

NAME EUCLID AVE ROAD

Class \_\_\_\_\_ Course Book #2 Party \_\_\_\_\_

# 51

1882

B. 51 S.  
X-SECS-

# FIELD NOTES

**EUGENE DIETZGEN Co.**  
MANUFACTURERS

DRAWING MATERIALS  
MATHEMATICAL AND SURVEYING INSTRUMENTS  
MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK  
NEW ORLEANS PITTSBURGH



Property of  
Watson Valle & Gough  
505 Spreckles Bldg.

MICROFILMED

DEC 30 1964

EUCALID AVE.

Book # 2

1+80

9+07?

- INDEX -

Euclid Ave BMS	2-3
" "	19-25
Cross Sections 0 to 45+59	A-18
Upper St. BMS	26-28
Check levels Upper to Euclid	29-30



Sta	+	-	Cal
B.M.	2.88	343.51	340.63
	2.76	343.63	340.87
	3.98	347.09	343.11
B.M.#1	1.67	341.71	346.54
			346.04
B.M.#4			331.14

Leveling Across Canyon

B.M.#2			331.14
	3.23	334.37	
T.P.	6.17	337.85	331.68
B.M.#3		6.70	331.15
			331.14

T.P.			331.68
	6.17	337.85	
B.M.#3		2.61	335.24
	6.53	341.77	

On Brass Plug N. End of ~~Plaza~~ N.W. Cor  
University & Euclid

City of San Diego DATUM.

2/6/26  
Coote  
Brewer

Top Conc. Post (SW. Cor.) So. End Conc. Wall - 30' Lt. of E  
(House # 3725 Euclid Ave.)

Nail in E. Side Power Pole # 4599 SDG & E Co.

- Discrepancy of 0.01 - No Correction -

From 4<sup>th</sup> line above -

NE Cor. Cement Step to house # 3544 Euclid Ave.  
Pt. of Sta 24



	+	H.	-	Σ
		341.77		
			11.86	329.91
	0.12	330.03		
			11.87	318.21
	0.42	318.63		
			11.18	307.15
	0.37	307.47		
Bu#4			10.12	297.35
	1.87	299.22		
T.P.			11.95	287.27
	0.75	288.02		
			11.59	276.43
	2.84	279.27		
			11.14	268.13
	2.14	270.29		
			9.32	260.95
	1.85	262.80		
Bu#5			7.02	255.78

Cont'd on Pg. 19

3

On N.W. Cor Cement Mark to house #323 Center St.  
 15' Rt. 35+85  
 Nail in Post (near top) Rt. Sta 37

Hub 22' Rt. 45+59.47 - On point of hill -



X- Sections -  
+ HI - EI

Bm 340.63

3.63 344.96

0+00

0-100

0-200

0+40

1+00

+50

+76

+80

Euclid Ave -

4

From Pgs Lt. Rt.

X Unit -  
(Pave)

$\frac{2.15}{100}$

$\frac{3.10}{30}$

$\frac{3.63}{30}$

$\frac{3.70}{30}$

$\frac{4.17}{100}$

$\frac{39.68}{100}$

$\frac{1.44}{100}$

$\frac{41.31}{30}$

$\frac{35.46}{30}$

$\frac{46.44}{30}$

$\frac{46.08}{30}$

$\frac{49.39}{30}$

$\frac{41.16}{30}$

$\frac{46.14}{30}$

$\frac{41.31}{30}$

$\frac{35.46}{30}$

$\frac{46.44}{30}$

$\frac{46.08}{30}$

$\frac{49.39}{30}$

$\frac{41.16}{30}$

$\frac{46.14}{30}$

$\frac{5.20}{30}$

$\frac{5.30}{30}$

$\frac{6.39}{30}$

$\frac{6.38}{30}$

$\frac{6.38}{30}$

$\frac{6.38}{30}$

$\frac{6.38}{30}$

End of curb 18' Lt.

$\frac{6.6}{18}$

Drop  
Inlets

$\frac{12.29}{10}$   
Flow Line

$\frac{79.0}{15}$   
Top

$\frac{8.10}{15}$   
Top

$\frac{10.85}{16}$   
Flow

2/8/26

Route  
Brower

Loccy

$\frac{46.14}{30}$

$\frac{4.11}{25.5}$   
walk

$\frac{46.14}{30}$

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$\frac{46.14}{30}$



2+00

+50

3

+50

A

+50

+

H1  
344.26

-

E1

5.61 338.65

6.27 344.94

Marchel  
3+9.6  
5.46  
Mr. Street  
Marchel

2/10 43.6

2/19 40.2

2/27 39.8

3/5 39.2

3/12 39.7

3/20 39.2

3/28 39.7

4/5 40.5

4/12 44.3

3/10 39.9

3/18 39.1

3/26 38.5

4/3 36.3

4/11 39.0

4/19 38.2

4/27 38.8

5/5 39.3

5/13 39.8

5/21 42.0

4/29 31.3

5/7 36.6

5/15 37.3

5/23 36.5

5/31 37.6

6/8 36.0

6/16 37.8

6/24 36.9

7/2 37.7

7/10 37.6

7/18 37.4

7/26 35.4

L1

R1

E1

In cr. A bury (Ard)



5+50

344.9v

6

+50

+80

7

5.00 339.9v

+50

4.10 344.0v

+90

Wanted  
7+87

4.00  
24.57

8

Lt.

