

1869



ENGINEERS'
LEVEL BOOK
No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

MICROFILMED

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

DEC 30 1964

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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W.D. 21 328

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except page # 31

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Seabreeze

Dr.

INDEXED

Lot 7

Lot 12

Lot 6

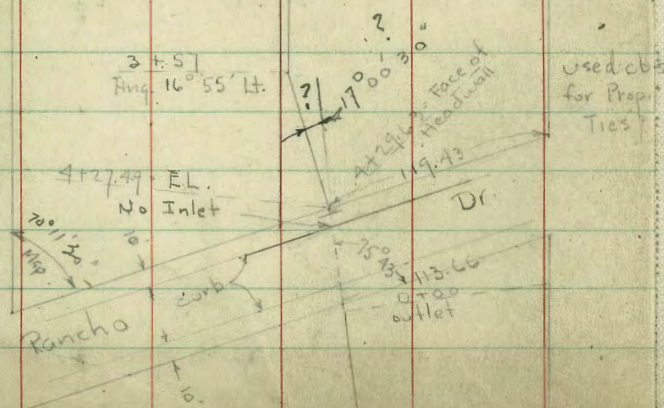
Lot 13

Block 23

Paradise Hills

Lauder

Cumberland



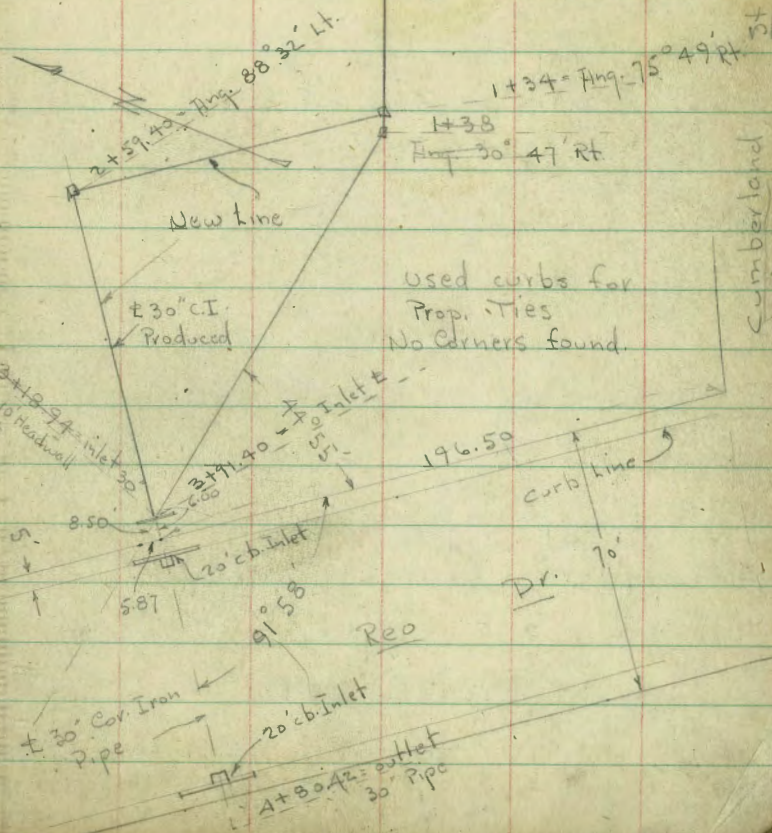
Drain Survey
#2468
W.O 90074

7-21-48
70.

Rancho

Block 20

Prop Drain



Levels along \pm of Prop. Culvert
in Block 23 - Paradise Hills

1+24 - 34' Rt. = \pm P. pole # 88474

1+10

0+75

0+62 - 13' Rt. = beg wire fence

0+35 = \pm Wash

0+25.52 - Ang $32^{\circ} 50'$ Rt. - Sect. on Split

0+00 = outlet of Exist. 24" RC Pipe

7.79 224.85 3.84 217.06

10.49 220.90 210.41

S.W. of
Rancho +
Cumber land.
1692 - P. 26

Lt. - \pm Rt. 2

6.1 ^{218.8}
25
10.1 ^{214.8}
13
 \pm Wash
7.2 ^{217.0}
5.8 ^{219.0}
20

4.9 ^{220.0}
25
8.6 ^{216.2}
8
 \pm Wash
5.8 ^{219.0}
4.4 ^{220.4}
20

3.0 ^{221.8}
20
4.5 ^{220.4}
7
7.1 ^{217.8}
 \pm
6.1 ^{218.8}
3.3 ^{221.6}
20

1.4 ^{223.4}
20
3.3 ^{221.6}
2
4.97 ^{219.88}
on Stub.
6.9 ^{218.0}
 \pm Wash
3.6 ^{221.2}
20

2.8 ^{222.0}
10
6.04 ^{218.81}
1.7 ^{223.2}
10

224.85 ✓

3+57: Ang. 16° 55' Lt. - Sect. on Spit

3+30

3+03 - 9.6 Lt. = Beg. wire fence

3+00

2+50

T.P. 0.20 212.18 11.87 212.98

2+44 - 4' Rt = ± p. pale 88475

2+00

1+81.5 - 13.1 Rt = end fence

1+75

1+50

3

Lt.

±

Rt.

3.5^{209.7}
20

4.6^{208.6}
3

3.80^{209.38}
on stub.

2.9^{210.3}
20

2.8^{210.4}
20

3.9^{209.3}
1

2.7^{210.4}
20

3.2^{210.0}
20

3.6^{209.6}
1

2.4^{210.8}
20

2.5^{210.7}
20

2.2^{211.0}
1

1.4^{211.8}
20

213.18 ✓

9.2^{215.6}
20

10.9^{214.0}
1

10.8^{214.0}
9

11.8^{215.0}
14

11.4^{213.4}
25

7.5^{217.4}
20

7.0^{217.8}
10

7.0^{217.8}
6

10.9^{214.0}
10

10.6^{214.4}
20

5.3^{219.0}
25

9.4^{215.4}
8

9.9^{215.0}
1 Wash

8.9^{216.0}
20

0+44 - 7.4 Rt = Beg wire fence

0+37 - 34.2 Rt = \pm House

0+30

Head wall

0+00 = outlet of 24" Cor. Iron pipe - no

Block 20 - Paradise Hills

Beg. Levels along \pm of Prop Culvert in

T.P. 3.75 205.03 11.90 201.29

Top Conc Headwall 7.08 206.10

4+29.63 = \pm inlet of 24" Cor. Iron pipe - in \pm
of 8' Conc. Headwall

3+90

3+77 - 10' Rt = \pm Dead man

3+64 - 5.8' Lt = end fence

3+61 - 4.6 Rt = \pm P. pole # 88476

Lt

#

Rt

4

206.23

+ 1.20

34.2

floor

202.7	202.4	201.1	198.6	200.8	204.1
2.3	2.6	3.9	6.4	4.2	0.9
20	6	1	\pm Ditch	4	20

204.1	204.3	199.79	204.7	204.1
0.9	0.7	5.24	0.3	0.9
10	5	FL Pipe	6	10

205.03 ✓

6.6	7.1	10.66	7.6	7.6
20	7	FL 24" pipe	4	20

6.2	5.7	5.4
20	20	20

213.18 ✓

+ Cumberland.
 check B.M. S.W. B.P. - Reo 4.58 194.86 194.88
 1692-P.27

10' Headwall - outs normal to Reo

3+18.94 = ± inlet of 30" Cor. Iron Pipe in ± ot.

T.P. 4.12 199.44 9.71 195.32

2+90

2+50

LT ± RT. C

145.3	141.65	137.48	141.57	145.0
4.1	7.79	11.96	7.77	4.4
20	5	F.I. Pipe	5	20
along Reo	Top-end Headwall		Top-end Headwall	along Reo
		199.44 ✓		
	8.8 146.2	9.4 145.6	14.8 140.2	10.8 144.2
	30		25	45
			± Ditch	
	8.0 147.0	7.7 147.3	8.2 146.8	11.8 143.2
	30		30	61
				± Ditch
		205.03		

INDEXED

W.K.

SEP 23 1948

Water line

PC: 4+98.70
EC: 4+94.18

$\Delta = 93^\circ 41'$
 $R = 45'$
 $L = 73.58'$

47.99

EC: 5+72.28

70'

15'

Conc. Pavc

Dr.
Conc. Pavc

Conc. Pavc

Wood Valve
Box

5'

4.4'

Reo

5'

9+04.87 PC
9+14.96 EC
 $\Delta = 25^\circ 42'$
 $R = 22.5'$
 $L = 10.09'$

RI

9+10

9+18.09

88°22'

9+49.55
inside of
20' opening
ob. Inlet

20' Cor. Iron
Pipe

Survey - Prop. Drain - Paradise Hills

W.O. 90074

7-22-48

47.99

134.25

4.07

186.86

234.95

7.0

10' opening Inlet

4+12.3 = E 18'

Pipe

Albemarle St
Conc. Pavc

2+27.27 = PC

Curbs do not seem
to fit Map data. on curve

$\Delta = 16^\circ 11'$
 $R = 945'$
 $L = 266.9'$

T = 134.35

4+58.03 =
off Prop. Cor.

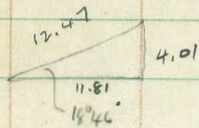
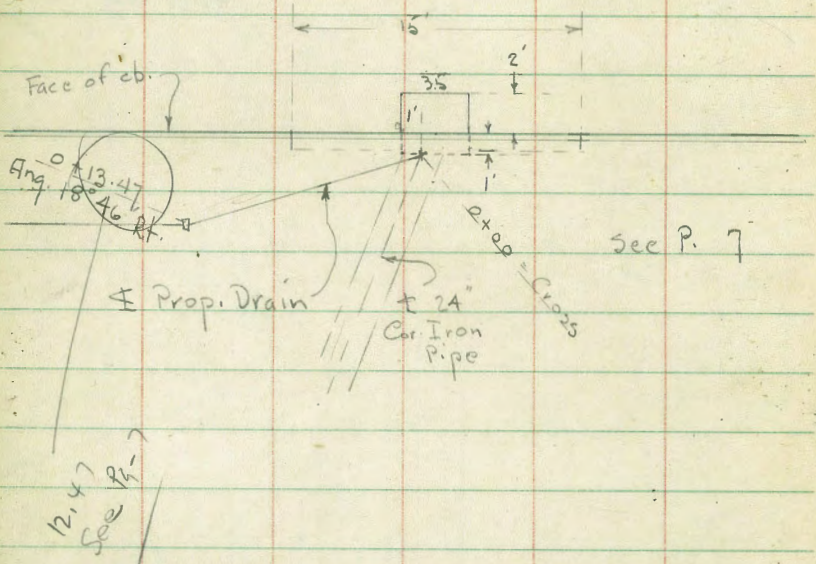
Prop
St. Drain

Rancho Dr.

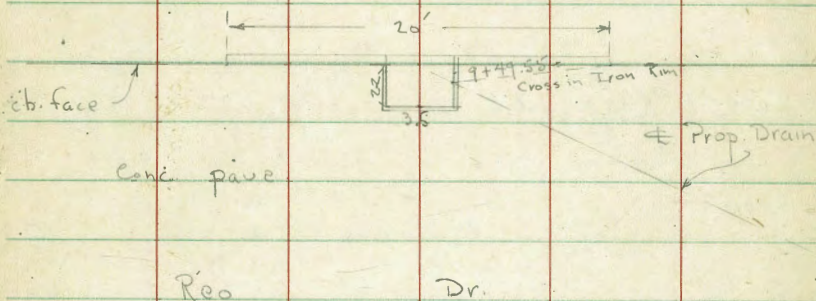
Note found for Detail
+ error in
Dist to Angl. Pt.

See P. 8

Detail of 15' opening Inlet on Albermarle
E. of Rancho. 25 x 3' Box



8
Detail of 20' cb. Inlet on Reo Dr.
= end of Prop. Drain - P: 7



2+35.5 = 1.9 Rt. = ± 3" Palm

2+33.5 = 5.5 Lt. = Cor 6" Conc wall

2+27.27 = P.C. Curve along cb.

2+12.5 = face cb on Ret

2+00

1+77 = face of cb on Ret. = end Lawn

1+68.03 = ^{opp} P.C. 10 Rad. + Prop. Cor - (S.E.)

1+30

Station	Notes	Station	Notes	Station	Notes
25.38	5.23 5.5 Top wall	25.1	5.5 5.5 ground		
214.6	6.0 20	215.26	5.35 on Stub	215.48	5.13 5 Top
		215.87	4.74 Top	215.23	5.38 9.4
				215.53	5.08 5 on Conc
215.43	5.18 6 Bk.	215.72	4.89 on Conc. Pav	216.11	4.49 10
215.28	5.33 10 out	215.82	4.79 10 Top cb	216.61	4.00 Top
				215.94	4.67 9.4
				216.12	4.49 5 = on Conc Pav
		214.9	5.7 20	216.7	3.9
				216.81	3.80 5 Top
				216.17	4.44 5 9.4
		215.1	5.5 19.8 along House	216.9	3.7
				216.86	3.75 5 = Top ch.
			220.61		

4+123 = \pm + \pm 18" Cor Iron pipe from
 10' opening cb Inlet on Rt - 3.5x3 Box
 T.P. 5.13 214.59 11.15 209.46

4+00

3+87 - 1.3' Rt = \pm 3" Palm

3+62 - 2.6 Rt. = \pm P. pole - # 87554

Block wall

3+50 - 5.6 Lt = Wly 8" Conc footing for prop

3+46 - 2.4 Rt = \pm Dead man

3+40 - 1.2' Rt = \pm 3" Palm

3+05 - 1.5 Rt = \pm 3" Palm + end of Lawn

3+00

2+92 - 20.8 Lt. = Cor. House (see Gar below)

2+70 - 1.8' Rt. = \pm 3" Palm

2+47 - Wly Conc Dr. = Beg. Lawn

Ely.

2+39 = edge Conc. Dr. + 5.8 Lt. = end wall

Dr. at

212.83	215.34	214.58	215.08	215.04	214.99	214.42
7.78	5.27	6.03	5.53	5.57	5.62	6.19
23.8	5.8	5.8	2.3	220.41 ✓	2.4	5
Gar.	Top	Dr	Brk.		Brk.	Dr. in gut.
end wall						

Lt. 9.78 204.81
 7.1
 = F.L. outlet
 18" pipe

214.59 ✓

208.4
 204.91 Rt 208.35 11 207.31
 6.2 9.68 6.24 7.28
 3 4 4
 = F.L. 18" pipe at Box Top Top
 cb Grate - Gut.

208.5
 12.1 12.25 13.09 207.52
 4.1 4.1
 Top Gut.

209.16 209.80 210.1 210.08 209.45

11.0 10.81 10.5 10.53 11.16
 15 5.6 4.3 4.3
 edge Conc. Top Gut
 cb

211.1 211.4 211.26 211.66

8.5 8.2 8.35 8.95
 20 4.6 4.6
 Top cb Gut

212.26 212.5

7.25 8.1
 20.8 20.8
 floor ground

214.70
 5.91

5+47.76

5+23.23 = on H.C. pave

Sects. on Radial Line
Curve in 2 parts

5+20.5 = end Conc. Pave

5+02.5 = face cb. on Ret. = end lawn

4+98.70 = P.C. 45' Rad. Curve

4+94.18 = E.C. = opp. P.C. 10' Rad. Ret.

4+68 - 17.5 Lt = ^{beg. lawn} Near Cor. Real Estate office

4+50

4+22 - 0.9 Rt = 3" Palm

Lt

±

Rt

12

^{208.5}
6.1
10

^{208.6}
6.0

^{208.51}
6.08
10.8
edge Conc. pave

^{208.97}
5.62
10
on Conc.

