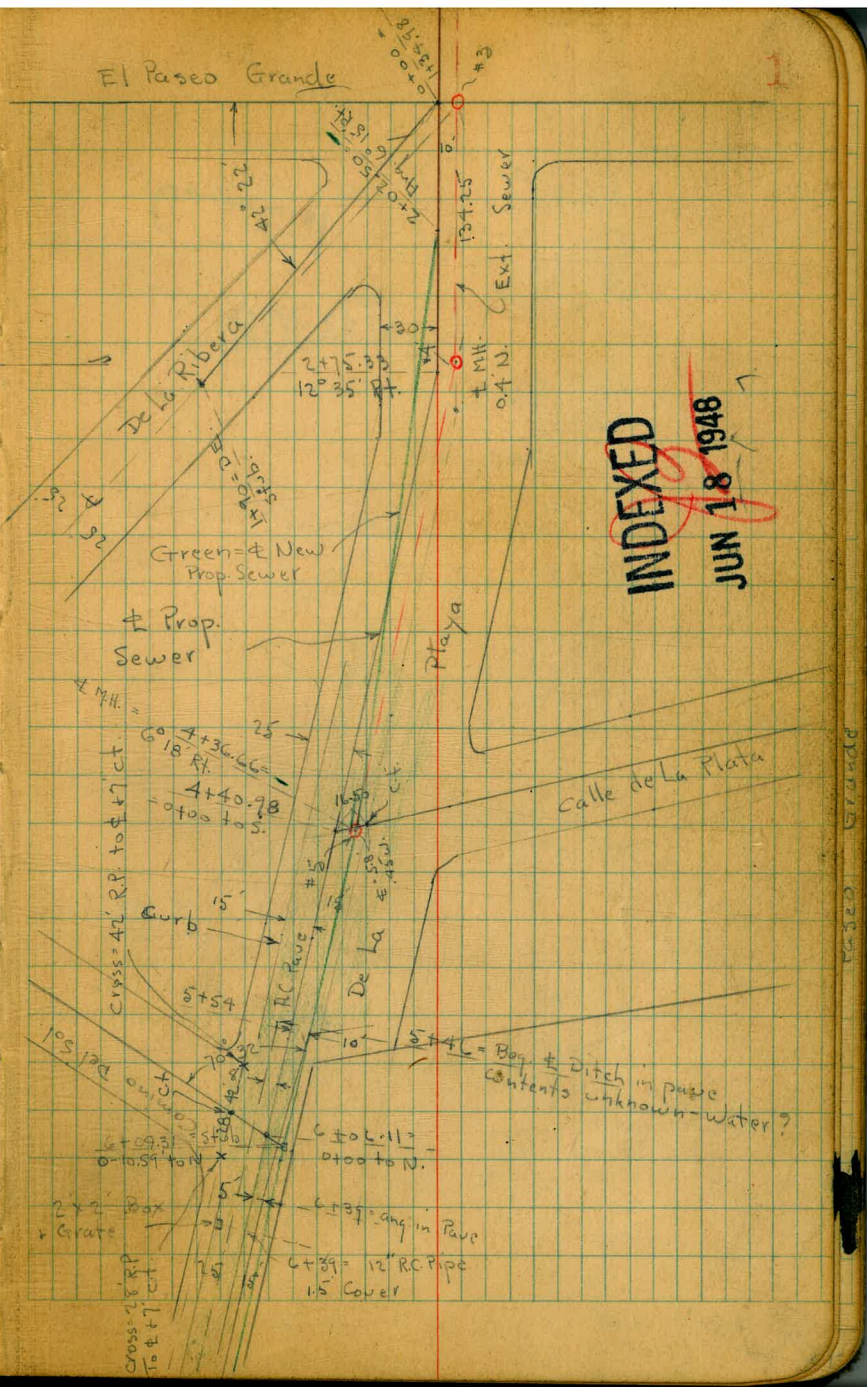
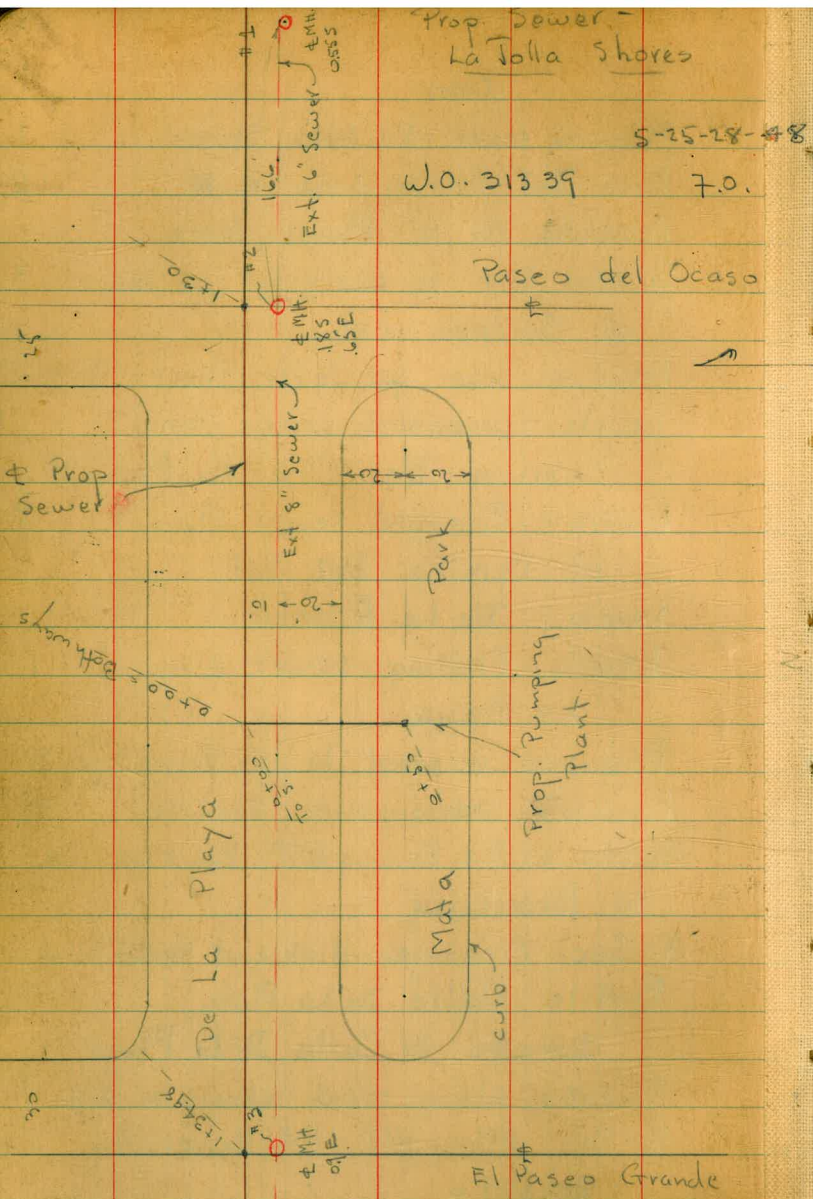
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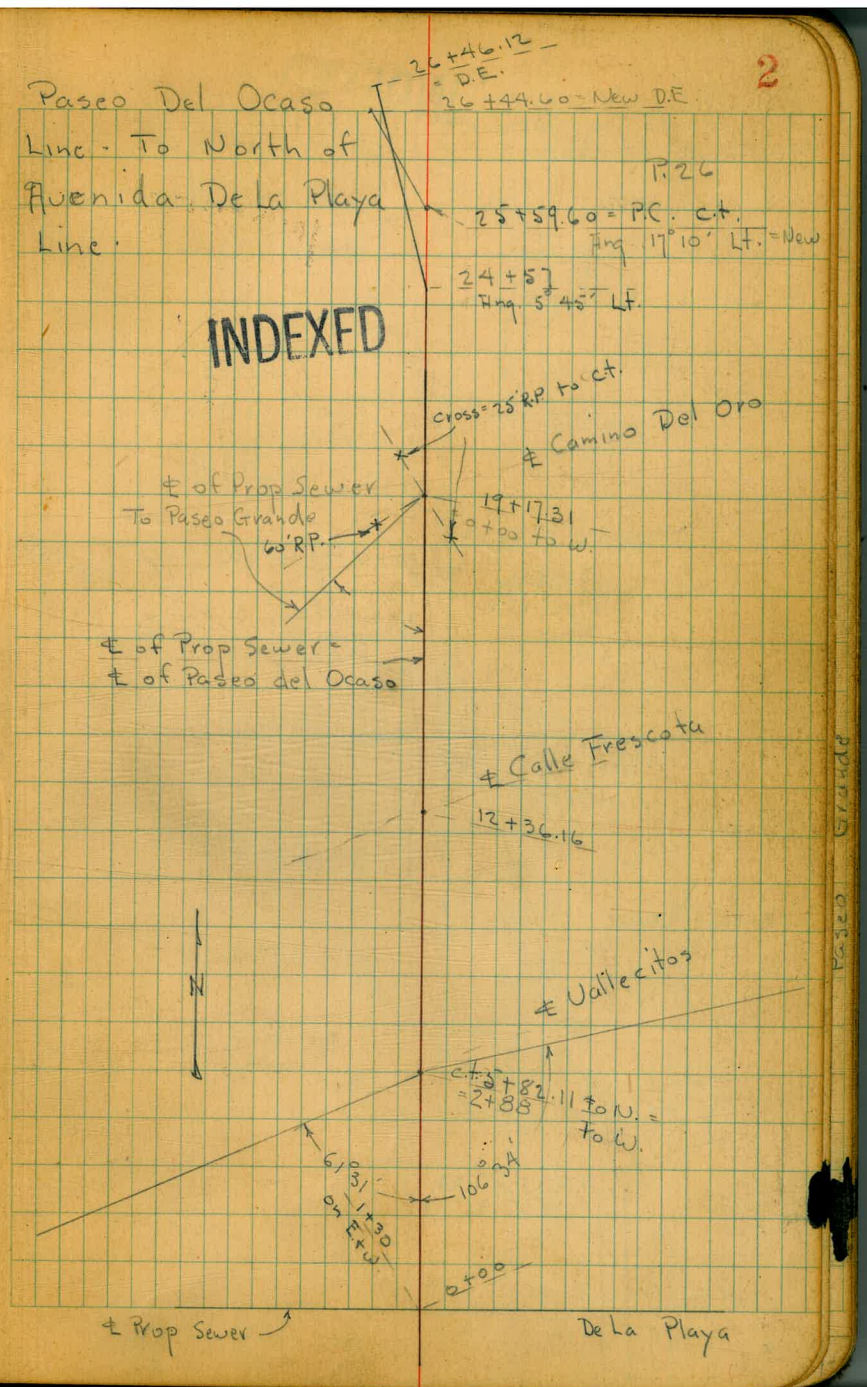
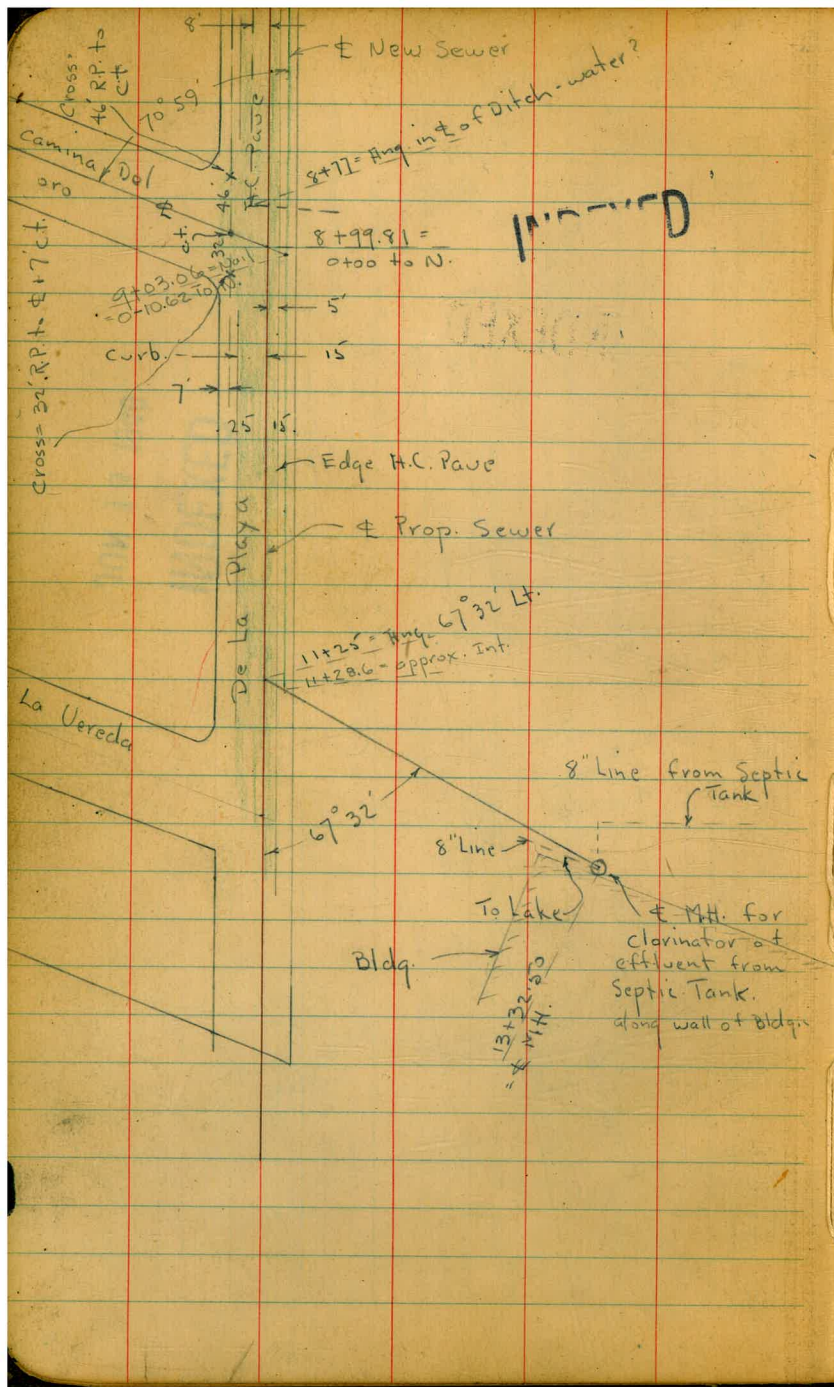
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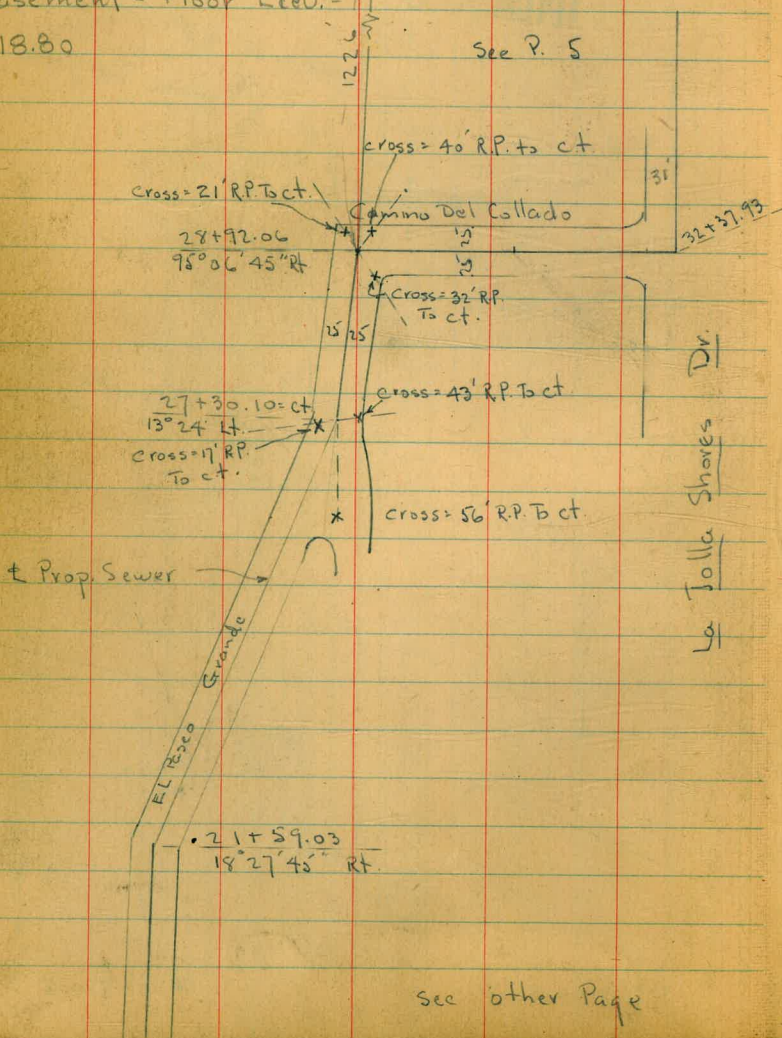


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Stadia Line to
Basement of Lab.
at Scripps inst.
1226' from 28+92.06
To Bottom of steps to
Basement - floor Elev. =
.18.80

U.S.C.+G Plug
in wall = El. 26.22

See P. 5

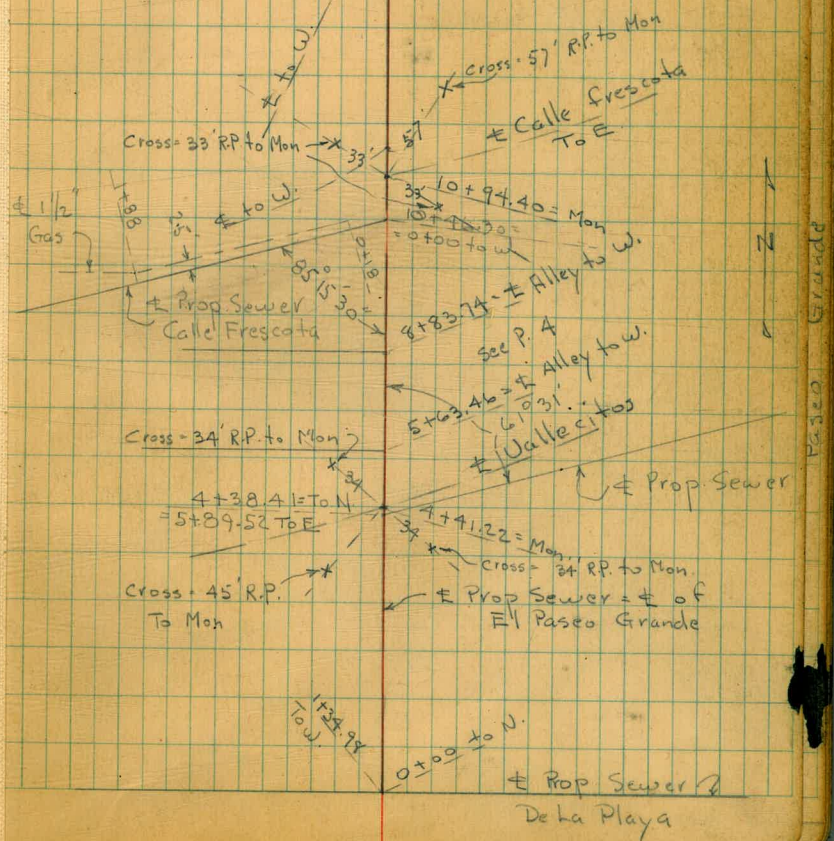


see other Page

Prop. Sewer in E
of El Paseo Grande
North of Avenida
De la Playa line

17+42
Line to Del Ocaso
= 3+17.75 To E.
Cross = 29' R.P. to Mon.
35' x 16' + 86.93 = Mon.
cross = 35' R.P. to Mon. at 90°

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Prop. Sewer
De la Playa

INDEXED



Camino Del Collado

Prop Sewer along La Jolla Shores Dr.