48.5	48.8	48.2
14/21	14/21	14/21
39/29	40.9	40.6
40.4	40.4	40.0
39.9	39.6	39.4
40.0	40.0	39.9

Rt.

6

40.3	40.1	40.1
41/21	40.1	40.1
40.5	40.5	40.6
41.5	41.5	41.5

Approx ± Klauber St.

43.0	40.8	40.2
10/20	11/20	10/20
39.9	39.9	39.7
40.0	40.0	39.9

Wanted 90

40.4	40.4	40.1
33/20	41/20	41/20
39.9	39.9	39.9
40.1	40.1	40.1

St.

41.1	41.1	40.5
21/10	21/10	21/10
39.8	39.8	39.1
39.9	39.9	39.9

Approx ± So. Above Dr.

39.6	39.5	39.5
44/21	44/21	44/21



8+50

9

+07

+50

10

+80

11

344.07

9.45

349.89

3.56

340.41

Manhole  
10248

346.3  
9.31  
41.51 ±

2+

R+

7

33.15  
10.97  
22.18

8/10 39.4  
1/9 39.2

8/10 39.3  
1/9 38.9

8/10 38.7  
1/9 39.1

12/10 38.2  
1/9 38.9

AC 39.4

15 39.5

4.7 39.3

18 39.1

1/3 38.7

1/3 38.7

1/2 39.4

2/10 38.7

4/10 39.5

2/10 38.8

2/8 40.1

10/2 39.8

1/1 39.1

1/8 39.6

1/3 39.7

1/1 39.4

1/5 38.9

1/4 39.6

8/10 39.8

1/10 43.3

1/10 41.9

1/10 40.7

1/10 42.6

1/10 41.0

9/10 40.6

1/10 41.1

1/10 41.7

2/8 40.1

10/2 39.8

1/1 39.1

1/8 39.6

1/3 39.7

1/1 39.4

1/5 38.9

1/4 39.6

8/10 39.8

2/8 38.7

6/5 38.9

2/10 38.4

1/8 39.0

AC 39.4

5/10 38.7

2/10 38.9

2/10 39.3

10.97

10.97

Drop Inlets

5.73

9.99

8/10 39.4

1/9 39.2

8/10 38.7

1/9 39.1

AC 39.4

4.7 39.3

1/3 38.7

1/2 39.4

4/10 39.5

Approx \* Lantana Dr.



11+50

349.89

12

Blm# 1

3.30 349.84

+50

13

+13

+29

+50

44.80

43.2

44.8

43.6

44.8

44.9

44.1

44.3

44.6

44.7

44.1

44.3

41.3

41.0

41.1

41.6

42.1

42.9

42.1

See Pg. 2

45.6

43.8

43.0

44.3

42.6

43.0

44.8

42.1

43.4

43.1

45.1

44.5

43.9

43.5

43.8

43.9

44.4

43.5

43.8

44.1

45.4

44.8

43.5

44.3

42.6

43.0

44.4

43.5

43.8

44.1

Approx # Castle St.

44.9

44.2

44.1

44.7

44.1

44.4

44.2

44.8

44.0

43.2

41.4

41.4

41.4

100

150

Graded St.

Lt.

Rt.

8



14

349.84

+24

+50

15

1.59

344.20

7.23 347.61

Manhole  
14+04.3

303.39  
0.61  
ch 57.3

+50

+83

16

+34

H

21/30	45.2	21/30	44.5
21/30	44.5	21/30	44.0
21/30	44.1	21/30	43.6
21/30	44.1	21/30	44.0
21/30	43.6	21/30	43.5
21/30	43.5	21/30	43.5
21/30	43.2	21/30	43.2

Approx H

In Phone Pole

21/30	41.9	21/30	41.5
21/30	41.7	21/30	41.4
21/30	41.1	21/30	41.7
21/30	41.5	21/30	41.8
21/30	41.9	21/30	42.0
21/30	41.1	21/30	41.1
21/30	41.1	21/30	41.1

On Com-Walk to house

21/30	41.4	21/30	41.8
21/30	41.0	21/30	42.0
21/30	40.4	21/30	40.8
21/30	40.9	21/30	40.8
21/30	40.8	21/30	40.8
21/30	40.6	21/30	40.6

On Com-WK

4.18  
30

R

1

9



16+50

344.20

+69

17

+10

+50

+56

18

5.78

338.47

1.71

340.13

+47

Lt.

$\frac{46}{30} 40.4$

$\frac{47}{15} 40.0$

$\frac{44}{11} 39.8$

$\frac{46}{23} 40.0$

$\frac{46}{24} 39.6$

Pt.

$\frac{44}{28} 39.5$

$\frac{46}{30} 39.6$

On Cem. Walk

$\frac{46}{30} 39.6$

$\frac{49}{16} 39.8$

$\frac{48}{12} 38.8$

$\frac{46}{17} 39.6$

$\frac{45}{20} 38.7$

$\frac{44}{24} 38.8$

On Cem. Wk.