^{209.54}
5.07

^{210.01}
4.58
10 = on H.C.

^{208.89}
5.70
10
along edge

^{209.50}
5.09

^{209.87}
4.72
10
along edge

^{209.09}
5.50
10
gut.

^{209.59}
5.00
10
along cb.

^{210.0}
4.60
Top
gut

^{209.76}
4.83
10 = conc.

^{210.04}
4.55
on Stub.

^{209.8}
4.8
15

^{210.04}
4.55
on Stub.

^{209.93}
4.66
3.7
Top cb
P.C.

^{209.29}
5.30
3.7
gut

^{209.57}
5.02
10
on
Pave

^{210.51}
4.09
17.5
floor

^{208.3}
5.3
17.5
ground

^{208.6}
6.0

^{208.69}
5.90
3.8
Top cb
gut

^{208.09}
6.50
3.8
gut

214.59 ✓

T.P. 4.62 199.60 12.89 194.94

8+00

7+86.4 - 4.4 Lt. = \pm + wly. of 10.3 x 10'
wood Valve chamber for pipe line.
Lid is locked - cant get Bottom

7+50

7+00

6+50

6+00

T.P. 1.02 207.87 7.74 206.85

5+72.24 = E.C.

E.C. Stub

Lt.

\pm

Rt.

13

12.0
10
195.9

12.5
195.4

12.47
3
10
195.40
edge

12.49
10
195.38

14.7
= approx. Bottom

11.71 = Top of box
4.4

11.0
10
196.9

11.2
196.7

11.35
3
10
196.52
edge

11.44
10
196.43

9.0
10
198.9

9.1
198.8

9.09
3
10
198.78
edge

9.26
10
198.61

6.1
10
201.77

6.3
201.57

6.06
3
10
201.81
edge

6.20
10
201.67

2.5
10
205.4

2.9
205.0

2.87
3
10
205.00
edge

3.11
10
204.76

207.87 ✓

7.3
10
207.3

7.74
on Stub
206.85

7.95
3
10
206.77
edge Conc.
Pave

7.94
10
206.65
Conc.

214.59

Profile of ϕ 24" C.I. Pipe across
 Rancho Dr. - Sketch - P. 1 - + Notes - P. 4

0+51.95 = out let of 24" C.I. Pipe = 0+00 - P. 4

0+49

0+39.2 = W. cb. = ϕ of 15' opening - See Detail above

0+24 = ϕ st

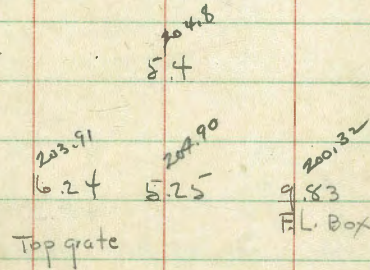
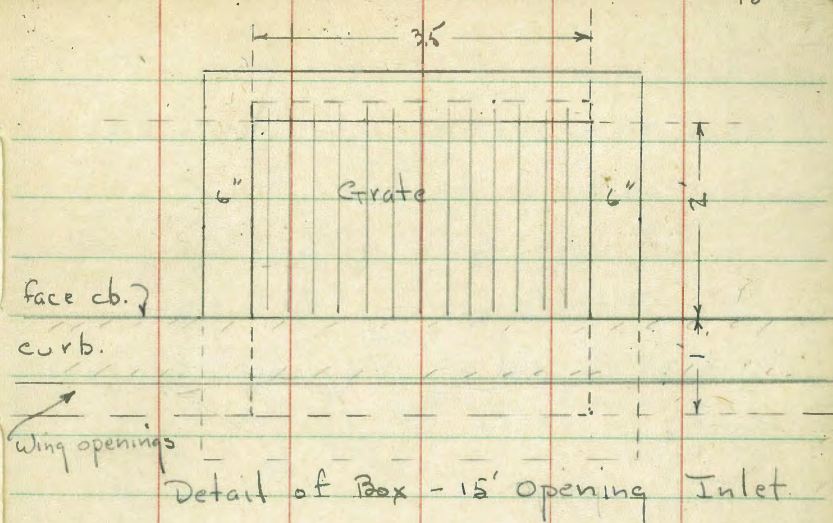
Rancho Dr.

0+08.2 = F. cb. - No Inlet.

0+00 = inlet of 24" C.I. Pipe = 4+29.43 - P. 4

8.87 210.15

st-b. 1+38
 201.28 = P. 4



204.76
 5.40

204.47 4.68
 204.86 5.29
 Top cb. 9.1

210.15

Relocation of Prop. Drain. Thru
Block 20 - Sketch - P. 1 - Levels from
outlet on Rancho to 1+34 = P. 4

2+35 - Pitch tapers off to Ang pt.

2+01 - 3.8 Rt = end of wire fence + Beg. Picket

2+00

1+70

1+42

1+38.8 - 3.6 Rt. = Cor. of wire fence

1+38 = Top of Vert. Bank to Drain ditch

Begin at 1+34 = Ang. $75^{\circ} 49'$ Rt.

2.68

203.96 ✓

201.28

16

1979 6.1 20	1983 5.7 2	1987 8.3 0.5 Bottom	1987 8.3 0.8	1987 8.3 0.8	1989 7.1 3	1985 6.5 20
1987 5.3 20	1981 4.9 1 Top	1983 7.7 1.6	1983 7.7 Bottom	1983 7.7 1.5	1984 6.6 2 Top	1985 6.5 20
1974 4.6 20	2000 4.3 1 Top	1965 7.5 0.9 Bottom	1965 7.5 Bottom	1976 6.4 1.2 Top	1976 6.4 1.5	
2003 3.7 20	2011 2.9 1 Top	1966 7.4 0.9 Bottom of Ditch	1966 7.4 Bottom of Ditch	1966 7.4 0.9 Bottom of Ditch	1963 5.7 1 Top	1986 5.4 20
		1999 4.1 Top		1965 7.5 Bottom		
		2007 3.25 on Stub.				
		203.96 ✓				

2+91.40 = Φ Inlet of 30" C.I. Pipe - Sec P. 1+6

3+85

3+60

3+30

3+00

2+75

2+61 - 1.5' Rt. = Φ P. pole # 477670-H

32 Rt. = fence 2.6' S. of end.

2+59.40 = Ang. $88^{\circ} 32'$ Lt. - Sect. on split

Lt.

Φ

Rt.

7

157.48
16.48
= FL. Inlet 30" Pipe

190.8	191.1	191.0	190.7	190.0	190.9	190.1
8.2	11.3	15.0	15.3	15.0	10.1	8.3
20	8	4	1	10	10	20
			Φ Drain			

190.1	190.2	190.0	190.1	190.1	190.9	190.7
7.9	13.8	14.0	13.9	13.9	9.1	8.3
25	5	3	3	3	15	20
		Φ Drain				

190.7	190.8	191.7	191.4	190.8	190.2
7.3	11.2	12.3	11.6	8.2	7.8
25	9	4	20	20	20
		Φ Drain			

191.8	190.9	193.4	193.9	190.5	190.7
6.2	7.1	10.6	10.1	7.5	7.1
30	20	4	20	20	20
		Φ Drain			

190.3	191.2	191.9	191.1	190.8	190.0	190.4	190.6
5.7	6.8	8.1	9.9	10.2	10.0	8.6	7.4
30	15	6	5	6	6	7	20

191.5	191.7	191.0	191.8	191.4
6.5	7.3	10.0	7.98	6.6
20	13	10	on stub.	20
		Φ Ditch		

203.96

4+80.42 = outlet of 20" Pipe

4+70

Curb Inlet - Box - Same

4+62.4 = w. cb. of Reo Dr. = $\frac{1}{2}$ of 20' opening

4+47.1 = edge Conc. pave

4+32

4+16.8 = edge Conc. pave

Box - Same as Detail - P. 15

4+02.2 = E. cb. at $\frac{1}{2}$ of 20' opening Inlet

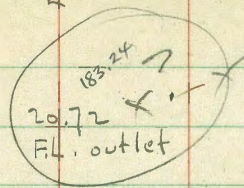
3+97

Lt.

#

Rt

18



194.0
10.0

144.48
142.51
147.61
9.48
10.45
19.35
Top
cb.
Top
grate
FL. of
Box

144.32
9.64

144.96
9.0

144.57
9.45

190.50
194.20
187.14
8.46
9.46
16.82
Top
cb.
Top
grate
FL.
Box

8.9
85.1

203.96 ✓

Levels along ± of Prop. Drain
 from Albemarle to Inlet on Sea Breeze
 Sketch P. 19

1+00

0+52.75 - stub - Ang. $60^{\circ}56'30''$ Rt.

0+47 = N. cb. Albemarle on Box to 15' opening
 curb Inlet

0+24 = ± st.

0+01.2 = cb. face - for elev. of Box See P. 9

0+00 = Cross on Top of Cover - also 0+00 to W.
 See P. 8+9

0-18.6 = outlet of 24" C.I. Pipe

11.17

226.63

215.46

sw. B.P.
 Ranch +
 Albemarle

Lt.

±

Rt.

20

217.11
 9.5
 5

216.7
 9.9

216.17
 10.46
 5 = Top
 cb.

214.83

11.80

on Stub.

209.47

17.16 = F.L. of Pipe
 (levelled over in Pipe)

214.43

12.20

Top cb.

213.41

13.22

Top
 grate

209.15

17.48

F.L. Box

214.33

12.30

214.41

12.22

on Cross

206.81

19.82

F.L. outlet.

226.63

2+18.3 = wly. of 6" Conc wall

2+00

1+72.8 = Fly. Dr.

1+60.8 = wly. of Conc. Dr.

1+57.8 = wly. of 3' Conc. flower box

1+50

1+11.4 = Fly. Dr.

1+03 = wly. of Conc. Dr.

Lt.

#

Rt.

21

221.7

222.58

4.9 = ground

4.05

Top wall

5.3
5 221.3

5.5
5 221.1

5.74
5 220.9

6.72
5 219.91
Conc.

7.15
5 219.48
Conc.

7.77
5 218.86
out

7.51
5 219.12
Conc.

7.6
5 219.0

7.6 = ground

5.69
5 220.94
Top Conc.

7.8
5 218.8

9.26
5 217.37
Conc.

9.51
5 217.12
Conc.

10.51
5 216.12
out

9.87
5 216.76

9.87 = Conc

226.63 ✓

3+68.5 - wly. 3' Conc. walk

T.P. 10.93 250.28 0.04 239.35

3+50

3+00

2+83

2+78

T.P. 13.20 239.39 0.44 226.19

2+50

2+31.7 = Ely. Dr

2+24.7 = wly of Conc. Dr

Lt.

±

Rt.

22

240.09
10.19

250.28 ✓

2.1 231.3

8.7 220.7
5

8.8 230.6

8.9 230.47
5 = Top
db.

10.4 229.0

12.4 227.0

239.39 ✓

1.4 225.2

223.11
3.52
Conc.

223.22
3.41
5
Conc.

222.57
4.06
226.63

221.88
4.75
5 = 9.4

5+40

5+00

4+60

4+30

4+00

3+97.5 = Ely. of Dr.

3+86.7 = wly. of Conc. Dr.

3+71.5 = Ely. of walk

Lt.

±

Rt

247.3
30

~~246.3~~
40
5

246.7
36

246.77
251
5-Top

71 246.2

54 244.9
5

51 245.2

245.31
4.97
5-Top cb.

74 242.9
5

73 243.0

243.00
7.28
5-Top
cb.

242.88
7.70
5-
Conc.

242.83
7.45
Conc.

242.17
8.11
5-9ut.

241.9
838
Conc.

240.19
10.10 Conc

250.28 ✓

= end.

in L of 10' Conc. Headwall

31.23' Rt. along \pm of pipe = inlet of 24" pipe

6.88' Lt. = outlet of 24" C.I. Pipe

7+80.35 =

7+50

7+00

6+50

6+00

+ Sea Breeze

Check B.M. = SW. B.P. Tibbemarle

2.69

247.59

✓ See D. 1092

5+83.72 = Ang 90° 03' 30" Lt.

Notes Reduced 2-21-49

247.70

8.58

F.L. outlet

247.72

2.56

31.23

Top Conc
Headwall

247.18

6.10

31.23 = F.L. inlet

246.68

3.60

on stub.

248.20

2.09

δ = Top
cb. +
9.4

248.6

1.7

15

247.3

5.0

10

247.9

2.4

247.94

2.34

δ = Top
cb.

249.0

1.3

5

247.8

2.5

247.72

2.36

δ = top cb.

247.8

2.5

248.0

2.3

5

247.4

2.9

247.57

2.69

δ = top cb.

247.49

2.79

on stub.

250.28 ✓

Walker
Johnson
Pope
Crawford
7-26-49

Location - Proposed Elec. Duct
Sewer
To Serve Proposed Pump Plant
Near Jenner And Coast Blvd.

1+86.59 Δ Lt. 22°26' on line

Note: * Indicates
Sta & Location of Duct
as Constructed.

NO. 20194

1+50 1.5 Lt. INDEXED
W.K.
JUL 28 1949

* 1+00 2 Lt.

0+92.82 Δ Rt. 51°59' Jet 1" x 1" Redwood & Disk

* 0+91 Pull Box 2.4 Lt.

* 0+85 5.1 Lt.

* 0+61 5 Lt.

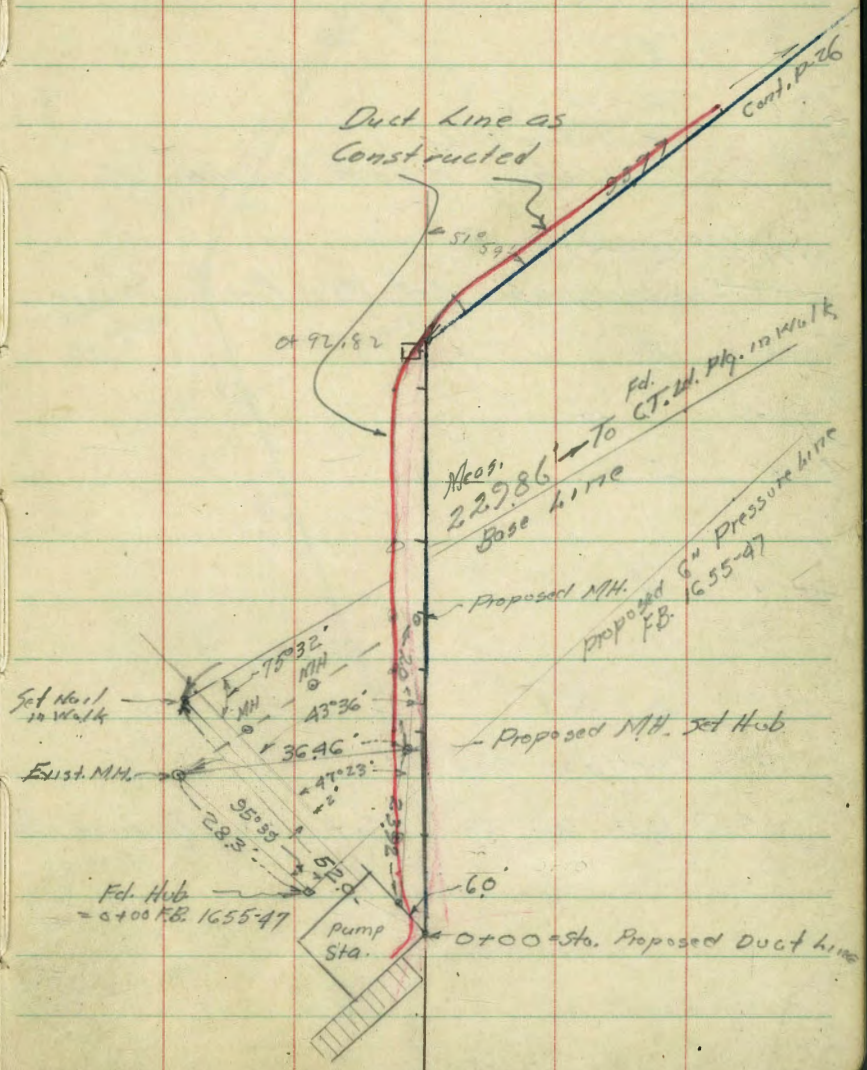
* 0+50 5.5 Lt.

