

1868

W. H. W. W.

W. H. W. W.

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

1-5 Alley BIK 168 Pacific Beach  
6-9 Prop. Storm Drain Mountain View Park  
10-13 Cross Sec. Kalmia 33<sup>rd</sup> to Gregory  
14-15 " " Felton St. Kalmia to Laurel

39-46 X- Sect Chatsworth - Coronado to Catalina  
47 X- Sec. Alley, BIK 317, Reed & Daleys <sup>Add.</sup>  
59 X- Sec. Alley BIK 281, S. D. land &  
61-68 <sup>Town Co's Add.</sup> Talbot - Catalina to Canyon  
67-71 Alley BIK 201, City Heights, X- Sec.

Ch  
H  
10  
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to b  
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80.6

Cross section  
 Alley BIK. 168 Pacific Beach  
 Morrell to Noyes  
 between Diamond & Emerald

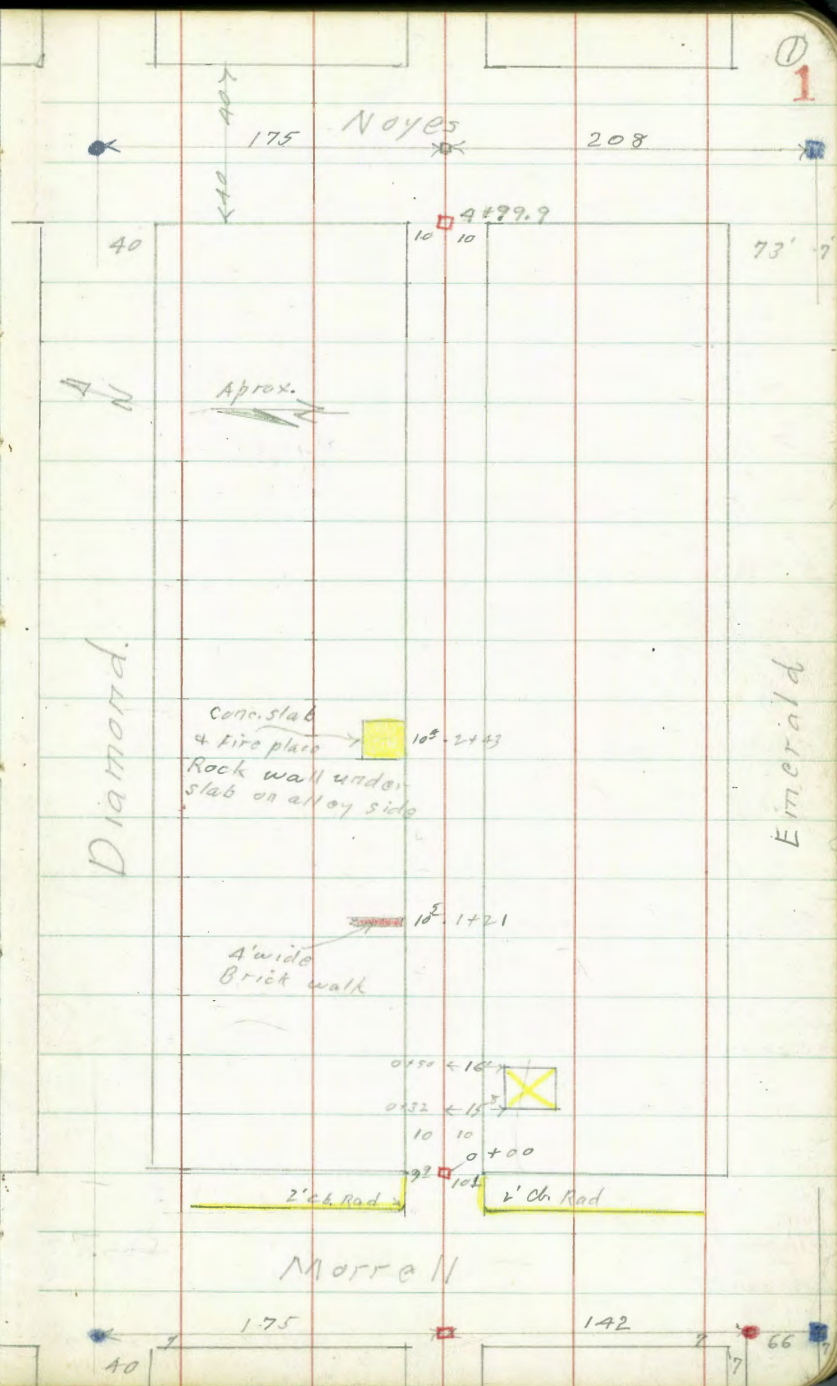
7-12-48  
 W.D. 25001

Sommermeier  
 McCoy  
 Melton

- = Ed. Corner, Man.
- = " L+T.
- = Set L+Disk
- = " Lx2 + "
- = " 1x1 + tack

INDEXED

~~Indexed~~  
 [Signature]



LEVELS BIK 168  
Pacific Beach  
INDEXED

0+44 14' Lt. = E. Sing. Gar. dirt floor

0+32 15' Rt. = Start double Gar. Conc. floor

T.P. 2.38 92.18 5.64 89.80

of cl. + 10' Rt. = End of cl.

0+00 = E. line Marrell 92' Lt. = end

0-20 = E. Cl. line Marrell (top of cl.)

0-20' = E. Gutter line Marrell (Dirt.)

R.W. 7' Disk  
Marrell  
+ Emerald

8.08 87.36

Set. B.M.  
#1

T.P. 1.20 95.44 6.41 94.24

T.P. 0.32 100.65 9.51 100.33

Diamond

Lament

3.81 109.84 - 106.03

S.W. B.P.

2028  
1.7  
164

80.06

2.1  
10

92.14

3.3  
25

93.93  
1.51  
100

93.04  
2.4  
100

91.17

4.27  
92  
86. End

92.35  
3.09  
50

91.34  
4.1  
50

90.94

4.5  
92  
87. End

91.12  
4.32  
12  
87.80

90.17  
5.3  
10

89.28

2.5  
10

90.74

5.0  
10  
85.74

91.12  
4.32  
12  
87.80

89.87  
5.6  
10  
95.44

89.68

2.5  
10

90.64

4.8  
10  
85.84

90.22  
5.22  
12  
85.00

89.54  
5.9  
10

88.98

3.2  
15.8  
85.8

90.58

4.86  
10  
85.86

89.07  
6.37  
50

88.24  
7.2  
50

89.07

3.11  
15.8  
85.8

89.64

5.8  
30  
84.84

87.73  
8.01  
100

86.54  
8.9  
100

Alley BIK. 168 P.B.

# INDEXED

Rock wall under alley side of slab  
10' w. No need to fit for grade

2+43 = 1/2 14x14 fire place + Conc. slab

2+00

1+50

walk

1+21 10' Lt. = 1/2 4" wide brick in Conc.

1+00

0+50 16' Rt. = End double car. Conc. floor.

72.18

Station	Description	84.68	86.05			
		7.5 100 Base wall	6.13 104 top slab			
		86.28	85.88	85.48	85.38	84.38
		5.9 30	6.3 10	6.7	6.8 10	7.8 50
		87.18	87.08	<del>86.78</del>	87.98	86.38
		5.0 25	5.1 10	5.4	5.2 10	5.8 12
			87.79			
			4.39 105 End walk			
		89.18	88.08	88.68	88.58	87.38
		3.0 50	4.1 10	4.5	4.6 10	5.0 15
		90.18	<del>89.88</del>	89.38	89.38	87.18
					88.88	
					87.03	
		2.0 30	2.3 10	2.8	2.8 10	3.3 16 End
						3.15 14 Car. floor
						3.4 50
						<u>92.18</u>

Alley BIK 168 P.B.

5+399 - ~~2~~ Noyas

# INDEXED

2 4+999 - W. line Noyas

2 4+50

1 4+00

1 3+50

1 3+00

T.P. 1.25 88.97 4.46 87.72

07 2+50

92.18

90.58	90.58	84.07	84.07	82.37	82.37	85.27	85.27
$\frac{1.6}{30}$	$\frac{1.6}{30}$	$\frac{4.1}{25}$	$\frac{4.9}{30}$	$\frac{5.16}{10}$	$\frac{5.16}{10}$	$\frac{3.3}{100}$	$\frac{3.3}{100}$
84.98	84.98	84.17	84.17	83.37	83.37	82.47	82.47
$\frac{7.2}{10}$	$\frac{7.2}{10}$	$\frac{4.8}{10}$	$\frac{5.13}{10}$	$\frac{5.6}{10}$	$\frac{5.6}{10}$	$\frac{6.5}{10}$	$\frac{5.13}{50}$
84.48	84.48	84.17	83.57	83.27	82.57	82.37	82.07
$\frac{7.7}{10}$	$\frac{7.7}{10}$	4.8	5.4	5.7	6.4	6.6	6.9
84.08	84.08	83.97	83.47	82.87	82.37	81.87	80.14
$\frac{8.1}{10}$	$\frac{8.1}{10}$	$\frac{5.0}{10}$	$\frac{5.5}{10}$	$\frac{6.1}{10}$	$\frac{6.6}{10}$	$\frac{7.1}{10}$	$\frac{8.8}{50}$
83.28	83.28	82.77	81.87	81.57	80.07	78.27	78.27
$\frac{8.9}{10}$	$\frac{8.9}{10}$	$\frac{6.2}{75}$	$\frac{7.1}{50}$	$\frac{7.4}{75}$	$\frac{8.9}{80}$	$\frac{10.7}{100}$	$\frac{10.7}{100}$

Alley Bk. 168. Pac. Beach

5

INDEXED

2

2

1

orig B.M.  
Page 2

2.72 106.02 (106.03)

1

T.P. 12.61 108.74 0.02 96.13

check of  
974.000

SS 4.97 91.18 (91.17)

T.P. 8.79 96.15 1.61 87.36

01

N.W.B.P.  
Emeralda  
Noyes

SS 11.28 77.69 (77.58)

88.97

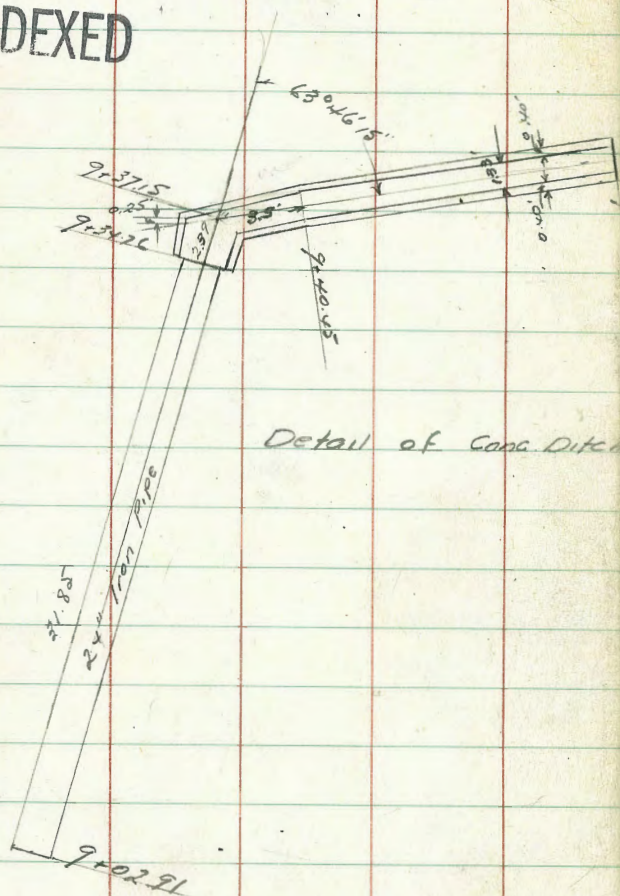


10-6-48  
Hendricks  
Roberts  
Greer  
Rorer

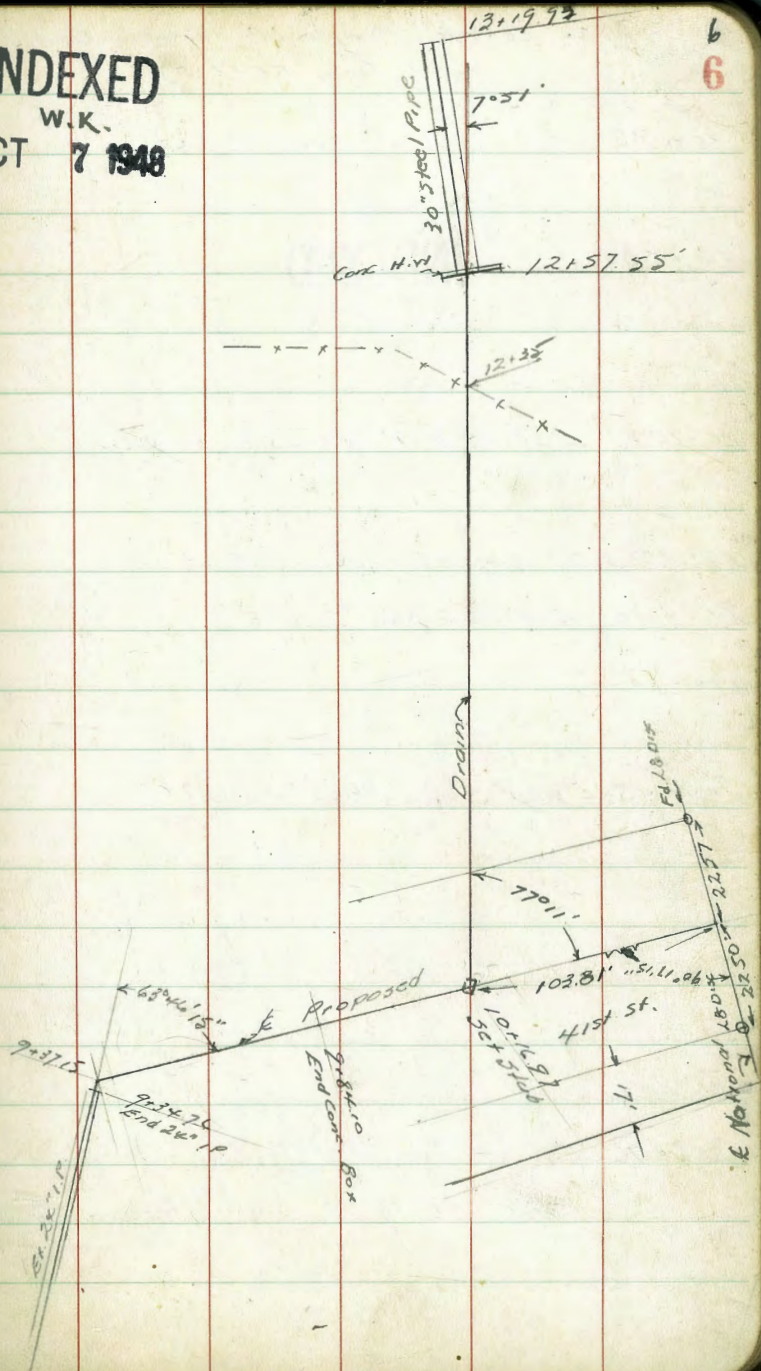
Extension Proposed Drain  
Mountain View Park  
Cont'd. From F19745-P-77

INDEXED  
W.K.  
OCT 7 1948

INDEXED



Detail of Conc. Ditch



6  
6

Levels Proposed Storm Drain  
(Cont'd. from FB1745)

10+78 12" Apricot tree 22' Lt.