$\frac{47}{19} 39.1$

$\frac{47}{17} 38.9$

$\frac{46}{18} 38.2$

$\frac{47}{17} 39.0$

$\frac{46}{21} 38.0$

$\frac{46}{20} 38.8$

$\frac{46}{20} 38.8$

Walk

On Cem. Wk. to House

$\frac{48}{24} 38.8$

$\frac{48}{24} 38.3$

$\frac{46}{24} 37.9$

$\frac{47}{24} 38.5$

$\frac{47}{20} 38.5$

$\frac{46}{21} 37.9$

Walk to house

Approx. Roselawn Ave

$\frac{3.18}{23} 36.9$   
To Roselawn Ave

$\frac{44}{30} 38.7$

$\frac{44}{30} 38.7$

$\frac{49}{100} 38.7$



18+50

349.13

19

+50  
364.7

4.74 335.88

20

8.95 331.18 331.14

+50

21

0.06 324.14

11.80 324.08

10.93 313.71

+50

0.67 313.83

171

See Pg. 2

$\frac{+12}{58} 290$

$\frac{+56}{28} 174$

$\frac{+11}{13} 147$

$\frac{+2}{14} 116$

$\frac{+37}{101} 101$

$\frac{+106.3}{13} 106.3$

$\frac{+99.9}{25} 99.9$

$\frac{+110}{31} 110$

$\frac{+19}{27} 157$

$\frac{+157}{138} 138$

$\frac{+157}{14} 116$

$\frac{+137}{101} 101$

$\frac{+106.3}{13} 106.3$

$\frac{+99.9}{25} 99.9$

$\frac{+110}{31} 110$

$\frac{+19}{27} 157$

$\frac{+157}{138} 138$

$\frac{+157}{14} 116$

$\frac{+137}{101} 101$

$\frac{+106.3}{13} 106.3$

$\frac{+99.9}{25} 99.9$

$\frac{+110}{31} 110$

198 94.0  
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x Draw

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100

Top A" Gate Valve  
(Water Line)

11



21+98 0.54 307.54 11.83 307.00

22

+50

+63

+80

23

+50

Bu+3

12.10 314.44

11.84 325.96

11.40 336.98

0.20 307.34

0.30 314.14

0.41 325.18

1.64 335.44 335.24

Lt.

Rt.

17

12.0  
51

1.0  
50

1.0  
50

1.0  
50

1.0  
50

1.0  
50

1.0  
50

Spine Slope  
Down

22.1  
54

16.4  
38

9.5  
18

2.9  
19

1.4  
19

1.9  
33

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Spine Slope  
Down



23+69

336.88

24

1.13

335.75

+50

4.64

340.39

25

+50

26

+50

27

Lt.

3/13 24.1 3/14 25.6 3/15 26.7 3/16 27.1 3/17 27.4 3/18 27.9 3/19 28.6 3/20 29.1 3/21 29.7 3/22 30.3 3/23 31.0 3/24 31.6 3/25 32.1 3/26 32.7 3/27 33.4 3/28 34.1 3/29 34.9 3/30 35.7

1/18 33.6 1/19 35.5 1/20 36.7 1/21 37.4 1/22 38.0 1/23 38.6 1/24 39.1 1/25 39.7 1/26 40.3 1/27 41.0 1/28 41.6 1/29 42.1 1/30 42.7

1/2 33.4 1/3 35.5 1/4 36.6 1/5 37.4 1/6 38.0 1/7 38.6 1/8 39.1 1/9 39.7 1/10 40.3 1/11 41.0 1/12 41.6 1/13 42.1 1/14 42.7

1/15 33.0 1/16 35.6 1/17 36.3 1/18 37.1 1/19 38.0 1/20 38.6 1/21 39.1 1/22 39.7 1/23 40.3 1/24 41.0 1/25 41.6 1/26 42.1 1/27 42.7

1/28 32.4 1/29 34.4 1/30 35.8 1/31 37.1 1/32 38.0 1/33 38.6 1/34 39.1 1/35 39.7 1/36 40.3 1/37 41.0 1/38 41.6 1/39 42.1 1/40 42.7

Rt.

