

1865

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

1  
Alley Blk. 29 Fairmount Add. 1-8  
To City Hgts  
Alley Blk 25 Bird Back 73-

Levels Alley Bk 29  
Fairmount Add. to City Hgts

Sketch F.B. 1831-P 32

6-23-48

W.O.# 31168

Sommermeier  
W. Moore  
L. Melton  
W. Duncan

0+89 23<sup>5</sup> Lt. =  $\Phi$  Sing Gar. Conc. Floor

0+84 9<sup>8</sup> Lt. = End picket fence.

0+75 10<sup>1</sup> Rt. = End picket fence

0+50

0+47 7<sup>6</sup> Lt. = (W)

0+27 9<sup>0</sup> Rt. = (W)

0+25 10<sup>1</sup> Rt. = Start Picket Fence  
10<sup>2</sup> Rt. = N.W. Cor. Garage.

0+11 10<sup>1</sup> Rt. = End Picket Fence.  
10<sup>2</sup> Rt. = S.W. Cor. Gar. South. Ent.

10<sup>1</sup> Rt. = start Picket Fence.

8<sup>2</sup> Rt. = Ctr. Mail box

10<sup>0</sup> Lt. =  $\Phi$  4" wide E.+W. Conc. wall

0+00 = N. line Polk. 9<sup>2</sup> Lt. = start picket fence

B.M.# 6  
1831  
78

5.14 347.94 — 342.80

Water reduced - 7-48  
Mark Level

1

INDEXED  
JUN 24 1948

346.30  
1.64  
23.5  
Floor

345.8  
2.1  
23

345.9  
2.0  
10

346.3  
1.6

346.6  
1.3  
10

347.1  
0.8  
12

347.2  
0.7  
25

345.0  
2.9  
25

345.2  
2.7  
11

345.6  
2.8  
10

345.7  
2.2

345.8  
2.1  
10

346.1  
1.8  
25

344.4  
3.5  
10

344.6  
3.3

345.0  
2.9  
10

2.70  
162  
E door

344.50  
3.44  
10  
Top wall

343.7  
4.2  
10  
Base wall

343.9  
4.0  
10  
Crd.

344.1  
3.8

344.4  
3.5  
7

344.9  
3.0  
10

344.9  
3.0  
15

347.94

Alley BIK 29

1+69 20<sup>3</sup> Lt. = <sup>No Apron.</sup> Sing. Gar. Conc. Floor

1+59 10<sup>2</sup> Rt. = End board Fence

1+44 10<sup>6</sup> Lt. = (W)

1+41 8<sup>2</sup> Rt. = (W)

9<sup>2</sup> Rt. = start board fence

1+25 10<sup>2</sup> Lt. = Start Cyclone wire fence

1+22 9<sup>2</sup> Rt. = N. Edge (N.W. Cor.) Conc. Drive

1+19 54' Rt. =  $\Phi$  Garage doors

1+16 9<sup>2</sup> Rt. = S. Edge (S.W. Cor.) Conc. Drive

T.P. 6.59 353.75 0.78 347.16

1+07 8<sup>2</sup> Rt. = (W)

1+01 8<sup>6</sup> Lt. = Pole # A4121

0+99<sup>5</sup> 9<sup>2</sup> Rt. =  $\Phi$  3' wide Conc. Walk

0+99 7<sup>5</sup> Lt. = (W)

347.94

112

~~349.33~~  
442  
20<sup>3</sup>  
Floor

~~347.6~~  
6.2  
20

~~348.1~~  
5.7  
10

~~348.2~~  
5.6

~~348.3~~  
5.5  
10

~~348.3~~  
5.5  
20

~~346.9~~  
6.9  
10

~~347.4~~  
6.4

~~347.4~~  
6.4  
10

~~347.37~~  
6.38  
9.9

~~347.66~~  
6.09  
30

~~348.3~~  
5.5  
34  
0.2  
Floor

~~347.37~~  
6.38  
9.9

~~347.66~~  
6.09  
20

353.75

~~347.17~~  
0.77  
9.8  
 $\Phi$  walk

347.94

Alley BIK 29

Not get rod on floor.

floor elev. shown may be  $\pm 0.05$  corr

16' Rt. =  $\pm$  Sing Bar. Conc. Floor.

2+18 14<sup>2</sup> Lt. =  $\pm$  8' wide Rough Conc. Apron

2+10 9<sup>2</sup> Rt. = (W)

2+09 10<sup>5</sup> Rt. = End wire fence

2+06 9<sup>8</sup> Lt. = (W)

2+02 17<sup>2</sup> Lt. = N.E. Cor. House

2+01 8<sup>5</sup> Lt. = Pole # A 41A1

17<sup>2</sup> =  $\Delta$  in house

1+94 10<sup>3</sup> Lt. = N.E. Cor. room. Jog in house

10<sup>8</sup> Lt. = S.E. Cor. Main House

1+79 7<sup>8</sup> Lt. = End Conc. slab.

1+77 12<sup>2</sup> Lt. =  $\pm$  door way to house

9<sup>3</sup> Lt. to 10<sup>2</sup> Lt. = 1' Jog in slab. <sup>1871</sup><sub>P.22</sub>

10<sup>2</sup> Rt. = start light wire fence.

1+75 10' Lt. = End Cyclone wire fence

walk + trash can platform.

1+73 7<sup>5</sup> Lt. = start Conc. Slab. = Combined

353.75

349.3  
4.5  
17

349.5  
4.3  
10

349.6  
4.2

349.7  
4.1  
10

350.0  
3.8  
14.3  
Apron

350.5  
3.60  
7.6  
Bar.  
Floor

346.5  
5.2  
10.8  
End slab

346.91  
4.84  
10.8  
slab

346.95  
4.82  
7.8  
slab

348.5  
5.2  
7.2  
slab

348.5  
5.2

349.0  
4.8  
10

350.0

3.8

12  
in doorway

348.86

4.87  
10.8  
on walk

348.89

4.86  
9.2  
walk

348.90

4.85  
7.2  
walk

348.5

5.2  
10  
End

348.86

4.89  
9.2  
S.W. Cor

348.85

4.90  
7.5  
S.E. Cor

348.5

5.3  
7.2

348.6

5.2  
10

348.8

5.0  
10

349.0

4.8  
2.0

353.75

## Alley BIK 29

♀

4

2+1	11 <sup>2</sup> Lt. = start 12th & wire fence					
	11 <sup>2</sup> Lt = End board shed					
2+10	3+25 11 <sup>2</sup> Lt. = start chicken wire fence	$\frac{2.2}{20}$	$\frac{2.2}{10}$	2.3	$\frac{2.6}{7}$	$\frac{2.5}{10}$
2+0	3+24 9 <sup>6</sup> Lt. = End woven wire fence.				$\frac{2.1}{15}$	$\frac{2.7}{25}$
	Also = start board shed.					
2+0	3+15 11 <sup>4</sup> Rt. End same No good fence					
2+0						
2+0	Pence. - No good.					
2+0	3+01 11 <sup>4</sup> Rt start board & wire					
	3+00 9 <sup>2</sup> Rt. = (W)					
	2+96 9 <sup>2</sup> Lt. = Pole # 4149 (tag gone)					
1+9	2+94 8 <sup>2</sup> Lt. = (W)					
	2+93 18' Rt. = ♀ double Bar. dirt floor.	$\frac{2.9}{14}$	$\frac{2.7}{10}$	2.5	$\frac{2.7}{10}$	$\frac{2.6}{18}$
						♀ doorway
1+7	2+86 8 <sup>4</sup> Lt. = Ctr. 2' Diam. Pepper tree					
	2+79 10 <sup>6</sup> Lt. = start woven wire fence.					
	2+77 13 <sup>6</sup> Rt. = ♀ 2' wide conc. walk.					
					$\frac{2.40}{13.5}$	$\frac{2.53}{30}$
					walk	walk
1+7	2+75 10 <sup>1</sup> Lt. = End picket fence.					
	2+56 9 <sup>4</sup> Lt. = (W)					
	2+50	$\frac{3.7}{10}$		3.7	$\frac{3.5}{10}$	
1+7	2+48 10 Rt. = (W)					
	2+34 10 <sup>1</sup> Lt. = Start picket fence					
1+7	2+20 17 <sup>6</sup> Lt. = ♀ Sing. Bar. dirt floor	$\frac{4.5}{17.5}$				

353.75

353.75

4+92 10' Lt. = End Conc. block wall

4+76 wall on poured Conc. footing  
10 Lt. = start 6" wide Conc. block

4+50

4+24 10' Lt. = End wire fence.

4+19 9' Lt. = deadman

4+10

4+09 9' Lt. = (W)

T.P. 1/2 Dist. 0.39 349.63 4.51 349.24 B.M. # 7  
4+02

3+97 9' Lt. = Pole # PA. 4171

3+70

3+54 9' Lt. = (W)

3+41 11' Rt. = End path & wire fence  
353.75

344.2 5.4 10 Top wall	344.1 8.5 10 Base wall	344.4 8.2 10 Ord	340.6 9.0	340.0 7.6 10
--------------------------------	---------------------------------	---------------------------	--------------	--------------------

344.3 5.3 10 Top wall	342.6 7.0 10 Base wall	343.2 6.4 10 Ord	342.2 7.4	342.0 7.6 10
--------------------------------	---------------------------------	---------------------------	--------------	--------------------

347.7 1.9 30	344.2 3.4 10	344.2 7.1 5	345.0 4.6	344.7 4.9 10	344.1 5.5 17	340.6 9.0 30
--------------------	--------------------	-------------------	--------------	--------------------	--------------------	--------------------

350.3 +0.7 20	349.8 +0.2 12	349.4 0.2 10	348.6 1.0	348.3 1.5 10	345.7 3.9 30
---------------------	---------------------	--------------------	--------------	--------------------	--------------------

349.63

351.4 2.4 25	351.1 2.7 10	350.9 2.9	350.5 3.3 10	351.6 2.2 14	349.7 5.1 30
--------------------	--------------------	--------------	--------------------	--------------------	--------------------

353.75



Alley Bk. 29

T.P. 0.38 337.15 12.86 336.77

5+29 10' Lt. = start Conc. block wall

5+27<sup>E</sup> 10' Lt. = <sup>walls, Conc. step,</sup> 3' wide gate way between

5+26 10' Lt. = End Conc. block wall

5+10 9' Lt. = start Conc. block wall

5+08<sup>A</sup> 10<sup>E</sup> Lt. = End Conc. Apron to

5+04 11<sup>E</sup> Lt. = (W)

4+92<sup>E</sup> 10<sup>E</sup> Lt. = start Conc. Apron

349.63

6  
6

341.2  
8.4  
10  
top wall

335.7  
13.9  
10  
Base wall

337.8  
11.8  
10  
Ord

336.2  
13.1

335.1  
14.5  
10

338.5  
11.1  
10  
top step

337.5  
12.1  
10  
Base step

338.1  
11.5  
10  
Ord.

341.1  
8.5  
10  
top wall

338.2  
11.4  
10  
Base wall

338.3  
14.3  
10  
Ord.

336.5  
13.1

335.5  
17.1  
10

341.8  
7.8  
10  
top of wall

339.6  
10.0  
9.9  
Base wall

340.1  
9.5  
9.2  
Ord

338.5  
11.1

337.6  
12.0  
10

341.35  
8.28  
1.42  
Gar. Floor

340.81  
8.82  
10.5  
Apron

340.5  
7.1  
10

338.7  
10.9

337.9  
11.7  
10

336.9  
12.7  
26  
Rim Canyon

333.2  
16.7  
40

341.43  
8.20  
1.45  
Gar. Floor

341.27  
8.36  
10.5  
Apron

349.63

4+67

$$\begin{array}{r} 332.2 \\ 5.9 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 332.1 \\ 5.1 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 331.0 \\ 6.2 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 330.8 \\ 6.4 \\ \hline \end{array}$$

$$\begin{array}{r} 329.8 \\ 7.4 \\ \hline 10 \end{array}$$

4+60

$$\begin{array}{r} 333.0 \\ 4.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 333.0 \\ 4.2 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 331.7 \\ 5.5 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 331.4 \\ 5.8 \\ \hline \end{array}$$

$$\begin{array}{r} 330.2 \\ 7.0 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 330.2 \\ 7.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 329.1 \\ 8.1 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 324.2 \\ 13.0 \\ \hline 35 \end{array}$$

5+59 11' Lt. = S.E. Cor porch

$$\begin{array}{r} 338.7 \\ +1.5 \\ \hline 11 \\ \text{Porch deck} \\ \text{Cornc.} \end{array}$$

$$\begin{array}{r} 332.2 \\ 5.0 \\ \hline 11 \\ \text{Base} \\ \text{footing} \end{array}$$

5+51 Cont.

$$\begin{array}{r} 329.2 \\ +2.0 \\ \hline 10.1 \\ \text{Tap wall} \end{array}$$

$$\begin{array}{r} 327.9 \\ 4.3 \\ \hline 10.1 \\ \text{Base} \\ \text{wall} \end{array}$$

5+51 10' Lt. = End Cornc. block wall.

$$\begin{array}{r} 334.4 \\ 2.8 \\ \hline 10 \\ \text{Grd} \end{array}$$

$$\begin{array}{r} 334.3 \\ 2.9 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 333.1 \\ 4.1 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 333.5 \\ 4.7 \\ \hline \end{array}$$

$$\begin{array}{r} 331.4 \\ 5.8 \\ \hline 10 \end{array}$$

5+39 6' Lt. = (W)

337.15

337.15

Alley BIK. 29

SE 7. B.M.  
07 2x2  
5.18442

8.19 328.96 B.M.#7

6+17<sup>AL</sup> =  $\phi$  Orange

5+96

5+94

5+79 11<sup>o</sup> Lt. = End Conc. Walk.

5+77<sup>AL</sup> = S-line Orange walk.

5+76<sup>2</sup> 8<sup>o</sup> Lt. = Sewer Clean out.

Also = Start N.4.S. Conc. walk  
of N.4.S. Conc. steps to house

5+74 10<sup>9</sup> Lt. = N.E. Cor. of bottom step

337.15

$\phi$

8<sup>9</sup>

330.3  
6.9  
60

329.4  
7.8

328.8  
8.4  
50

328.3  
8.9  
100

330.0  
7.2  
70

329.4  
7.8  
35

329.1  
8.1  
10

328.8  
8.4

328.6  
8.6  
10

328.4  
9.0  
50

327.6  
9.6  
100

330.4  
6.8  
70

329.8  
7.4  
35

329.6  
7.6  
10

329.4  
7.8

329.0  
8.2  
10

328.6  
8.6  
50

328.1  
9.1  
100

330.24  
6.9  
11<sup>o</sup>  
walk

330.1  
7.1  
10

330.1  
7.1

329.6  
7.6  
10

328.2  
9.0  
50

330.28  
6.87  
103

330.0  
7.2  
103

330.3  
6.9  
103

330.3  
6.9  
10

330.3  
6.9

329.5  
7.7  
10

on Base  
walk Conc.

337.15

Curb Levels <sup>COLIMA</sup> Electric Ave to

La Jolla Measa Dr

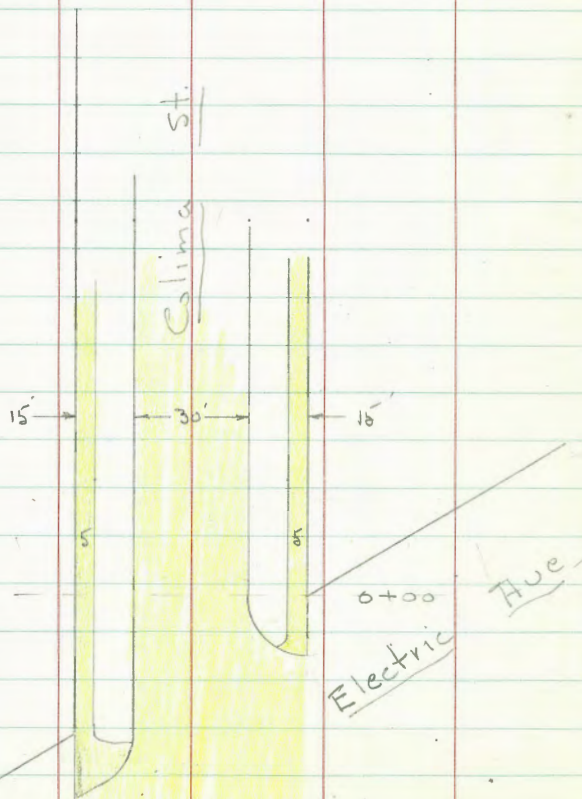
Sketch Below shows Beginning +

Typical cb. + walk location - See Plan.

2237-L for Details - Construction follows

Plan, Except for Alley Returns, put in with

S Rad. instead of Sharp ang. shown



# 2666

W.O. 25001

INDEXED

W.K.

SEP 7 1948

8-27-48

Osborne  
Hardin  
Decker  
Hatch

9  
9

Notes Reduced  
9-15-48  
H. Remington

# Curb Levels along Colima

0+50

0+00 = P.C. S.E. Ret. + opp. S.E. Prop. Cor.

± of Ret.

0-15 = S. end S.E. Ret. = S.L. Colima

0-35.1 = P.C. N.E. Ret.

± of Ret.

0-52.7 = Nly. end of N.E. Ret.

Req. Reg. Sections

S. end = S.L. Colima

± = Mid point

P.C. = wly. end.

S.w. Ret.

P.C. = w. end.

± = Mid. point

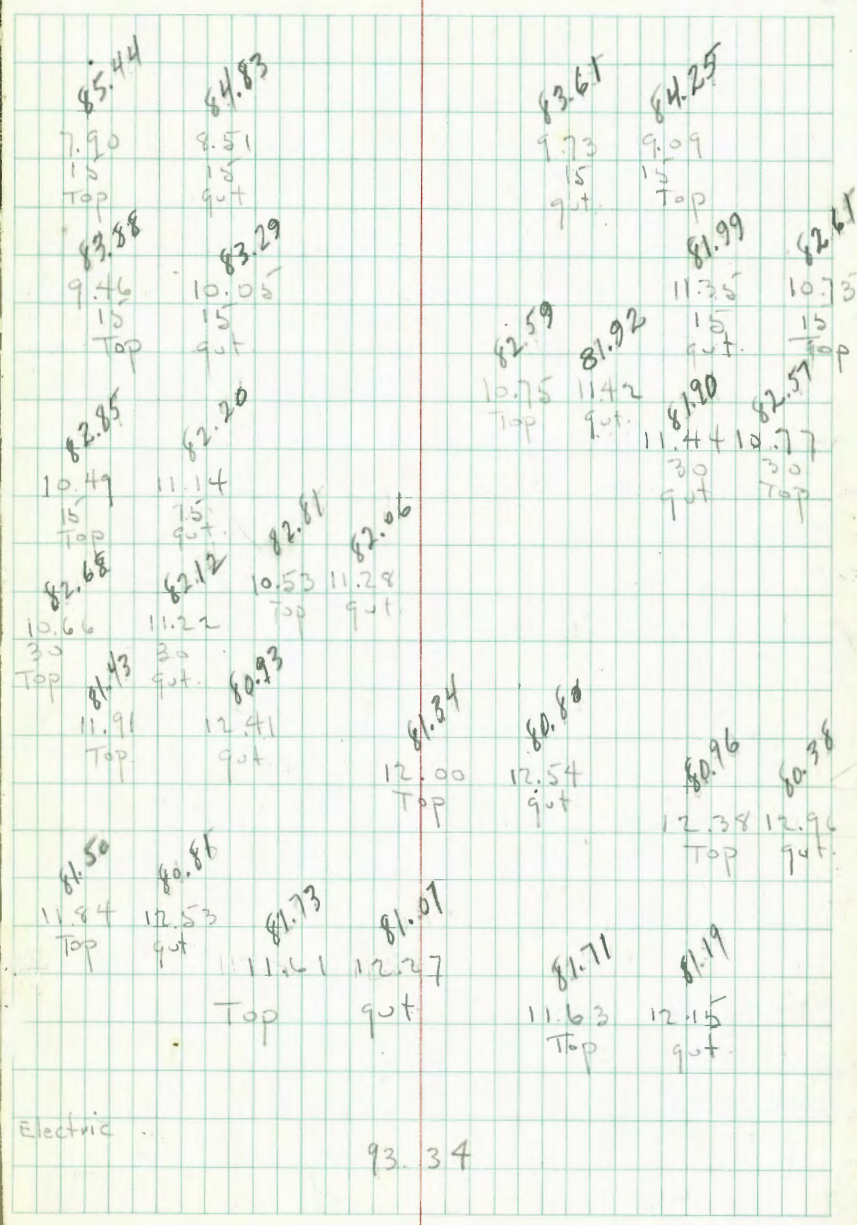
Nly. end = N.L. Colima

Rods on NW. Ret. Colima + Electric

	10.27	93.34	1.10	83.07	NE. Ret.
B.M.	6.19	84.17		77.98	SW B.P. Colima La Jolla Blvd

Lt. 15 - N. ob. ±

Rt. 15 = 10



Electric 93.34

N. end = N.L.

± Ret.

3+02 = P.C. = M.E. Ret.

S. end = S.L.

± Ret.

2+67.6 = P.C. S.W. Ret. Beaumont

N. end = N.L.

± Ret.

2+32.3 = P.C. N.W. Ret. Beaumont.

2+00

1+50

N. end Ret. = N.L.

1+19 = P.C. Alley Ret. on Lt. - 5' Rad.

1+00

N. end Ret. = N.L.

0+89.5 = P.C. Alley Ret. on Lt.

Note - 5' Radius on Alley Returns - Plan shows sharp angle

92.54

0.80  
30  
Top

91.53

1.81  
30  
Top

91.53

1.81  
30  
Top

91.91

1.43  
30  
Cut.