10+50

INDEXED

10+16.97 L.Lt. 77°11' Rt 63 to Backline

10+10 = 10" Apricot tree 18.5 Lt.

9+84.10 End Conc Box.

9+40.45 L Wall & Wall Steps Down)

9+37.15 L.Rt 63° x 61.15"

9+34.76 End Pipe

0.94 36.19

35.25

278  
8' 278  
8' 278  
20

279 284 287 270  
8' 8' 7' 4'  
20 346 5 12

284 280 275 278 268  
7' 8' 8' 8' 7'  
0.67 0.67 0.67 0.67  
Wall FL FL Wall

277 278 276 276 278 273 276  
6' 7' 8' 8' 8' 7' 6'  
0.67 0.67 0.67 0.67 0.67 0.67  
Wall Wall FL FL Wall Wall

270 275 276  
6' 8' 8'  
0' 0' FL  
Wall FL

272 277 278 277 277  
6' 8' 8' 8' 8'  
1' 1' FL 1' 1'  
Wall FL FL FL Wall

NW 1/4 41st & National

12+57.55 Beg. 30" Steel Pipe

12+41

12+35 Barbed Wire Fence

12+30

12+23

12+00

11+50

11+04 10" Apricot tree 28' Lt

11+00

36.19

10<sup>80</sup> 7<sup>06</sup>  
FL HW



26° 27° 28° 29° 30°  
5<sup>2</sup> 8<sup>2</sup> 9<sup>2</sup> 10<sup>2</sup> 7<sup>2</sup> 7<sup>2</sup>  
24 22 19 13 20

Notes Reduced 10.7-98

11<sup>7</sup>

10<sup>7</sup>

10<sup>9</sup> 10<sup>6</sup> 10<sup>7</sup>  
20 20

10<sup>0</sup>

9<sup>0</sup> 9<sup>2</sup> 9<sup>0</sup>  
20 20

B-17

0.94 35.25 35.25

1311993 End. 30" Steel Pipe

36.19

H W B B 4151-6 National

22.07

14.12

FL

Cross Section Kalmia St. + Felton St.

Levels next page

Laural St.

N.O. 25001

Nov. 1-48 10  
S. J. 599  
Smith  
Bocher  
Gorget  
Clark

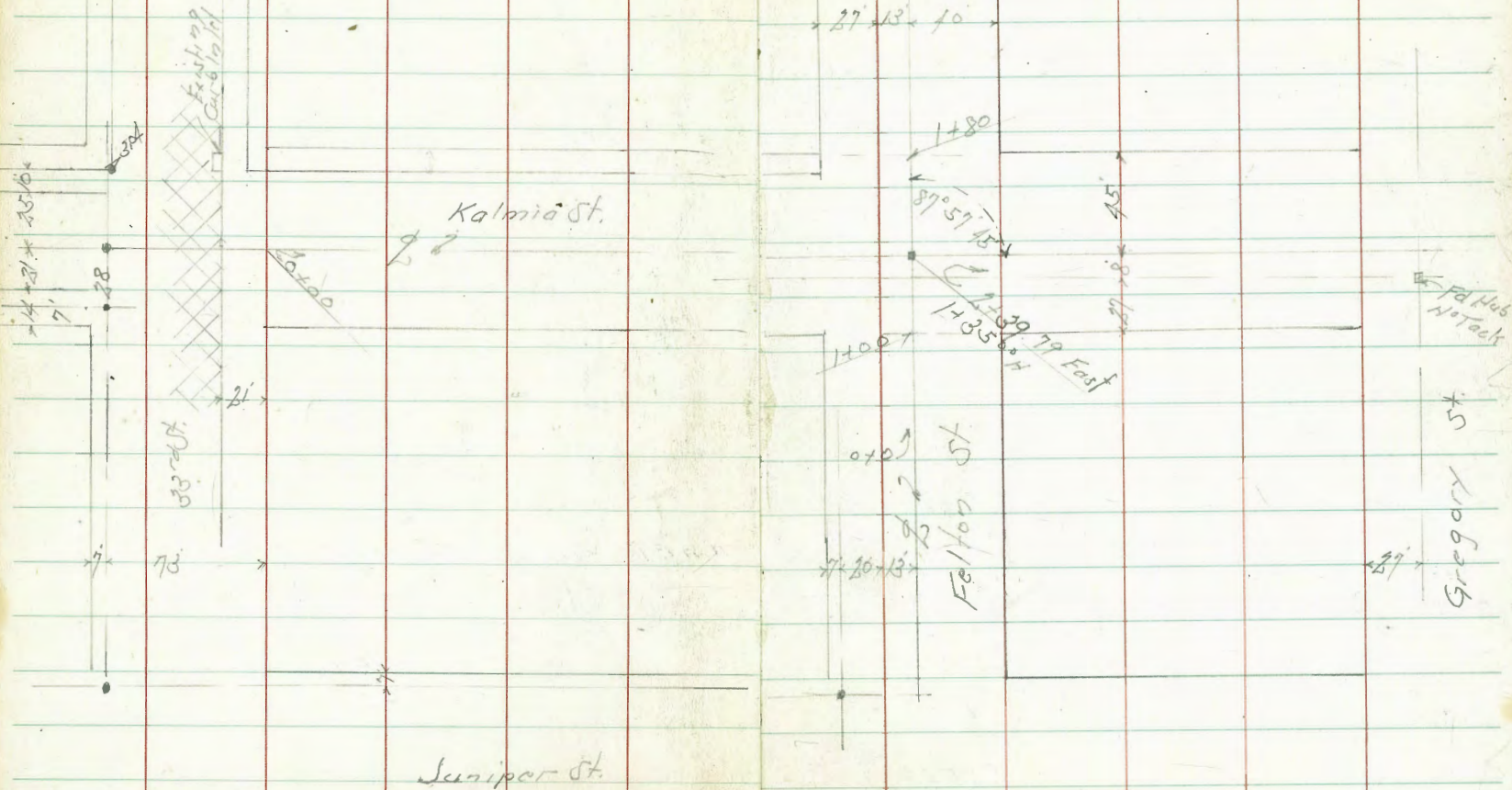
10

- Hub Found
- Lead + Tack Found
- Hub Set.

Fd Hub → Res. Pipe  
+ R.W. Hub  
Road Disc.

INDEXED

WK  
NOV 4 1948





Kalmia St.

# INDEXED

12  
12

TP 7.59 271.46 280 263.87

+99.79 - M.L. Felton Taken Line of Felton

4.1	270.4	269.4	269.9	259.1	256.9
+5.7		+1.7	+0.2	9.5	7.8
15		35		5	5

+68

160	270.7	269.0	263.5	256.5	257.4
15		15	1.2	8.2	10.2
		35		5	5

+36

160	269.0	267.7	261.9	258.0	250.0
15		15	8.8	6.7	14.7
		35		11	35

1710

0.0	244.7	263.8	261.7	252.5	240.1
15		8.9	13.0	12.2	21.1
		35	23		35

0483

261.1	256.5	244.2	240.1	235.2	235.6
15	8.2	10.5	6.2	12.1	12.1
	35	35	35	35	35

264.67

264.67

Bottom  
1/2

Kalmia St

INDEXED

4 + 0

TP 128 248.35 1316 247.13

2 + 50

TP 0.78 260.29 11.95 259.51

3 + 23

2 + 99.79 = E.L. Felton Taken on line of Felton

2 + 39.79 = L Felton Taken of Line Felton

271.46

<del>10.7</del> 6.7	<del>11.6</del> 11.6	<del>8.4</del> 8.4	<del>6.5</del> 6.5
247.6	248.7	251.9	255.2
<del>11.4</del> 10.6	<del>10.6</del> 10.6	<del>8.6</del> 8.6	<del>6.5</del> 6.5
248.9	250.3	251.08	254.0
<del>11.6</del> 11.6	<del>10.6</del> 10.6	<del>14.2</del> 14.2	<del>6.5</del> 6.5
156.3	155.5	157.3	159.0
<del>7.7</del> 7.7	<del>7.7</del> 7.7	<del>7.8</del> 7.8	<del>6.5</del> 6.5
263.8	264.1	263.7	261.8
<del>6.2</del> 6.2	<del>6.2</del> 6.2	<del>6.2</del> 6.2	<del>10.4</del> 10.4
268.2	268.1	265.43	261.2
<del>6.2</del> 6.2	<del>6.2</del> 6.2	<del>6.2</del> 6.2	<del>10.4</del> 10.4
271.46	271.46	271.46	271.46

4+

2

PT

13



Cross Section Fallon St.  
 South of Kalmia to South of Laurel St.  
 Sketch Page

2+50

INDEXED

2+0

TP

11.05 275.02 1.52 263.97

0+75

TP

11.48 265.49 0.72 254.01

+50

0+0

TP

0.05 254.73 12.32 254.68

BM

1.57 267.00 265.43

072 Hub  
 Kalmia +  
 Fallon  
 page 13

Lt. = 21

Rt. = 5

14

14

272.8	271.3	268.6	265.2
272.0	271.0	269.9	266.3
253.7	256.4	257.1	258.4
240.6	245.3	252.6	254.3
227.1	227.1	237.3	246.3
254.68	254.73		

Fulton St.

BM			6.05	297.57
TP	10.21	303.64	7.61	293.42
TP	11.02	301.04	0.18	290.03
BM	11.02	290.20	6.06	279.18
TP	7.48	285.24	0.49	277.76
TP	12.79	278.23	0.11	265.46

SMBP  
No. 3228  
297.62  
  
SMBP  
Laurel  
33205  
278.98

4+30

3+90

3+50

TP	3.48	265.57	12.93	262.09
----	------	--------	-------	--------

3+0

275.02

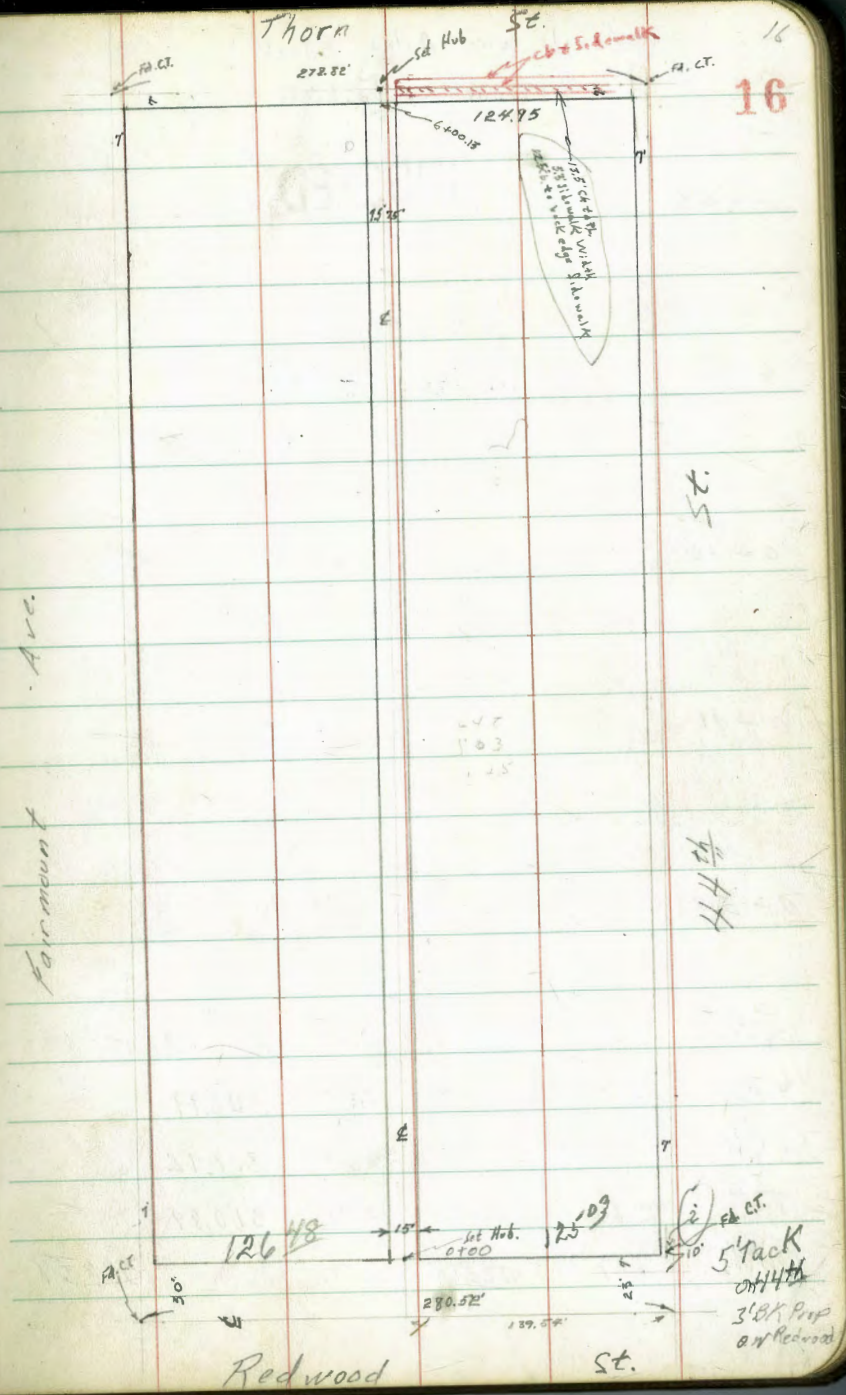
LT								
				252.55				
				248.3				
				244.9				
				241.1				
				236.5				
				231				
				227.5				
				223.65				
				220				
				217.7				
				214				
				211.5				
				208				
				205.7				
				202				
				200				
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				110				
				107.4				
				105				
				102.1				
				100				
				97.4				
				95				
				92.1				
				90				
				87.4				
				85				
				82.1				
				80				
				77.4				
				75				
				72.1				
				70				
				67.4				
				65				
				62.1				
				60				
				57.4				
				55				
				52.1				
				50				
				47.4				
				45				
				42.1				
				40				
				37.4				
				35				
				32.1				
				30				
				27.4				
				25				
				22.1				
				20				
				17.4				
				15				
				12.1				
				10				
				7.4				
				5				
				2.1				
				0				

275.02

Roberts  
McLay  
W. Moore  
Jones  
12-27-48  
W.O. 31588

Cross Section  
Alley Block 1 Clifton's Add.  
Redwood to Thorn between  
Fairmount and 44th  
T.P. 21

INDEXED  
WIK  
DEC 28 1948



Levels on Alley Block I  
Cliffans Addition

INDEXED

0+03

0+00

North P.L. Redwood

0-10

0-11

0-30

E Redwood (Dirt Graded  
No Ch. or Sidewalk)

T.P.	7.79	<u>310.98</u>	7.87	303.19
T.P.	5.09	311.06	7.57	305.99
Set B.M.			6.84	306.72
T.P.	2.67	313.56	12.71	310.89
B.M.	1.01	323.60		322.59

4t.

