

1867

WALTER

ENGINEER'S

NOTEBOOK

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Sides 1 on 1.
For Single Track Embankment.

MICROFILMED
DEC 30 1964

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

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(RECORD YOUR JOB)
PLEASE

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Check Side walk. Beryl St.

7-6-48
W.O. 31120

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Sommermeier
McCoy

Sta.	Thickness on Lt.	walk width	Thickness on Rt.	Rise to back of walk
		South side of Beryl		
0+70	3 7/8 0.32	4' 11 5/8" 4.97	4" 0.33	5/8" .05
0+60	3 3/4 0.31	4' 11 7/8" 4.99	3 5/8" 0.30	1" .08
0+50	3 3/4 0.31	4' 11 3/4" 4.98	4" 0.33	1 .08
0+40	4 0.33	4' 11 3/4" 4.98	4 1/8" 0.34	1 1/8" .09
0+30	3 7/8 0.32	4' 11 1/2" 4.96	4 1/8" 0.34	5/8" .05
0+20	3 3/4 0.31	4' 11 1/2" 4.96	4" 0.33	0 .00
0+10	4 0.33	5.00	4" 0.33	1.00
0+00 = E. line Cass	4" 0.33	5 1/2 5.04	4" 0.33	3/8 .03

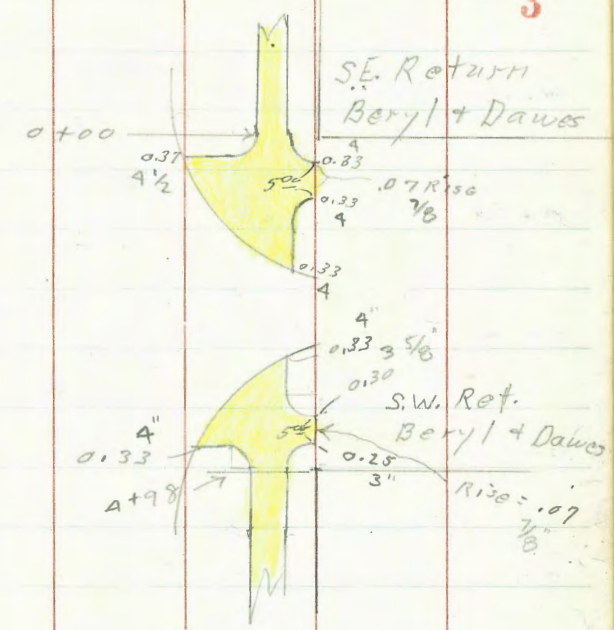
INDEXED WB	Thickness left edge	Width	Thickness Rt. Edge	Rise to back ①	
				1	
1+60	3 7/8 0.32	4' 11 3/4" 4.98	3 7/8 0.32	5/8 .05	
1+50	4" 0.33	4' 11 7/8" 4.99	4 1/8 0.34	3/4 .06	
1+40	4" 0.33	4' 11 3/4" 4.98	4 1/4 0.35	1/8 .01	
1+30	3 7/8 0.32	4' 11 1/2" 4.96	3 7/8 0.32	3/8 .03	
1+20	3 7/8 0.32	4' 11 3/4" 4.98	4 0.33	5/8 .05	
1+10	4" 0.33	4' 11 7/8" 4.99	4 1/8 0.34	3/4 .06	
1+06 5' =	E. line drive 0.30	3 5/8 4.97	4 0.33	5/8 .05	
0+98 5' =	W. line drive 0.31	3 3/4 4.97	4 0.33	1/4 .02	
0+90		3 3/4 0.31	4' 11 3/4" 4.98	4 0.33	1/4 .02
0+80		3 7/8 0.32	4' 11 5/8" 4.97	4 0.30	1/4 .04

Sidewalks South side Beryl

Sta.	Thickness Lt. Edge	width	Thickness Rt. edge	Rise to back.		Thickness Lt. Edge	width	thickness Rt. Edge	Rise to back ^②
					3+50	3 3/4"	4' 11 1/8"	3 3/4"	1" ²
						0.31	4.92	0.31	.08
2+50	3 7/8"	4' 11 1/2"	3 1/8"	3/8	3+40	4 1/8"	4' 11 7/8"	4 1/8"	1"
	0.32	4.96	0.32	.03		0.34	4.95	0.34	.08
2+40	3 7/8"	4' 11 1/2"	4"	1/2	3+30	4"	4' 11 1/2"	4"	1"
	0.32	4.96	0.33	.01		0.33	4.96	0.33	.08
2+30	3 5/8"	4' 11 1/2"	3 7/8"	1/2	3+20	4 3/8"	4' 11 1/2"	4"	1"
	0.30	4.96	0.32	.04		0.36	4.96	0.33	.08
2+20	3 7/8"	4' 11 3/4"	4 1/4"	1/4	3+10	4"	4"	4"	3/4"
	0.32	4.98	0.35	.02		0.33	5.00	0.33	.06
2+10	3 5/8"	4' 11 3/4"	4"	5/8	3+00	4"	4"	4"	1"
	0.30	4.98	0.33	.05		0.33	5.00	0.33	.08
1+96 E Drive	3 7/8"	5	3 1/8"	5/8	2+90	4 1/8"	4"	4"	5/8"
	0.32	5.00	0.32	.05		0.34	5.00	0.33	.05
1+88 W. Edge drive	3 7/8"		4"	5/8	2+80	4 1/4"	4 1/8"	4 1/8"	7/8"
	0.32	5.00	0.33	.05		0.35	5.00	0.34	.07
1+80	3 7/8"		4"	1/8	2+70	4"	4' 11 5/8"	4"	7/8"
	0.32	5.00	0.33	.07		0.33	4.97	0.33	.07
1+70	3 3/4"		3 3/4"	1/2	2+60	3 3/4"	4' 11 3/8"	3 7/8"	1 1/8"
	0.31	5.00	0.31	.04		0.31	4.95	0.32	.09

Sidewalks South side

	thickness lt. edge	width	Beryl thickness Rt. edge	Rise to back
4+50	3 7/8" 0.32	4' 11 5/8" 4.97	3 7/8 0.32	3/4" .06
4+41 E. line drive	3 5/8" 0.30	4' 11 5/8" 4.97	3 3/4 0.31	5/8" .05
4+33 W. line drive	3 3/4 0.31	4' 11 5/8" 4.97	3 3/4 0.31	3/4" .06
4+20	3 3/4 0.31	4' 11 5/8" 4.97	4 0.33	1" .08
4+10	3 3/4 0.31	4' 11 1/2" 4.96	3 3/4 0.31	7/8" .07
4+00	4 0.33	4' 11 1/2" 4.96	4 0.33	1" .08
3+91 E. line drive	4 0.32	4' 11 5/8" 4.97	4 0.33	7/8" .07
3+83 W. line drive	3 5/8 0.30	4' 11 1/2" 4.96	3 5/8 0.30	1 1/4" .10
3+70	3 3/4 0.31	4' 11 1/2" 4.96	3 1/8 0.32	7/8" .07
3+60	3 1/8 0.32	4' 11 1/2" 4.96	4 1/8 0.34	1 1/8" .09



4+98 B.C. walk at Return	3 3/4 0.31	4' 11 3/4" 4.98	4 1/4 0.35	7/8 .01
4+90	4 0.33	5' 00" 5.00	4 1/8 0.34	5/8 .05
4+80	3 1/2 0.29	4' 11 5/8" 4.97	3 5/8 0.30	5/8 .05
4+70	3 5/8 0.30	4' 11 5/8" 4.97	3 3/4 0.31	3/4 .06
4+60	3 1/8 0.32	4' 11 5/8" 4.97	4 0.33	3/4 .06

Sidewalks. S. Side Beryl

		thickness Lt. Edge	width	thickness Rt. Edge	Rise		Thickness Lt. Edge	width	Thickness Rt. Edge	Rise [Ⓢ] to back
4	0+90	3 3/4" 0.31	4-11 3/4" 4.98	3 7/8" 0.32	1" .08	1+90	4 1/8" 0.34	5.00	4 1/4" 0.35	4 7/8" .07
4	0+80	3 7/8" 0.32	4-11 3/8" 4.95	3 7/8" 0.32	7/8" .07	1+80	3 3/4" 0.31	4-11 1/2" 4.96	4" 0.33	1" .08
4	0+70	3 5/8" 0.30	4-11 3/8" 4.95	4" 0.33	3/4" .06	1+70	3 7/8" 0.32	4-11 3/4" 4.98	3 7/8" 0.32	1" .08
4	0+60	3 1/2" 0.29	4-11 5/8" 4.97	3 1/2" 0.29	1" .08	1+60	4" 0.33	4-11 1/2" 4.96	3 7/8" 0.32	1" .08
4	0+50	3 1/2" 0.29	4-11 7/8" 4.99	3 7/8" 0.32	3/4" .06	1+50	4 1/4" 0.35	4-11 3/8" 4.95	4 1/8" 0.34	1" .08
4	0+40	3 1/2" 0.29	4-11 5/8" 4.97	4" 0.33	3/4" .06	1+40	3 3/8" 0.28	4-10 3/4" 4.90	3 7/8" 0.32	5/8" .05
3	0+30	3 3/4" 0.31	4-11 5/8" 4.97	4" 0.33	7/8" .07	1+30	4 1/8" 0.34	4-11 1/2" 4.96	4" 0.33	1" .08
3	0+20	3 7/8" 0.32	4-11 5/8" 4.97	4" 0.33	3/4" .06	1+20	3 3/8" 0.28	4-11 3/4" 4.98	4" 0.33	1 1/4" .10
3	0+10	4" 0.33	5.00	4" 0.33	3/4" .06	1+10	3 7/8" 0.32	4-11 1/2" 4.96	3 7/8" 0.32	1 1/2" .12
3	0+00: E. line Dawes	4" 0.33	4-11 3/4" 4.98	3 7/8" 0.32	7/8" .07	1+00	3 7/8" 0.32	4-11 3/8" 4.95	3 7/8" 0.32	1 1/8" .09

	South Side Beryl		Thickness	Rise
	Thickness N. Edge	Width	S. Edge	
2+90	3 7/8" 0.32	4' 11 3/8" 4.97	4" 0.33	7/8 .07
2+80	3 7/8" 0.32	4' 11 3/4" 4.98	4 1/4" 0.35	5/8 .05
2+70	4 1/2" 0.37	4' 11 1/2" 4.96	4 1/8" 0.34	5/8 .05
2+60	4 3/8" 0.36	4' 11 1/2" 4.96	4 1/4" 0.35	1 1/4 .10
2+50	4 1/8" 0.34	4' 11 1/2" 4.98	3 7/8 0.32	1/2 .04
2+40	5" 0.42	4' 11 1/2" 4.96	4 1/4 0.35	3/4 .06
2+30 on N. Edge 2+28 on S. Edge	4 9/8" 0.38	4' 11 1/2" 4.96	4 1/4 0.35	7/8 .07
2+20	4" 0.33	4' 11 3/4" 4.98	3 7/8 0.32	5/8 .05
2+10	3 7/8" 0.32	5.00	3 7/8 0.32	5/8 .05
2+00	4 1/8" 0.34	4' 11 5/8" 4.95	4 3/8 0.36	5/8 .05

	Thickness	Width	Thickness	Rise
	N. Edge		S. Edge	
3+80	3 3/4 0.31	4' 11 1/2" 4.96	4 1/4 0.35	5 5/8 .05
3+70	4 0.33	4' 11 5/8" 4.97	3 7/8 0.32	4/8 .06
3+60	4 0.33	4' 11 5/8" 4.97	4 0.33	3/8 .03
3+50	4 0.33	4' 11 3/4" 4.98	4 0.33	1/4 .02
at. drive 3+45	4 0.33	4' 11 3/8" 4.95	4 0.33	3/8 .03
at. Drive 3+36	4 1/8 0.35	4' 11 7/8" 4.99	3 7/8 0.32	3/8 .03
3+30	4 0.33	5.00	3 3/4 0.31	3/8 .03
3+20	4 1/8 0.34	4' 11 3/8" 4.95	4 1/8 0.34	1/2 .04
3+10	4 1/8 0.34	4' 11 1/4" 4.94	3 7/8 0.32	5/8 .05
3+00	4 1/2 0.37	4' 11 1/4" 4.94	3 1/4 0.35	3/4 .06

Sidewalks South side Beryl.

Thickness N. Edge Width Thickness S. Edge Rise to back

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End. Job	Thickness N. Edge	Width	Thickness S. Edge	Rise to back
4+14±	4"	5.00	4"	3/8
	0.33		0.33	.03
4+10	3 7/8	4' 11 1/2"	4"	1/4
	0.32	4.96	3.3	.02
4+00	4	4' 11 1/2"	4"	3/8
	0.33	4.96	0.33	.03
3+90	4	4' 11 1/2"	4"	1/2
	0.33	4.96	0.33	.04

Sidewalk check North side Beryl.

Thickness N. Edge Width Thickness S. Edge Rise to back

	Thickness N. Edge	Width	Thickness S. Edge	Rise to back
0+90	3 5/8	4' 10 7/8"	3 3/4	6 7/8
	0.30	4.91	0.31	.07
0+80	4 1/8	4' 11 1/4"	4	1/4
	0.34	4.94	0.33	.02
0+70	3 3/4	4' 11 5/8"	3 7/8	1/4
	0.31	4.97	0.32	.02
0+60	3 3/4	4' 11 7/8"	4	1"
	0.31	4.99	0.33	.08
0+50	3 7/8		3"	3/4
	0.32	5.00	0.25	.06
0+40	3 1/2	4' 11 1/2"	3 3/4	1/2
	0.29	4.96	0.31	.04
0+30	3 7/8		4	1 1/2"
	0.32	5.00	0.33	.12
0+20	3 7/8		3 3/4	1 7/8"
	0.32	5.00	0.31	.15
0+10	3 3/4	4' 11 3/4"	3 3/4	1 7/8"
	0.31	4.98	0.31	.15
0+00 = E. line Cass	4 1/2	5' 5 3/8"	4	2 1/8"
	0.37	5.05	0.33	.17

Side walk	Check		North side		of Beryl		Thickness		Thickness		⑦ Rise
	thickness N. Edge	Width	Thickness S. Edge	Rise	Thickness N. Edge	Width	Thickness S. Edge	Rise			
1+90	3 1/2" 0.129	4' 11" 4.92	3 3/4 0.31	3/8 .03	2+90	4 1/8 0.34	4' 11 3/8" 4.95	4 1/8 0.35	7 5/8 .05		
1+80	4 0.33	4' 11" 4.92	4 1/8 0.34	1/8 .01	2+80	3 7/8 0.32	4' 11 1/2" 4.96	4 3/4 0.39	1/4 .02		
1+70	4 1/8 0.34	4' 11 1/8" 4.93	3 7/8 0.32	0 .00	2+70	4 0.33	4' 11 1/2" 4.96	4 1/4 0.35	-1/8 -.01		
1+60	4 1/8 0.34	4' 11" 4.92	4 0.33	1/8 .01	2+60	4 0.33	4' 11 1/2" 4.96	4 1/8 0.34	1/8 .01		
1+50	4 1/8 0.34	4' 10 3/4" 4.90	4 0.32	1/8 .01	2+50	4 1/8 0.34	4' 11 1/2" 4.96	4 0.33	1/2 .04		
1+40	4 1/4 0.35	4' 11 1/2" 4.96	3 5/8 0.30	-1/8 -.01	2+40	4 0.33	4' 11 1/4" 4.94	4 1/8 0.34	1/2 .04		
1+30	3 5/8 0.30	4' 11 3/8" 4.95	3 3/4 0.31	3/8 .03	2+30	4 1/4 0.35	4' 11" 4.92	4 1/4 0.35	1/4 .02		
1+20	3 7/8 0.32	4' 11 1/2" 4.96	3 7/8 0.32	1/2 .04	Driveway 2+215	3 7/8 0.32	4' 11 1/4" 4.94	4 0.33	3/4 .06		
1+10	3 3/4 0.31	4' 11 3/8" 4.95	3 3/4 0.31	3/8 .03	2+10	3 7/8 0.32	4' 11 1/8" 4.93	3 7/8 0.32	5/8 .05		
1+00	4 1/8 0.34	4' 11 3/8" 4.95	4 3/8 0.36	3/4 .06	2+00	4 0.33	4' 11 3/8" 4.95	4 0.33	1/2 .04		