90.99

2.25  
30  
Cut.

91.30

2.04  
Top

90.05

3.29  
15  
Top

87.42

5.92  
30  
Top

86.32

7.02  
15  
in cut.

86.69

6.65  
5  
Top

92.76 Lt

0.58  
Top

91.30

2.04  
Top

90.05

3.29  
15  
Top

87.42

5.92  
30  
Top

86.32

7.02  
15  
in cut.

86.69

6.65  
5  
Top

92.02

1.32  
Cut.

91.05

2.29  
15  
Top

89.51

3.83  
15  
Cut.

88.51

4.82  
15  
Top

87.59

5.75  
15  
Top

86.92

6.42  
30  
Top

85.98

7.36  
5  
Cut.

91.38

0.30  
15  
Top

90.41

2.93  
15  
Cut.

89.51

3.83  
15  
Cut.

88.51

4.82  
15  
Top

87.59

5.75  
15  
Top

86.92

6.42  
30  
Top

85.98

7.36  
5  
Cut.

±

Ret.

11

90.86

2.46  
15  
Cut.

89.68

3.66  
15  
Cut.

88.68

4.66  
15  
Cut.

87.86

5.48  
15  
Cut.

86.94

6.40  
15  
Cut.

86.76

6.58  
30  
Cut.

85.98

7.36  
5  
Cut.

91.15

2.19  
Cut.

89.68

3.66  
15  
Cut.

88.68

4.66  
15  
Cut.

87.86

5.48  
15  
Cut.

86.94

6.40  
15  
Cut.

86.76

6.58  
30  
Cut.

85.98

7.36  
5  
Cut.

91.54

1.80  
Cut.

90.35

2.99  
15  
Top

88.68

4.66  
15  
Cut.

87.98

6.36  
15  
Cut.

86.94

6.40  
15  
Cut.

86.76

6.58  
30  
Cut.

85.98

7.36  
5  
Cut.

91.87

1.47  
Top

90.35

2.99  
15  
Top

88.68

4.66  
15  
Cut.

87.98

6.36  
15  
Cut.

86.94

6.40  
15  
Cut.

86.76

6.58  
30  
Cut.

85.98

7.36  
5  
Cut.

91.54

1.80  
Cut.

91.30

2.04  
Top

90.05

3.29  
15  
Top

88.51

4.82  
15  
Top

87.59

5.75  
15  
Top

86.92

6.42  
30  
Top

85.98

7.36  
5  
Cut.

92.16

1.18  
Top

90.67

2.67  
Cut.

89.51

3.83  
15  
Cut.

88.51

4.82  
15  
Top

87.59

5.75  
15  
Top

86.92

6.42  
30  
Top

85.98

7.36  
5  
Cut.

93.34

5+50

5+00

N. end Ret. = N.L.

4+56.1 = P.C. Alley Ret. on Lt. = 5' Rad.

4+50

N. end Ret. = N.L.

4+27.4 = P.C. Alley Ret. on Lt. = 5' Rad.

4+00

3+50

S. end Ret. = S.L.

⊕ Ret.

3+37.2 = P.C. of S.E. Ret.

T.P. 12.83 105.91 0.26 93.09

103.65 Lt. 22.5 15 Top  
 103.04 2.87 15 Top  
 102.45 3.46 15 fut.  
 Rt 103.06 2.85 15 Top  
 100.84 5.71 15 fut.  
 100.84 5.11 15 Top  
 99.35 6.53 30 Top  
 98.89 7.02 30 fut.  
 101.48 4.43 15 Top  
 99.66 6.25 15 Top  
 99.01 6.90 15 fut.  
 96.72 7.19 15 fut.  
 97.95 7.93 15 fut.  
 98.60 7.31 15 Top  
 98.57 7.34 30 Top  
 98.43 7.48 30 fut.  
 96.36 7.55 15 Top  
 97.76 8.15 15 fut.  
 97.19 8.72 15 Top  
 96.56 9.35 15 fut.  
 95.73 10.18 15 fut.  
 96.36 9.55 15 Top  
 95.10 10.81 15 Top  
 94.43 11.48 15 fut.  
 93.42 12.49 15 fut.  
 94.13 11.78 15 Top  
 92.91 13.00 15 fut.  
 93.55 12.36 15 Top  
 92.55 13.36 9 fut.  
 95.25 12.66 15 Top  
 13.40 12.80 9 fut. Top  
 92.51 93.11

105.91

N. end Ret. = N.L.

7+64.4 = P.C. of Rad. Alley Ret. on Lt.

+ 50

7+00

S. end Ret. = S.L.

± Ret.

6+74.6 = P.C. of S.E. Ret. - Waverly

N. end Ret. = N.L.

± Ret.

6+39.3 = P.C. of NE. Ret. - Waverly

S. end Ret. = S.L.

± Ret.

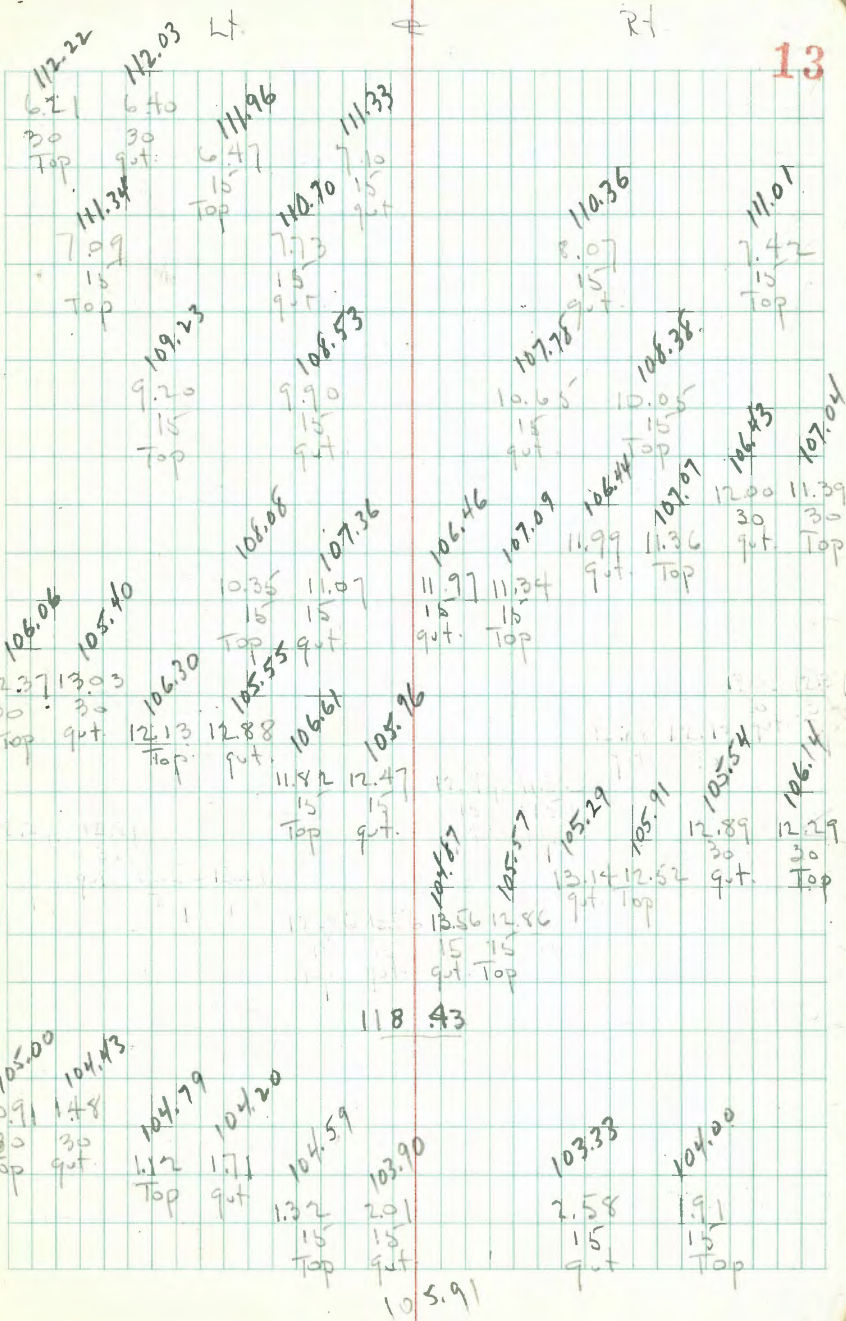
6+04.7 = P.C. of SW. Ret. Waverly

T.P. 12.60 118.43 0.08 105.83

N. end Ret. = N.L.

± Ret.

5+69.8 = P.C. of N.W. Ret. - Waverly Ave





S. end = S.L.

± Ret.

10+15.1 = P.C. S.E. Ret. - Bellevue

N. end = N.L.

± Ret.

9+75.9 = P.C. N.E. Ret. - Bellevue

S. end = S.L.

± Ret.

9+41.8 = P.C. S.W. Ret. - Bellevue

N. end Ret. = N.L.

± Ret.

9+06.6 = P.C. of NW. Ret. - Bellevue

T.P. 12.42 130.67 0.18 118.25

8+50

8+00

S. end Ret. = N.L.

7+93.4 = P.C. of 5' Rad Alley Ret. on Lt.

Lt. †

120.51 10.16 30 Top	119.91 10.86 30 9.4 Top	120.72 9.95 Top	124.55 6.12 15 Top	123.99 6.79 15 9.4 Top	122.77 7.90 9.4 Top	123.41 7.26 Top	122.11 8.56 9.4 Top	122.74 7.93 Top	121.99 8.68 30 9.4 Top	122.64 9.03 30 Top
118.54 12.11 30 Top	117.96 12.71 30 9.4 Top	118.31 12.36 Top	117.74 12.93 9.4 Top	118.11 12.56 15 Top	117.51 13.16 15 9.4 Top	120.34 10.33 15 9.4 Top	121.01 9.66 15 Top	120.67 10.00 9.4 Top	121.23 9.44 Top	120.93 9.74 9.4 Top
115.62 2.81 15 Top	115.05 3.38 15 9.4 Top	130.67	118.62 12.05 15 9.4 Top	119.27 11.40 15 Top	115.58 2.85 15 9.4 Top	116.26 2.17 15 Top	112.97 5.46 15 9.4 Top	113.61 4.82 15 Top		
112.87 5.56 30 Top	112.42 6.01 30 9.4 Top	113.13 5.30 15 Top	112.81 5.62 15 9.4 Top	112.54 5.89 15 9.4 Top	118.43					

N. end - NL.

Ret

12+44.4 = PC. NW. Ret Taft

T.P. 13.18 156.24 0.14 143.06

12+00

11+50

N. end Ret - NL.

11+30.1 = PC. 5' Rad. Alley Ret. on Lt.

N. end Ret - NL.

11+01.6 = PC 5' Rad. Alley Ret. on Lt.

11+00

T.P. 12.69 143.20 0.16 130.51

10+50

15

145.50 10.74 Top	144.93 11.31 30 put	145.43 12.81 Top	144.80 11.44 put	145.04 11.70 15 Top	144.36 11.88 15 put	143.32 12.92 15 put	143.98 12.26 15 Top
141.13 2.07 15 Top	140.45 2.75 15 put	136.69 6.51 15	136.07 7.13 15 put	139.40 3.80 15 put	140.04 3.18 15 Top	134.95 8.25 15 put	135.51 7.69 15 Top
134.04 9.16 30 Top	133.62 9.58 30 put	132.81 8.39 15 Top	132.29 8.91 15 put	132.52 10.68 30 put	132.28 10.92 15 Top	131.75 11.45 15 put	
132.14 11.06 15 Top	131.57 11.63 15 put	130.44 12.76 15 put	130.97 12.23 15 Top	127.70 2.97 15 Top	127.01 3.66 15 put	143.20 12.596 4.71 15 put	126.47 4.20 15 Top
						130.67	

N. end Ret. = N.L.

14+67.8 = P.C. of S Rad. Alley Ret. on Lt.

S. end = S.L. - Note: Ret. Broken down Here  
= end of cb. on South

14+54.0 = P.C. of S.W. Ret. Taft =

T.P. 9.91 165.24 0.91 155.33

N. End = N.L.

14+38.8 = P.C. S Rad Alley Ret. on Lt.

Check BM - NE. Taft 8.81 147.43 147.52 = Book

14+00 See Next page

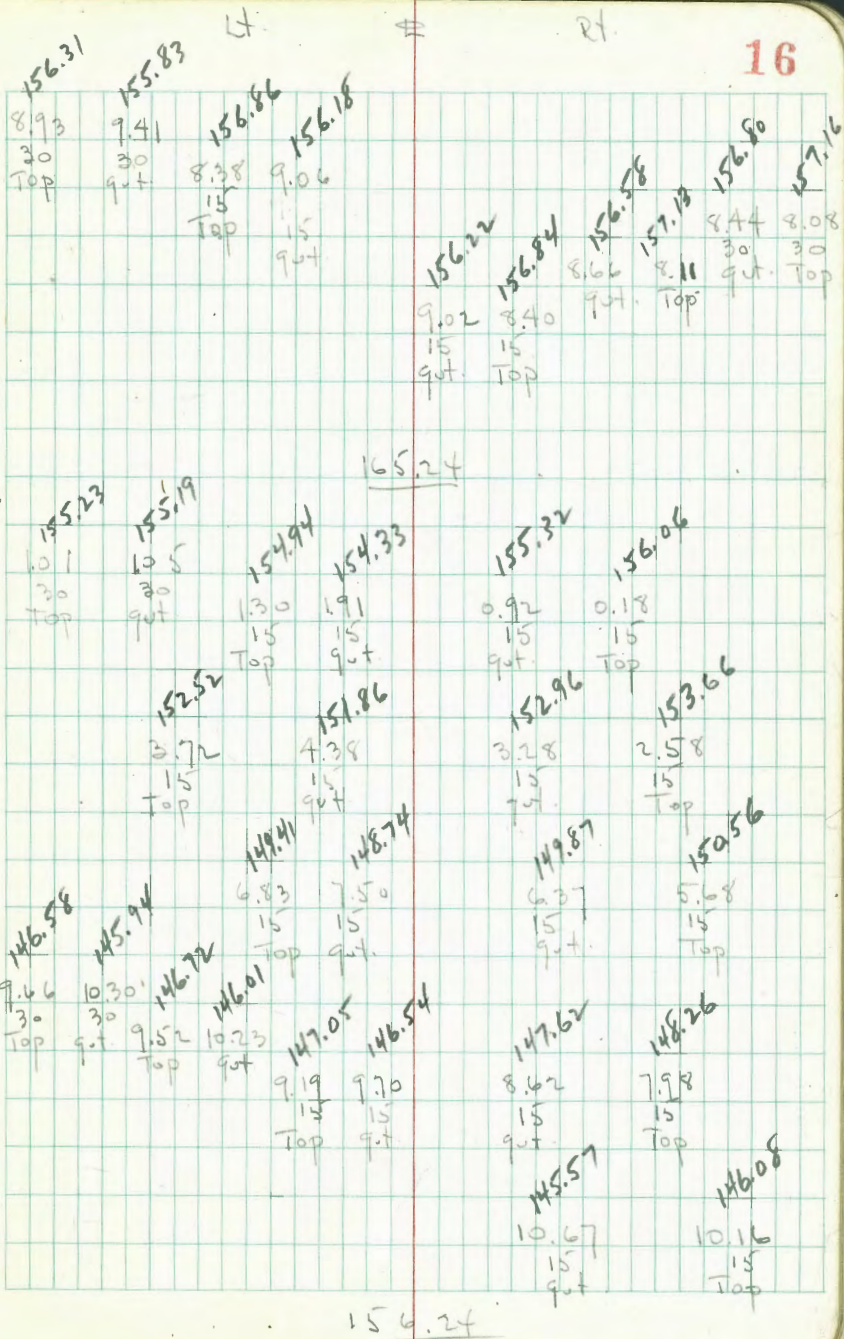
13+50

N. end = N.L.

Ret.

13+13.6 = P.C. of N.E. Ret. - Taft.

12+79.6 = Mid Point of Int.



.09 diff. Between B.M.'s

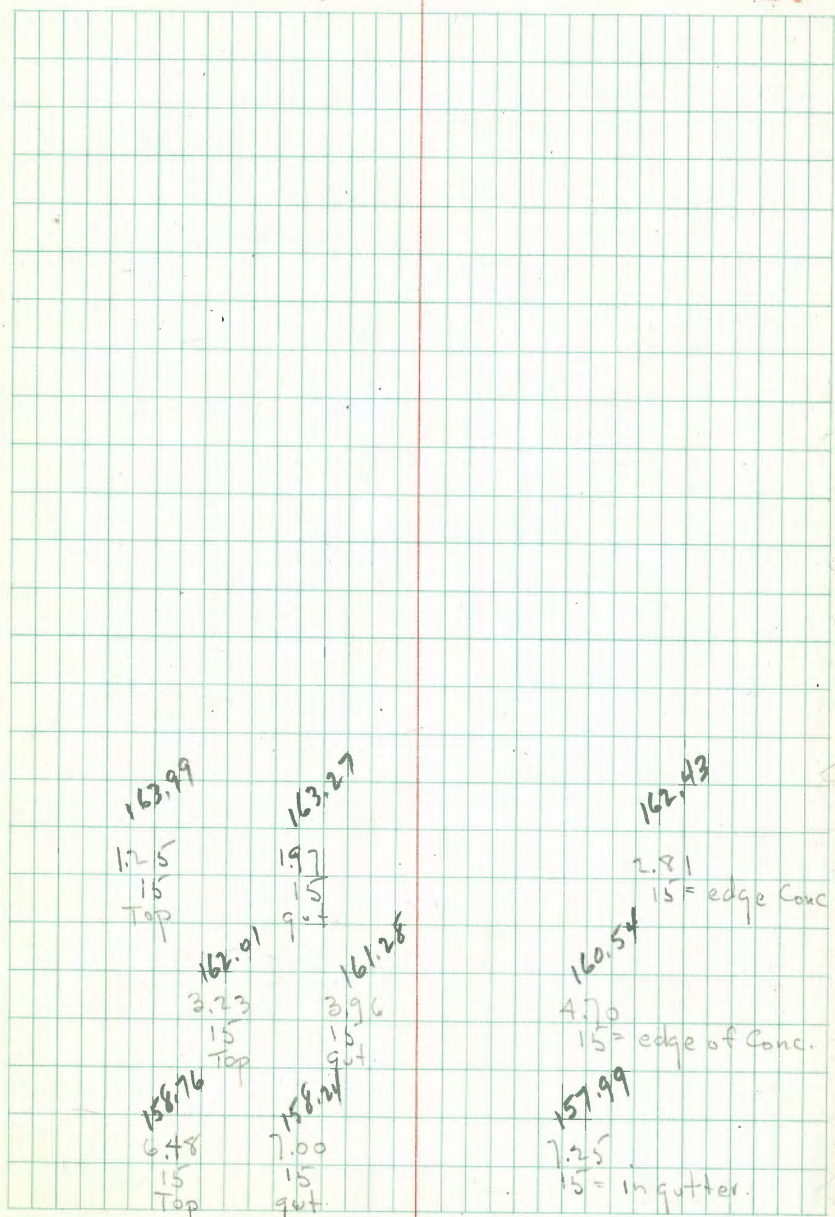
Starting B.M.		5.13	77.98	77.98
0.04	83.11	19.22	83.07	
0.23	93.29	13.28	93.06	
0.53	106.34	12.45	105.81	
0.03	118.26	12.52	118.23	
0.26	130.75	12.57	130.49	
0.02	143.06	13.19	143.04	
T.P.	0.90	156.23	9.91	155.33

Rest of Ret. is Broken out.