13



27+50

340.31

9  
9.51

330.88

28

0.10

330.98

+50

29

+50

30

0.00

319.13

11.85

319.13

+50

31

H

$\frac{15.2}{20} = 0.76$	$\frac{18.1}{20} = 0.905$	$\frac{20.8}{20} = 1.04$	$\frac{23.2}{20} = 1.16$	$\frac{25.7}{20} = 1.285$	$\frac{28.1}{20} = 1.405$	$\frac{30.3}{20} = 1.515$	$\frac{32.4}{20} = 1.62$
$\frac{13.4}{20} = 0.67$	$\frac{17.2}{20} = 0.86$	$\frac{20.6}{20} = 1.03$	$\frac{22.5}{20} = 1.125$	$\frac{25.0}{20} = 1.25$	$\frac{27.5}{20} = 1.375$	$\frac{29.8}{20} = 1.49$	$\frac{31.8}{20} = 1.59$
$\frac{12.7}{20} = 0.635$	$\frac{16.5}{20} = 0.825$	$\frac{19.7}{20} = 0.985$	$\frac{22.1}{20} = 1.105$	$\frac{24.4}{20} = 1.22$	$\frac{27.0}{20} = 1.35$	$\frac{29.3}{20} = 1.465$	$\frac{31.2}{20} = 1.56$
$\frac{11.4}{20} = 0.57$	$\frac{16.6}{20} = 0.83$	$\frac{20.0}{20} = 1.0$	$\frac{22.6}{20} = 1.13$	$\frac{24.9}{20} = 1.245$	$\frac{26.9}{20} = 1.345$	$\frac{29.4}{20} = 1.47$	$\frac{31.1}{20} = 1.555$
$\frac{10.2}{20} = 0.51$	$\frac{16.0}{20} = 0.8$	$\frac{18.1}{20} = 0.905$	$\frac{21.5}{20} = 1.075$	$\frac{23.3}{20} = 1.165$	$\frac{26.3}{20} = 1.315$	$\frac{28.4}{20} = 1.42$	$\frac{30.6}{20} = 1.53$
$\frac{8.8}{20} = 0.44$	$\frac{15.6}{20} = 0.78$	$\frac{14.5}{20} = 0.725$	$\frac{21.6}{20} = 1.08$	$\frac{22.1}{20} = 1.105$	$\frac{26.0}{20} = 1.3$	$\frac{28.2}{20} = 1.41$	$\frac{29.2}{20} = 1.46$
$\frac{10.2}{20} = 0.51$	$\frac{10.7}{20} = 0.535$	$\frac{10.8}{20} = 0.54$	$\frac{10.7}{20} = 0.535$	$\frac{10.7}{20} = 0.535$	$\frac{10.7}{20} = 0.535$	$\frac{10.7}{20} = 0.535$	$\frac{10.7}{20} = 0.535$

14



31+50

319.13

0.23

307.80

11.52

307.57

32

+50

33

+50

7.36

303.44

11.72

296.08

34  
34

6.09

297.35

297.35

+50

35

1.65 299.59

5.50

297.94

Lt.

8.60

28.10.5

28.05.0

28.05.0

28.05.0

28.05.0

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17.1

17.1

See Pg. 3

6.09  
30  
Rem. Mark.



35+50

299.59

36

Contours-

+50

37

11.74 287.85

+50

0.74 285.59

38

11.36 277.43

+50

3.09 280.32

39

11.79 268.53

0.95 269.48

2+

$\frac{13.7}{30}$

$\frac{+21}{21}$

$\frac{+0.6}{30}$

$\frac{0.6}{30}$

$\frac{3.4}{30}$

$\frac{30.15}{30}$

$\frac{+21}{15}$

$\frac{+0.6}{15}$

$\frac{2.7}{6}$

$\frac{3.4}{30}$

$\frac{+1.2}{30}$

$\frac{0.3}{15}$

$\frac{1.8}{15}$

$\frac{2.7}{6}$

$\frac{1.3}{30}$

Contours-

Contours-

$\frac{300}{46}$

$\frac{295}{7}$

$\frac{6.4}{95.2}$

$\frac{290}{9}$

$\frac{285}{10}$

$\frac{295}{24}$

$\frac{290}{9}$

$\frac{10.8}{84.7}$

$\frac{285}{10}$

$\frac{280}{34}$

$\frac{295}{61}$

$\frac{290}{37}$

$\frac{285}{11}$

$\frac{10.8}{84.7}$

$\frac{280}{27}$

$\frac{275}{43}$

$\frac{290}{31}$

$\frac{285}{20}$

$\frac{12.4}{74.7}$

$\frac{280}{6}$

$\frac{275}{32}$

$\frac{270}{44}$

$\frac{285}{40}$

$\frac{280}{17}$

$\frac{275}{11}$

$\frac{12.4}{74.7}$

$\frac{270}{8}$

$\frac{265}{21}$

$\frac{260}{31}$

$\frac{255}{43}$

$\frac{280}{41}$

$\frac{275}{11}$

$\frac{11.8}{80}$

$\frac{270}{7}$

$\frac{265}{19}$

$\frac{260}{29}$

$\frac{255}{38}$



24.

Pt.

17

39+50

269.48

40

11.80 257.68

+50

1.43 259.11

11.99 247.12

41

0.76 247.38

12.01 235.37

+50

0.60 236.47

42

+50

43

$\frac{250}{72}$   $\frac{275}{43}$   $\frac{270}{23}$   $\frac{265}{8}$

$\frac{275}{57}$   $\frac{270}{27}$   $\frac{265}{7}$

$\frac{275}{76}$   $\frac{270}{52}$   $\frac{265}{37}$   $\frac{260}{27}$   $\frac{255}{13}$   $\frac{250}{3}$

$\frac{265}{54}$   $\frac{260}{43}$   $\frac{255}{30}$   $\frac{250}{27}$   $\frac{245}{15}$   $\frac{240}{4}$   
 $\frac{270}{70}$   $\frac{275}{94}$

$\frac{260}{54}$   $\frac{255}{45}$   $\frac{250}{29}$   $\frac{245}{19}$

$\frac{255}{84}$   $\frac{250}{74}$   $\frac{245}{67}$   $\frac{240}{57}$   $\frac{235}{40}$   $\frac{230}{24}$   $\frac{225}{8}$   
 $\frac{260}{94}$   $\frac{255}{107}$   $\frac{270}{137}$   $\frac{275}{163}$