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27+35 = D.E. = stub.

Mon.

Camino Del Oro

31' 19+79.19

curb line

N

Mon.

Calle Frescota

31' 12+98.13

W.L. La Jolla Shores Dr.

20'

Mon.

Vallecitos

31' 6+64 = 0+00 to W.
6+44.00

Prop. Sewer

Prop. Sewer

30' 6" 26'

4' Water line

5'

0+00 = 4+56.30 on line to W.

De La Playa

ct.

31'

5

40+65 = D.E. = stub.

31'

39+01.37 = stub
Hng. 32° 37' Rt.

Camino De La Calina

1" Pipe

34+87.93

31'

Camino Del Collado

4" Water

32+37.93 Hng 90° Lt.

ct.

4" Gate

6" Water
6x8 Gate Box

4'

27+35 = D.E. = stub.

Levels along Prop. Sewer on
De La Playa - from 0+00 by Prop.
Pumping Plant at Mata Park - West
to Ocean.

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B.M.	3.57	7.02	3.51
T.P.	7.37	11.61	2.78
T.P.	1.36	9.93	3.04
€ Profile - on H.C. Pave			
0+00 = opp. € Mata Park	1.36	8.57	
9.7 Rt = gut	1.97	7.96	
" " = Top cb	1.37	8.56	
0+50	2.59	7.34	
1+00	3.58	6.35	
1+34.98 = € Paseo Grande 0+00 to N.	3.92	6.01	
1+70	4.19	5.74	
2+00	4.46	5.47	
2+33 = €	4.66	5.27	
9.6 Rt = closest to cb	5.38	3.55	gut
	4.79	5.14	Top
2+75.33 = Ang. 12° 35' Rt = nail			
€	4.95	4.98	
3+00	5.15	4.78	
+50	5.37	4.56	
4+00 = €	5.62	4.31	
15' Rt = cb	6.26	3.67	gut
	5.68	4.25	Top

B.P. in Sea wall
Av. De La Playa
c.t. € La Playa
+ De La Playa
= spike = 0+00
at Park

on spike
= €

99.3

6

4+40.98 = € Calle de la Plata = 0+00 to S.			- on Pave
€ = Nail	5.93	4.00	
5+00	6.29	3.64	
+50	6.49	3.44	
6+06.11 = € Camino Del Sol = 0+00 to N.			
€	6.95	2.98	
T.P. 3.22	<u>6.20</u>	6.95	2.98
6+50	3.40	2.8	
7+00	3.68	2.52	
+50	4.03	2.17	
8+00 = €	4.25	1.95	
15' Rt = cb	4.77	1.43	gut
	4.18	2.02	Top
5' Lt = edge H.C. Pave	4.22	1.98	
8+50	4.52	1.68	
8+99.81 = € Camino Del Oro = 0+00 to N.			
€ = Nail	4.80	1.40	
9+50	5.04	1.16	
10+00	5.30	.9	
10+50	5.56	.64	
11+00	5.80	.4	
15.2 Rt = cb	6.37	-.17	gut
	5.73	.47	Top
48' Lt = edge H.C. Pave	5.76	.44	
T.P.			
= B.M. 2.61	<u>6.12</u>	2.70	3.50 - 3.87

11+25 = Ang. $67^{\circ}32'$ Lt. = line to $\$$ M.H.
 for Chlorinator - Near Cor. of New Bldg.
 Entire Sewerage of All the buildings
 could be picked up here - or along line to E.

11+25 = $\$$	5.80	.32
AC. Pavc		
11+34.6 = $\$$ on edge of	5.81	.31
+50	5.2	.9
12+00	5.0	1.1
+50	4.9	1.2
13+00	4.6	1.5
+32.50 = $\$$ M.H.	4.1	2.0 - dirt
8" pipe from E.	8.13	-2.01 = Flow line
Top M.H.	3.84	2.28
= end		

Levels - Prop. Sewer along $\$$ Camina
 Del Oro - La Playa - North - P. 4

INDEXED

0+00 = 8+99.81 on La Playa Line
 Both ways
 Nail = $\$$ 6.32 7.72 1.40 - P. 6

0+16 = gutter.	6.71	1.01
0+24.3 = edge of Pavc	6.49	1.23
0+50 = on dirt	6.1	1.6
1+00 = $\$$	6.2	1.5
15' Lt. = gut.	6.8	.9
" = Top cb Typical	5.75	1.97
15' Rt. = gut. all way	6.6	1.1
" " = Top	5.79	1.93
1+50	6.0	1.7
2+00	5.7	2.0
+50	5.5	2.2
3+00	5.3	2.4
+50	5.2	2.5
4+00	4.9	2.8
0+00 = stub to w.		
4+11.62 = $\$$ Vallecitos	5.0	2.7
set B.M. on S.W. F.H.	2.61	5.11
4+50	4.8	2.9
5+00	4.8	2.9
+50	4.6	3.1

B.M. - P. 7 335
F.H.

8.46

5.11

8

7.72

5+66.62 = ± Alley on Rt. Prod. = 0+00 to E.

±		4.6	3.1
6+00		4.5	3.2
+50		4.7	3.0
7+00		4.4	2.9
+50		4.8	2.9
8+00		4.9	2.8
T.P.	4.88	7.64	4.96
			2.76
8+50		5.1	2.5
9+00		5.1	2.5
+50		5.1	2.5
10+00		5.0	2.6
10+31.43 = ± Calle Frescota		5.1	2.5
+50		5.2	2.4
11+00		5.3	2.3
+50		5.2	2.4
12+00 = D.E.	- ±	5.4	2.2
15' Lt. = gut.		6.0	1.6
	Top cb.	5.36	2.28
15' Rt. = gut.		6.0	1.6
	Top cb.	5.26	2.38
Paseo Grande + Frescota			
Set. B.M. - Top S.E. F.H.		0.19	7.45

Levels - Prop. Sewer along E of 20' Alley
in Block 34 - 0+00 = 5+66.62 - Del Oro line

0+00		5.3	3.2
+15 = gutter		5.4	3.1
+30 = E.L. Camino Del Oro		4.6	3.9
9.8' Lt. = gut.		5.1	3.4
" " = Top cb - end Ret.		4.91	3.55
9.8' Rt. = gut.		5.2	3.3
" " = Top cb		5.12	3.34
0+50		4.5	4.0
1+00		5.1	3.4
1+53.14 = Ang. 23° 39' Lt.		5.04	3.42
			on stub
2+00		4.8	3.7
+50		4.8	3.7
3+00		4.6	3.9
3+55 = D.E.		3.09	5.37
			on stub

8.46 - P. 8

Levels along Prop. stub sewer along
E of Vallejos to Comfort Sta. - P. 4

0+00 = 4+11.62 - on Camino Del Oro line

+50 5.9 2.6

1+00 6.0 2.5

+50 6.1 2.4

2+00 6.2 2.3

2+48.5 = E of E. side of 26' by 123 wide

Bldg - Comfort Sta. couldn't find pipes outside
of Bldg.

± along Bldg 6.0 2.5

Floor elev. 6.30 2.2

Levels along Prop. Sewer along E of
Camino Del Sol - 0+00 = 6+06.11 on La Playa ^{line}

BM = Nail 5.93

8.91

INDEXED 2.98

6+06.11 - P. 6

0+16 = gutter - Pavc 6.38 2.53

0+28 = edge of Pavc 5.86 3.05

+50 = dirt 5.8 3.1

1+00 5.7 3.2

+50 5.5 3.4

2+00 5.4 3.5

15' Lt - gut 6.1 2.8

Top cb 5.42 3.49

15' Rt - gut 5.9 3.0

Top cb 5.35 3.56

2+11 - 116 Lt = ^{lowest} Pipe on New Units 7.89 1.02 FL Pipe

2+50 5.3 3.6

2+00 5.2 3.7

3+28 = D.E. 5.1 3.8

Levels on Prop. Short stub in
De La Ribera from 0+00 = 1+34.98 on La
Playa Line = E. FL. Paseo Grande - See P. 1

INDEXED

0+00 = Nail	2.89	6.02	- P. 6
0+13 = gutter. - Pave	3.52	4.39	
+50	3.35	5.56	
1+00	3.98	4.93	
1+17.5 = end of Pave	4.17	4.74	
+50	4.2	4.7	
1+90 = D.E.	4.42	4.59	- on stub.

Levels on Prop. Sewer along E of
Paseo Grande N. of La Playa

10

0+00 = 1+34.98 on La Playa Line = 6.01 - P. 6

5.01 11.02

INDEXED

0+00 = on Pave	5.01	6.01
0+10 = gutter	5.55	5.47
+50	5.53	5.49
1+00	5.49	5.53
1+06 = end F.C. Pave Req. oil Pave - Fair Cond	5.50	5.52
1+50	5.4	5.6
2+00	5.2	5.8
+50	5.1	5.9
3+00 = E	5.1	5.9
15' Rt. = gut	5.3	5.7
" " Top cb	4.19	6.83
90' Rt = Vac. Lot.	3.5	7.5
15' Lt. = gut	5.8	5.2
" " Top cb	5.18	5.84
100' Lt. = low Vac. lot.	6.4	4.6
3+50	5.0	6.0
4+00	4.9	6.1
See 15-1 - P. 72 for loc. of Drain		
4+41.22 = E Vallecitos	5.0	6.0
5+00	4.6	6.4
+50	4.5	6.5

Paseo

11.02

6+00			4.4	6.6
+50			4.2	6.8
7+00			4.3	6.7
100' Lt = Vac. lot			6.0	5.0
100' Rt = Vac. lot			1.3	9.7
7+50			4.7	6.3
T.P.	2.30	<u>8.74</u>	4.58	6.44
8+00			2.8	5.9
+50			3.4	5.3
8+83.74 = 0+00 to W. = \pm 20' Alley.				
\pm			3.60	5.1
9+00			3.7	5.0
+50			4.1	4.6
10+00			4.4	4.3
+50			4.6	4.1
check Top F.H.			1.31	7.43
to E.				-P. 8
10+94.40 = \pm Calle Frescata			4.8	3.9
11+50			5.0	3.7
12+00			5.5	3.2
+50			5.8	2.9
13+00			6.0	2.7
100' Lt = Vac. Lot			6.2	2.5
13+50			6.2	2.5
14+00			6.3	2.4
T.P.	5.05	<u>7.47</u>	6.32	2.42

Grande

7.47

11

14+50			4.9	2.6
15+00			5.0	2.5
100' Rt. Vac. lot			2.2	5.3
15+50			5.3	2.2
16+00			5.6	1.9
+50			5.5	2.0
oro to W.				
16+86.93 = \pm Camino Del			5.4	2.1
17+00			5.4	2.1
+50			5.2	2.3
18+00			5.0	2.5
+50			5.0	2.5
19+00			4.7	2.8
+50			4.3	3.2
20+00			4.0	3.5
+50			3.2	4.3
21+00			2.3	5.2
T.P.	12.67	<u>17.84</u>	2.30	5.17
21+36.4 = end oil + Beg. AC. Pavel			11.63	6.21
21+59.03 = Ang. 18° 27' 45" Rt			10.84	7.00
21+70 - 43' Lt = \pm House			9.90	7.9
22+00 on pave			9.40	8.4
+50			7.69	10.15
23+00			5.89	11.95
15.4 Lt = gut			6.44	11.44
" " = Top cb.			6.02	11.82

on ct.
= floor.

23+00 - Cont.				
100' - Lt. - Vac lot.	8.7	9.1		
14.6' Rt. = gut.	6.05	11.79		
" " Top cb.	5.55	12.29		
50' Rt. - Vac lot.	4.0	13.8		
23+50	4.20	13.6		
24+00	2.44	15.40		
+50	0.72	17.12		
T.P. 12.87 <u>30.55</u>	0.16	17.68		
25+00	11.66	18.89		
+50	10.00	20.55		
26+00	8.26	22.29		
75' Lt. - Vac lot.	10.9	29.7		
50' Rt. - Vac lot	6.5	24.1		
26+50	6.49	24.06		
27+00	4.86	25.69		
Set B.M. - Top Hyd. Paseo Del Ocaso	3.30	27.25		
27+30.10 = Ang. 13° 24' Lt.	3.77	26.78	on ct	
+50	3.13	27.42		
28+00	2.19	28.36		
+50	1.12	29.43		
28+92.06 = Ang 95° 06' 45" Rt.	0.27	30.28	on ct.	
T.P. 12.59 <u>42.87</u>	0.27	30.29		
29+50	10.33	32.54		
30+00 - ±	8.24	34.63		
14.5' Lt. - gut.	8.66	34.21		
" " - Top	8.18	34.69		

30+00 - Cont.				42.87
75 Lt. - Vac lot.	8.8	34.1		
15.4 Rt. = gut.	8.69	34.18		
" " = Top cb.	8.19	34.68		
75 Rt. - Vac lot	9.1	33.8		
30+50	6.42	36.45		
31+00	4.40	38.5		
31+50	2.48	40.39		
32+00	0.71	42.16		
32+06.93 = W.L. La Jolla Shores Blvd. = ct.				
T.P. on ct 5.52 <u>47.86</u> 0.53.			42.34	
32+37 - 62 Rt. = N.W. Cor. 6x8' Water Gate Box.				
8.9 Rt. = ± 6" Water pipe - E+W.				
8.9 Rt. - Top 6" pipe	7.91	39.95		
Conc bottom of Box	11.09	36.77		
32+37.93 = Ang 90° Lt. = end				
± on nail	4.64	43.22		
Set B.M. on C+G Plug on s.w. Cor.	4.92	42.94		

↑
U.S.G.S.

INDEXED

6-7-48

Levels on Existing Sewer along
La Playa See Page - 1 for location
M.H. #1 = E. of Paseo Del Ocaso

9.09 17.66 8.57 - ⁰⁺⁰⁰ spike

Top Rim 2.95 14.71

Flow line - 6" Sewer 7.51 10.15

M.H. #2 = \pm Paseo Del Ocaso + La Playa

Top - ^{To E.} 6.06 11.6

F.L. - ^{8" To W.} 10.53 7.13

T.P. 1.16 9.73 9.09 8.57

M.H. #3 = \pm EL Paseo Grande

Top 3.39 16.34

F.L. - 8" 7.92 1.81

M.H. #4 = W. of Paseo Grande - 12425

4.62 15.11

9.85 8.48

M.H. #5 = \pm Calle De La Plata

Top 5.55 4.18

F.L. - 8" Line 10.11 - .38

Line Continues on to W. - loc. unknown

-70.

Levels on Prop. Sewer along \pm 13
of De La Playa - from 0+00 to E
0+00 = By Pump Sta.

10.50 19.07 8.57 = spike ₀₊₀₀

0+00 = spike - on Pavement _{A.C.} 10.50 8.57

+50 9.42 9.65

1+00 4.28 10.82

1+30 = 0+00 to N. 7.73 11.34

+50 7.47 11.60

2+00 6.54 12.53

+50 5.59 13.48

3+00 = \pm 4.57 14.5

9.7 ft. gut 5.15 13.92

" " Top cb 4.52 14.55

+50 3.32 15.75

+80 2.64 16.43

4+06.30 = 0+00 to N. line 21 E. of EL. ^{La Jolla Shores Blvd}

\pm = Nail 1.66 17.41

Levels on Prop. Sewer along \neq
of Paseo Del Ocaso - 0+00 - 1+30
on La Playa Line to E. - H.C. Pave allway

3.63 14.97 11.34 = Nail-1+30

0+00	on Pave	3.63	11.34	
+10	= gutter	4.18	10.79	
+50		3.74	11.19	
1+00		3.93	11.04	
+50		4.20	10.77	
2+00		4.48	10.49	
+50		4.62	10.35	
55.3'	Lt. - Low House	5.37	9.60	floor
3+00		4.85	10.12	
+50		5.10	9.87	
4+00	\neq	5.30	9.67	
15' Lt.	= gut.	6.10	8.87	
	Top cb.	5.41	9.56	
15' Rt.	= gut.	5.39	9.58	
	Top cb.	4.87	10.1	
4+15	- 49' Lt. \neq New House	5.16	9.81	floor
4+50		5.60	9.37	
75' Rt.	= Vac. Lot	4.3	10.7	
87' Lt.	= Plumbing outlet 4' Soil - New House	7.05	7.92	
5+00		5.86	9.11	
+50		6.07	8.9	
5+82.11	= \neq Vallecitos	5.93	9.04	c.t.