* 0+41 5.1 Lt.

* 0+31 4.6 Lt.

* 0+15 4.2 Lt.

* 0+00 Duct 21 Lt
0+00 Set. Hub 2" x 2" x 10"



4158.15

4+48.15

* 3+65 Pull Box 1 RT.

* 3+51 7.5 RT.

* 3+40 6.5 RT.

* 3+21 E

* 3+14 2.5 LT.

* 2+95 Pull Box 3' LT.

Everything Ahead 10' too Long

2+78.35 (wood)

~~2+88.35~~ = A Rt. 51°45' Set 1" x 1" Redwood + Disk

* 2+76 E

* 2+60 3' LT

* 2+41 5' LT

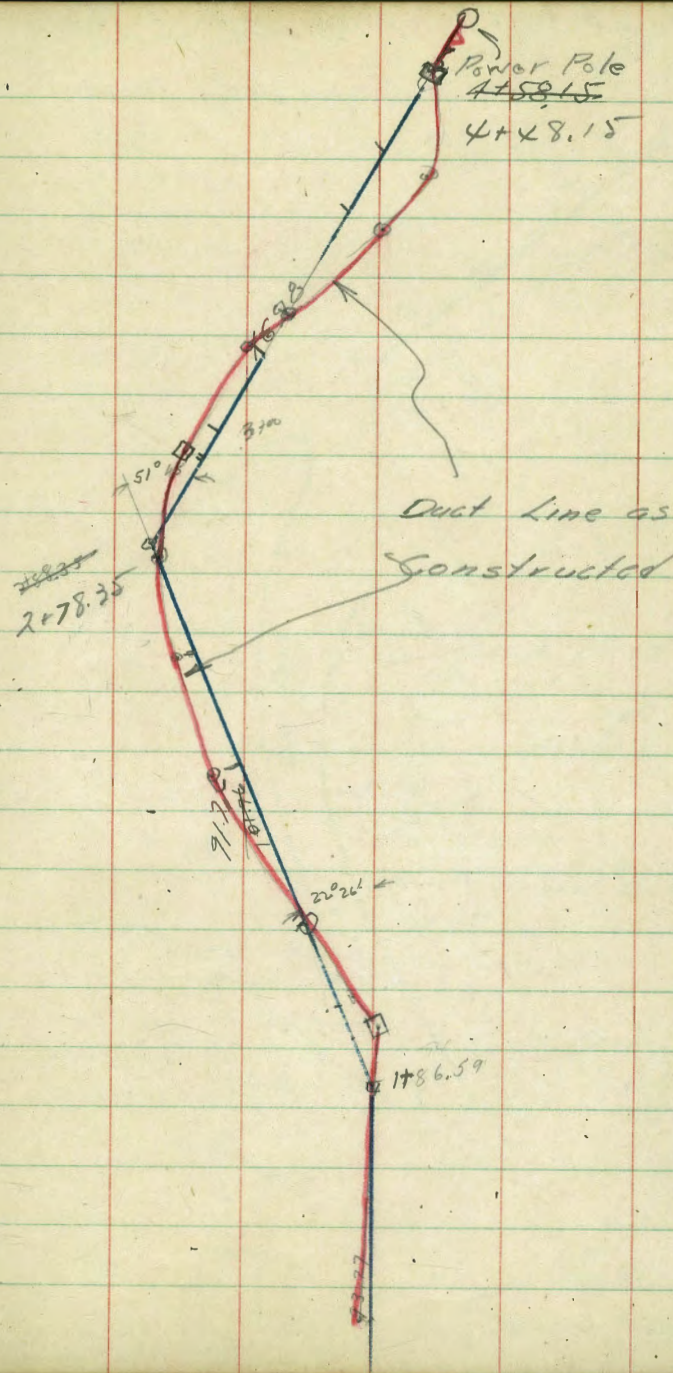
* 2+14 E

* 2+00 2.3 RT.

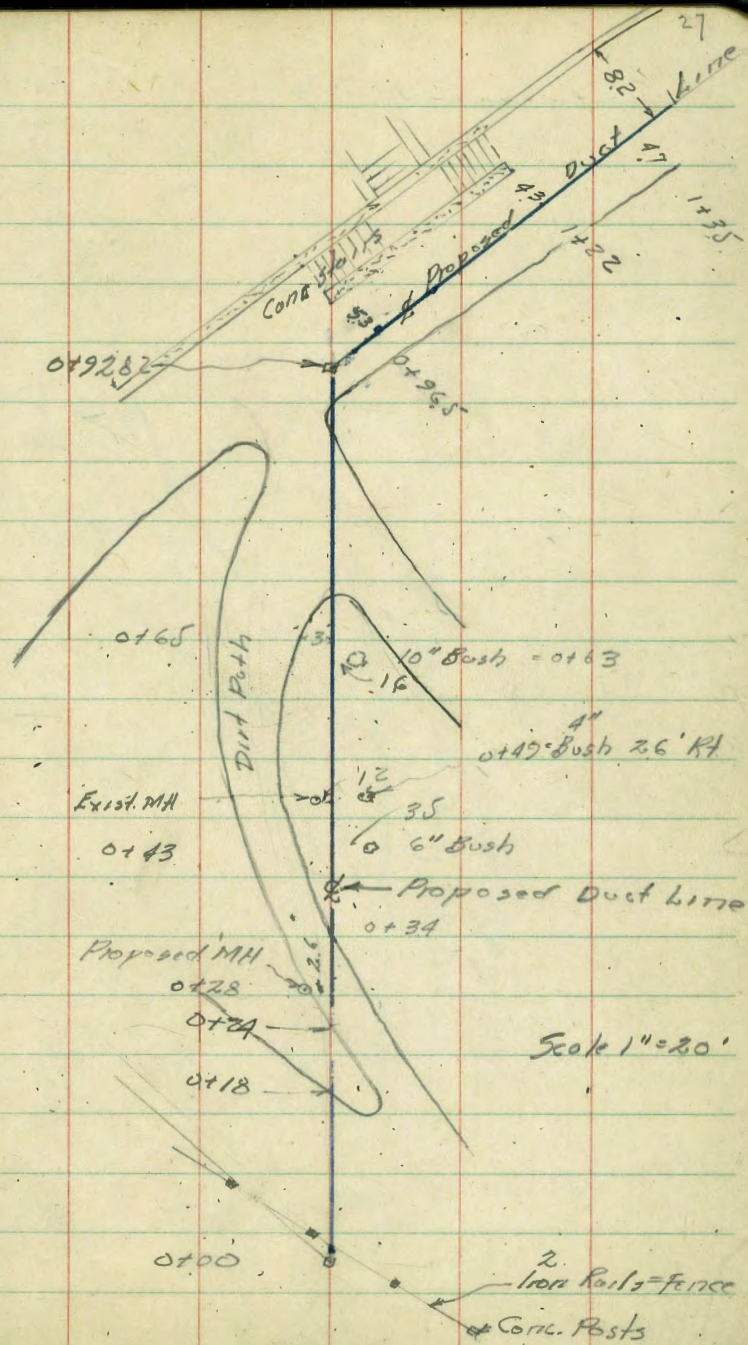
* 1+94 Pull Box 4.3' RT.

1+86.59 = B Lt. 23°36' Set 1" x 1" Redwood + Disk

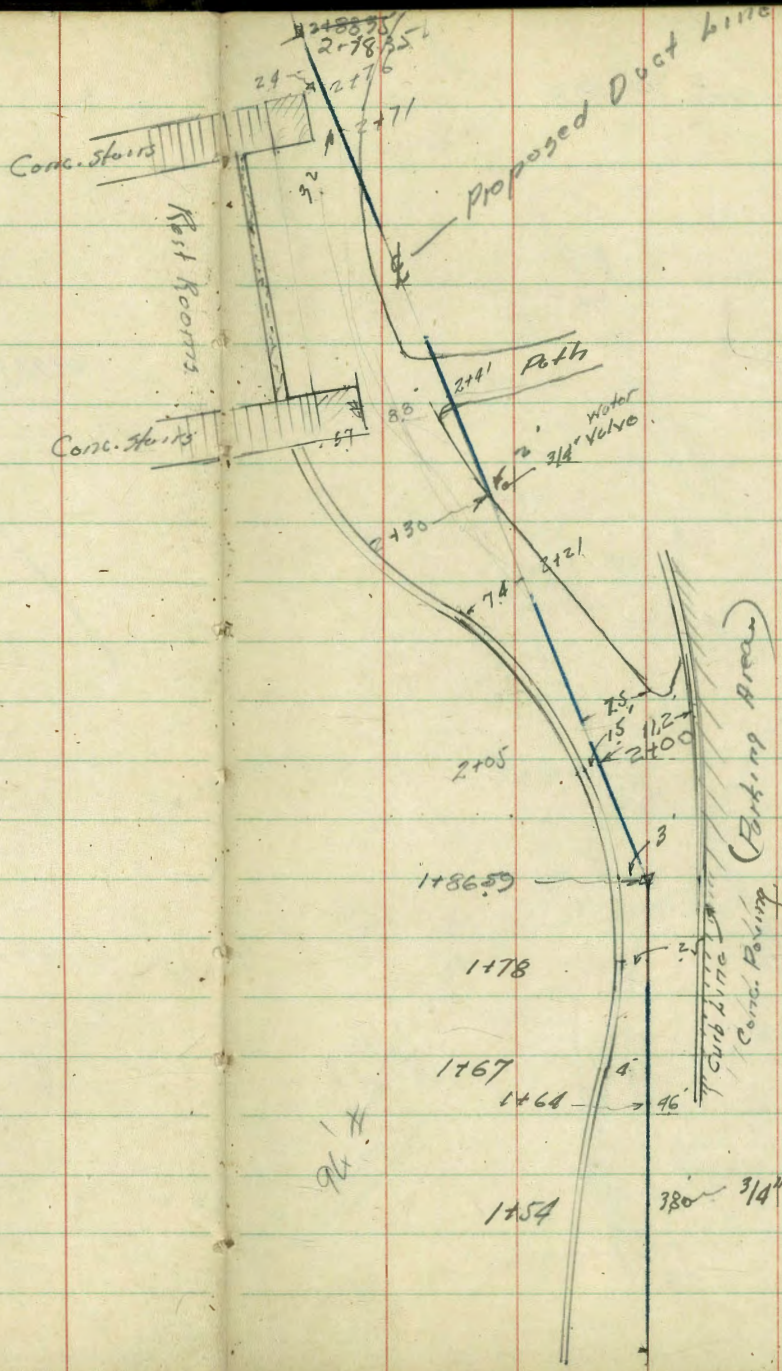
Cont. from P. 25



Details, Walks etc for
 - Location Proposed Duct
 Line P-25-26



Cont. from P-27

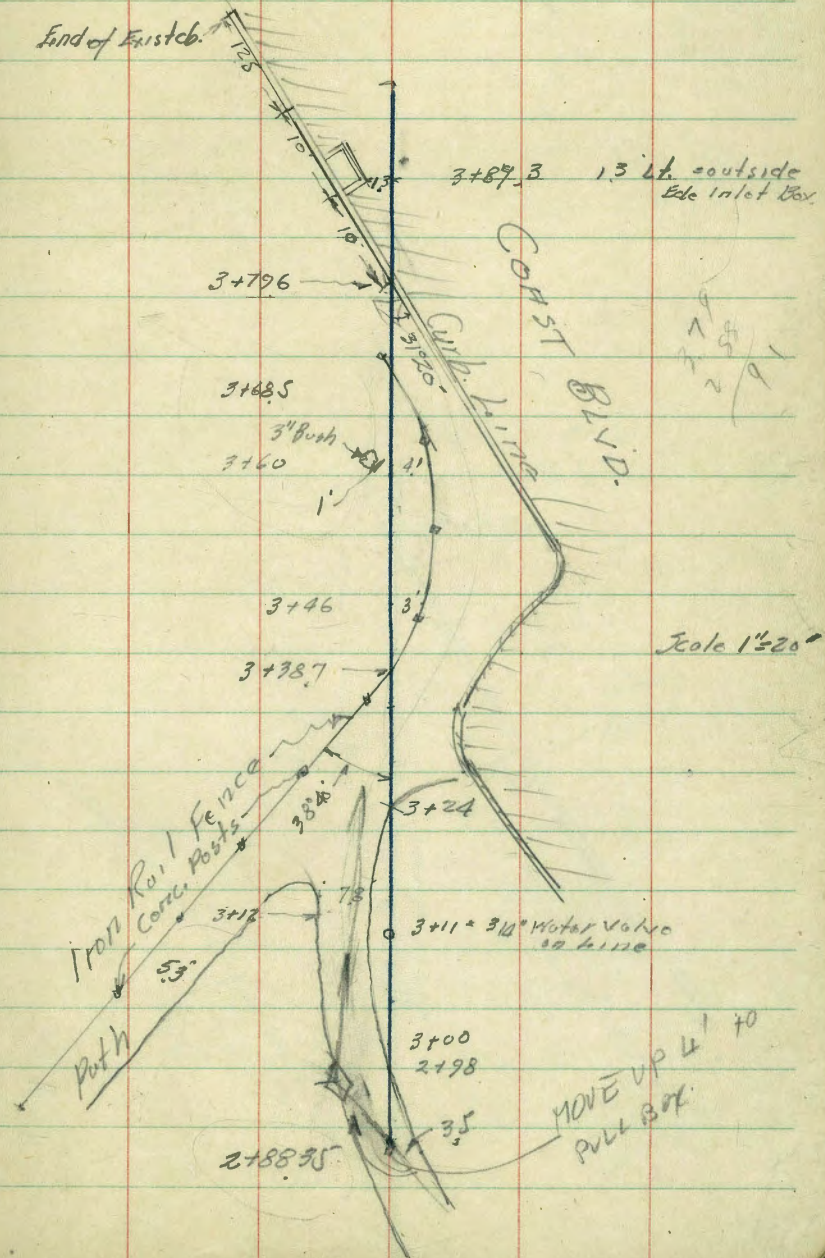


2+30
 1 86
 44

Scale 1"=20'

