

NAME EUCLID-DIVISION  
Job 251 A.I.D.#19  
Class \_\_\_\_\_ Course \_\_\_\_\_ Party \_\_\_\_\_

Division West

Alignment  
WATSON, VALLE & GOUGH, INC.  
X-Sections

368

1891

## FIELD NOTES

No. 403P

ESPECIALLY ADAPTED  
TO THE USE OF  
ENGINEERING STUDENTS

---

**EUGENE DIETZGEN Co.**

MANUFACTURERS

**DRAWING MATERIALS  
MATHEMATICAL AND SURVEYING INSTRUMENTS  
MEASURING TAPES**

CHICAGO SAN FRANCISCO NEW YORK  
NEW ORLEANS PITTSBURGH



MICROFILMED

DIVISION ST.  
DEC 30 1964

Euclid Ave. to Laurel Ave.

Job # 251

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Alignment: DIVISION ST. Laurel to end of Job	29-30
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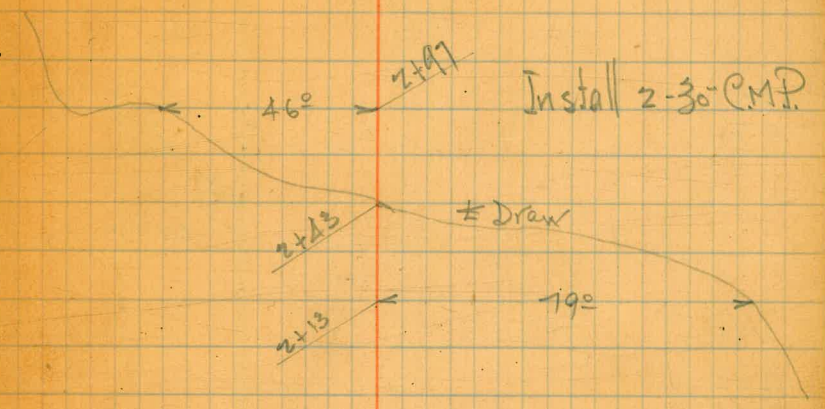
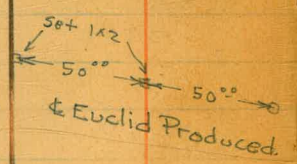


Sta.      Dist.      Angle  
 Az.    Def.       $\neq$  Ties-

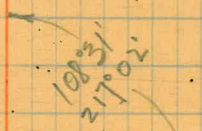
2017<sup>00</sup>

V

0+00 =  
 52+97.05  
 Original Survey



Found  $1\frac{1}{4}$ " Pipe



6/22/27  
 Coate  
 Culver  
 Morgan



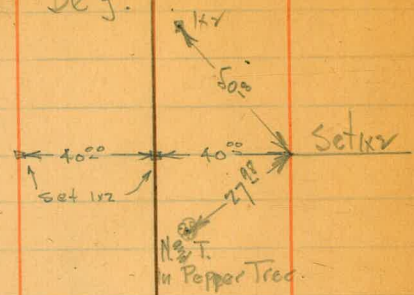
Sta.

Dist-

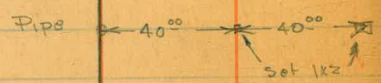
Angle  
Az. Def.

± Ties-

11+00  
P.O.T.



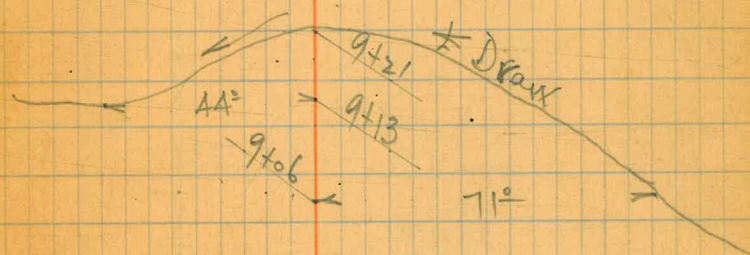
2617°



Set Lead & Tack  
 6+99± on  $\downarrow$   
 5+28  
 CPC

0°  
 6+99±  
 Find 1/2" Pipe

Install 24" CMP

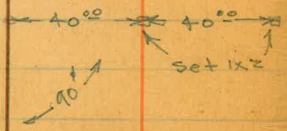
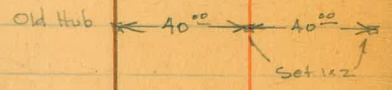