INDEXED

14

14.97

6+00		5.97	9.0	
+50		5.08	9.91	
7+00	8.91	19.57	4.31	10.64 = Nail
7+50		8.16	11.41	
44' Lt.	= House	6.99	12.58	floor
8+00		7.43	12.14	
+50	\neq	6.72	12.85	
100' Lt.	= Vac. Lot.	8.2	11.4	
9+00		6.06	13.51	
+50	\neq	5.40	14.17	
49' Lt.	= House	4.86	14.71	floor
10+00		4.90	14.67	
+50		4.63	14.94	
11+00	\neq	4.37	15.20	
100' Lt.	= Vac. Lot	6.4	13.2	
11+50		4.06	15.51	
12+00		4.12	15.45	
12+36.16	= \neq Calle Frescota	4.02	15.55	c.t.
12+50		4.07	15.50	
13+00		4.32	15.25	
+50		4.39	15.18	
14+00	3A2	18.31	4.68	14.89
4+10.46	Lt. House	3.20	15.11	floor
14+50	\neq	3.61	14.70	
100' Lt.	= Vac. Lot	8.1	10.21	

Everything on Rt. is High

18.31

15+00 - ±	3.75	14.56	5.98 = El. floor (Cont.)
71' Lt. = House	3.50	14.81	floor.
15+50	4.01	14.30	
16+00	4.25	14.06	
16+25 = 64' Lt. = House	8.5	9.81	10.00 ground floor
"	6.85	11.46	floor
16+50	4.41	13.90	
dk 17+00	4.54	13.73	
+50 - ±	4.82	13.49	
100' Lt. = Vac. Lot.	10.1	8.2	
18+00	5.05	13.26	
+50	5.30	13.01	
19+00	5.99	12.32	
19+17.31 = Del Oro Camino	5.62	12.69	ct.
T.P. 10.60 23.29	5.62	12.69	
19+32 = gutter	10.73	12.56	
+50	10.43	12.86	
100' Lt. = Vac. Lot.	15.1	8.2	
20+00	9.68	13.61	
+50	8.75	14.54	
21+00 - ±	7.94	15.35	
100' Lt. = Vac. Lot	11.7	11.6	
21+50	6.99	16.30	
22+00	5.94	17.35	
22+50 - ±	4.67	18.62	
100' Lt. = Vac. Lot.	7.9	15.4	

23+00 - ±	3.38	19.91	
15.4' Lt. - gut.	3.83	19.46	
" " Top cb	3.38	19.91	
54' Lt. = House	2.63	19.66	
14.6' Rt. - gut.	3.53	19.76	
" " Top cb	3.04	20.25	
23+50	2.15	21.14	
24+00	0.81	22.48	
T.P. 8.46 30.94	0.81	22.48 = Nail	
24+50	7.16	23.78	
75' Lt. = Vac. Lot	9.4	21.6	
24+57 = Ang. 5° 45' Lt.	6.97	23.97 on Nail	
check B.M. - F.H. - P. 12	3.69	27.25 - 27.25	
25+00	5.98	24.96	
25+50	5.17	25.77	
6.2' Lt. - gut.	5.35	25.59	
" " Top cb	4.92	26.02	
" " Top cb	4.91	26.03	
25+70 = closest to cb.	4.91	26.03	
4.8' Lt. - gut	5.09	25.85	
" " Top cb	4.67	26.27	
26+00 -	4.60	26.34	
26+46.12 = D.E. - on Pav	3.82	27.12	
5.0' Rt. = cb. - 90° to cb.			
" " gut.	3.61	27.33	
" " Top cb.	2.98	26.96	

Levels on La Jolla Shores Dr.

0+00 = 4+06.30 on La Playa Line			
0+00 - BM. 0.68	18.09	17.41	nail
0+45 = edge of AC Pavc	1.57	16.6	
1+00 = on Dirt	2.9	15.2	
1+50	3.6	14.5	
2+00 - ±	3.8	14.3	
100' Lt. = Vac. Lot	4.4	13.7	
2+50	4.1	14.0	
3+00	4.3	13.8	
11' Lt. =	gut.	4.9	13.2
" "	Top cb.	4.18	13.91
29.9' Rt. = edge 18' Conc. Pavc	3.07	14.92	
3+50	4.8	13.3	
3+65 - ±	5.0	13.1	
76' Lt. = House	3.10	14.99	floor
4+00	5.2	12.9	
+50	5.6	12.5	
5+00 - ±	6.0	12.1	
29.9' Rt. = edge Pavc	4.58	13.41	
48' Lt. = House	5.29	13.80	floor
5+50	6.3	11.8	
6+00	6.7	11.4	
6+44 = ± Vallecitos	6.7	11.4	
7+00 - ±	6.2	11.9	
29.9' Rt. = edge Pavc	5.05	13.04	

INDEXED

18.09

16

7+50	5.6	12.5	
75' Lt. = Vac. Lot	5.7	12.4	
8+00	5.1	13.0	
T.P. 13.01	25.93	5.17	12.92
8+50	12.6	13.3	
9+00	11.8	14.1	
29.8' Rt. = edge Pavc	11.23	14.70	
9+50	10.9	15.0	
10+00	9.8	16.1	
10+50	8.6	17.3	
55' Lt. = House	7.30	18.63	floor
11+00	7.1	18.8	
29.8' Rt. = edge Pavc	6.36	19.57	
11+50	5.9	20.0	
12+00	4.8	21.1	
62' Lt. = New House	6.65	19.28	F.L. outhet.
12+50	3.8	22.1	
12+98.13 = ± calle Frescota	3.0	22.9	
29.8' Rt. = edge Pavc	1.38	24.55	
13+50	2.4	23.5	
13+60 - 51' Lt. = House	1.85	24.08	floor
14+00	1.8	24.1	
11.2' Lt. =	gut.	2.4	23.5
" "	Top cb.	1.30	24.63
100' Lt. = Vac. Lot	2.4	23.5	

28.93

14+50		1.4	24.5
T.P.	7.91	<u>33.06</u>	0.78 25.15
15+00 - ±		8.0	25.1
29.8' Rt. = edge Pave		6.82	26.24
15+50		7.6	25.5
15+85 - 114' Lt. = New House		10.20	22.86
16+00		7.2	25.9
+50		6.8	26.3
17+00 - ±		6.3	26.8
29.8' Rt. = edge Pave		4.88	28.18
17+50		5.9	27.2
17+80 - 79' Lt. = New House		8.00	25.06
18+00		5.6	27.5
18+50		5.3	27.8
19+00 - ±		5.4	27.7
30' Rt. = edge Pave		3.70	29.36
11.4' Lt. = gut.		6.0	27.1
" " = Top cb.		5.02	28.04
75' Lt. = Vac. Lot		7.3	25.8
19+50		5.8	27.3
19+79.19 = ± Camino Del Oro		5.9	27.2
20+00		6.0	27.1
20+50		5.8	27.3
21+00		5.2	27.9
30' Rt. = edge Pave		3.94	29.12
100' Lt. = Vac. Lot.		10.6	22.5

on F.L.
outlet.F.L.
outlet.

17

33.06

21+50		4.7	28.4
22+00		4.1	29.0
62' Lt. = House		5.00	28.06 floor
22+50		3.3	29.8
T.P.	12.35	<u>42.03</u>	3.38 29.68
23+00		11.3	30.7
30' Rt. = edge Pave		9.95	31.08
75' Lt. = ± Prop. House		14.0	28.0 ground
23+50 - ±		10.1	31.9
72' Lt. = House		9.96	32.07 floor
24+00		8.5	33.5
100' Lt. = Vac Lot		12.0	30.0
24+50		6.7	35.3
25+00 - ±		4.9	37.1
30' Rt. = edge Pave		3.00	39.0
67' Lt. = House		6.40	35.6 floor
25+50		3.2	38.8
26+00		1.8	40.2
100' Lt. = Vac. Lot.		7.0	35.0
T.P.	6.45	<u>47.16</u>	1.32 40.71
26+50		5.8	41.4
27+00		5.1	42.1
30.2 Rt. = edge Pave		3.11	44.05
11.4 Lt. = gut.		5.9	41.3
" " = Top cb.		5.49	41.67
100' Lt. = Vac. Lot.		9.5	37.7

47.16

27+35 = D.E. 4.83 42.33 on Stub.
 check B.M. - C+G Plug 4.26 42.90 42.94-P.12

Levels on Prop. Sewer along \pm of N.
 20' Alley in Block 34 - 0+00 = 8+83.74 on
 Paseo Grande Line

B.M. = Top F.H. 2.72 10.17 7.45 Paseo Grande
 + Frescota

0+00 - on oil Pave	5.0	5.2	
0+15 = gutter edge of oil Pave	5.6	4.6	
0+30 = w.L. Paseo Grande	5.7	4.5	
0+40 = end of Returns - \pm	5.2	5.0	
10' Rt = end Ret - gut.	5.7	4.5	
" - Top cb.	5.30	4.87	
10' Lt = end Ret. - gut.	5.8	4.4	
" - Top cb.	5.00	5.2	
0+50	4.9	5.3	
1+00	6.0	4.2	
1+50	6.5	3.7	
2+00 = D.E.	7.08	3.09	on Stub.

Levels on Prop. Sewer + Pump site
 in Mata Park - see P. 1 - for sketch

0+00 - spike in La Playa
 4.48 13.05

INDEXED

8.57 = Spike
0+00

0+15 = on pave	4.24	8.81
0+30.2 = cb. around Park		
\pm - gut.	4.63	8.42
\pm - Top cb.	4.00	9.05
50' Lt. - along cb. - gut.	3.43	9.62
Top cb.	2.79	10.26
50' Rt. along cb. - gut.	5.93	7.12
Top cb.	5.17	7.88
0+50 = \pm Park = Dirt - \pm	3.7	9.4
50 Lt.	2.3	10.8
50 Rt.	4.9	8.2
0+51.6 - 4.5 Rt. = \pm 4" Flag Pole		
" - 30 Rt. = \pm 5' Palm		
0+52 - 20.5 Lt. = \pm 5' Palm		
0+70.1 = S. cb. around Park		
\pm gut.	4.06	8.99
Top cb.	3.45	9.60
50' Lt. along cb. - gut.	2.81	10.24
Top cb.	2.20	10.85
50' Rt. along cb. - gut.	5.22	7.73
Top cb.	4.52	8.53

18

Levels along Prop. Sewer along
± of Calle De La Plata - South of
De La Playa Line - 0+00 = 4+46.98 on
La Playa Line - Pave - all way.

B.M.	5.90	10.14	4.24	± ct. P. 6
0+00 = Nail		6.14	4.00	P. 6
0+10.7 = 0.45' Rt. = ± Sewer M.H. - See P. 13 + 1				
Top - Rim	5.93	4.21		
0+40 = gutter. (New)	6.45	3.69		
0+67 = 33' Rt. = Cor. House				
±	5.88	4.26		
33 Rt.	6.30	3.84		floor
"	6.2	3.9		ground.
1+00	5.77	4.37		
1+50	5.59	4.55		
2+00	5.20	4.94		
147 Rt. = gut.	5.67	4.47		
" " Top cb	5.16	4.98		
15 Lt. = gut.	5.65	4.49		
" " Top cb	5.02	5.12		
2+50	4.94	5.20		
75 Rt. = Golf Course	6.9	3.2		
75 Lt. = Vac. Lot.	3.7	6.4		
3+00	4.70	5.44		
3+50	4.45	5.69		
4+00	4.15	5.99		
3+40 - 51 Lt. = ± New House	2.29	7.85		floor

INDEXED

4+50		3.88	6.26	
4+65 - 40' Rt. = ± House		3.20	6.94	floor
5+00		3.68	6.46	
T.P. 10.78	17.24	3.68	6.46	5'00 - Nail
5+21 = gut.		11.03	6.21	
5+42.39 = ± Paseo Dorado		10.09	7.15	
5+63 = gut.		10.16	7.06	
6+00 = ±		9.23	8.01	
41' Rt. = New House		8.71	8.53	floor.
6+50		8.17	9.07	
54.5 Rt. = House		6.72	10.52	floor
7+00		7.28	9.96	
7+50		6.36	10.88	
75 Rt. = Vac. Lot		6.7	10.5	
8+00 - Nail - B.M.		5.48	11.76	
8+30.72 = ± Paseo Grande		4.85	12.39	
8+50		4.37	12.87	
9+00		2.48	14.76	
9+15 - 41' Rt. = House		0.17	17.07	floor
T.P. 13.04	29.93	0.35	16.89	
9+50		12.26	17.67	
10+00 = ±		8.53	21.40	
15' Rt. = gut.		9.17	20.76	
" " Top cb		8.59	21.34	
15 Lt. = gut.		8.98	20.95	
" " Top cb.		8.38	21.55	

29.93

10+50		4.35	25.58	
35' Lt = House		1.91	28.02	floor
		3.2	26.7	ground
11+00 = BM Nail		1.34	28.59	
11+08.29 = Paseo Del	Ocaso	0.91	29.02	
T.P.	12.90	42.50	0.33	29.60
11+50		10.61	31.89	
12+00 = ±		6.31	36.29	
75' Lt = Vac Lot		5.4	37.1	
12+50		1.76	40.74	
T.P.	12.91	54.21	1.20	41.30
13+00 = Nail = D.F.		7.40	46.81	

Lots Higher on Both Sides

BM on 13+45 - Stub.
La Jolla Shores -

5.21 49.00

21

Levels on Prop Sewer along E of
Paseo Grande - S. of Dela Playa

0+00 = 1+34.98 - on La Playa Line - ^{Pave all way}

BM = Nail 9.30 15.31 INDEXED 6.01 ^{11.34.98} P. 6

0+00		9.30	6.01
0+10 = 0.9 Lt = ± Mt	See P. 13+1	8.93	6.38 on Rim
0+33 = gut		9.42	5.89
0+50		9.18	6.13
1+00		8.52	6.81
75' Rt = Vac Lot		8.6	6.7
1+50		7.83	7.48
2+00		7.15	8.16
2+23.26 = ± Alley to Lt = 0+00 to E.			
± Nail		6.85	8.40
2+50		6.42	8.89
52' Rt = House		5.81	9.50 floor
3+00		5.59	9.72
15' Rt	gut	6.29	8.09
" "	Top - cb	5.65	9.66
75' Rt = Vac Lot		6.5	8.8
15' Lt	gut	5.89	9.42
" "	Top cb	5.31	10.00
every thing on Lt. is Higher.			
3+50		4.94	10.37
4+00		4.07	11.24
4+25 - 44' Rt = House		3.16	12.15 floor

15.31

4+50		3.42	11.89	
4+78 = gut.		3.56	11.75	
4+94.48 = Φ	Dorado Pasco	2.58	12.73	
T.P.	6.64	19.37	2.58	12.73
5+14 = gut.		7.00	12.37	
5+65 = Ang. - 22° 06' Rt.		5.90	13.47	Nail
6+00		5.74	13.63	
100' Rt. = House		6.15	13.22	floor
6+50 = Φ		5.41	13.96	
7.5' Rt. = Closest to cb.	gut.	5.75	13.62	
	Top cb.	5.23	14.14	
6+70 = 40' Rt. = House		4.91	14.46	floor
7+00		5.64	13.73	
12.7' Rt. =	gut.	6.38	12.99	
" " =	Top cb.	5.84	13.53	
7+22.40 = DE = Nail		5.91	13.46	
12.8' Lt. =	gut.	6.12	13.25	
" =	Top cb.	5.55	13.82	
check R.M. - 9+00 - Dela Plata		7.61	11.76	11.76 - P.20

Levels on Prop Sewer along Φ ²²
of 20' Alley - E. of 2+2326 on Pasco
Grande Line - at 00

	INDEXED	
2+2326 = Nail	9.09	17.55
0+00	9.09	8.46
0+15 = gut.	9.19	8.36
0+30 = E.L. = end of Pave	8.93	8.62
10' Rt. = end cb. Ret. =	8.43	9.12 gut
"	8.18	9.37 Top cb.
10' Lt. = end Ret.	8.80	8.75 gut.
	8.52	9.03 Top cb.
0+60 = Dirt	8.5	9.1
25' Rt. = Back of House	3.23	14.32 floor
1+00	5.6	12.0
1+30	4.8	12.8
26' Lt. = Φ House	3.71	13.84 floor
1+60	3.9	13.7
1+85 = DE. = stub.	3.27	14.28
50' Rt. = Vac Lot.	1.4	16.2
50' Lt. = " "	3.2	14.4

Levels on Prop. Sewer along E of Paseo Del Ocaso - S. of De la Playa
0+00 = 1+30 on La Playa Line - Paved
all the way

INDEXED

B.M.	10.03	<u>21.37</u>	11.34	= 1+30 Nail P. 13
0+00			10.03	11.34
0+10 =	- 0.6 Lt. = ± M.H.		9.82	11.55 on Rim
0+30 =	gut.		10.18	11.19
0+50			9.39	11.98
1+00			8.24	13.13
1+50			7.28	14.09
1+85 =	31' Rt. = House		5.59	15.78 floor
41' Lt. =	House		4.10	17.27 floor
2+00			6.21	15.16
2+50			5.19	16.18
3+00 = ±			4.06	17.31
15' Rt. =	- gut.		4.72	16.65
"	Top cb.		4.12	17.25
75' Rt. =	Vac. lot.		4.4	17.0
15' Lt. =	= gut.		4.28	17.09
"	Top cb.		3.61	17.76
75' Lt. =	Vac. lot.		1.8	19.6
3+50			2.96	18.41
4+00			1.80	19.57
75' Rt. =	Vac. lot.		3.0	18.4
4+50			0.72	20.65

21.37

4+76 =	gut.		0.78	20.59
T.P.	8.52	<u>29.47</u>	0.42	20.95
4+94.31 =	E Paseo Dorado		7.99	21.48
5+13 =	gut.		8.35	21.12
5+50 =	±		7.32	22.15
40' Rt. =	House		7.04	22.43 floor
every thing on left. is Higher				
6+04 =	Ang 20° 05' Rt. = ±		6.70	22.77
9.4' Lt. =	gut.		6.82	22.65
	Top cb.		6.26	23.21
6+50 =	±		6.20	23.27
12.6 Rt. =	gut.		6.77	22.70
"	Top cb.		6.30	23.17
7+00 =	±		5.87	23.60
8' Rt. =	gut.		6.36	23.11
	Top cb.		5.76	23.71
75' Rt. =	Vac lot		7.3	22.2
7+30 =	±		5.54	23.93
7.4' Rt. =	closest cb. - gut.		5.94	23.53
	Top		5.39	24.08
57' Rt. =	House		5.74	23.73 floor
7+50			5.28	24.19
7.9 Rt. =	cb.			
8+00 =	±		4.38	25.19
12.4' Rt. =	cb.			
42' Rt. =	House		3.05	26.42 floor

	29.47			
8+39.27 = Ang. 23° S 130° Rt.	3.86	25.61	±	
11.5' Lt. = gut	4.16	25.31		
	Top cb.	3.55	25.92	
8+50 - ±	3.74	25.73		
100' Rt. = Vac. lot	7.0	22.5		
9+00	3.50	25.97		
82 Rt. = cb.				
9+20 - 54' Rt. = House	4.66	24.81	floor	
T.P. 5.94	32.84	2.57	26.90	
9+50	6.49	26.35		
49 Rt. = cb.				
9+70 - ±	6.25	26.59		
46 Rt. = gut	6.53	26.31		
	Top cb.	5.90	26.94	
100' Rt. = Vac. lot	10.6	22.2		
10+00 - ±	5.85	26.99		
5.5 Rt. = cb.				
10+30 - ±	5.37	26.47		
82 Rt. = gut	5.73	27.11		
" = Top cb.	5.09	27.75		
42' Rt. = House	4.74	28.10	floor	
10+60 89 = D.E. = Nail	4.77	28.07		
12.3 Rt. = cb.				
check 11+00 Nail - P. 21	4.26	28.58	28.59	

24

Levels on Prop. Sewer along
W. side of La Jolla Shores Dr
S. of De La Playa 0+00 = 4+06.30 on
La Playa Line - unpaved.