	Sidewalk check.		North		
	Thickness N. Edge	Width	Thickness S. Edge	Rise	
3+90	4 0.33	4'11 1/2" 4.96	3 7/8 0.32	1/2 .04	
3+80	4 1/8 0.34	4'11 3/8" 4.95	4 1/2 0.37	5/8 .05	
3+70	4 0.33	4'11 5/8" 4.97	4 5/8 0.38	3/8 .03	
3+60	4 1/4 0.35	4'11 1/2" 4.96	4 1/8 0.34	5/8 .05	
3+50	4 0.33	4'11 1/2" 4.96	4 1/4 0.35	3/8 .03	
3+40	3 7/8 0.32	4'11 3/4" 4.98	3 5/8 0.30	1/2 .04	
3+30	4 1/8 0.34	4'11 5/8" 4.97	4 3/8 0.36	5/8 .05	
3+20	4 0.33	4'11 5/8" 4.97	4 1/8 0.34	1/2 .04	
3+10	4 0.33	4'11 5/8" 4.97	3 7/8 0.32	7/8 .07	
3+00	4 1/8 0.34	4'11 3/4" 4.98	4 0.33	3/4 .06	

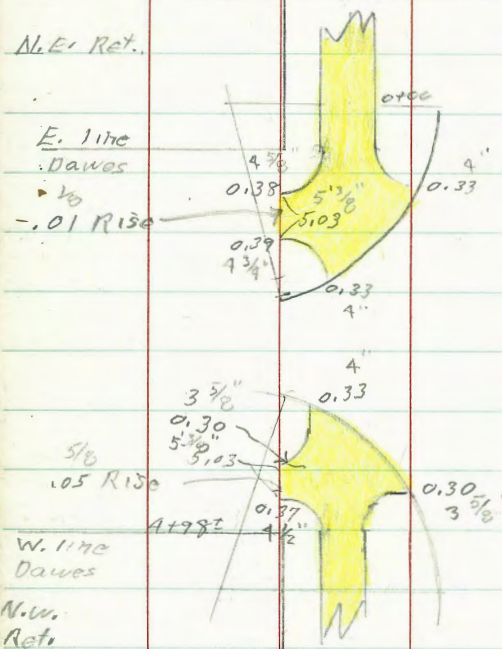
	Side of Beryl				(8)
	Thickness N. Edge	Width	Thickness S. Edge	Rise to back	
4+80	4 1/2 0.37	4'11 3/8" 4.95	4 1/4 0.35	8 1/2 .04	
4+70	4 1/8 0.34	4'11 3/4" 4.98	4 0.33	1/2 .04	
4+60	4 1/8 0.34	4'11 3/4" 4.98	4 1/8 0.34	3/8 .03	
4+50	4 1/4 0.35	4'11 1/4" 4.94	4 1/4 0.35	1/2 .04	
At. Drive 4+46	4 1/4 0.35	4'11 3/8" 4.95	4 1/8 0.34	1/2 .04	
At. drive 4+37	4 3/8 0.36	4'11 3/4" 4.98	4 1/8 0.34	1/4 .02	
4+30	3 7/8 0.32	4'11 1/2" 4.96	4 0.33	1/2 .04	
4+20	4 1/4 0.35	4'11 1/2" 4.96	4 1/8 0.34	3/8 .03	
4+10	4 1/4 0.35	4'11 1/2" 4.96	4 1/8 0.34	1/8 .01	
4+00	4 0.33	4'11 7/8" 4.99	4 1/8 0.34	1/4 .02	

Sidewalk Check

North

Side of Beryl

9



	Thickness N. Edge	width	Thickness S. Edge	
W. line Daves A+98t	4 1/2"	5.00	4 1/8"	3/8"
	0.31		0.34	.03
A+90	4 1/4"	5.00	3 3/4"	5/8"
	0.35		0.31	.05

	Thickness N. Edge	Width	Thickness S. Edge	Rise
A+ Drive 0186	4 1/4"	4' 11 3/4"	4"	1/2
	0.35	4.98	0.33	.04
0180	3 7/8"	4' 11 3/4"	4"	1/2
	0.32	4.98	0.33	.04
0170	4"	4' 11 3/4"	4"	1"
	0.33	4.98	0.33	.08
0160	3 7/8"	5.00	4"	5/8"
	0.32	5.00	0.33	.05
0150	4 1/2"	4' 11 7/8"	4"	5/8"
	0.34	4.99	0.33	.05
0140	4"	4' 11 7/8"	4"	5/8"
	0.33	4.99	0.33	.05
0130	4 1/4"	4' 11 3/4"	3 7/8"	5/8"
	0.35	4.98	0.32	.05
0120	4"	4' 11 5/8"	4"	5/8"
	0.33	4.97	0.33	.05
0110	3 7/8"	4' 11 1/4"	4"	1/2"
	0.32	4.94	0.33	.04
0100 = E. line Daves	4 1/4"	4' 11 3/4"	4 1/4"	5/8"
	0.35	4.98	0.35	.05

Sidewalk Check				North Side of Beryl				(10)			
	Thickness N. Edge	Width	Thickness S. Edge	Rise		Thickness N. Edge	Width	Thickness S. Edge	Rise		
1+80	4" 0.33	4' 11 3/4 4.98	4 1/4 0.35	3/4 .06	2+80	4 1/8 0.34	5.00	3 7/8 0.32	10 3/4 .06		
1+70	4 1/4 0.35	4' 11 7/8 4.99	4 0.33	1/2 .04	2+70	4 0.33	4' 11 5/8 4.97	3 7/8 0.32	1 .08		
at Drive 1+625	4 0.33	5.00	4 1/8 0.35	5/8 .05	2+60	4 1/4 0.35	4' 11 3/4 4.98	3 7/8 0.32	5/8 .05		
at Drive 1+55	4 1/8 0.34	4' 11 7/8 4.99	4 0.33	1 .08	2+50	4 0.33	4' 11 1/2 4.96	3 7/8 0.32	7/8 .07		
1+50	4 0.33	5.00	4 9/8 0.38	1 .08	2+40	4 1/4 0.35	4' 11 5/8 4.97	3 7/8 0.32	3/4 .06		
1+40	4 0.33	5.00	4 0.33	3/4 .06	2+30	4 0.33	4' 11 5/8 4.97	4 0.33	7/8 .07		
1+30	3 7/8 0.32	4' 11 3/4 4.98	4 0.33	5/8 .05	2+20	4 0.33	4' 11 3/4 4.98	4 0.33	7/8 .07		
1+20	4 0.33	4' 11 3/4 4.98	4 0.33	7/8 .07	2+10	4 0.33	4' 11 3/4 4.98	4 0.33	3/4 .06		
at Drive 1+08	4 3/4 0.39	4' 11 3/4 4.98	4 0.33	7/8 .07	2+00	4 1/4 0.35	4' 11 7/8 4.99	4 1/8 0.34	1/2 .04		
1+00	4 5/8 0.38	4' 11 3/4 4.98	in Drive	5/8 .05	1+90	4 1/8 0.34	4' 11 3/4 4.98	4 0.33	5/8 .05		

Sidewalk Check

North side of Beryl

(11)

	Thickness N. Edge	Width	Thickness S. Edge	Rise
3+80	4 1/8 0.34	5.00	4 0.33	3/4 .06
3+70	4 0.33	4' 11 7/8" 4.99	4 0.33	7/8 .07
3+60	4 0.33	4' 11 3/4" 4.98	4 0.33	5/8 .05
3+50	4 0.33	5.00	3 7/8 0.32	5/8 .05
3+40	4 0.33	4' 11 1/2" 4.96	4 1/8 0.34	5/8 .05
3+30	4 0.33	4' 11 5/8" 4.97	4 0.33	3/4 .06
3+20	3 7/8 0.32	4' 11 3/4" 4.98	4 0.33	1/2 .04
3+10	4 0.33	4' 11 3/4" 4.98	4 0.33	3/4 .06
3+00	3 7/8 0.32	4' 11 5/8" 4.97	3 7/8 0.32	3/4 .06
2+90	3 7/8 0.32	4' 11 7/8" 4.99	3 7/8 0.32	1/2 .04

End. of
Job.

4+14±

4+10

4+00

3+90

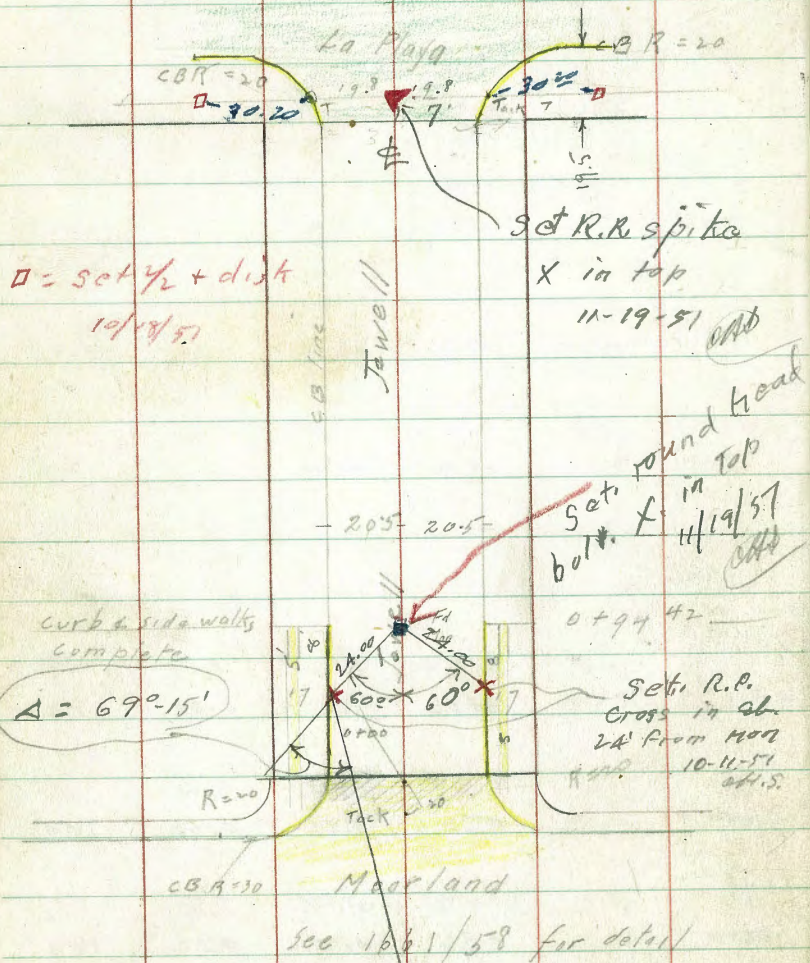
Thickness N. side	Width	Thickness S. side	Rise
3 7/8	5.00	4	3/4
3 7/8	4' 11 7/8" 4.99	3 7/8	3/4
3 7/8	4' 11 5/8" 4.97	3 7/8	1/2
3 7/8	5.00	3 7/8	3/8

11

X section

Jewell
Moorland to La Playa
W0 25001

INDEXED



NW.BP

4+7.0 Moorland Dr
33.86 BA
should be 33.68

Begg
Sherman
Burch

22/7/48
Plotted
TPS 1273-1276
1-24-52-MQ

12

12

~~Indexed~~
B

See P. 65 for New Sections

checked

Ingraham & Moorland 1661 /58

1+00 ✓

+ 94.42 ✓

0+82 = ± 15' Dr. back of walk to Doub. qgr.
Has been going over cb. - will need Dr.

+ 75

+ 50

Dirt in Roadway has been changed
Will take new sections
See P. 65

0+25

Notes: New Notes are act. Elev.

0+00²

edge of exist pav

234.06 ?
± 500.65
23.88 = Right Elev.

Set B.M. on web at P.C.

TP 2.29 29.53 7.91 27.24

1.29 25.15 33.86 B.M.

Note: The Hundreds in this 33.68 = True elev.
Elev. where Transposed - everything should be .18 lower.

	LT		RT	
25.2	24.7	23.6	23.6	24.0
4.3	4.8	5.9	5.9	5.5
37.5	20.5	6	6	20.5

1313

	LT		RT	
4.4	24.40	24.1	23.9	23.4
37.5	5.13	5.4	5.6	6.1
	CB	9	10	10
	end	20.5		20.5

	LT		RT	
	24.35	23.7	23.1	23.0
	5.18	5.8	6.4	6.5
	CB	9		9

	LT		RT	
	24.27	23.7	23.0	23.1
	5.26	5.8	6.5	6.4
	CB			7

	LT		RT	
	24.18	23.5	22.8	22.7
	5.35	6.0	6.7	6.8
	CB	9		9

	LT		RT	
	24.09	23.55	23.47	22.68
	5.44	5.98	6.06	6.85
	51	9		20.5
	20.5			9

Note: for checking - used wrong Elev. as shown here - every thing is 1.8 High - including New shots.

checked - 10-26-50
7.0.

Pencil check = Sect. o.k.
Red check = changes
See new Sect.

3+50

3+08 34.7 RT side walk 2.5 wide

3+00

+53 226A P Poleo P 3745

2+50

2+00

1+64 - 37.7 Lt. 4' 8' Conc. Dr.

1+50

29.53

25.55
61
floor.

Lt.

±

Rt.