18

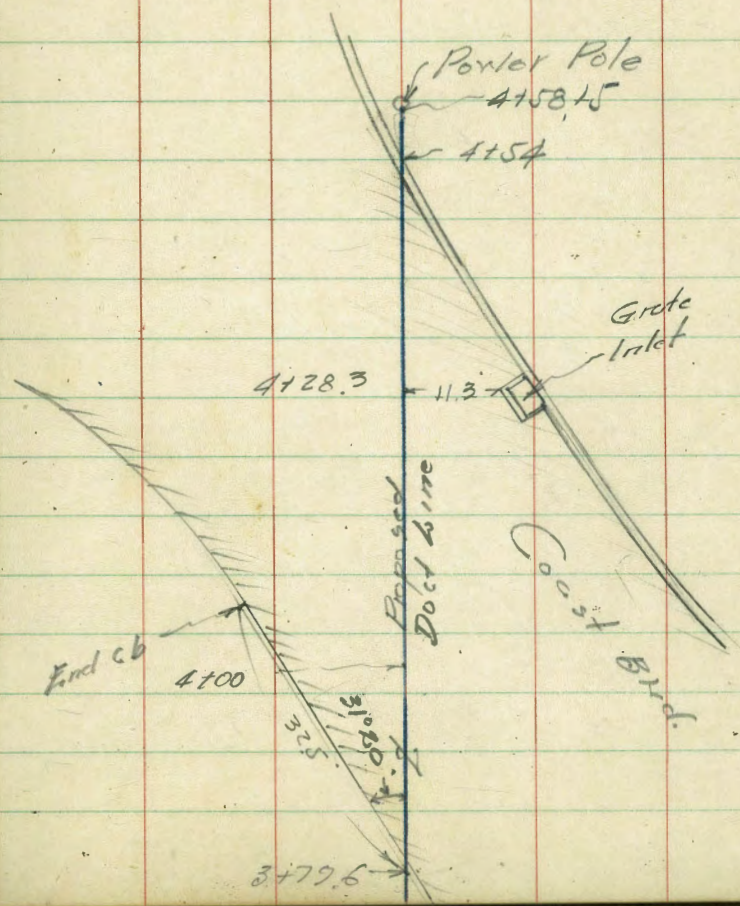
Cont. from P-28



Cont. from p-29

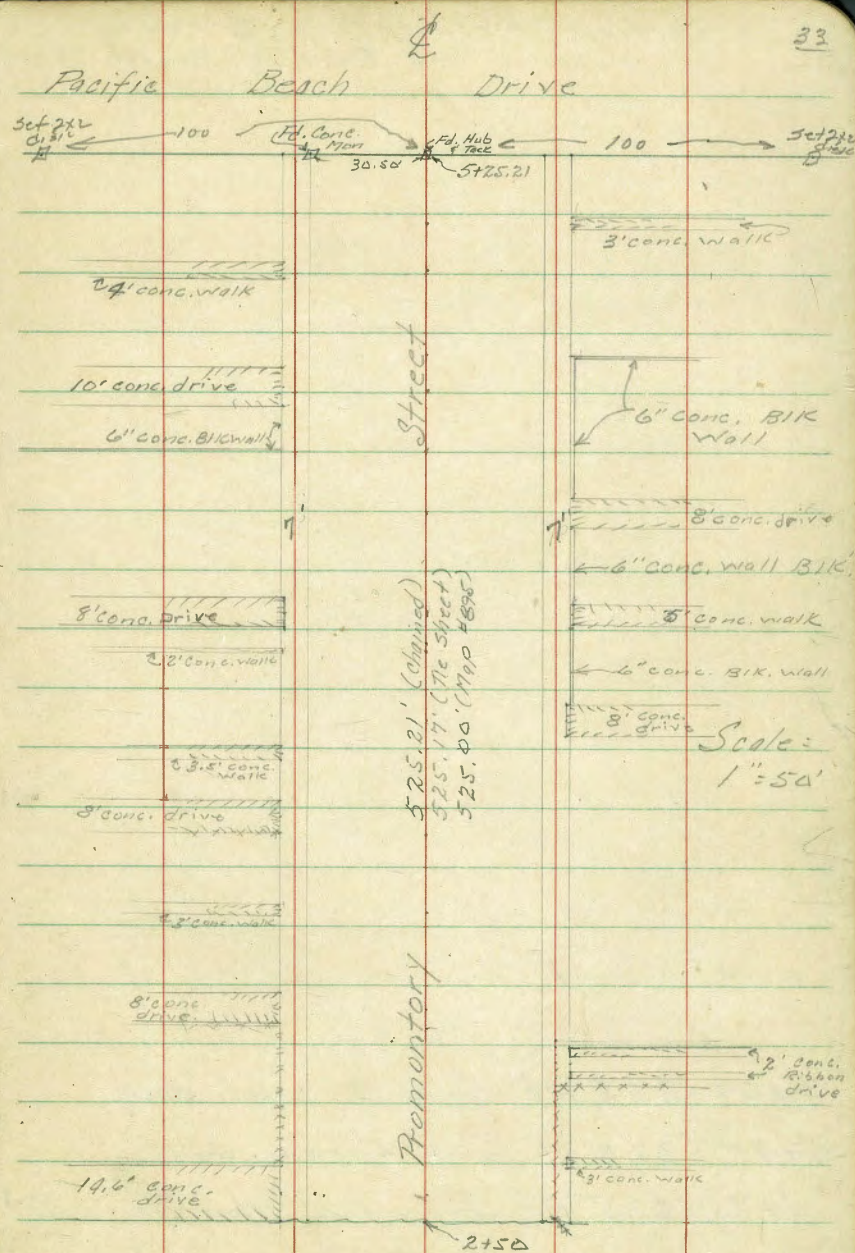
455
200
170

455
370
19



X-Section - Promontory Street
Fortuna to Pacific Beach Drive

- 4+66 - 37.5' Lt to & 10' conc drive
- 4+50 - 37.6' Lt to start 6" conc. blk wall
- 4+34 - 37.3' Rt to & 8' conc. drive
- 4+08 - 37.2' Rt to & 5' conc. walk
- 4+07 - 36.8' Lt to & 8' conc. drive
- 4+00 - 37.5' Lt to end wire fence
- 3+98 - 37.1' Lt to & 2' conc walk
- 3+89 - 37.5' Rt to 6" Conc. Block Wall
- 3+80 - 36.3' Rt to & 8' conc. drive
- 3+71 - 37.3' Lt to & 3.5' conc. walk
- 3+54 - 37.5' Lt to & 8' conc. drive
- 3+50 - 37.8' Lt start wire fence
- 3+30 - 37.3' Lt. to & 3' conc. walk
- 3+05 - 37.5' Lt. to & 8' conc. drive
- 3+00 - 37.5' Lt to end picket fence & 6" conc. found
- 2+91 - 37.5' Rt to 2' Ribbon Conc. drive
- 2+85 - 34' Rt. to 4' picket fence
37.5' Lt to start picket fence (6" conc. found)
- 2+65 - 36.5' Rt to & 3' conc. walk.
- 2+57 - 37.5' Lt to & 14.6' conc. drive
- 2+51 - 33.5' Rt to 4' picket fence
- 2+47 - 37.7' Rt to dog in 6' picket fence



X-section - Promontory Street
Fortuna to Pacific Beach Drive

34

5+09 = 37.5' Rt. to $\frac{1}{2}$ 3' conc. walk

4+97 = 37.8' Rt. to $\frac{1}{2}$ 4' conc. walk

4+75 = 37.5' Rt. to end 6" conc. BIK wall

X-Section - Promontory Street
Fortuna to Pacific Beach Drive

0+47 - 3' conc. walk

0+44

0+42

0+30 - 3' conc. walk

0+00 = No. P.L. Fortuna St.

0-37.5 = R. Fortuna St.

0-61

0-64

0-73 = So. line P.L. Fortuna

B.M.

6.74 51.61

7.59 44.02

44.87

Lt.

R+

35

8.6	8.7	8.6	8.4	7.9	6.6	5.7	4.9
50	37.5	20	20	20	37	39	50
45.0	43.1	43.3	43.2	43.7	45.0	45.9	44.2
8.57	8.27						
50	37.5						
43.4	43.4						
8.2	7.6	7.2	6.8	6.2	5.3	4.5	
50	37.5	20	20	21	37.5	50	
44.1	44.9	45.5	46.1	46.4	46.4	46.8	
7.0	6.7	6.1	5.5	5.2	5.2	4.8	
50	37.5	20	20	20	37.5	50	
45.3	45.7	45.8	46.3	46.8	47.1	47.2	
6.3	5.9	5.8	5.3	4.8	4.5	4.1	
50	37.5	20	20	20	37.5	50	
45.4	45.7	45.9	46.4	47.2	47.7	47.7	
6.2	5.8	5.7	5.2	4.4	3.9	3.9	
50	37.5	20	20	15	37.5	50	
46.4	46.2	46.3	47.1	47.4	47.7	47.5	
6.2	5.4	5.2	4.5	4.2	4.1	4.1	
50	37.5	20	10	20	37.5	50	

51.61

Left in Conc. Man. 7' line Fortuna & Promontory

Left & Fortuna & Ingraham

N-section - Promontory Street
Fortuna to Pacific Beach Drive

2+00

1+80 = ± 3' Conc. Walk

1+55 = ± 8' conc. drive

1+50

1+31 = ± 3' conc. Walk

1+05 = ± 8' conc. drive

1+00

0+87.5 = ± 3.5' Conc. Walk

0+70

0+57 = ± 11' Conc. Drive

0+56 = ± 8' conc. drive

43.0
8.6
50

42.9 Lt
8.7
37.5

42.7
8.9
20

42.6
9.0
20

43.10 Rt
8.6
37.5

43.2
8.4
50

43.16
8.45
50

43.07
8.54
37.6

8.8
50

42.8
8.8
37.5

42.5
9.1
20

42.5
9.1
20

42.8
8.8
37.5

42.8
8.8
50

42.6
9.0
50

42.5
9.0
37.5

42.5
9.1
20

42.6
9.0
20

43.2
8.4
37.5

43.6
8.0
50

42.8
8.8
50

42.6
9.0
37.5

42.6
9.0
20

43.1
8.5
20

43.9
8.16
37.5

44.1
7.8
50

43.14
8.47
50

43.18
8.43
37.7

44.2
7.17
38

44.67
6.94
50

37.61

V-Section - Promontory St
Fortuna to Pacific Beach Drive

3+54 = \$ 8' conc. drive
3+50
3+30 = \$ 3' conc. walk
3+05 = \$ 8' conc. drive
3+00
2+91 = \$ Ribbon conc. drive
T.P. 61.74 50.78 7.57 44.04
2+65 = \$ 3' conc. walk
2+57 = \$ 14.6' conc. drive
2+22

	44.75	44.55	Lt.	\$	Rt.	37
	6.03	6.23				
	50	37.5				
	44.70	44.4		44.1	44.2	
	6.1	6.4		6.7	6.6	
	50	37.5		20	20	
	44.40	44.31		43.7	43.8	
	6.38	6.47				
	50	37.5				
	44.18	44.03				
	6.60	6.75		44.1	44.2	
	50	37.5		20	20	
	44.2	43.8		43.6	43.9	
	6.6	7.0		7.2	6.9	
	50	37.5		20	20	
	44.2	43.4		43.3	43.4	
	6.9	7.4		7.5	7.4	
	50	37.5		20	20	
	44.2	43.7				
	7.07	7.00				
	50	37.5				
	50.78					
	43.36	43.91				
	8.25	8.20				
	38.5	50				
	43.90	43.76				
	7.77	7.85				
	50	37.5				
	43.4	43.5		43.3	43.6	
	8.1	8.1		43.0	43.8	
	50	37.5		20	24	
	43.4	43.8				
	8.0	7.8				
	33.5	50				
	51.61					

X-Section - Promontory 3+
Fortuna to Pacific Beach Drive

Lt. C Rt. 29

0.01
46.13
4.88 46.14

= L. & C. T. So. P.L. Pacific Beach Dr & Ingraham

T.P. 3.59 51.02 3.35 47.43

6+06

+1.30 13.0 11.5 1.3 2.7 3.8
100 50 50 50 50 100
52.20 53.8

6+00

+1.14 11.4 9.6 2.9 3.9 4.4
100 50 50 50 100
52.20 50.3 48.3 49.5 46.9 44.4

5+69

+1.14 1.14 0.8 2.3 3.3 4.2 5.0
100 50 20 20 20 50 100
52.20 50.0 48.5 47.8 47.5 46.6 45.8

5+65

+2.5 2.5 0.4 1.9 2.7 3.1 3.7 4.5
100 50 20 20 20 50 100
48.9 49.0 46.7 48.1 47.1 47.1 46.3 45.8

5+75, 17 = 50. Prop. Line Pacific Beach Dr.

1.9 2.8 3.3 4.1 4.3 4.5 4.5
50 20 20 20 20 37.5 50
48.9 45.87 45.92

5+09 = \$ 3' conc. walk

4.81 4.86 37.5 46.6 46.1 45.8 45.8 45.9
50 37.5 50 50 50 37.5 50

5+00

2.4 3.6 4.7 4.7 5.0 5.0 4.9
50 37.5 20 20 20 37.5 50

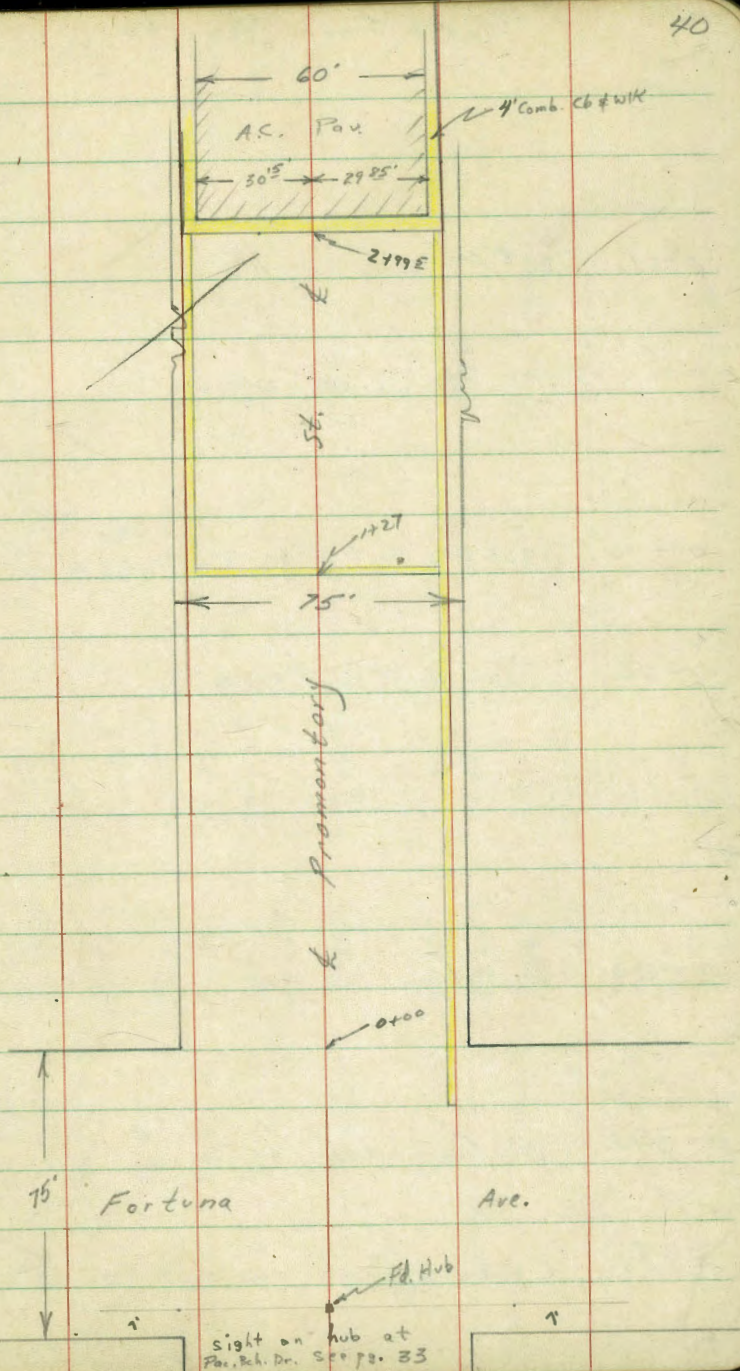
50.78

X-Sect. Promontory
(Fortuna south to Payment)

10-10-49
Robert
Hendricks
Greer
Bunch
w.p. 25020

Map 895

INDEXED
M.K.
OCT 11 1949



0+01 26¹/₂' Rt Fire plug

47.7	47.7	47.3	46.6	46.5	46.36	45.3	44.5	44.4
3.6	3.6	4.0	4.7	4.8	4.94	5.0	6.8	6.9
50	37 ¹ / ₂	40	7	25	32 ¹ / ₂	39	60	100

0+06 S. Prop. Line Fortuna

0-10 30¹/₂' Rt East Edge 3' walk (Beginning N. & S. walk)

45.19
5.11
302

0-12 38¹/₂' Rt. P. Pole #P1549

0-17

46.9	48.2	48.8	48.2	47.7	47.8	47.0	46.4	46.0	46.3	46.8	46.0	45.5	45.2	45.1	45.0
4.4	3.1	3.5	3.1	3.6	3.5	4.3	4.9	5.3	5.0	5.5	5.7	7.0	7.4	7.7	8.1
200	138	184	100	50	37 ¹ / ₂	6	49	20	24	37 ¹ / ₂	50	100	121	126	135

0-20

47.0	48.2	48.2	47.8	47.2	47.1	46.5	46.3	45.7	45.6	45.4	45.0	43.9	43.9	43.4	43.3
4.3	3.1	3.1	3.5	4.1	4.2	4.8	5.0	5.6	5.7	5.9	6.3	7.4	7.9	8.0	8.1
200	138	134	100	50	37 ¹ / ₂	6	50	20	24	37 ¹ / ₂	50	100	121	126	135

0-37¹/₂ ℳ Fortuna

47.3	48.2	47.7	45.8	45.5	46.1	45.0	44.6	43.9	42.9	42.8
4.0	3.1	3.6	4.5	4.8	5.2	6.3	6.7	7.9	8.4	8.5
200	142	100	50	37 ¹ / ₂	52	37 ¹ / ₂	50	100	150	200

BM 643 51.30

44.87

L & C.T. ℳ Fortuna & Ingraham

2+00

1+50

T.P.