$\frac{265}{85}$   $\frac{260}{76}$   $\frac{255}{65}$   $\frac{250}{55}$   $\frac{245}{45}$   $\frac{240}{32}$   $\frac{235}{11}$   
 $\frac{255}{102}$   $\frac{260}{126}$   $\frac{265}{151}$   
T. Ridge

6.6

6.6

10.1

8.39.4

6.38.4

13.4

15.19.4

17.6

18.9

$\frac{260}{7}$   $\frac{255}{15}$   $\frac{250}{27}$   $\frac{245}{20}$

$\frac{260}{5}$   $\frac{255}{14}$   $\frac{250}{27}$   $\frac{245}{11}$

$\frac{245}{10}$   $\frac{240}{22}$   $\frac{235}{39}$

$\frac{235}{14}$   $\frac{230}{25}$   $\frac{225}{44}$   $\frac{220}{53}$   $\frac{217}{58}$   
# row

$\frac{230}{4}$   $\frac{225}{35}$   $\frac{220}{62}$  then up  
wash

$\frac{220}{12}$   $\frac{215}{61}$  then up  
wash

$\frac{215}{45}$   $\frac{210}{37}$  then up  
wash



43+50

236.47

44

+34.80

On split of angle  
3.78 237.69

11.75 244.44

+50

0.63 243.81

11.40 255.21

45

$\frac{259}{16}$

$\frac{255}{18}$

$\frac{250}{19}$

8.7

$\frac{245}{6}$

$\frac{240}{11}$

+20

0.34 254.87

4.47 259.34

Bk#5

3.15 255.89 255.76

See Pg. 3

3.15 259.43

+50

+59.47

Continued In Bk#3, Pg. 1

Lt

Rt

18

15.9

9.6

33.3

33.2

36.2

36.5

36.7

36.8

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

36.9

$\frac{260}{144}$

$\frac{255}{52}$

36.9



BENCH LEVELS  
Cent'd from Pg. 3

Btu#5

1.91	257.69	11.49	246.20
0.20	246.40	11.88	234.50
0.13	234.65	12.06	222.59
0.57	223.16	11.66	211.50
0.48	211.98	11.20	200.78
5.97	206.75		

255.78

See Pg. 3 This book

2/10/26  
Route  
Brewer

Btu#6

11.91	216.03	2.63	204.12
11.12	225.49	1.66	214.37
11.72	236.83	0.38	225.11
11.61	246.41	2.03	234.80
11.90	256.98	1.33	245.08
8.28	264.95	0.31	256.67

On Hub 15 Rt 18+85



Btu#7	264.95	3.49	261.46
		11.90	253.05
0.43	253.48	11.45	247.03
0.06	247.09	11.96	230.13
0.24	230.57	12.07	218.50
0.07	218.57	12.03	206.54
1.88	208.47	11.74	196.68
1.01	197.69	9.37	188.37
Btu#8		7.51	184.09
3.23	191.60	0.04	187.45
3.40	187.49	5.57	193.37
		2.49	184.99
Btu#9		11.57	181.80
		1.91	187.38
		8.55	175.44
2.22	177.66	5.00	177.66
11.60	184.76		

On Hub 72 Rt 54+01.55 (Top of Ridge)

Spike in Root of Sycamore 18' Lt. 60+50  
(Near Cholla Creek)

Spike in Eucalyptus Tree 35' Rt. 72+93  
(So. Side of End Tree)



		184.76		
			10.65	173.61
36#10	10.95	184.56		
			2.36	182.20
	2.79	184.99		
			5.83	179.16
	11.45	190.61		
			0.41	190.20
	10.75	200.95		
			0.19	200.76
	11.75	212.51		
			0.13	212.38
	11.96	224.34		
			0.26	224.08
	12.04	236.12		
36#11			0.44	235.68
	11.54	247.44		
			2.00	245.44
	7.21	252.43		
36#12			1.73	250.70
	1.88	252.59		
			6.79	245.79
	0.66	246.45		
			3.02	243.43
	5.29	248.72		

Hub 10 Pt 87+05 ✓ (On Ridge)

Hub 17 Left 100+50 ✓ (Edge Mesa)

On 2x2 Hub ≠ P.O.T. 109+28.03 (Top Knoll)



	228.72		
Bm#13	0.40	228.32	
	11.86	236.86	
	0.20	237.06	
	11.76	225.30	
	0.46	225.76	
	11.74	214.02	
	0.25	214.27	
	8.47	205.80	
	8.49	214.29	
Bm#14	3.55	210.74	
	0.91	211.65	
	11.98	199.67	
	0.95	200.62	
	11.83	188.79	
	2.77	191.56	
Bm#15	7.62	183.94	
	0.72	184.66	
	12.09	172.57	
	0.47	173.04	
	12.01	161.03	
	1.33	162.36	
T.P	11.79	150.57	
	0.11	150.68	
	11.94	138.74	

Top of Steel Axle  $\pm$  Sta 119+22.98

Top 4x4 Stk.  $\pm$  Sta 132+19 "B" Line -

On Hub 30' Rt. 139+50 "A" Line

Hub 16' Rt. 145+50



	+	Hl	-	El
				138.74
	0.56	139.30		
			11.28	128.02
3 <sup>rd</sup> #16	0.71	128.73		
			6.02	122.71
			6.26	116.45
	3.59	125.86		
			8.38	117.48
	4.23	121.71		
			0.55	121.16
	11.43	132.59		
			0.18	132.41
	11.53	143.94		
			0.29	143.65
	8.10	151.75		
3 <sup>rd</sup> #17			4.21	147.54
	0.48	148.02		
			11.74	136.28
	0.80	137.08		
			11.86	125.22
	0.16	125.38		
			11.76	113.62
	0.21	113.83		

Lt.