14

14

25.1	25.3	25.0	24.8	25.2	25.7	25.6	25.7
4.4	4.2	4.5	4.7	4.3	3.8	3.9	3.8
37.5	20.5	8		8	20.5	37.5	50

25.51

4.02
34.7

25.0	25.0	25.2	25.1	24.6	24.5	25.0	25.6	25.2
4.5	4.5	4.3	4.4	4.9	5.0	4.5	4.5	4.7
50	37.5	20.5	7	6		6	20.5	37.5

25.1	25.0	25.0	25.1	24.6	24.3	25.0	25.0	24.9	24.9
4.4	4.5	4.5	4.4	4.9	5.2	4.5	4.5	4.6	4.6
50	37.5	20.5	7	6		6	20.5	37.5	50

25.2	24.9	25.3	24.3	24.1	24.9	24.7	24.7
4.3	4.6	4.2	5.2	5.4	4.6	4.8	4.8
37.5	20.5	8	6		6	20.5	37.5

25.16 Elev. - (not rod.)
Dr. 37.7

24.9	25.0	24.8	24.1	24.4	24.4	24.3
4.6	4.5	4.7	5.4	4.7	5.1	5.2
37.5	20.5	10		37.5	20.5	37.5

29.53

+53 37.5 ft beg fence lath ✓

~~+53 22 ft beg fence 24" out~~

5+50

5+00

+93 38 ~~ft~~ ^{RT.} 8 Wide apron in process of construction

+54 Pole P3765 ✓ 23 ft

~~4+50 Beg wire fence 24" out~~

T.P. 6.11 30.90 4.74 24.79

4+00

29.53

26.0	26.1	25.9	26.1	26.3
4.9	4.8	5.0	4.8	4.6
37.5	20.5		20.5	37.5

25.9	25.5	25.6	26.1	26.6
5.0	5.4	5.3	4.8	4.3
20.5	10		20.5	37.5

27.27
3.63
38

25.8	25.4	25.1	25.7	26.0	25.9	25.9
5.1	5.5	5.8	5.2	4.9	5.0	5.0
37.5	20.5	2		20.5	37.5	50

30.90

25.3	25.5	25.1	25.5	25.0	25.2	25.8	25.6	25.5	25.5
4.0	4.0	4.4	4.0	4.5	4.3	3.7	3.9	4.0	4.0
50	37.5	20.5	11	9		6	20.5	37.5	50

29.53

+35

25.5	25.7	24.9	25.2	25.40	26.0	26.5
5.4	5.2	6.0	5.7	5.5	4.9	4.4
37.5	20.5	6		6	20	37.5

+25

25.8	25.9	25.4	25.7	26.1	26.4	26.6
5.1	5.0	5.5	5.2	4.4	4.5	4.3
37.5	20.5	6		6	20.5	37.5

+03 37.5 19 end koth fence ✓

6+00

26.0	26.0	25.4	25.6	26.2	26.5	26.8
4.9	4.9	5.5	5.3	4.7	4.4	4.1
37.5	20.5	6		6	20.5	37.5

~~6+00 22.0 12" Pepper~~

+98 28.5 R 12" Olive

~~+84 22.3 11 10" Pepper~~

+84 28.3 R 6" Olive

+71 27.6 R 6" Olive ✓

~~+68 22.4 12" Pepper~~

+66 22.4 RT Pole 460963 H JP3744

5+59 27 RT 24" Olive ✓

30.90
~~29.53~~30.90
~~29.53~~

0 +75 N Prop La Playa

0 +~~33~~ 56 CB line La Playa

90 + 37.5 La Playa

Prop + 19.5 curb line La Playa

0 + 00
6 + 53 ~~32~~ paving. 5 line La Playa

+ 50

+ 45

30.90

17 17

23.21	22.72	23.20	22.70	23.20
7.69	8.18	7.70	8.20	7.70
CB	18		3/8	CB
23.27	22.86	23.13	22.78	23.26
7.63	8.04	7.77	8.12	7.64
CB	37.5			CB

23.15	23.05	22.20
7.75	7.85	7.70
37.5		37.5

23.24	22.78	22.84	23.05	22.85	22.61	23.20
7.66	8.12	8.06	7.85	8.05	8.19	7.70
CB	9	20		20	9	CB
BC	40					38
						BC CB

23.30	22.84	22.88	22.68	23.16
7.60	8.06	8.02	8.22	7.74
CB	18	9	9	18
CB				CB
				CB

25.1	25.3	23.6	23.3	23.5	23.3	24.9	25.7	25.8
5.8	5.6	7.7	7.6	7.4	7.6	6.0	5.2	5.1
37.5	21	18	9		18	25	30	37.5

25.2	25.5	24.5	24.1	24.0	23.7	24.9	26.6
5.7	5.4	6.4	6.8	6.9	7.2	6.0	4.3
37.5	20.5	14	10		15	20.5	37.5

30.90

		4.73	26.46	26.44 ^{0/2}
p. 31	31.19	1.40	28.88	
TP	7.35	30.28	7.97	22.93
	<u>30.90</u>			

(Bench book) La Playa & Ingraham
lead & Tack $\frac{1}{2}$

Replace Lot Stakes Lot 72
Gilcher Tract.

Roberts
W. Moore
J. Clark
4-27-49
W.O. 21001

Map 3280-B, 3461-B, 1829 J.T. 3787

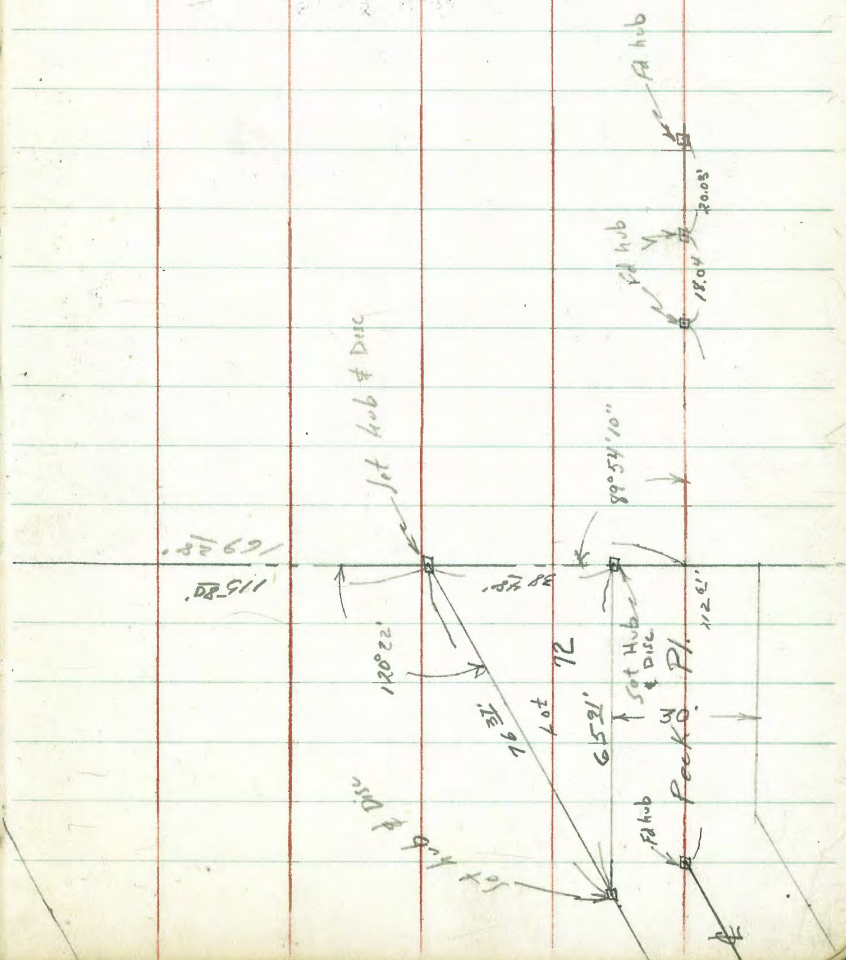
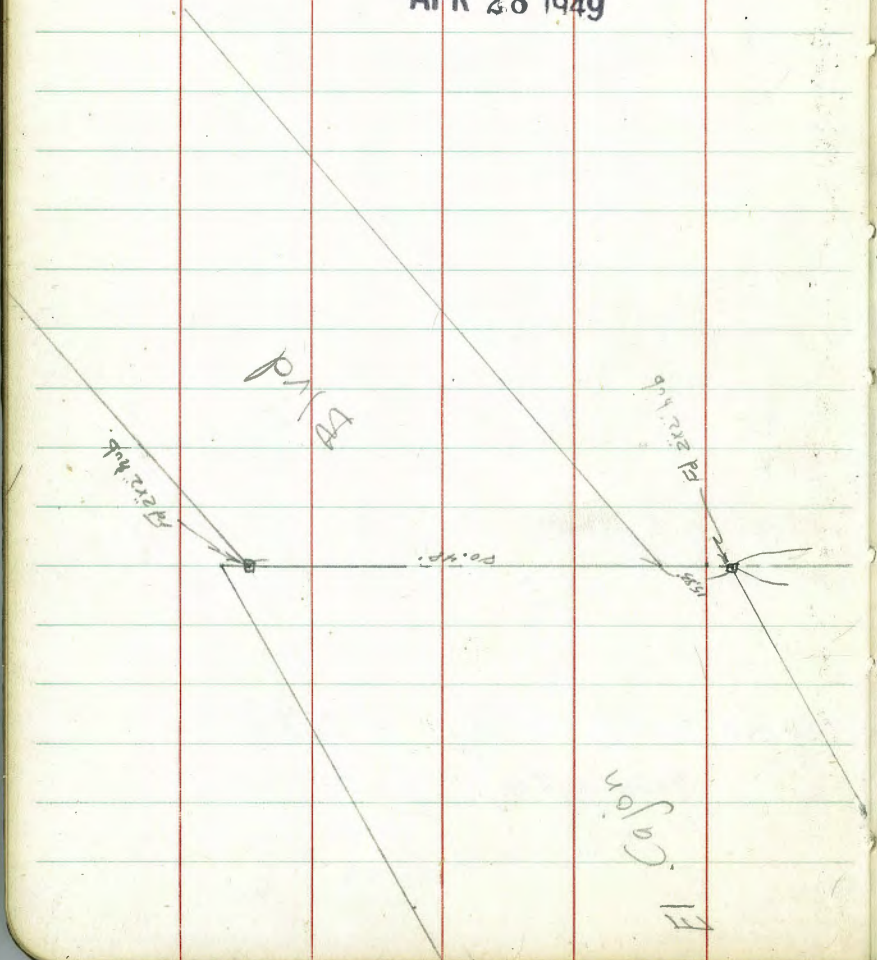
FB 1691, 1826

INDEXED

WK

APR 28 1949

19¹⁹



Re. X section Alley R/R/F
Alta Vista Suburb

D Smith
W Moore
J Clark

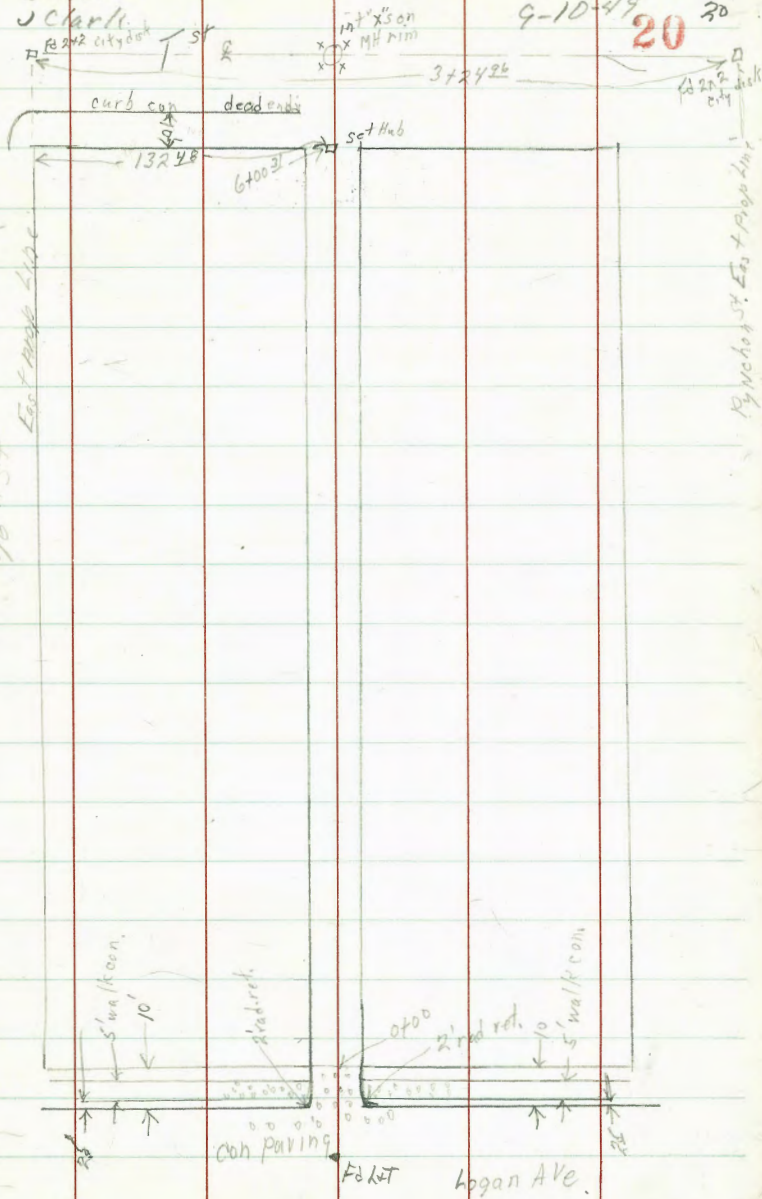
W.O. 95001
9-10-49 20

INDEXED
WK
MAY 11 1949

notes Transcribed
McClaren 6/9/49

notes Recorded
Green Profile 3376
McClaren
6/9/49

46th St East Prop Line



Re X section Alley
 Blk "F" Between 46th & Pynchon

Loganto Tst West East
 Lt Rt **21** 21

0+50 6³ Lt & power pole #177224

0+30

0+28 6³ Lt & Anchor dead man

0+45 101^S Lt R 18" cor pipe drain + 6¹/₂ long slide on headwall
 pipe runs N+S

0+00 W prop Logan Ave c&g con paving

0-10 North side

0-30 E Logan Ave

BM H 94 112⁴⁸

10757 ct E Alley
 + E Logan Ave
 FB 1727-29

101.85
 105.92
 106.94
 106.94
 105.92
 106.94

103.1
 102.5
 104.2
 107.4
 107.6
 107.1
 107.5
 108.3

102.26
 105.20
 102.8
 105.2
 107.6
 107.2
 107.6
 108.8

106.1
 106.9
 107.38
 107.63
 107.01
 107.13
 107.32
 107.78
 108.2
 108.7

106.12
 105.68
 106.77
 106.21
 107.40
 106.95
 107.01
 107.21
 107.70
 107.85
 108.42

106.69
 107.54
 108.28

112⁴⁸

cont

1730

1720

8² RT Ebd 4' cyclon fence

TP,

6⁵²

114¹²

4²²

107⁵⁰

1700

8⁶ Lt begin 4 1/2' board fence

1700

8² RT begin 4' cyclon fence

0796

9⁶ Lt NE cor forms for con. under clothes line

0780

0770

23' SE cor house 26' along line

9⁶ Lt SE cor forms for con. under clothes line

0755

LT

R

RT

22 22

106.0

82

75

105.7

84

50

106.4

72

75

106.6

75

75

107.6

65

75

108.1

60

50

114¹²

105.3

72

100

104.7

75

70

105.1

70

25

105.8

62

75

106.1

64

25

106.9

58

25

108.0

45

50

105.4

72

23

105.76

67

95

105.1

64

25

105.6

69

75

105.9

65

75

108.0

45

50

105.84

64

25

105.1

67

25

105.0

75

100

103.6

52

70

104.6

72

50

104.9

75

25

106.7

52

75

106.7

52

25

106.7

52

25

107.9

45

50

112⁴⁸

cont

3+25

3+00

6th Lt E power pole # JPA R78035

3+00

8th Lt End 5' board rail fence

2+50

8th Lt begin 5' board rail fence

2+50

7th Lt end 4 1/2 wire fence

2+00

7th Lt begin 4 1/2 wire fence

1+77

6th Lt E anchor deadman

1+60

1+50

7th Lt E power pole # JPA R75557

1+48

8th Lt End 4 1/2 board fence

RT
 109.4
 92 82 70 60 52 56 60 70
 86 50 42 78 75 75 50 85

105.1
 92 68 42 47 42 48 54 66 62
 100 50 75 75 75 50 67 68 100

105.3
 88 76 64 48 48 45 42 45 54
 100 75 50 75 75 75 30 50 80 75 street

105.0
 92 73 72 62 60 58 58 54 70 52
 77 76 50 75 75 75 50 80 110 135

105.0
 92 82 74 62 65 64
 75 50 75 75 75 80

114.18

23²³

cont

5706

5700

4450 6² LT & power pole # JPA 298036

4425

4400

3775

3750

100	72	74	62	42	12
50	75	75	75	15	50
104.1	106.4	107.0	107.9	109.5	112.7

24 24

102.0	103.8	106.1	106.5	107.1	108.7	110.0
122	102	80	76	70	52	41
100	50	75	75	75	25	50

100.6	102.1	103.2	103.8	104.3	104.9	105.9
135	120	108	103	98	92	82
90	50	75	75	75	25	50

100.9	101.8	102.7	102.9	103.3	104.0	104.9
132	123	114	112	108	101	92
80	50	75	75	75	25	50

102.7	103.4	103.2	103.4	103.6	103.6	104.9	107.0
115	102	102	102	105	105	92	72
90	50	75	75	75	17	50	100

103.0	104.2	104.6	104.5	104.1	104.7	105.8	106.4
114	92	95	95	100	94	82	72
55	50	75	75	75	50	70	85

103.6	104.8	105.1	104.9	105.4	106.0	106.0	106.9	105.9	106.6
105	93	92	92	82	82	72	82	82	72
90	50	37	25	75	75	40	55	55	90

11412

cont

Lt

E

Rt

25²⁵

67003

107.5	108.0	110.3	110.6	111.3	112.6	113.5	114.4
75	70	42	44	32	24	15	06
50	25	75		5	75	25	50

5799E

8² Rt End wire 4' fence also sta to apron

113.6	113.7	113.79
127	127	127

5796

12² Rt NW cor Rear garage 24' along line back

con floor apron opens on T¹ st

127	127
-----	-----

TP 8² Prop. on hub disk

520

115⁰⁰

432

109⁰⁰

107.4	108.4	110.3	111.0	111.3	111.5	113.9	114.1
67	57	38	32	28	25	02	00
50	30	77	75	2	75	12	25

577B

5752

8² Rt begin wire 4' fence

104.7	107.2	110.5	110.7	111.6	112.9	114.0
94	62	35	34	25	12	01
100	50	75		75	15	40

5750

5745

102.7	105.1	108.1	110.0	110.3	111.4	111.9	113.1
114	90	60	46	38	22	23	10
100	50	12	75	75	25	25	50

114¹²

cont.