Sta. Dist. Angle Az. Def. ± Ties:

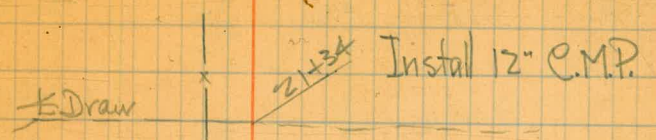
2617.00

12+86.39  
P.O.T.



Set Lead & Tack  
19+00.95 & Pavc  
5-4-28  
EPC

Set Lead & Tack  
14+00.82 & 12+86.39  
on & Pavc  
5-4-28  
EPC



19+00.95  
Find 2x2



14+00.82  
Find 3\"/>

12+86.39  
Find Conc. Man  
12\"/>

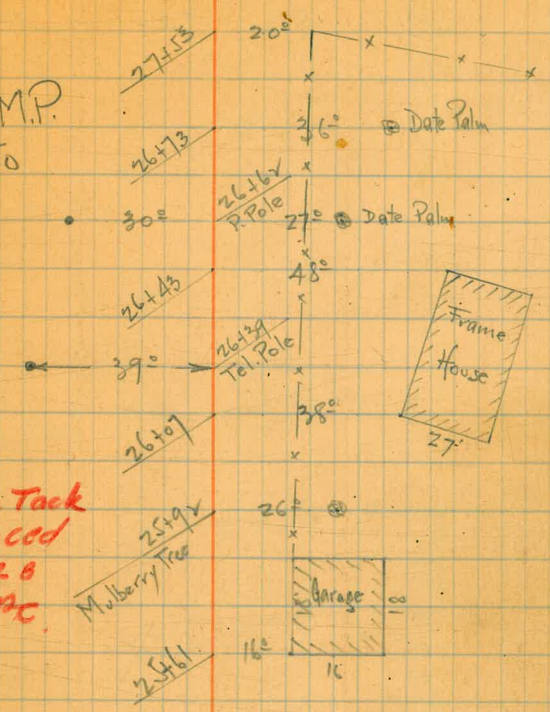
12+60  
Force Car



Sta.	Dist.	Angle AZ	Def	Ties -
	1222 21			
26+17 <sup>00</sup> P.I.		180°01' 360°02 1/2	0°01' R.	<p>N. 9.5 T. P. Pole 54"</p> <p>Found Conc. Mon. 12' Sq.</p> <p>4.4" N. 9.5 T. Tel. Pole</p>
				<p>40° ←</p> <p>← 40°</p> <p>Set 1x2</p> <p>26+17<sup>00</sup> Conc. Mon.</p> <p>90°</p>
	2617 <sup>00</sup>			
23+58.79 P.O.T.				<p>40°</p> <p>40°</p> <p>Set 1x2</p> <p>90°</p> <p>50.00</p> <p>40°</p> <p>40°</p>