B.M. 12.90	30.31	INDEXED	17.41	4+06.30 Nail-P13
0+00 = on pave	12.90		17.41	
0+50 " "	12.11		18.20	
0+65 = end of Pave	11.85		18.46	
1+00 - Dirt	11.3		19.0	
30' Lt. edge 18' Conc.	10.11		20.20	
1+50	10.1		20.2	
1+85 - 63' Rt. = House	10.46		19.85	floor
2+00	8.8		21.5	
2+50	7.4		22.9	
3+00	5.9		24.4	
30' Lt. = edge Pave	4.45		25.86	
11' Rt. = gut	6.5		23.8	
" " Top cb.	5.66		24.65	
55' Rt. = House	5.93		24.38	floor
3+50	4.5		25.8	
75 Rt. = Vac. Lot	5.5		24.8	
4+00				
35' Rt. = House	6.80		28.51	floor
4+41.6 = edge of Pave AC.	1.77		28.54	
4+94.40 = ± Paved	0.25		30.06	on Nail
T.P. 10.63	40.69		0.25	30.06

40.69

5+47.5 - edge H.C. Pave	9.40	31.29	
5+80 - \pm - Dirt	9.3	31.4	
75' Rt. = Vac. Lot	10.8	29.9	
6+00	9.0	31.7	
27.5 Lt. - edge Pave	7.03	33.66	
6+30 - \pm	8.4	32.3	
65' Rt. = House	9.01	31.68	floor
6+42 - Ang 17° 18' Rt.	8.04	32.65	on Stub.
6+70 - 11.7 Rt. = cb.			
7+00	7.2	33.5	
60' Rt. = House	8.19	32.50	
7+50	6.5	34.19	
8+00 - \pm	5.8	34.9	
30.3 Lt. = edge Pave	4.53	36.16	
11.3 Rt. = gut.	6.5	34.2	
Top cb.	5.60	35.09	
58' Rt. = House	6.64	34.05	
8+50	5.1	35.6	
8+90 - 11' Rt. = cb.			
9+00 - \pm	4.2	36.5	
100' Rt. = Vac. Lot	9.8	30.9	
24.5 Lt. = edge Pave	3.73	36.96	
9+04.68 = Ang 15° 50' Rt.	4.19	36.50	Stub.
9+50	3.5	37.2	
10.8 Rt. = cb.			

40.69

25

10+00	2.4	38.3	
75' Rt. = Vac. Lot	8.0	36.7	
10+50	1.3	39.4	
T.P. 11.68	<u>51.99</u>	0.38	40.31
11+00 - \pm	11.1	40.9	
35.3 Lt. = edge Pave	9.85	42.14	
11' Rt. = cb.			
11+33.18 = Ang 11° 17' Rt.	9.93	42.06	Stub.
11+60 - \pm	9.1	42.9	
11' Rt. = cb.			
75' Rt. = Vac. lot.	14.9	37.1	
12+00	8.1	43.9	
12+50	6.6	45.4	
12+55 - 16.3 Lt. = \pm 4x4	Gras. Co. M.H.		
Top Rim.	5.36	46.63	
13+00	5.1	46.9	
11' Rt. = cb.			
55' Rt. = House (front)	3.07	48.92	upper floor.
Basement floor			
85' Rt. = Plumbing	12.44	39.55	Base floor
13+55 = D.E.	3.00	48.99	49.00 Stub.
16 Lt. = edge Pave	2.33	49.66	
21.8 Rt. = cb. = gut.	3.8	48.2	
Top cb.	2.95	49.04	
75' Rt. = Vac. Lot	5.5	46.5	

Levels

9-23-48 - 7.0.

change in loc. of D.E. at N. End
of Paseo Del Ocaso - Sec P. 2

INDEXED

B.M. 4.25 31.50 27.25 Top. Hyd. P. 12

24+57 = old Ang. Pt. 7.53
 25+00 6.50
 25+59.60 = Ang 17° 10' Lt. 5.31 on ct.
 26+00 = S.I. Lt. = Gas - closest. 5.06
 10.1' Lt = gut. (nearest) 5.66
 " " Top. cb. 5.39
 26+44.60 = D.E.
 ± on Nail 4.66
 54 Rt. = ± water line (about 7' out from cb. Here)
 12.6 = ^{curb at} 90° to cb. gut. 4.16
 Top 3.53

Note: Gas line is about 5' out from cb.

9-23-48 - 7.0.

26

Levels along New Line along Camino
Del Oro - Bet. Paseo Del Ocaso + EL Paseo
Grande - Loc P. 2 + 3 - No Utilities

INDEXED

B.M. 0.19 12.88 12.69 - 19+17.31 ct. P. 15

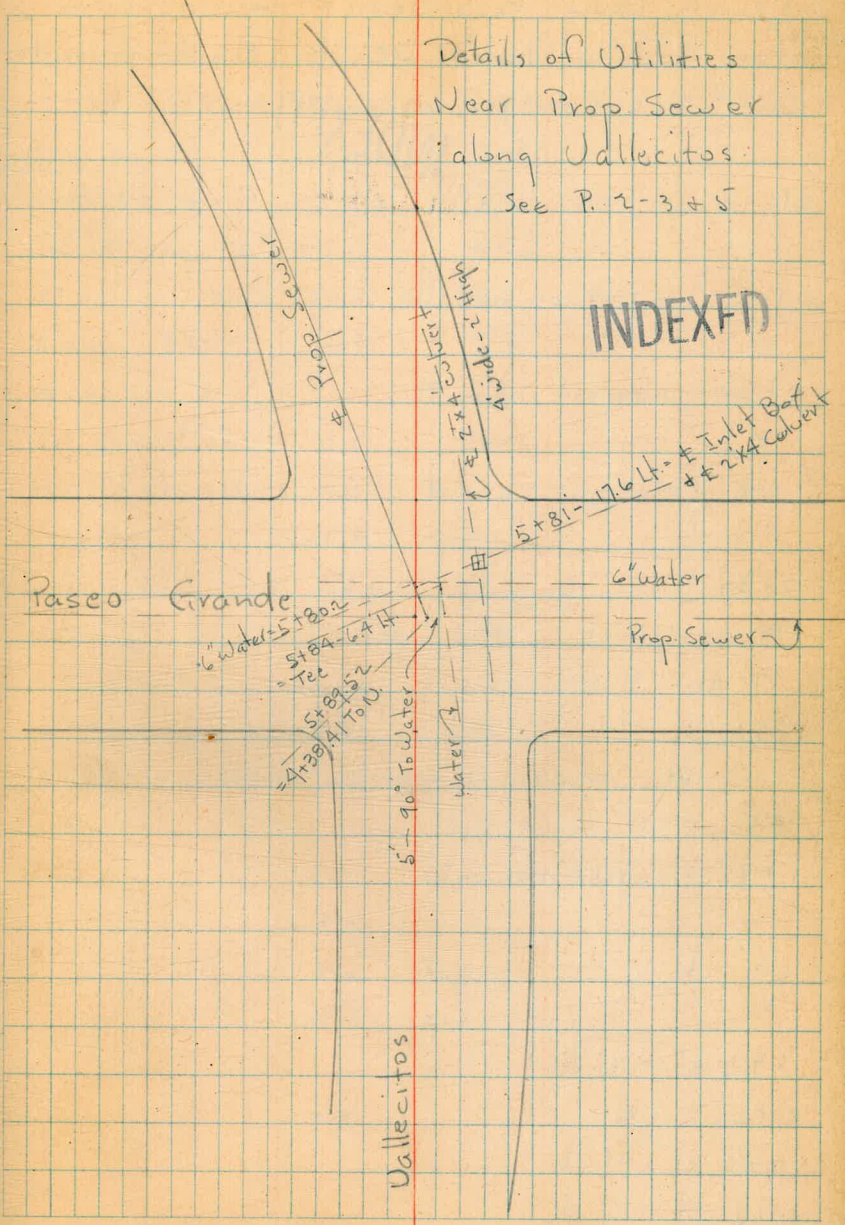
0+00 = ct. = ± Del Oro + 19+17.31 on Del Ocaso
 ± = on ct. 0.19
 0+30 = edge H.C. Pave 0.90
 0+60 = Dirt 2.7
 1+00 = ± 5.0
 10.7 Lt. = ^{on Lt} Nearest cb. - gut. 4.7
 Top 3.91
 1+50 7.8
 2+00 9.8
 2+18 = closest cb. on Rt.
 ± 9.9
 10.2 Rt. = gut. 10.0
 " " Top 9.70
 2+50 10.2
 3+04 = edge of oil pave 10.6
 3+17.75 = ± Paseo Grande 10.62 on Nail
 = 17+42

Levels along Prop. Sewer in Calle Frescota
 - Paseo Grande to Camino Del Oro. See P. 3 + 4

B.M. 0.00 7.45 INDEXED 7.45 Top Hyd. P. 8

- 0+00 = 10+46.30 on Paseo Grande
- ± Nail 3.29
- 0+33 = edge of oil pave 4.4
- 0+57 = closest to cb. on Lt. 4.6
- ± 4.6
- 4.1 Lt. = gut. 4.7
- " " Top cb. 3.99
- 1+10 4.6
- 1+60 = closest to cb. on Rt. 5.3
- ± 5.3
- 4.7 Rt. = gut. 5.4
- " " Top 4.82
- 2+10 5.2
- 2+55 = closest to cb. on Lt. 5.3
- ± 5.3
- 4.1 Lt. = gut. 5.4
- " " Top 4.67
- 2+95.25 = 9+98.80 on Camino Del Oro 4.8
- ± 4.8

Note: New 1/2" Gas line 2.5' N. of ± sewer from
 0+18 to 1+88 - then angles north - See plan
 Best location could work out with Foreman



Levels along Prop. Sewer in Vallejos
 from LaJolla Shores Dr. to Paseo Grande
 See P. 2-3-5+27

INDEXED

BM. 7.06 16.10 9.04

c.t. = Vallejos
 + Paseo Del
 Ocaso
 P. 14

0+00 = 6+64 on LaJolla shores line

± 4.6 11.5

0+34 = Nearest cb. on Rt.

± 5.2

6.4' Rt. = gut 5.4

" " = Top 4.46

0+85 = ± 5.5

14' Lt. = S. cb.

17' Rt. = N. cb.

1+20 = ± 5.9

21.7' Rt. = N. cb.

8.8' Lt. = S. cb.

1+75 = closest cb. on Lt.

± 6.3

5.6' Lt. = gut 6.4

" " = Top 5.75

24.3' Rt. = N. cb.

2+25 = ± 6.6

23.5' Rt. = N. cb.

7.7' Lt. = S. cb.

16.10

2+62 = edge A.C. pave 6.81

2+88 = 5+82.11 on Paseo Del Ocaso - Ang. Pt.

± = on ct 7.06

T.P. 3.76 12.80 7.06 9.04

3+16 = edge F.C. Pave 4.26

3+60 4.6

4+00 5.3

4+40 = ± 5.8

5.4' Rt. = N. cb.

4+75 = Nearest cb. on Rt.

± 6.0

5' Rt. = gut 6.2

" " = Top 5.14

5+20 6.2

5+48 = edge oil pave 6.2

5+89.52 = 4+38.41 on Paseo Grande

± 6.7

Levels along Prop Sewer in Camino Del Sol + De La Ribera - cont. sta. from 3+28 = D.E. on Camino Del Sol - See P. 4

B.M.	6.01	8.99	INDEVENT	2.98	6+06.11 La Playa - P. 6
3+28 = old DE - See P. 9 for					
±				5.2	
3+53.50 = Ang. Pt. -					
±				5.1	
3+62.1 = cross 4" Water					
4+00				5.2	
+50				5.1	
5+00					
±				5.0	
15.1 Lt. =				5.5	
" " =				5.01	3.98
14.9' Rt. =				5.5	
" " =				4.90	
5+23.50 = D.E.				4.9	

Levels along New Prop Sewer in De La Playa - from 2+02.50 on old line to Int. with stub line to Beach club. - P 1+2

B.M.	4.63	9.61	INDEVENT	4.98
2+02.50 = Ang. 6° 15' Rt.				
±				4.16
2+55 - Nearest cb. on Rt.				
±				4.76
5' Rt. =				5.16
" " =				4.58
3+00				4.96
+50				5.04
4+00				5.23
4+26 = Cross water line				
4+36.66 = ± Exist. M.H. = Ang. 6° 18' Rt.				
± on Rim				5.41
4+47 - Cross 2" Gas				
4+33 - 18.5' Rt. = Ang. in water line				
4+52.1 10' Rt. = " " Gas "				
4+60				5.58
5+00 ±				5.79
10.1 Rt. = Gas				
18.4 Rt. = Water				
5+50				6.14
5+52 = edge H.C. pave = S. edge also				6.16

9.61

6+00		6.7	
6+07 -	9.2 Rt. = Ang to N. of Gas Line		
6+09.31 =	0-10.59 to N. = on E Camino Del Sol.		
± on stub.		6.80	
	3.88 <u>6.69</u>	6.80	2.81
6+50	-	4.1	
7+00 -	±	4.3	
	3.9 Rt. = edge Pavc	4.18	
7+50		4.5	
8+00		4.8	
	18' Rt = Water		
8+50		5.0	
8+74 =	cross water to club.		
8+77 =	edge H.C. Dr.	5.15	
9+03.06 =	0-10.62 to N. = E Camino Del Oro		
± on Nail		5.26	
9+15 =	edge Dr.	5.39	
9+50		5.6	
	4.6 Rt. = edge Pavc	5.53	
10+00		5.5	
+50		6.0	
T.P.		5.29	1.40 = P.6 0+00 Del Oro

30

Levels Thru Test Holes - 3" Dia. - for location of Culverts + Water table.

on Paseo Del Ocaso - See P. 15

20+70 = ± Culvert.

16' Lt. = Top pipe

34' Lt. = end pipe

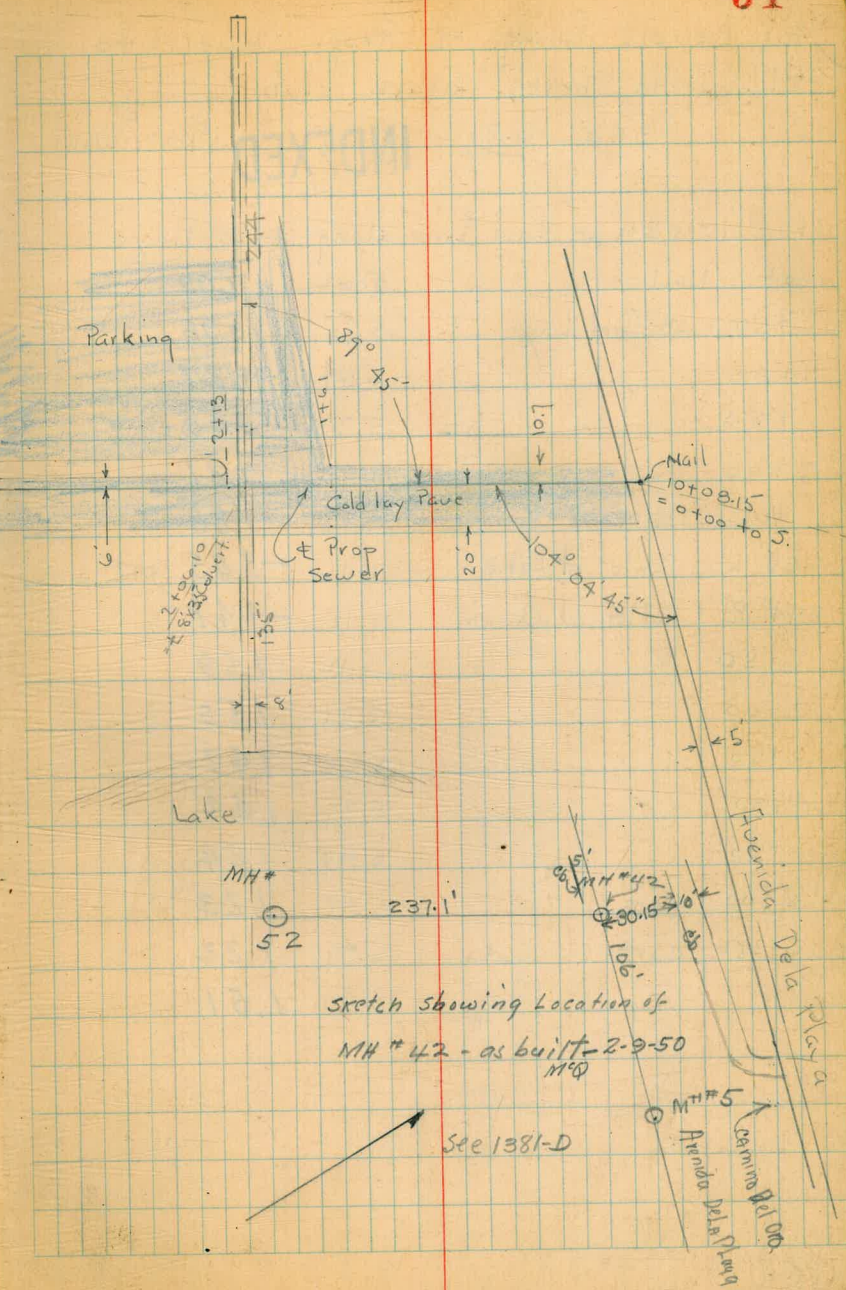
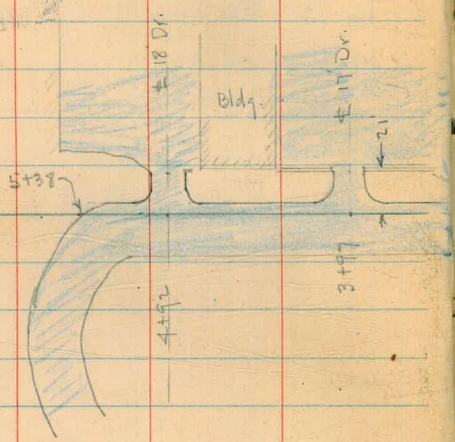
INDEXED

Loc Prop. Sewer to LaJolla Shores
Beach Club - 10-22-48

7.0

W.O. 21339

INDEXED



Levels along ϕ Prop. Sewer to
La Jolla Shores Beach club.