Lt.

E

RT

26 26

BM

744

10756

ct & Alley +
2 Logan B/R #
10754 ✓

6730²¹ R "T" st

1039

114

80

1065

88

25

10855

6

1010111

1105

48

25

1125

25

50

6710²¹ S curb line "T" st 79²¹ to curb end no return

10484

1056

60

10

1091

60

26

10758

742

25

TC

1070

80

25

94

10894

600

75

94

1087

63

72

72

1095

5

5

72

1107

43

75

1121

22

25

50

1134

16

50

6708 70²¹ Lt & power pole # JPA 278865

115⁰⁰

Bird Rock Ave Pump. Sta.

W.O. 2019A
9-15-49

Sommermeyer
McCoy
Allen
Rorer

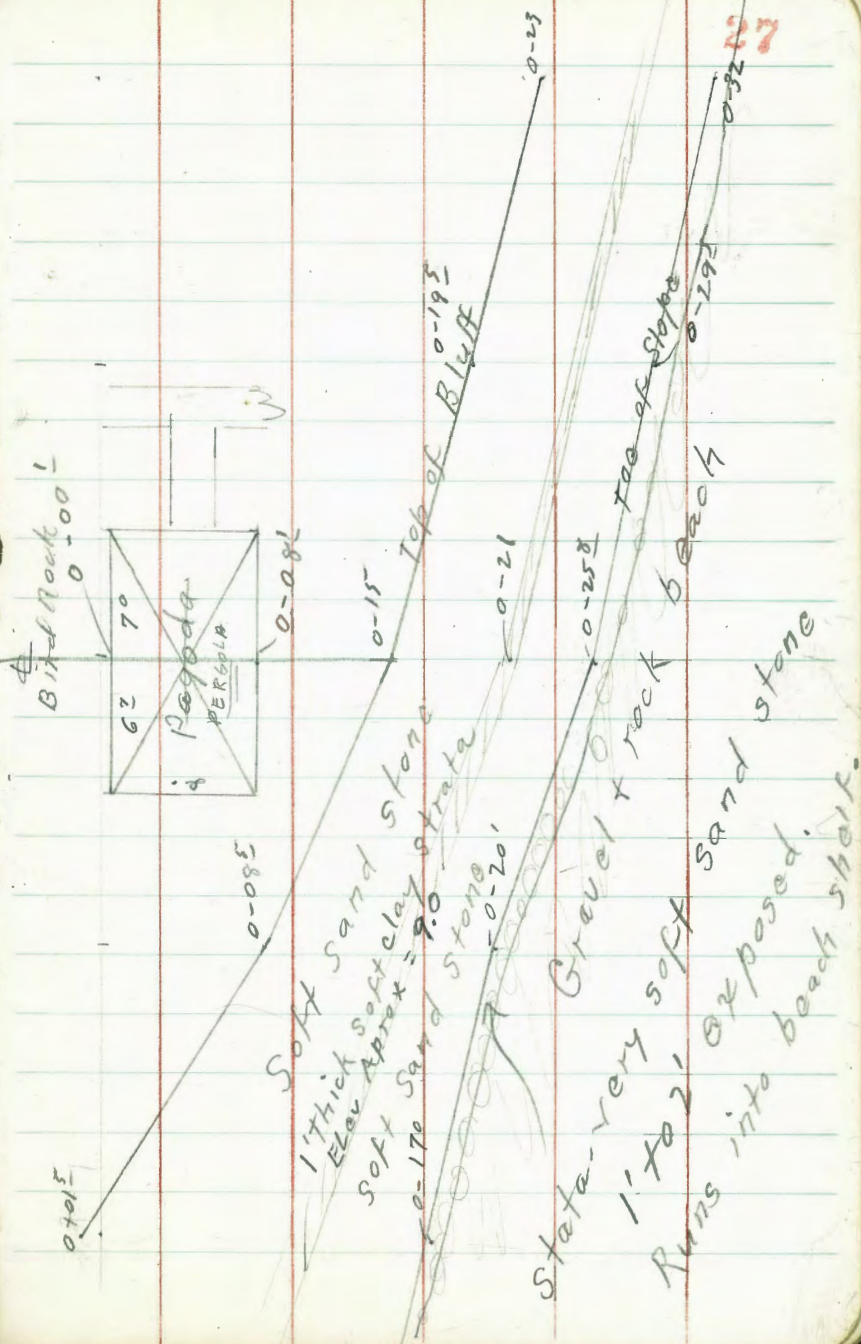
INDEXED

W.K.
SEP 16 1949

SEC FB 1646
38

Soft strata at sta. of 0-21
+ at 0-25⁸ run at approx same
elevation to north + south.

Balance of bluff is of
fairly soft sand stone,
bottom soil over burden
averages approx. 23.00' in
elevation.



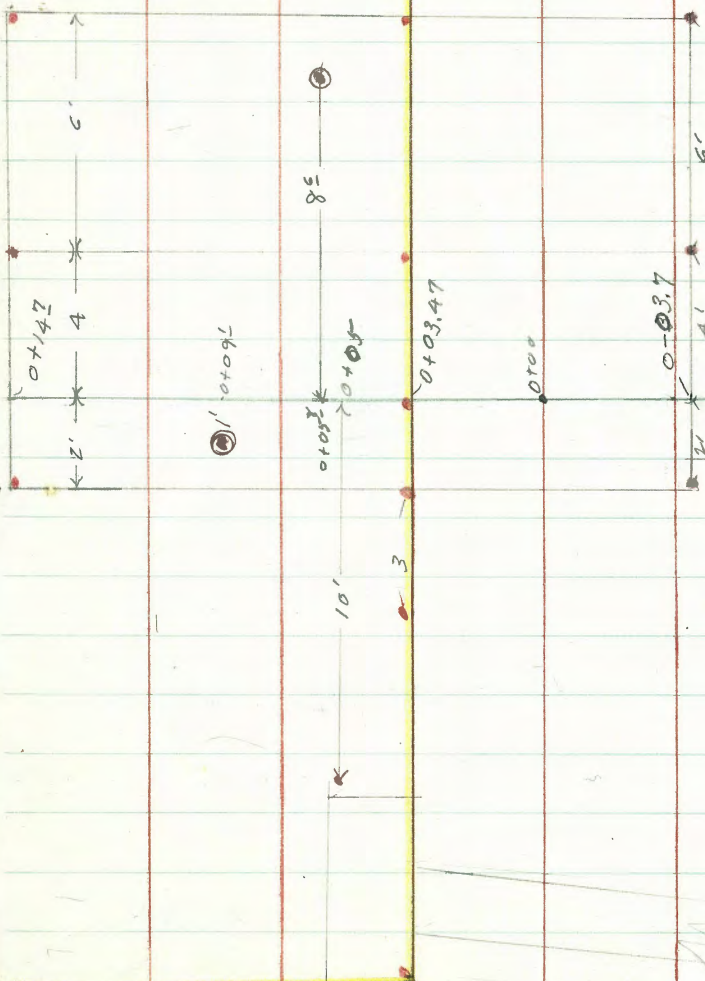
Bird Rock
Ave
Conn. P. 29



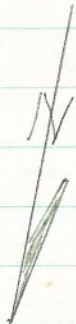
⊕ 2' → 0+299

⊕ 35' → 1' ⊕ 34' → ⊕
0+241

← 62' → 0+21' * 0+20.41' → 13' → ⊕



Bird Rock
Ave
Cont. P. 30



④ 0+574
074

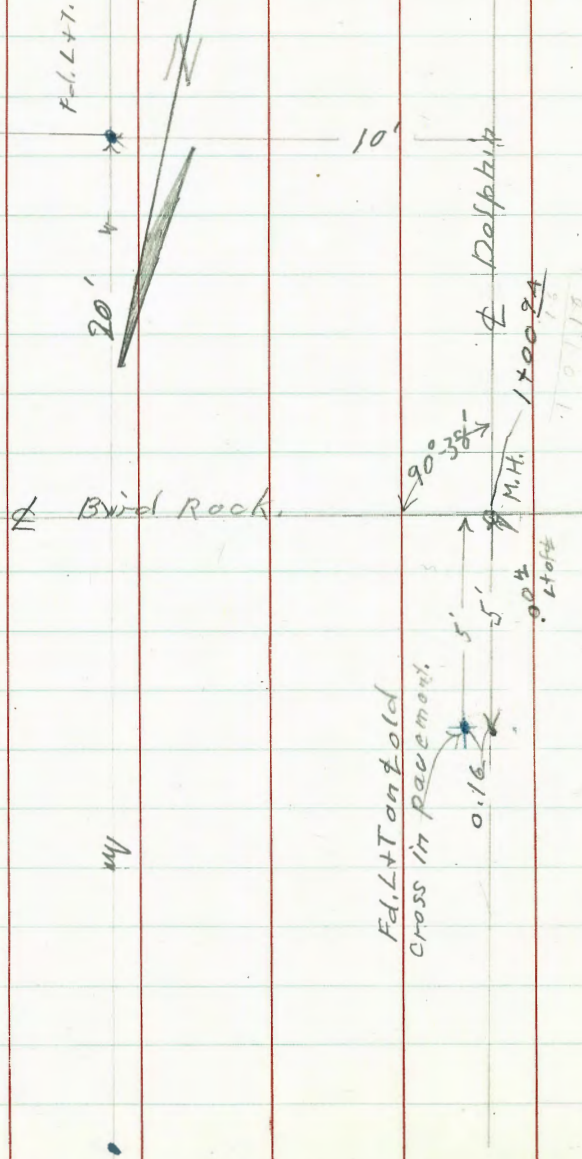
⑤ 1¹/₂ 0+53.7

0+392 x 1¹/₂ 1' Diam. cap, bolted down
8 Legs.

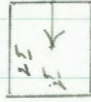
0+351 + 1¹/₂ ①

FROM P. 28

See tie sheet 1719 for tracts.



Gas Co.
Box.



10' → +0914

+087 ← 13'

174

+0805
From P. 29

176

30

Bird Rock Sewer Pump house

31

0-29³

2.4
15
T.S

0-30

13.1
30

0-32

2.5
30
T.S

0-35³ = \pm P.O.T. (on beach)

-2.00

T.S. = Toe of slope

to height of 2' to 3'

Toe of slope under cut about 2' in

could get.

20% grade for 30' or as far as we

Rocky beach slopes out at about

on P.O.T. 0-35³ (by stadia below 25.16) 27.16 -2.00

P.O.T. (0-13³) 6.68 25.16

SE. 10' L+T.
Dolphin
Bird Rock,

4.21 31.84 — 27.63

FB 1646
39

by hand level.
Above figures are elevations

31.84

0+012

$$\begin{array}{r} 24.9 \\ 30 \\ \hline \text{T.B.} \end{array}$$

0-08

$$\begin{array}{r} 24.5 \\ 15 \\ \hline \text{T.B.} \end{array}$$

0-15

$$\begin{array}{r} 24.8 \\ \hline \text{T.B.} \end{array}$$

0-17

$$\begin{array}{r} -0.7 \\ 30 \\ \hline \text{T.S.} \end{array}$$

0-19

$$\begin{array}{r} 21.7 \\ 15 \\ \hline \text{T.B.} \end{array}$$

0-20

$$\begin{array}{r} -0.5 \\ 15 \\ \hline \text{T.S.} \end{array}$$

0-21 (See page 27)
(1' thick grey clay strata)

9.0~~0-22~~

0-23 (T.B. = Top of bluff)

$$\begin{array}{r} 15.4 \\ 15 \\ \hline \end{array}$$

$$\begin{array}{r} 24.1 \\ 30 \\ \hline \text{T.B.} \end{array}$$

0-25⁸ (See page 27)
1' to 2' very soft sandstone

$$\begin{array}{r} 0.2 \\ \hline \text{T.S.} \end{array}$$

Above figures are elevations

0+01.5

8x8 Posts.
 0+01 = Ely. face link fence barricade

0-03.7

0-8.1

0-15 = Top bluff
 15' RT = \pm old wood staves

0-18.5 16' Lt. = \pm 36" Corr. Iron drain pipe

0-23 30' Rt. = T.B.

Rods shown.
 Regular Cross sec. from here on.

31.84 - P.31

\pm Post	\pm Post	\pm Post	\pm Post	\pm Post	\pm Post	\pm Post	\pm Post	\pm Post	\pm Post
29.5	23.5	17.5	9	7	7	14.1	22.1	22.7	End

24.5	24.7	24.9	25.4	25.8					
7.3	7.1	6.9	6.4	6.0					
30	15		15	30					

6.7
 2

26.2
 5.6
 Floor
 Pagoda

25.2
 6.6
 4

25.3
 6.5
 10

24.84
 7.0
 T.B.

7.3
 10

12.5
 15
 on
 steps

25.6
 6.2
 20

25.6
 6.2
 30

17.74
 14.1
 16
 Invert
 outlet

24.14
 7.7
 30
 T.B.

31.84

0+21⁰ prop. M.H.

0+20⁴

0+14⁷

0+09¹ prop. M.H.

0+05⁸

0+05

cont.

0+03⁴¹ (P.28)

31.84

24.89

$\frac{6.95}{6.7}$

24.69

$\frac{7.15}{2}$

$\frac{24.57}{7.33}$

$\frac{23.96}{7.88}$

19.33

$\frac{12.51}{15}$
invert
boy

23.96

$\frac{7.88}{15}$

24.94

$\frac{6.90}{15}$

$\frac{23.93}{7.91}$
P

$\frac{25.01}{6.83}$
G

$\frac{24.26}{7.58}$
P

$\frac{25.03}{6.81}$
G

25.44

$\frac{6.40}{15}$
G

$\frac{25.17}{6.67}$
G

$\frac{24.49}{7.35}$
G

24.88

$\frac{6.95}{15}$
G

$\frac{25.37}{6.47}$
G

$\frac{24.15}{7.09}$
G

$\frac{25.28}{6.56}$
13'

24.88

$\frac{6.96}{7}$

$\frac{24.74}{7.10}$
86'

25.08

$\frac{6.76}{10}$

31.84

0+80^s 17^sRt. } = invert catch basins
17A Lt.