Install 18" C.M.P.  
Sta. 27+50

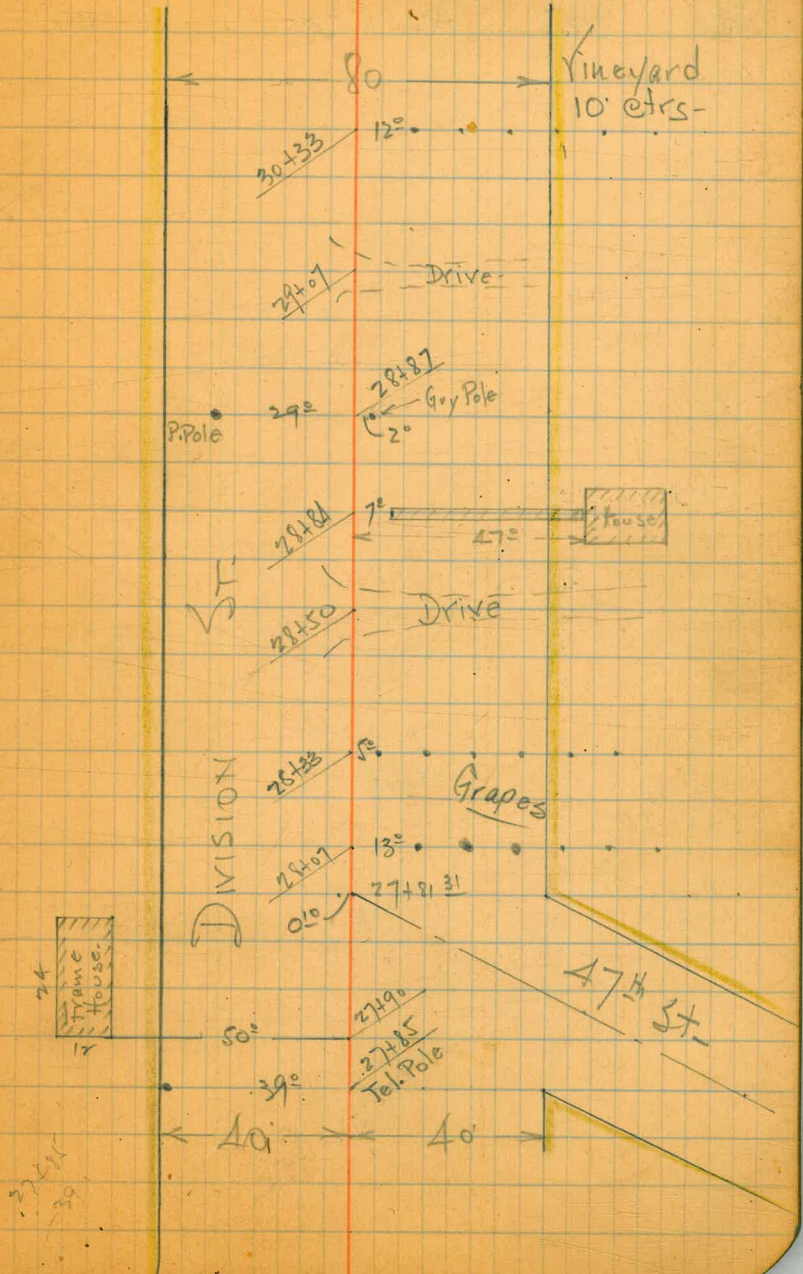
Set Lead & Tack  
as Referenced  
5-9-28  
EPC.





Sta      Dist      Angle  
 Az.      Def      ± Ties -

122281



27-85  
39°



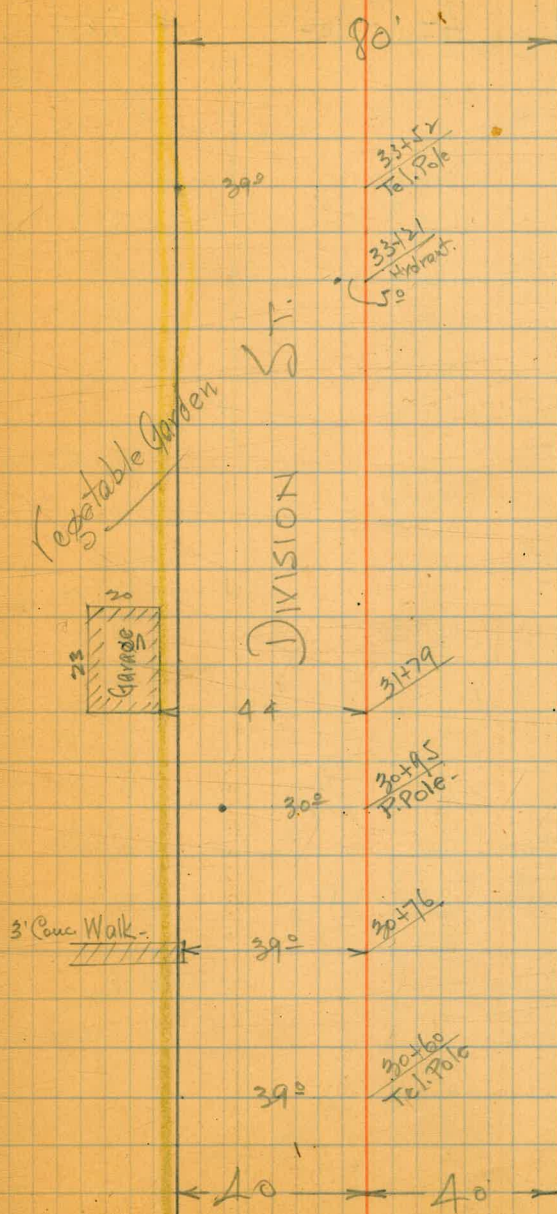
Sta.