3.20 6.71

INDEXED

8P. in Sea
Wall

0+00 = 10+08.15 on Last Line along De la Playa

0+00 = Nail	5.62	1.09	
+50 = on Cold lay	5.75	0.96	
1+00	5.44	1.27	
+50	5.31	1.40	
2+00	4.90	1.81	
+06.10 = ϕ 8x3.8 Culvert. Conc. Box	4.83	1.88	
135' Lt. = Inlet at Lake	10.16	-3.45	= F.L. of Box
244' Rt. = Outlet at Ocean	11.12	-4.41	= " " "
2+50 = ϵ	5.12	1.59	
3+00	5.21	1.50	
+50	5.24	1.47	
4+00	5.27	1.44	
+50	5.47	1.24	
5+00	5.48	1.23	
5+38 = curb. = gut.	5.49	1.22	
Top	5.20	1.51	

Vista Del Mar

1+91.34 = E.L.
Cross

M.H.

8" Sewer Ave

Prop. Pressure
Sewer

20'

St.

Gravilla

0+68.29 = Cross
Ang. 22° 30' Lt.

0+55 = Cross
Ang. 22° 30' Rt.

13'

0+30.18 = E.L.

Conc. Pavc

Neptune

0+00 = Cross in cb. Place



Electric Ave.

33

INDEXED

12+12.07 Cross
Ang. 44° 44' Rt.

12+18.77 = Cross-Fd.
21" Sewer
1646 - P. 27

20'

30'

Conc. Pavc

St.

9+92.77 = E.L. - Cross

La Jolla

9+89.71 = Nail
Ang. 11° 36' 30" Rt.

Blud.

8+90.88 = W.L.
= Cross

20' 30'

Gravilla

Levels along \pm of Prop. Pressure
Sewer in Gravilla - from Tank at
Neptune to Trunk Sewer at Electric

3333

W.O. 60207

INDEXED
WK
MAR 18 1949

3-17-49

Osborne
Hardin
Hatch
Shepard

B.M. 10.40 30.36

19.96

0+36.06
1646-P.28

Loc	10.24	20.12	Top
0+00 = ^{Face} Cross on cb.	11.18	19.18	Gut
0+15 = Conc. Pavc	10.55	19.81	
0+30	10.10	20.26	
0+50 = Ang. 22° 30' Rt.	9.39	20.97	on Cross.
0+68.29 = Ang. 22° 30' Lt.	8.24	22.12	" "
1+00	6.74	23.62	
1+50	4.44	25.92	
1+61.5 = Cross 6" Sewer	3.75	26.61	\pm
5' Rt. = \pm Sewer M.H.	9.42	20.94	F.L. M.H.
2+00	1.37	28.99	

T.P. 12.97 42.73 0.60 29.76

2+50 9.04 33.69

42.73

3+00	3.94	38.79
T.P. 13.09	<u>55.56</u>	0.24 42.47
3+50	11.60	43.96
4+00	6.56	49.00
4+15 = Bk	5.24	50.32
4+50	3.75	51.81
5+00	1.50	54.06

T.P. 13.10 68.09 0.57 54.99

5+50	11.84	56.25
6+00	9.59	58.50
6+50	7.56	60.53
7+00	5.82	62.27
7+50	4.12	63.97
8+00	2.44	65.65
8+50	0.79	67.30

T.P. 10.60 78.16 0.53 67.56

8+93 = Beg. H.C. Pavc Bk = end Conc. \pm	9.29	68.87
9+14 = Gut.	9.72	68.44
9+42 = \pm	8.43	69.73

x

78.16

71.79

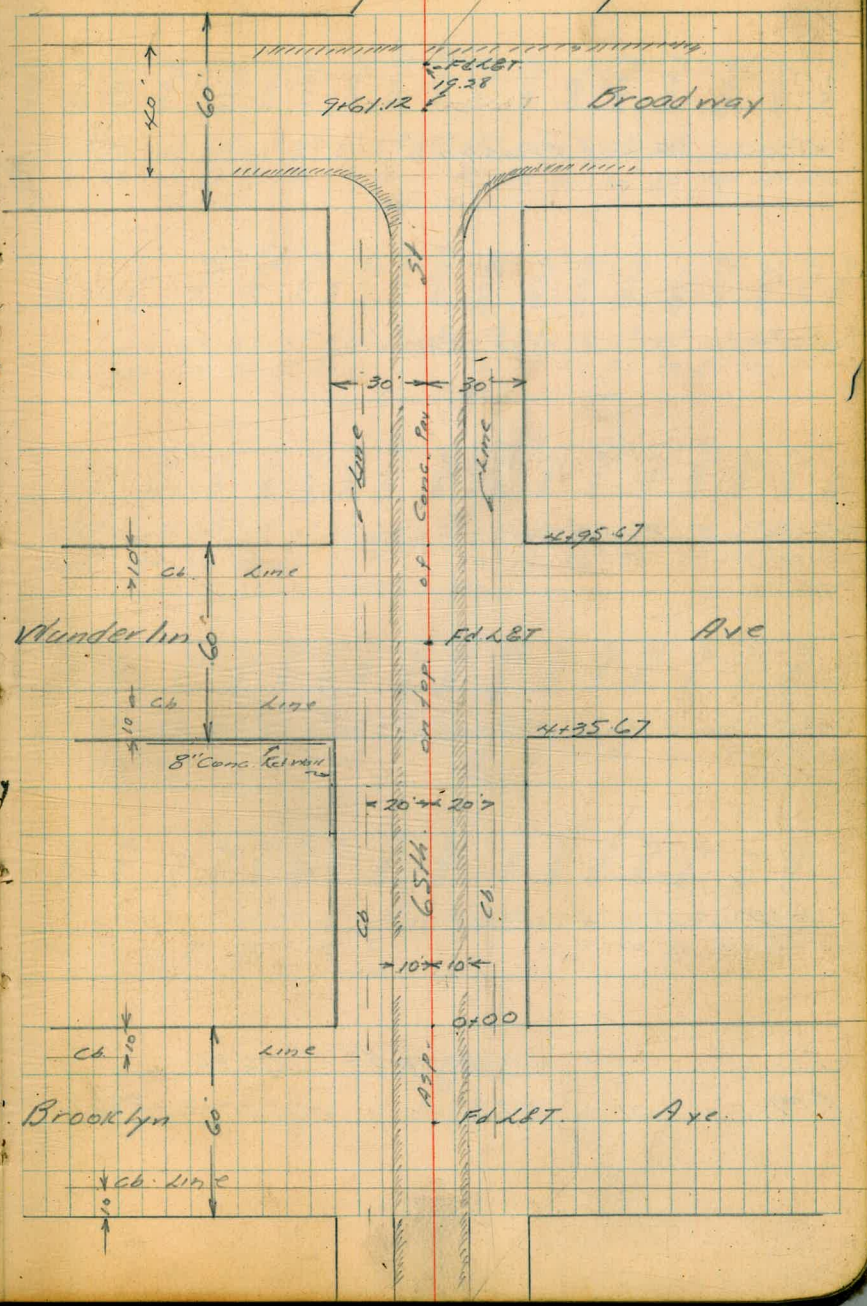
85

9+70 = g.t.	7.70	7046	
9+80.71 = Ang. $11^{\circ}36'30''$ Rt.	7.27	7089	Nail
Check B.M. - S.E. B.P. ^{Pave}	6.69	71.47	1646 - P. 29 71.47
9+92.5 = end H.C. + Beg. Concr.	6.96	7120	
10+00	6.82	7134	
10+50	5.70	7246	
11+00	4.55	7361	
11+50	3.40	7476	
12+00	2.57	7559	
12+12.07 = Ang. $44^{\circ}44'$ Rt.	2.44	7572	on Cross
12+18.77 = Fd. Cross	2.29	7587	on Cross

9-30-49 Profile of Ex Paving on 65th St
 Hendricks Brooklyn to Broadway to Estab. Co. Gr
 Roberts
 Greer
 Bunch

INDEXED
 W. K.
OCT 4 1949

*Notes Reduced & Plotted
 Profile # 2134
 McClennen
 9/5/49*



0+00 to line Brooklyn

0+10 do. Cb line Brooklyn

0+30 do Brooklyn

0+50 do Cb line Brooklyn

0+60 do line Brooklyn

T.P. - 0.04 276.30 11.57 276.34
 B.M. 1.01 287.91 286.90

271.1	271.6	271.2	272.3	271.8	271.5	270.5	267.6	267.85	268.03	267.76	267.9	268.1	267.0	266.1	262.2	260.4	260.0
5 ¹²	4 ¹⁵	5 ¹	4 ⁰	4 ¹⁴	4 ⁸	5 ¹⁰	8 ⁷	8 ¹⁴	8 ¹⁷	8 ¹⁴	9 ⁰	9 ¹¹	9 ¹⁰	10 ¹³	14 ¹	15 ²	16 ¹¹
200	150	106	103	50	34	25	16	10	10	15	20	30	30	50	100	150	200
								Pay	Pay								
270.9	271.5	271.3	269.9	268.8	268.2	267.4	267.57	267.70	267.40	267.1	267.6	267.5	267.1	265.5	261.9	259.9	259.2
5 ¹⁴	4 ¹⁰	5 ⁰	4 ⁴	7 ¹¹	8 ¹	8 ¹⁹	8 ²³	8 ²⁰	8 ²²	9 ¹¹	8 ⁷	8 ¹⁰	9 ¹⁴	10 ¹¹	14 ⁴	16 ⁴	17 ¹
200	150	100	50	26	22	16	10	10	10	15	20	20	30	50	100	150	200
								Pay	Pay								
271.0	271.5	271.3	269.8	268.2	266.8	267.03	267.17	266.88	266.7	266.8	266.7	265.2	261.4	259.7	258.7		
5 ¹¹	4 ¹⁰	5 ⁰	6 ¹¹	8 ¹	9 ¹³	9 ¹⁷	9 ¹³	9 ¹³	9 ¹⁴	9 ⁶	9 ¹⁴	9 ⁶	11 ¹	14 ¹	16 ¹	17 ⁶	
200	150	95	50	27	16	10	10	10	16	26	30	30	100	150	200		
								Pay	Pay								
269.9	270.1	270.2	269.1	268.2	267.7	266.2	266.57	266.66	266.49	265.9	266.2	266.0	264.5	261.3	258.5	258.0	
6 ¹⁴	6 ¹¹	6 ¹	7 ¹⁰	8 ¹	8 ¹	10 ¹	9 ¹³	9 ¹⁴	9 ¹⁴	10 ⁴	10 ⁴	10 ³	11 ⁵	15 ⁰	17 ⁸	18 ¹¹	
200	150	100	50	30	21	15	8	8	15	21	30	50	100	150	200		
								Pay	Pay								
269.9	269.8	269.9	268.6	267.6	267.3	265.8	266.25	266.29	266.17	265.5	266.0	265.5	264.2	261.1	258.9	257.6	
6 ¹⁴	6 ¹⁴	6 ¹⁴	7 ⁷	8 ²	9 ⁰	10 ⁵	10 ⁵	10 ⁰	10 ³	10 ⁸	10 ³	10 ⁸	12 ¹	15 ¹¹	18 ⁰	18 ⁷	
200	150	100	50	30	19	15	8	10	8	15	21	30	50	100	150	200	
								Pay									

276.30
 & 187. 65th. & Wunderlin

3+00

$$\begin{array}{r} 280.20 \\ 928 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 280.26 \\ 928 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 279.97 \\ 957 \\ \hline 0 \end{array}$$

2+50

$$\begin{array}{r} 278.15 \\ 1133 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 278.20 \\ 1128 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 277.26 \\ 1152 \\ \hline 10 \end{array}$$

TP 13.1K 289.48 + 0.04 276.34

$$\begin{array}{r} 276.10 \\ 020 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 289.48 \\ 11 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 275.87 \\ 043 \\ \hline 10 \end{array}$$

2+00

$$\begin{array}{r} 274.06 \\ 228 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 274.13 \\ 217 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 273.83 \\ 257 \\ \hline 10 \end{array}$$

1+50

$$\begin{array}{r} 271.92 \\ 428 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 272.04 \\ 426 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 271.78 \\ 452 \\ \hline 10 \end{array}$$

1+00

$$\begin{array}{r} 269.77 \\ 103 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 269.97 \\ 104 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 269.72 \\ 104 \\ \hline 10 \end{array}$$

0+50

276.30

276.30

4+85.67 No. Cb. line Wunderlin

287.0	287.6	290.9	270.4	290.5	290.6	287.8	287.25	288.00	287.71	287.4	289.3	289.2	288.6	287.2	285.5	284.5	
1K	1M	1M	30	29	29	5	5	37	5	10	15	23	30	50	100	150	200
200	150	100	50	30	20	14	10										
								Pay	Pay								

4+65.67 R. Wunderlin

286.4	287.9	289.0	289.2	289.0	287.0	287.0	287.05	287.08	286.22	286.5	286.8	286.8	286.0	284.6	283.7		
7	5	K	K	K	K	K	6	6	6	6	6	6	7	8	9		
200	150	100	50	27	15	10											

4+45.67 So. Cb. line Wunderlin

285.4	286.7	287.6	287.9	287.9	287.4	286.1	286.20	286.25	285.95	285.7	286.9	286.9	285.1	283.8	282.7		
8	6	5	5	5	6	7	7	7	7	7	6	6	6	8	10		
200	150	100	50	30	22	14	10										

4+35.67 So. line Wunderlin

285.4	285.91	286.1	286.55	286.91	287.36	287.4	287.54	287.1	285.8	285.82	285.55	285.1	287.1	286.9	286.3	284.8	283.4	282.3
8	7	7	6	4	6	6	5	7	7	7	7	8	6	6	7	8	10	11
200	200	160	160	100	50	30	30	15										

B17 647 293.37 2.58 286.90 286.90

R. Wunderlin

293.37
284.24
287.09
287.26
284.12
Fl. of 10
School

4+00

3+50

287.48

289.48

6+50

296.17
98
10
296.93
90
10
296.25
98
10

6+44.8 End SW 24' Rt.

297.00
96
24
296.99
96
29

6+00

294.00
126
10
294.12
125
10
293.91
127
10

5+85.3 Beg SW on Rt (24' Rt)

293.74
13
24
50
293.83
127
29
50

T.P. 13.40 306.62 0.15 293.22

306.62
291.21
215
10
291.36
215
10
291.11
225
10

5+50

287.3	291.0	292.0	291.4	291.1	290.7	288.4	288.41	288.45	288.18	287.8	289.8	290.1	290.3	289.8	288.7	287.9
CL	24	14	20	23	25	50	48	48	51	56	36	33	31	36	X7	53
200	150	100	50	30	19	14	10	10	14	20	30	50	100	150	200	

4+95.67 Ho. Line Wandering

293.37

293.37

9+21.

9+00

8+50

T.P. 1177 $\frac{318.17}{\quad}$ 0.22 306.40

8+00

7+50

7+00

$\frac{306.62}{\quad}$

$\frac{311.92}{625}$
10

$\frac{312.17}{600}$
10

$\frac{312.20}{597}$
10

$\frac{310.79}{728}$
10

$\frac{311.03}{714}$
10

$\frac{311.05}{710}$
10

$\frac{307.82}{1035}$
10

$\frac{308.09}{1008}$
10

$\frac{308.18}{999}$
10

$\frac{318.17}{305.10}$
10

$\frac{305.27}{304}$
10

$\frac{305.25}{307}$
10

$\frac{302.25}{427}$
10

$\frac{302.55}{404}$
10

$\frac{302.46}{416}$
10

$\frac{299.52}{700}$
10

$\frac{299.71}{691}$
10

$\frac{299.61}{701}$
10

$\frac{306.62}{\quad}$

T.P.

BM. 5.95 312.22 312.2x

9+61.12 E Broadway (& Conc Pav)

9+41.12 So. Edge Conc Pav. Broadway

318.17
✓

BP 30 Line Broadway 1' E of Vly. Edge Pav. 65th St.

312.27	312.97	313.29	313.62	313.75	314.33	314.51
5.90	5.20	4.78	4.55	4.42	3.84	3.16
45	30	10		10	39	50

311.50	312.32	312.81	313.03	313.19	313.75	313.86
6.67	5.85	5.36	5.14	4.98	4.42	4.23
50	30	10		10	39	50

318.17
✓

X Sections Orange

Begg # H024
 Doyle W.O. 31425
 Greer 10/19/49
 Bunch

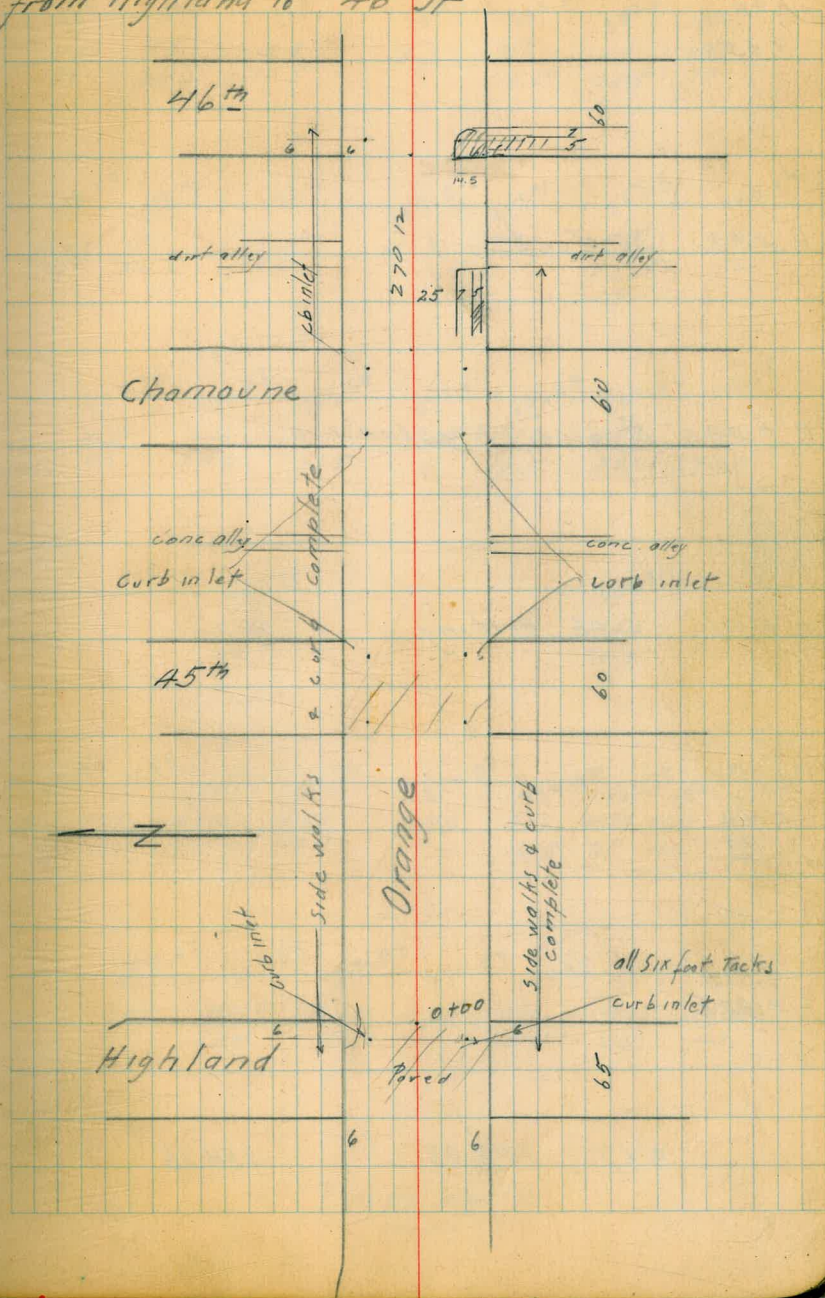
Orange

BM NW BP 354.16 Highland
 352.56 45th
 out 351.20 Channonne
 353.94 46th

INDEXED
 W.K.
 OCT 20 1949

Notes Reduced
 V.W. 10-20-49

from Highland to 46th St



+50

0 + 03 BC of curb.