4.28

47.73
↑

7.85

48.45

1+27

North Edge ^{cont.} 4' Walk (E & W) 32.9' x 2 3' Walk
Running N & S

1+14

0+97

0+50

51.30
↑

43.0	42.8	42.6	42.8	42.78	42.9	42.1
47	49	51.1	49	49.5	48	46
50	372	329 WK		52 WK	372	50

43.2	43.1	42.97	43.4	43.5	42.15	43.2
45	46	47	43	42	458	45
50	372	329 WK		19	32 WK	50

47.73
↑

43.3	43.20	43.4	43.60	43.5
8.0	8.10	7.86	7.70	7.8
50	372		32	50

43.5	43.9	44.1	44.21	44.97	45.3	44.3.7
7.8	7.6	7.2	7.09	7.6	8.0	7.6
50	372		32 WK	50	60	87

47.3	47.4	47.1	46.9	45.5	45.21	45.4	45.5
4.0	3.9	4.2	4.4	5.8	6.8	7.9	7.8
50	372		11	29	32 WK	60	82

47.7	47.7	47.1	46.8	46.47	46.5	43.8	43.9
3.6	3.6	4.2	4.5	4.83	4.8	7.5	7.4
50	372		29	32 WK	34	57	84

51.30
↑

Start. B.M.

check 2.29 4487 = 4487

T.P. 4.18 47.16 4.75 42.98

3+53^E

3+03^E Gutter

3+03^E Curb

2+99^E Begin N'Walk & Curb

2+85

2+50

47.73
↑

40.62	40.53	40.15	39.73	39.74	40.45	40.92	41.00
7.11 34.15	7.20 30.15	7.57 30.15	8.00 30.15	7.99	7.18 29.85	6.81 29.85	6.78 35.15
			6.95 30.15	7.25	6.91 29.85		
	4.35	4.27	4.80	4.25	4.35		
	6.38 34.15	6.46 30.15	6.93	6.48 29.85	6.48 30.15	6.48 30.15	
	4.13	4.42	4.87	4.39	4.15		
	6.4 50	6.81 37.5 Edge WIK	6.86	6.54 33.80 Edge WIK	6.41 37.5	6.41 37.5	6.41 37.5
	4.55	4.59	4.17	4.63	4.17	4.20	
	6.4 50	6.14 32 WIK	6.0	6.0 32 WIK	6.0 37.5	6.0 50	
	42.1	43.24	42.3	42.18	42.0	42.6	
	5.6 50	4.49 32 WIK	5.4	5.45 32 WIK	5.3 37.5	5.1 50	

47.73
↑

Cont'd From Page 44

1+00

0+80 20.54 & 17' Drive open in curb

0+50

0+196 Pav. Edge

0+00 North Prop. Line Moorland

0-10 Curb Line Moorland

0-25 & Moorland Drive

BN 0.41 $\frac{34.09}{\lambda}$

33.68

NWBP Ingraham & Moorland $\frac{34.09}{\lambda}$

4.811	27.59	27.59	27.6	27.39	27.79	27.80
5.98	6.5	6.5	6.5	6.7	6.3	6.29
20.6	20.6	10.2	6.5	10.2	20.4	20.4
cb	Gutt				Gutt	cb (Drive)

27.85
6.24
20.5
cb

28.85	27.89	27.99	27.99	27.89	27.49	27.93
5.24	6.2	6.1	6.1	6.2	6.6	6.16
20.6	20.6	10.2		10.2	20.5	20.3
cb	Gutt				Gutt	cb

29.40	28.91	28.90	28.71	28.43	27.99	28.40
4.69	5.18	5.19	5.34	5.66	6.10	5.64
20.8	20.8	10.25		10.25	20.3	20.3
cb	Gutt				Gutt	cb
bc	bc				bc	bc

30.36	29.87	29.55	29.17	28.97	28.66	28.31	27.94	27.57	27.39	27.85	26.17	26.69
3.73	4.12	4.34	4.92	5.12	5.43	5.78	6.15	6.52	6.70	6.24	7.72	7.40
100	100	50.5	50.5	37.5	20.5		20.5	37.5	50.5	50.5	100	100
cb	Gutt	bc	bc						Gutt	cb	Gutt	cb
									bc	bc		

30.15	29.25	29.03	28.67	28.44	28.00	27.63	27.42	26.31
3.74	4.84	5.06	5.42	5.15	6.09	6.46	6.67	7.78
100	50	37.5	20.5		20.5	37.5	50	100

1772 216' Lt. Center 14" Pepper tree

1750

1742 375' Rt & 25' Conc. Walk

1737 233' 6" Shrub?

1725 375' Rt & 83' Conc. Drive

1724 295' Lt & Double Ribbon Drive { 2' strips
65' overall

1714⁴⁹ End Cb. & Walk

1703 20.4' Rt & 18.5' Drive open in cb.

34.09
/

4

4

Rt 46

29.19	28.69	28.09	27.99	27.49	27.09	27.39	27.49	27.89
49	5.4	6.0	6.6	6.6	7.0	6.7	6.6	6.2
50	37.5	21	20.5		20.5	22.5	37.5	50

27.57	27.89
6.52	6.20
37.5	50
conc.	conc.

27.53	27.89
6.52	6.20
37.5	50
conc.	

28.37	28.09
5.72	6.00
37.5	27.5
conc.	conc.

28.39	28.13	28.05	27.97	27.49	27.59	27.59	27.29	27.09	26.97	27.09	27.09
52	5.7	5.96	6.04	6.12	6.6	6.5	6.8	7.0	7.12	7.05	7.00
50	37.5	29.5	24.5	20.5	20.5	10.2	10.2	20.5	20.5	24.5	27.5
		Walk	Walk	cb	Gut			Gut	cb	Walk	Walk

26.76
233
20.4
Drive

34.09
/

Cont'd From Page 46

2+84 375' Rt. & 8' Conc. Drive

2+82 375' Lt. & 7' Conc. Drive

2+52 375' Rt. & 2' Conc. Walk

2+50

2+28 375' Rt. & 7' Conc. Drive

2+00

T.P. 480 32.38 6.51 27.58

34.09

Lt.

R

R

47

27.49

489
376
conc.

27.60

478
50
conc.

29.04

334
50
conc.

28.68

370
375
conc.

27.43

495
375
conc.

27.53

485
50
conc.

28.38

4.0
5.0

28.28

4.1
37.5

27.98

4.4
22

27.78

5.1
20

27.48

4.9

27.08

5.3
19

27.48

4.9
24

27.38

5.0
37.5

27.38

5.0
50

27.36

5.2
37.5
conc.

27.33

5.95
50
conc.

28.38

4.0
5.0

27.98

4.4
37.5

27.88

4.5
22

27.18

5.2
19

27.58

4.8

27.28

5.1
17

27.48

4.9
20

27.08

5.3
37.5

27.08

5.3
50

32.38

Cont'd From Page 47

448

28.18	28.58	28.58	27.48	27.58	27.28	27.88	28.18	28.18
42	3.8	3.8	4.9	4.8	5.1	4.5	4.2	4.2
50	37.5	21	19		17	22	37.5	50

4423 33' Lt. & 25' Conc. Walk

28.39	28.44	28.48
3.99	3.74	3.90
50	37.5	33
conc.	conc.	conc.

4400

29.18	28.98	28.78	27.68	27.88	27.38	28.28	28.28	27.98
3.2	3.4	3.6	4.7	4.5	5.0	4.1	4.1	4.4
50	37.5	21	19		18	26	37.5	50

3463 37.5' Rt. & 8.5' Conc. Drive

28.07	28.12
4.31	4.26
37.3	50
conc.	conc.

3450 37.6' Rt. & 25' Conc. Walk

29.08	28.68	28.38	27.58	27.88	27.48	27.88	27.98	27.98	28.12
3.3	3.7	4.0	4.8	4.5	4.9	4.5	4.4	4.4	4.26
50	37.5	21	20		17	25	37.6	37.6	50
							conc.	conc.	conc.

3400

28.78	28.38	28.18	27.38	27.78	27.48	27.68	27.58	27.68
3.6	4.0	4.2	5.0	4.6	4.9	4.7	4.8	4.7
50	37.5	22	19		25	26	37.5	50

2499 37.6' Rt. & 3' Conc. Walk

27.56	27.68
4.82	4.70
37.6	50
conc.	conc.

32.38

32.38

5463 27' Lt Center 14" Pepper tree

5450

25.78	25.68	26.08	26.98	26.68	27.38	27.78
6.6	6.7	6.3	5.4	5.7	5.0	4.6
50	37.5	19		20	37.5	50

5446 37 1/2' Rt & 2 1/2' Conc. Walk

5436 37 1/2' Rt & 8 1/2' Conc. Drive

27.68	28.04
4.70	4.34
37.6	50
conc.	conc.

27.78	28.08
4.60	4.30
37.6	50
conc.	conc.

5400

26.48	26.88	27.28	27.48	26.98	27.68	28.08	27.88
5.9	5.5	5.1	4.9	5.4	4.7	4.3	4.5
50	37.5	20		16	25	37.5	50

4472 36 1/2' Lt & 2 1/2' Conc. Walk

4450

27.44	27.37
4.94	5.01
50	36.3
conc.	conc.

27.48	27.58	27.48	27.58	27.28	27.88	28.18	28.18
4.9	4.8	4.9	4.8	5.1	4.5	4.2	4.2
50	37.5	19		17	22	37.5	50

32.38

32.38

Cont'd From Page 49

6+93 38^E' Lt. Center P. Pole #5P1647

6+86 27' Lt. Center 24" Cypress Tree

6+74³⁹ { 20^E' Lt. Center 3' Euc. Tree

{ So. Prop Line La Playa

6+70 22' Rt Center Fire Hydrant

T.P. 3.02 30.45 4.95 27.43

25.45 24.75 25.35 24.65 24.25 24.35 24.75 24.55
 5.0 4.7 5.1 5.8 6.2 6.1 6.2 5.7 5.9
 50 37.5 32 27 16 29 37.5 50

25.65 25.75 25.65 24.95 24.55 24.65 25.05 25.35 24.95
 4.8 4.7 4.8 5.5 5.9 5.8 5.4 5.1 5.5
 50 37.5 24 19 5.9 13 23 37.5 50

~~30.45~~

6+50

6+42 26' Lt. Center 26" Euc. Tree

6+08 27' Lt Center 40" Eucalyptus Tree

6+00

5+91 39^E' Rt & 2^S' Conc. Walk

26.28 25.98 25.78 25.38 24.88 24.78 24.48 24.18 24.58
 6.1 6.4 6.9 7.0 7.5 7.6 7.9 7.9 7.8
 50 37.5 33 25 20 20 20 37.5 50

26.28 25.42 25.02 25.98 25.98 25.42 26.08 26.48
 6.1 6.9 7.3 6.4 6.4 6.9 6.3 5.9
 50 37.5 21 6 24 37.5 50

26.28 26.52
 6.10 5.86
 39.4 56
 conc conc

~~32.38~~

~~32.38~~

7+27⁸⁸ Curb Line

7+28⁸⁸ Edge Conc. Gutter

7+16⁷ & Pav. Strip

T.P. (7+03⁶) & Yosemite # Edge Pav.

Check			1.94	33.68	= 33.68
T.P.	8.59	35.62	3.42	27.03	

7+09

7+03⁶ Pav. Edge

6+98

30.45

24.80	25.29	24.52	25.02	24.40	24.89	24.72	24.42	24.52 (51)	24.01
5.32	5.83	5.10	5.10	5.72	5.23	5.40	5.90	5.60	5.11
100	100	37.5	37.5	Gutt	cb	cb	6.16	100	100
Gutt	cb	Gutt	cb	Gutt	cb	cb	Gutt	cb	Gutt

24.84	24.60	24.44	24.28	24.65
5.28	5.52	5.18	5.84	6.07
100	37.5		37.5	100

24.09	24.76	24.58	24.47	24.16
5.08	5.36	5.54	5.65	5.96
100	37.5		37.5	100

Starting BM

25.02	24.83	24.76	24.71	24.68	24.64	24.61	24.58	24.52	24.45	24.29
5.43	5.01	5.69	5.24	5.77	5.81	5.44	5.87	5.93	6.00	6.11
100	50	37.5	24.5	10.25		10.25	20.5	37.5	50	100

24.90	24.67	24.61	24.57	24.52	24.50	24.45	24.39	24.29	24.31	24.15
5.55	5.78	5.24	5.28	5.93	5.95	6.00	6.06	6.11	6.14	6.30
100	50	37.5	20.5	10.25		10.25	20.5	37.5	50	100

24.55	25.35	24.25	24.45	24.15	24.05	24.15
5.9	6.1	6.2	6.0	6.3	6.4	6.3
50	37.5	20		20	37.5	50