Dist

Angle  
Az. Def.

\*Ties-

1222  $\frac{31}{2}$





Sta.

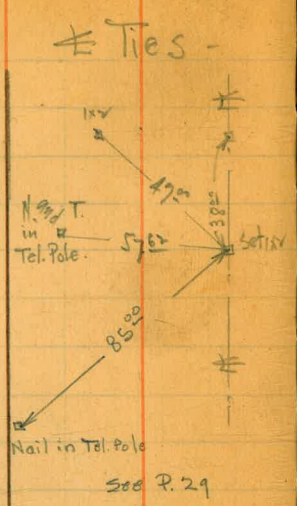
Dist.

Angle  
Az. Def.

END  
35+81.10  
P.O.T.



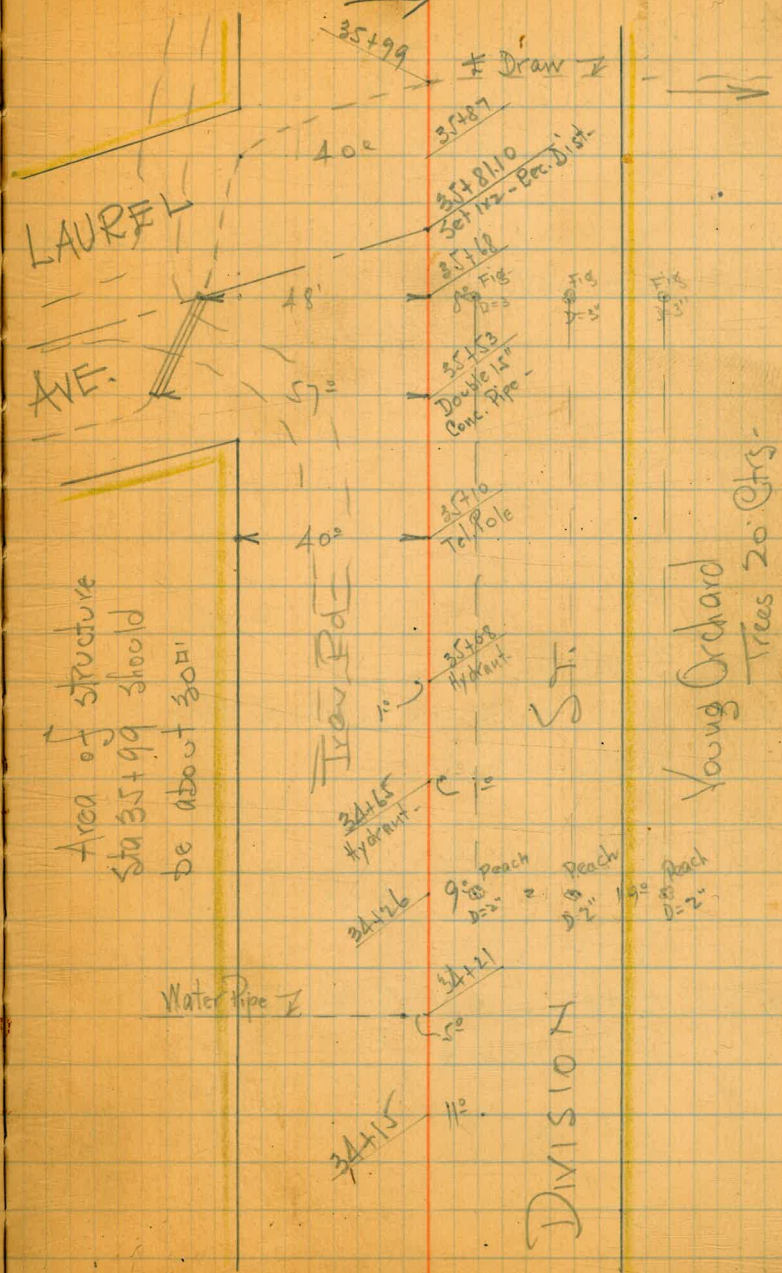
1222 3/4



cont. on page 29

End Curve Men. 12" 39. 27  
Highland Ave -

7



Area of structure  
Sta 35+99 should  
be about 300 ft

Young Orchard  
Trees 20' Cts.