0+70 15^sLt. = X in db. 464 27.20 = B. N. # I

0+57⁴ Exist M.H.

0+53² Exist M.H.

0+39² 1' diam. bolted cap.

0+35[±] (P.29) Exist M.H.

0+29² (P.28) Exist M.H.

0+24¹ (P.28) ^{of M.H.} INVERT = INVERT box M.H.
4^sRt. Pipe leads out thru bottom

3184

25.29
8.55
174
INVERT

26.92
5.25
Rim

26.44
5.40
15
Rim

25.93
5.93
1'
top cap.

25.77
6.07
12
Rim

25.53
6.31
2
Rim

25.29
6.55
35
Rim

25.82
6.52
T
Rim

23.57
8.25
175
INVERT

25.40
6.44
75
Rim

14.24
17.6
44
Invert

35

1701L 5 Lt. = L+T. (P.30)

17009L Φ Dolphin

0791L 10' Lt. = Ctr. 2^Ex2^E Gas. Valve box

0787

27.64
4.18
5

27.64
4.20

27.58
4.46
10
RIM

26.96
4.88
13

X-Sept. 20' Alley in Block 25
 Ocean Beach - for Grade est. only

4926

W.O. 25020

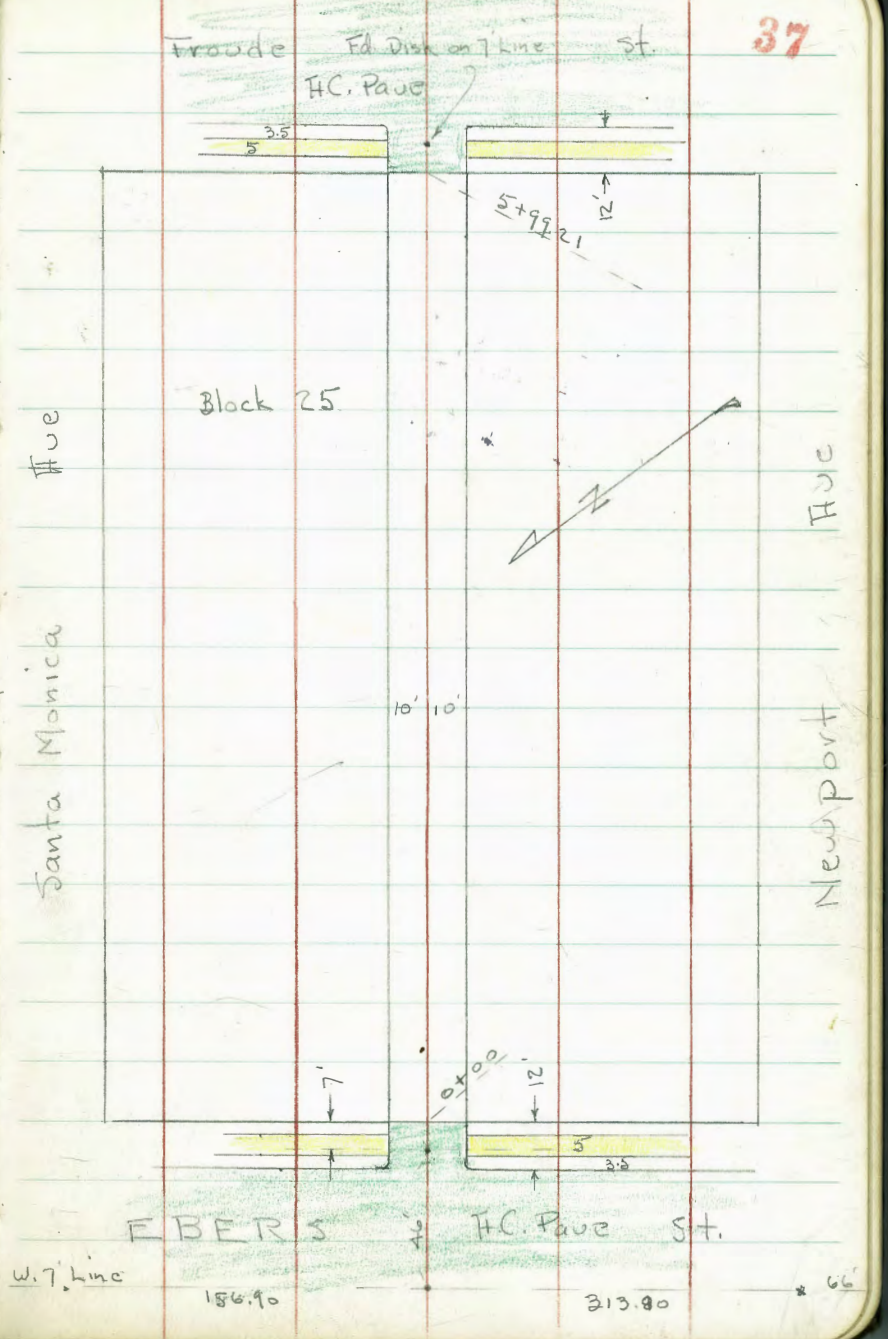
2-3-50

Osborne
 Hardin
 Hatch
 Shepard

INDEXED
 MAY 15 1950

levels next Page

Revised 5-6-50
 P.W.S.



X-Sect. Alley - Blk. 25 - Sketch - P. 37

1+33 - 10.6 Lt = \pm Conc apron to Sing. Car

1+10 - 8' Rt = \pm Pole # A4680

1+00.5 - 9' Rt = Bdg lath fence

1+00

T.P. 13.00 67.50 1.12 54.50

0+60

0+25

0+21 - 8' Rt = \pm Tel. pole # 50at 12-H

0+05 - 7.8' Rt = \pm Deadman

0+00 = E.L. Ebers + edge of AC. Pavc

Re checked - 10-7-53 - 7.0 - New shots are actual Elev.

0-12 = E. cb.

Consider \pm of Alley as E. & W.

B.M. 12.61 55.62 43.01 S.W. 2.P.

Lt. = N. \pm

Rt. = S 38

58.62
8.88
14.8
floor

58.11
9.39
10.6
apron

56.3
11.2
15

50.19
11.6
10 7

55.1
12.7

55.2
12.7
3

56.1
11.4
10

56.3
11.2
15

67.50

55.6
0.0
15

52.1
2.9
10

52.1
3.5

53.1
1.9
10

53.0
2.6
15

49.4
6.2
10

49.2
6.6
5

50.9
6.5

50.1
4.8
10

51.9
3.8
15

46.74
8.88
9.9
Top

46.41
9.21
9.9
gut.

46.07
9.55

46.36
9.26
10
gut

46.43
9.19
10
Top

47.05
8.57
50
Top

46.37
9.25
55
gut

46.12
8.90
Top
2 Rad.

46.03
9.59
10

45.92
9.70

45.83
9.79
10
gut

46.42
9.20
Top
2 Rad.

45.35
10.27
50
gut

46.06
9.56
50
Top

Ebers & Newport

55.62

3+00

2+66 - 10.6 Rt = Beg. 8" Conc. wall (Brick) 6' High

TP 12.75 79.66 0.59 66.91

2+57 - 12.7 Rt = Sing. Gar. Conc. floor

Beg. New Notes - P. 70

2+50 - 10.4 Rt = end wall

2+41 - 13.8 Lt = ~~of~~ Car. gone - slab still in Sing. Gar. - Conc. floor

2+00 - 9.4 Rt = E P. pole # A4670 - B.M. → 65.10
10.3 Rt = Beg. 6" Conc. wall

1+97.5 - 12.2 Lt = end apron

1+70 - 12.5 Lt = Beg. Conc. apron to 3 car Gar.

1+50 - 9.5 Rt = end lath + Beg. board fence

1+44 - 8.7 Lt = 8" Conc. Dr. to Sing. Gar.

LT.		RT.
682	681	683
11.0	11.6	11.4
15	10	9.9 = along wall

66.8
13.2
10.6 = ground at wall

79.66

66.56
0.94
12.7
floor

64.9	64.5	65.8	65.8	67.50
2.6	3.0	1.7	1.7	0.00 64.34
10		10	10.4	10.4 - Bot. Top. wall

64.40

3.10
13.8
floor

62.0	61.8	61.3	62.4	62.3	64.82
5.5	5.2	6.2	5.2	5.2	2.68 61.11
15	10		10	10.3	10.3 Bot. Top wall wall

61.53
12.2 = apron

61.77 20 floor gar.
60.30 12.5 apron

59.0	58.3	54
8.5	9.2	8.4
10		10

59.03

58.61

8.47
21.8
floor

8.89
8.7
Dr

67.50

4+89 - 10.3 Rt. = end wall

4+75

4+50 - 10.4 Rt. = Beg. 6" Conc. wall
10' Rt. = Ely of Conc. Slab.

4+48 - 9.8' Rt. = Φ of outlet of 6" Tile drain under
Conc. Slab.

T.P. 12.64 91.79 0.51 79.15

4+38 - 9.6' Rt. = end Conc. found.

4+24 - 9.5' Rt. = Beg. Conc. foundation to Sing. Gar.
opens to west.

4+00

3+79 - 18.2 Lt. = Φ Doub. Gar. Conc. floor

3+50

3+24 - 9.8' Rt. = end wall

Lt.

Φ

Rt.

83.2

82.1

82.9

8.1
10

9.1
5

8.9
5

7.3
10

6.14
10.3

= Top wall

80.5

79.5

80.3

11.3
10

12.3
10

11.5
10

10.81
10

7.14
10.4

= Top wall To E. Top slab.

91.79

78.6

1.1

9.6 ground

78.92

0.74

9.6 Top.

77.1

2.6

9.5 ground

78.06

0.60

9.5 Top Conc. found.

76.1

3.6
15

75.5

4.2
10

74.1

5.3
10

75.3

4.5
10

75.8

3.9
15

41.2

5.45

18.2 floor

71.1

8.0
10

70.8

8.9
10

72.0

7.7
10

79.66

40.40
86.40

5.39
10.3

Top wall

84.5

85.65

7.3

10

10.81

10

Top slab.

80.98

7.14

10.4

12.64

9.8

IE of Drain

79.15

12.64

9.8

IE of Drain

0.60

9.5 Top Conc. found.

69.5

10.2

9.8 = ground

5+99.21 = W.L. Froude - edge H.C. Pavement
 Wall ends at cb. on Rt.

5+80

5+71 - 99' Rt. - end slab. + Beg. 6" Conc. wall

5+56 - 99' Rt. - Beg. Conc. Slab. to Sing. Gar.

5+50

T.P. 11.71 103.15 0.35 91.44

5+22 - 12.8 Lt = end Conc. apron

(was Gar.)

5+04 - 12.4 Lt = Beg. Conc. apron to Small House

5+00

41

Lt

±

Rt.

98.30 97.72 98.00 98.45 99.09
 4.85 5.43 5.15 4.70 4.06
 10.1 10.1 9.9 9.9 9.9 = Top cb.
 Top gut gut + wall

95.6 95.6 96.1 96.35
 7.6 7.6 7.1 6.80
 10 9.9 9.9
 Top wall

94.56 95.54 94.45
 8.59 7.61 8.70
 9.9 9.9 14.9 = floor
 Slab. Top wall Gar.
 94.19 94.33

8.96 8.82
 9.9 14.8 =
 Cov. Back edge

5 3 9
 92 92 93
 10.7 10.9 9.3
 10 10

103.15

88.62 88.62
 2.92 3.07
 14.4 floor 12.8 = apron

88.62 87.99
 3.17 4.00
 10.4 floor 12.4 = apron

87.1 87.2 86.7 86.4 87.0 88.6
 4.7 4.8 5.7 5.4 4.0 3.2
 15 10 5 10 15

91.29

check Starting BM	706	43.01	43.01
142	50.07	11.58	48.65
0.46	60.23	12.85	59.77
0.51	72.62	13.12	72.11
0.65	85.23	12.92	84.58
T.P.	2.87	97.50	96.63
check B.M.	5.15	104.14	104.31
T.P.	6.71	109.29	102.58

6 + 11.21 = w. cb.

6 + 03.21 = High point in Pave

Some Diff. - checked Back to orig B.M.

97.27	96.61	98.22	97.58	97.86	98.19	98.95	99.80	100.40
5.88	6.54	4.93	5.57	5.29	4.96	4.20	3.35	2.75
50	50	Top	10		10	Top	50	50
Top	9+	3' Rad	9+		9+	3' Rad.	9+	Top
98.28	98.05	98.28	98.71	99.03				
4.87	5.10	4.87	4.44	4.12				
10.1	10.1		9.9	9.9				
Top	9+		9+	Top				

103.15

Check S.E. Cor. P.L. 1261

INDEXED

MAY 15 1950

Sommermeier
Sherman
Bunch

12[#] pull at ⁴⁻¹⁹⁻⁵⁰~~74°~~ for 50'

Tape checked 22[#] pull at ^{74°}~~78°~~ Temp. 100'

1+00 (100' @ 75° Temp. 22[#] pull

0+00 = N.W. Cor. Muirlands Terrace Unit #1
Map. 2532

▣ = set stub.

Map. Dist. - not chained
0-934.71 = S.E. Cor. P.L. 1262
Map 2532

43

Sly. line Muirlands
Terrace

offset line

c' ○ Fd. 2" I. pipe L.S. 2334



▣ Fd. Conc. Man. L+T.

PL. 1261

6+50 (50' @ 70° - 12# pull)

6+00 (50' @ 70° - 12# pull)

5+50 (50' @ 70° - 12# pull)

5+00 (50' @ 70° - 12# pull)

4+50 (50' 70° - 12# pull)

4+00 (50' - 70° - 12# pull)

3+50 (50' - 70° - 12# pull)

3+00 (100' @ 70° - 22# pull)

2+00 (100' @ 70° - 22# pull)

C. offset
Line

← 6' →

sty line Muirland Terrace Unit #1 Produced

← 6' →

44

P.L. 1261

P.O.T.
12+00.02 (20.88 @ 68° - 5[#] pull.)

Station 11+97.96

11+79.14 (100.18' @ 68° - 22[#] pull.)

10+78.96 (100.17' @ 71° - 22[#] pull.)

9+78.79 (100.35' @ 74° - 22[#] pull.)

8+78.44 (78.44' @ 68° - 14[#] pull.)

8+00 (100' @ 74° - 22[#] pull.)

7+00 (50' @ 70° - 12[#] pull.)

5' offset BL

Line

← 6' →

55° 05' - 40"

500 P.47

45

3 | 165° - 17'
55° - 05' - 40"

5 Ly. Line Muirlands Terrace Unit #1 produced

← 6' →

12+73.35 (below) = Correct Stationing
 12+74.29 (Detail)

This point appears to be proper position for monument.