0 + 00 E Line Highland

- 0.08 curb grating

- 0.12

- 0.325

3.87

358.03

354.16

353.62	352.7	353.2	353.3	353.2	353.1	353.85
441	53	4.8	4.7	4.8	4.9	4.8
66	24.1	12.5		12.5	25.5	66

353.80	352.9	353.5	353.8	353.7	353.5	354.14
423	51	4.5	4.2	4.7	4.5	3.89
66	24.2	12.5		12.5	25.5	66

353.88	353.07	353.54	353.95	353.89	353.49	354.17
415	4.96	4.49	4.08	4.14	4.54	3.86
66	24.6	12.5		12.5	26	25.95

352.98
5.05
28.7

353.34
4.69
30.8

353.83	353.35	353.33	353.76	354.07	354.04	353.73	353.70	354.25
420	4.68	4.70	4.27	3.96	3.99	4.30	4.33	3.78
66	40	24	12.5		12.5	25	40	66

354.05	353.59	353.89	354.28	354.30	353.98	354.41
3.98	4.44	4.14	3.75	3.73	4.05	3.62
40	24	12.5		12.5	25	40

358.03

1+47.04 EC of curb 2' R.

1+45.04 alley line

1+45.04 alley line

1+23.04 BC of 2' Radius

1+10 to 1+20 curb destroyed on Rt.

1+00

358.03

353.3 353.35

47 468
40 40

353.2 353.42

4.8 4.61
40 40.1

353.1 353.09 352.4 352.6

4.9 4.94 5.6 5.4
26.2 26.2 24. 12.5

353.19 352.5 352.8

4.84 5.5 5.2
26.1 24.1 12.5

353.15 352.5

4.88 5.5
BC of 2' 24.1

353.21 352.5 352.8

4.82 5.5 5.2
24 12.5

353.02 352.5

5.01 5.5
CB 24.1 9

352.6

5.4 4.85
25 CB

353.18 **45**

353.50

4.53 4.9
40 40.5
CB

352.8 352.8 352.6 353.26 352.8

5.2 5.2 5.4 4.77 5.2
12.5 2.5 2.5 4.75
CB

352.9 352.8 352.8 353.19 353.58

5.1 5.2 5.2 4.84 4.45
12.5 25.4 27.4 38.8
CB end of
CB

352.8 353.23

5.2 4.80
25.4 25.4
CB

353.0 352.9 352.8 353.48

5 5.1 5.2 4.55
12.5 25.5 CB

358.03

3.96 356.51 ✓
356.52 5.48 352.55 352.56

12 E line of curb

2+70.9 W Line 45th on As Parking

2+40

2+18 90° Rt 10' of.

2+00

1+55 S 90° Lt 12' of

BM 4554

352.56 352.08 351.97 352.17 352.31 352.13 351.65 351.78 352.38
5.77 5.91 6.06 5.86 5.72 5.90 6.38 6.25 5.61
cb 38 24 12.5 12.5 12.5 25.5 40 cb

352.49 352.04 352.28 352.47 352.23 351.71 352.33
5.54 5.99 5.75 5.56 5.80 6.32 5.70
cb 24 12.5 12.5 25.5 cb

352.68 352.0 352.0 352.1 352.1 351.8 352.50
5.36 6.0 6.0 5.9 5.9 6.2 5.53
24 12.5 12.5 25.5 cb

352.07 352.88
5.96 5.15
25.5 32.6

352.85 352.2 352.3 352.3 352.3 352.1 352.77
5.18 5.8 5.7 5.7 5.7 5.9 5.26
cb 24 12.5 12.5 25.5 cb

353.28 352.46
4.75 5.57
331 24.1
side walk
edge

358.03

2+00 drive Rt 11 wide

1+93

1+47⁰⁵ BC of 2' corb

1+45⁰⁵ alley

Alley

1+25⁰⁵ alley

1+23⁰⁵ BC of 2' Ret

51
356.50

352.21
4.30
50
351.96
4.55
cb
351.77
4.74
40
conc

351.96
4.55
50
351.55
4.96
39.9
conc

351.46
5.05
39.6 R
cb
351.81
4.65
5.6
conc

352.28
4.23
50
352.07
4.44
cb
351.90
4.61
40
conc alley

351.82
4.69
cb
351.4
5.1
5.4
351.4
5.1
12.5
351.4
5.1
12.5
351.7
4.8
351.4
5.1
12.5
351.3
5.2
25.5
351.3
5.3
27.5
351.65
4.86
cb

351.80
4.71
cb
351.1
5.4
23.9

351.61
4.90
cb
351.1
5.4
25.5

351.48
5.03
cb
350.7
5.8
24
351.0
5.5
12.5

351.1
5.4

351.1
5.4
12.5

350.9
5.6
25.5

351.33
5.8
cb

351.70
4.81
cb
351.0
5.5
23.8

351.75
4.76
26
351.3
5.2
24
351.2
5.3
24
351.3
5.2
12.5

351.6
4.9

351.3
5.2
12.5

351.73
4.78
40
conc

351.2
5.3
25.5

352.20
4.50
50
351.2
5.3
27.5
351.55
4.96
cb

352.23
4.28
50
conc Par

351.82
4.69
cb

351.69
4.82
39.5
Par

350.72
5.79
25.5
351.75
4.96
32

351.1
5.4

351.46
5.05
25.5
cb

351.2
5.3
25.5

351.2
5.3
27.5
cb

351.3
5.2
25.5

351.3
5.3
27.5
cb

351.1
5.4
25.5

+12E curb line

7.7E grid of drain

R+70.2 W Line Chamoune

R+66 BC of curb ret

R+50

R+13. 10' wide Drive

51
~~356.50~~

351.20	350.68	350.45	350.59	350.56	350.57	350.44	350.34	351.00
531	583	606	592	595	594	607	612	531
	40	24	12.5		12.5	21.5	40	CB

350.27
6.24
29
7.11

350.06
6.45
29.9
9.41

351.08	350.36	350.81	350.86	350.73	350.33	351.11
543	615	570	565	578	618	540
CB	244	12.5	14.1	12.5	25.7	CB

351.14	350.5	350.6	350.8	350.7	350.5	351.08
537	60	59	57	58	60	543
CB	24	12.5		12.5	25.5	CB

351.20	350.5	350.8	350.9	350.9	350.6	351.07
531	60	57	56	56	59	544
CB	23.7	12.5		12.5	25.5	CB

350.79
5.72
25.5

351.51
5.00
32.5

51
~~356.50~~

1+00

T.P. 5.56 ⁹⁸ 357.99 4.09 ⁴² 352.47

+ 92 drive Rt 9 wide

+ 62 drive way 12' wide 24 ft

0+50

60 E = E Line Chamoune
= 0+00 ahead

52 E

48 E curb line

30 E Chamoune

⁵¹
356.52

352.52 351.9 352.0 352.0 352.0 351.7 50 352.46
5.46 6.1 6.0 6.0 6.0 6.3 5.52
2.4 12.5 12.5 12.5 25.3 .66

257 ⁹⁸
29

351.71 352.52
4.80 3.99
2.5 3.25

352.41 351.75
4.10 4.76
3.3 2.4

352.05 351.6 351.7 351.7 351.7 351.5 352.08
4.16 4.9 4.8 4.8 4.8 5.0 4.43
.66 23.8 12.5 12.5 25.3 .66

351.74 351.19 351.51 351.49 351.31 351.23 351.69
4.77 5.32 5.00 5.02 5.20 5.28 4.82
.66 2.4 12.5 12.5 25.3 .66

grid of catch basin 5.66

351.80 351.26 351.22 351.25 351.12 351.16 351.08 350.61 351.64
4.71 5.25 5.29 5.26 5.39 5.35 5.43 5.90 4.87
.66 4.0 2.4 12.5 12.5 25.3 4.0 4.6

351.46 351.15 351.15 352.06 351.10 351.22 351.21
5.05 5.36 5.36 4.45 5.41 5.29 5.30
4.0 23.5 12.5 12.5 25.3 4.0

356.52 ⁵¹

1+95 20' Drive way

1+85 20

1+47⁰⁶ BC of curb 2" Rad

1+45⁰⁶ alley East

1+25⁰⁶ alley

1+23⁰⁶ BC of 2" Rad

98
357.99

353.53
4.41-
332

352.60
5.38
24

353.23
475
66

352.6
5.4
24

352.8
5.2
125

352.8
5.2
125

352.9
5.1
245

352.8
4.2
26

353.8
3.6
40

354.4

352.95
5.03
66

352.3
5.7
24.1

353.17
4.81
40

353.00
4.98
66

352.8
5.2
26

352.5
5.5
24

352.7
5.3
125

352.7
5.3
125

352.5
5.5
125

352.2
5.8
23

352.9
5.1
26

353.0
5.0
36

353.9
4.1
40

352.0
5.0
40

352.80
5.8
66

352.6
5.4
26

352.3
5.7
24

352.4
5.6
125

352.5
5.5
125

352.4
5.6
125

352.4
5.5
125

352.1
5.8
125

352.71
5.7
125

352.87
5.7
125

352.78
5.2
60

352.2
5.8
75.3

352.4
5.5
25.3

352.65
5.3
25.3

352.9
5.1
40

98
357.99

Orange

from Highland to 46

52

BM

405 353.93
94 35394

46 46st

30 E

353.69	353.70	353.73	353.71	353.71	353.65	353.62
429 40	428 24	425 12.5	427	427 12.5	433 25	436 40

12 E curb line

353.91	353.32	353.53	353.67	353.70	353.54	353.23	353.03	353.63
407 06	466 40	440 24	431 12.5	428	444 12.5	475 25	495 40	435 06

B + 70 12 W Line 46 5st

353.96	353.32	353.56	353.67	353.41	352.96	353.64
402 05	466 24.1	442 12.5	431	457 12.5	502 24.9	434 06

2 + 66

353.92	353.3	353.5	353.6	353.5	353.0	354.4	354.2	354.7
406 06	407 24	415 12.5	44	45 12.5	50 24	26 26	33 37	33 40

98
357.4

98
357 99

12-23-49
 Hendricks
 Johnson
 Greer
 Cota

Profile of Calle De La Plata
 from Dorado to Calle De La Playa

These profiles to determine
 amount of Paving to be replaced
 due to settlement in placing sewer
 See P 57 for Grades of
 improvement.

1+00

0175

0150

0125

0100

0-17 Sewer 17H.

B17 2.41 $\frac{9.99}{\lambda}$

INDEXED
 N.K.
 FEB 6 1950

(758)
 Assumed

G.H.		$\frac{k}{\text{on sub grade slope}}$		53 G.R.T.
5.37	5.5	5.38	5.2	5.27
4.66	4.4	4.61	4.8	4.72
15	2		2'	15
5.45	5.6	5.52	5.4	5.56
4.54	4.4	4.47	4.6	4.43
15	2		2'	15
5.62	5.7	5.66	5.2	5.57
4.37	4.3	4.33	4.2	4.42
15	2		2	15
5.71	6.1	5.76	5.5	5.86
4.28	3.9	4.23	4.4	4.3
15	2		2	15
5.85	6.1 6.1	5.82	5.6 5.6	6.16
4.15	3.9 3.9	4.7	4.3 4.2	3.83
15	10 2		2 10	15
5.90	6.0	6.04	6.0	6.32
4.10	4.0	3.95	4.0	3.67
15	10	Rim 17H	10	15

NE of Dorado & La Plata

Cont'd from p. 53.

2+50

2+25

2+00

1+75

1+50

1+25

9.99
7

G. L.

on subgrade
stage

54
G. R.

450	48	456	48	457
549	52	543	52	540
15	21		21	15

459	48	470	49	480
540	52 52	529	51	519
15	7 2		21	15

471	48	484	46	480
529	50 52	515	54	519
15	8 2		21	15

499	50	497	51	502
500	48 50	502	49	497
15	7 2		21	15

490	59	510	52	518
509	48 51	489	48	481
15	7 2		21	15

524	58	525	51	522
475	46 45	474	49	477
15	7 2		2	15

4+00

3+75

3+50

3+25

3+00

2+75

9.99
x

G

on Sub grade
stake

55
G

358	25	362	36	360
621	65	637	64	639
15	2		2	15

387	39	380	38	374
612	61	615	62	625
15	2		2	15

395	39	403	39	397
604	61	596	61	603
15	2		2	15

412	39	418	39	426
587	61	581	61	573
15	2		2	15

428	44	429	43	431
521	55	520	57	568
15	2		2	15

445	46	444	45	456
554	55	555	55	543
15	2		2	15

See p 57 for Grade
of Improvement.

4+45 BC Cb. Ret. Rt.

353	37	352	38	394
646	63	647	62	605
15	9		10	15

4+25

350	38	356	33	389
649	62	643	61	610
15	10		5	15

4+10 BC Cb. Ret. Rt.

355	31	358	33	372
649	69	641	67	627
15	2		2	15

Grades of Improvement
Lo Plata St.

4+45 BC Cb. Ret. Lt.
4+25
4+10 BC Cb. Ret. Rt.
4+00
3+75
3+50
3+25
3+00
2+75
2+50
2+25
2+00
1+75
1+50
1+25
1+00
0+75
0+50
0+25
0+17 EC Cb. Ret. Lt.
0+00 EC Cb. Ret. Rt.
0-17

Gr. Lt.		Gr.	Gr. 57
3.49		3.86	3.92
3.54		3.89	3.93
3.58		3.90	3.93
3.64	3.83	3.93	3.93
3.78	4.00	4.11	4.04
3.92	4.20	4.34	4.17
4.06	4.34	4.48	4.30
4.20	4.48	4.62	4.44
4.34	4.61	4.75	4.56
4.48	4.75	4.88	4.68
4.63		5.02	4.81
4.77		5.15	4.94
4.91		5.29	5.07
5.05		5.42	5.20
5.19		5.56	5.33
5.33		5.69	5.46
5.48		5.83	5.59
5.62		5.97	5.72
5.71		6.09	5.88
5.75			
5.84		6.15	6.16
5.89		6.04	6.32
		Rim 17H	

Survey along Φ of Road Shown on Misc Mpp# 213

By W.L. Bauer

$10+08.08 = \text{Pin} = \text{P.I.} - \text{Ang. } 55^{\circ} 25' 45'' \text{ Rt.}$

INDEXED
W.L.K.
FEB 6 1950

$7+45.36 = \text{Hub.} - .03 \text{ W. of } \Phi - \text{Pins} - 25' \text{ from Hub.}$

$6+54.66 = \text{City Mon. } 0.27 \text{ West. of } \Phi$
($330.14 \text{ W. of Cor.} - \text{B. } 1799 - \text{P. } 39$) also see Ties to
2" Pipes to W.

$3+90.20 = \text{Pin} - 0.10 \text{ W. of } \Phi$

Pins Noted are - $3/4"$ Diam. Iron ϕ

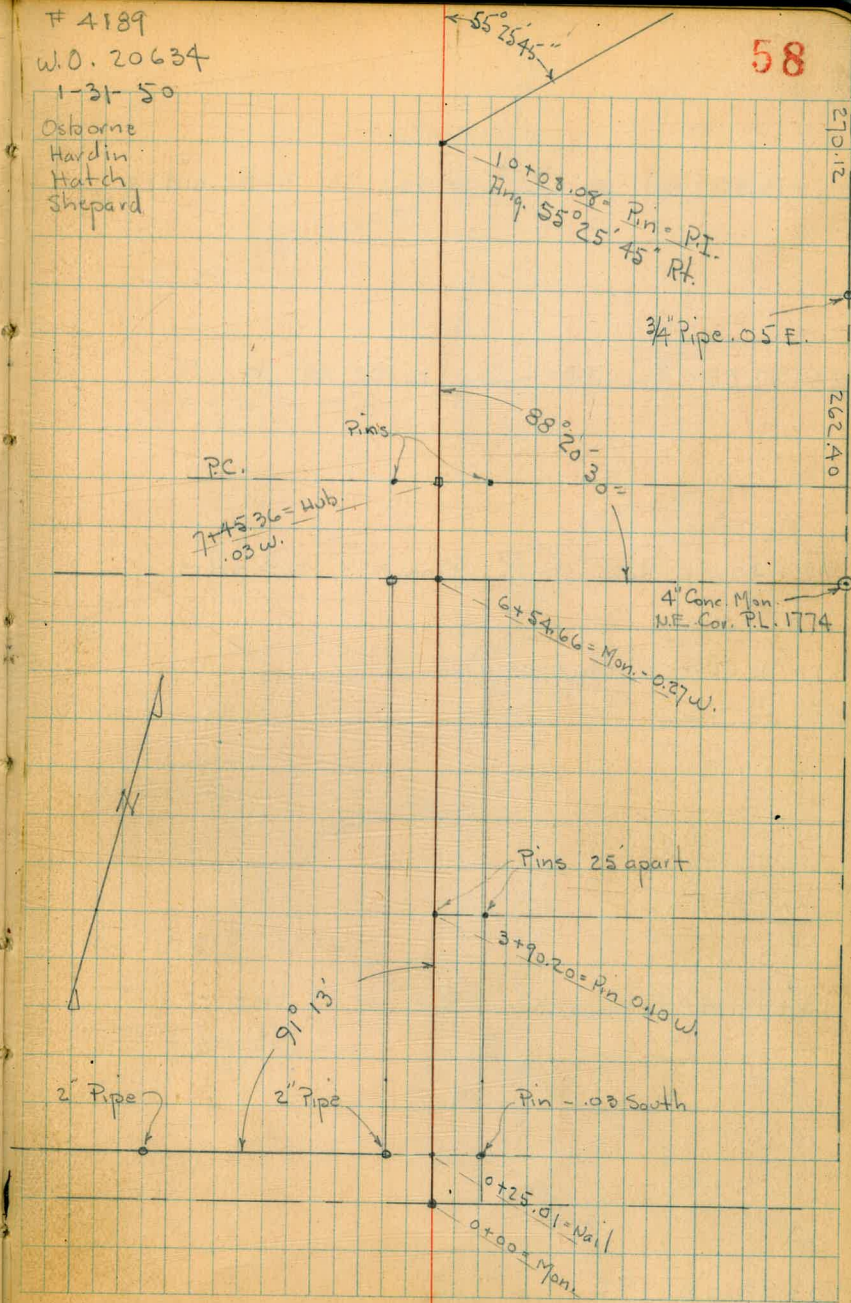
$0+25.01 = \text{Int. with Line Thru } 2" \text{ pipes}$