15+81.2 = P.C. of N.W. Ret. - La Jolla Mesa Dr  
(Linda Rosa on Plan)

15+50

15+00 - curb and walk on N. only



Prop. Sewer - Pressure Lines

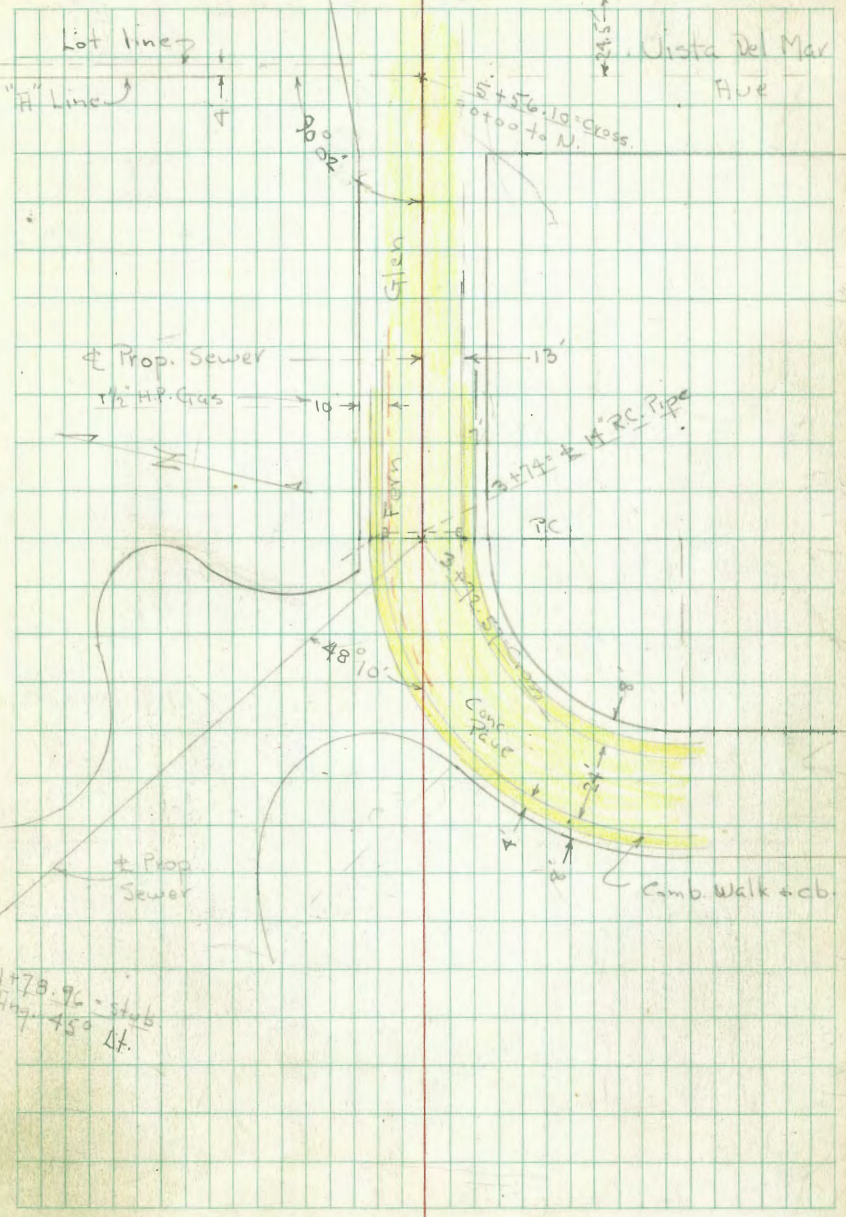
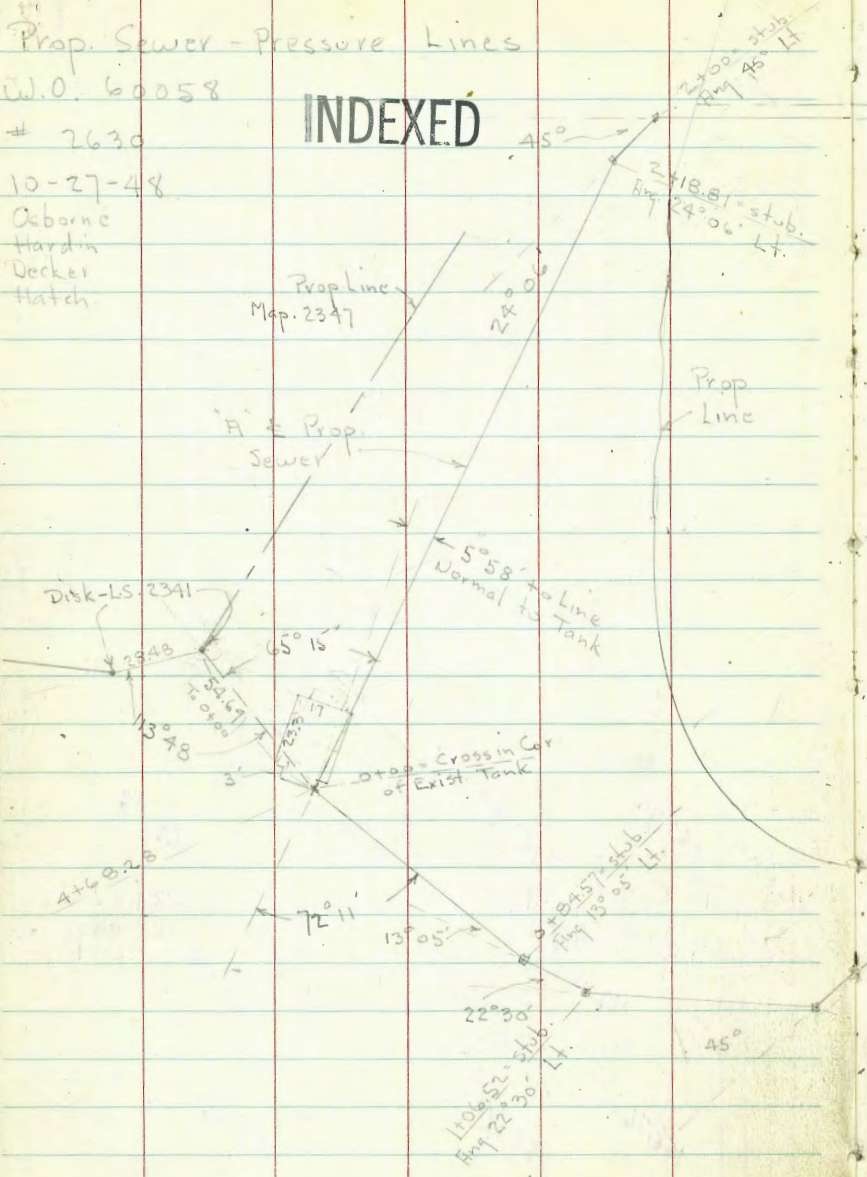
W.O. 60058

# 2630

10-27-48

Osborne  
Hardin  
Decker  
Hatch

INDEXED



La Jolla Blvd.

Water

16+56.21  
Htg 44° 57' Rt

16+12  
Htg 45° Rt

6" Sewer

M.H.

Fern Glen

11+98.03=Stn  
Htg 45° Lt

Monte Vista Ave.

M.H.

Exist. C Sewer

10+35

11+136.33  
Htg 45° Rt

Prop. Sewer

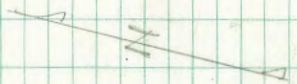
Westbourne St.

26'

2.6" Gas

19+11.54  
Htg 27° 30' Lt

20+10.28 Ed. Nail  
C 1.5" Gas Gate Box



Levels along  $\pm$  of Prop. Pressure Line  
 Sewer - from Tank along Ocean to Westbourne  
 + La Jolla Blvd.

INDEXED

BM.	0.64	60.16		59.52	sw. B.P. Belvedere + Monte Vista 1370 - P. 42
	0.58	47.56	13.18	46.98	
	0.42	34.74	13.24	34.32	
	0.01	22.30	12.45	22.29	
	6.33	17.14	11.49	10.81	
Show in Top B.M. on Disk 2.14 E. of Disk			10.14	7.00	
0+00 = Cross on Cor. of Conc. Tank					
0+00 = Top			12.48	04.66	
= Sand			15.7	1.4	
0+30 = $\pm$			16.5	.6	
30' Lt.			7.9	9.2	
0+47 = 14.8' Lt. = $\pm$ M.H.					
0+50 = $\pm$			13.3	3.8	
15' Lt.			7.7	9.4	
30' Lt.			3.5	13.6	
0+84.57 = Ang. 13° 05' Lt.			12.61	3.53	on Stub.
1+06.52 = Ang. 22° 30' Lt.			13.17	3.97	on Stub.
12' - Lt. - on split of Ang.			11.2	6.0	
30' Lt.			4.3	12.8	
1+16.5 = $\pm$ Sewer - Conc. Cased					
$\pm$ = Top Conc. Cover.			12.39	4.75	

1+39.8 - 18 Rt = M.H.				
1+45 = $\pm$	10.4	6.7		
20' Lt. = in Draw	7.6	9.5		
1+59 = $\pm$ Sewer - Conc. Cover.				
$\pm$ on Conc	10.54	6.60		
1+78.96 = Ang. 45° Lt.				
$\pm$ - on Stub.	9.12	8.02		
40' Lt. - on split	+2.1	19.2		
2+00 = $\pm$	7.5	9.6		
2+15	6.4	10.7		
+23	8.7	8.4		
+30	6.2	10.9		
2+50	4.9	12.2		
15' Lt.	2.2	14.9		
30' Lt.	4.1	13.0		
50' Lt. = Bank	+3.2	20.3		
T.P. 12.02 = 28.43	0.73	16.41		
3+00 = $\pm$	11.1	17.3		
20 Rt.	6.5	21.9		
25 Lt.	12.1	7.3		
50 Lt. = Top Bank	8.1	20.3		
3+25	9.5	18.9		
25 Lt.	9.6	18.8		

		29.45		
3+42.9 - 6.8' Lt = M.H.				
T.P.	12.15	39.57	1.01	27.42
3+45 =		11.6	28.0	
3+52 = Edge of Walk		10.07	28.50	
3+57 = c.b. face - Top		9.93	29.64	
- Conc. Pavc - gut		10.61	28.96	
3+72.57 = Ang. 48.10' Lt.		9.86	29.71	on Cross
3+74 = ± of 14" RC. Pipe Culvert Bet. 15' opening curb Inlets.				
±		9.97	29.70	
12' Lt = F.L. Box of Inlet		15.35	24.22	
12' Rt = F.L. Box of Inlet		14.45	25.12	
4+00		8.54	31.03	
4+02.5 5.3' Lt = ± M.H.				
4+50		6.28	33.29	
5+00		4.04	35.53	
5+50		1.89	37.68	
5+56.10 = 0+00 of "A" Alternate line to N.				
		1.60	37.97	on Cross
5+60.4 = 19' Lt = M.H.				
5+87.8 = end Conc. + Beg AC Pavc		0.69	38.89	
T.P.	13.05	51.95	0.67	38.90

21

		51.95		
6+00		12.49	39.46	
+50		9.98	40.97	
7+00		7.85	44.10	
+50		5.90	46.05	
8+00		4.39	47.56	
+50		3.57	48.38	
9+00		4.14	47.81	
+50		5.07	46.88	
10+00		5.57	46.38	
10+15 = Approx. ± 6" Sewer				See Sketch - get FL. From Plan
10+35 = Ang. 45° Rt.		5.57	46.38	
T.P.	12.68	59.54	5.11	46.84
10+60		12.09	47.43	
11+00 (Poor Cond)		9.62	49.90	
11+06.9 = edge AC Pavc		9.61	49.91	
11+50		4.8	54.7	
11+98.03 = Ang. 45° Lt.		1.41	58.11	on Step
T.P.	5.84	63.95	1.41	58.11
11+62.8 = ± ± 6" Sewer along Fern Glen				
52.6 W. = M.H.		16.64	47.31	F.L.
along Sewer Line				



12+45	6.5	57.4
12+85	3.0	61.0
13+00	2.5	61.5
13+50	0.5	63.5

T.P. 11.29 74.80 0.44 63.51

13+76 - 26' Lt. = ~~to~~ M.H. Sewer 23.96 50.84 F.L.

14+00 10.1 64.7

+50 8.5 66.3

15+00 7.0 67.8

+50 5.4 69.4

16+00 4.3 70.5

16+05.6 = edge A.C. Pave 4.30 70.50

16+12.47 = Ang. 45° Rt. 4.30 70.50 = on nail

16+31.2 = Cross Gas Line

16+50 3.17 71.13

~~16+63.3 = Cross Water Line - Line changed.~~

~~16+71.81 = Ang. 44° 57' Rt. 2.89 on nail~~

~~17+00 2.37 This Line is~~

~~+50 1.45 15' W. of E.L.~~

~~18+00 0.56~~

~~Void - See Next Page~~

T.P. 8.10 79.14 0.86 73.94

18+50 4.05

19+00 3.10

+50 2.29

20+00 1.17

Void.

19+87.9 = 4' x 4' Conc. St. Drain M.H.

F.L. Box 8.47

- 6' x 6' Water Gate M.H.

F.L. Box 8.26

20+12.55 = Fd. Nail 0.95

on nail

S.W. F.H. Belvedere

T.P. 5.69 82.85 1.98

77.14

16+50 = Same as opp. page

16+56.21 = Ang. 44° 57' Rt. 11.05 71.80 on nail

17+00 10.11 72.74

+50 9.08 73.77

18+00 8.17 74.68

+50 7.40 75.45

19+00 6.48 76.37

+50 5.71 77.14

19+71.54 Ang. 22° 30' Lt. 5.37 77.48 on nail

19+86.4 - 5.2 Lt. = ± 4' x 4' St Drain MH				
Flow line of Box		70.67	from opp.	Page
20+00.28 = Ang. 22° 30' Rt. 4.84		78.01	on nail	
20+02.3 - 2.5 ft. = ± 6' x 6' Water MH				
Flow line Box		70.78		
20+10.28 = Fd. Nail = Prop Sewer 4.68		78.17	on nail	
n.w. Westbourne + La Jolla Blvd. B.M. on B.P.		4.52	78.33	
T.P.	0.01	77.17	5.69	77.16
	3.14	67.66	12.65	64.52
check starting B.M.		8.14	59.52	59.52

Levels along  $\pm$  of Prop. Alternate  
Sewer Line from Vista Del Mar + Fern  
Glen to Septic Tank. - sketch - P. 18

0+00 = Cross = 5+56.10 on first line

0+00 2.10 40.07 37.97 - on Cross

0+15.5 = gut 2.70 37.34

" = Top cb 2.13 37.94

0+19.5 = edge walk 2.09 <sup>37.94</sup>

0+28 2.1 38.0 W.K.

**OCT 28 1948**

0+35 0.7 39.4

0+60 1.3 38.8

1+00 -  $\pm$  2.3 37.8

10' Lt. 2.0 38.1

10' Rt. 2.8 37.3

1+50 3.0 37.1

1+90 3.8 36.3

2+00 - Ang. = 45° Lt 5.58 34.49 on stub

10' Rt. on split 7.8 32.3

10' Lt. " " 4.5 35.6

2+18.81 - Ang 24° 06' Lt. 8.31 31.76 on stub

2+40 7.5 32.6

2+80 13.7 26.4

10' Lt. 13.2 26.9

10' Rt. 19.7 20.4

T.P. 0.67 27.64 13.10 26.97

24

27.64

3+20 9.5 18.1

3+60 14.1 13.5

4+00 14.6 13.0

T.P. 0.52 15.37 12.79 14.85

4+35 4.4 10.0

4+45 - Dirt 10.0 5.4

4+68.28 = 0+00 of First Line = Cor Tank.  
on Cross 10.71 04.66 = 04.66

Oct. 29, 1948  
B.F.H.

Survey to locate Limits of Prop.  
Easement Along Prop. Pressure Sewer  
Along Fern Glen Colony - See P. 18

W.O. 60058

49  
1-24-48

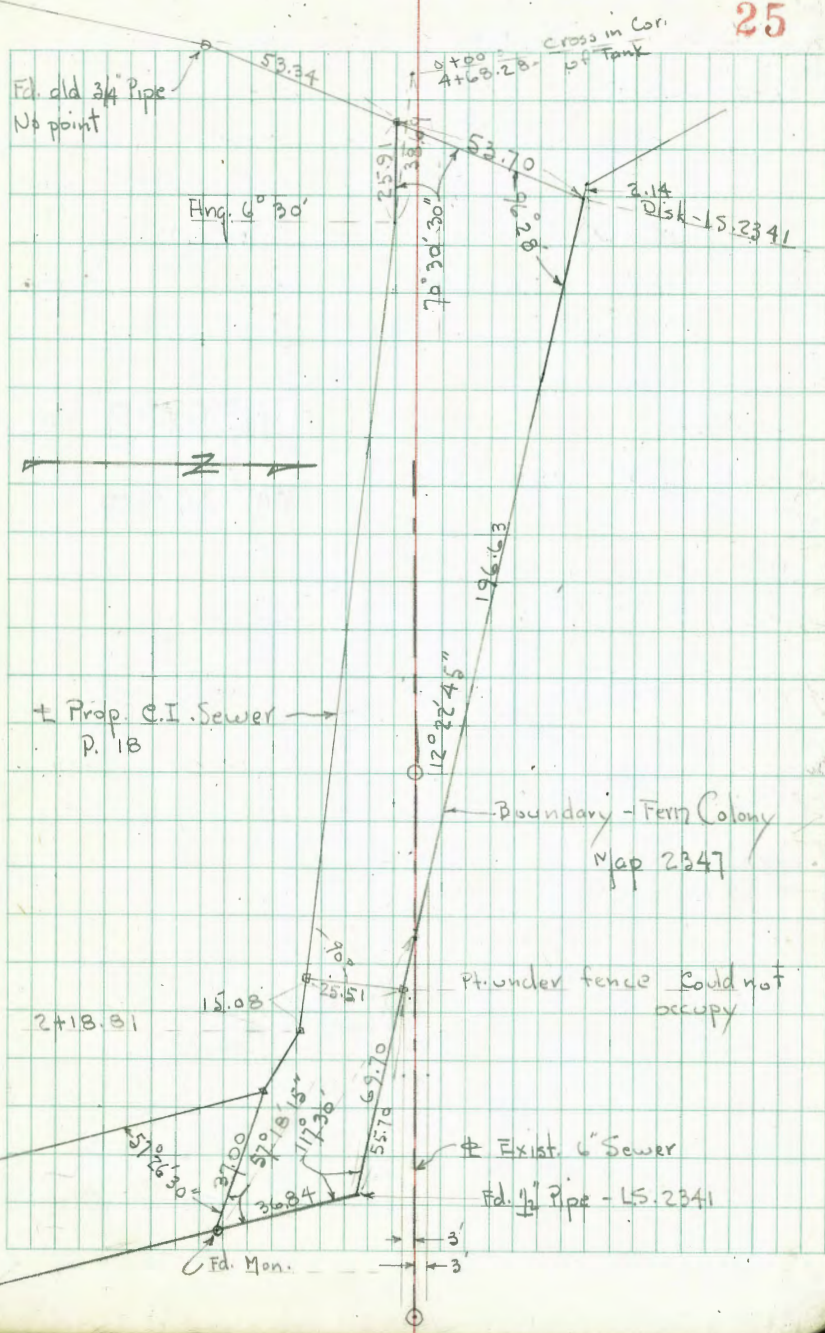
**INDEXED**  
WK  
JAN 26 1949

Osborne  
Hardin  
Bunch

Map 2347

3660-B

Survey A-986



Walker Johnson Pope Crainford  
 4-25-49 Location Existing Concrete Retaining  
 And Sea Wall, Along Hwy Lines  
 Lot 6, 7 Fern Glen Colony  
 for Purpose: To obtain Easement  
 Proposed  
 for Concrete Walk adjacent to  
 Existing Wall And Foot Bridge  
 from Existing Conc. Steps to Septic  
 Tank Near SWLY Cor. Lot 7

Cont. on P. 27

INDEXED

WK

MAY 26 1949

0+31.06 = A Pt.  $14^{\circ}30'28''$  (Wall 1.3' Lt.)

0+25 = 2.15' Lt. = Wall

0+20.3 = 2.97' Lt. = Wall

0+11 = 1.62' Lt. = Wall

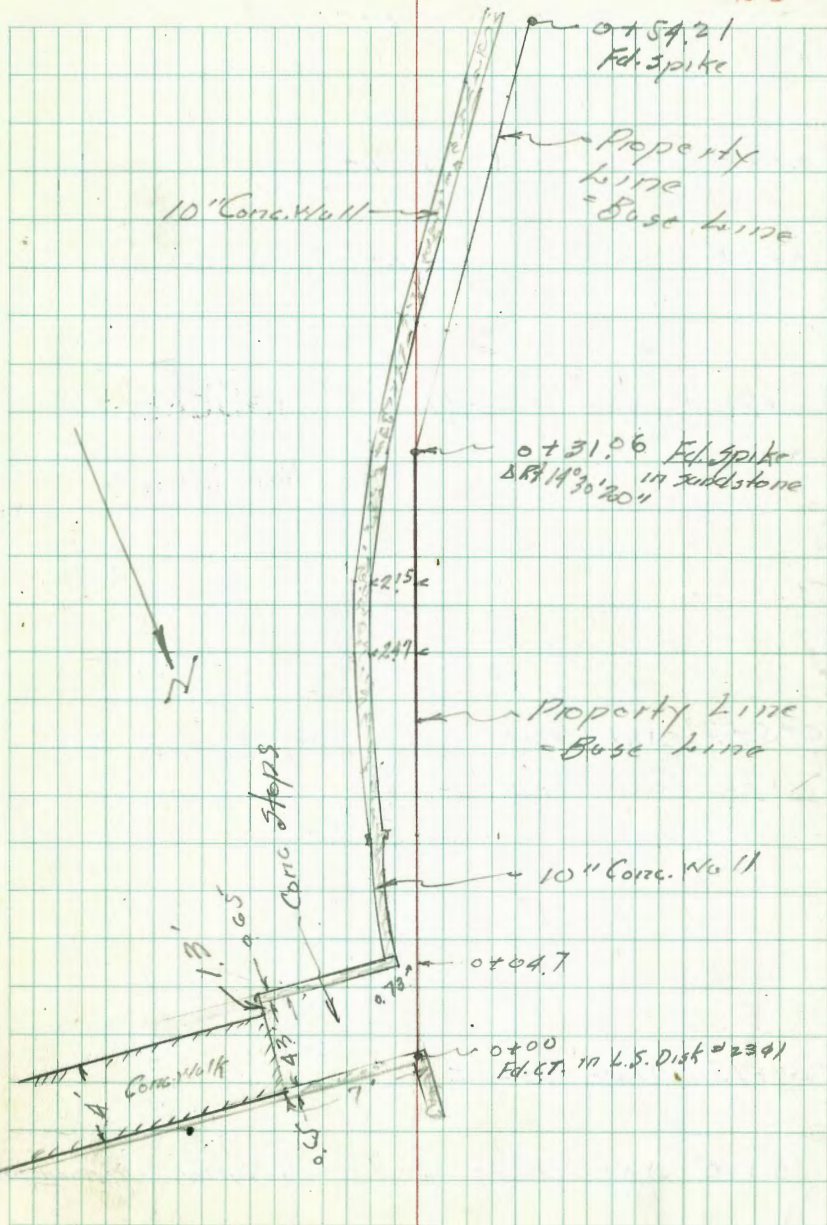
0+04.7 = 0.73' Lt. = Wall = cor. steps.