	$\frac{5.1}{50}$	305.86			
	$\frac{5.3}{72}$	305.68			
	$\frac{6.6}{75}$	304.38			
	6.7	304.28			
	$\frac{6.5}{7.5}$	304.48			
	$\frac{5.2}{50}$	305.18			
	$\frac{6.4}{50}$	304.58			
	$\frac{6.8}{7.5}$	304.18			
	6.8	304.18			
	$\frac{6.6}{7.5}$	304.38			
	$\frac{6.9}{50}$	304.08			
	$\frac{6.0}{100}$	304.98			
	$\frac{6.4}{50}$	304.58			
	7.1	303.88			
	$\frac{7.3}{50}$	303.48			
	$\frac{7.0}{50}$	303.78			
	7.1	303.88			
	$\frac{7.6}{50}$	303.38			
	$\frac{7.5}{100}$	302.88			
	$\frac{6.7}{100}$	303.78			
	$\frac{7.0}{50}$	303.88			
	7.1	303.88			
	$\frac{7.6}{50}$	302.68			
	$\frac{8.4}{100}$	302.58			
	$\frac{7.0}{100}$	303.98			

Rc.

17

17

310.98

C.T. 5' and 5' to N.W. Corner 44th and Redwood

Fire hydrant S.E. Corner Thorn and 44th.

N.W. B.P. Highland and Thorn

1+00

0+98.5

No. Edge Conc. Slab

0+86.5

13.6' Rt. to So. Edge, Conc. Slab. Single garage

0+60

8.0' Rt to Water Meter box

Measurements to Center of Box

0+51

6.7' Lt to P.P. JPA 315

Measurements to back of Poles

0+50

0+40

on &amp; a Sewer M.H.

5' Dia. Conc. Slab around MH

0+30

Lt.

$$\frac{2.0}{25} \quad 308.98$$

$$\frac{1.8}{75} \quad 309.18$$

$$1.8 \quad 309.18$$

$$\frac{1.6}{75} \quad 309.38$$

$$\frac{1.5}{17.5} \quad 309.48$$

Rt.

18

18

$$\frac{1.59}{13.6} \quad 309.39$$

Apron

$$\frac{1.40}{17.6} \quad 309.58$$

Floor

$$\frac{1.94}{13.6} \quad 309.04$$

Apron

$$\frac{1.44}{17.6} \quad 309.54$$

Floor

307.18

307.68

307.48

307.48

308.28

$$\frac{3.8}{25}$$

$$\frac{3.3}{75}$$

3.5

$$\frac{3.3}{75}$$

$$\frac{2.7}{25}$$

307.23

375

306.78

306.98

306.38

306.68

306.88

$$\frac{4.2}{25}$$

$$\frac{4.0}{75}$$

4.6

$$\frac{4.3}{75}$$

$$\frac{4.1}{25}$$

310.98

310.98

1+82 So. Edge Conc. Apron Double Garage

1+75 7.1' Rt. to Meter box

1+72 So. Edge Conc. Slab. Double garage

1+67 8.7' Rt. to No. Edge Shed

1+50 8.7' Rt. to So. Edge Shed

T.P. 7.03 317.09 0.92 310.06

1+27 6' Rt. to Meter box

1+25 9' Lt. to Meter box

1+19 No. Edge Conc. Apron

1+00.5 So. Edge Conc. Apron of Double Garage

310.98

lt. 2 311.20 311.71 Rt. 19

5.81  
7.8  
Apron

5.88  
2.8  
Floor

19

311.37

310.99

5.72  
1.5  
Floor

6.10  
9.1  
Apron

310.19

310.49

310.19

310.39

310.39

6.9  
1.2

6.6  
7.5

6.9

6.7  
7.5

6.7  
1.2

317.09

309.97

1.01  
13.3  
Apron

0.88  
17.3  
Floor

310.70

309.73

1.25  
13.4  
Apron

0.98  
17.3  
Floor

310.98

Lt.

¢

Rt.

20

20

2+30 6.7 Rt. to Meter box

2+26 6.8 Lt to P. Pole PA. 3175

2+25 9.5 Rt. to End board Fence

2+19 8' Lt. to Meter box.

2+01 8.5 Rt. Beg. Board Fence

2+00

1+97 No. Edge Conc. Apron

1+95 7' Lt to Meter box

1+91 No. Edge Conc. Slab.

311.49

311.69

311.59

311.49

311.49

 $\frac{5.6}{12}$  $\frac{5.7}{7.5}$ 

5.5

 $\frac{5.6}{7.5}$  $\frac{5.6}{12}$ 311.49  
 $\frac{5.60}{8.2}$   
Apron311.79  
 $\frac{5.30}{2.8}$   
Floor

311.63

311.67

 $\frac{5.76}{15}$   
Floor $\frac{5.72}{9.7}$   
Apron317.09317.09

2+83 So. Edge Conc. Slab Double Garage

2+80 & 3' Sidewalk 10.5' Rt

2+77 6.1' Rt. to Meter box

T.P. 4.84 319.99 1.94 315.15 No. 1 P.P. JPA 3205

2+50

2+46.5 No. Edge Conc Slab

2+41 & of the Single Garage

2+33 So. Edge Conc. Slab Single Garage

317.09

Lt.

Rt

6.10  
9.7  
Apron

2.813.32  
4.67  
10.5

6.37  
10.5  
Floor

21

311.89

312.29

312.39

319.99

312.79

312.79

4.2  
25

4.8  
12

4.7  
7.5

312.49  
4.6

4.3  
7.5

4.3  
25

312.81

4.28  
10.7  
Apron

312.84

4.25  
26.5  
Floor

312.53

4.56  
10.3  
Apron

317.09



3+50 8.5' Rt to Board Fence (Begin.)

3+49.5 6.4' Lt. to P. Pole 571 3205

3+46 No. Edge Conc. Slab

3+44 6.5' Lt to Meter box

3+29.5 So. Edge of Conc. Slab Double Garage

3+29 8.7' Rt to End of board Fence

3+24 7.5' Rt to Meter box

3+00 Begin board Fence 8.5' Rt.

2+99 No. Edge Conc. Slab.

319.99

Lt.

314.59

$\frac{5.4}{15}$

314.99

$\frac{5.0}{7.5}$

Rt.

314.87

5.1

314.79

$\frac{5.2}{7.5}$

Rt.

314.69

$\frac{5.3}{15}$

22

314.79

$\frac{5.20}{10.5}$   
Apron

314.78

$\frac{5.21}{12.5}$   
Floor

314.51

$\frac{5.48}{10.4}$   
Apron

314.73

$\frac{5.26}{12.4}$   
Floor

313.19

$\frac{6.8}{15}$

313.29

$\frac{6.7}{7.5}$

313.39

6.6

313.59

$\frac{6.4}{7.5}$

313.69

$\frac{6.3}{7.2}$

313.41

$\frac{6.28}{9.0}$   
Apron

313.71

$\frac{6.28}{10.9}$   
Floor

319.99

4.

4

PK

4+10 No. Edge Conc. Slab

4+05 7.5' Lt to Meter box

4+01 So. Edge Conc. Slab Single Garage

3+97 No. Edge Conc. Slab

3+83 5.4' Rt to Meter box

3+80 8.9' Rt. End of Board Fence  
So. Edge of Conc. Slab - Double Garage

3+78 8.8' Rt. to 2' sidewalk

3+64 6.3' Lt to Meter box

3+59 4 Single Garage

319.99

315.29

315.19

315.29

314.99

315.04

315.39

4.7  
15

4.8  
7.5

4.7

5.0  
7.5

4.95  
8.7  
Apron

4.60  
12.3  
Floor

314.82

314.82

5.17  
11.1  
Apron

5.17  
11.2  
Floor

314.73

314.75

5.26  
11.0  
Apron

5.24  
11.5  
Floor

314.71

5.22  
9.8

315.18

314.97

4.81  
21.5  
Floor

5.02  
18  
Apron

319.99

4+49.5 7.4' Rt End of House 7.3' Rt begin board Fence

4+46.5 7.2' Rt to Gas Meter

4+43 E Single Garage

4+40 7.3' Rt End of Porch and begin house

4+35 12.7' Lt to Conc. Slab <sup>So. Edge</sup> Single Garage

4+25 5.6' Rt to Meter box

T.P. 5.7' 321.70 4.03 315.96

4+17 2.1' Rt to Conc. Wall of Porch

4+15 5.3' Rt to 3' dia. Euc. Tree (Inside Edge)

4+11 5.7' Rt. to Very Rough Conc. Sidewalk set askew to Alleg

319.99

Lt.

Rt.

315.80  
5.9  
7.4  
Dirt  
315.54  
6.16  
7.4  
Bottom  
Foundation

24

316.13

5.57  
2.3  
Floor

315.70  
6.0  
7.3  
Dirt  
315.38  
6.32  
7.3  
Bottom  
Foundation

315.96

5.74  
12.7  
Apron

321.70

315.49  
4.5  
7.1  
Dirt  
315.31  
4.62  
7.1  
Bottom of  
Foundation

315.42

4.57  
5.7  
Conc  
4.8  
5.7  
Dirt

319.99

Lt.

Rt.

Rt.

5+29.5 8.6' Rt. to Conc. Apron of Single Garage Facing South

5+29 So. Edge Conc. Slab Double Garage

5+00

4+98 7.5' Rt So. Edge Conc. Slab

4+86 7.1' Lt to P. Pole P.A. 3265

4+81.5 7.6' Rt End Board Fence So. Edge Conc. Slab Double Garage

4+78.5 5.8' Lt to Meter box

4+50 12.5' Lt Conc. Slab (No. Edge)

321.70

317.64

4.06  
18.3  
Floor

316.80

4.9  
15

317.52

4.18  
10.3  
Apron

316.80

4.9  
7.5

316.60

5.1  
15

316.70

5.0  
7.5

316.60

5.1  
15

316.48  
5.02  
7.5  
Apron

316.49  
5.51  
15.4  
Break  
conc.

316.42  
5.28  
17.3  
Floor

316.54  
5.13  
7.6  
Apron

316.00  
5.70  
15.3  
Break  
conc.

316.30  
5.40  
17.2  
Floor

316.08

5.70  
12.5  
Apron

315.70

6.0  
7.5

315.60

6.1  
7.5

315.90

5.8  
7.5

316.00

5.7  
15

321.70

5780

5776 5.7' Rt. to Meter box

5763

5750

5748 7.8' Rt End of Garage

5744 No. Edge Conc. Slab.

5740 7.2' Lt to Meter box

5735 6.2' Rt to Meter box

5732 7.9' Rt to Edge of Garage

321.70

318.40	318.10	316.20	315.90	315.40	316.30	317.80	317.30
$\frac{31}{25}$	$\frac{36}{10}$	$\frac{55}{25}$	$\frac{58}{7}$	63	$\frac{54}{2.5}$	$\frac{39}{7.5}$	$\frac{44}{25}$

317.70

$\frac{40}{25}$

317.50

$\frac{42}{15}$

317.90

$\frac{3.80}{12.1}$   
Floor

317.60

$\frac{41}{25}$

317.40

$\frac{43}{25}$

317.72

$\frac{3.98}{10.0}$   
Apron

317.00

47

317.40

43

$\frac{54}{2.5}$

$\frac{39}{7.5}$

317.90

$\frac{43}{25}$

317.01

$\frac{4.69}{8.6}$   
Floor

317.80

$\frac{45}{25}$

317.30

$\frac{44}{15}$

317.20

$\frac{472}{124}$   
Floor

321.70

Check 1.51 322.63 = 322.59

T.P. 10.91 324.14 6.19 313.23

6+40.13 E Thorn

6+17.6

6+13.63 Cb. line

T.P. 6.68 319.42 8.96 312.74

6+00.13 So. Prop. Line Thorn St.

5+96 5.2' Rt to Exposed Water Main

321.70

N.W. B.P. Highland and Thorn

317.92	315.22	311.92	309.42	306.82
$\frac{15}{100}$	$\frac{42}{50}$	75	$\frac{10.0}{50}$	$\frac{12.6}{100}$
317.42	313.92	311.42	310.73	308.12
$\frac{2.0}{100}$	$\frac{5.5}{50}$	$\frac{82}{75}$	8.4	
318.12	315.12	311.82	310.52	308.66
$\frac{13}{100}$	$\frac{43}{50}$	$\frac{7.6}{7.5}$	8.0	8.9
			8.0	$\frac{8.9}{50}$
				113
				$\frac{10.76}{50}$
				$\frac{14.0}{100}$
				$\frac{133}{100}$
				305.42
				306.09
<u>314.50</u>	<u>313.10</u>	<u>312.90</u>	<u>312.20</u>	<u>311.42</u>
$\frac{72}{25}$	$\frac{8.6}{7.5}$	$\frac{8.8}{7}$	9.5	9.9
				$\frac{745}{100}$
				$\frac{14.66}{50}$
				311.04
318.90	318.30	313.70	312.80	313.10
$\frac{2.8}{30}$	$\frac{3.4}{17}$	$\frac{8.0}{7.5}$	$\frac{8.3}{7}$	8.9
				$\frac{8.6}{3}$
				$\frac{8.0}{3.5}$
				7
				$\frac{4.2}{7.5}$
				$\frac{4.5}{2.5}$