Rt. 23

2/20/26

Cate  
Bower  
Locey

Notes  
K  
P

Nail in Cor. Fence Post Lt. Sta 149 ✓

Nail in Curb at beginning of Return  
Lt. 138+37 ✓



	1.	113.83	10.76	103.07
Sta #18	6.38	109.45	5.57	103.88
	4.18	108.06	0.16	107.90
	11.80	119.70	0.17	119.53
	11.82	131.35	0.14	131.21
Sta #19	9.67	140.88	10.32	130.56
			1.93	138.95
	4.39	143.34	0.28	143.06
Sta #20	9.16	152.22	1.85	150.37
			0.10	152.12
	12.05	164.07	0.06	164.01
	11.92	175.93	0.11	175.82
Sta #21	7.79	183.61	2.25	181.36

Nail in Post SW. Cor. Lowe Station S.D. & A.R.R. ✓

On Conc Monument # Sta 172+30 ✓

Nail in Tel. Pole 145' Lt 179+25

Nail in Tel. Pole No. Side Imperial Ave.  
10' Rt ± Survey (Back of Pole)



6.29 187.65

181.36 Bl#21

2.62 185.03 191.31

Q#Q. Bl#7 No. side Imperial Ave 22 ft  
Sta 69+06 County station-

6.29

Note:

Difference between city and  
County datum = City 0.00, County +6.12



# UPPER ST. B.M.S

191.31 EHC Bl#7, 2' Lt. 69+06 County —

2.58	193.89	10.04	183.85
0.52	194.37	11.21	173.16
0.29	173.45	10.95	164.50
1.25	163.75	9.07	154.68
1.08	155.76	6.54	149.22
2.51	151.73	10.50	141.23
0.19	141.42	10.94	130.48
0.65	131.13	10.21	120.92
1.83	122.75	3.91	118.94
		7.93	114.82
2.16	116.98		

Bl#5

On N.W. Cor. Conc Pump Base ✓ at Service Sta. NE Cor  
Imperial Ave & Upper St



	11698		
	0.20	105.47	11.71 105.27
	0.02	93.48	12.01 93.46
	0.81	84.70	11.59 81.89
B <sup>m</sup> #1			2.80 79.90
			5.69 77.01
	5.85	82.83	
	5.69	86.98	1.54 81.59
B <sup>m</sup> #3			3.13 83.85
			0.23 86.75
	11.22	97.99	0.08 97.91
	11.22	109.13	4.54 104.59
	7.86	112.45	
B <sup>m</sup> #2			5.49 106.96
			0.34 112.11
	10.48	122.59	
	11.77	133.97	0.24 122.20

Nail in Power Pole SW Cor Upper & Royal ✓

Nail in Gum Tree & Upper St at Sta. 13+25

On Hub 60' Rt & app. Sta 8+64 ✓



	133.97	0.48	133.49
J.P.	4.61	138.10	11.71
B.W.#1	1.81	128.20	9.57
			118.63

Top 3x3 Stk. Sta 0+00 ~~Market & Upper~~  
 This B.W. washed out -  
 See Pg. 29 for new one.



Check Levels Upper St to Euclid Ave along R.R. 29

Btu#2

106.96

Btu#1 Washed out so checked from #2  
See Pg. 27

10.55 117.51

0.86 116.65

10.39 127.04

0.00 127.04

11.00 128.04

6.38 131.66

1.10 132.76

6.38 126.38 126.39

1+00

10.5

See T.P. Pg. 28  
Upper St.