0+00.37 = Int. Wall to steps Wall = 0.15' Lt.

0+00 = Fd. Hd & Disk

all  
distances to wall  
are seaward side

26



0192 Wall = 1.78' Lt.

0183 Wall = 3.65' Lt.

0177 Wall = 4.98' Lt.

0170.4 Wall = 4.27'

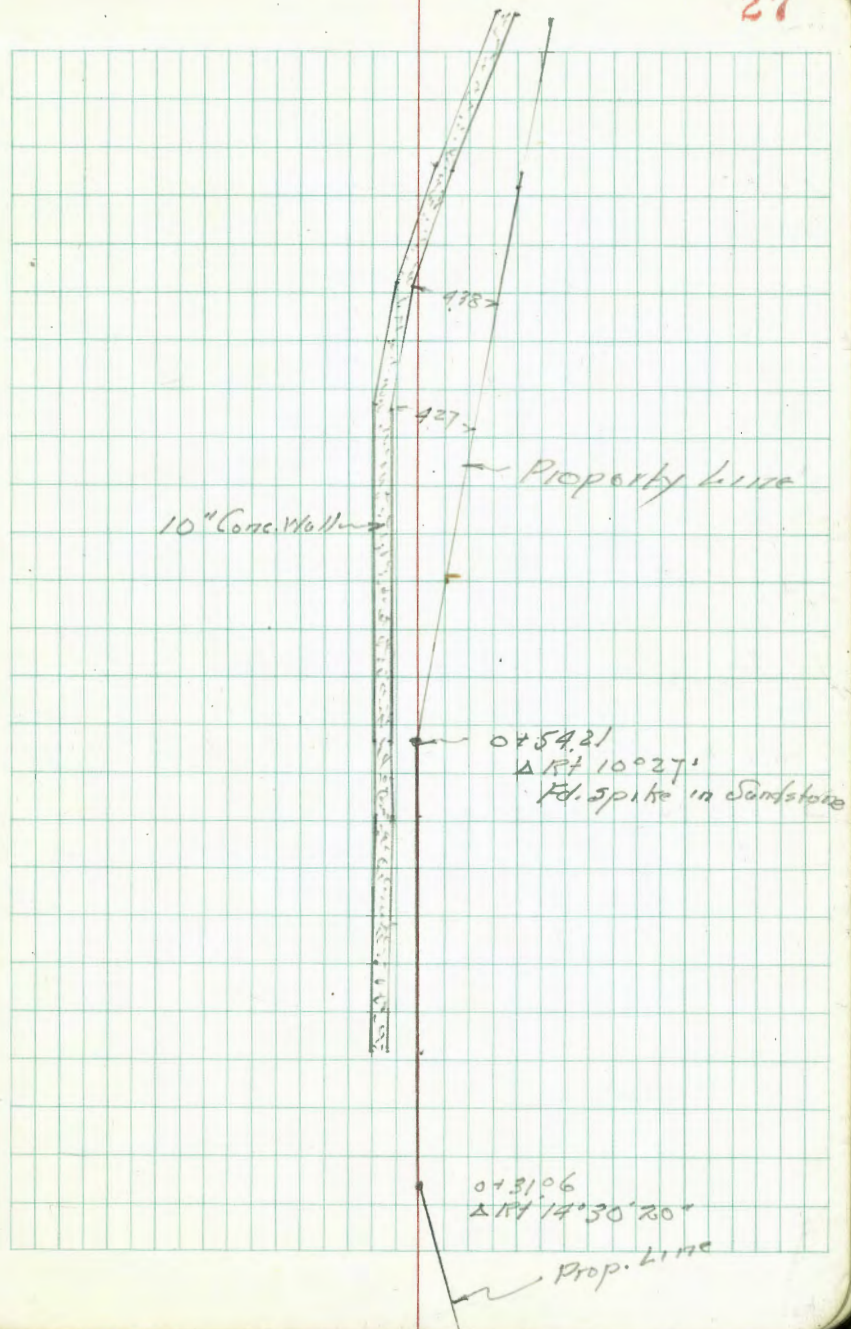
0154.21 =  $\Delta Rt$   $10^{\circ}27'$  Wall = 1.29' Lt.

0150 Wall = 1.32' Lt.

0137.5 Wall = 1.56' Lt.

0131.06 =  $\Delta Rt$   $14^{\circ}30'20''$  Rd. Spike in Sandstone

27



1759.48 =  $\Delta$  Lt  $23^{\circ}05'30''$  Wall = 5.46' Lt.  $\frac{1}{2}$  to Back Turn.

1751.3 Wall = 3.97' Lt.

1745 Wall = 3.2' Lt.

1737.9 Wall = 2.66' Lt.

1732 Wall = 1.43' Lt.

1726 Wall = 0.83' Lt.

1720.1 Wall = 1.52' Lt.

1718.36 =  $\Delta$  Lt  $60^{\circ}36'30''$

1717 = Wall = 2.05' Lt.

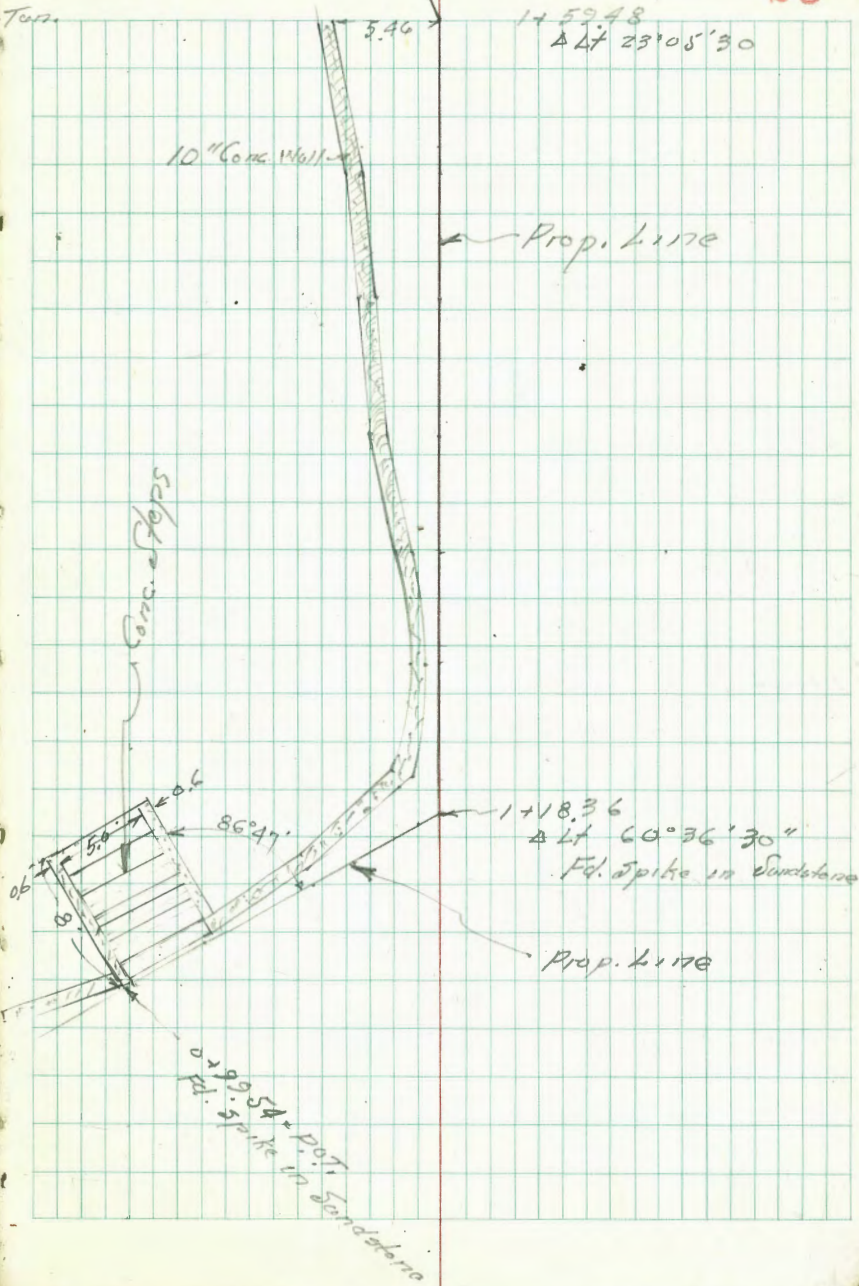
1711 Wall = 0.85' Lt.

1704.3 Wall = 0.27' Lt.

0799.54 Conc. step 0.16' Lt.

28

1759.48  
 $\Delta$  Lt  $23^{\circ}05'30''$



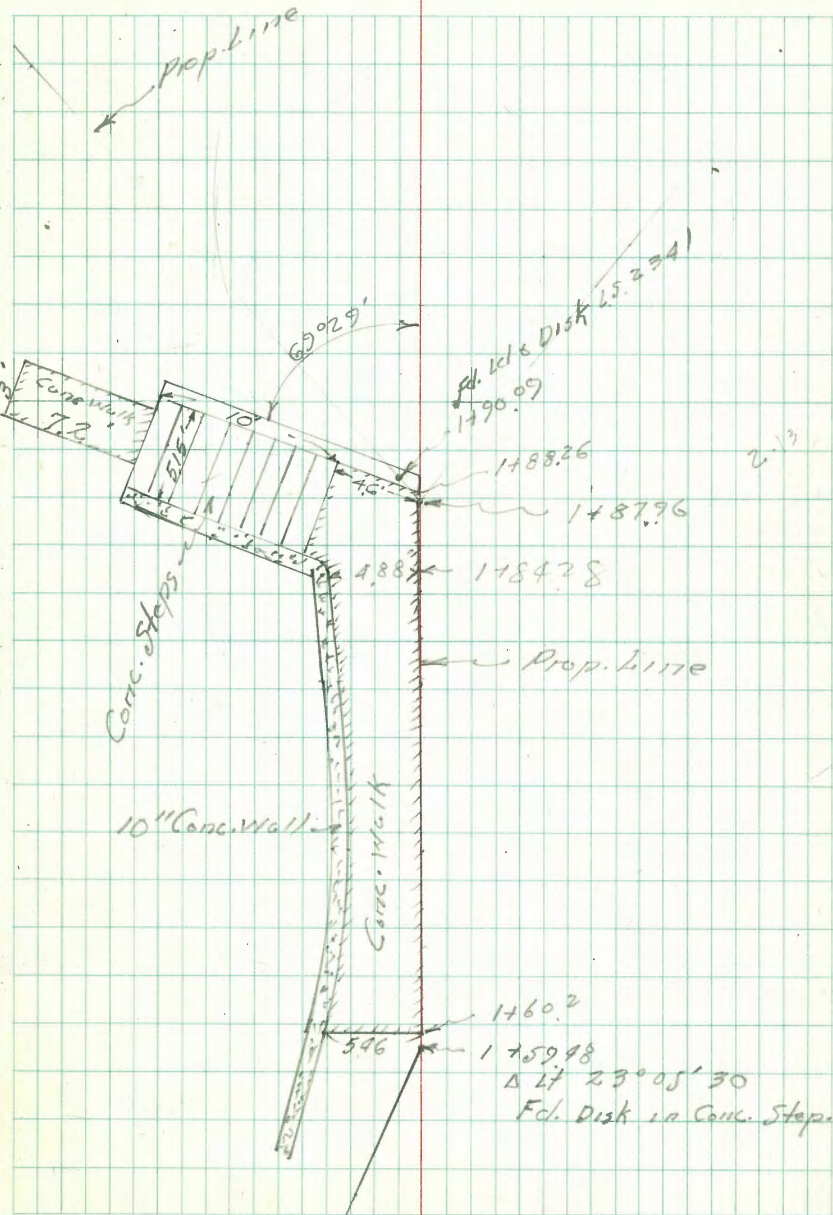
1+84.28 Wall = 4.88' Lt.

1+78.43 Wall 4.25' Lt. - Top of Wall

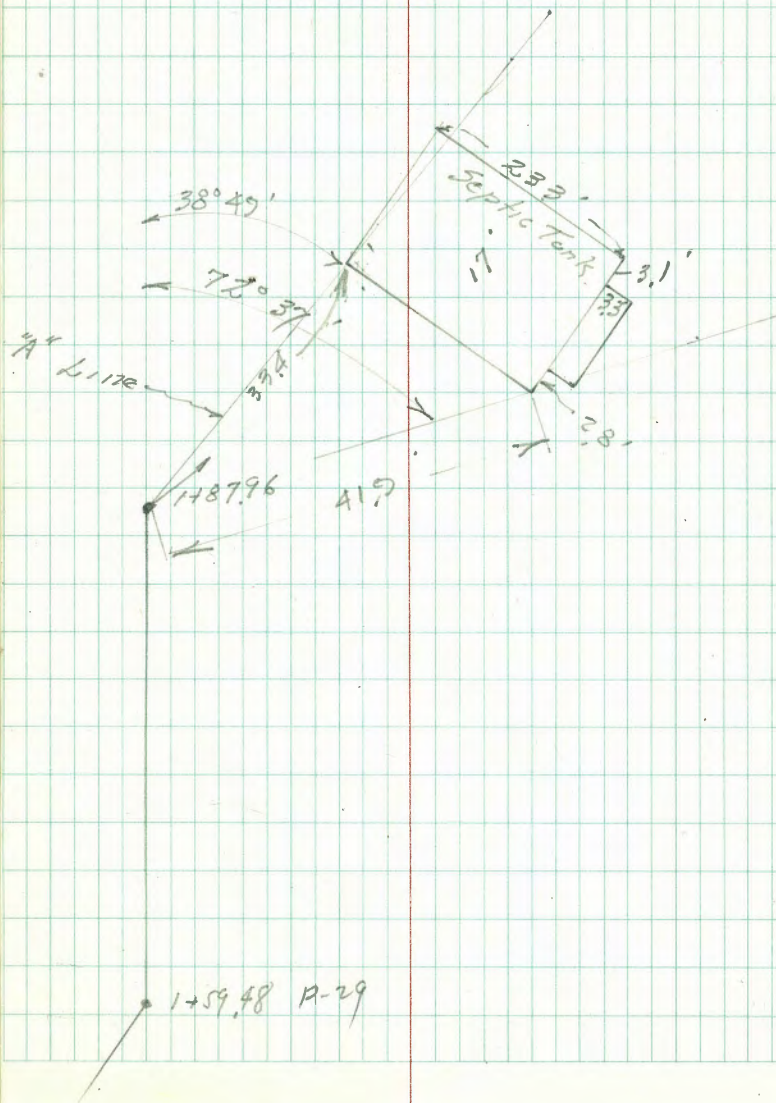
1+69.6 Wall 3.9' Lt.

1+60.2  
1+59.48

1+59.48 = ALT.







Levels on Existing Core Wall  
 Location P-216-30.

0+15

569  
 3.5  
 on wall

0+77

464  
 4.38  
 on wall

0+70.4

456  
 4.27  
 on wall

0+54.21

391  
 1.29  
 17.00 wall

0+50

391  
 1.32  
 on wall

0+31.06

408  
 1.3  
 on wall

0+20.3

448  
 2.47  
 on wall

0+00 on Top wall

433 433  
 7  
 on wall = Top stop

7.83 12.49

4.66

BM Cross on Top Tank (0+00 P-20)

12.49

Lt 2  
 8650  
 61120

Levels on wall  
Cont. from P-31.

1460.2

137.9

129.7

1418.36

1410

1406

049954

0492

12.49

ht.

Base  
line

32

5.10 927 924  
546 Walk Walk  
on wall 546

522  
266  
on wall

530

622

632  
on wall

5.90 5.95  
8.27 0.27

5.90 5.87  
8.2 0.6  
on wall on wall

5.98  
1.78  
on wall

12.49

Cont. P. 34

0+22

8.5

0+19.5

11.0

0+08

11.2

0+01

7.5

=0700

1+87.96

6.53

E Profile Levels "A"-Line to Cor Septic Tank

Levels on Wall Cont from P. 32

1+8826 = Diag. Section

2.37

14.6

on wall  
= Top Step  
= Walk

2.48	5.46	6.43	5.54	6.53
12	46	46	000	Walk
on wall	on wall	on wall	on wall	of wall
Bk.		= Bottom step		

1+8428

12.49

2.38

N.E. Cor  
Steps  
= Top step.

6.74	4.95
4.88	4.88
Walk	Wall
of wall	

12.49

2 Profile "A" Line  
Sketch P-38

0433 ✓ on Cor. Conc. Tank

0427

34

784

79

X-sect - East-West Alley BIK 109.  
Univ. Heights. Between Kansas & Utah

Johnson  
Clark  
Gregory 3+39.82 = E Utah st.  
10-10-49  
W.O. 31748 3+13.82 = East Cb line Utah  
2+99.82 = East line Utah st.

INDEXED  
W.K.  
OCT 11 1949

1449.91 = Int of E-W ALLEY

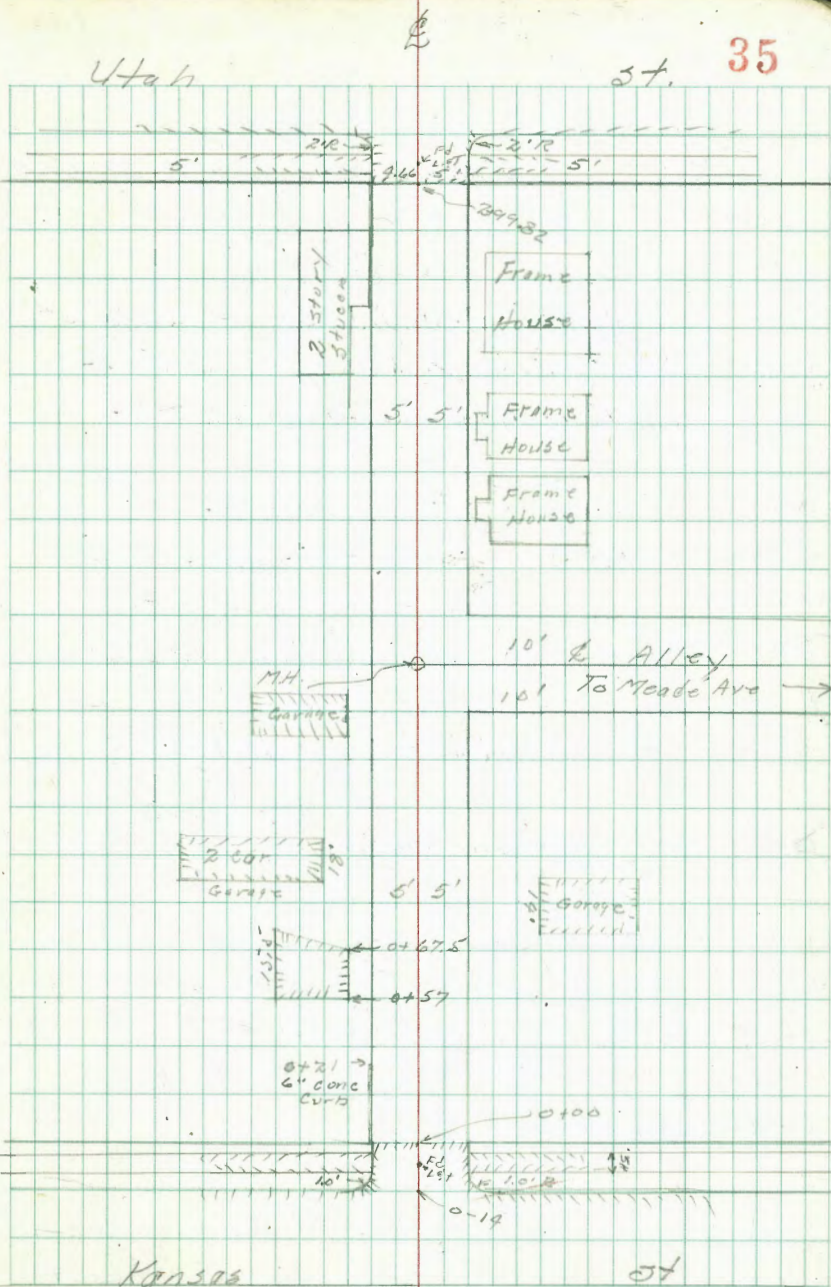
1437 = E Garage 29.3' x 12' conc. floor

0480 = E Garage 17.5' x 12'

0465 = E Garage 26.6' x 12'

0421 = 6" conc curb 4.8' x 12'

0400 = West Prop. line Kansas st.