30.45

Survey for 36" drain

4-17-50 at Catalina Blvd. + Jennings

Moose
8899
Crawford

INDEXED

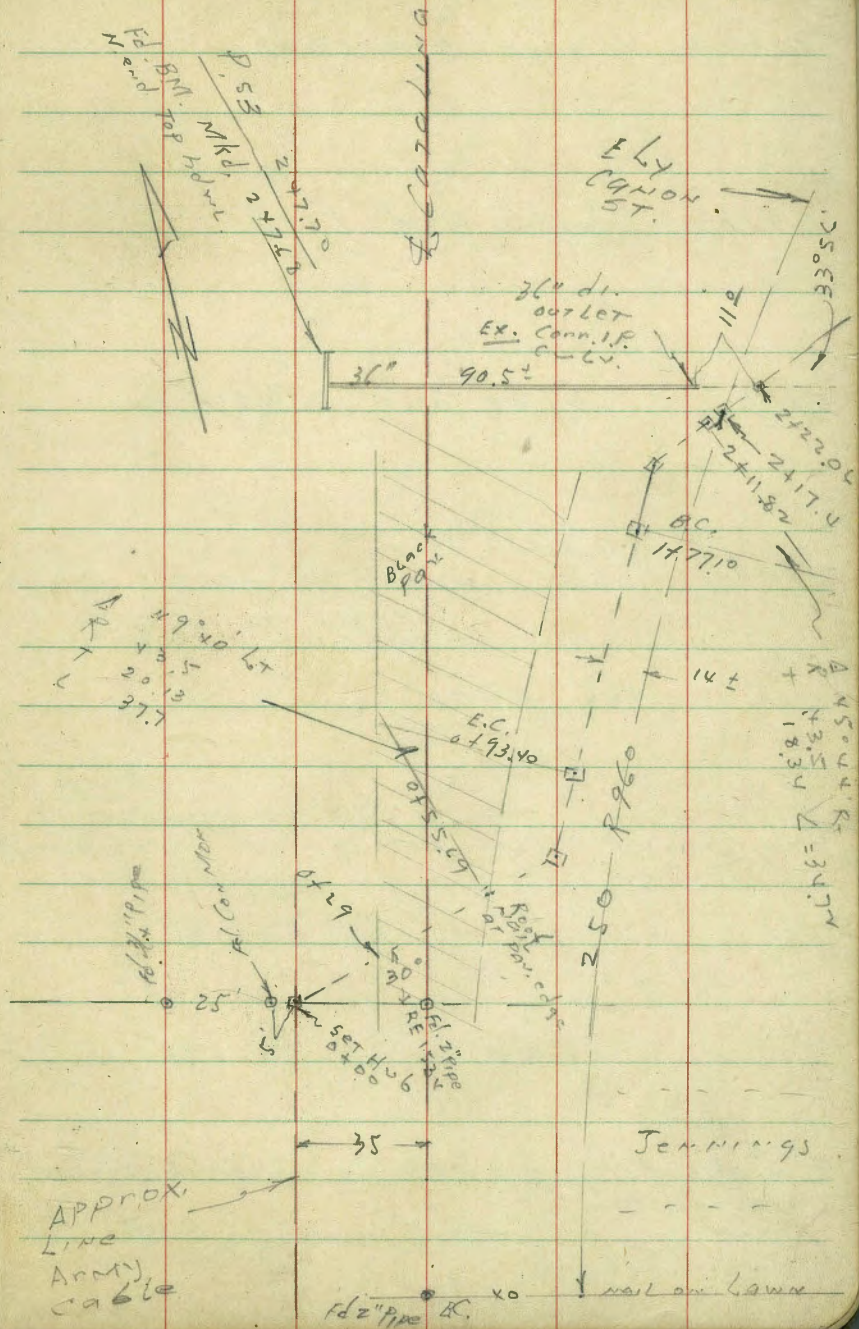
M.K.
APR 18 1950

W.D. 20658

□ set Hubs & disks

Note: large water line
and H.P. Gas
on Catalina Blvd.

South line Colonial Manor



Levels for drainage

0+291 W. edge Blk Pav.

0+18 Shoulder Old F.L.L.

0+11 8' Lt to S. side 4.5 d. Palm

0+00 U.S. Cable approx 30" deep

x56 25226

T.P. (70 247.70

Pholps

247.68

T.P. 255 250.40 851 251.85

T.P. 3.53 260.36 5.96 256.83

B.M.
NW BP 2.11 262.79 260.68 Record
Carolina Blvd
and
Santa Barbara

Lt

2493
30

Rt 53

2
2495
5.1
10

2495
28

2495
2.8
10

2493
5.0
8
Palm

2495
4.5

2491
2.6
10

2495
48

25226

Found
MKd BM N. end Inlet to W.L.
EXISTING CULV.
ACROSS CATALINA

Mkd on curb by BLISS

260.68

1450

1

0193.40 EC

0174.54 2 curve

0157.7 Edge BLK Pav

0155.69 BCLT

0140.5 2 Pav

2474
4.9

2473

2473

2480
3

248.11
5

2482

2489
3

252.26

2+22.06 Increase line of existing 36" Culv

2+17.4 Ely Canyon St

2+11.87 E.C.

2+03.2 E of Tel. Co. D.M.

1+94.5

1+85.8

1+77.10 BCR

244.03 L.T. 7
 8.23
 26.
 INLET
 36"

243.7
 8.6
 ground

240.70
 11.55
 11
 36" pipe
 outlet

243.2
 9.1

R 55

243.9
 8.4
 10

243.2
 8.6

243.5
 8.8
 12

246.8
 11.5
 12

244.5
 11.8
 10

244.2
 8.1

244.1
 10.2

249.0
 11.3
 10

245.1
 11.6
 10

245.6
 11.7

245.9
 11.4
 10

247.1
 11.2
 10

247.5
 11.8

248.3
 11.0

247.0
 11.3
 15.5
 E. edge Blk
 Pav

247.3
 11.9

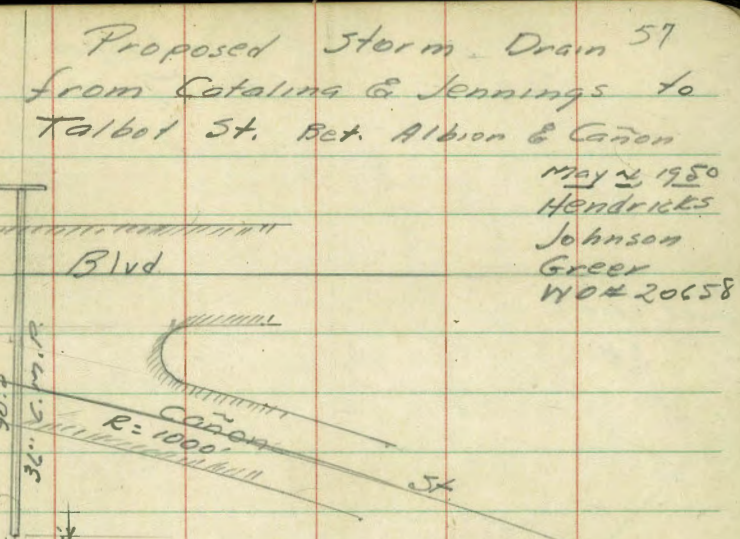
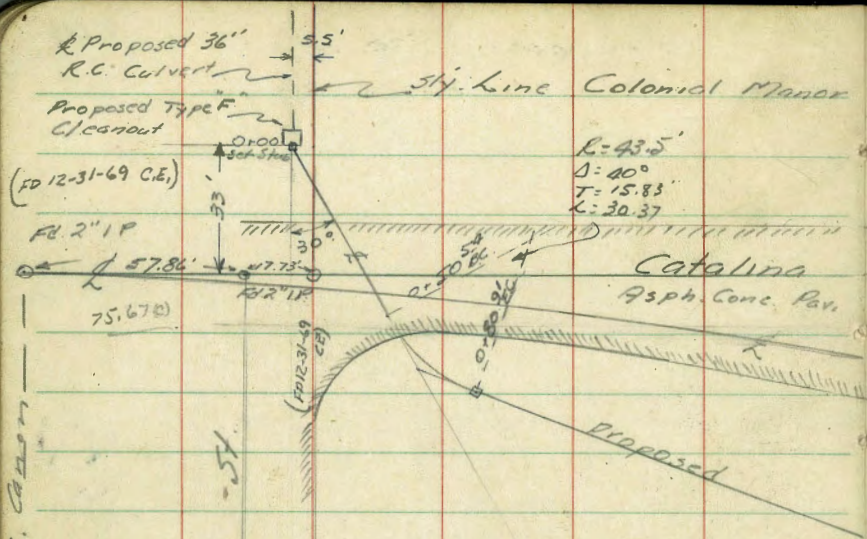
248.1
 11.5
 12.47 H
 8.9
 4.2
 10

252.26

3 + 22

2 + 72

238¹
142240³
120252.26REDUCED A 19.50
P.V.5.



Proposed Storm Drain 57
 from Catalina & Jennings to
 Talbot St. Bet. Albion & Cañon
 May 4, 1950
 Hendricks
 Johnson
 Greer
 No. 20658

INDEXED
 MAY 5 1950
 N.Y.C.

R=43.5
 Δ=55°
 T=22.64
 L=41.76

R=43.5
 Δ=10°
 T=3.81
 L=7.57

Cont'd P. 58

BE. Cañon

Jennings - 54'

(FD 12-31-69 C.E.)

FR 2" IP

75.67

(FD 12-31-69 C.E.)

Proposed

Catalina Blvd
 9.5 ph. Conc. Pav.

Storm Drain

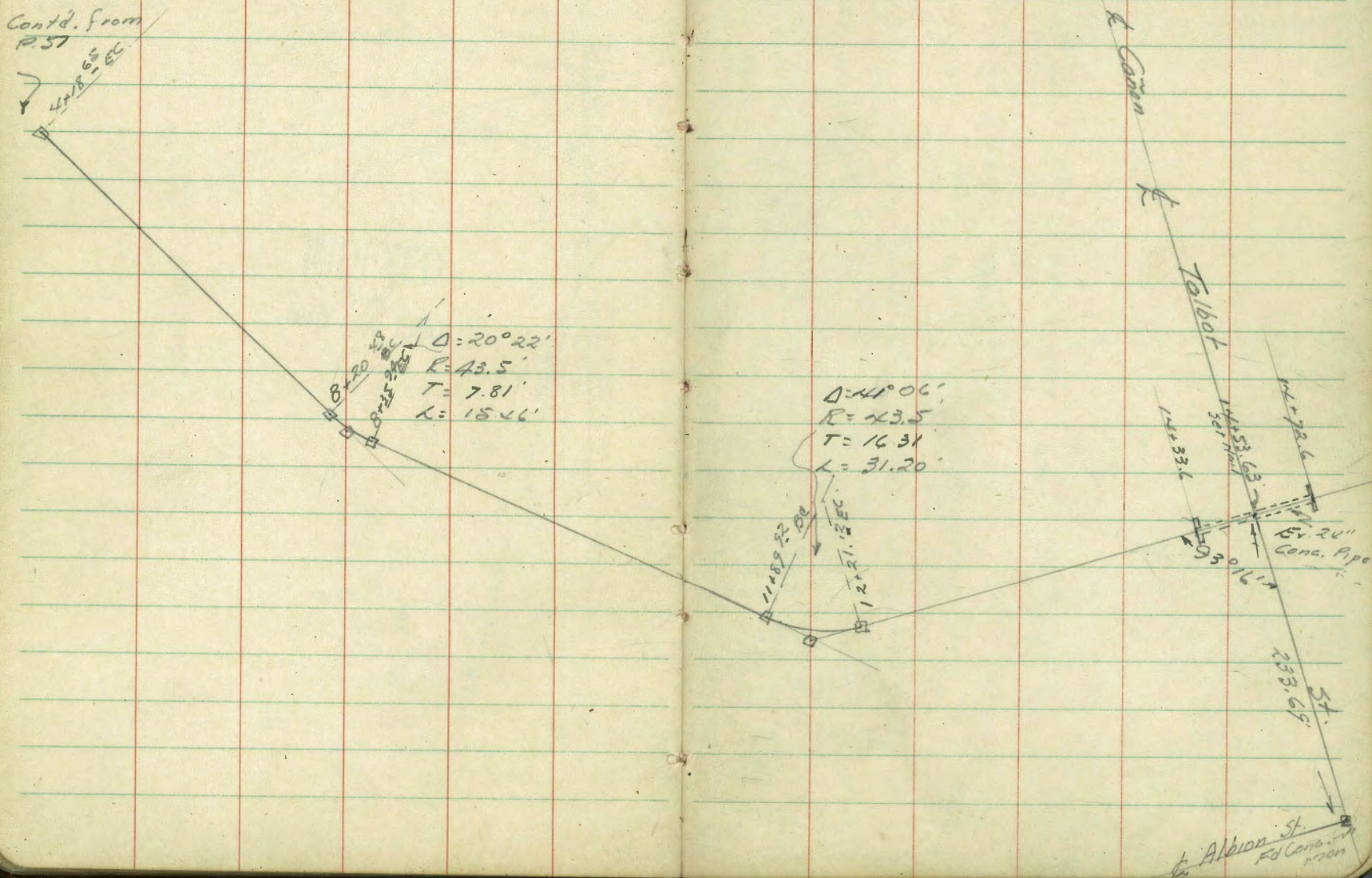
150.04'

Drain

1868 BC

Proposed Storm Drain
Contd. from P. 57

Contd. from
P. 57

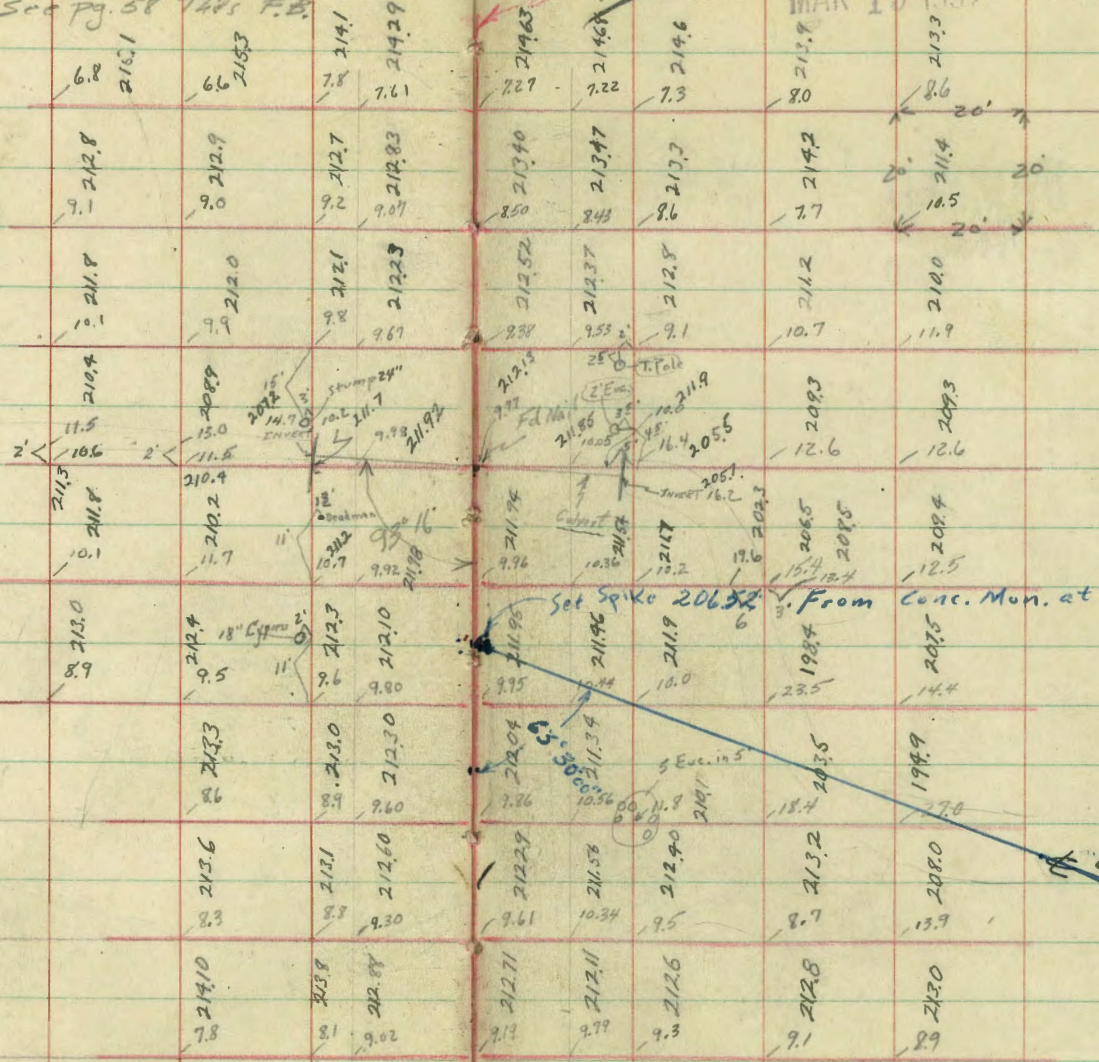


Robert's
 Mosse
 Pullen
 3-14-51
 W.O. 20658

Topog of Area Around Culvert
 In Talbot 234 West of Albion
 See pg. 58 this F.B.