DIVISION



Bench Levels  
DIVISION STREET  
West from Euclid -

B<sup>m</sup>

182 126.11

11.72 114.39

0.58 114.97

0.26 114.71

8.94 123.65

11.40 114.25

0.31 114.56

11.60 100.96

3.37 104.33

6.42 97.91

B<sup>m</sup>

10.76 108.67

0.70 107.97

11.22 119.19

4.23 114.96

6.22 121.18

5.36 115.82

B<sup>m</sup>

0.67 116.49

9.55 106.94

1.54 108.48

124.29

On 2x2 Hub 75' South Sta 52+97.05 -  
0+00 Going West.

On 1x2 Hub 75' Pt. Sta. 9+00

On 1x2 Hub 75' Lt. 12+60 On Fence Line -



		108.48		9.86	98.6w
	5.60	104.84		8.91	95.31
B <sup>W</sup>	1.33	96.64		11.73	84.91
	9.14	94.05		7.06	86.99
	1.28	88.57		11.95	76.32
B <sup>W</sup>	1.02	77.34		8.52	68.82
B <sup>W</sup>	3.73	72.55		5.62	66.93
				5.26	67.29
	1.09	68.38		10.29	58.09
	0.39	58.48		11.17	47.31
	2.00	49.31		6.09	43.22
	10.94	54.16		4.64	49.5w

73.055

On 1x2 Hub 70' Pt. Sta 20+95

On 1x2 Hub 75' Lt Sta. 26+17

B<sup>W</sup> In Tel. Pole S. Side St. at 47<sup>th</sup> (Fairmount B<sup>M</sup>)

$$\begin{array}{r} 73.055 \text{ County} \\ - 6.120 \\ \hline 66.935 \end{array}$$

On 1x2 Hub SW Cor LAUREL & Division



# X-Sections -

Bm

608 130.37

124.29

See Pg. 10

130.37

0+00

126.7	127.2	128.0	126.9	126.3	125.0
3.7	3.2	2.4	3.5	4.1	5.4
$\frac{3.7}{50}$	$\frac{3.2}{40}$	-	$\frac{3.5}{30}$	$\frac{4.1}{40}$	$\frac{5.4}{50}$

+50

124.0	124.4	124.2	127.4	126.9	125.3	122.7	122.4
6.4	6.0	4.2	3.0	3.5	5.1	7.7	10.0
$\frac{6.4}{50}$	$\frac{6.0}{15}$	$\frac{4.2}{12}$	-	$\frac{3.5}{15}$	$\frac{5.1}{27}$	$\frac{7.7}{40}$	$\frac{10.0}{50}$

+69

124.0	123.6	124.8	125.6	124.1	120.9	118.3
6.4	6.8	5.6	4.8	6.3	9.5	12.1
$\frac{6.4}{50}$	$\frac{6.8}{40}$	$\frac{5.6}{17}$	-	$\frac{6.3}{25}$	$\frac{9.5}{40}$	$\frac{12.1}{50}$

+83

123.4	123.2	124.7	125.5	124.9	118.9	116.5
7.0	7.2	5.7	4.9	6.7	11.5	13.9
$\frac{7.0}{50}$	$\frac{7.2}{40}$	$\frac{5.7}{18}$	-	$\frac{6.7}{15}$	$\frac{11.5}{40}$	$\frac{13.9}{50}$

+07

0.24 118.90

11.71 118.16

121.8	122.2	122.3	119.8	118.3	114.1	112.3
8.6	8.2	8.1	10.6	12.1	16.3	18.1
$\frac{8.6}{50}$	$\frac{8.2}{40}$	$\frac{8.1}{40}$	-	$\frac{12.1}{15}$	$\frac{16.3}{40}$	$\frac{18.1}{50}$