X-Section E-W Alley - BIK 109 - Lint.  
Hght - Kansas to Utah

2+16 = Start Frame House 9' RT  
 2+08 = End of Frame House 9' RT  
 2+00 = Start 5' picket fence 5.4' Lt  
 2+00 = 4.8' Lt = 12" plaster wall 4.5' High

1+97 = E Steep - 6.2' RT  
 1+86 = Start Frame House 9' RT  
 1+79.91

1+69.91

1+59.91 = West Line N-S Alley

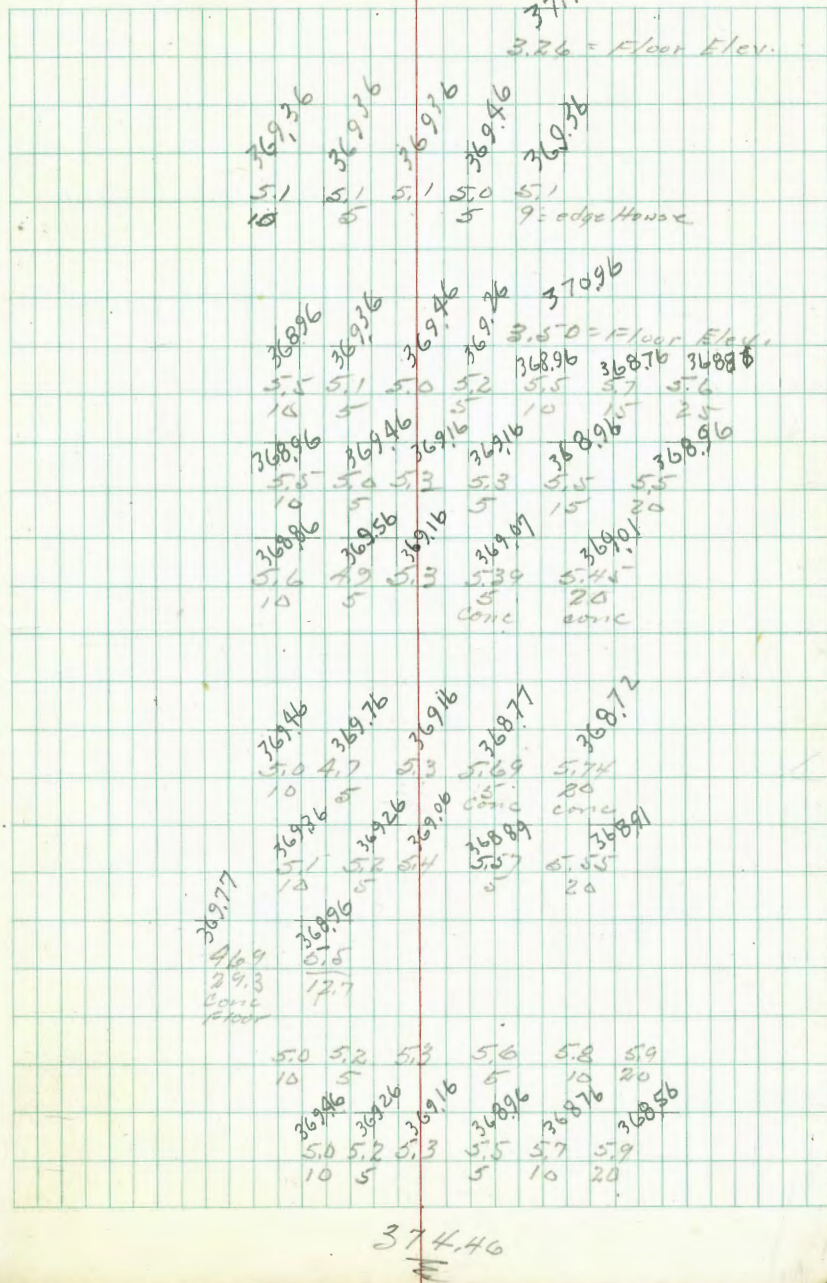
1+56 = Start 4' board fence 6.5' Lt  
 1+56 = power pole 3.2' Lt A 2872  
 1+49.91 = E Int. E-W & N-S Alley 5.81  
Rim 19.4.  
368.65

1+39.91 = East line of N-S Alley  
 1+39.91 = End 35' picket fence 5.4' RT  
 1+37 = E cone drive 12.7' Lt 15' wide

1+29.91

1+19.91

LT E RT 37





X-section - E-W Alley BIK 109  
Uni. Hghts - Kansas to Utah

0.02  
366.78

6.15 366.80

3.35 372.95 6.20 369.60

3.41 372.39

3139.82 = 4 Utah st.

3+13.87 = East Curb line Utah st.

3+03.82 = End Rail fence 6' RT  
E. Prop. line Utah st.

2+99.82 = End 4" Conc. Curb

T.P. 5.64 375.80 4.30 370.16

2+91.5 = End of Stucco House. Projection sticks

2+81 = End frame House 7.7 RT

2+80.5 = Start of 2.5' Rail fence 6.0 RT

2+70 = Deadman 3.7 LT

2+66 = Start 4" conc curb 4.7 LT

2+63.5 = Start Stucco House

2+63.5 = End 4.5' wire fence 5.7 LT

2+61 = Start Frame House 7.7 RT

2+52

2+45 = 1/2 Power pole 3.9 LT PA 2856

2+38 = End frame House 9.9 RT

2+34 = Start 4.5' wire fence 6' LT

2+31 = End 5' picket fence 5.4 LT

2+26 = 1/2 Street 6.4 RT

LT 2

RT

38

S.E.B.P. - Kansas of Meade

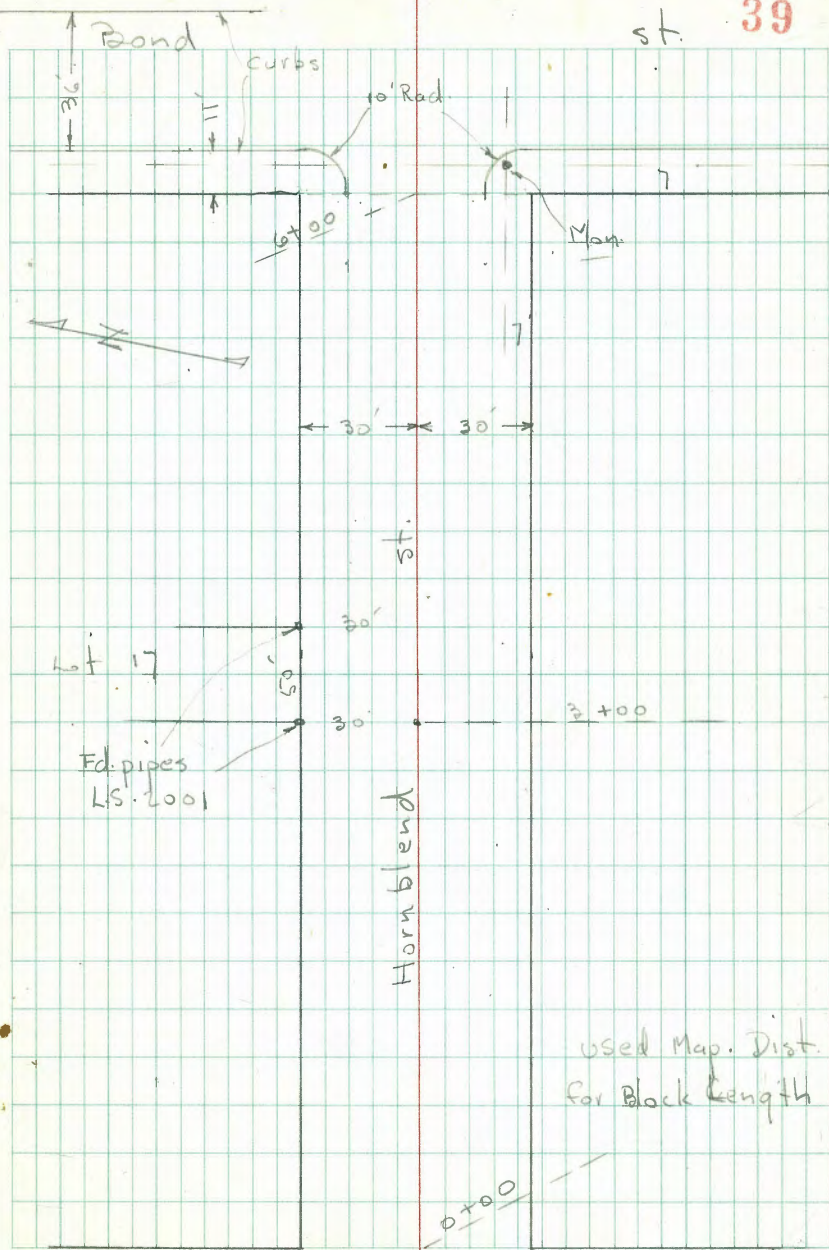
371.44  
4.34 4.66 4.96  
54 50  
370.65 370.25 370.39 370.04 370.01 370.03 370.40 369.75 370.11  
5.15 5.55 5.41 5.72 5.79 5.77 5.40 6.05 5.69  
cb cut cb cut cb cut cb cut cb  
370.60 370.44 370.26 370.33 370.48  
5.20 5.36 5.55 5.47 5.32  
cb cut cb cut cb

0.3 in Alley

372.80  
370.21  
4.25  
4.7  
Floor Elev. = 366

369.96 369.76 369.86 371.56  
2.90 = Floor Elev.  
4.5 4.7 4.6 4.8 5.1 5.4 5.1  
10 5 5 10 15 25  
369.56 369.76 369.06 369.06

374.46



used Map. Dist. for Block Length

Pico in swamp - No Points found. st



ends i' w. of line  
 6+00 = w.L. Bond. = end of obs. - Ret. on Rt.

5+50

5+00

4+50

4+00

3+50

3+38- 30' ht. = ± 10' Conc. Drive

3+20- 30' ht. = ± 3' Conc. walk

3+00

2+50

5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.4.2 4.0	4.4.0 4.0	4.3.3 4.0	4.3.6 4.0	4.3.7 4.0	4.2.56 4.0	4.3.4 4.0	4.4.4 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.5.0 4.0	4.4.0 4.0	4.3.3 4.0	4.3.6 4.0	4.3.9 4.0	4.3.5 4.0	4.4.7 4.0	4.4.9 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.6.0 4.0	4.5.1 4.0	4.4.6 4.0	4.4.4 4.0	4.4.2 4.0	4.4.7 4.0	4.4.6 4.0	4.4.6 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.5.2 4.0	4.5.1 4.0	4.4.6 4.0	4.4.4 4.0	4.4.2 4.0	4.4.7 4.0	4.4.6 4.0	4.4.6 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.5.2 4.0	4.5.1 4.0	4.4.6 4.0	4.4.4 4.0	4.4.2 4.0	4.4.7 4.0	4.4.6 4.0	4.4.6 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.5.2 4.0	4.5.1 4.0	4.4.6 4.0	4.4.4 4.0	4.4.2 4.0	4.4.7 4.0	4.4.6 4.0	4.4.6 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.5.2 4.0	4.5.1 4.0	4.4.6 4.0	4.4.4 4.0	4.4.2 4.0	4.4.7 4.0	4.4.6 4.0	4.4.6 4.0
5.34 4.31 ± 5 Floor Gar.	5.30 4.35 Dr.	5.29 4.36 at Porch	5.28 4.37 30' = walk	4.5.2 4.0	4.5.1 4.0	4.4.6 4.0	4.4.4 4.0	4.4.2 4.0	4.4.7 4.0	4.4.6 4.0	4.4.6 4.0

Bond + Hornblend.

Set B.M. on S.W. 7 Mon.

722 2.43

- End.

6 + 11 = Line of W. cb. - Should be 12 cbs.

Roadway is 36 Bet. cbs.

6.58	7.9	6.7	7.9	7.2	7.9	8.1	7.05	8.7	7.11
top.	put	top	put	put	put	put	top	put	put
3.07	1.8	2.93	1.9	1.9	2.5	1.8	1.6	1.5	2.54

9.65

Lt. # Rt.

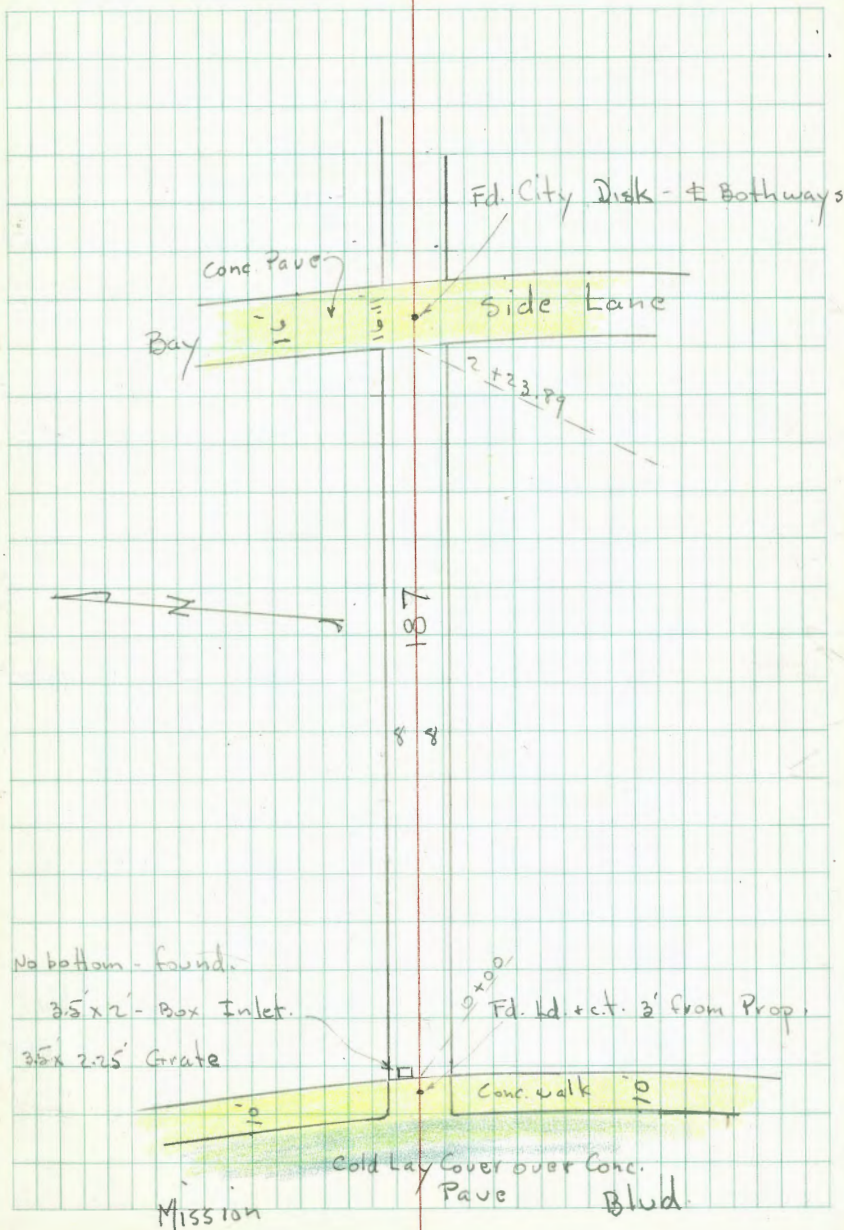
X-Sept. 16 Alley in Block 187  
Mission Beach

# 4406  
W.O. 31604

INDEXED  
W.R.  
APR 13 1950

Reduced 4-13-50  
W.R.

43





1+50

1+46 - 11.1' Lt. = end apron

1+31 - 8' Rt. = end Conc. walk

1+24 - 11' Lt. = Beg. Conc. apron to Doub. Gar. used as House

1+23 - 9.5' Lt. = # Pipe # A 825

1+12 - 8' Rt. = end wall + Beg. 2' Conc. walk along House

1+11 - 8.8' Lt. = # Apron to Doub. Gar. - Conc.

1+01 - 8' Rt. = Beg. 4" Conc. wall = base of fence

1+00 - 8' Rt. = end of walk at step

0+99 - 10' Lt. = # 3' Conc. walk

0+81 - 8' Rt. = Beg. 2' Conc. Walk along House

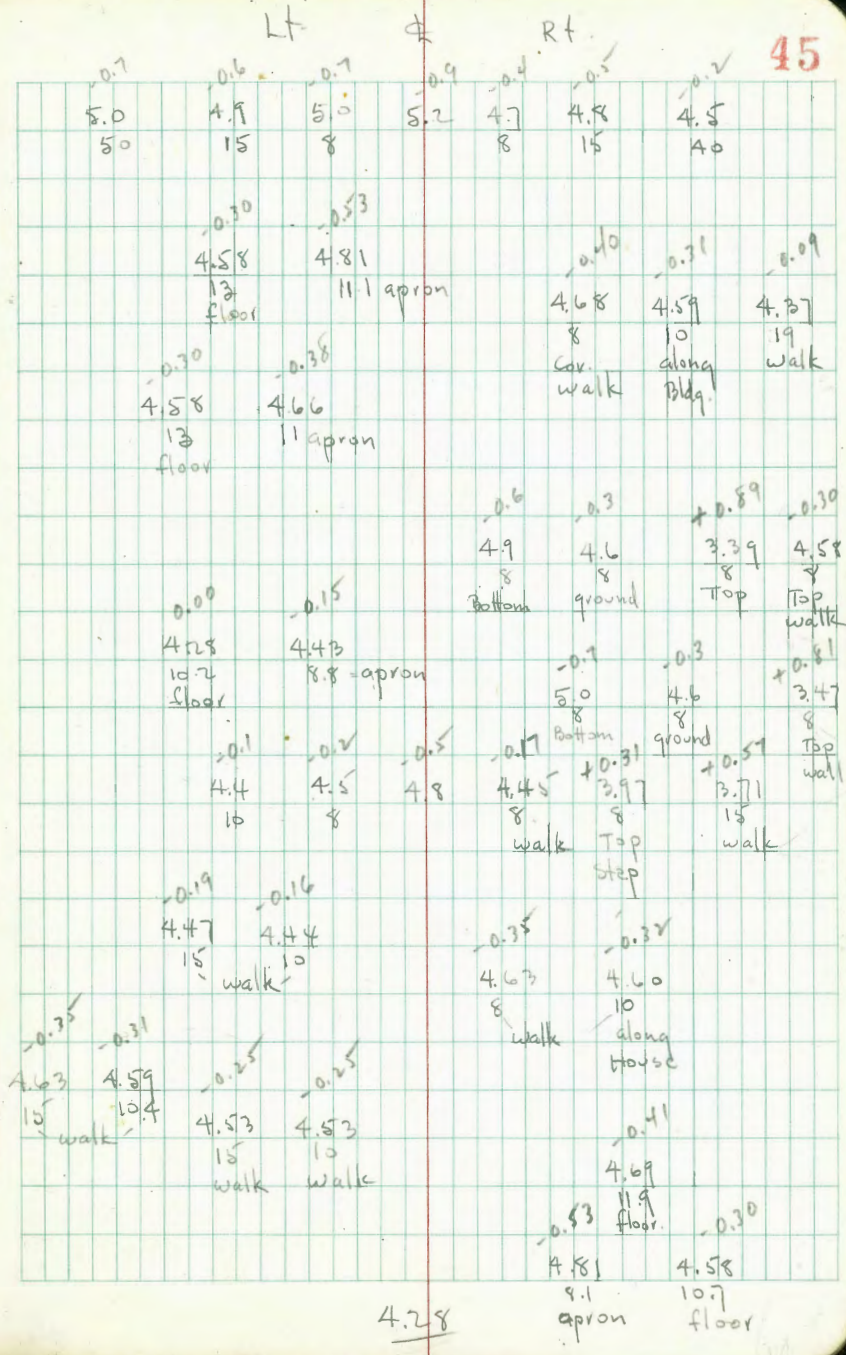
0+81 - 6.5' Rt. = # P. pole # P.A. 822

0+75 - 10.4' Lt. = # 2.5' Conc. walk

0+72 - 10' Lt. = # 2.5' Conc. walk

0+71 = 11.9' Rt. = # Sing. Gar. Conc. floor

0+54 - 8.1' Rt. = end Conc. apron





check T.P.

4.49

- 0.26

- 0.25

- from B.M.

2+31.95 = ± Bayside lane

outs are along curve on w.l.

is .030' w. - Rods on edge and

2+23.89 = w.l. Bayside lane - edge of Conc. Pavc.

T.P. 5.02 4.23 5.07 - 0.79

2+04 - 8.3' Rt. = ± 5' Conc. walk

2+01 - 8.5' Rt. = end fence

2+00

1+88 - 8.2' Rt. = end Bldg. + Beg. fence

1+81 - 8.3' Rt. = Beg. Stucco Bldg.

1+81 - 7.2' Rt. = ± Pipe # PA. 830

1+74 - 7.9' Rt. = ± Conc. apron to Sing. Gar.

1+64 - 10.7' Lt. = ± of 11' Conc. slab. to House

Lt.

±

Rt.

46

-1.11	-0.97	-0.93	-0.90	-0.89	-0.93	-1.16
5.34	5.20	5.16	5.13	5.12	5.16	5.39
70	20	8	8	8	20	70

-0.92	-0.70	-0.76	-0.87	-0.69	-0.71	-0.91
5.15	4.93	4.99	5.10	4.92	4.94	5.14
70	20	8	8	8	20	70

4.23

-0.54

4.82

8.3

walk

-0.34

4.62

15

-0.6

4.9

20

-0.8

5.1

8

-0.8

5.1

8

-0.6

4.9

8

-0.6

4.9

8.2 = ground

-1.0

5.3

8.3

Bottom of found.