0+50

12.6

Btu#1

11.15 121.61

Set new Btu 12' East 0+00 on Hub

Btu#2

106.96

6.88 113.84

3.98 109.86

4.93 114.69

3.84 110.85

3.85 114.70

4/23/26  
Coote  
Losey  
Bell



114.70

4.56 110.14

3.68 113.82

4.20 109.62

4.23 113.85

4.25 109.60

4.56 114.16

Blu # 18

4.35 109.81 110.00

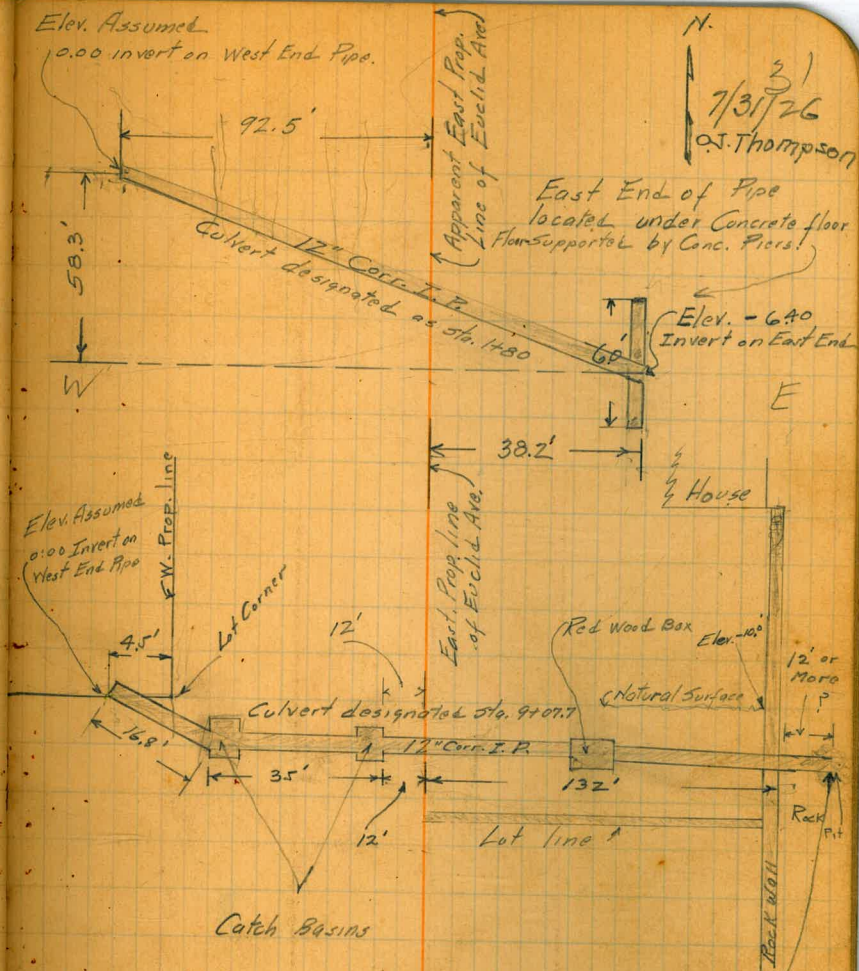
Euclid Ave. Blu. Adjusted to Co. Datum.

$$\begin{array}{r}
 103.88 \text{ Blu \# 18 City Datum} \\
 + 6.12 \text{ Correction to County Datum} \\
 \hline
 110.00 = \text{Elev. of Blu \# 18 Euclid Ave} \\
 \text{using County Datum.}
 \end{array}$$