$0+00 = \text{city Mon.} - \text{Replacing Pipe shown on Misc. Map\# } 213$

See B. 1799 - P. 39 + B. 1849 - P. 58

F 4189
W.O. 20634
1-31-50
Osborne
Hardin
Hatch
Shepard

58



25+13.86 - Hub at E.C. - Pins - 25' Both sides

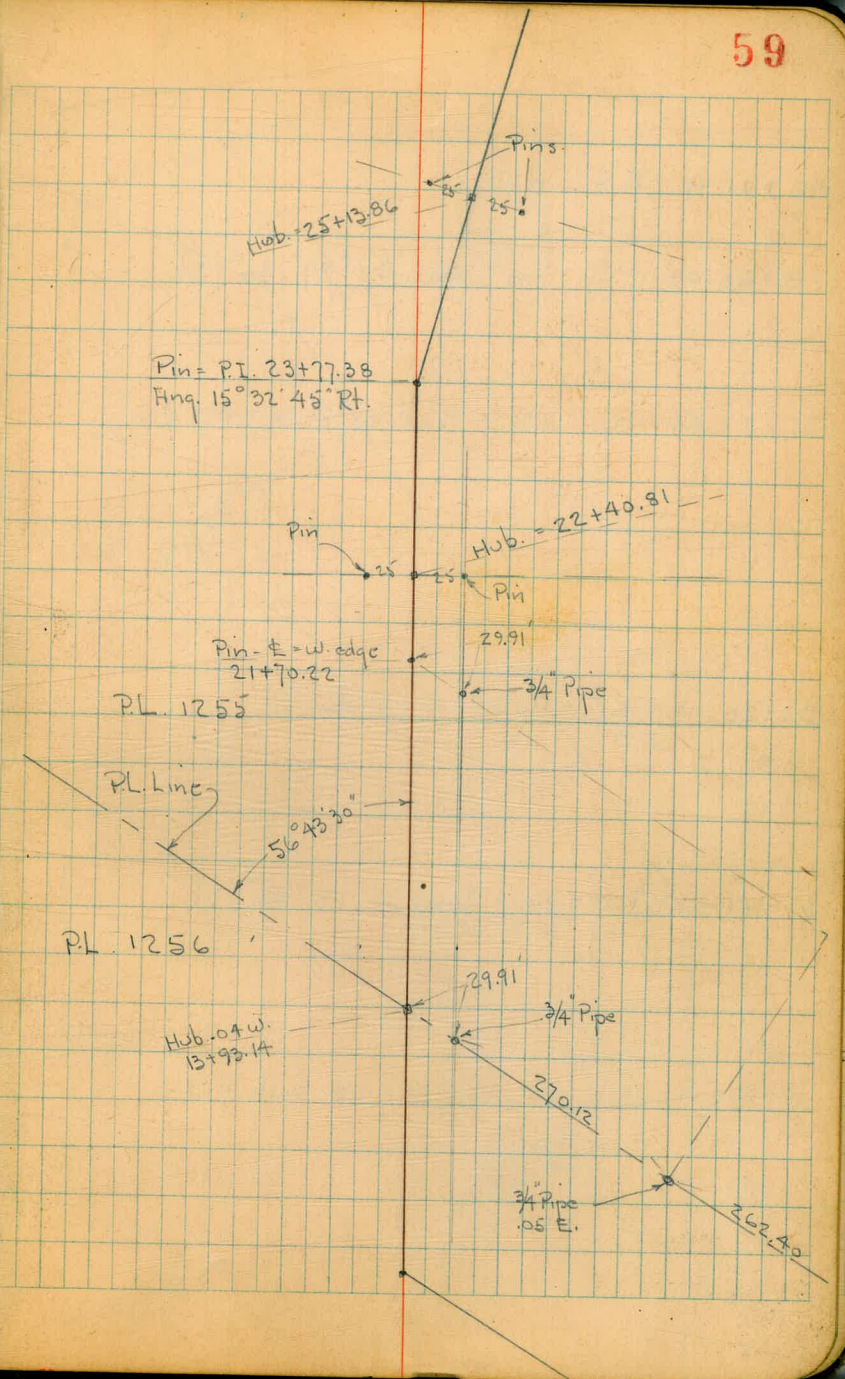
23+77.38 = Pin - P.I. - Ang. 15° 32' 45" Rt.

22+40.81 = Hub. at P.C. Pins - 25' Both sides

21+70.22 = w. edge of Pin

13+93.14 = Hub. of w. of Φ - on P.L. Line

10+08.03 = P.I.



$$40 + 01.14 = E.C. = \text{Hub}$$

$$38 + 65.03 = P.I. = \text{Pin} - \text{Ang. } 30^\circ 27' 30'' \text{ Lt.}$$

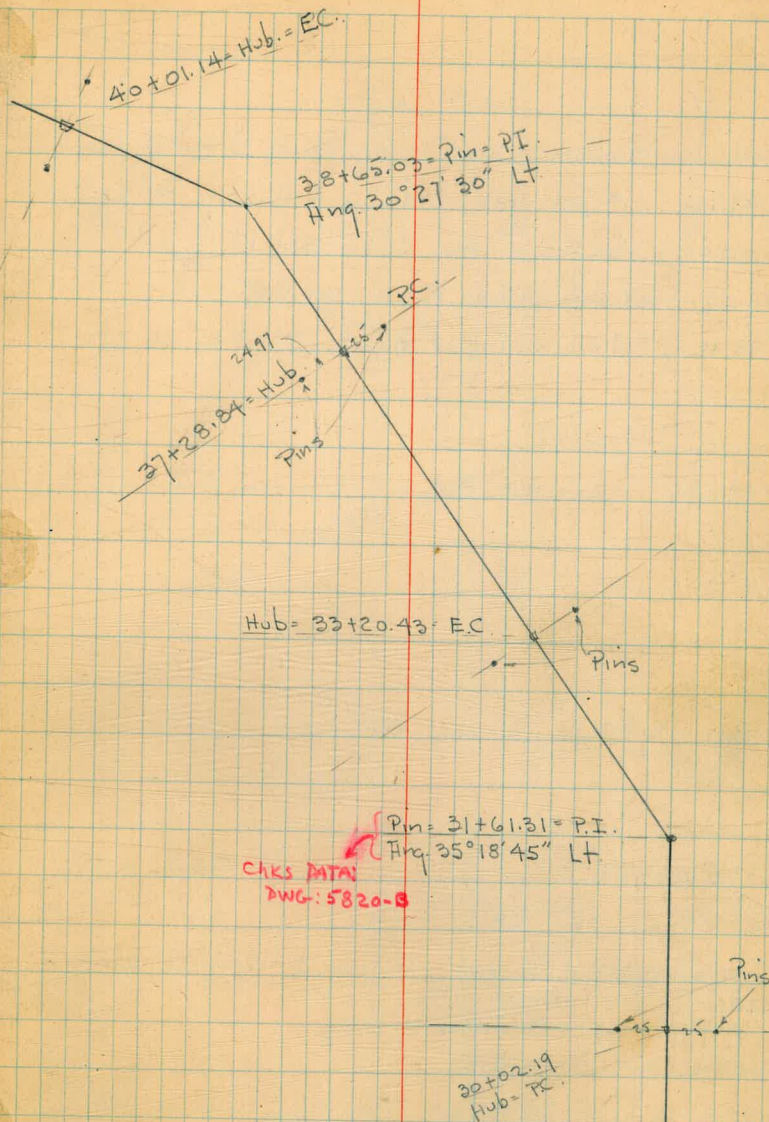
$$37 + 28.84 = P.C. = \text{Hub} - \text{Pins } 25' \text{ Rt. } \pm 24.97' \text{ Lt.}$$

$$33 + 20.43 = E.C. = \text{Hub}$$

Pins =

$$31 + 61.31 = P.I. = \text{Pin} - \text{Ang. } 35^\circ 18' 45'' \text{ Lt.}$$

$$30 + 02.19 = \text{Hub} - P.C. \quad \text{Pins} - 25' \text{ Both sides}$$



apart along Boundary of Tract #1 - Ang. $67^{\circ} 39' 30''$ Bet. Chord + Bound.
 $53+47.76$ = Set Hub Midway Between Pins - 53.03
 $53+10.20$ = Set Hub - Ang. $3^{\circ} 26' 15''$ Rt.
 $53+01.09$ = Set Hub. on E.C. Midway bet. Pins
 $51+98.42$ = Set Hub on Int. of Tangents - Ang. $46^{\circ} 42'$ Lt.

$50+94.75$ = Set Hub Midway Between Pins

$47+87.25$
 Fd. Pins - Set Hub Midway Between

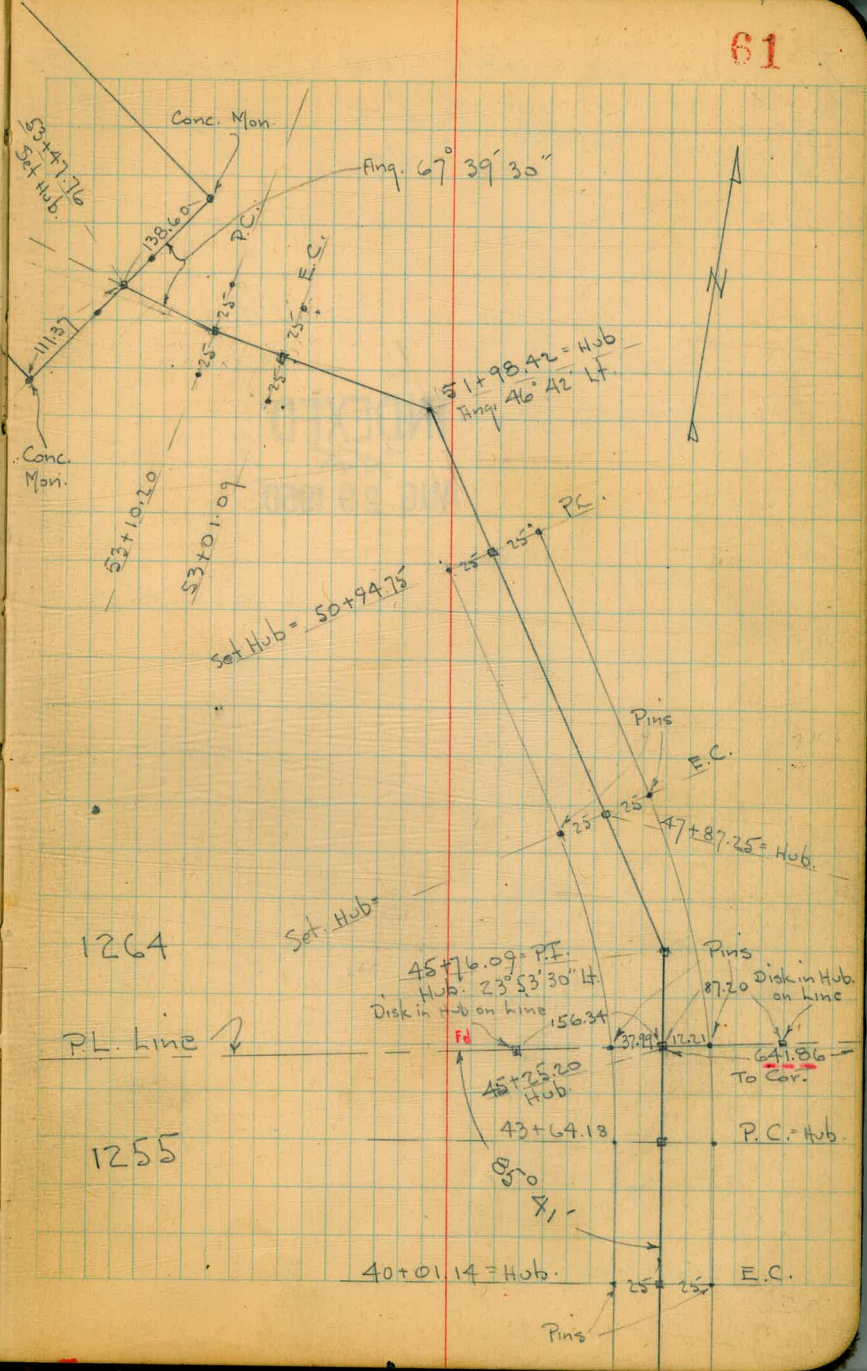
$45+76.09$ = P.I. = Set Hub. on Int. of Tangents
 Ang. $23^{\circ} 53' 30''$ Lt.

$45+25.20$ = Hub. on Int. of Tang. + True P.L. line
 641.86 To 3×3 Post. - Nail in Top.
 Pin 37.99 Lt. 0.065 - Pin 12.21 Rt. 0.025

$43+64.18$ = P.C. = Hub.

Prod. & N. from $38+65.03$ Thru this Hub to int. for P.I.
 Bauer Must of Ran along Side Lines

$40+01.14$ = E.C. = Hub. - Pins = $25'$ Both Sides



1264

PL. line ↓

1255

$40+01.14$ = Hub.

Pins

E.C.

P.C. = Hub.

641.86 To Cor.

Disk in Hub on line

Pins

$47+87.25$ = Hub.

E.C.

Pins

P.C.

$51+98.42$ = Hub
 Ang. $46^{\circ} 42'$ Lt.

Set Hub = $50+94.75$

$53+01.09$

$53+10.20$

Conc. Mon.

Ang. $67^{\circ} 39' 30''$

Conc. Mon.

$53+47.76$
 Set Hub.

X Sec Alley Blk 104 University Hts

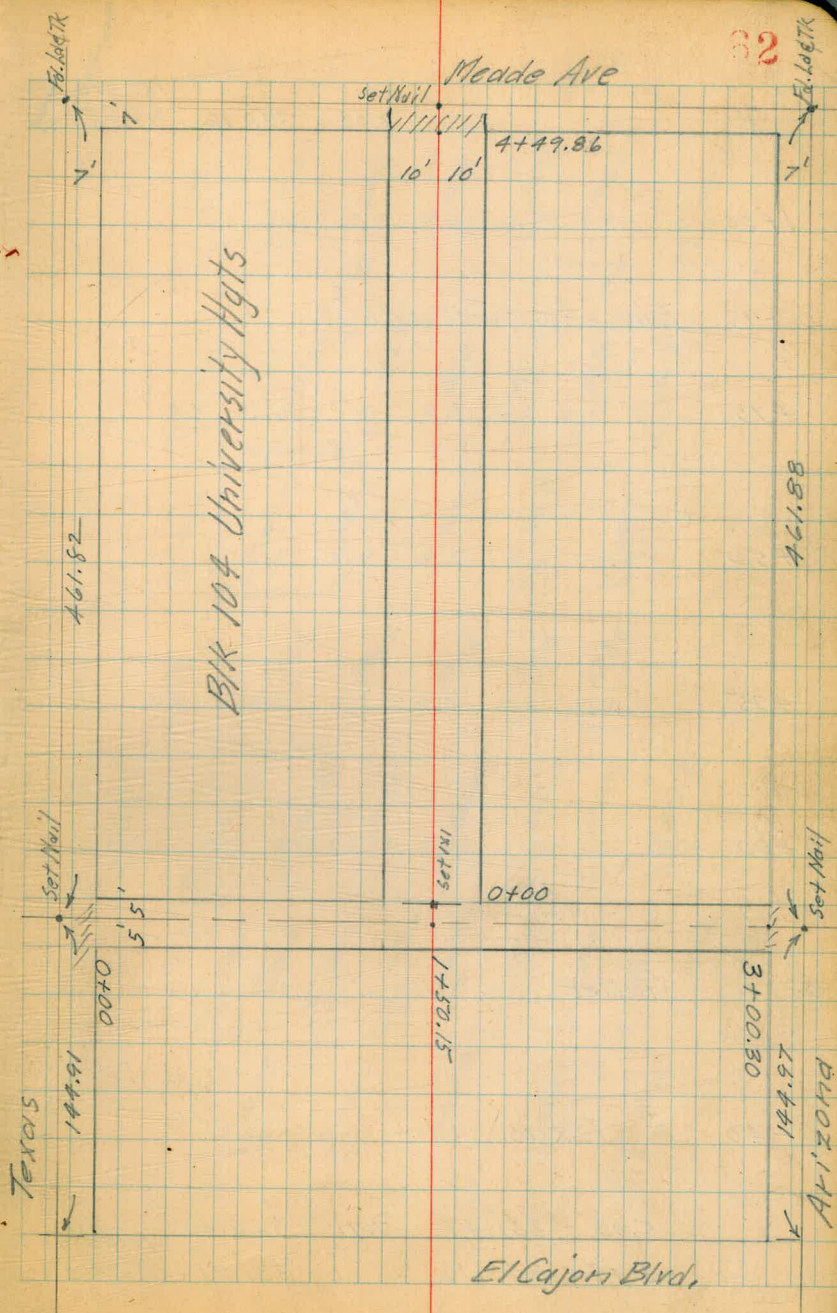
Begg
Johnson
Allen

25 Aug 50

W.O.

?