-0.5

4.8

8.3 = ground

-0.55

5.13

7.9

apron

-0.10

4.98

8.9

floor

+0.32

7.96

13.9

floor at House

-0.31

4.59

13.9

at House

-0.55

4.83

10.7

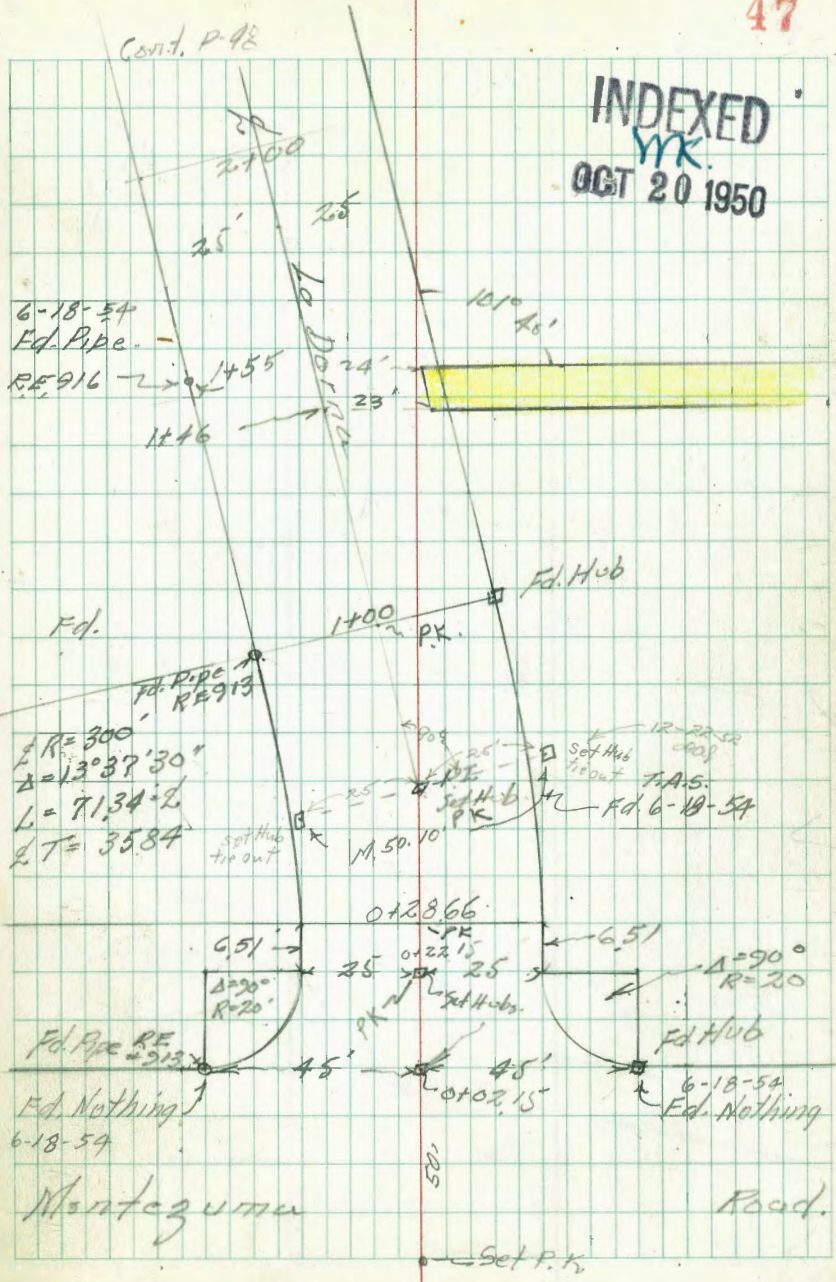
Conc.

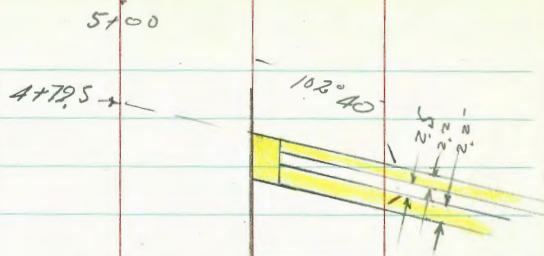
4.28

CROSS SECTION LA DORNA ST.  
from Montezuma  
To North End City Edge.

Walker  
Pope  
R. 585100  
1078-50  
NO 25020  
Orig. Sections in FB 1669-27

INDEXED  
M.R.  
OCT 20 1950





4+00

3+00

20' 7+63

cont. P-55

25' <- 20' >

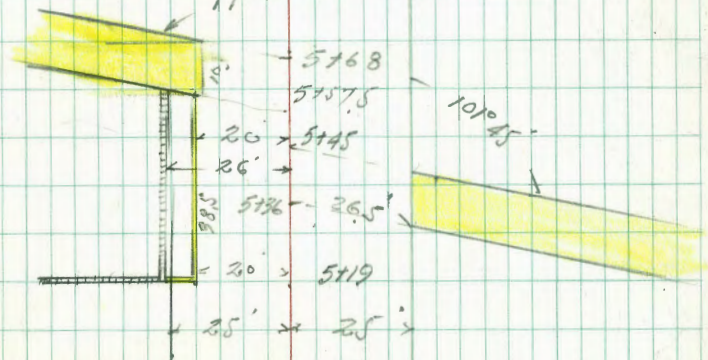
7+00

La Dama

6+12.45

6+00

7+02.0'



La Dorna

1401 25 Lt = Pole \* P. 278507

1400 = E.C.

0465

T.P. 503 450.65 639 445.62 <sup>on Pipe</sup> 2498 Lt 1400

0722.15 = B.C. Lt

0702.15 = H.L. Montezuma

0-14

0-17

Reduced by P. Hom

0-87.85 = L. Montezuma

T.P. 5.32 452.01 3.20 446.69 <sup>L Hub</sup> 0702.15

T.P. 3.77 449.89 7.42 446.12

T.P. 7.08 453.54 8.60 446.46

0.78 453.06 454.35

445.8	446.0	446.4	446.5	446.0	445.7	446.6	447.3	447.7
29 40	27 25	28 20	22 19 Edge	27 16 Edge	21 19	24 25	29 35	30 35
446.8	446.7	446.6	445.8	445.4	445.9	446.8	447.4	447.7
39 40	40 35	41 22	40 21 Edge	45 41 Edge	48 42 Edge	39 17	33 25	30 35
448.0	447.8	446.9	446.7	446.8	446.3	447.2	447.2	447.9
40 40	42 25	51 19	58 17 Edge	52 17 Edge	57 18 Edge	48 21	48 24	41 25 Edge
448.64	448.8	446.8	447.8	446.2	446.8	446.8	447.1	448.5
397 45	39 36	52 32	42 25 Edge	58 23 Edge	52 23 Edge	52 25 Edge	49 31	48.5 34 Edge
446.6	446.6	446.6	446.6	446.8	446.9	446.9	447.5	447.7
59 8	54 5	59 5	52	52	51 25 Edge	51 25 Edge	45	4.3 25
446.0	446.2	446.6	446.9	446.9	447.1	447.1	446.9	447.1
5.0 25	5.8 25	59 25	51	51	51 25	49 25	51 25	
446.5	447.1	447.3	447.4	447.5	447.6	447.7	447.7	
5.5 25	4.9 25	4.2 25	4.6 452.01	4.5 25	4.4 25	4.3 25		
B.M. on S. Cone No. 13498.77							181650	

La Donna St.

3+50

7.08 448.19 2.54 441.11

3+00

2+5 22.84 #278506

2+50

2+00

1+55 diag. -H edge Conc. DING

1+50

1+46 South Edge Conc. DING

450.65

433.5 436.0 436.1 440.0 439.6 440.4 441.2 441.4 440.8 440.9 442.2 50

14.7 12.2 12.1 8.2 8.6 7.8 7.0 6.8 7.4 7.3 5.0

50 25 22 16 14 19 20 22 25 50

437.2 438.1 441.9 441.4 441.9 442.7 443.0 441.9 442.1 442.9

13.5 12.6 8.8 9.3 8.8 8.0 7.7 8.8 8.6 7.8

40 25 18 16 17 17 19 21 25 40

Toe fill Edge oil Edge oil Toe fill

441.3 443.0 444.8 444.1 444.6 444.4 444.6 444.3 444.3

9.4 7.7 5.9 6.6 6.1 6.2 6.1 6.9 6.4

40 25 17 18 13 14 25 40

Toe fill Edge oil Edge oil

443.1 444.5 445.7 445.9 445.1 445.4 445.6 446.3 446.3 446.4

7.6 6.2 5.0 4.9 5.6 5.3 5.1 4.4 4.9 4.3

40 25 23 18 16 15 17 25 40

Edge oil Edge oil

446.98 447.17 447.93

3.67 3.48 2.72

24 27 45

DRIVE DRIVE DRIVE

444.1 444.9 445.9 446.0 445.1 445.6 445.6 447.2 447.7

6.6 5.8 4.8 4.7 5.6 5.1 5.1 4.5 5.0

40 25 23 19 18 17 16 25 40

Edge oil Edge oil Lower Lower

446.83 446.86 447.95

3.82 3.29 2.70

23 26 45

DRIVE DRIVE DRIVE

450.65

5+57.5

5+19

5100

4+80 N Side Ribbon Drive

4+72 = South Edge Conc. Ribbon Drive

4+50

4+23 22 Lt = Power Pole 274586

4+00

AA7.26 Lt  
 0.93 3.05 2.85  
 26.1 26 20  
 Tile Wall on 6" Wall on 6" Wall

AA7.12 AA8.97 AAA.29  
 1.07 4.22 3.90  
 26.1 26 20  
 on Tile Wall on Conc. Wall on 6" Conc. Wall

AA9.0 AA2.1 AA3.4 AA3.1 AAA.3 AA5.3 AA6.1 AA6.7  
 9.8 6.1 4.8 5.1 2.9 2.9 2.1 1.5  
 50 25 15 12 17 17 25 20  
 Edge of Edge of

AA6.27 AA6.81  
 2.22 1.38  
 24 50  
 Drive Drive  
 AA5.25 AA4.86  
 3.94 1.33  
 23 50  
 Drive Drive

AA35.0 AA38.0 AA40.6 AA40.8 AA42.3 AA43.5 AA45.2 AA46.5  
 13.2 10.2 7.6 7.7 5.9 4.7 3.0 1.7  
 50 25 16 14 18 18 25 50  
 Edge of Edge of Edge of

AA3.5 AA36.5 AA36.9 AA39.9 AA40.6 AA41.3 AA42.0 AA44.1  
 14.7 11.7 11.3 8.3 7.6 6.9 6.2 3.1  
 56 25 21 15 19 19 25 50  
 oil

5+75 = Reg. 6" Conc. Wall 25.3' d.

5+73 20' Lt. 170.562

TP. 8.81 454.14 2.86 445.33

5+50

5+45 = 11 edge Conc. Drive

5

5+36 = Sedge Drive

5+68 at edge Conc. Drive

5+57.8 = Reg. Conc. Drive  
448.19

446.10  
8.09  
25.9  
at wall

444.2	445.10	444.7	444.5	445.6	446.6	447.1	447.8	448.4
40	309	35	37	2.6	1.6	1.1	0.9	10.2
26	20	19	15		15	17	25	35
at wall	Wall		Edge oil		Edge oil		Low in	Low in

447.56	447.16
0.53	0.03
26.5	39.5
Drive	Drive

447.96	448.12
0.73	0.07
26.5	39
Drive	Drive

443.04	444.95	445.33	445.24
5.15	324	286	2.95
45	23	21	19
Drive	Drive	Drive	Drive

442.99	445.02	445.32	445.18
5.20	317	2.87	301
45	23	21	19
Drive	Drive	Drive	Drive

448.19

6+50 = End of Wall on Lt.

6+35.1

6+35 = Step up in Wall

6+29.1

6+29 = Step up in Conc. Wall

6+25 = 2 3' Conc. Walls

6+08.1 Step up in Wall (High Side)

6+08 = Step up in Wall (Lower Side)

6+00

445.9

8.2  
35

446.2	447.36	447.5	447.3	448.0	448.4	449.0	449.4	53
7.9	6.78	6.6	6.8	6.1	5.7	5.1	4.7	4.2
26	25.3	20	16	14	14	16	25	20
Lawn	Wall		Edge of		Edge of			

447.34

6.80  
25.3  
Wall

446.89

7.25  
25.3  
Wall

446.92

7.22  
25.3  
Wall

446.46

7.68  
25.3

446.17

7.27  
37  
Wall

446.09

8.05  
28  
Wall

446.44

7.70  
28.3  
Wall

446.53

7.61  
25.3  
Wall

446.10

8.09  
25.3  
Wall

445.6

8.5  
35  
Lawn

445.5

8.6  
26  
Lawn

446.11

8.03  
25.5  
Wall

445.9

8.2  
16  
Edge of

446.7

7.4  
14  
Edge of

447.5

6.6  
14  
Edge of

448.1

6.0  
16

448.7

5.4  
25

448.4

4.7  
10



Cont. P-58

7+63 = Bag. 4' Combination Walk & Curb on Lt.

7+50

Home Made Walk Not Good

7+35 = 4' end Conc. Walk on Rt.

7+11 = 3' Conc. Walk

7+00

Home Made Walk Not very Good

6+97 = Bag Conc. Walk on Rt. Along St.

6+88 20' Lt. Pole # JP 371122

Lt.

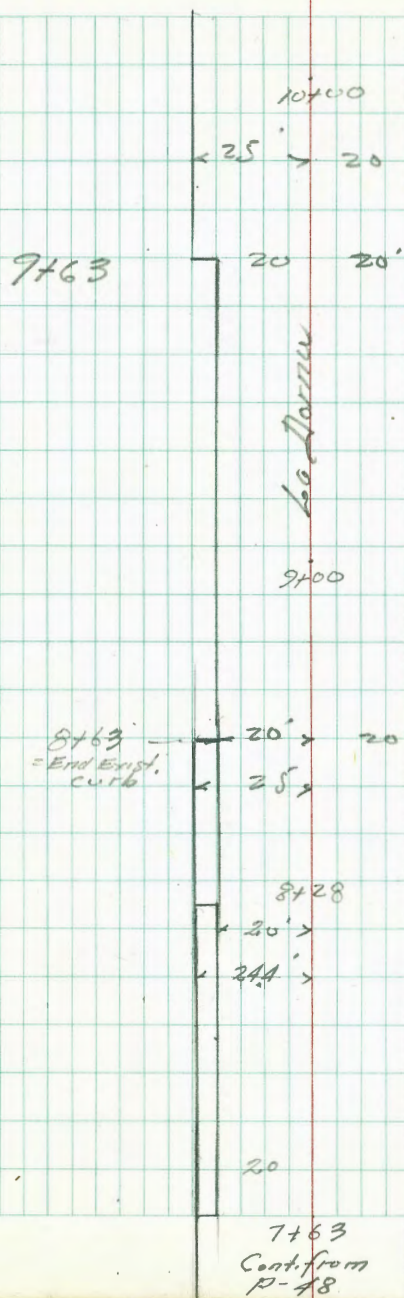
Rt.

Rt.

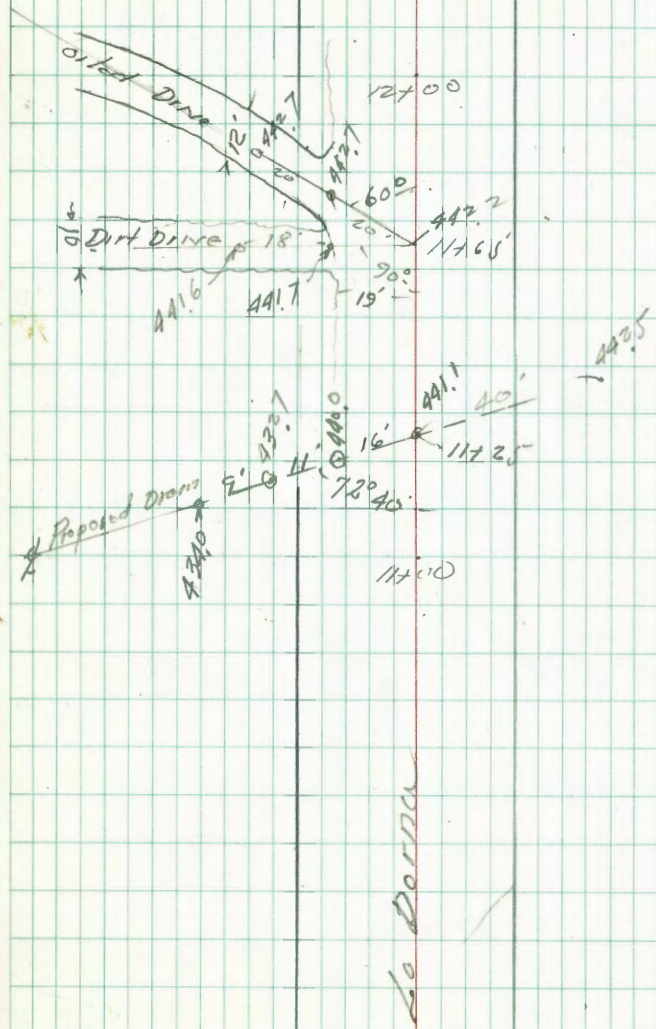
54

447.7	448.51	448.4	448.5	448.1	448.8	449.3	449.8	450.0	450.5
67 40	563 244 Walk	57 25	56 22	60 18 Edge of	53	48 145 Edge of	43 16	41 25	36 30
						449.96		450.08	
						118 153 Walk		106 19 Walk	
						449.71	449.87	450.44	
						933 153 Walk	427 198 Walk	370 32 Walk	
						449.6	449.75	450.2	450.8
75 42	59 34	60 25	60 21	63 17	55	49 14	439 153 Walk	39 25 Low	33 35 Low
						449.88	449.88		
						432 163 on Walk	426 193 Back edge Walk		

454.14



No Need to Extend Drain East of West Curb

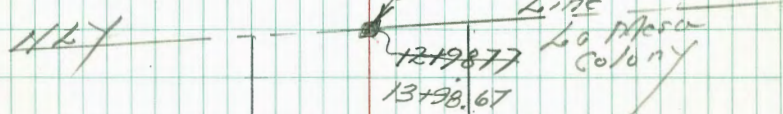


INDEXED

OCT 20 1950

mk

Elev 454.28 FBIGED 85  
B.M. on Conc. Line Mon.



La Duran

8+27 = N end Drive on Lt. <sup>Conc.</sup>

8+22 = Conc. Walk on Lt.

8+09 = Beg. Conc. Drive on Lt.

Beg. Walk on Rt.

8+03 = Elec. Pole 20' Lt. E 77894

8+00

7+88 = 3' Conc. Walk

7+73 = N edge Conc. Drive

7+65 = South Edge Conc. Drive on Lt.  
Cont. from P-54

58

Lt.				Rt.		
595 335 Drive	581 295 Drive	579 225 Bit	613 20 Drive			
AA8.19	AA8.33	AA8.35	AA7.95	AA8.96	AA9.09	AA9.73
583 335 Drive	577 294 Walk	577 225 Bit	621 20 in Drive	518 19.8 Cut	456 14.8 Cb.	441 31 Walk
AA8.31	AA8.37	AA8.37	AA7.93			
57 35 Low	574 294 Walk	577 20 Cb.	60 20 Bit	53	51 14 Edge cut	53
AA8.4	AA8.44	AA8.37	AA8.1	AA8.8	AA9.1	AA9.09
572 38 Walk	561 294 Walk	564 20 Cb.				
AA8.42	AA8.53	AA8.50	AA9.1	AA8.8	AA9.1	AA9.09
568 336 Drive	561 294 Walk	563 225 Bit	610 20 in drive			
AA8.46	AA8.53	AA8.51	AA8.04			
568 336 Drive	561 294 Walk	565 225 Bit	613 20 in drive			
AA8.46	AA8.53	AA8.51	AA8.01			

9+25 16" Plumage Pole 20.3' Lt.

9+10 20' Lt. = Pole Anchor

(Not taken in order)

8+99 = N edge Conc. Dr.

(Not taken in order)

(8+90) = S. edge Exist. Conc. Drive

TR. 176 452,95 ✓ 5.25 448,19

9+00

8+93 20.5' Lt. 173601 Pole

8+90 = End Exist. cb on Pt.

8+63 = N end Exist. cb.

8+50 45414

447.1	447.4	447.7	447.5	448.4	448.5	448.9	449.4	449.7
70 35	67 25	69 19	66 18	59	56 45	52 5	47 25	44 35
<u>452.95</u>								
					448.7	449.0		
					5.4 148 Gut. oil	4.74 148 cb		
	448.4	448.4	448.7	448.5	448.8	449.4	449.9	450.1
57 35 Lawn	57 25 Lawn	58.5 20 cb.	6.3 20 Gut. oil	56 148 Gut. oil	53 148 Gut. oil	4.65 148 cb.	4.2 25	4.0 35
		448.7	447.7	454.14				
		58.5 20 cb.	6.4 20 Gut. oil	447.7				

11+25

TR 5.52 447.07 11.40 441.55

11+00

18.0  
45

10+63 Tel Pole 20' Lt. 498719

10+50

10+00

9+84 = 12" Ruc. Tree 11' Rd

9+50

9+49 20.5' Lt = 2 14" Plumosa Palm

9+40 = 2.8' Coric. Walk

452.95

129  
50

A34.8	133.8	134.4	140.2	139.8	141.1	141.5	141.8	142.8
123 26	133 27	127 25	139 17	138 15	6.0	5.6 16	5.3 25	4.3 35
				56.0 oil	447.07	Edge oil		

A32.4	A32.6	A33.4	440.4	440.4	441.2	442.1	443.1	444.0
186 38	209 31	126 25	126 16	12.6 19	11.8	10.9 16	9.9 25	9.0 35
		Too Fl		Edge oil		Edge oil		

A37.5	A39.6	440.2	441.8	441.7	443.0	444.1	445.0	445.8
15.5 40	13.4 25	12.8 21	11.2 16	11.3 14	10.0	8.9 15	8.0 25	7.2 35
				Edge oil		Edge oil		

A43.2	A44.9	445.2	445.9	445.3	446.0	446.5	447.6	447.2	447.4	447.6
9.8 25	8.1 25	7.7 20	7.1 17	7.7 15	7.0	6.5 10	5.9 13	5.8 21	5.6 25	5.0 35
				Edge oil		Edge oil				

446.8	447.2	447.0	447.5	447.5	447.8	448.2	448.6
6.2 25	5.8 25	6.0 16	5.5	5.5 12	5.2 13	4.8 25	4.0 35
		Edge oil		Edge oil			

447.4	447.4
5.4 32	5.5 19
Walk	Walk
	452.95

Lt.

L

Rt.