Identical Points

Corrected Sta.: 12+74.29

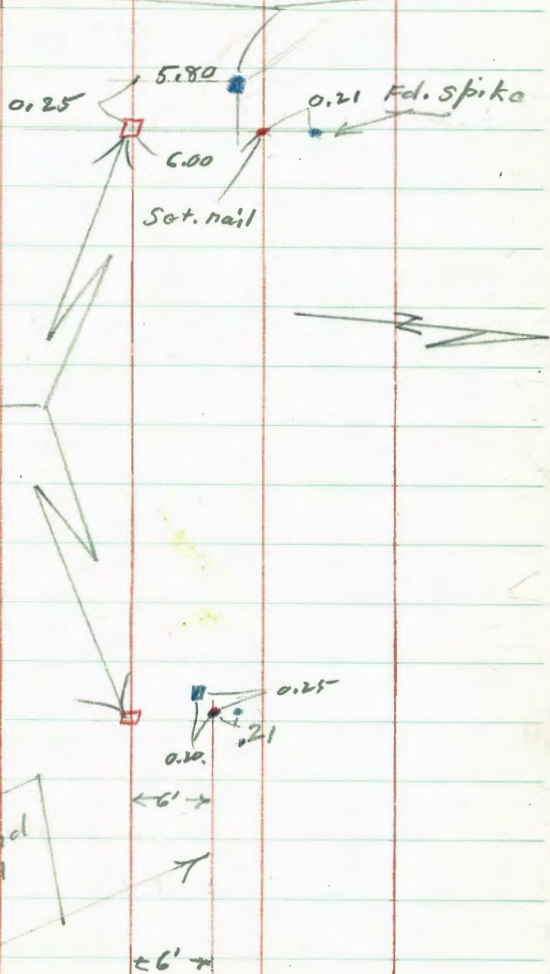
P.O.T.

12+74.35 (23.89 @ 70° - 6th pull.)

12+50.46 (50.44 @ 69° - 12th pull.)

slightly line Muir land
 Terrac. Unit #
 produced

Mon. has been moved.
 Fd. Mon. loose + out of place.



Locate S.E. Cor. Lot 13 Miramar Terrace.
as found set.

47

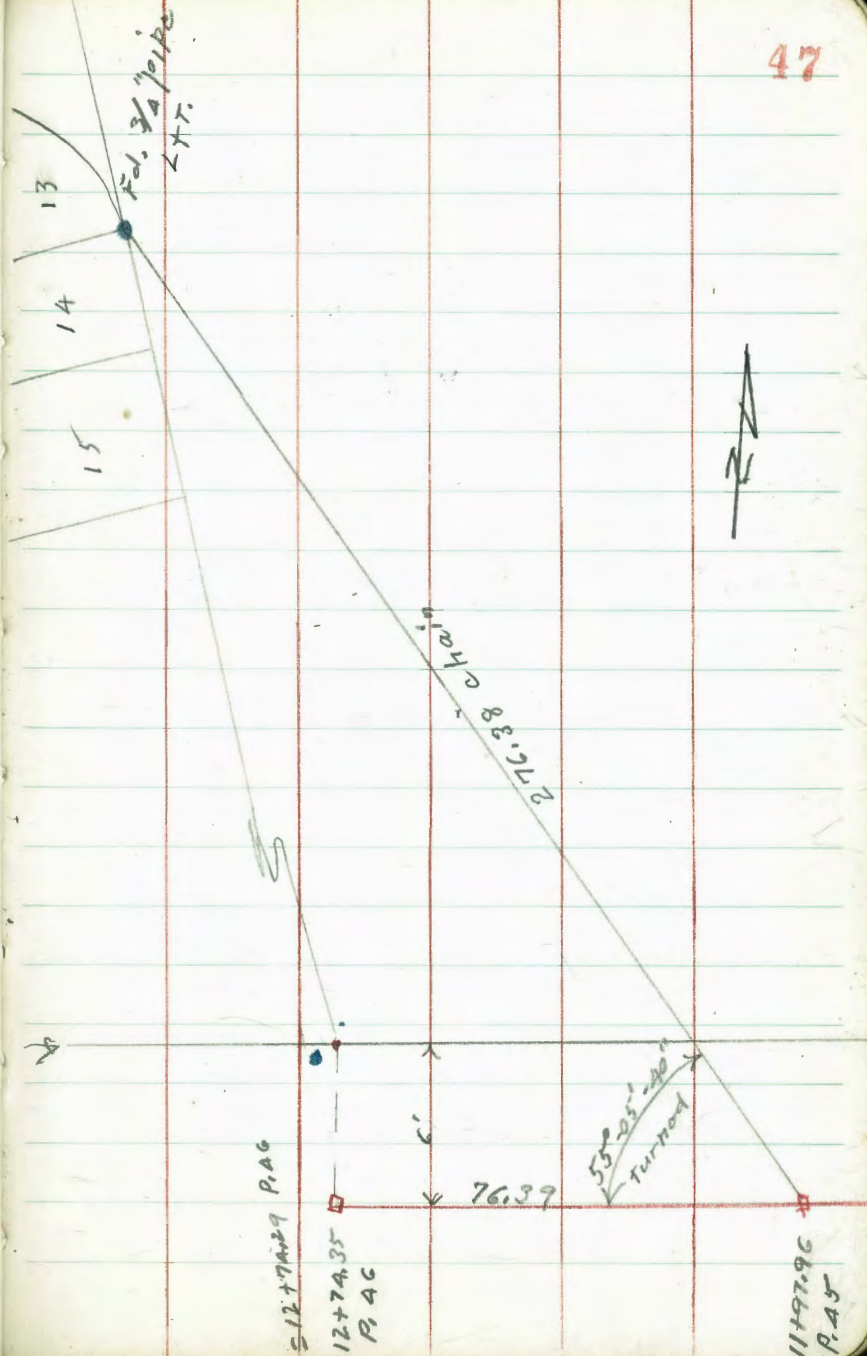
38.41 @ 90°-10" pull
 78.28 @ 66°-22" "
 68.00 @ 57°-20" pull
 71.72 @ 69°-20" "

276.41 = 276.38 corrected.

INDEXED
 MR
 MAY 15 1950

3/165-17 120
 550-05'-40"

sly. line Muirlands Terrace.



Fd. N.W. 7' L+T. Fay + Center.

check tie shoot for tacks.

Fd. N.W. 7' L+T. Fay + Rusbuille = Point R.

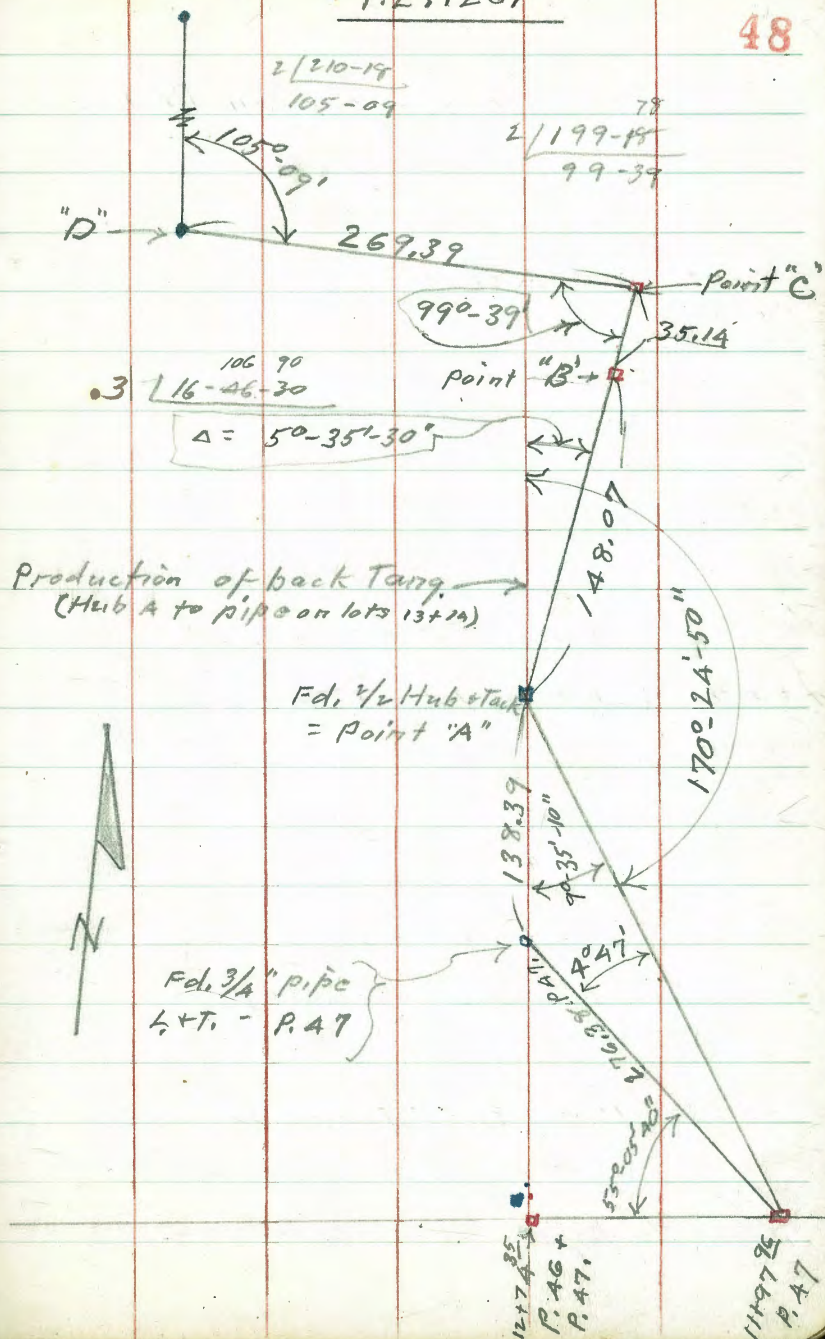
set. 141 - P.O.T.

set 1/1 P.O.T. = Point "B"

Fd. 1/2 Tack Cor. lots 10+11 Miramar Ter. Map 1750

Fd. 3/4" pipe cor. lots 13+14 Miramar Ter. Map. 1750

See P. A9 for chaining



Data for distances on P. 48.

0+35.14 = set Δ stub = Point "C".

= 0+00

From stub P.O.T. "B"

= set P.O.T. "B"

1+48.07 (21.67 @ 68° - 5# pull.) = stub P.O.T.

1+26.40 (27.23 @ 72° - 6# pull.)

0+99.17 (33.25 at 73° - 6# pull.)

0+65.92 (25.92 @ 74° - 5# pull.)

0+40 (21.00 @ 76° - 5# pull.)

0+19.00 (19.00 @ 76° - 5# pull.)

0+00

From Point "A"

1+38.39 = Fd. $\frac{1}{2}$ (Point "A" P. 48)

+59.76 @ 76° - 14# pull.

0+78.63 (78.63 @ 76° Temp 20# pull)

0+00

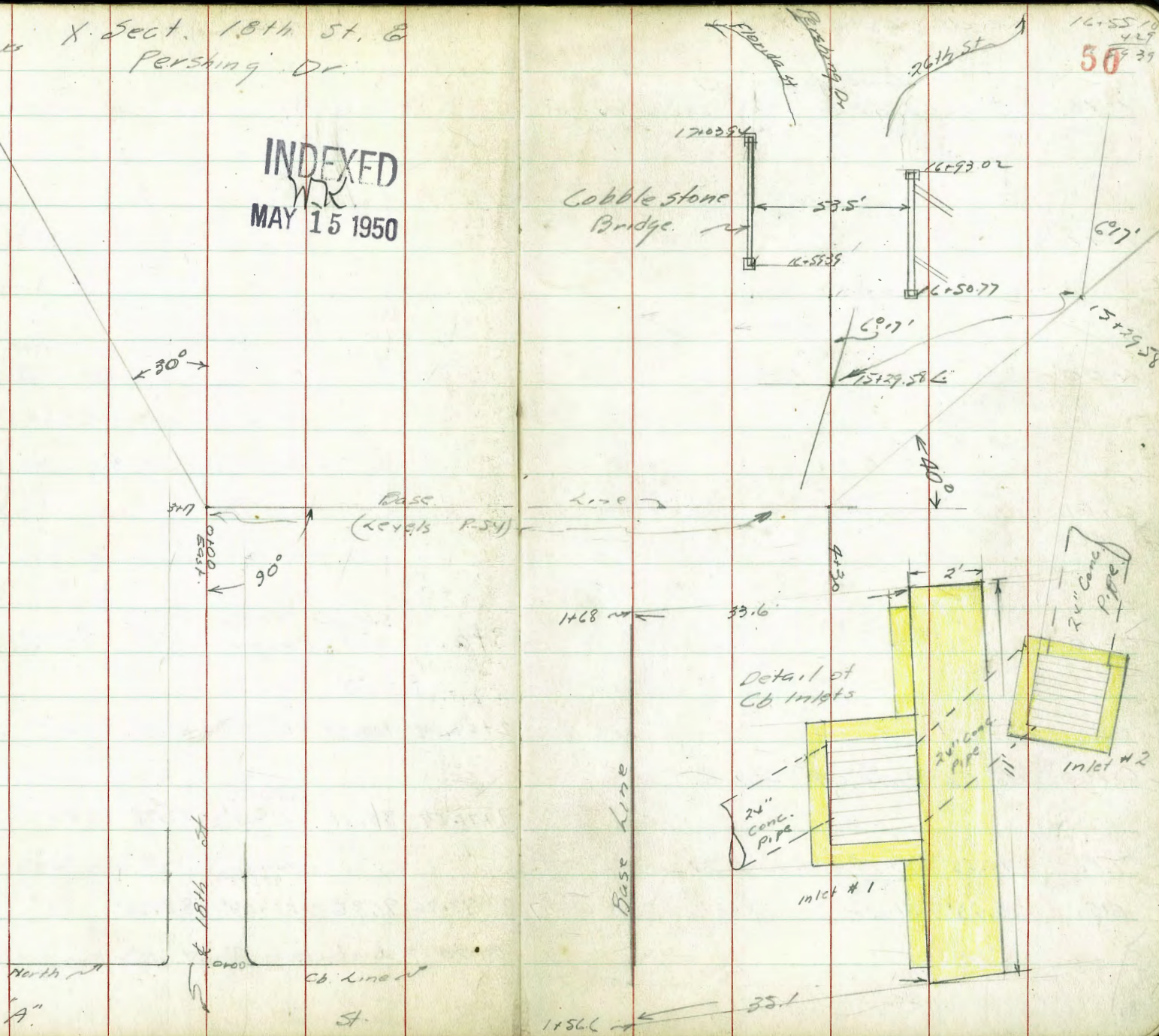
From $\frac{3}{4}$ " pipe. Cor. lots 13 & 14

Sta.	Slope Dist	Vert. angle	Horiz. Dist.	Temp	Tape pulls
= L+T. = Point "D"		cos = .97508			
2+69.39	100.22	$12^\circ-49'$	97.72	68°	22#
		cos = .96479			
1+71.67	85.71	$15^\circ-15'$	82.71	65°	20#
		cos = .97385			
0+88.96	91.36	$13^\circ-08'$	88.96	75°	20#
0+00 = A stub = Point "C" - page 48					

5-11-50
Hendricks
176 Coey
Greer
Gravelford
1404 20008

X Sect. 18th St. &
Pershing Dr.

INDEXED
WR
MAY 15 1950



1+18 E 10' Conc. Dr. on Rt
 End. Cb on Lt. Reg. 8' Conc (Ret. Vain)
 Lowest

92⁹² 92⁹² 91⁹⁰ 90⁸⁹ 89⁸³ 90⁴³ 90²⁷ 89⁷⁸ 90⁴³ 88⁴⁸
 26 26 26 26 26 13 13 27 26 50
 G G G G G G G G G

1+11

89⁶⁶ 90⁶
 26 26
 G G

1+00

89¹⁰ 89⁵⁵ 89⁷² 89⁵⁶ 89⁴ 89⁶⁷
 26 13 13 26 26
 G G G G G

0+60

87³⁰ 87²⁰ 87⁷⁴ 87⁹¹ 87⁷² 87³⁹ 88⁰⁴
 26 26 13 13 26 26
 G G G G G G

0+10

86²³ 85⁶⁵ 86⁰² 86⁰⁸ 85⁷⁸ 85³⁴ 85⁸³
 26 26 13 13 26 26
 G G G G G G

0+00 No. Cb line A St.