321.70

£

£

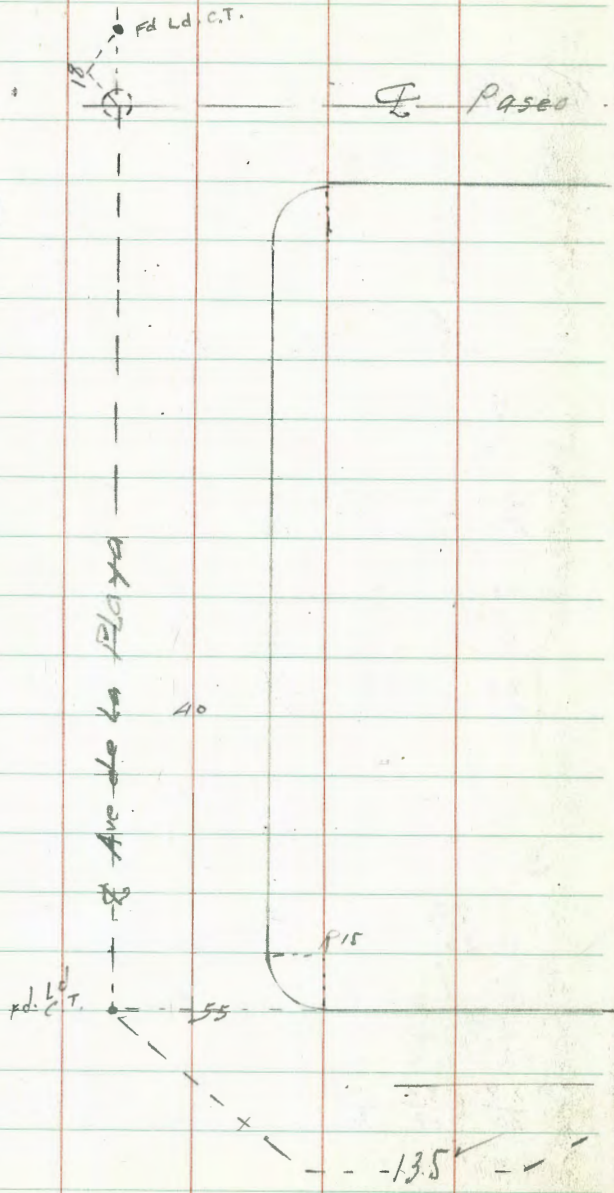
Rt

27

check Existing 8" Con. Curbs on  
Calle Clara

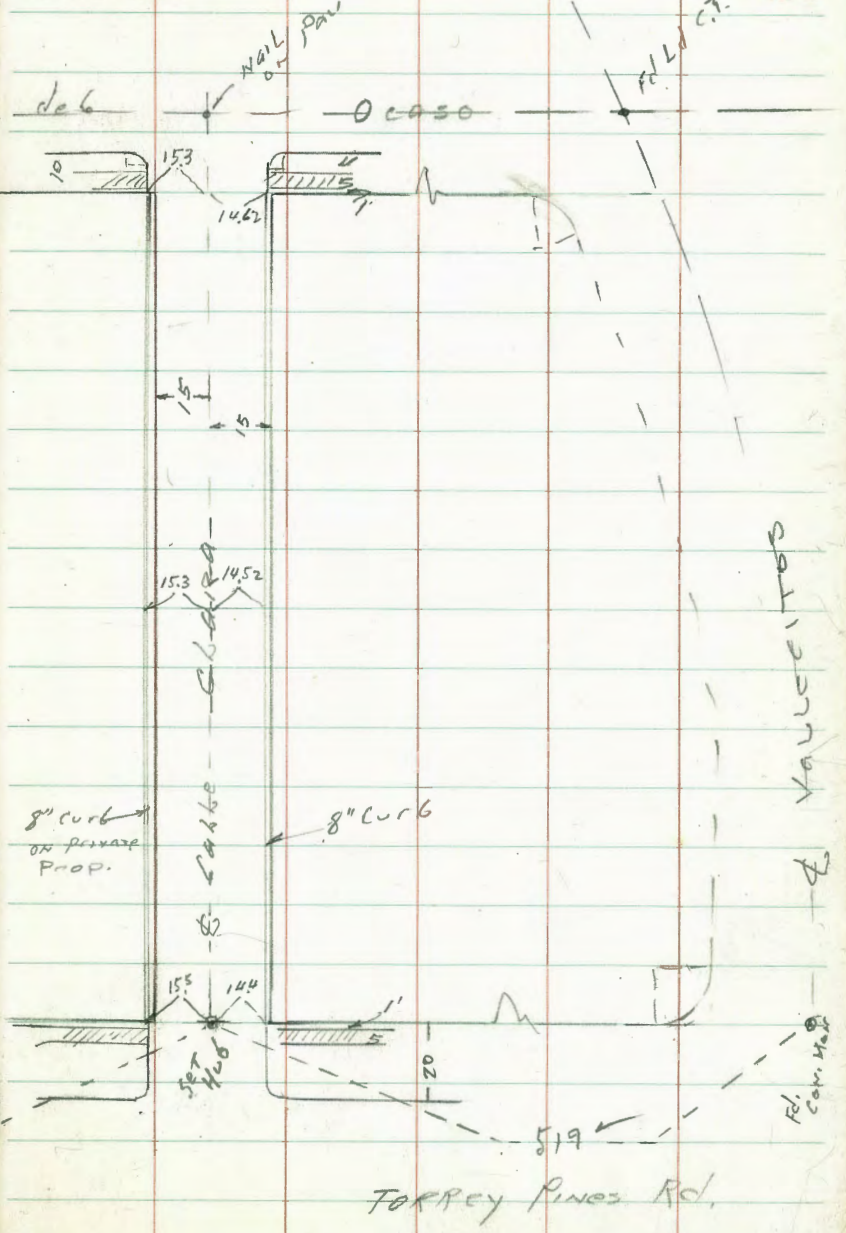
W.O. 21001

INDEXED  
WK  
MAR 14 1949



Moore 3-11-49  
8099  
Sherman

28



X-Section Alley BK 33 Ocean Beach

(Sunset Cliffs to Ebers between Newport & Niagara)

10-10-49

Roberts

Hendricks

Greer

Bunch

W.O.# 31638

Map 279

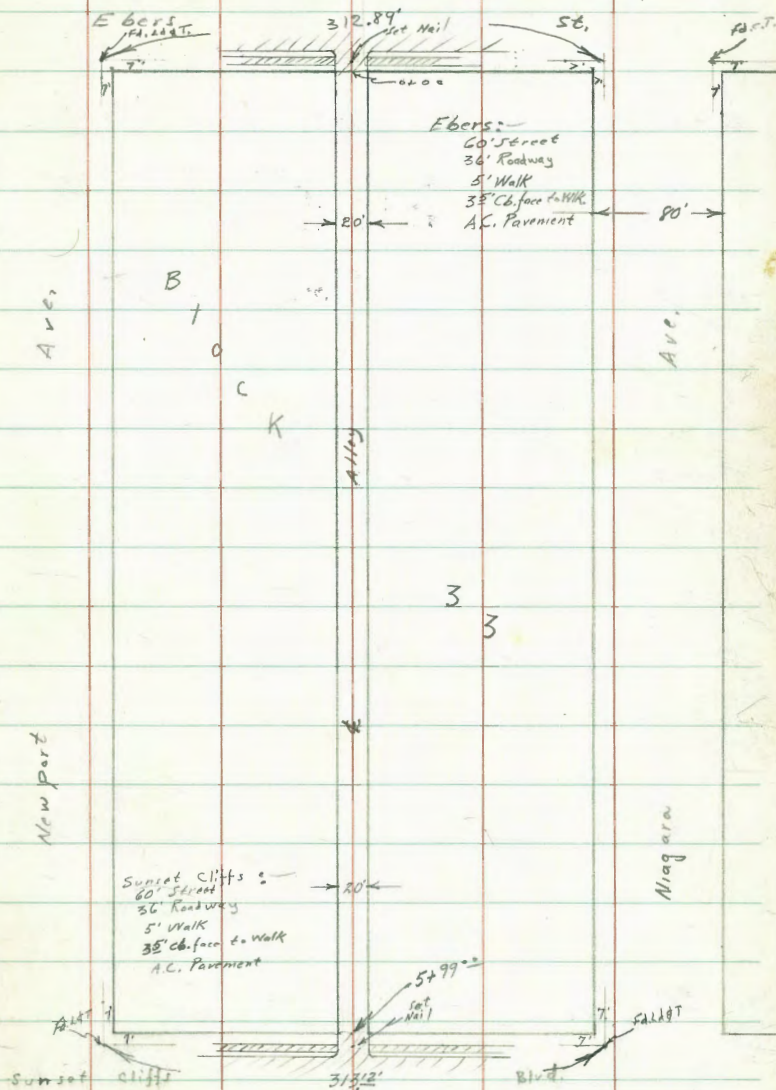
K.P. 776

INDEXED

W.K.

OCT 14 1949

NOTES REDUCED by MORGAN  
10-18-49





0+20	9' Rt End Ret. Wall							44.76	45.28
								28	28
								98	98
0+08	9' Rt Begin 05' Conc. Ret. Wall							46.16	46.46
								71	6.80
								92	93
0+00	10' Lt Conc. Ret. Wall Begins at End Curb Prop. Line Ebers Edge Pav.			47.92	47.50	47.03		47.16	47.39
				534	576	623		610	587
				66	92	9		925	9
0-10	E.C. Curb Returns			47.80	47.27	47.02		46.91	47.35
				546	599	624		635	591
				10	10			10	60
				66	9			9	60
0-12	Curb Line			48.69	48.14	47.83		47.24	47.22
				489	518	543		602	6.04
				66	90	12		12	10
				66	9	9		624	6.47
								10	6.57
								12	5.99
								9.44	7.52
								66	4
									6.90
									66
0-30	£ Ebers			48.97	48.03	47.70		47.57	46.54
				429	523	556		569	672
				30	10	10		10	50
BM	10.20	53.26	43.06	SWBP Newport £ Ebers					

0+96 15' Lt End Triple Garage

3894  
2.75 2.75  
152 132  
F1 Apron

0+72 15' Lt Begin Triple Garage

3911  
2.58 2.66  
152 132  
F1 Apron

0+67 10' Lt End Conc. Ret Wall

3937  
2.32 2.3 2.6 2.7 38.99  
10.1 10.1 20 20  
Ret Wall

T.P. 0.79 41.69 12.36 40.90

41.69

0+50 Ret. Wall 10' Lt

45.40  
7.16 12.3 12.5 12.4 12.4 12.9  
10 10 10 10 10 20  
Ret Wall

0+32 15' Ret Double Garage

43.81  
2.45  
132  
F1

0+25 Ret. Wall 10' Lt.

4789  
44.66 44.16 43.76  
5.37 8.6 9.1 9.5  
10 10 10 10  
Ret Wall

53.26

53.26

1780 15.2 Lt & Single Garage

1775<sup>E</sup> 9' Rt to Brick incinerator 2'x3'

1757<sup>S</sup> 15.3 Lt & Single Garage

1750

1749 8<sup>E</sup> Lt P. Pole #A4726

1732 9<sup>E</sup> Rt & Single Garage

1705<sup>E</sup> 13<sup>E</sup> Lt & Single Garage

1700

41.69

6.60  
15.2  
Fl.

6.60  
15.3  
Fl.

6.7  
17

6.5  
10

6.5  
5

6.7  
5

6.6  
20

6.4  
5

6.2  
10

5.9  
20

36.99  
47  
15

36.69  
5.0  
10

36.89  
48

36.89  
48  
10

36.99  
47  
20

41.69

35.09

35.09

6.77  
17  
Apron

34.92

6.77  
17  
Apron

75.29

35.49

35.79

5.9  
Dist  
Fl.

36.79

4.90  
13<sup>E</sup>  
Fl.

36.89

35.79

5.9  
Dist  
Fl.

36.89

7.04  
12.2  
Apron

34.65

2+61 15.3' Rt & Double Garage

2+50

2+41 16.5' Rt & Single Garage

2+07 15' Rt & Single Garage

T.P. 2.90  $\frac{36.41}{1}$  8.18 33.51 Nail in P. Pole #? 24 2+40

2+00

1+93 13.5' Rt & Single Garage

$\frac{41.69}{1}$

At

&

E.

$\frac{32.81}{20}$

$\frac{32.91}{10}$

$\frac{32.71}{3.7}$

$\frac{32.71}{10}$

$\frac{32.81}{3.6}$

$\frac{32.61}{3.8}$   
 $\frac{13.3}{13.3}$

32.93

$\frac{33.41}{16.5}$   
 $\frac{16.5}{16.5}$

3.48  
142  
Apr 00

3.00  
16.5  
FI

33.81

$\frac{2.60}{15}$   
FI

$\frac{36.41}{1}$

$\frac{33.79}{15}$

$\frac{34.19}{10}$

$\frac{33.79}{7.9}$

$\frac{33.79}{3}$

$\frac{34.09}{10}$

$\frac{33.89}{15}$

34.49

72  
136  
Dist  
FI

$\frac{41.69}{1}$

3740 14' RT & 4 Car Garage

3720 14' RT & Single Garage

3709 18.6' RT & Single Garage

3702 14' Lt Begin 4 Car Garage Dirt Floor

3700 & Manhole

2781 8.7' Lt. P. Pole #?

2775 11.1' RT. & 2' Conc. Walk

36.4

Lt

£

Rt

NO BIST  
4.0  
4.0

32.11  
4.24  
1.24  
32.39  
4.02  
1.86  
11.86

32.01  
4.4  
14.1

32.21	32.21	31.81	31.73	31.61	32.01	32.11
7.2 15	4.2 10	4.6 5	4.8 3 MAN RHS	4.8 3	4.4 10	4.3 19

32.72  
36.9  
11.1

32.71  
37.0  
14

36.41

lt

\*

30.09

30.42  
5.99  
14.9

4741 Rt End 4 Car Garage

4711 14.4 Lt Begin 4 Car Garage

4702 15' Rt Begin 4 Car Garage

4700 10.3 Lt Begin of walk going into Apron

3799 8.9 Lt P.Pole # PA 4766

3789 15.5' Rt & Single Garage

3750

36.41

31.07

5.57  
14.5  
walk

31.10

5.31  
10.3  
walk

31.01

5.74  
10

30.31

6.1  
7

30.11

6.3  
10

30.01

6.4  
10

30.01

6.4  
20

30.10  
6.31  
11.1  
Apron

30.94  
6.00  
15.1

30.62  
5.79  
14.4  
FI

30.38  
6.09  
10.3  
Apron

31.41

5.0  
20

31.21

5.2  
10

30.91

5.5

30.81

5.6  
5

31.21

5.2  
8

31.01

5.4  
0

30.81

5.6  
25

36.41

4+975 13.9 Rt & 2' Conc. Walk

4+965 10.4 Lt & 2' Conc. Walk

4+955 139' Rt End 3 Car Garage

4+87 14.6 Lt End 4 Car Garage

4+535 14.5' Lt, Begin 4 Car Garage  
13.8' Rt Begin 5 Car Garage

4+49 10.4' Lt & 2' Conc. Walk  
10.8' Rt & 2.5' Conc. Walk

4+45 14.4' Lt End 4 Car Garage

36.41

Lt

Rt

2942

Rt

36

3039  
6.02  
24

3019  
6.22  
10.4  
Walk

6.99  
13.9  
Walk

6.99  
28

2977  
6.64  
11.9

3039  
6.02  
14.6  
Fl.

2972  
6.69  
10.5  
Apron

3032  
6.09  
14.5  
Fl.

2986  
6.55  
10.3  
Apron

2971  
6.70  
13.8  
Fl.

3066

3036  
5.75  
28

3009  
6.32  
10.4  
Walk

3001  
6.4  
10

2957  
6.9

2941  
7.0  
3

2971  
6.7  
10

3006  
6.35  
10.8  
Walk

3005  
6.36  
11.4

2986  
6.55  
25

3059  
5.82  
14.4  
Fl.

3032  
6.09  
10.4  
Apron

36.41

5+50

5+36 14.1' Rt End 4 Car Garage

5+17 14.4' Lt & Single Garage

5+07 15.44' & Single Garage

5+02 14.4' Rt Begin 4 Car Garage

5+00 8.7' Lt P. Pole #? 14.4' Rt 3.5' Conc. Walk

T.P. 3.39 32.60 7.20 29.21

36.41

← 29.10 28.50 28.20 28.10 28.20 28.90 27.80  
 3.5 4.1 4.4 4.5 4.3 4.2 4.8  
 20 10 3 6 10 20

29.25  
3.35  
 14.1'

29.50  
 3.1  
 14.4'

29.98  
2.62  
 15.4  
 Ft.

29.33  
3.27  
 14.4  
 Ft.

30.00 29.60 29.00 28.90 29.20 29.44 29.64  
 2.6 3.0 3.6 3.9 3.4 3.16 2.8  
 16 10 4 10 10 14.4 Walk 30

32.60



Check 6.56 26.04 = 26.04

6+29 £ Sunset Cliffs

6+11 Curb Line

6+09 BC. Curb Returns

5+99 Prop. Line Sunset Cliffs

5+71

32.60  
/

N.W. B.P. Niagara & Sunset Cliffs

				2630		2616	2610	2603	
				6.30		6.44	6.50	6.57	25.95
				50		10	10	10	30
2669	2615								
				2667	2609	2612	2608	2599	1599
5.91	6.45	5.73	6.57	6.48	6.52	6.61	6.61	5.99	2661
50	50	12	12	10		10	12	12	12
cb	Gutt	cb	gutt				gutt	cb	gutt
				1761	2625	2617	2619		
				5.99	6.35	6.43	6.41	6.14	2646
				10	10		10	10	10
				cb	gutt		gutt	cb	cb
				2750	2677	2652	2655	2678	2680
				2760					
				5.2	5.17	6.08	6.05	5.92	5.8
				24	10		10	10	23
				cb	gutt		gutt	cb	
				2894	2790	2740	2760	2730	
				3.7	4.7	5.2	5.0	5.3	
				16	10	9	10	22	

32.60  
/

7-Sect. Chatsworth Blvd. - from  
 Catalina to Coronado - for Grade est.  
 Sketch in Book 1386 - P. 1 - Shows  
 Location of improvements - same as  
 now - will refer to it. - Consider Chatsworth  
 as E. + W. - 0+00 will be 250' W. along the  
 E. of a 465' Rad. Curve.