60

13+00

12+68 = Pole Anchor 21' Lt

12+50

13+46 = Elec Pole #E-271119 21' Lt

12+40 = oiled drive on Lt

chk. starting 1100

T.P. 249 3.78 458.06

001  
454.28 = 1100  
P-49

T.P. 1048 455.73 1.82 445.25

12+00

11+75

11+50

447.07

Lt.

Rt.

Rt.

61

451.4	451.5	451.0	451.3	451.4	451.6	451.5
69	66	71	68	67	65	66
40	25	17	15	15	25	35
		Edge oil		Edge oil		

447.8	448.1	448.3	448.7	448.6	448.8	449.0
10.3	10.0	9.8	9.4	9.5	9.3	9.1
40	25	17	15	15	25	35
		Edge oil		Edge oil		

447.0	447.3	447.5	447.9
11.1	10.8	10.6	10.2
50	25	17	

458.06 ✓

443.0	444.2	444.2	444.8	445.3	445.9	446.4
4.1	2.9	2.9	2.3	1.8	1.2	1.0
40	25	16	15	15	25	35
		Edge oil		Edge oil		

438.9	439.6	440.9	440.8	441.8	442.8	443.2	444.0	445.0
8.2	7.5	6.2	6.3	5.3	4.3	3.9	3.1	2.1
50	40	25	17	15	15	15	25	35
				Edge oil		Edge oil		

435.3	436.1	437.6	440.9	440.3	441.6	442.0	441.7	441.5	442.
11.8	11.0	9.5	6.2	6.8	5.5	5.1	5.4	4.6	3.9
50	40	25	17	15	15	15	17	25	35
					447.07				



Go North

14+90 Under Construction

More Cutting

14+06 Under Construction

More Cutting

13+28.77

Note: Subdivider would like to have  
3.5' to 5.0' cut below Elev. as shown  
on this Section: "Says His Eng."

13+50

15806

Lt

L

R

62

A51.1	A51.6	A52.6	A52.0	A54.3
7.0	6.5	5.5	7.1	3.8
40	25		25	40

A50.7	A51.5	A52.9	A53.6	A53.7
7.4	6.6	5.7	7.5	7.9
40	25		25	40

A53.5	A53.8	A54.1	A54.0	A54A	A55.0	A53.9
7.6	7.3	7.0	7.1	3.7	3.1	4.2
40	25		25	35	150	

2' Cut under  
Bluff to  
oil Road.

A52.4	A52.8	A52.8	A53.0	A52.9	A53.3	A53.4
5.7	5.3	5.3	5.1	5.2	4.8	4.7
40	25	19		14	25	35

15806

Elev. on Basements with Plumbing  
on W. side. of La Dorna

1-29-51 - 7.0.

8+59-72' Lt. Nthly. of House = most  
of plumbing.

7+90-69' Lt. = E. of House - Basement.

6+27-90.1 Lt. Nthly of House - Plumbing

5+55-85' Lt. = E. Wly. of Basement.

4.      €

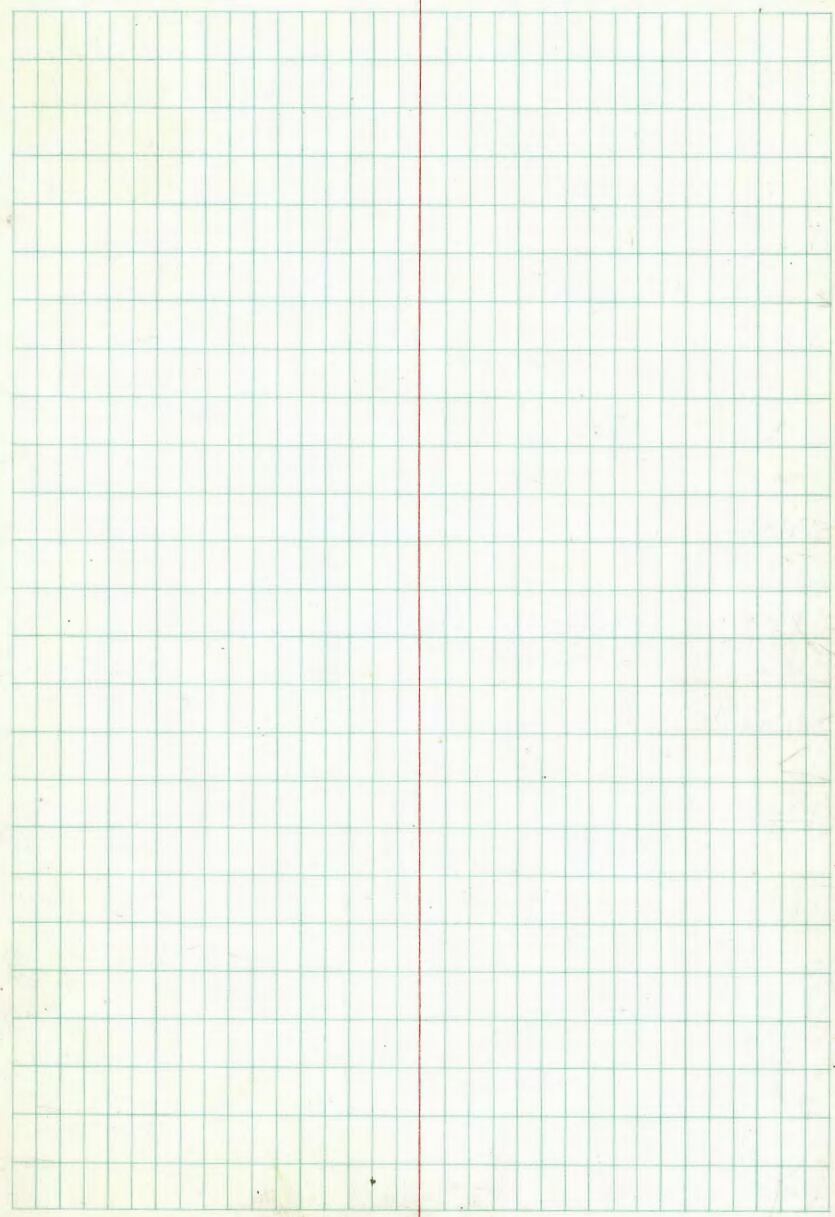
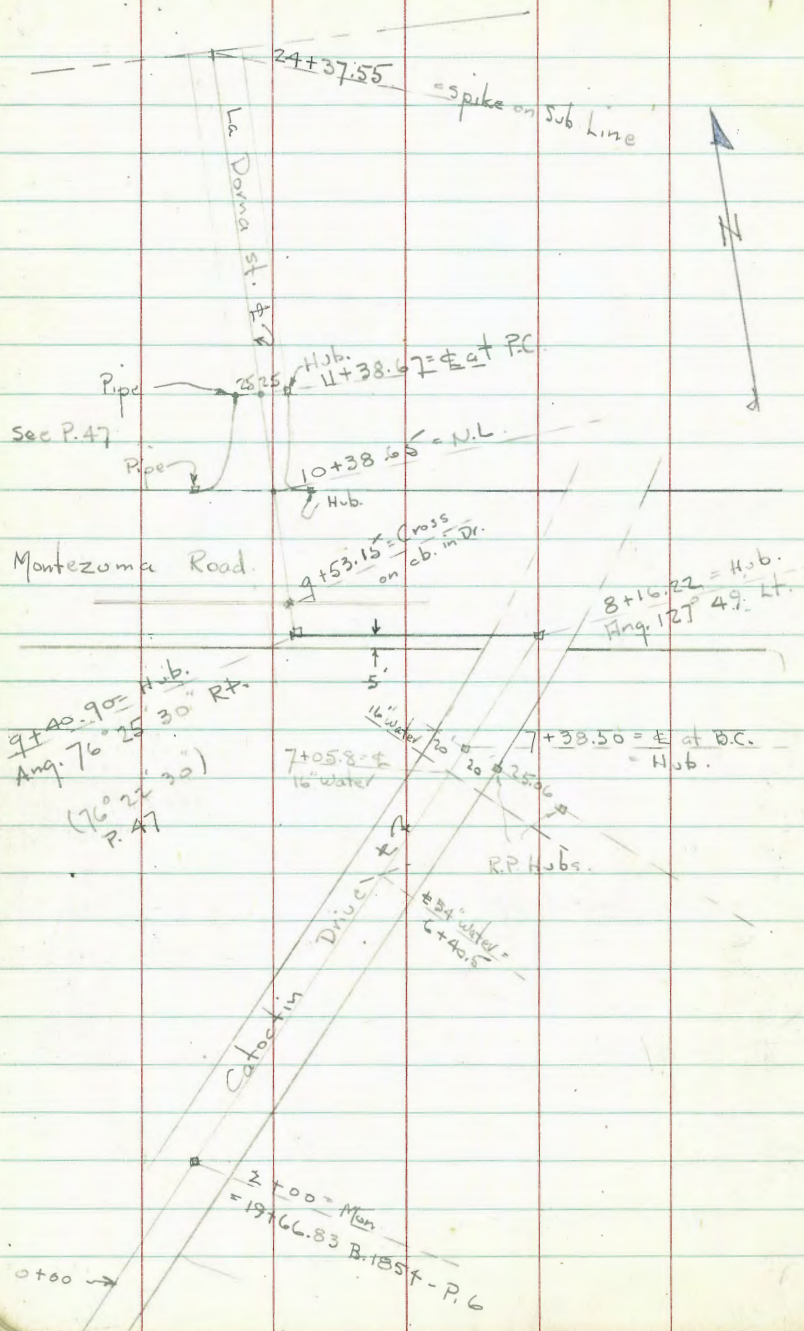
63

440.88 = Elev. floor  
72.0 of basement.

441.80 = Elevation  
69.0 floor basement.

438.97 = Elev. floor  
90.1 Basement.

434.83 = Elev. floor  
85' Basement.



Levels along  $\pm$  of Prop Sewer in  $\pm$  of  
Catactin to Montezuma  $\pm$  of La Dorna

#  
w.o. 10-10-51 70.

4+00

3+50

2+82 - 147 Lt. Ely. House + Conn. to tank

2+50 - 100' Rt. = Ely. House & Conn. to tank.

2+00

1+50

1+00

0+50

0-12- 137 Rt. = Wly. of House Conn.

B.M. = spike in Pole - Rt. 2+00 455.26

#

	49.2	53.3	
	75		
	vac lot.	53.5	
		54.0	52.75 = Top GI 147 Pipe to Tank
		54.4	53.0 100 = ground at Tank
		54.8	
	High on Lt.	55.3	55.1 100 = vac. Lot
		55.9	
		56.3	
		56.6	57.1 137 = ground. floor. about Same
	458' not shown		

used Elev. Rod. - Actual Elev. shown

9+00 - 15' Lt. = ground near tank = Conn.

9+53.8 - curb face on Ret.

8+16.22 = Ang. 127° 49' Lt. 122 Rt. 90° to Back Tang.

8+00

I.P. on F.H. 451.73

7+50

7+05.8 = Cross  $\pm$  of 16" Water 447.66 = Top of pipe.

7+00

6+57 - 96' Lt = wly. of House - Conn.

6+40.5 = Cross  $\pm$  of 54" Water 446.36 = Top of pipe

6+20 - 85' Lt = wly. of House - Conn.

6+00 - 98' Rt - By N.E. ly. of Courts

5+36 102' Lt = Conn. at wly. of House

5+15 233' Rt = lowest pt. of Conn. for group of Houses - + Court.

5+00

4+50

Lt.

$\pm$

Rt.

66

50.9  
15' ground

47.8

47.75  
9'.

48.28  
Top cb.

47.2

51.3  
127' = Conn.  
ground.

47.8

49.2

50.6

51.7

51.3

ground 96'

51.7

51.7

85' ground.

52.0

53.5  
98' ground - fig. 4 under  
at Courts. (for Courts  
in Back)

51.5

52.5

102' ground  
at Cor. House

52.8

53.4 ground  
98' =  
NW Cor.  
Courts =  
Conn.  
100 long.

50.3 ground  
233' = N.E.  
Cor.  
House

53.0

53.2

13+80

13+30 - 65' Lt. = Conn. at Sly. of House - 2' Below  
floor will make Conn. of House

13+00

12+80

12+50

12+15 - 75' Rt. = Conn. at Nly. of House

12+00

11+50

11+38.67 = P.C. B.M. on pipe on Lt. 445.62 - P. 49

11+30 - 146' Lt. = N.E. Cor. House (does Lot face Montezuma)

11+00

10+40.65 = end of exist. Crossing

10+38.65 = N.L.

9+53.3 = curb face = edge of Dr.

9+44.65 = Beg. Exist Crossing. - Plan 4192-B

9+40.90 = Ang. 76° 25' 30" Rt.

Lt.

=

Rt.

67

40.5

38.57  
floor  
elev.

37.2  
65 = ground

42.4

44.0

37.9  
75 = Vac.  
lot

44.7

45.3

45.4

47.2  
75 = ground

42.9  
60  
Vac. Lot  
low spot

45.4

45.9

47.5  
146 = ground

46.1

46.3

46.8

47.50

top cb.  
in Dr.

47.22

gt.

47.92 = on Hub

19+50 = 47' Lt. =  $\pm$  House - Can make Conn. 1' Below ground at House  
 19+15 =  $\pm$  House on Rt. = High  
 18+98 = 72' Lt. = Nly. of House  
 18+65 =  $\pm$  House on Rt. = High  
 18+30 = 69' Lt. =  $\pm$  House - Base.

18+00

17+50 =  $\pm$  House on Rt. = High

17+00

16+90 =  $\pm$  House on Rt.

16+66 = 90.1 Lt. = Nly. of House - Basement plumbing

16+50

16+00 =  $\pm$  House on Rt. = High

15+95 = 85' Lt. =  $\pm$  wly. of basement

15+50

15+10

14+75 =  $\pm$  House on Rt. = High

14+30

14+20 =  $\pm$  House on Rt. = High

Lt.

$\pm$

Rt.

68

46.9 ground	48.96 47 = floor.	48.0
40.88 72 = Base floor		48.4
41.80 69 = Base floor.		48.9
		48.9
43.8 75 Vac. lot.		48.7
		49.3
38.97 90.1 = Base Floor		47.5
		47.1
		45.9
34.83 85 = Basement floor		45.8
		44.4
33.5 75		43.1
		41.9
30.9 75 Vac. Lot.		40.5

24+37.55 = spike on Sub. line

24+00

23+70 - 223' Lt. =  $\pm$  House

23+50

23+05 - 198' Lt. = Conn. at House

23+00

22+50

22+00

T.P. Rock on Rt.

446.64

21+50

21+00

ground on Rt. is high

20+50

20+00

Lt.

#

Rt.

69

50.49  
Top cb.  
end

50.00  
18.2-gut.

50.7

50.53  
17.9-gut.

51.01

Top-end  
cb.

50.7

47.1  
ground

47.44  
22.3 floor

50.6

45.4  
ground

45.80  
19.8 floor

49.2

45.7

36.1  
75-Vac.  
Lot

42.1

45.0

31.3  
75  
Vac.  
Lot

42.3

45.3

47.2



D. Smith  
C. Allen  
R. Taylor  
A. Parks  
C. O'Neil

# Survey to Extend Storm Drain

San Miguel just North of Ocean View

wo# 21072

1/14/53

70

Ref. tie sheet #3438

plans 5987-L

San Miguel Ave.

Chimneys  
10' throat  
35' x 22' grade

set hub

0-0725

2700' of Pipe

0-4298 of Pipe

0-1572 of Pipe

99.05'

10'

2700'

Turned as per tie sheet

E Ocean View Blvd.

248.76' tie sheet

FK-17

FK-17

0-1572 of Pipe  
0-4298 of Pipe  
0-0725 of Pipe  
Note: Existing pipe is 150' S.W. of line.  
Need 15' catch basins for line + extend to channel

1140 set in place

INDEXED

JAN 19 1953

Extend Storm Drain San Miguel Ave.  
Lt-North

Rt-South

71

0+88

0+75

0+51 End existing pipes & pipes 0<sup>85</sup> North of line

0+42

0+29<sup>40</sup> Fly cb line & catch basin

0+14<sup>2</sup> & San Miguel

0+00 Fly cb line & catch Basin

TP <sub>4</sub>	0 <sup>65</sup>	43 <sup>33</sup> ↓	8 <sup>25</sup>	42 <sup>68</sup> ↓
TP <sub>3</sub>	0 <sup>08</sup>	50 <sup>23</sup> ↓	12 <sup>27</sup>	50 <sup>85</sup> ↓
TP <sub>2</sub>	0 <sup>53</sup>	63 <sup>12</sup> ↓	12 <sup>21</sup>	62 <sup>52</sup> ↓
TP <sub>1</sub>	0 <sup>25</sup>	75 <sup>30</sup> ↓	12 <sup>65</sup>	75 <sup>05</sup> ↓
B.M.	1 <sup>56</sup>	87 <sup>70</sup> ↓		86 <sup>14</sup>

N.E.P.  
Franklin  
Cuyamoca

57 <sup>9</sup>	57 <sup>2</sup>	57 <sup>8</sup>	57 <sup>6</sup>	57 <sup>5</sup>	57 <sup>9</sup>	57 <sup>2</sup>	57 <sup>9</sup>	57 <sup>9</sup>	57 <sup>9</sup>
25	15	10	5	5	5	5	5	5	5
45	42	42	42	42	42	42	42	42	42
25	14	10	X	7	4	10	10	10	25
40	40	40	40	40	40	40	40	40	40
25	7	5	2	2	2	2	2	2	2
91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>	91 <sup>2</sup>
25	5	5	5	5	5	5	5	5	5
141	0	170	0	0	171	462	0	171	0
25	25	5	25	25	25	25	25	25	25
gnt	cb	gnt	cb	cb	gnt	cb	cb	gnt	cb
42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>
25	25	25	25	25	25	25	25	25	25
142	0	162	0	0	153	366	0	153	0
25	25	5	25	25	25	25	25	25	25
gnt	cb	gnt	cb	cb	gnt	cb	cb	gnt	cb
42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>	42 <sup>21</sup>
25	25	25	25	25	25	25	25	25	25
142	0	158	0	0	143	331	0	143	0
25	25	5	25	25	25	25	25	25	25
gnt	cb	gnt	cb	cb	gnt	cb	cb	gnt	cb

43 33↓

Lt = North

Rt = South

72

BM starting p 71

120

86<sup>13</sup> ✓ ✓TP<sub>2</sub>87<sup>83</sup> ✓

1278

6<sup>58</sup>75<sup>05</sup> ✓TP<sub>7</sub>12<sup>86</sup>75<sup>63</sup> ✓0<sup>33</sup>62<sup>77</sup> ✓TP<sub>6</sub>11<sup>35</sup>63<sup>10</sup> ✓0<sup>49</sup>51<sup>75</sup> ✓TP<sub>5</sub>9<sup>26</sup>51<sup>94</sup> ✓0<sup>65</sup>42<sup>68</sup> ✓

1446

1430

1420

1417

Reduced by Loobhead 120-53

120 <sup>8</sup>	131	134	12 <sup>22</sup>	140	132	144	143	72
25	15	5	146	5	15	15	25	50
20.5	20.2	29.2	20.2	29.2	29.2	28.9	29.2	25.4
124	130	136	136	136	138	144		
24	15	5	5	5	15	25		
26.8	26.8	26.1	29.2	29.8	29.8	29.2		
64	64	72	133	135	135	144		
25	15	8	5	5	5	25		
270	271	261	221	202	202	202		
28	15	70	110	124	124	138	140	
13	15	1	5	5	15	15	25	

14333 ✓

Wot# 25020-

Aug 10, 1954

C. Allen

D. Smith

D. Sisson

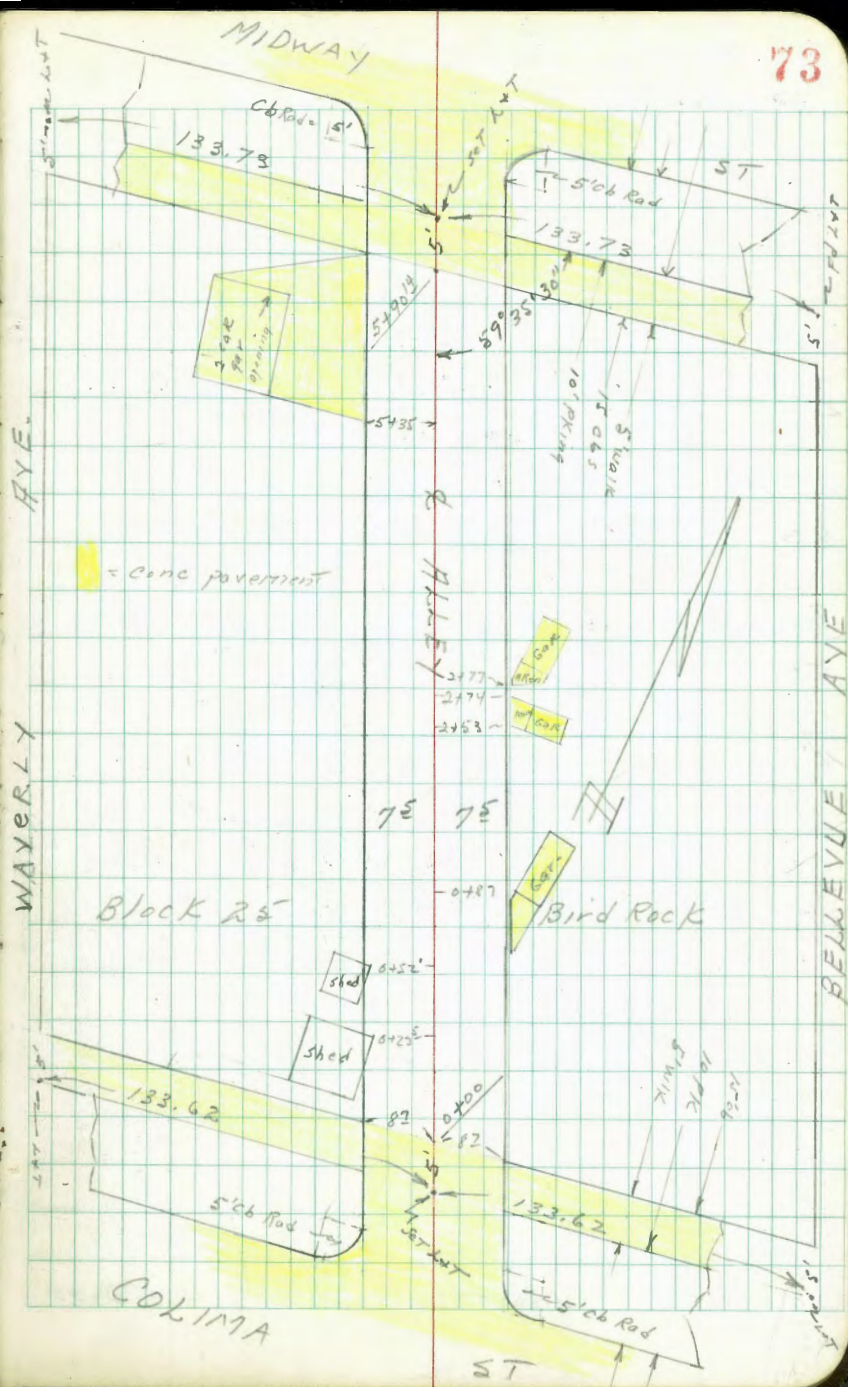
Ref. TP sheets - 1706, 1705. C. Powell

Dwg 2238-L.