Euclid Ave

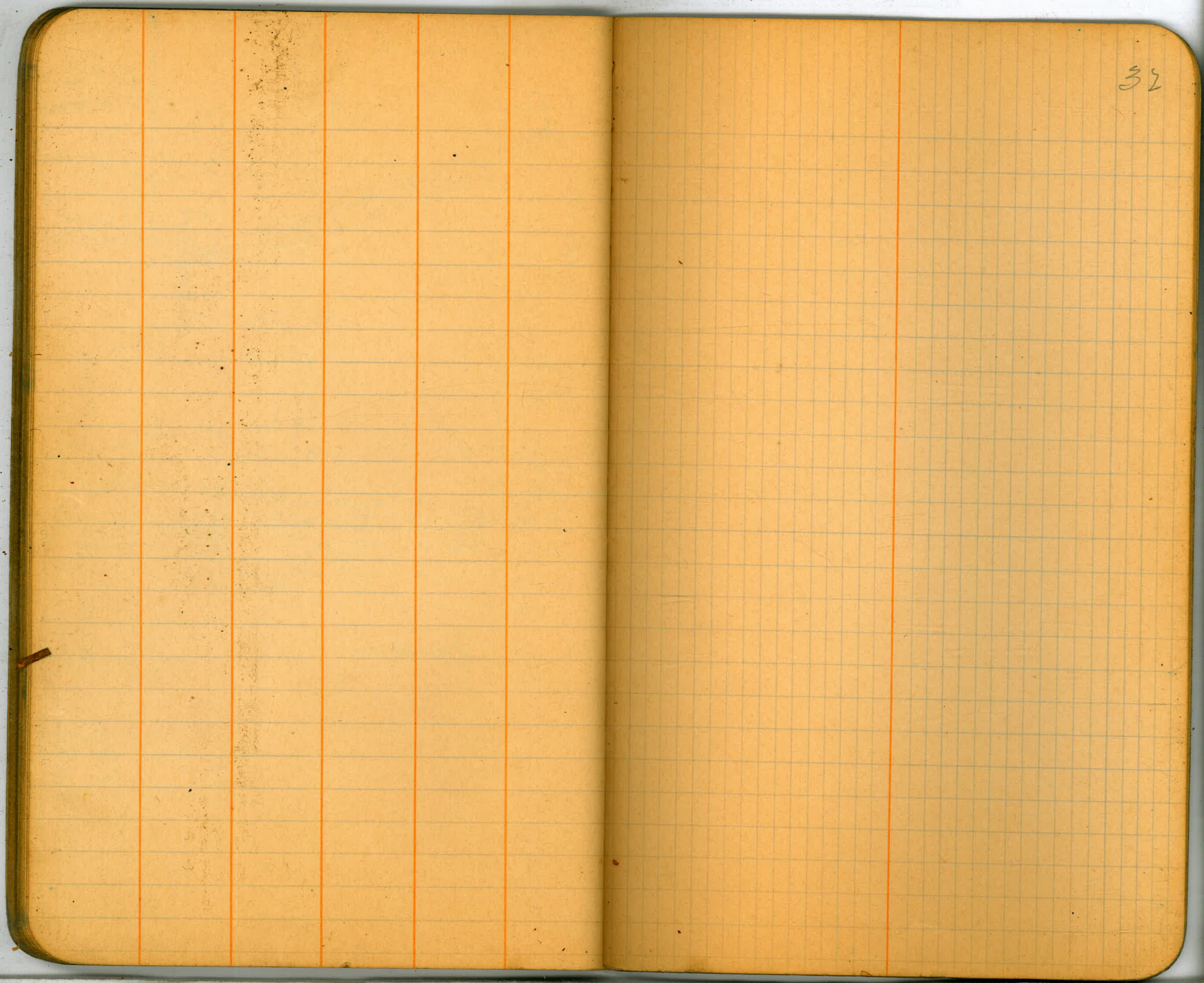
Culvert Dope



July 31 - 1926  
O.J. Thompson  
Rob Key  
Bill Spencer

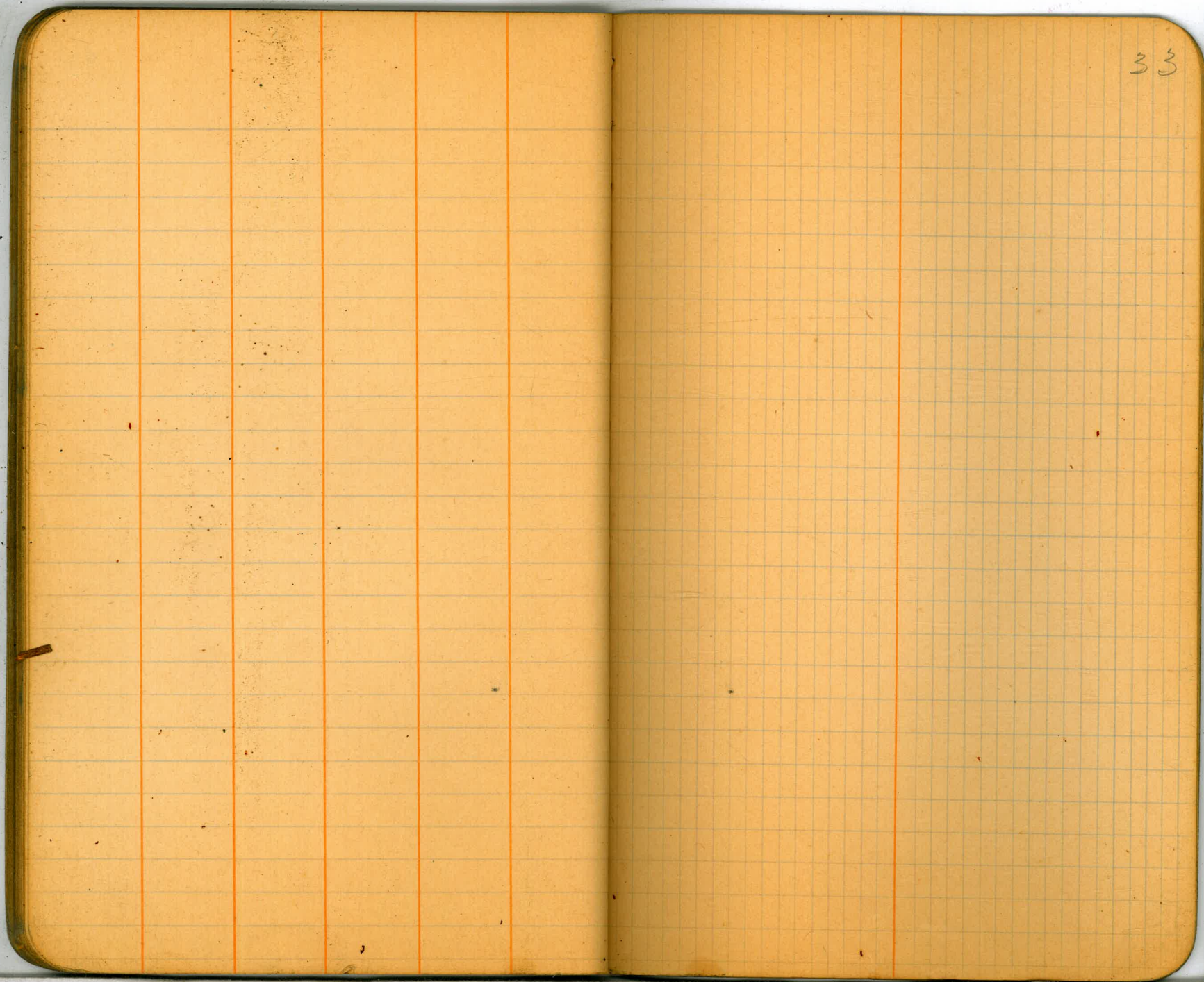
Invert  
Appx. 22'  
Lower than  
West End.





32





33



34



35



36



38.20  
92.50  
130.70