T.P. 0.34 193.37 12.74 193.03

1+50

**INDEXED**  
 N.K.  
 JAN 27 1950

1+00

0+50

Sections are Radial

0+00 - is 17 E. of E.L. Catalina

B.M. 4.16 205.77

201.61 - N.E. B.P.

# 4146  
W.O. 25020

Osborne  
Hardin  
Hatch  
Shepard

39

LT = N. & RT = S

SEE FB 2037

33

5.5 35	200.6	8.2 35	197.6	10.0 20	195.8	10.18 9.5 edge	195.59	10.47	195.30	10 10 edge	194.91	11.1 15	194.7	10.3 35	195.5	12.4 50	193.4
5.3 50	200.5	6.0 35	199.8	7.2 20	198.6	6.93 9.7 edge	198.84	7.22	198.53	10.4 edge	198.06	7.5 15	197.9	7.3 35	198.5	8.1 100	197.7
3.5 35	202.20	3.6 27.1 edge	202.16	4.53 4.5 edge	201.94	4.82	201.95	5.19 10.3 edge	201.58	5.5 35	200.3	5.5 35	200.3	5.5 35	200.5	5.5 35	200.5
		2.92 35	202.85	2.83 10	202.94	3.12	202.65	3.60 10 edge AC curve	202.17	3.1 35	202.7	3.1 35	202.7	3.1 35	202.4	3.1 35	202.4

Chatsworth  
+ Catalina

205.77

Chatsworth

4+00

3+70 = Lowest pt. on Rave

10' see B. 1386-P-11 for Culvert

3+60 = Show Conc. Slab. culvert on Rt

3+50

3+00

2+50 = P.C. of Curve

2+00

	183.3	182.3	185.6	184.7	184.61	184.74	184.64	185.2	184.5	178.8	177.9
	10.1	17	7.2	8.7	9.76	8	8.13	9.7	9.9	14.6	15
	10.0	5.0	3.5	1.5	9.3	6.1	10.8	2.0	3.5	5.5	10.0
	183.1	181.7	185.6	184.1	183.94	184.02	183.74	184.3	183.0	178.4	162.3
	10.3	11.7	7.2	9.3	9.43	9.35	9.63	9.1	10.4	18.0	3.1
	10.0	5.0	3.5	2.0	9.4	9.3	10.7	3.0	3.5	7.3	9.0
					184.07	184.09	183.66	182.68	183.0	177.0	166.5
		12.2	8.1	9.3	9.3	9.28	9.71	10.69	16.4	26.9	
		5.0	3.5	9.4	9.4	10.8	10.8	13.0	3.5	6.0	in Wash
					184.28	184.30	184.03	184.8	183.6	177.7	
		10.182.8	8.185.4	9.184.28	9.184.30	9.184.03	9.184.03	9.184.8	9.183.6	15.177.7	
		5.0	3.5	9.4	9.4	10.6	10.6	12.7	3.5	5.0	
					185.2	185.9	185.42	185.9	186.3	184.8	181.8
		8.185.2	7.185.9	7.185.77	7.185.72	7.185.42	7.185.42	7.185.9	7.186.3	8.184.8	11.181.8
		5.0	3.5	9.3	6.5	10.10	10.10	2.0	3.5	5.5	10.0
		182.4	189.3	188.5	189.43	189.21	187.70	188.9	189.6	190.0	
		4.0	4.1	4.9	4.94	5.16	5.67	4.5	3.8	3.4	
		5.0	3.5	2.3	9	10.4	10.4	2.5	3.5	5.0	
		195.7	193.4	191.5	191.86	191.62	191.32	192.4	191.8	192.7	
		2.3	0.0	2.1	1.51	1.75	2.05	1.0	1.6	1.0	
		5.0	3.5	2.0	9.3	10.5	10.5	2.5	3.5	10.0	
					edge	193.37	193.37	193.37	193.37	193.37	

Chatsworth

T.P. 13.24 218.40 0.33 205.16

7+00

6+50

6+00

5+50

I.R 13.06 205.49 0.94 192.43

5+00

4+50

4+25

4.201.5 100	4.202.8 35	4.202.7 26	4.201.6 22	4.202.51 9.4	4.202.63 2	4.202.62 10.6	4.202.2 22	4.202.7 35	4.202.5 100
5.199.9 50	5.200.5 35	5.199.3 27	5.198.6 23	5.199.47 9.4	5.199.67 5.82	5.199.54 10.6	5.199.1 22	5.199.5 35	5.198.7 50
5.198.2 50	5.197.4 35	5.196.7 26	5.195.3 22	5.196.32 9.4	5.196.48 9.01	5.194.29 10.6	5.195.1 22	5.196.4 35	5.193.8 100
5.194.5 50	5.194.2 35	5.192.5 20		5.193.07 9.3	5.193.20 12.29	5.193.11 10.6	5.192.4 20	5.193.2 35	5.192.0 50
5.187.6 80	5.188.9 45	5.190.5 25	5.189.7 20	5.189.99 9.4	5.190.10 3.27	5.190.01 10.6	5.189.0 23	5.189.7 35	5.188.0 100
5.183.5 50	5.187.4 35	5.187.0 25		5.186.87 9.4	5.187.02 35	5.186.84 10.6	5.187.4 25	5.186.7 35	5.186.3 50
5.182.5 50	5.180.7 35	5.185.4 20		5.185.57 9.3	5.185.66 7.71	5.185.57 10.6	5.185.7 35	5.182.0 50	
					193.37				

Chatsworth

10+00

T.P. 1178 229.08 1110 217.30

9+50 = ct. for sketch  
 9+31.87 = \$ at M.L. of Orchard - See B. 1386-P-2

Set BM. on ct. 3.76 214.64

9+00

8+75

8+50

8+00

7+50

15.1 100	11.1 40	11.9 35	10.1 29	11.9 9.6 F	11.8 82	11.9 10.4 F	12.3 20	11.6 32	8.3 35	7.2 50	7.2 100
216.7	217.4	214.8	214.0	215.22	229.08	215.20					
1.7 50	1.0 40	3.6 35	4.4 26	3.18 9.7 F	3	3.20 10.6 F	4.2 9	3.1 31	4.04 35	1.3 50	
210.8	214.6	212.6	211.9	213.06		213.15	212.6	213.9	216.0	216.7	
7.6 100	3.8 40	5.4 35	6.2 25	5.34 5.6 F	5.15	5.2 10.4 F	5.2 9	4.5 32	2.4 35	1.7 100	
	211.7	211.7	210.8	212.03	212.19	212.120	211.5	213.2	213.8		
	5.7 50	5.7 35	7.6 27	5.9 5.6 F	6.21	5.2 10.3 F	5.4 21	5.2 32	4.6 50		
	209.8	209.8		210.82	211.08	211.06	210.5	211.8	212.8		
	9.6 50	8.6 35		7.2 9.2 F	7.32	7.3 10.4 F	7.9 20	6.6 35	5.1 0		
206.1	206.7	208.5	207.8	208.26	208.43	208.39	208.1	209.0	210.4		
12.3 100	11.7 43	9.9 35	10.2 19	10.14 9.4 F	9.97	10.01 10.4 F	10.3 9	9.4 35	8.2 100		
204.0	205.9	205.7	204.7	205.56	205.73	205.60	205.3	206.0	206.0		
14.4 45	12.5 35	17.7 26	13.7 22	12.4 9.4 F	12.67	12.80 10.6 F	13.1 23	12.4 35	12.4 50		



Chatsworth

15+00

14+70 = lowest pt. on Pauc- for Culvert See

14+50

14+00

13+50

13+17.84 = ct. = + S. 7' Line Prod. of Del Mar.

B.M. on above ct.

13+00

T.P. 2.74 219.03 12.79 216.29

12+50

5.1 100	6.0 50	6.0 35	6.0 20	7.04 9.6	6.22.05#	7.09 10.4	7.6 20	8.0 35	10.2 45	12.206.9
213.9	213.0	213.0	213.0	211.99	212.05#	211.94	211.9	211.0	208.8	44
6.213.5	6.212.8	6.212.1	7.211.80	7.211.90	7.211.82	7.211.3	7.211.3	7.209.5	9.209.4	
50	35	19	9.6	13	10.5	20	35	42	50	
5.212.1	7.212.0	5.212.7	7.211.90	7.211.94	7.211.82	7.211.7	7.211.7	10.208.6	10.208.4	
50	40	35	9.6	9	10.5	20	35	45	55	
4.214.7	7.211.8	6.212.7	6.212.6	6.212.55	6.212.45	5.213.6	5.213.2	11.208.0	12.206.1	
100	45	35	20	48	6	18.4	35	47	100	
5.213.4	6.212.7	5.213.59	5.213.68	5.213.60	5.214.7	4.214.7	5.214.0	8.210.1	10.208.9	
50	0	35	35	10.4	12	32	35	48	55	
4.214.1	4.214.4	3.215.14	3.215.29	3.215.19	4.215.0	3.215.5	5.213.2	6.212.6		
50	35	9.4	7	10.5	20	35	50	100		
12.216.2	12.216.9	12.215.9	12.216.83	12.217.01	12.216.7	11.217.4	10.218.3	10.218.2		
50	35	23	9.6	9.6	19	25	37	50		
			229.08	219.03						

Chatsworth

17+75

B. 1386 - P. 4

17+74.53 = opp. Hub. - N. + S. 7 Coronado - Sec

17+50 = Beg. Cold lay shoulder on Lt.

17+25

17+00

T.P. 4.63 217.94 5.72 213.31

16+50 = Beg. Cold lay shoulder on Rt.

16+00

15+50

2.8 50	3.1 40	4.0 35	5.4 20	5.0 12	4.9 15	4.8 10	4.8 10	4.7 20	4.6 35	5.2 50
2/15.71	2/14.8	2/13.9	2/12.5	2/12.9 Lt.	2/12.99	2/13.14	2/13.12	2/13.2	2/13.3	2/12.7
4.2/6.5	2.2/5.7	4.2/3.9	5.2/2.9	4.2/3.3	4.5/2/3.39	4.2/3.50	4.2/3.47	4.2/3.6	3.2/4.1	2.2/4.6
50	35	33	20	edge	edge	edge	edge	edge	edge	edge
1.3 50	1.6 40	3.9 35	2.9 20	4.2/3.0	4.2/3.54	4.2/3.69	4.2/3.61	4.2/3.4	3.2/4.1	3.2/4.3
2/16.6	2/16.3	2/14.0	2/13.0	2/13.5	2/13.64	2/13.52	2/13.61	2/13.4	2/14.1	2/14.3
0.2/17.5	1.2/16.2	3.2/14.1	4.2/13.0	4.2/13.51	4.2/13.64	4.2/13.52	4.2/13.61	4.2/13.2	3.2/4.1	3.2/4.3
10.4	4.0	3.5	2.0	9.7	4.3	3.0	10.3	2.0	3.5	10.6
2/15.3	2/15.0	5.4/2/3.6	5.2/2.7	5.2/2/3.19	2/17.94	2/13.3	5.2/2/3.15	6.2/2.7	5.2/2/3.2	5.2/3.0
3.7 50	4.0 35	5.4 33	5.2 20	5.2 12	5.2 15	5.2 10	5.2 10	6.2 20	5.2 35	5.2 50
2/15.4	2/13.2	2/12.7	2/12.76	2/12.96	2/12.78	2/12.78	2/12.2	2/12.8	2/11.3	2/11.0
3.6 100	5.2 35	6.2 20	6.2 15	6.2 13	6.2 10	6.2 10	6.2 20	6.2 35	6.2 50	6.2 100
5.2/2.7	5.2/3.0	5.2/2.5	6.2/2.44	5.2/2.52	6.2/2.41	6.2/2.41	6.2/2.2	6.2/2.8	6.2/2.19	6.2/2.98
5.0	3.5	2.0	9.6	5.1	6.2	6.2	2.0	3.5	5.0	9.6
			F	219.03	F	F				



Chatsworth

Dixon  
check B.M. N.W. B.P.

9.05 197.66 197.67

B-1386-P. 21

T.P. 1.18 206.71 12.41 205.53

19+00 = end.

18+50

18+25

18+00

Ltr

#

Rt.

46

5.209.7 50	5.209.0 35	5.208.3 20 edge	5.208.86 9.08 9.6	5.209.06 8.88	5.208.99 9.00 10.3	5.208.5 9.4 20 edge	5.209.1 8.8 35	5.210.4 5.5 50
5.211.1 50	5.211.1 35	5.210.0 20 edge	5.210.82 9.6 9.6	5.211.01 9.3	5.210.92 10.3 10.2	5.210.3 20 edge	5.210.9 35 40	5.211.7 5.5 50
5.212.6 50	5.211.0 35	5.211.3 20 edge	5.211.69 9.6 9.6	5.211.87 9.0	5.211.73 10.3 10.2	5.211.2 20 edge	5.211.7 35	5.211.6 5.5 50
5.212.9 50	5.212.6 35	5.212.0 20 edge	5.212.34 9.6 9.6	5.212.50 9.4	5.212.45 10.3 10.2	5.212.3 20 edge	5.212.2 35	5.212.0 10.0 50

Moore  
Begg  
Crawford Blk 317 Reed and Dabey's Add  
4-7-50

V.O. 31811

□ 307 202 Hub disk

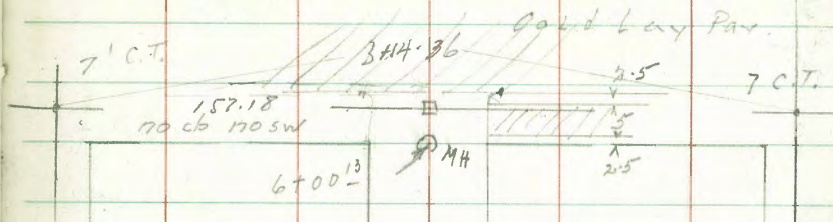
INDEXED

M.K.

APR 11 1950

29th St

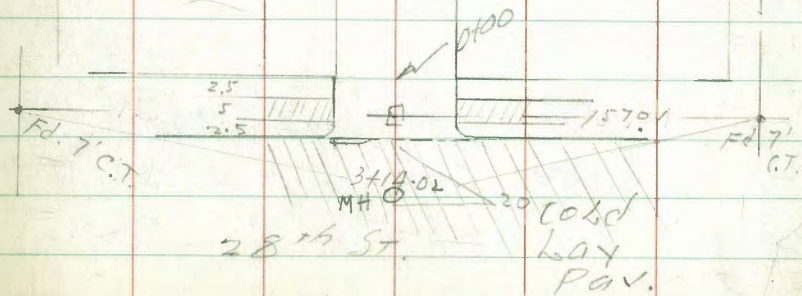
47



Franklin

MH 0 @ Soil Sample 2+90  
10 10

□ 1100 P.O.T.