Map 1083

X-Section Alley Block 25, Bird Rock Add.

INDEXED  
AUG 12 1954



X- Sec Alley BIK 25, Bird Rock  
 9<sup>2</sup> RT= swly cor Garage - Conc floor  
 0+87- 7<sup>2</sup> RT= end Conc Drive

0+78- 6<sup>2</sup> LT= 2.3' conc walk

0+75

0+75-

0+74- 8<sup>0</sup> LT= 2 36" Fuc tree

0+73- 6<sup>3</sup> LT= begin 5' high board fence

0+61- 7<sup>8</sup> RT= begin Conc drive

0+52- 5<sup>0</sup> LT= NELY cor shed - wooden floor

0+50

0+28- 5<sup>0</sup> LT= 2 10" Power Pole # 514516H

0+25-

0+23<sup>5</sup> 5<sup>0</sup> LT= NELY cor shed wooden floor

0+11- 5<sup>5</sup> LT= 2 dead trees -  
 Section taken along property on 3rd row.

0+00- Nly Line Colima ST-

Section taken along curb line  
 0-17<sup>2</sup> - Nly Curb line Colima ST

TP. 6.83 117.50 9.41 110.67  
 BM. 0.08 120.08 120.00

LT= wly

15' Alley RT= FLY  
 6' 22 5' 15 112.05  
 7' 9 9' 14  
 Dr Floor

74

110.60	6 <sup>90</sup>	7 <sup>53</sup>	8 <sup>57</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>
	50 Topcb	50 POT	17 <sup>5</sup> Top cb	17 <sup>5</sup> BC POT	8 <sup>2</sup>	8 <sup>2</sup>	11 <sup>5</sup> BC POT	11 <sup>5</sup> BC Topcb	50 POT	50 Topcb	
110.6	6 <sup>28</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.6	6 <sup>28</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.9	6 <sup>16</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.7	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.5	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.48	7 <sup>02</sup>	6 <sup>100</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.48	7 <sup>02</sup>	6 <sup>100</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.5	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
110.7	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
111.2	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
111.2	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
111.4	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
111.4	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
111.5	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
111.5	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.00	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.00	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.02	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.02	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.41	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.41	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.86	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
112.86	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
113.4	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
113.4	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
113.7	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
113.7	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
113.37	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
113.37	6 <sup>100</sup>	7 <sup>5</sup>	6 <sup>18</sup>	5 <sup>21</sup>	5 <sup>50</sup>	5 <sup>13</sup>	4 <sup>94</sup>	4 <sup>28</sup>	3 <sup>21</sup>	2 <sup>68</sup>	
117.50 X											

NW BR Midway ST + Bellevue

X-See Alley BIK 25, Bird-Rock

2+36-7<sup>6</sup> RT= begin 8' high conc block wall-

2+25

2+05-18' RT= Swly cor 2 car garage

2+00

1+72-7<sup>6</sup> RT= end 4' high wire fence

TP<sub>2</sub> 5<sup>35</sup> 115.28 7.57 109.93 #448825H

Nail in pole 5' 1764

1464-5<sup>0</sup> LT= end 5' high board fence  
5<sup>0</sup> LT= of Power pole #448825H-

1+50

1+44-5<sup>0</sup> LT= of Deadman.

1+25

1+00

0+94-7<sup>3</sup> RT= begin 4' high wire fence

LT= July

X

108.0	108.5	109.2	109.5	109.9
7 <sup>3</sup>	7 <sup>0</sup>	7 <sup>1</sup>	7 <sup>2</sup>	7 <sup>3</sup>
17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>
108.8	108.8	108.6	108.6	108.0
6 <sup>5</sup>	6 <sup>5</sup>	6 <sup>2</sup>	6 <sup>2</sup>	6 <sup>10</sup>
7 <sup>3</sup>	7 <sup>3</sup>	7 <sup>3</sup>	7 <sup>3</sup>	7 <sup>3</sup>
109.0	109.0	109.2	109.2	109.4
8 <sup>4</sup>	8 <sup>2</sup>	7 <sup>10</sup>	7 <sup>10</sup>	6 <sup>8</sup>
17 <sup>5</sup>	17 <sup>5</sup>	6 <sup>0</sup>	7 <sup>10</sup>	7 <sup>5</sup>
109.9	110.0	110.0	110.7	110.7
7 <sup>5</sup>	7 <sup>5</sup>	7 <sup>5</sup>	7 <sup>5</sup>	7 <sup>5</sup>
110.3	110.3	110.3	110.7	110.7
7 <sup>2</sup>	7 <sup>2</sup>	7 <sup>2</sup>	7 <sup>5</sup>	7 <sup>5</sup>
17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>
110.5	110.5	110.5	110.7	110.7
6 <sup>8</sup>	6 <sup>8</sup>	6 <sup>8</sup>	6 <sup>8</sup>	6 <sup>8</sup>
7 <sup>5</sup>	7 <sup>5</sup>	7 <sup>5</sup>	7 <sup>5</sup>	7 <sup>5</sup>
111.2	111.2	111.2	111.2	111.2
6 <sup>10</sup>	6 <sup>10</sup>	6 <sup>10</sup>	6 <sup>10</sup>	6 <sup>10</sup>
17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>

117<sup>50</sup> X

4- see Alley BIK 25 - Bird Rick ad.

LT = wly

75 Alley

RT = Ely.

76

3400 - 7<sup>8</sup> RT = begin 4' high haquire fence

8<sup>9</sup> RT = swly coc garage

2489 - 7<sup>6</sup> RT = end single conc apron + floor

6<sup>8</sup> LT = begin 4' high wire fence

2485 - 7<sup>5</sup> LT = end 3<sup>5</sup> high wire fence

2483 - 7<sup>5</sup> LT = 4 3' wide conc walk

gar opens to south on slant + Apron

2477 - 7<sup>6</sup> RT = begin single gar. conc floor

2475

2474 - 7<sup>6</sup> RT = end 2 car Gar. conc floor + Apron

2468 - 6<sup>3</sup> LT = 2 12" power pole # JPA 5439.

2453 - 7<sup>8</sup> RT = begin 2 car garage - conc floor + Apron.

2450 - RT = end 8' high conc block wall.

2445 - 7<sup>5</sup> LT = begin 3<sup>5</sup> high wire fence

	5 <sup>8</sup> 110.3	4 <sup>7</sup> 110.6	110.7	4 <sup>3</sup> 111.0	3 <sup>7</sup> 112.6
	17 <sup>5</sup>	7 <sup>5</sup>	4 <sup>6</sup>	7 <sup>5</sup>	15 <sup>5</sup>
				21 11	112.02
				386	326
				76	104
				Apron	Brk in Apron
2201	110.26				112.09
		7 <sup>2</sup> 110.56			3 19
502		7 <sup>0</sup>			108
17 <sup>5</sup>		wlk			Floor
					At gar dock
				111.00	
				428	
				7 <sup>5</sup>	4 10
				Apron	Brk in Apron
				8 11	3 88
					115
					on apron
		5 <sup>5</sup> 110.3	4 11.4		
		7 <sup>5</sup> 110.10	4 <sup>9</sup>		
				4 <sup>5</sup>	
				7 <sup>5</sup>	
					110.78
					4 50
					Apron
				4 8 110.35	
				Apron	
				7 100 110.1	
					402
					92
					floor
				5 11 110.4	
				4 9	
				8 2	
				9 1	
					6 14
					108.9
					8 12
					foot

115.28 π

X-sec Alley BIK 25, Bird Eock

Apron Parallels Alley Line

opens to Ely - opening Parallels Waverly Ave

4411- 7<sup>8</sup> LT= begin conc Apron for 2 car gar.

4400

3496- 7<sup>6</sup> LT= end Conc Apron for 2 car gar.

conc floor

Apron parallels Alley Line

gar opens to Ely - opening Parallels Waverly Ave

3480- 7<sup>6</sup> LT= begin conc Apron for 2 car garage

TP<sub>3</sub> 5.53 117.27 3.54 111.74

3480- 8<sup>6</sup> LT= end 4' high cyclone fence

3475

3466- 9<sup>0</sup> LT= begin 4' high cyclone fence

3455- 7<sup>7</sup> RT= begin 5' high board fence

3454- 11<sup>6</sup> LT= & Door to single gar. conc floor

gar open to Nly. See above

3450- 7<sup>7</sup> LT= Nely cor gar - conc floor

3425

3424- 7<sup>6</sup> LT= end 4' high wire fence

3415- 7<sup>7</sup> RT= end 4' high hq wire fence

LT= WLY-

APly

RT= ELY-

177

	111.5		111.92		
	5.8		5.35		
	17.5		7.5		
	111.74		111.45		
	5.53		5.62		
	134 Floor		7.5 Apron		
			111.57		
			5.90		
			7.5 Apron		
			111.3		
			4.0		
			3.9		
			7.5		
			117.27		
			111.8		
			7.5		
			111.30		
			3.8		
			11.5 Floor		
			111.0		
			4.3		
			7.5		
			111.0		
			4.3		
			7.5		
			111.2		
			4.1		
			111.09		
			4.0		
			7.5		
			111.3		
			4.0		
			7.5		
			111.5		
			3.108		
			7.5		
			3.2		
			17.5		
			115.28		



5400 - 7<sup>5</sup> RT = wly of fence

4793 - } 7<sup>5</sup> LT = begin 6' wide Conc base for fence

4778 - } 7<sup>5</sup> LT = 4' wide Conc walk

4775 - 7<sup>4</sup> LT = begin 6' high Redwood board fence

4763 - 15<sup>5</sup> LT = 2 car garage - dirt floor

4750

4745 - 7<sup>2</sup> LT = end 7' Redwood board fence  
Conc Base

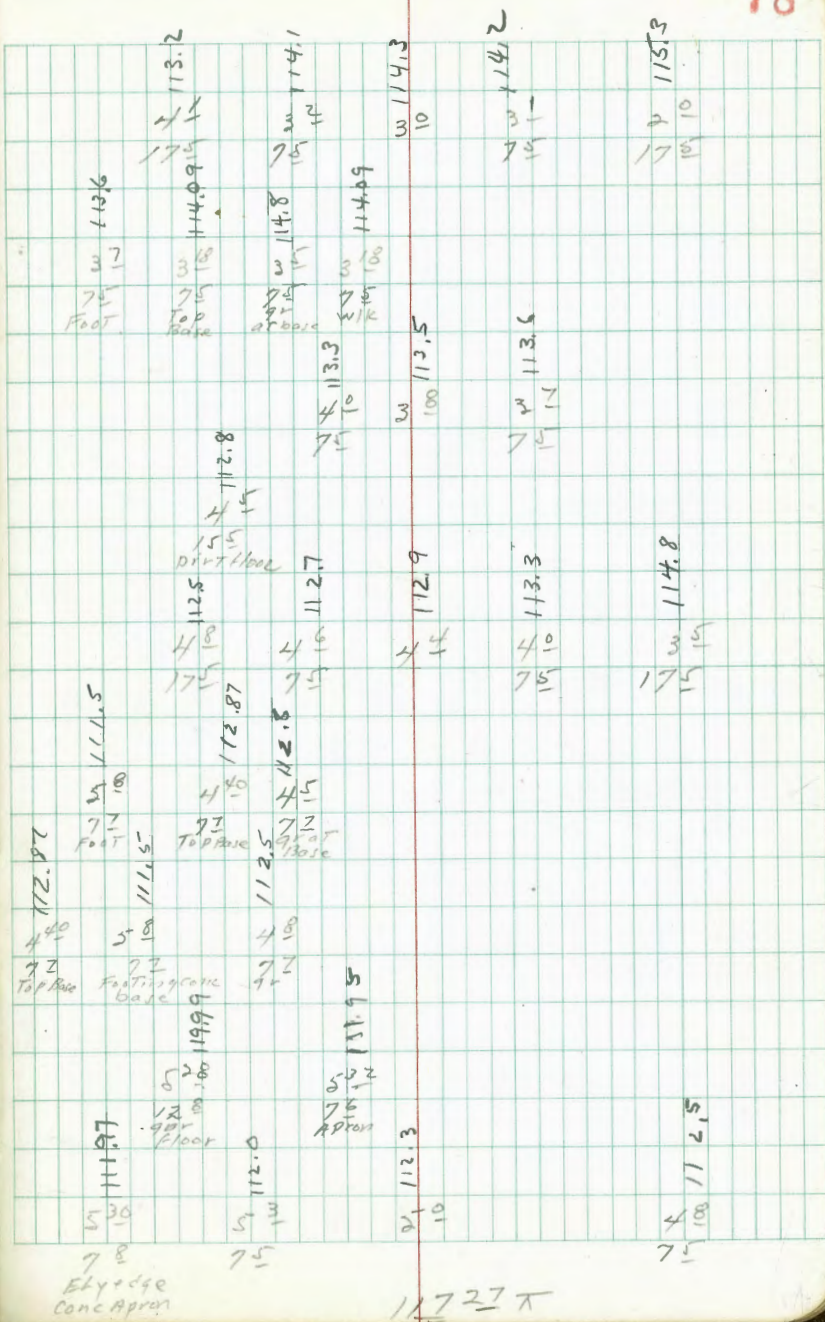
4743 - 6<sup>2</sup> LT = 12" Power pole # PA5465

4733 - 7<sup>2</sup> LT = begin 7' Redwood board fence  
One Conc base

4732 - 7<sup>6</sup> LT = end Conc Apron 2 car gar  
128' LT = conc floor at NELY cor gar

4725 - 7<sup>8</sup> LT = Ely edge Conc Apron

7<sup>7</sup> RT = wly board fence



Ely edge  
Conc Apron

11727 X

TP5

6+67<sup>5</sup> = Sly curb Line Midway ST

Alley Returns have 5' Radius.

8<sup>2</sup> RT= end ely curb Alley. } Section  
 8<sup>2</sup> LT= end Wly curb Alley. } Taken along  
 on skew along prop sly line  
 8<sup>7</sup> LT= end Conc Apron } Midway.

5+90<sup>14</sup> = sly Line Midway ST - sly edge Conc Pav -

5+84 - 7<sup>5</sup> RT= end board fence

7<sup>6</sup> RT= wly of Board fence

5+75 - 7<sup>5</sup> LT= ely edge Conc Apron.

TP4 5.21 120.12 2.36 114.91

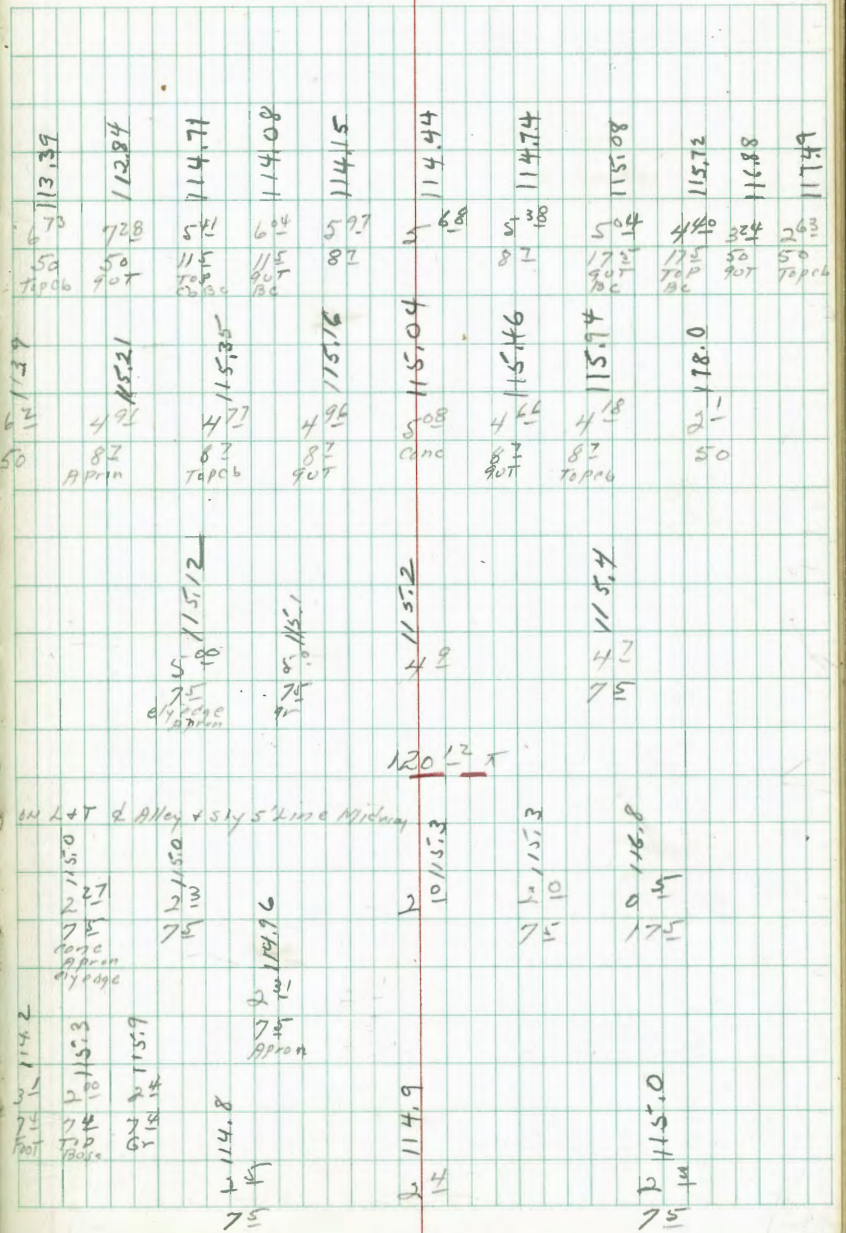
5+50 - 7<sup>6</sup> RT= wly board fence

opens to Wly.

5+35 - 7<sup>5</sup> LT= begin Conc Apron - 2' corner - Conc Base

5+34 - 7<sup>4</sup> LT= end 6' high board fence

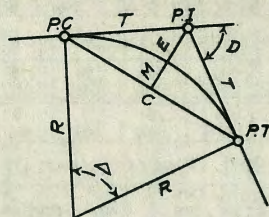
5+25



117.27 x

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

Radius  $= R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve  $= D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent  $= T = R \tan \frac{\Delta}{2}$  (3) Length of Curve  $= L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate  $= M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers } \frac{\Delta}{2}$  (6)

External  $= E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec } \frac{\Delta}{2}$  (9)

Long Chord  $= C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I.  $- T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C.  $+ L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 — Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$  and from Table V correction = .10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

$$\begin{array}{r} 444.29 \\ 0.25 \\ \hline 444.54 \\ 9.71 \\ \hline 434.83 \end{array}$$

$$\begin{array}{r} 555 \\ 10.38 \\ \hline 1593 \end{array}$$

$$\begin{array}{r} 790 \\ 1040 \\ \hline 1830 \end{array}$$

$$\begin{array}{r} 627 \\ 1039 \\ \hline 1666 \end{array}$$

$$\begin{array}{r} 859 \\ 1040 \\ \hline 1899 \end{array}$$

N.E. Toft 147.52

77.98  
 6.19  
 84.17  
 1.10  
 83.07  
 13.27  
 93.34  
 0.26  
 93.08  
 12.93  
 105.91  
 0.08  
 105.83  
 12.60  
 118.43  
 0.18  
 118.25  
 12.42  
 130.67  
 0.16  
 130.51  
 12.69  
 143.20  
 0.14  
 143.06  
 13.18  
 156.24  
 0.91  
 155.33  
 9.91  
 165.24

5421  
 5106  
 23 15  
 5421  
 4533  
 995  
 1882  
 11836  
 47031.30  
 1905  
 20-10.28  
 60-96.90  
 19-71.58  
 38.74  
 141836  
 4112  
 145948  
 2849  
 148796  
 15948  
 1810  
 17943  
 15948  
 248  
 18428  
 4884  
 23.89  
 8.06  
 31.95  
 24 37.55  
 11 38.67  
 12.9888

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.0. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-10) \* 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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