MAR 15 1951

{ Red Limespid
 20' Squares }



check to Start B.M.	0.24	233.98			
T.P.	12.62	234.22	0.30	221.60	
T.P.	0.66	221.90	13.02	221.24	#54624 Nail W.W. Polo Canyon Talbot
B.M.	0.28	234.26		233.98	Sight on Conc. Mon. Albion &

Survey for Boundary of Police
Pistol Range - See Hard Copy for
Topo.

#4693

INDEXED

10-31-50

W.O. 20006

NOV 1 1950

Osborne
Hardin
Hatch
Rimmer

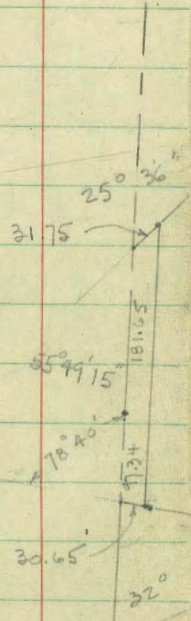
See B. 1435 - P. 5

T.P. 19

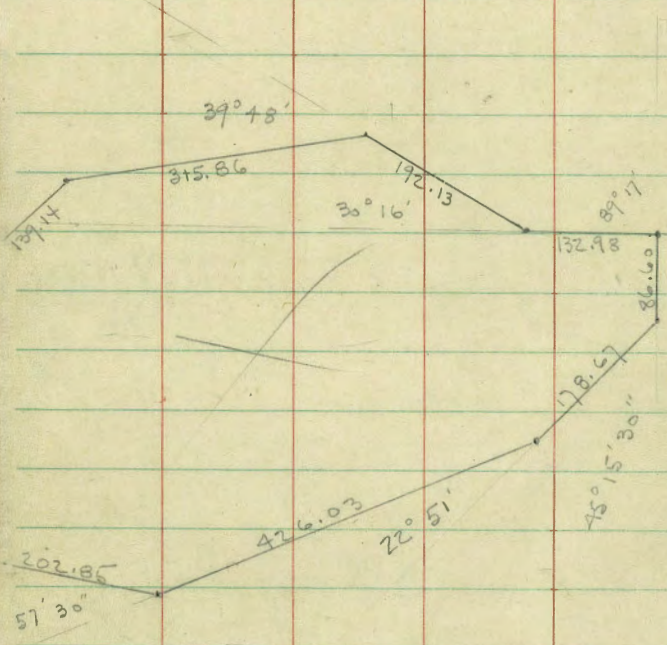
1453 - 79

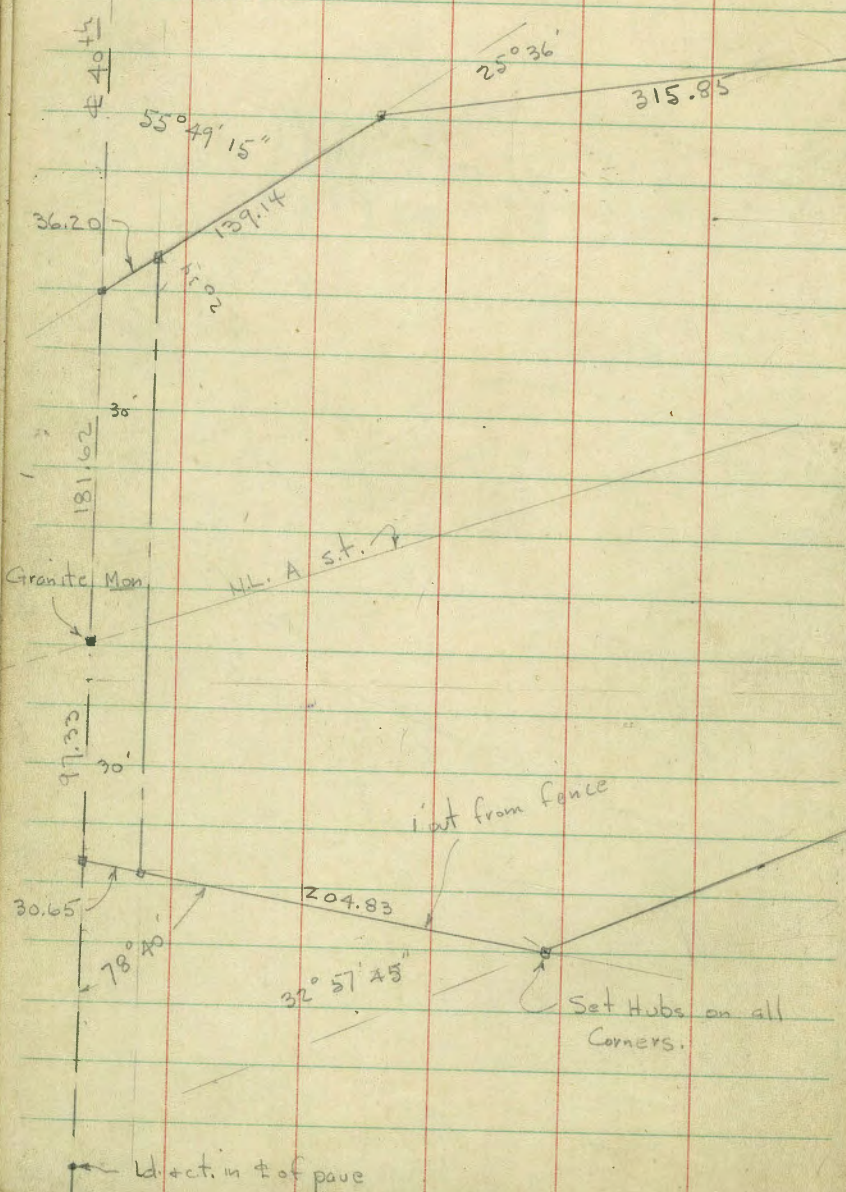
1448 - 73

Map # 517 - Marlow Park



N. G. Sec P. 61-63

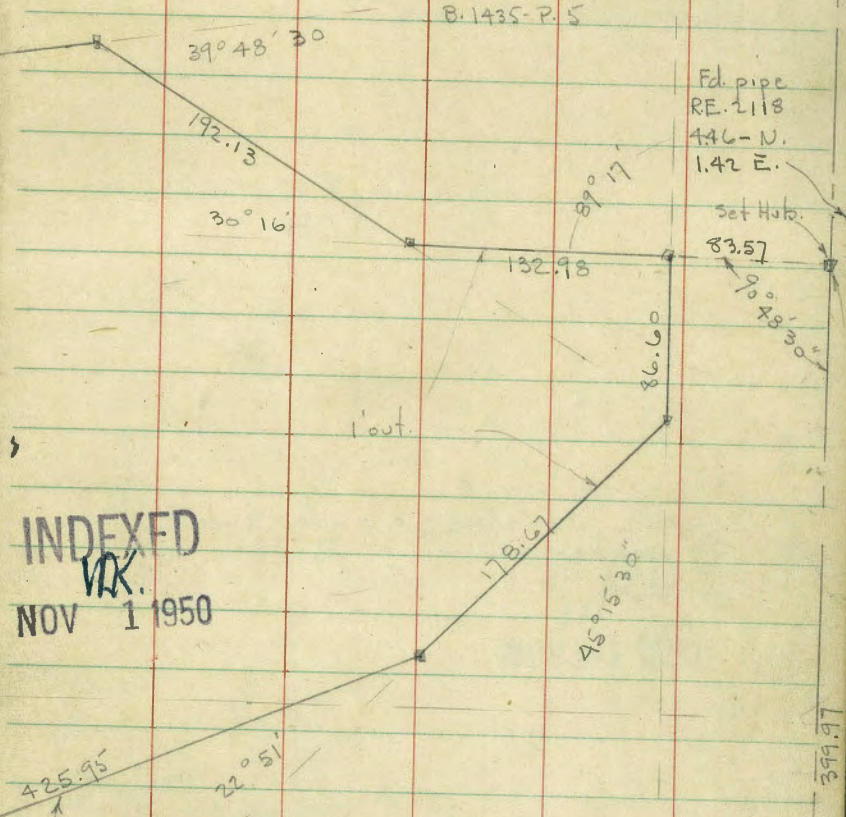




INDEXED
 V.R.
 NOV 1 1950

This line 2' out from High wire fence
 all others are 1' out.

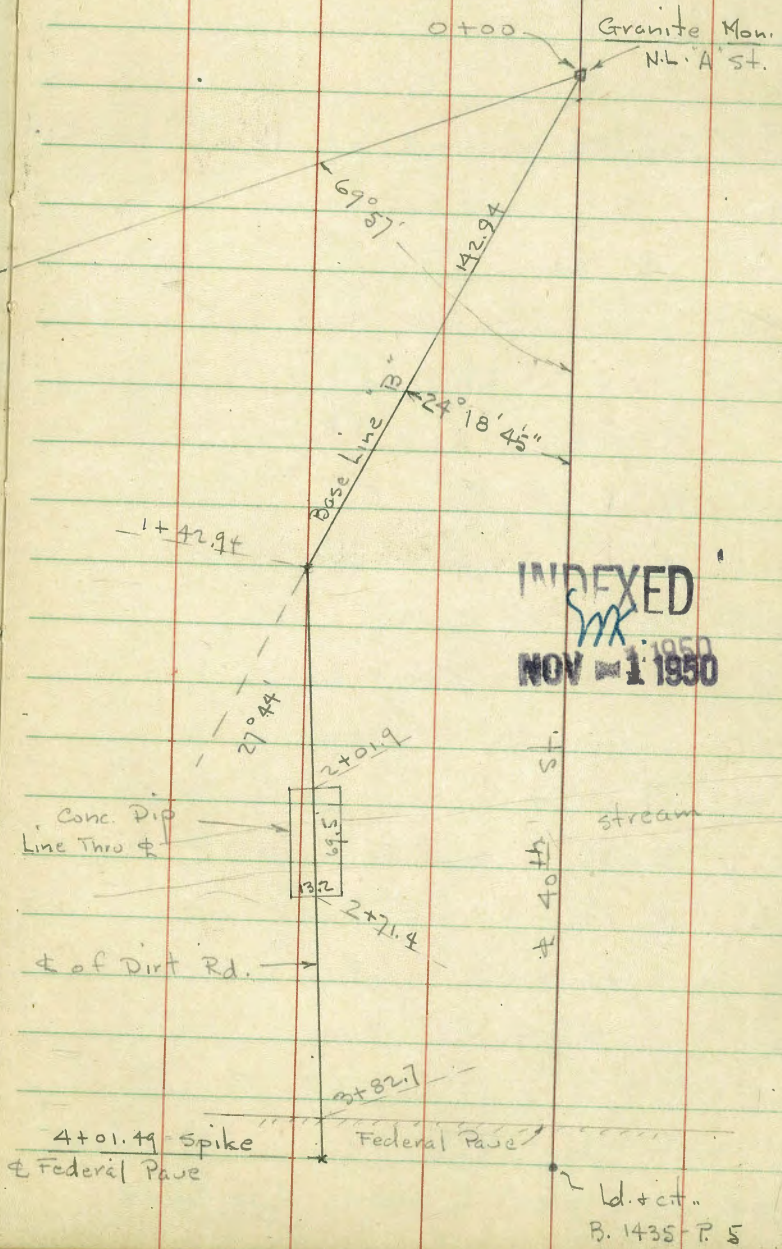
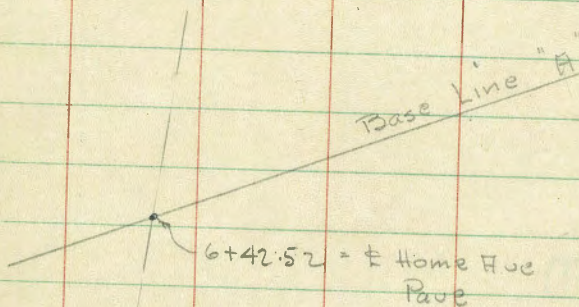
61
 Line to nail-15 w. of old
 Hub. on N.L. Beech st.
 B. 1435-P. 5



See B. 1435-P. 5 (on N. edge
 of Fed. Blvd.)
 Moni

Base Lines to show loc. of
Exist. Dirt. Access Roads.

See P. 63 for offsets
To Rd.



ld. + c.t.
B. 1435 - P. 5

Offsets to Existing Dirt Road from
Base Line "H"

0+00 = Granite Mon. = \pm Rd. thru Gate

+45 - 11' Rt. = \pm 36" Euc.

1+00 = \pm Rd.

+48 - 16' Lt. = \pm 60" Euc.

+50 - 2' + 21' Rt. = Rd.

2 ~ 10' + 29' Rt. = Rd.

+12 - 4' Lt. = \pm 50" Euc.

+18 - 4' Lt. = \pm 40" Euc.

+95 - 10' Lt. = \pm 40" Euc.

3 - 5' + 24' Rt. = Rd.

+58 - 7' Lt. = \pm 24" Euc.

4 ~ 9' Lt. + 9' Rt. = Rd.

+62 - \pm 30" Iron Pipe Culvert.

+68 - 8' Rt. = \pm 40" Euc.

5 ~ \pm + 15' Lt. = Rd.

5 ~ - 11' Lt. = \pm 30" Euc.

6 ~ 17' Rt. + 17' Lt. = Rd.

6+23.5 = Edge Pavc

6+42.52 = spike = \pm Home Hue Pavc

Add. Elev. + Topo. Poe + Alley - Blk. 16

5129

1-27-51

7.0.

W.O. 20553

0+30 - Top cb. = 71.33

0+30 - Top water pipe = 69.05

0+02 - 2' Rt. - E.C. - Top cb. = 71.78

0+00 - 2' Rt. - P.C. - Top cb. = 71.80

Top 4" water = 69.56 - at 0+00

I.E. of Box = 67.68

Top Grate - 2.5' out from cb. - \pm = 71.25

Used cb. line as base

INDEXED
JAN 29 1951

0+30

17.5 - 13' Rt. = \pm
+10.6 - 15' Rt. = \pm
+7.3 - 15' Rt. = \pm
+0.5 - 15' Rt. = \pm

0+00

\pm 2' x 2' Box - 1.5' Lt.
2.5' x 2' Grate

2' Rt. = \pm
2.5'

Poe St

4" C.I. water main

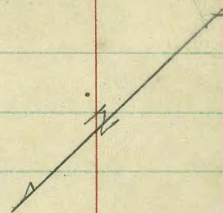
24" R.C. pipe

2.5

5

2.5

64



Deadman
10" Palm
Guy Pole
W.M.

72.01 = Top cb.