TP  
1701 on Pole  
0 + 07

8.72	101.84	0.34	93.12
------	--------	------	-------

0 + 01 beg Stucco Blkg 11.9.19

0 + 0.0 end of cb 9.96 9.9

Reduced April 11, 1950  
John Firebaugh

0 - 10 curb line 28 St end of Par

0 - 30 of 28 St

NEBP	241	93.46	4.94	91.05	91.05
TP	253	95.99	10.11	93.46	
BM	612	103.57		97.45	

90.2	91.2	90.2	91.2	93.5	93.5	48
3.7	2.2	2.7	2.5	0.0	10	
10	8		6	9		

89.2	89.2	90.1	90.6
3.6	3.6	3.4	2.9
10		7	11.9

89.87	89.7	89.8	90.2	89.94
3.59	3.8	3.7	3.5	3.52
9.9	9.9		9.9	curb
cb				

88.50	87.85	89.67	88.75	88.99	89.11	89.70	89.21	90.00
4.96	5.61	3.79	4.71	4.47	4.35	3.76	4.25	3.46
50	50	50	10.9		10.9	50	50	50

87.78	88.7	88.85	83.58	88.98	89.41
5.68	4.8	4.61	4.48	4.48	4.05
50	10	M.H.	Flow Line	10	50

28th + OceanView Blvd

NEBP OceanView Blvd + 29th St

0+76 Sec

972	972	972	972	980	986	986
3.9	4.1	3.9	4.1	3.8	3.2	3.2
20	10	7	7	10	10	15

0+72 end of Ret Wall & Pipe face  
 Vertical face 13.0R

905	905	941	975	972	976	981	973	92.66
11.3	11.3	7.7	4.3	4.4	4.2	3.7	4.5	9.18
20	12	10	7	7	7	10	13.0	conc slab

Ret Wall

0+52 Sec

900	900	900	958	955	958	963	966	963	92.61
11.8	11.8	11.8	6.0	6.3	6.0	5.5	5.2	5.6	9.23
20	10	9.0	8	6	8	10	12.8	12.8	conc slab

Wall

0+37 11.7 vertical face  
 beg conc. ret wall & Pipe fence

900	903	902	945	941	942	950	951	952	959	92.70
11.8	11.5	11.5	7.3	7.7	7.6	6.8	6.7	6.6	6.0	10.0
20.8	10	9	9	7.7	6	9	10	11.7	11.7	conc paving

Strucco Dred top of ret wall

0+37 end of concrete Bldg 11.7 ft

0+23 Pole 460856 # 8.8 Lt.  
 note offset to poles property side

903	903	903	930	925	929	932	942	941	91.59
11.5	11.5	11.5	8.8	9.3	8.9	8.1	7.6	7.7	10.35
25	10	9.0	7	6	7	10	11.8	11.8	floor of Bldg

101.84

101.84

TP 510 104.82 2-12 99.72

1+35 Tel pole 9.0L Prop edge JTA 2811

1+34 d S. gar dirt floor 10.4R

1+30 end Picket Rt 10.4

1+25 beg picket 10.4R

1+00 sec PPole A 2810 9.3 Rt Prop. edge

0+85 beg bd fence 10.5Rt

0+80 d Sng gar 10.4 Rt dirt floor  
fin

101.84

6 4 R

99.5 99.2 99.2 100.5 100.5

2.4 1.9 1.9 1.3 1.3  
20 16 10 10.4  
floor

99.5 99.1 99.1 99.4 99.8 99.5

2.7 2.7 2.7 2.4 2.0 2.3  
19 10 7 10 20.  
Fram  
dirt

101.84

99.0  
2.7  
10.4

1+87 beg Picket Rt 10.6

1+85 Sing gar 144 ft 11.7 Lt apron 10 W

1+80.5 of Sing gar bd 13.3 Rt 10 wide conc of 10.8 Rt

1+75 S E cor Stucco Bldg 9.6 Lt

1+71.5 E edge of conc slab

1+64.5 of conc steep 3.6 wide x 17 8.0 Lt

1+55 W edge of conc slab

1+43 beg Stucco Pwel SW cor 9.8 Lt

1+42 end of Picket 9.8 Lt

104.82

L

S

R

99.8

99.81

5.0

5.01

14.4  
floor

11.7  
apron

100.81

100.99

4.01

3.83

10.8

13.3

apron

floor

99.8

99.9

5.4

4.9

9.6

9.6

fdt

99.9

100.2

100.9

101.10

101.63

4.9

4.5

3.9

3.72

3.19

9.6

10

11.6

20

101.08

100.88

100.85

100.2

3.74

3.94

3.97

4.6

floor

9.8

8.0

8

99.9

100.2

100.2

100.2

100.2

101.07

101.47

5.1

4.8

4.7

4.7

4.0

3.75

3.35

9.8

9.8

9.8

10

11.5

20

fdt

conc

104.82

R+50 SE cor Bd gar 9.1 Lt

R+45 of Sing gar dirt 12.5 R

R+45 of gar 9.1 Lt conc floor

R+41 end of bd fence 12.5 R

R+30 { 11.7 R beg bd fence  
9.3 Lt SW cor Bd gar

R+23 of Sing gar dirt floor 10.3 R

R+06 of Sing gar dirt floo 10.3 R

R+00 { end Picket 10.5 R  
P Pole 10 R A 2830  
Prop edge

104 82

99.90 100.1 100.3 100.7  
4.92 4.7 4.5 4.1  
0.070 10  
9.1

99.90 101.2  
4.92 3.8  
9.1 12.5

98.2 99.1 99.6 100.0 100.3 100.8  
6.1 5.7 5.2 4.8 4.5 4.0  
2.0 7 7 10.3

100.8  
4.0  
10.3

99.2 99.2 100.4 100.9 101.9 102.3  
4.9 4.9 4.4 3.9 3.9 2.5  
1.0 7 10 11 2.0

104 82

B+98 3' conc walk 10.1R

B+96 N.E cor Bd Dwell 10.2 R

B+90  $\frac{1}{2}$  Sewer MH

B+76 N.W cor dwelling 10.1 R

B+74

B+69 E edge conc apron 10.2R

B+54 8.8 ft Tel Pole 460854 H  
Prop edge

B+51 Wedge DBI gar  
conc apron 10.3R

104.82

L

E

R

102.70

8.12  
10.1  
walk

41.0

10.2 ft  
red wood mud sill

377  
Rim

10.2  
3.9  
ft

1004  
4.4  
75

1005  
4.3  
10

1004  
4.4  
5

1007  
4.1  
5

1013  
3.1  
10.1

101.80  
3.02  
10.1  
3' conc walk

100.82  
4.00  
10.2

101.02  
3.80  
floor 12.1

100.68

414  
10.3

101.00  
3.78  
12.3  
floor

104.82



3+50 end Bd fence 10.2 R  
 3+50 end shed beg bd fence 9.6 L  
 3+42 Tel Pole 8.7 L 460853A  
 3+42 beg Bd fence 10 R  
 3+42 2' wide con steps 10 R

3+28 9.6L end bd fence } beg shed 5d

3+09 d E 2 19.6 10 9 R

3+08 3 wide con stop 9.5 L

3+04 d W 2' R 10.8 R

T.P. 5.24 106.52 4.14 10068

3+00 { beg Bd fence 9.6  
 P Pole 9.3 R prop edge 2.850 A  
 10H 82

100.9  
 3.9  
 9.5  
 shed

100.6  
 4.2

101.5  
 3.7  
 10

102.20  
 2.60  
 Top of  
 bot step

100.10  
 4.72  
 11  
 door sill

99.92  
 4.90  
 9.5

100.51  
 4.31  
 10.9

101.41  
 3.41  
 21.90

100.53  
 4.29  
 10.8

101.41  
 3.41  
 21  
 90

100.8  
 4.0  
 2.0

101.0  
 3.8  
 9.6

101.2  
 3.6

101.6  
 3.2  
 10

102.2  
 3.6  
 10

104.82

4+82 end fence 10.6 R

4+81 3' conc Wlk 11 R

4+73 E edge " " 14 L

4+58 W edge Dbl gar 14 L

4+50 end bd fence 10.1 L

JP. 430 107.27 <sup>2</sup> 355 102.974+00 P.Pok P.A. 2870 9.5 RR  
prop-else

3+68 beg bd fence 10.2 R

3+56  $\frac{1}{2}$  Sing bd gar 10.4 R104.82

L

R

R

1031	1029	1027	1024	102.43	
4.2 18	4.4 10	4.6 10	4.9 10	4.94 11	
10312	102.20				
4.5 14	4.07 14				
1029	1029	1029	1028	1028	1024
4.4 20	4.4 10	4.5	4.7 10	4.7 10	4.9 15
				fence	

1019	1011	1015	1015
3.8 25	3.7 10.1	3.3 10.1	3.3 10.1
	fence		fence
1009	1011	1012	1018
3.9 20	3.7 9.8	3.6	3.0 10
	fence		
			1015
			3.2 10.4

104.82

5+50 beg Conc Wall 10' FT

5+33 } conc apron 17.8 FT

10.4 Lt  
beg ornamental wire 2" pipe posts  
10.5 Lt  
end bd fence

5+33 } end bd fence

5+17 } 5 1/2" gar 8' wide apron

5.02 } TPole 9.8 FT PA 2882 prop. use.

5+00 } 10.2 Lt beg bd fence

5+10 } TPole 9.1 Lt 460852 H

H+98 } E edge conc apron 11.7 L

H+83 } Wedge conc apron DBL gar

107.27

56

10.3  
fence

102.8  
4.5  
10

102.3  
5.0  
5

102.9  
5.3  
10

101.8  
5.5  
10

101.2  
6.1  
ft.

103.0  
4.3  
15

103.1  
4.2  
10

102.5  
4.8  
10

102.2  
5.1  
10

102.21  
5.06  
17.8

102.25  
5.02  
19.3

102.2  
5.0  
18

102.4  
4.9  
20

102.5  
4.8  
10

102.6  
4.7  
10

103.1  
4.2  
10

102.28  
4.9  
13.3  
ft.

102.21  
5.06  
11.7

102.34  
4.93  
13.2  
gar

102.36  
4.91  
10.4

107.27

6+10<sup>13</sup> Wcb line 29

6+00<sup>13</sup> Prop line 29 St

536 102.16 10.47 96.80

5+90

5+81 beg conc ret wall 8"

5+72

5+56 Sing gar 14.7 ft

107.27

948	963	955	956	9575	9658	9659	9719
7.4	5.9	4.7	6.6	6.41	5.58	5.57	4.97
50	10	5		10	2+ret	10	cb
dirt						old	50

964	972	9681	973	9669
5.8	4.5	3.35	4.9	5.47
base conc	10	M.H. rim	10	cb
ret wall				10R

1005	10167	988	983	986	974
6.7	5.60	8.5	9.1	8.7	9.9
fdt	10.2	5		10	10.1
10.2	conc				fdt
	ret wall				

1018	10226
5.7	5.01
ret wall	10.1
fdt	fence
	beg conc
	ret wall

1022	1018	1009	1005	1009	998
5.1	5.5	6.4	6.8	6.4	7.5
10.3	7	5		10	10.1
wire					fdt
conc					

10305	1027	1018	1015	1009
4.22	4.6	5.5	5.7	6.4
14.2	10.3		10	fdt 10.1
	wire			wall
	gate			

107.27

4.70 97.46 97.45

6+30 of 29th.

6+11 edge of cold lay paring

102.16

Starting BM

93.96  
8.20 6.30 5.24  
50 50  
cold lay

93.26  
8.90 7.15 6.81 6.50  
50 10 10  
cold lay

102.16

1/2 sec 20" Alley

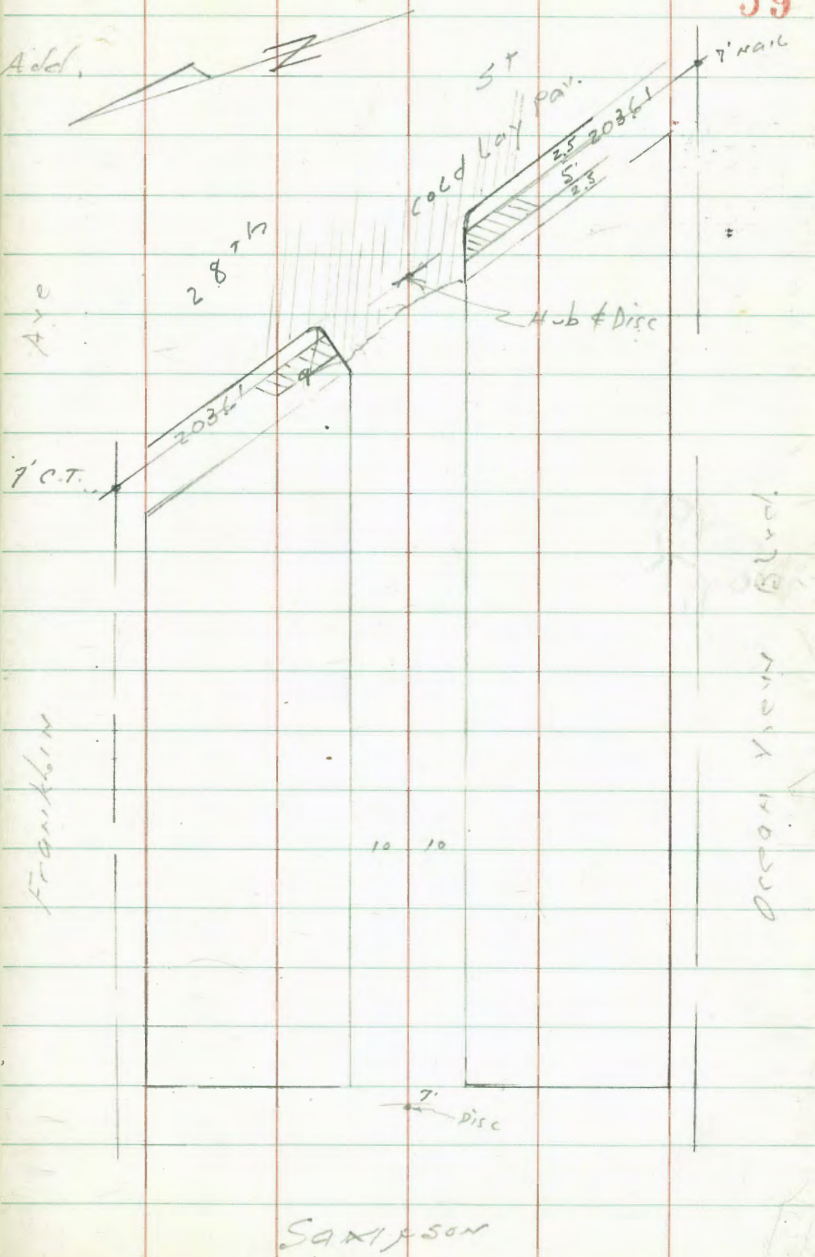
BLK 281 San Diego Land & Town Co. Add.

59

INDEXED  
W.K.  
APR 11 1950

118 10 31 811

Contd. Blk. 1847-63



Point of st

INDEXED  
OCT 18 1950

30' dia Rod

2+39.7 w.l.

Nix line P.L. 182

Prop. opening

Talbot St

Catalina Blvd.