86¹⁹ 85⁶⁰ 85⁶⁰ 85⁹³ 85⁷⁶ 85⁶⁷ 85²⁷ 84⁷⁴ 85⁵¹
 26 26 26 13 13 26 26 26 26
 G G G G G G G G

T.P. 12.65 93.75 0.10 81.10

93.75

B.M. 13.13 81.20

68.07 NE BR 18th & B St.

2+73

2+41 Double Euc. Tree @ 10" & 16" 31' Rt.

2+30 Power Pole # C1408 28.5 Rt.

2+20

7P 11.23 $\frac{10 \times 66}{x}$ 0.32 93.43

2+00

1+40

1+22.5 & 8" Conc. Ret. Wall on Rt. to East.

 $\frac{93.75}{N}$

102 ⁸	97 ⁹	95 ⁶	96 ¹⁰	95 ²⁸	96 ⁸	96 ^{95²⁶}	95 ²⁵
35	16	13		24	31	39	42
		Pav.		Pav.			Pav.

103.7	95 ⁹	93 ⁶⁰	94 ²²	94 ⁰¹	95 ¹	95 ⁴	94 ⁰²
50	19	14		19	24	32	53
		Pav.		Pav.			Pav.

102.7	95 ¹	93 ²⁰	93 ⁸⁶	93 ⁸⁶	93 ⁶²	93 ⁵	93 ³	92 ⁸²
50	21	16		20	27	50	100	127
		Pav.		Pav.	Pav.			

Conc. 1404 33' Lt 1+28

102 ⁶	92 ⁷	93 ²⁰	93 ⁵	92 ⁸⁵	92 ⁵⁵
50	18		24	50	Pav.
	Pav.				100'

99 ³	91 ⁰⁰	91 ⁴	91 ⁰²	91 ⁰	91 ⁵⁷	88 ¹
50	21		17	35	41	75
	Pav.			Pav.	Pav.	

90 ⁸⁰	92 ¹³
36	41

5+00

124³ 116⁰ 113²⁰ 113⁴⁰ 113⁴ 112⁴⁰ 113² 114¹ 110⁴
 35 12 7 10 22 25 34 50
 Pay. Pay. Pay.

4+50

118⁸ 115⁸ 111⁸ 108¹⁹ 108⁸² 109⁰⁰ 108³² 109⁴ 110⁴ 107⁸
 30 20 9 5 15 24 27 40 50
 Pay. Pay. Pay.

T.P. 12.88 117.24 0.30 104.36

4+00

112⁴ 107⁸ 103⁹⁷ 104²⁵ 104⁶⁵ 103²² 105²² 100³ 100⁰⁰ 100⁰⁰
 32 7 3 15 29 40 44 87 100
 Pay. Pay. Pay. Pay. Pay. Pay. Pay. Pay. Pay.

3+50

110⁰ 102² 99⁸² 100¹⁷ 101⁰¹ 99⁸¹ 99⁰⁰ 99⁰⁵
 50 2 4 17 30 35 out-60
 Pay. Pay. Pay. Pay. Pay. Pay. Pay. Pay. Pay.

3+17 L. 30 Lt. (rt. to Backline)

100⁵ 100⁰ 97¹⁶ 98⁵⁵ 98⁵³ 97⁰⁸
 39 16 11 17 34

2+86

103² 97² 97¹⁵ 96⁸⁰ 96¹² 96⁴⁴ 96⁰⁸
 36 15 12 18 38 50

104.66

Cont'd. from R53

R

54

TP. 11.50 93.43 (93.43)

(Top Conc 1707 R52)

TP. 0.75 104.93 13.06 104.18

5+40

127 ²	119 ³	116 ⁴	110 ⁷	116 ⁶	116 ⁵	117 ⁰	117 ⁵	113 ⁷
38	17	9		12	19	22	30	48

117.24
X

Levels on Pershing

54-A

Cb Inlet #2

93⁰⁸
Grate F.L.

Cb Inlet #1 (see sketch P. 50)

94⁶⁸ 93⁶⁴ 89¹¹
Cb. Grate F.L.

1+50

91⁰ 95⁴ 94⁹ 94⁸ 94³⁰ 93²⁴ 93⁵⁵ 92⁸²
70 42 28 41 50 67 93
Pav.

TP. 8.03 $\frac{103.33}{1}$ 9.62 95.30

1+00

99⁵ 98⁴ 96⁸ 96³ 95⁵ 94⁹ 92²³ 93⁵²
100 50 26 29 38 50 65 90
Pav. Pershing

0+47

98²² 98⁵⁷ 98¹⁰ 98⁵ 97⁴ 95⁸⁷ 96²⁵ 95³⁵
100 50 35 27 12 31 47
Pav. Edge

0+37

0+37 → 99⁰⁰ 92¹⁰ 98⁵⁵ 96⁷² 95⁹³
83 10 25 39
Pav. Edge

0+00 = (4.90 off 3.17 P. 53)

104.92

Cont'd. from 5VA

4+00

TP. 3.83 98.58 8.58 94.75

3+50

3+00

2+36 top slope

2+18 top slope

2+00

103.33

Base
line

55

109⁰ 108⁵ 94⁰ 93⁶ 94³⁴ 95⁵² 96⁸²
60 53 41 12 38 81
Pav.

106⁸ 106¹ 94⁸ 94⁶ 94⁹³ 95²⁰ 96²³
50 39 27 24 48 82
Pav. Pav.

108⁴ 107⁵ 95¹ 94⁸ 94⁶² 95²² 95²⁸
28 27 16 30 53 79
Pav. Pav.

102⁴ 102¹ 101⁵ 101⁵ 93⁹ 94¹⁵ 94⁴⁷ 94²¹
30 22 18 9 35 58 83
Pav. Pav.

99⁸ 97⁵ 93⁶ 94¹⁵ 94²⁷ 93⁹⁵
28 6 37 60 54
Pav. Pav.

99⁵ 95⁵ 95² 94⁰ 93⁶ 94¹⁰ 94⁰⁴ 93²²
47 20 7 22 35 61 85
Pav. Pav.

6+50

115² 113⁶ 93⁶ 92¹ 92⁷ 92⁸⁰ 93¹⁴ 93²⁶
 57 42 27 26 36 58 83
 Pay

6+00

113⁶ 112⁰ 93⁸ 93² 92⁶ 93⁰⁴ 93⁵⁰ 93⁷⁵
 58 44 29 21 34 58 84
 Pay

5+50

112⁰ 111¹ 94⁴ 93⁶ 92² 92²⁷ 93⁶³ 94²⁴
 58 47 33 19 31 57 83
 Pay

5+00

110⁹ 110⁰ 94⁴ 93¹ 92⁶ 92⁷⁹ 93⁶⁶ 95⁰⁰
 58 50 36 5 24 50 75
 Pay

4+50

110² 109⁴ 94⁶ 93³ 93³ 93⁵¹ 94²⁶ 95⁶²
 66 56 48 13 10 27 79
 Pay

4+30 L. 40² Lt (R) Ls to Back Tan

94² 93² 93⁶ 93⁸⁹ 95⁵ 96⁷⁶
 56 21 4 30 70
 Pay

98.58
 /

Base
 Line

Base
Time

57

9:50

117 ²	118 ²	90 ⁰	89 ⁷	87 ⁵	87 ⁵⁷	89 ⁹⁷	90 ⁰⁰
42	31	11		24	30	52	77
					Pay.		

9:00

122 ⁶	117 ⁵	90 ⁷	90 [±]	90 [±]	90 ³⁹	90 ⁷⁵	90 ⁷⁷
48	30	12		18	31	53	78
					Pay.		Pay.

8:50

122 ⁵	119 ⁵	91 ⁶	91 ⁷	90 [±]	90 ⁸²	91 ²⁰	91 ²³
46	32	15		21	32	55	80
					Pay.		Pay.

8:00

118 ¹	116 ²	92 ⁴	92 ⁰	91 ³	91 ³¹	91 ⁷⁸	91 ⁷³
44	34	16		22	33	55	80
					Pay.		

7:50

116 ⁸	114 ⁸	92 ⁶	92 ⁵	91 ⁷	91 ²¹	92 ³²	92 ³⁸
55	37	20		27	33	56	80
					Pay.		Pay.

TP.

1.10	94.10	5.58	93.00
	<u> </u>		

7:00

116 ⁴	113 ⁹	93 ¹	92 ²	92 ³	92 ³⁶	92 ⁷⁵	92 ⁹¹
55	39	22		22	36	57	82
					Pay.		

98.58

Contd from p 57

Base
Line

58

B17 029 90.17 424 89.86 89.88

(BP Top Corn. Pillar East side Cobbler bridge
Marshing Dr. & Florida.)

12+50

114⁹ 103⁷ 84⁵ 84⁵ 84⁸⁰ 85²² 85³⁰
60 26 18 7 31 56
Pav.

12+12

105⁴ 101³ 93⁸ 84⁷ 84⁸ 85²⁵ 85⁴⁸ 85⁸⁰
60 42 20 12 13 36 60
Pav.

11+50

120⁷ 113⁹ 86³ 86² 85⁹⁰ 86²⁶ 87⁰²
60 21 5 21 44 70
Pav. Pav.

11+00

121³ 119⁹ 86³ 86³ 86⁶¹ 87⁰⁷ 87⁷⁵
37 22 2 26 48 73
Pav. Pav.

10+50

119⁷ 119⁵ 117⁹ 87⁸ 87⁸ 87⁵⁹ 88⁰⁰ 88⁶⁰
40 28 23 5 30 50 75
Pav. Pav.

10+00

118⁰ 117⁵ 88⁶ 88⁶ 88⁵⁹ 88⁹³ 89¹⁶
40 25 7 32 51 75
Pav. Pav.

9410
K

15+29.58 ← Lt sect. taken Rt to Ball Tan. 84⁴-82⁷ 85⁵ 85⁷⁸-85⁴ 84⁵³
59 53 45 7 24

14+75 101⁰ 97¹ 83⁹ 85¹ 85²⁵ 85²⁵ 85⁴ 84⁴⁷
60 56 43 37 21 4 31

14+50 108⁵-105¹ 84⁵ 84⁹ 84⁶ 85⁸ 85³⁶ 85⁷ 84⁶⁶
70 57 42 38 33 18 7 35
Pay

14+00 113¹ 110² 84³ 84⁸⁷ 85²⁰ 85²³ 84⁷⁴
60 48 36 12 14 39
Pay. Pay.

13+50 115⁵ 111⁵ 84⁹ 84⁷⁴ 84⁸⁹ 85²⁰ 84⁹¹
60 42 29 6 20 45
Pay. Pay.

13+00 117¹ 109² 84⁵ 84⁷ 84⁷² 85⁹ 85⁰⁰
60 35 23 2 25 49
Pay. Pay.

90.17
x

Cont'd. from P. 59

Pass
line

60

17+03.94 End Bridge on Lt.

$86^{\circ} 34'$ $85^{\circ} 21'$
 23 23

16+50.77 Beg Bridge on Rt.

86° $86^{\circ} 00'$ $85^{\circ} 50'$ $85^{\circ} 23'$
 42 25 25

16+00

82° 82° $85^{\circ} 6'$ $85^{\circ} 58'$ $85^{\circ} 10'$ $84^{\circ} 80'$
 55 48 20 27 25

90.17

8-22-50

Hendricks
Cota
Greer
Crawford
NO# 31696

X SECT. SANTA BARBARA PLACE
MISSION BLVD. to BAYSIDE WALK
(Map 1809 sheet 5)

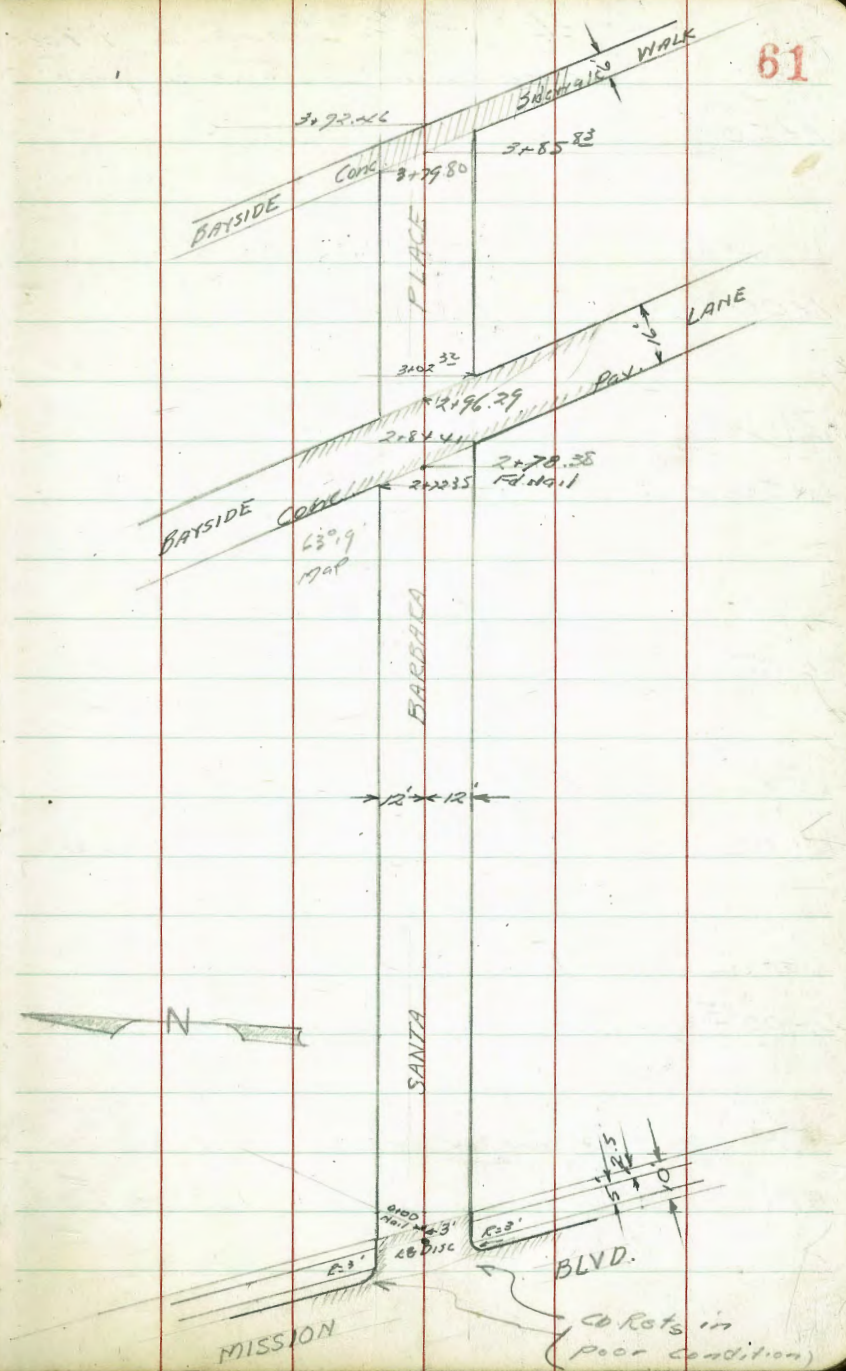
INDEXED

AUG 23 1950

Reduced

B.L.C. 9/23/50

61



Levels Santa Barbara Place

1+50

1+00

0+50

0+25

0+00 E Line Mission Blvd (Section at R.L.)