2' cb. Rad

Alley - Blk. 16

P. pole # P 3675

71.43

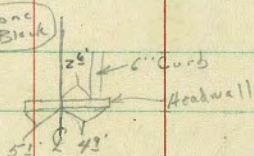
1.5'

19+00

18+82.2 12' Lt to Hibiscus

18+82 6' Lt to Ret wall (Conc Block)

18+80 10" Conc. Headwall



18+73.75 5' Rt to 75' Conc. Drive E. Curb Line

18+58.86 E Morningside

18+33.86 W.L. Morningside

17+75.22 61' Lt to End 30" Conc. Pipe

BM 7.88 187.66X

179.78 SNBP Midwick & Morningside See FB 2092 page 72

6.0 181.86

66.8 180.98
Top Headwall

179.74 180.35
7.92 731
9.4 cb

179.60
8.06

179.21
8.45

179.01
11.65
61.4
INVERT

187.66X ✓

T.P. 1134 196.87 \times 2.13 185.53

20+09⁴ 1/2¹ to shed 6² \times 6⁵
Wooden Picket Chicken Pen (Lean to)

20+02 5' Rt center 5" Tree

20+00

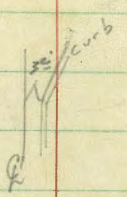
184.8
2.9

19+90 1/2¹ South 3 board 3' Fence

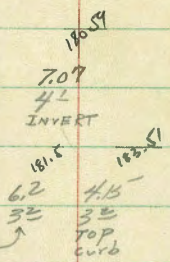
19+50 6⁹ Rt center 4" Tobacco Tree

19+49² 4¹ Rt END 15" conc. pipe & begin a
Jerry built wooden top of 12² \times 12² ~~curb~~

19+39² 3² Rt to L in 6" Curb



This is top of Conc. Pipe Footing
of Curb is Lower Than Ret. Wall
before Culvert was extended.



19+28¹ 6² 3¹ 4' Conc. Block wall (Leaning badly)



187.66 \times

183.1 182.4
4.6 5.3
Grd. Foot
187.66 \times

Contd From Page 67

T.P. 10.61 206.18T 1.30 196.57

21+74.19 Edge Conc. Strip

21+59.95 W. Curb Face Rec Drive

21+50

20+80

20+44

20+32

20+15.70 { 17' R+ to Wooden Culvert
12' Lt to Shed
7' Lt to Conc. BR Wall

196.87X

Lt

Q

R 68

176 195.11

195.24 144.73
1.63 2.14
Cb 60t

193.55 194.45 195.14
3.32 2.56 11.23
Grote Cb INVERT

2.1 194.8

3.3 193.6

7.6 189.3

9.7 197.2

16.2 185.7 191.8
15.1
172
Dirt INVERT

196.87X ✓

Cont'd From Page 68

2752.5

14' Rt to Conc. Curbing

Lt

E

Rt 69

0+50

"A" Line

7.9 201.3

23+58.38

0+00 = "A" Line

L. Rt

6.4 199.8

23+10

L. Lt

8.4 197.8

22+50

9.9 196.3

22+20

10.5 194.68

22+19

105' Rt to Ob. 55' Lt to Ob.

E. Curb Line Peo Dr.

11.11 195.07
Get Curb
Gene

22+03.95

Edge Conc. Strip

10.86 195.30

206.87

206.187 ✓

Cont'd From Page 69

16

±

70

2+65

3.4 ^{205.3}

2+25

L. Lt

3.1 ^{205.6}

2+00

3.0 ^{207.68}

T.P.

6.39

211.687

0.89

205.29

211.687 ✓

1+48

0.9 ^{205.3}

1+20

3.8 ^{204.4}

1+13

14' Rt End Curbing begin Conc. Block Wall

1+07.3

53' Rt to Center P. Pole # JP 88592

1+00

"A" Line

206.187

3.9 ^{202.9}

206.187 ✓

Cont'd From Page 70

24+40

24+20

24+08 9³' Rt Begin Board Fence

24+00'

23+67

23+65 12' Rt to Center P Pole # JP88591

T.P. 9.50 211.12~~X~~ 10.06 201.62

3+04.08 Cb. Face Center Inlet (Albemarle) END "A" Line

211.68~~X~~

70

71

72

71

13.3 197.8

10.6 200.5

13.6 197.5

10.8 200.3

13.6 197.5

11.4 199.7

13.7 197.7

13.2 197.7

211.12~~X~~ ✓

208.33 227.29 244.94
3.35 4.59 6.74
Cb. Gate INVERT

211.68~~X~~ ✓

Cont'd From Page 71

25+31.43 L. Rt. = 6700" B Line

25+22.40 E Rancho

25+07.40 W. Curb Line

24+97.50 W. L. Rancho Drive

24+79.52 43' Lt to END 24" Corr. Pipe

24+71

14' Rt to NW Cor. House
24+57.5 112' Rt END FENCE

211.12 π

Lt.

E

Rt.

72

5.11 206.01

5.00 206.14

206.14
2/98 5.57 206.56
Cb Gut

206.3
4/8

198.69
12.23
432
INVERT

12.7 198.4

211.12 π 1

Cont'd from Page 72

72 73

T.P. 7.71 216.95 ~~1.88~~ 209.24

1+80 136' Rt to N.W. Cor House

1+50 438' Lt to SW Cor House

1+482 59' Rt to T' Conc Drive

14472 4' Lt to Fence Corner

1+38.52 { 25' Rt to Drive Way Opening
E. Curb Line Rancho

1+32.16 "B" Line L. Rt

1+00 "B" Line

0+50 "B" Line

211.12 ~~1.88~~

228.3
C.P.

227.71
3.41 2.79
G.P. C.B.

227.97
3.15

226.67
1.45

226.16
4.96
211.12 ~~1.88~~ ✓

2+8802

82' East to an E/S Fence
1. Lt 90°

2+658

51' Rt to NE Cor Garage

2+454

63' Rt to Conc Drive
4.6 Rt to VW Cor Garage

2+27

64' Rt to Conc Drive

2+1719

13' Lt to 18" Conc pipe (Rt 45)

2+085

4' Lt to Fence Cor

2+036

14' Rt NE Cor House

2+025

42' Lt SE Cor. House

2+00

216.25 A

Lt

E

Rt

77

212.0
4.9

211.2	206.2	208.6	211.4	211.4	211.97
5.8	10.7	8.3	5.6	5.5	4.9
60	30	10	3		63
					CONC

206.8	205.99	210.0	210.6
10.1	11.86	6.9	6.4
19	13		
	INVERT		

213.4	209.4	209.8	210.4
3.6	7.6	7.2	6.6
31	19	7	

210.0
6.9

216.25 A

3+70

2.4 214.6

3+66.5

115' Rt END wall

3+61.7

10 Lt to END ^{29"} CORR. PIPE

266.84
10.11
10
INVERT 5.0 212.0

3+42

5.1 211.8

3+22.4

94' Rt to END FENCE BEYOND CONC. ^{LOW} BLK WALL

7.6 209.4

3+16

6.5 210.4

3+02

5.2 211.8

2+98

216.95A

216.95A ✓

28+12.01 E. Curb Line Rancho Dr.

204.81
7.85 7.83
Curb Cb.

Curb Inlet 29.85' From L. W. Curb Line Rancho Dr.

204.93 203.94 200.84
7.73 8.72 10.32
Curb Grate Invert

T.P. 7.84 212.66T 5.71 204.82

212.66T /

28+05.63 L Lt

204.82
5.71

27+00

205.54
4.99

26+00

205.95
4.58

T.P. 3.22 210.53T 9.64 207.31

210.53T /

3+18.92 Curb Face Center Inlet (Albemarle)
END "B" Line
216.95T

214.49 213.47 207.87
2.46 3.48 9.58
Curb Grate Invert
216.95T /

28492 3' Lt to Center P. Pole # 88476

28490

209.0
3.7

28475 4' Lt to Dead man

28472 22.5' Rt to NE Cor. House

28460

207.3
5.4

28458.5 14.5' Lt to SE Cor. House

28450 29.1' Rt to NW Cor. House

28437 14.5' Lt to SW Cor. House

28423.3 4.2' Lt to 8" Conc. Ret. Wall

208.51	207.6	206.3	205.8
4.5'	5.1'	6.4'	6.9'
Top	GrD		10

28413

205.7
7.0

212.66 T

212.66 T ✓

check

2.27 210.39 = 210.41

SWBP Cumberland $\frac{1}{2}$ Rancho Dr

29+20

50' Lt END conc. Ret. Wall $\frac{1}{2}$ Fence

28497⁴² = Sta. 3+57 See Page 1

212.66X

208.7
7.0

212.66X ✓

Notes Reduced. 5-25-51
R

TIES ~ "A" - ST.

Bot 39th & 40th ~ MARILYN PARK

Mulser

Pope

010V1

11-24-53

▲ = Fd. Granite Mass

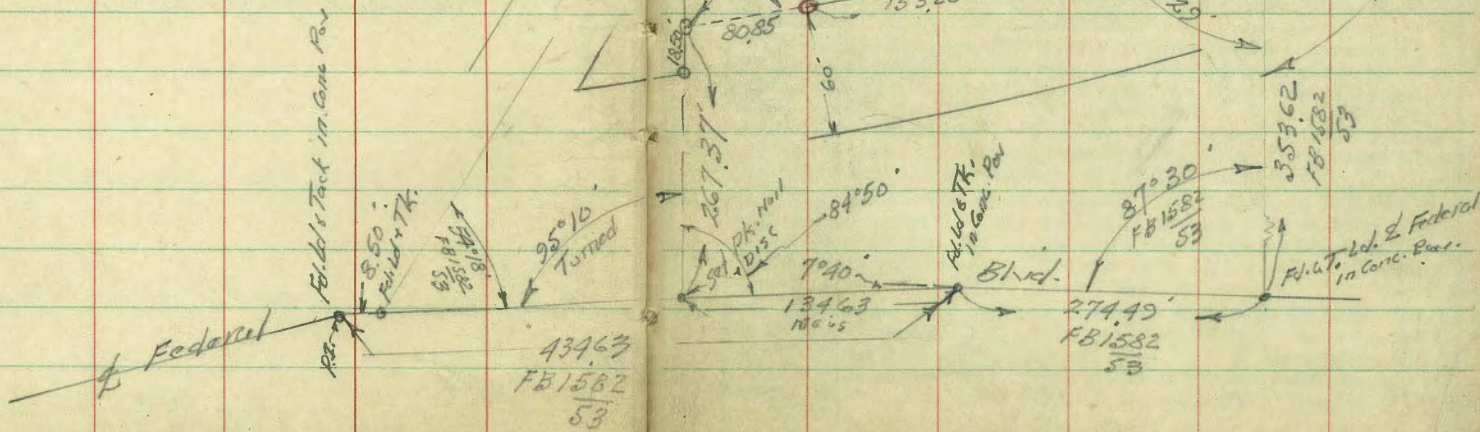
○ = Set 1" x 24" Galv. Iron Pipe with Cement & Disc.

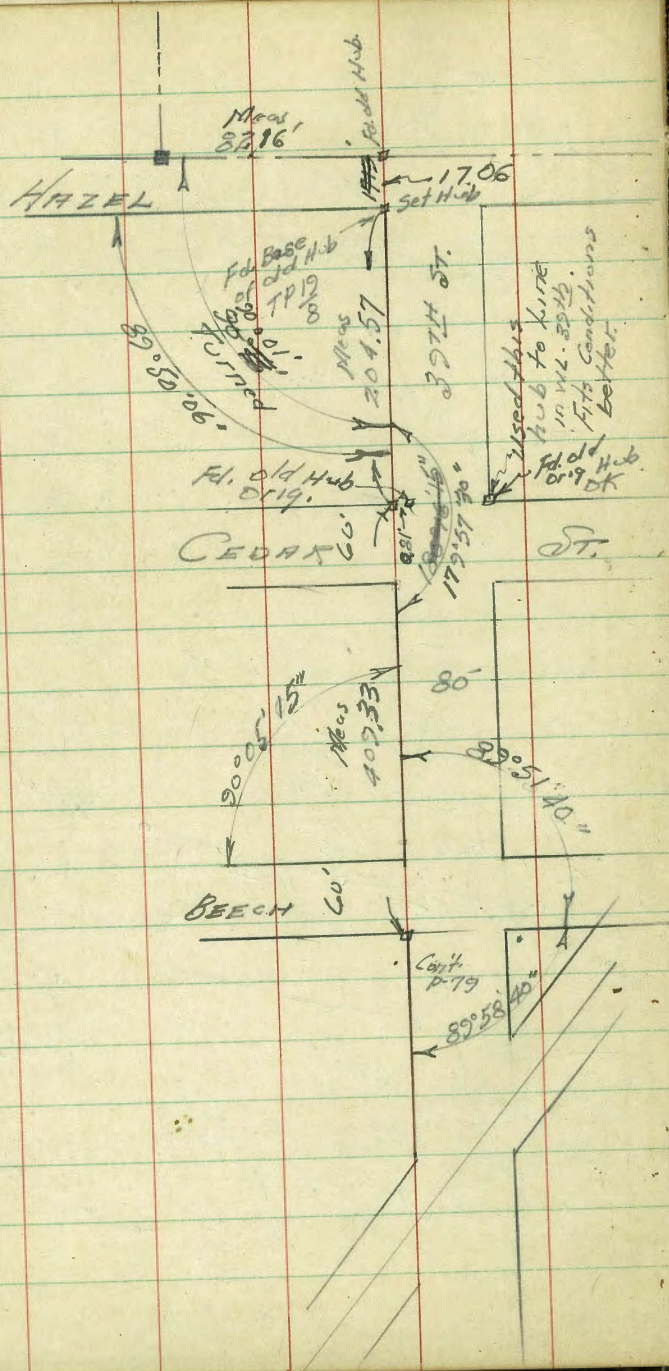
110 20006

Fd. 2" x 2" Hub
LS 2201

INDEXED
FFB 25 1954

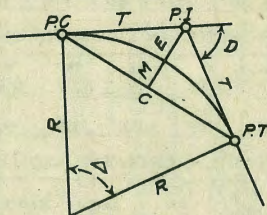
Fd. 1" Pipe
LS 2261
Replaced 9/15/55
C.A.





DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R \left(1 - \cos \frac{\Delta}{2}\right) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R + \cos \frac{\Delta}{2} - R \quad (8) = R \text{exsec} \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=62^{\circ} 10'$ $D=8^{\circ} 20'$. From Table IV for 1° curve $T=3454.1$ and $+8\frac{1}{3}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.—Sta. P.I.— $T=157+45.50$. Also from (4) $L=746.00$ and P. T.—Sta. P. C.+ $L=164+91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance= 158 —Sta. P. C.=54.50, hence offset= $7.27 (54.50 \div 100)^2=2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)=2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.—(in minutes) $.3 \times C \times D^{\circ}$ or =defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve= $.3 \times 54.5 \times 8\frac{1}{3}=136.2'$ or $2^{\circ} 16.2'$, or= $2.50 \times 54.5=136.2'$ from Table III. For Sta. 159 deflection angle= $2^{\circ} 16.2' + 8^{\circ} 20' \div 2=6^{\circ} 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E=960.6$ for $8^{\circ} 20'=960.6 \div 8\frac{1}{3}=115.27$ and from Table V correction=.10 or $E=115.37$ ft. Or suppose $\Delta=32^{\circ}$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $\div 42=5.5$ or $D=5^{\circ} 30'$.

3+796
2883
913

4+58.15

3+796

7845

to
of
ple
.9.
A.

210.41
 10.49
 220.90
 3.84
 217.06
 7.79

9.9

224.85
 11.87

212.98
 0.20

213.18
 11.90

201.28
 3.70

205.03
 9.71

195.32
 4.12

199.44

213.66
 6.69
 206.97

215.46
 5.18

220.61
 11.15

209.46
 6.13

214.59
 7.74

206.85
 1.02

207.87
 12.89

194.98
 4.62

199.60

57.86
 17.73
 75.59

7730.16
 13

729.88

7330.18
 3

2798

213.66
 6.53
 207.13

DISTANCES FROM CENTER OF ROADWAY FOR
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) + 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.