Fd. spike

40' 20' 20'

Manor Way

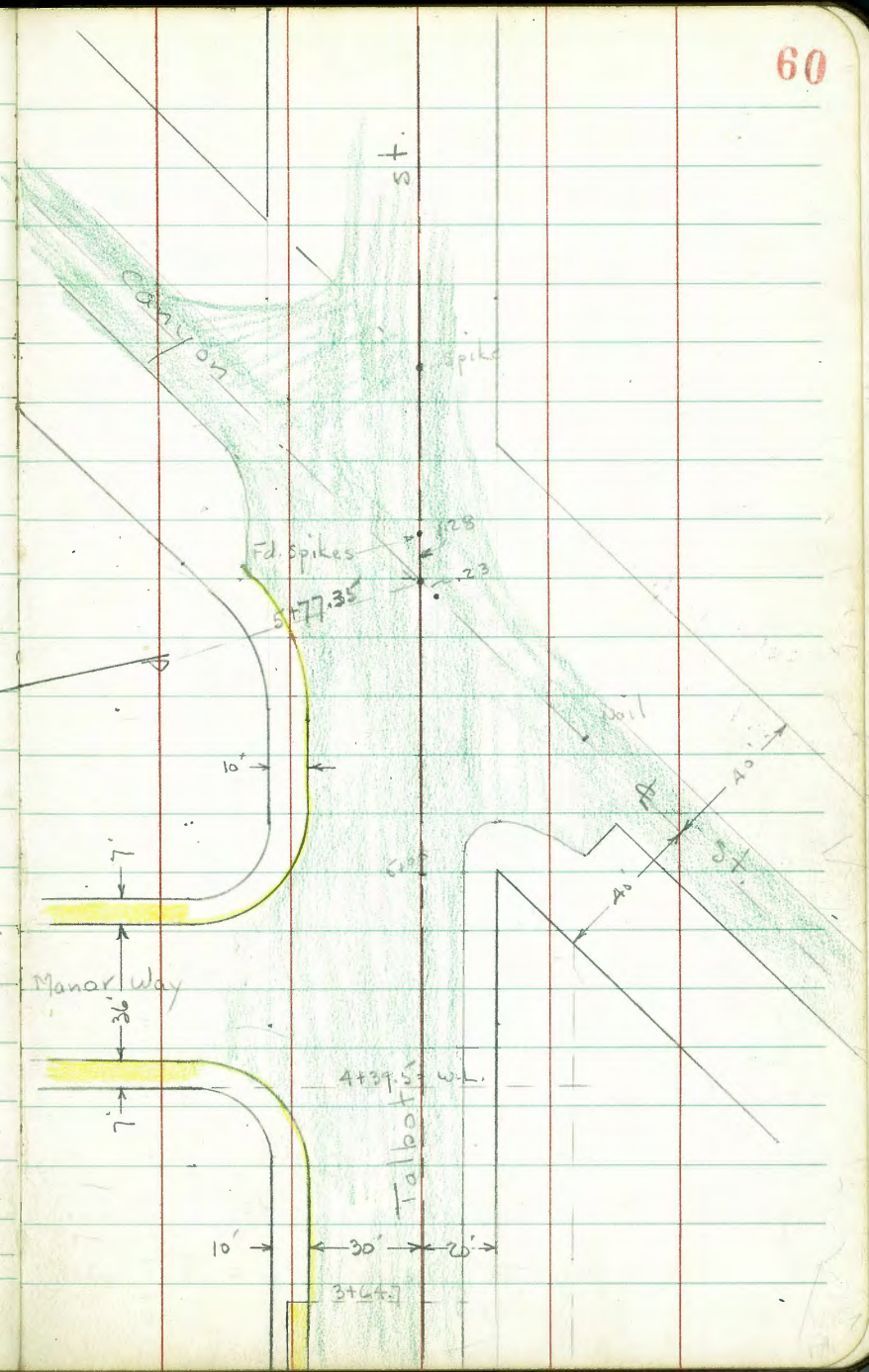
7' 36' 7'

4+39.5 w.l.

Talbot St

10' 30' 20'

3+64.2



X-Sect. Talbot St. - Catalina to

Canyon -

# 4598

10-10-50

W.O. 25020

7.0.

cont on P. 63

0+40

I.P. 0.58 261.02 1.18 260.44

0+28 = E. cb to N.

0+15 = Ely. of A.C. to S.

0+00 = † Catalina

1.18 261.62 2.33 260.44 = Nail in

B.M.

2.12 262.77

260.65 N.W. B.P.

Lt.

E = PL  
Line

Rt.

61

256.71	256.05	256.35	256.37	256.21	256.3	256.5
4.31	4.97	4.67	4.65	4.81	4.7	4.5
54.7	54.7	30		11	20	40
Top	gut.			edge	A.C.	

256.34	256.51	256.48	256.55	256.24	256.3	256.3
5.28	5.11	5.14	5.17	5.38	5.3	5.3
92	40	30	15	20	40	
gut. in Drive			edge	A.C.		

256.51	256.68	256.71	256.62	256.47	256.35	255.99
4.81	4.94	4.91	5.00	5.15	5.27	5.63
92	40	30		20	40	80

257.11	256.72	256.57	256.74	256.64	256.56	256.24
4.51	4.70	4.75	4.88	4.98	5.06	5.38
92	40	30	20	40	80	

SE. Pole Talbot

261.62

Santa Barbara  
+ Catalina



Rods around N.E. Ref. - Talbot + Catalina  
 every 10' around. - Beginning at N. end  
 on Catalina - 62' Rad.

T = 261.62

261.62

62

96.5 = E.C.

5.33 256.29

T

6.01 255.61

q

P.C. = N. end 5.24 256.38 = gut. in Dr.

10' S. 4.79 256.83 T = Top

5.36 256.26 q = gut

20' 4.83 256.79 T

5.44 256.18 q

30' 4.89 256.73 T

5.47 256.15 q

40' 4.92 256.70 T

5.58 256.08 q

50' 4.93 256.69 T

5.55 256.07 q

60' 4.97 256.65 T

5.57 256.05 q

70' 5.04 256.58 T

5.69 255.93 q

80' 5.17 256.45 T

5.78 255.84 q

90' 5.27 256.35 T

5.94 255.68 q

Talbot

2+76 = 6.8' Rt = 8" water gate 3.30 Top cap

2+64.7 = ± Point

T.P. 1.43 255.41 7.04 253.98 = Nail in Pole

2+56 = 13' Lt. = ± 15" Gas Co. Gate Cap

2+51 = 15' Rt. = ± P. pole # 3757

2+39.7 = W.L. Point

2+19 = 31.5' Lt. = ± Tel. pole # 511670-H

2+00

1+50 = on Conc. Dr. on Lt. - Doub. Grav.

1+39 = 31.5' Lt. = ± P. pole # J.P. 3786

1+38 = 19.7' Rt. = ± Guy Pole

1+00

0+71 = 17.2' Rt. = ± P. pole # P 3799

0+70

Cont. from P. 61.

Lt

#

Rt.

63

254.10 252.47 252.39 252.55 252.59 252.49 252.6 253.2 253.4  
 1.31 2.94 3.92 2.86 2.82 2.92 2.8 2.2 2.1 2.4 3.3  
 100 40 30 15 11 16 18 20 40 90  
 edge

252.87 255.41

8.15 13  
 Top gate cap 253.83 253.01 252.91 253.38 253.35 253.11 253.2 254.1 254.1 253.9  
 7.39 9.01 9.05 7.64 7.67 7.91 7.8 6.9 6.9 7.1  
 40.5 40.5 35 15 15 15 17 20 40  
 Top in put edge 8 9  
 cb. 256.13 254.39 253.76 254.07 254.05 253.8 253.9 255.1 255.3 254.4

4.7 6.43 7.26 6.95 6.97 7.13 7.1 5.9 5.7 6.6  
 40 Top 30 15 11 17 20 40 50  
 put. edge

257.95 256.44 254.55 254.99 255.13 254.91 254.8 257.6 256.9  
 3.07 4.58 6.47 6.03 5.89 6.11 6.2 3.4 4.1  
 49.5 40 30 15 11 16 20 40  
 floor Grav. Dr. put edge

259.1 256.2 256.10 255.46 255.82 256.00 255.80 255.8 259.1 259.0 258.9  
 1.8 1.9 4.8 4.90 5.56 5.20 5.02 5.22 5.2 1.9 2.0 2.1  
 40 36 32.5 Top 30 15 11 16 19 40 50  
 put. edge

254. 259.1 256.62 256.49 255.91 256.19 256.32 256.08 256.2 259.9 260.0 259.8  
 4.7 1.9 4.4 4.53 5.11 4.83 4.70 4.94 4.8 1.1 1.0 1.2  
 40 38 35 33.1 33.1 15 11 13 16 20 40  
 Top put. edge

261.02

Rods around Returns at Point St.

T = 261.02

30' Rad.

N.W. Ret. 47.2' around - 4 parts - 11.8' each			
Req. = P.C. on Talbot.	6.83	254.19	T
2+16.7 - 30' Lt.	7.58	253.44	q
11.8 - E. = 1/4	7.11	253.91	T
	7.80	253.22	q
1/2	7.36	253.66	T
	8.00	253.12	q
3/4	7.43	253.59	T
	8.02	253.00	q
11.8 = E.C.	7.38	253.64	T
	7.98	253.04	q
40' N. along cb. (Roll type)	6.65	254.37	T
	6.94	254.08	q

See sketch - P 60

T = 261.02

30' Rad.

N.E. Ret. 47.4' around - 4 - 11.8' each			
40' N. of P.C. along	7.18	253.84	T
E. cb. Point	7.49	253.53	q
P.C.	8.11	252.91	T
	8.72	252.30	q
11.8 - S = 1/4	8.46	252.57	T
	9.15	251.87	q
1/2	8.97	252.05	T
	9.67	251.35	q
3/4	9.55	251.47	T
	10.19	250.83	q
11.8 = E.C.	10.24	250.78	T
= 3+12.7 - 30' Lt.	10.96	250.06	q

Talbot.

Cont. on P. 67

4+41 - 2' Lt. = £ 15" Gas Gate Cover

4+39.5 = w.L. Manor Way

4+33 - 17.7' Rt. = £ P. pole # 3725

4+16.5 = P.C. 30' Rad. on Lt.

T.P. 2.28 245.11 12.58 242.83

3+70

3+64.7 = end of walk (5.7) on Lt

3+64 - 31.4 Lt = £ P. pole # J.P. 3736

3+60 - 18.6 Rt. = £ Guy Pole

3+44 - 30' Lt = £ 4" Drain in cb.

3+30

3+13.5 - 30' Lt = £ 4" Drain in cb.

2+89.7 = F.L. Point

Lt.

£

Rt

65

241.46

3.65  
12  
on cap.

241.79

241.12

241.51

241.67

241.51

241.31

241.4

242.3

244.0

3.32

3.99

3.60

3.44

3.60

3.80

3.7

2.9

1.1

Top

40.5

30

15

11

11

20

38

40

243.78

243.11

243.38

243.27

243.20

243.4

244.0

245.8

245.7

1.83

2.00

1.63

1.72

1.91

1.7

1.1

40.7

40.6

Top

30

15

11

11

20

38

40

50

Rt. Ret.

got

edge

edge

247.27

246.53

246.97

247.00

247.75

247.0

248.0

8.14

8.88

8.44

8.41

8.66

8.4

7.4

Top

30

15

11

11

20

40

248.24

7.17  
30  
I.E.  
Drain

249.82

249.06

249.45

249.46

249.33

249.7

250.5

5.59

6.35

5.96

5.95

6.08

5.7

4.9

Top

30

15

11

11

20

40

5.25  
30  
I.E.  
Drain

252.16

251.44

251.38

251.51

251.56

251.45

252.0

252.0

3.25

3.97

4.03

3.90

3.85

3.96

3.4

3.4

Top

40.2

40.2

30

15

11

11

20

40

cross

got.

255.41

edge

edge

Rods around 30' Rad Returns - Manor Way

N.W. Ret. - 47.2' around - 4 - parts - 11.8' each

PC. on Talbot. = 4 + 16.5	1.33	243.78	T
	2.00	243.11	9
11.8 = 1/4	2.26	242.85	≠
	2.95	242.16	9
1/2	3.17	241.94	T
	3.84	241.27	9
3/4	3.93	241.18	T
	4.58	240.53	9
11.8 = E.C.	4.56	240.55	T
	5.16	239.95	9
40' N. along cb. (roll Type) Begins.	5.64	239.47	≠
	5.97	239.14	9

N.E. Ret. - 47.2' - 4 - 11.8' each.

E. cb. - Manor 40' N. of P.C. along cb. (roll type 10' N. of P.C.)	6.73	238.38	T
	7.04	238.07	9
P.C. - on Manor	6.50	238.61	T
	7.04	238.07	9
11.8 = 1/4	6.89	238.22	T
	7.41	237.70	9
1/2	7.32	237.79	T
	8.01	237.10	9
3/4	7.97	237.14	T
	8.57	236.54	9
11.8 = E.C. Talbot - 5 + 12.5	8.83	236.28	T
	9.54	235.57	9

Talbot

5+78-47.6 Lt. = end cb.

5+77.35 =  $\Phi$  Canyon +  $\Phi$  Talbot

5+55

Canyon + Talbot  
Set. BM = Nail in N.W. Pole 5.34 233.98

T.P. 5.48 339.32 11.27 333.84  
239.32 233.54

5+42- 21.7 Lt. =  $\Phi$  Tel. pole # 5 11.62 - H

5+39 = P.C. of cb. on Lt.

5+25 = Brk. in cb.

4+89.5 = E.L. Manor Way

4+76- 6.4 Rt. = 8" Water Gate Cap

4+64.5 =  $\Phi$  Manor Way

Cont. from P. 65

Lt.

$\Phi$  = PL  
Line

Rt.

67

934-Top 19.00 = gut.  
47.6 47.6  
230.06 229.39 230.55 231.05 232.90 234.32 234.79 235.1

9.26 9.93 8.77 8.27 6.42 5.00 4.53 4.2  
4.66 30 21 on spike 20 29 40  
Top gut. edge

232.16 231.63 232.55 233.18 234.62 235.69 235.87

7.16 7.69 6.77 6.14 4.70 3.63 3.45  
32.5 32.5 15 20 40 44  
Top gut. edge  
P.C.

239.32  
~~339.30~~

233.84 233.15

11.27 11.96  
30 30  
Top pit

235.22 239.22 239.81 235.04 235.34 235.62 236.51 237.50 238.26

9.89 10.79 10.30 10.07 9.77 9.49 8.54 7.61 6.85  
30 30 15 14 20 40 55.3 70.6  
Top gut.  $\pm$  edge

237.90 237.33 237.60 237.68 237.75 237.63 237.7 238.5 240.1 239.56  
7.21 7.78 7.57 7.43 7.36 7.48 7.4 6.6 5.0 6.4 5.55  
40.9 30 15 11 edge 20 38 40 50 75.7  
Top gut. edge edge edge

238.84 239.34 239.47 239.60 239.71 239.61 239.42 239.4 240.0 242.3 242.9  
6.27 5.77 5.64 5.51 5.40 5.50 5.69 5.7 5.1 2.8 2.2  
100 60 40 30 15 11 edge 20 51 40 50  
Cross gut. on Canyon

245.11

Lt.

~~Et~~

Rt.

68

6+00- end.