INDEXED
W.K.
AUG 29 1950



7

3.29

328.18

1X1 STA. 0+00
N&S ALLEY

1+00

+92 End of parallel walk

+75

+50

+25

0+00 R

0-14 Gutter

0-40 & Texas

5.02

331.47

7.71

326.45

Texas &
Medde
SEBP

2.75

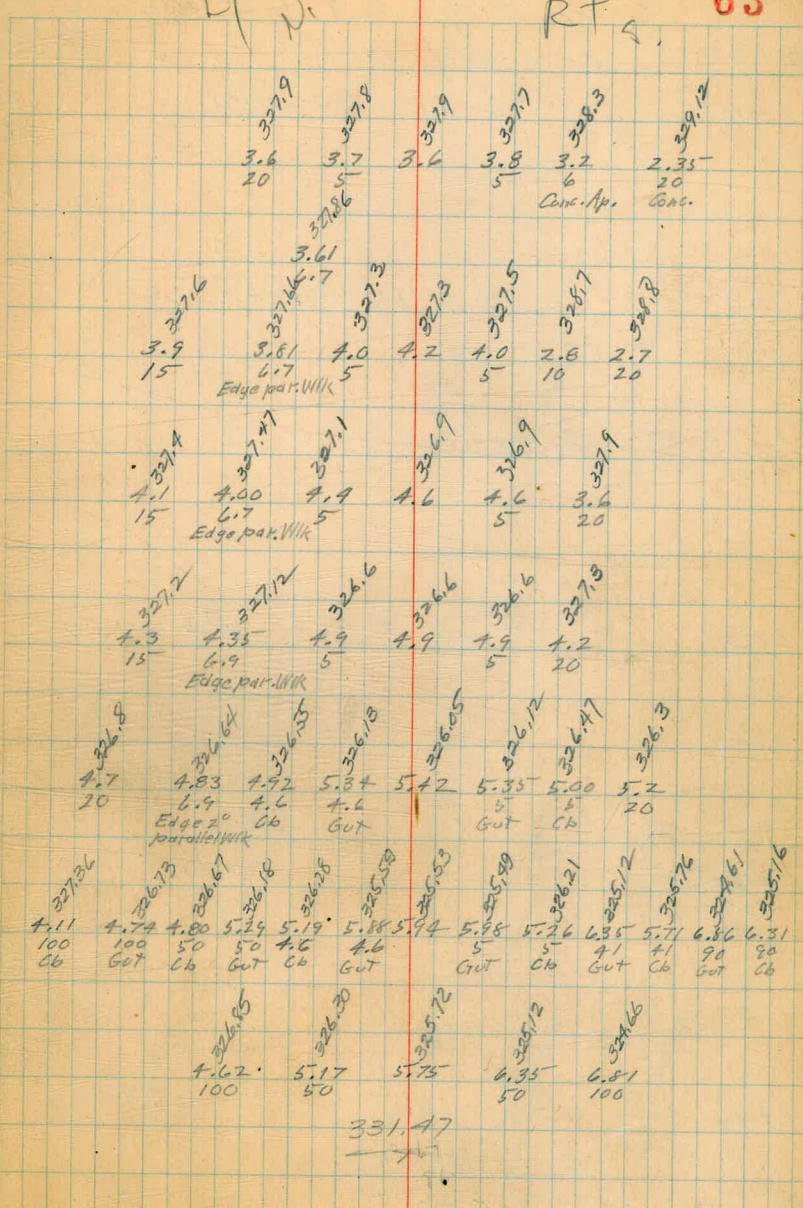
334.16

331.41

Lt N.

Rt A.

63



X Sec Alley Blk 104 University Hts.
 1+98 end bldg 11.1 R
 1+97 $\frac{1}{2}$ P Pole 4.4 PH 2450

1+59 $\frac{1}{2}$ 7.6 $\frac{1}{2}$ beg Picket fence

1+50 $\frac{1}{2}$ $\frac{1}{2}$ cross Alley

1+38 $\frac{1}{2}$ P Pole 3'R PA 2450

1+25

1+16

7.5R 335.70

328.18

328.2
 7.5
 5.0
 5.0
 330.7
 332.2
 8.5

327.9
 7.4
 7.1

327.8
 7.9

329.7
 6.0
 5

330.4
 5.5-6
 6

330.74
 4.76
 10.5
 Bldg

327.8
 7.9
 5

327.9
 7.8

328.16
 7.54
 6
 above
 conc

328.74
 6.96
 12

335.70

2+57 by House 70 R

2+55 $\frac{1}{2}$ 5.3 Wide Walk

2+50 70 Lt Beg House

2+33 $\frac{1}{2}$ garage Sing Rt 8.6

2+17 end of fence 6.8 Lt

2+06

10 44 338.62

7.5%

328-18

2+00

335.70

332.53
6.09
7

331.97
6.65
10.2
EW Walk
2.5 wide

331.4
7.2
5.2

331.2
7.4
5.1

331.3
7.3
5.1

331.96
4.66
8.6

331.1
7.5
3.5

330.9
7.7
7

330.5
8.1
5.1

330.5
8.1

330.5
8.1
5

330.5
8.1
10

330.9
7.7
2.5

338.62

330.5
5.2
7

330.1
5.6
5

330.1
5.6
335.70

330.7
5.5
3

330.7
5.7
5

333.0
4.7
10

333.1
2.6
2.0

X Sec Alley Blk 104 University

H5 Contd

E4W Alley

66

3+1430

3+0030

Prop Line on Asphalt Paving

3+907

beg Wall 4.7 RR
7.3 R end of base

3+78

beg Wall 5.8
end of House 7.0 Lt

2+60

338.62

0.16 CB 7	0.77 7	0.80 4.7 9	0.90 7	0.89 5	0.90 7	0.25 18
338.96	337.85	337.82	337.72	337.73	337.72	338.27
0.27 CB A.7	0.57 4.7	0.56 7	0.55 5.0	0.27 CB		
338.35	338.05	338.06	338.07	338.35		
4.1 7	4.4 5	4.4 5	4.6 5	4.6 7		
334.5	334.2	334.2	334.0	334.0		
5.5 7.1	5.6 5	6.3 3	6.4 5	6.3 5	6.0 10	6.3 18
333.1	333.0	332.3	332.2	332.4	332.6	332.7
338.62			338.62			

Top of Wall

X Sec Alley Blk 104 University Hts.

1+50 13 1/2 end wire fence beg wire fence 109

1+00 beg woven wire fence 13.0 ft.

0+89 10.3 1/2 pole A4323

0+62 10.4 ft dead man

0+50 end of fence 9.3 R

Alley

0+28 9.9 5 ft end rubble wall

0+15

0+02 9.5 R beg picket fence
rubble cement wall wire fence

0+00 T INTERSECTION

904 337.22

338.18

8.0 20	7.0 10	6.2 10	5.6 10	5.0 10
329.2	330.2	331.0	331.6	331.9
8.2 25	7.9 10	7.6 10	5.6 10	4.6 20
329.0	329.3	329.6	330.6	332.6

8.3 20	7.4 10	7.8 10	7.7 10	7.7 10	7.2 20
328.9	329.8	329.9	329.5	329.5	330.0

8.7 10	8.3 10	7.9 10
329.1	328.9	329.3

9.1 10	9.0 10	8.6 10
328.1	328.2	328.6

337.22

2+50

2+45 $\frac{1}{2}$ S. gar 17° R.

2+33 10/16 P Pole PA 4353

2+09 $\frac{1}{2}$ single double garage 17.1 R.

2+02 end Picket fence 10.2 R.

2+00

1+15 fence picket

1+70 single gar 9.9 R.

1+55 $\frac{1}{2}$ 3' conc wall 10 R.

337.22

68

331.8
5.4
20

332.8
4.4
10

333.6
3.6

333.7
3.5
10

334.10
3.12
17

333.90
3.32
17.1

331.0
6.2
25

331.5
5.7
10

332.4
4.8

332.5
4.7
10

331.50
5.42
9.9

331.69
5.53
10

337.22

Alley Bk 104 University #15
4700 13.7/wire fence

3+84 }
3+73 } 10 R 5 stumps
3+73 } 14 R. To 33 R apron 3 wide floor 4.64
3+50 13 R cypress

3+46 105% P Pole JPA 4369
3+46 end of 4 car garage 16.2 ft

TP 5-24 339.90 256 334.66

3+33 1/2 5 gar 17 R

3+13 1/2 5 gar 17 R

3+04 1/2 5 gar 17 R

3+03 beg 4 car garage 15.9 ft

3+00

337.02

334.4
5.5
25

335.1
4.8
10

335.1
4.8

335.4
4.5
10

335.4
4.5

69

334.0
5.9
25

334.5
5.4
10

334.7
5.2

335.0
5.4
10

335.0
4.88
14
Apron
gar 4.64 ft

335.12
4.78
33

333.96
5.94
16.2

339.90

334.32
2.90
17

334.37
2.85
17

333.19
3.33
15.8

332.8
4.4
25

334.1
3.1
10

334.3
2.9

334.2
3.0
10

337.43

59

Alley Blk 104 University Hg

Contd.

- 849 331.41 331.41
SE BP.

Texas & Mead

x ? x

+16 curb line

H+4986 Prop line Meade

H+46 & 48 10.49 2 Palms

339.90

334.29
5.66
10

Par

334.39
5.51

334.77
X.573
10
9

334.71
5.19
6

334.62
5.28
10.0
9.44

334.54
5.36
Par

335.06
4.84
10.2
5.7

335.26
4.64
6

339.90

Calle Corta
Proposed sewer.

3-13-52

Sommermeier

W.O. 62248

Be99

Oltman

Not check each other.

Note - Tacks on Calle Corta do

Used data on sheet 17-1 (Ref. 3124-B)

4+35.95 - End of line

2+78.71 = Δ 17° 21' Lt.

2+78.70 = 1/2 P.O.T.

2+32 = End 1/2 - 1" thick oil & rock

oil & rock.

1+19 = end Concrete Pavement + start 1/2" to 1" thick

La Jolla Shores Dr.

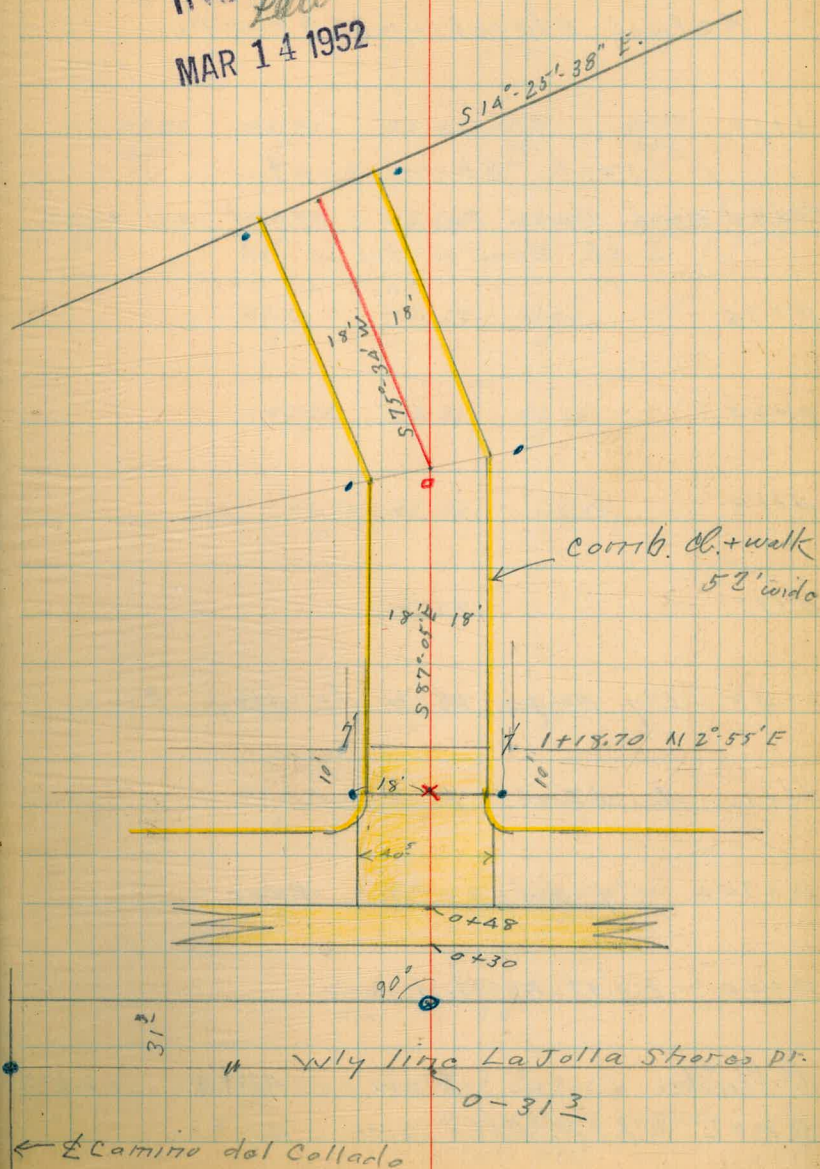
1+08.70 = Cross in Pavement. Ely. 10' line

Shores Dr.

0+00 = Existing M.H. Calle Corta + La Jolla

INDEXED

MAR 14 1952



Calle Corta
Levels

72

Direct Elev. rod used.
Actual elevations shown.

47.49

1+50

rock skim coat.

1+19 - end Conc. Pavc. + start ail +
Ch. denotes top of ch
" " back of walk

0+96

0+80

0+58

0+53

0+48 Fly edge 18' wide strip Pavc.

0+39 ± 18' strip pavc.

0+30 = wly edge Conc. Pavc

0+00 = Existing M.H.

B.M. #1. Elev. = 42.94

B.M. #2 N.E. Lt. Calle Corta. 43.83

	45.93 203 W	45.77 15 W	45.43	45.32 15 W	45.50 202 W		
	44.11 203 W	43.77 15 W	43.75	43.60 5	43.46 15 W	43.66 203 W	
		42.70 5	42.59	42.46 5			
		42.92 5	42.81	42.68 5			
		42.78 5	42.70	42.52			
			42.64				
		42.85 5	42.80	42.61 5			
		42.89 5	42.81	42.65 5			
		42.74 5	42.65	42.57 5			
		40.63 Rim	31.93 IE				

U.S.G.S. Plate Ctr. S.W. Ret. LaJolla Shores
Driv + Calle Collado
(also - P18)

4+35²⁵ 18'± Lt. + Rt. = cont curb + walk.

4+00

3+50

3+00

2+78.91 = Δ 17° 21' Lt. (data sheet 17-)
see sketch
sec. on split

2+50

2+32 = Emd oil + rock skim coat.

2+00 Put here

2+00

2+20 Extra Section

61.02	60.89		60.3	60.85	61.05
203	Top. cl.			Top. cl.	203
W					W

J.M.

58.8

56.86

56.68

56.4

56.67

56.80

203

15

15

203

W

Cl

Cl

W

53.6

53.64

53.48

53.4

53.26

53.37

203

15

15

203

W

Cl

Cl

W

50.9

49.9

48.2

50.21

50.00

49.56

49.59

203

15

49.3

15

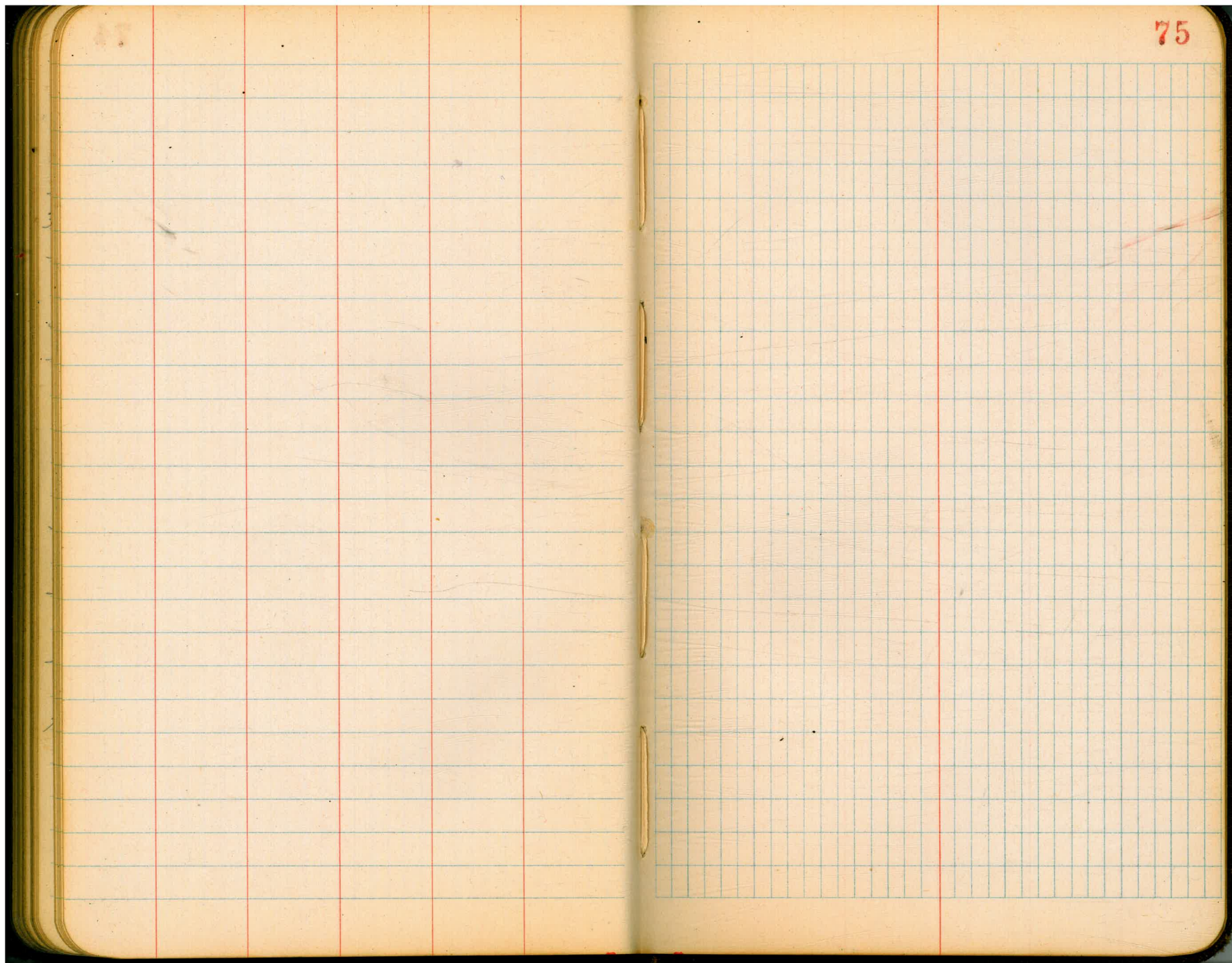
203

W

Cl

Cl

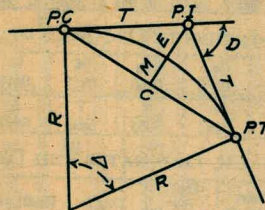
W





DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

Radius= $R = \frac{50}{\sin. \frac{\Delta}{2}}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) Δ = Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8 \frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 - Sta. P. C. = 54.50, hence offset = $7.27 \frac{54.50}{100} = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8 \frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8 \frac{1}{3} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

0-11.16

9+03.06

899.8
34
9+03.2

11.25

11+28.6

Ocaso Bet.
Del Oro + Frescoq
on W.

6+54 - 15° 11

7+87.67 - 4° 50

9+17.07 - 11° 51'

11+34.66 - 15° 31'

536.0

443

247

1226-

10-31 Hendricks

R.E. 4847

5278'

98055' 40"

US. C+G

26.22

- Top wall - By Bldg.

Floor - Basement 18.80

4153

83

4070

51473
40567

98040
1928

96112

5553
3595

6008

1282
48

1340

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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