0-00²⁵ Edge Conc Paving Section on Diagonal

East Cb Line Mission Blvd

T.P. 4.33 4.44 0.11
 B.M. 7.14? 7.03

12	12	12	12	24
19	12	11	18	25
20	15	10	12	22
20	10	12	22	
22	12	Pav.	12.2	23 Cb
12	12	12.2	12.5	12.5 Pav.
12	12	12.2	12.5	12.5 Pav.

(June)
 64 48 91 97-0 98-0 91-0 88-0 92-0 89-0 89-0 87-0
 50 50 26 26 142 142 12 12 16.5 16.5 50 50
 Cb Cb Cb Cb Cb Cb Cb Cb Cb Cb Cb Cb
 B.P. 2nd Wall & Santa Barbara Place

4.44

2+91.4 Beg. 4th Bend Wall 4.6' Lt

Edge Taring (Section on Diagonal)

2+96.29 East Line Bayside Lane

2+87.33 E Bayside Lane (Section on Diagonal)

2+84.41 Rt. Ls to Prop. Line on Rt.

2+78.38 W. Line Bayside Lane
section on Diagonal

2+72.35 Rt. Ls to Prop. Line on Lt.

T.P. 4.76 4.28 4.92 -0.48

2+50

2+00

449

10.76	10.96	10.81
5.04	5.14	5.09
13.43	13.43	13.43
-1.17	-1.17	-1.14
50	13.43	13.43
		50

0.89	0.96	0.97
5.13	5.10	5.11
12	12	12

4.94	0.96	1.10	0.93	1.04
5.11	5.14	5.10	5.11	5.11
25	13.43	13.43	13.43	25

0.96	1.0	0.95	0.91
5.11	5.11	5.11	5.11
12	8	12	12

438

L&T Top of C6 13' Rt 2+75±

0.6	0.8	1.0	0.9	0.7
5.11	5.11	5.11	5.11	5.11
18	12	11	12	16

0.6	0.8	1.0	1.0	0.8
5.11	5.11	5.11	5.11	5.11
18	12	12	12	20

444

B.M. 0.81 7.03 7.03

TP. 8.42 7.84 7.86 -0.58

3+85⁸³ Edgr Conc Side walk (Bayside Walk)
(Section on Diagonal)

3+79.80 End Brick Wall 11 1/2 ft.
Rt. Ls to Prop. Line on Lt.

3+45

3+02.32 Rt. Ls to Prop. Line on Rt.

4.28
1

B.P. Sea Wall & Santa Barbara P.C.

0.47	0.34	0.50
4.75	4.2	4.28
3.28		13.43

0.5	0.1	0.2	0.1
4.75	4.4	4.5	4.4
12		12	20

0.5	0.1	0.2	0.2	0.0
4.8	4.4	4.5	4.5	4.3
20	11	12	20	

5.07	5.07	5.07	5.08
20	11	12	

4.28
1

New Sections of Jewell - Mooreland
to La Playa - See P. 12 + 13 for Orig.

W.O. 31922 10-26-50 - 7.0.
4789

INDEXED
OCT 27 1950

2+50

2+00

1+64-37.7 Ltr: \$ 8' Conc. Dr.

1+50

1+00

0+94.42 = end cb. + walks

0+92 = \$ 15' Dr. - See P. 13

0+50

0+00.2 = edge Conc. Pav. + P.C. Returns.

See Orig. for Poles + Trees.

B.M.

B.M.

23.88 = 0 in cb. w. side at P.C.

33.68 = N.W. B.P. Ingraham + Moore land.

True elev.

office bench book shows this as
33.86 - See P. 13 this book

Lt.

±

Rt.

65

25.0 24.5 24.5 24.7 24.8
37.5 20.5 20.5 37.5

25.1 24.9 24.5 24.4 24.4 24.7 25.0
50 37.5 20.5 20.5 37.5 50

25.37
61
floor.
Gar.

24.98
37.5 - Dr.

24.8 24.5 24.3 24.0 24.3 24.1
37.5 20.5 14 20.5 37.5

25.2 25.0 24.5 23.8 23.6 23.4 23.9 24.1 23.6
50 37.5 20.5 17 15 20.5 37.5 50

24.38 24.27 24.20 24.0 23.6 23.4 23.5 23.4 23.51 23.69 23.76
33.5 26.5 Top 23.5 gut. 10 10 20.5 gut. Top 26.5 33.5
endwalk endwalk endwalk

24.06 23.4 23.1 22.9 22.8 22.7 23.23
Top 20.5 gut. 10 10 20.5 gut. Top

23.88 23.34 23.38 23.27 22.9 22.46 22.92
Top 20.5 gut. 10 10 20.5 gut. Top

These are act. elev.
Not Rods.

4+93- 37.5 Rt. = £ 8' Conc. Dr.

4+90- 37.6 Lt. = £ 3' Conc. walk

4+50

4+33- 37.5' Lt. = £ 8' Conc. Dr.

4+18- 37.6' Lt. = £ 9' Conc. Dr.

4+07- 37.7' Lt. = £ 2.6' Conc. walk

4+00

3+55- 37.5' Lt. = £ 3' Conc. walk

3+50

3+08- 34.5' Rt. = £ 2.5' Conc. walk

3+00

Lt. £ Rt. 66

27.06
27.25
52.5
Floor
Gar.

25.83
50
at Porch
25.72
37.6 = walk

25.7 24.9 24.8 25.1 26.0 25.8
37.5 20.5 20.5 22 37.5

25.73
50
Dr.
25.60
37.5 = Dr.

25.97
57 = Floor
Gar.
25.47
37.6 = Dr.

25.83
51.6
at Porch
25.50
37.7 = walk

25.6 25.5 24.9 24.7 24.6 25.6 25.5 25.7
50 37.5 20.5 20.5 22 37.5 50

25.64
51.6
at Porch
25.49
37.5 = walk

25.5 25.3 24.8 24.6 24.7 25.3 25.5
37.5 23 20.5 20.5 22 37.5

25.31
34.5
walk
25.44
50
at Porch

25.5 25.6 24.9 24.5 24.6 24.6 25.2 25.3
50 37.5 20.5 18 20.5 37.5 50

6+63.32

6+53.32 = SL. la Playa + edge H.C. Pavc

6+35'

6+00

5+79- 369' Lt. = ± 2' Tile walk

5+50

5+44- 37.5' Lt. = ± 8' Conc. Dr.

5+24- 37.2' Lt. = ± 4' Conc. walk

5+02- 37.5' Lt. = ± 2.5' Conc. walk

5+00

Lt.

±

Rt.

67

23.7
37.5

22.97
Top
9ft.

22.52
21.4

22.77
10

22.86

22.64
10

22.52
21.4
9ft.

22.99
Top

24.4
37.5

24.4
37.5

24

22.89
Top

22.63
18
9ft.

22.70
10

22.68

22.57
10

22.47
18.1
9ft.

22.95
Top
end/co.

24.6
24

25.0
37.5

25.2
37.5

25.6
24

23.9
18

23.4

23.7
20.5

26.3
22

26.5
37.5

25.7
50

26.0
37.5

25.8
20.5

24.4
19

24.8

24.9
20

26.3
20.5

26.0
37.5

26.8
50

25.74
47
at Porch

25.79
36.9 = walk

25.8
37.5

25.7
20.5

24.8
19

25.2

25.1
19

26.0
20.5

26.2
37.5

26.31
61.5
Gar. floor

25.84
37.8 = Dr.

26.04
51.2
at Porch

25.86
37.2

25.79
50
at Porch

25.72
37.5 = walk

25.6
50

25.6
37.5

25.2
20.5

25.1

25.4
20.5

27.0
37.5

27.2
50

D. Smith
G. Pope
B. S. S. S. S.

Note:
all inlet boxes are
32x35" inside 24" opening

INDEXED
MK
DEC 22 1950

Jewell
Paya

Jewell St.

W0#31922

12-21-50

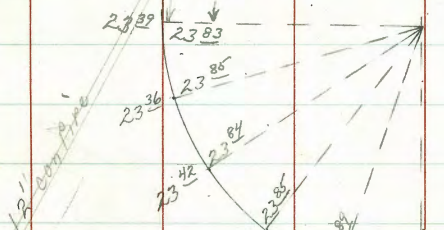
Note All Radius' are 20'
Length Ret = 315'
5 parts 63 ea.

36' Rdwy

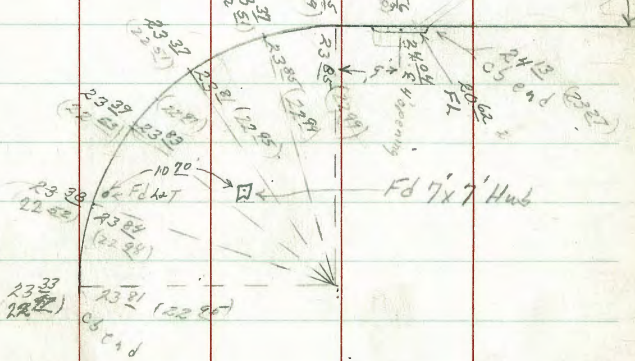
2351 24.00

195 cbs

2024 FL 2334 2385 24" opening



24" Con Pipe



Fd 7'x7' Hub

Corrected Elevations in parentheses this (22.99)
P.H.M. - 12-27-50

B.M. 2388

misc NW Co. Ret.
P. 05+13

195 cbs

36'

Rdwy

195 cbs

Begin New Sections - Alley - Block

25 - O.B. from 2+50 on - Sec P. 39

10-7-53- 7.0.

3+50- 8.3' Rt. = \pm P. pole # A 4640 74.19 =

3+49.5 10.3' Lt. = end wall

3+49- 10.1' Rt. = Nly. of 6" Conc. wall - 7' High

3+28- 8.7' Lt. = \pm 3' Conc. walk Thru wall

3+24.5 -

3+01.4- 0.5' Rt. = \pm Sewer M.H. 67.90 = wly. Rim

3+00.5= 10.1' Lt. = Beg. Conc. Block wall - 6" wall

3+00- 10' Rt. = Beg. Conc. Sect. poured outside

2+98.8- 10' Lt. = end House

2+88.2- 10' Lt. = end fence + Beg. House

2+75

2+68- 10.1' Lt. = Beg. Picket fence

10.8' Rt. = Beg. 8" Conc. Block wall

2+66- 10.7' Rt. = end apron

2+60- 10.5' Lt. = \pm 12" Conc. Apron to Sing. Gar.

2+50- 10.4' Rt. = Beg. Conc. apron

Lt. # Rt. 70

BM = spike 71.6 70.8 70.7 71.9
10 6 10

71.4

10.3
ground

71.9

10.1 = ground
at end

70.52 70.32 70.24
15 10 8.7
walk

70.1 69.1 69.0 69.1 69.6
10 4 6 9.9 = By
Cor. of wall

68.5 67.8 67.8 68.0 68.4
10 4 6 10 = By wall

67.70 66.8
floor 10 = gr.

66.2 65.9 65.9 66.6 66.7
10 6 10 10.6 = By wall

66.70

10.7

apron

66.74 65.85
17.5 10.5
floor apron
gar.

65.83
12.4
apron

66.53
15
floor Gar.

5+01 - 9.1' Rt. = ± P. pole # J.P.A. 4620 BM. spike 88.55

5+00 - 10.3' Lt. = end apron

4+90 - 10.5' Rt. = end Conc. wall

4+60

4+50 - 10.4' Rt. = Req. 6" Conc. wall - 3' High

4+49 - 10' Rt. = end Slab

4+48 - 9.5' Rt. = outlet of 6" Tile Drain under slab.

4+38 - 10.2' Rt. = Req. Conc. Slab.

4+38 - 9.6' Rt. = end found. to Gar.

4+30

4+24 - 9.5' Rt. = Req. ^{Sec P. 4} Conc. found. to Sing. Gar.

apron at wall - for line of Gar. under apts.

4+00 - 10.2' Lt. = Sly. of Conc. wall + Req. Conc.

3+79 - 18.2' Lt. = 4 Doub Gar. - Conc. floor

3+75

	Lt.	±	Rt.	
	87.21 10.7 Top 8' wall to N.	86.20 10.3 10	86.5 10	86.0 86.6 87.6 88.0 6 7 10 86.46 10.5 = Top + gr.
	82.88 18.7 floor	81.81 10.1 apron	81.3 8	81.7 83.0 83.1 9 10 by wall
				81.2 84.61 10.4 Top wall gr.
				80.0 81.02 10 Top gr. Conc.
				79.15 9.8 = I.E.
				79.35 10.2 = Conc
				78.5 78.92 9.6 Top found. ground.
	79.76 18.9 floor	78.39 10.2 apron	77.8 9.5 = By gar.	77.5
				77.3 79.06 9.5 Top found. gr.
	77.75 18.7 floor gar.	75.51 10.2 apron	75.5 10	74.6 75.3 10
	74.21 18.2			
		73.3 10	72.6	73.1 10

B.M. = Top - end Ret. - S. side 99.10

5+99.21 = w.L Froude - See P. 41

5+97.2 - 2.9' L. = Cons. Co. 14' Gate Cap.

5+90 = Brk in Top of wall - 9.9' Rt.

5+80

5+71 - 9.9' Rt. = end slab. + Req. 6" Conc. wall

5+56 - 9.9' Rt. = Req. Conc. apron to Sing. Gar.
under Apt.

5+35

5+22 - 12.5' L. = end apron.

5+04 - 12.5' L. = Req. Conc. apron - to House
(was. Gar)

Lt

#

Rt.

72

98.30 = check

10.1
Top cb.

97.73

2.9
Top
Cover

97.2 97.36 98.38
9.9 To West 9.9 To E.

95.5
10

95.6 96.0 96.35
9.9 Top
wall

94.57 95.54 94.45
9.9 Top apron wall 14.9 = floor
gar.

94.17 94.37
9.9 = apron 14.8 = at Bldg.

95.2 90.7 90.6 91.0 92.1
10 8 6 10

88.76
12.8 apron.

88.66 87.82
16.4 floor 12.5 apron

8

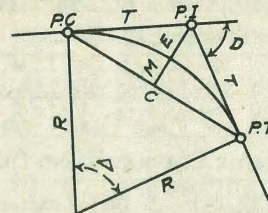
74

37

37

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve— D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve— $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External— $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ —Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $+8\frac{1}{8} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.—Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158—Sta. P. C. = 54.50, hence offset = $7.27 \frac{54.50}{100} = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $\frac{(54.50)^2}{2 \times 688.26} = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^2$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{8} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' + 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 + 8\frac{1}{8} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $+42 = 5.5$ or $D = 5^\circ 30'$.

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

Table with 10 columns and 10 rows of minute values in decimals.

TABLE II.—INCHES IN DECIMALS OF A FOOT.

Table with 11 columns and 11 rows of inch values in decimals.

TABLE III.—RADIUS, ORDINATES AND DEFLECTIONS.

Large table with 5 columns for Radius, Ordinate, Tangent, Deflection, and Degree, repeated for degrees 0 to 30.

NOTE. Chord Deflection = 2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Table with 9 columns: Central Angle, Tangent, External, Central Angle, Tangent, External, Central Angle, Tangent, External.

13.5
58
77

1080 351
1168 536

2644

101.5
58
107.3
137
938

92.9
63
57.2

104.2
7.5
112.0
97
13

74

12.31
71.09
103.40
174
107.46
12.54
114.00
1.4
112.86
12.68
125.84
7.00
118.54
7.62
126.17
10.98

1088
71
968
114.99
009
118.06
101.16
131.0

9529
602
320232

11724
694
11020

9017
501
55.6
2460
345
7052

9410
9009
401

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 47.9. For slopes of 1 on 1 see inside of front cover.

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