228.71	229.38	230.82	232.01	232.96	233.83	233.9	233.52
10.61	9.94	8.50	7.31	6.36	5.49	5.4	5.8
50	40	25	12		17.5	20	40
edge					edge		

239.32  
~~339.30~~

Reference - T.P. sheet 2558

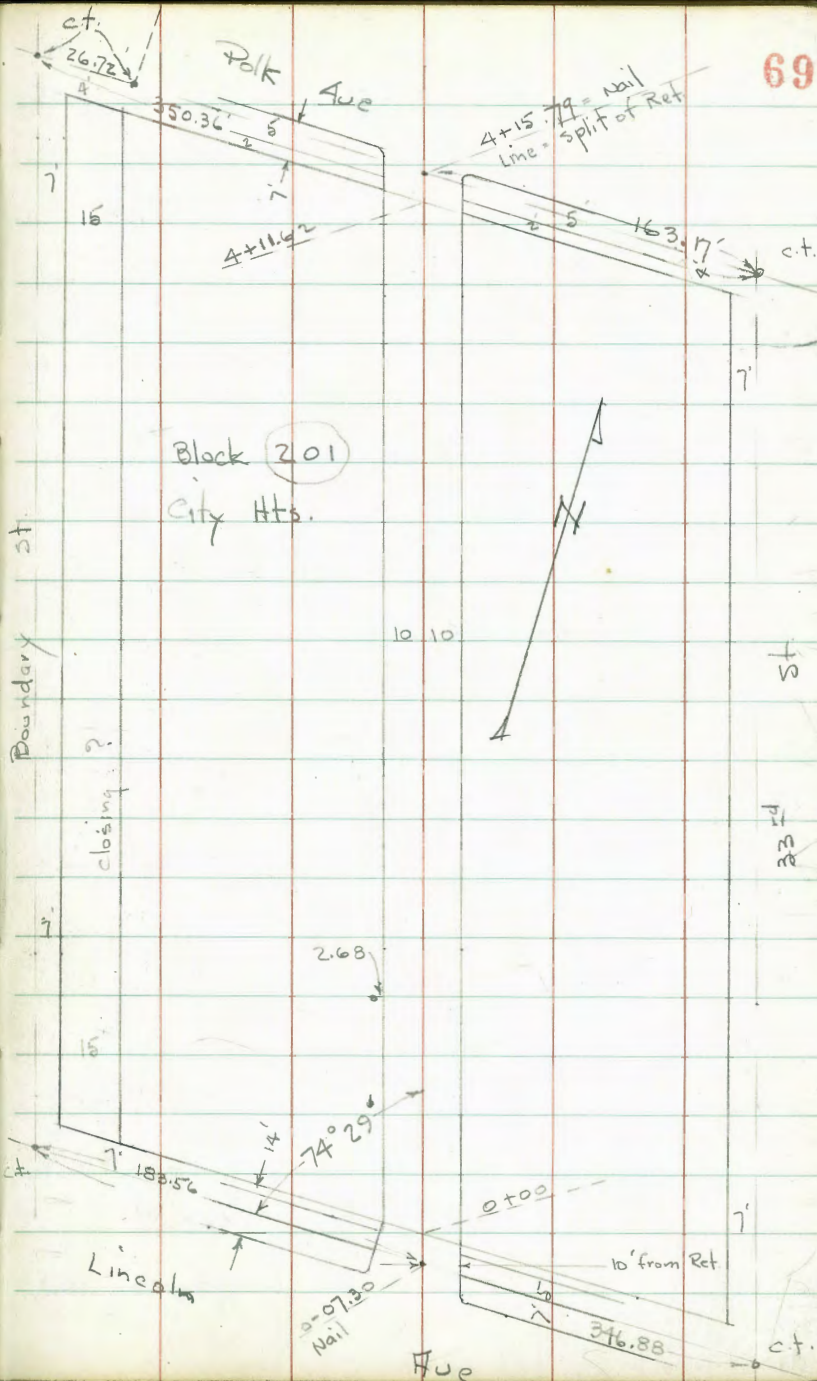
T.P. Book 23 - P. 1 + 2

Books 1265 - P. 30 + 1293 - P. 75

Map. 1007 - City Hts.

Returns are set to give East Tier of  
Lots 140' at 90° - leaving all excess in tier  
to West. - More Research Needed.

PLOTTED BY  
R.W. DE MASS  
6-13-51





7-Sect. 20 Alley in Block 201 - City Hts.

# 5317

W.O. 25020

6-8-51

7.0.

Lt.

Rt.

70

INDEXED

JUN 11 1951

1+50

42.2

41.6  
10

41.5

42.6  
10

42.8  
15

1+10 - 15.3 ft. = Apron to Sing. Gar. Conc. floor.

41.15

15.3 = Conc. apron

41.63

18.4 = floor

1+00

39.6  
20

39.2  
10

39.1

40.1  
10

41.0  
15

0+50

37.7  
15

37.6  
10

37.5

38.2  
10

38.4  
15

0+35 - 12' Rt. = N. cor. House

37.4

12  
ground

37.55

floor

0+31 - 0.3' Rt. = Sewer MH

37.31

= Rim

0+00 - N.L. Lincoln - edge A.C. - Sect. along N.L.

37.24

10.3  
Top  
of curb.

36.93

10.3  
gut.

36.76

37.16

10.4  
gut.

37.53

10.4  
Top.

0 - 14.4 - N. cb. Lincoln

37.67

Top

37.00

6.0  
gut.

37.32

cb.

36.35

14.1  
on grate  
of Inlet.

36.49

36.78

10.3  
gut.

37.40

Top  
of Rad.  
Ret.

36.97

6.0  
gut.

37.64

Top

Used Elev. Rod. - Actual Elev. Shown. - 300' Not.

86.0

337.32 = 11 in ±

Inlet - alley Ret.

7.40

345.92

0.82

338.52

B.M.

5.90

339.34

333.44 = N.W. C.P. Boundary + Univ.

Set B.M. = 7' ct. N.E. Bancroft + Polk

344.64

4+19.2 = S. cb. line of Polk

See sketch for prop sta.

4+12.2 = edge A.C. pave + curbs - Sect. along S.L.

3+85

3+50 - wooden shed on Rt.

3+00

2+92 - 8.1 Lt. = 10' Conc slab

2+84 - 6.8' Lt. = 10' Conc apron to Sing Gar.

2+50 = Lt. + old Gar. - Not Used. = Dirt floor

2+12 = 7.2' Rt. = 10' Conc apron to Sing Gar.

2+00

1+70 = 11.5 Rt. = 10' Sing Gar - Dirt floor

Set B.M. = Nail in Pole # PA449 Lt. = 1+70

343.51

Lt.

±

Rt.

71

47.31	46.68	48.19	47.60	47.88	48.30	48.88	49.51	50.01
Top	4.0 gut	Top 2' Rad.	8.6 gut		12.2 gut	Top 2' Rad.	5.0 gut	Top

48.24	48.12	48.19	48.68	48.93
Top cb.	10.5 gut		10.5 gut	Top cb.

48.5	49.1	49.4	50.1	50.4
15	10		10	15

47.2	48.2	48.6	49.0	49.0
15	10		10	10.8 = shed floor

46.7	46.7	46.7	47.8	48.3
15	10		10	15

46.68	46.65
11.1 of fence	8.1 = Conc.

46.20	46.40
13 floor	6.8 apron

44.9	45.3	45.6	46.2	46.4
11.4 floor	10		10	15

44.53	45.11
7.2	10.6 = floor

43.2	43.2	43.4	44.3	44.0
15	10		10	15

42.9
11.5 = floor

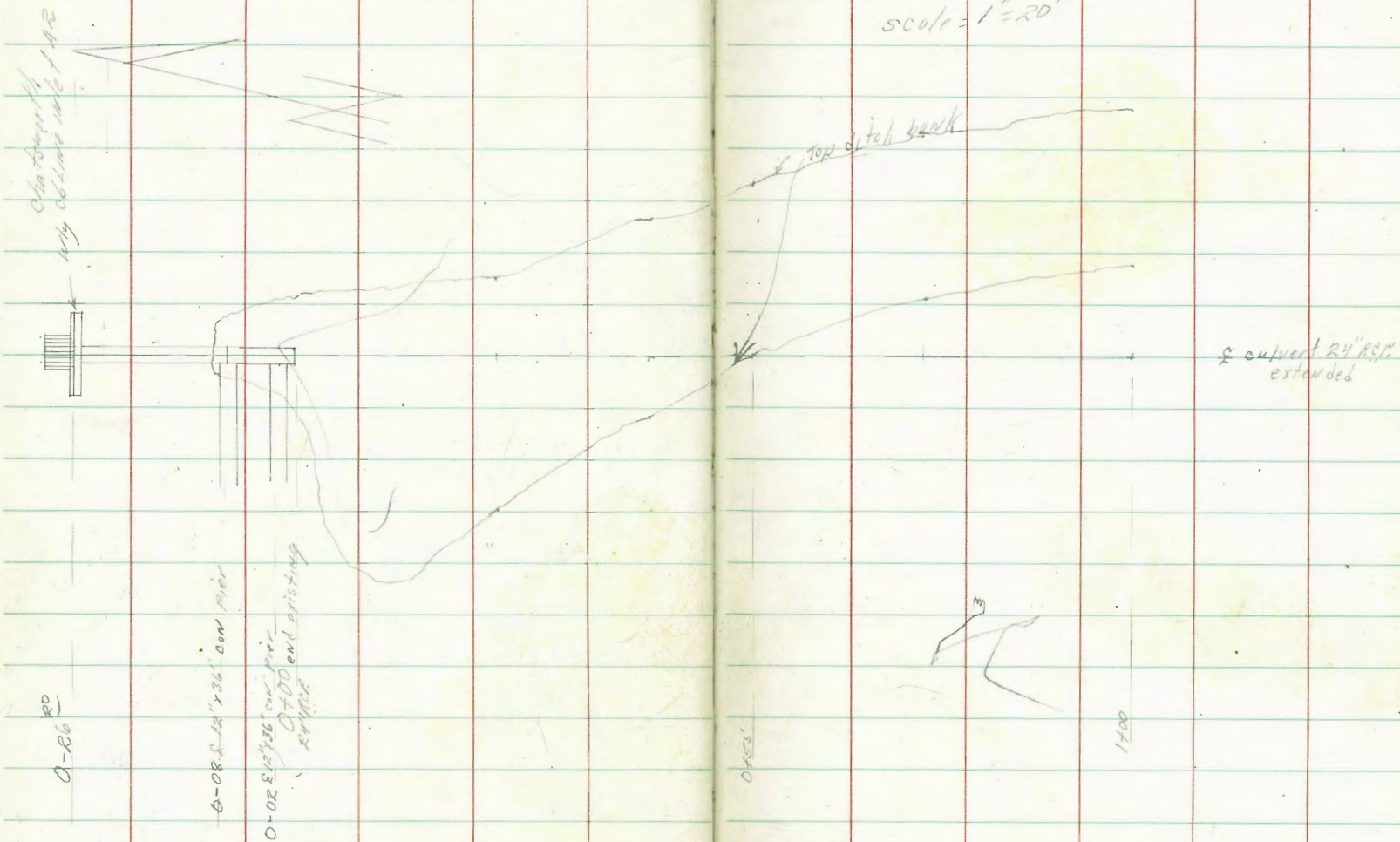
D. Smith  
J. Rorer  
R. Taylor

Survey to Extend & bring culvert to bottom of wash  
on Chatsworth approx 300' Nly of Catalina.

Wot # 21/63  
8-19-53

72

scale = 1" = 20'



LT-Nly

2

NT-Sly

73

0742

1773	1750	1472	1490	1743	1763
18	41	152	161	48	21
23	16	10	7	20	

0723

1762	1762	1622	1690	1752	1770
24	32	154	151	34	21
25	9	7	18	30	

0700

1782	1781	1666	1689	1664	151	1758
02	10	125	219	142	122	40
25	7	6	10	6	8	33
			91			20

0-10

0<sup>o</sup>

TP<sub>2</sub>

055

17913

13<sup>20</sup>

478<sup>58</sup>

17913<sup>1</sup>

---

30

1828

0-21

0-26<sup>20</sup> Fly cc Live Chatsworth Blvd.

1824	1826	1838	1892
254	342	793	1279
Top cc	grate	10 inlet w/ly	12 outlet Fly

TP<sub>1</sub>

119

19178<sup>1</sup>

12<sup>98</sup>

19059<sup>1</sup>

B.M.

196

20357<sup>1</sup>

20161

NEBR  
Chatsworth  
Catalina

19178<sup>1</sup>

Lt Nly

2

At = Sly

74

BM starting

061 201<sup>4</sup>

TP4 12<sup>20</sup> 202<sup>25</sup> 004 190<sup>05</sup>

TP3 12<sup>23</sup> 190<sup>09</sup> 127 177<sup>86</sup>

1700

0475

0455

INDEXED  
JEN  
AUG 20 1953

175L	172Z	1404	1604	174L	1760	1790
32	62	187	182	64	3L	0L
40	29	22	16	11		10

1750	123	1613	1413	174L	1750	1745
33	68	174	174	60	4L	06
35	26	21	12	7		10

174L	1723	1625	1625	1228	1745	1745
30	58	166	166	58	26	06
40	20	13	8	13	13	25

17913<sup>4</sup>







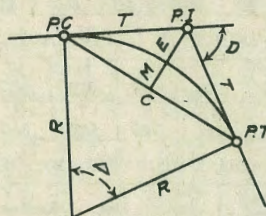






# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

- Radius= $R = \frac{50}{\sin. \frac{D}{2}}$  (1) Degree of Curve= $D$  and  $\sin. \frac{D}{2} = \frac{50}{R}$  (2)  
 Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)  
 Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)  
 External= $E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos. \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)  
 Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta=62^{\circ} 10'$   $D=8^{\circ} 20'$ . From Table IV for  $1^{\circ}$  curve  $T=3454.1$  and  $\div 8\frac{1}{2}=414.49$  ft. From Table V correction=.36 or  $T=414.85$  ft. P. C.=Sta. P.I.— $T=157+45.50$ . Also from (4)  $L=746.00$  and P. T.=Sta. P. C. +  $L=164+91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance= $158 - \text{Sta. P. C.}=54.50$ , hence offset= $7.27 (54.50 \div 100)^2=2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26)=2.16$  ft.

**Deflections.**—Deflection angle= $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft.=(in minutes)  $.3 \times C \times D^{\circ}$  or=defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve= $.3 \times 54.5 \times 8\frac{1}{2}=136.2'$  or  $2^{\circ} 16.2'$ , or= $2.50 \times 54.5=136.2'$  from Table III. For Sta. 159 deflection angle= $2^{\circ} 16.2' + 8^{\circ} 20' \div 2=6^{\circ} 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^{\circ}$  curve  $E=960.6$  for  $8^{\circ} 20'=960.6 \div 8\frac{1}{2}=115.27$  and from Table V correction=.10 or  $E=115.37$  ft. Or suppose  $\Delta=32^{\circ}$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E=230.9$  and  $\div 42=5.5$  or  $D=5^{\circ} 30'$ .

Eberri + Niag SEBP 52.23  
 - 17 Newpi SWBP 43.06  
 Niagara + Sunfat NWBP 26.04

9.03  
 9.52  
 10.22

535  
 597  
 648

11.85  
 10.72  
 9.92

6.48  
 6.80  
 7.10

7.09  
 7.12

36  
 60  
 96

216.7  
 96  
 312.7

9.25  
 9.62

171  
 11.62  
 13.33

4.30  
 4.26  
 4.44

648  
 710  
 1358  
 679

544  
 606  
 690  
 544  
 1234  
 619

53.98  
 465  
 58.83  
 61.02  
 2.19

DISTANCES FROM CENTER OF ROADWAY FOR  
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2  
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) \* 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.