118.9

+22

119.3	119.4	118.3	116.1	116.9	114.1	112.9	111.5
10.4	10.5	0.6	0.8	2.0	1.8	6.5	7.4
$\frac{10.4}{50}$	$\frac{10.5}{40}$	$\frac{0.6}{16}$	-	$\frac{2.0}{15}$	$\frac{1.8}{20}$	$\frac{6.5}{40}$	$\frac{7.4}{50}$

R

R



+43

118.90

+78

0.88

108.03

11.75

107.15

✓

+35

+42

On Angle of Wash

+50

(R)

118.9

11

115.9	115.9	114.9	113.3	112.3	110.2	109.0	108.1
30	35	40	56	66	87	99	108
50	40	28	13		31	40	50

108.9	108.7	106.9	107.8	107.5	105.4	105.9	114.1	102.6
100	107	120	111	114	135	130	148	163
50	40	26	13		11	28	40	50

108.03

105.1	104.4	101.4	100.1	99.8	98.9	98.5
29	36	66	79	82	91	95
50	40	22		23	40	50

104.7	113.4	97.6	96.5	96.5	93.7	96.0	96.0
33	46	104	115	115	143	120	120
50	40	21		14	24	40	50

91.2	92.2	92.2	93.3	94.6	95.2	97.0
17.0	158	158	147	134	128	110
150	100	50		50	100	150

97.9	97.6	96.3	93.5	92.2	97.5	98.4	91.3
101	104	117	145	118	105	96	87
50	40	26	13		6	40	50

(R)



2+84

108.03

3

11.65

118.56

1.12 106.91

+50

+68

4

6.45

123.31

1.70 116.86

+50

R

108.03

12

94.0	92.8	95.2	96.2	97.8	99.6	105.0	107.2
$\frac{14.0}{50}$	$\frac{15.2}{40}$	$\frac{16.8}{30}$	$\frac{11.8}{17}$	$\frac{10.2}{17}$	$\frac{8.4}{13}$	$\frac{3.0}{40}$	$\frac{0.8}{50}$

96.6	96.5	98.3	101.0	103.1	106.5	110.0	112.9
$\frac{11.4}{50}$	$\frac{11.5}{40}$	$\frac{9.7}{15}$	$\frac{7.0}{12}$	$\frac{4.9}{12}$	$\frac{1.5}{27}$	$\frac{+2.0}{40}$	$\frac{+1.9}{50}$

118.56

103.0	105.6	111.3	113.5	116.1	119.3	121.1
$\frac{15.5}{50}$	$\frac{12.9}{40}$	$\frac{7.2}{13}$	$\frac{5.0}{13}$	$\frac{2.4}{19}$	$\frac{+0.8}{40}$	$\frac{+2.6}{50}$

105.9	108.3	110.7	113.7	115.4	117.7	119.5	120.9
$\frac{12.6}{50}$	$\frac{10.2}{40}$	$\frac{7.8}{34}$	$\frac{4.8}{11}$	$\frac{3.1}{11}$	$\frac{0.8}{28}$	$\frac{+1.0}{40}$	$\frac{+2.4}{50}$

107.9	111.0	112.5	114.4	115.5	117.2	119.5	120.6
$\frac{10.6}{50}$	$\frac{7.5}{40}$	$\frac{6.0}{34}$	$\frac{4.1}{18}$	$\frac{3.0}{18}$	$\frac{1.3}{20}$	$\frac{+1.0}{40}$	$\frac{+2.1}{50}$

123.31

113.7	114.3	114.0	117.2	118.7	119.8	121.0
$\frac{9.6}{50}$	$\frac{9.0}{40}$	$\frac{9.3}{24}$	$\frac{6.1}{19}$	$\frac{4.6}{19}$	$\frac{3.5}{40}$	$\frac{2.3}{50}$

R



123.31

+50

+78

6

+28

6.99

118.85

11.45 111.86

+76

R

Lt.

Rt

13

				123.3			
1145	1149	1154	1169	1184	1190	1211	122.0
88	84	79	64	49	43	22	13
<u>50</u>	<u>40</u>	<u>34</u>	<u>23</u>	<u>1</u>	<u>21</u>	<u>40</u>	<u>50</u>

1149	1159	119.0	121.2	121.8
84	74	48	21	15
<u>50</u>	<u>40</u>	<u>1</u>	<u>40</u>	<u>50</u>

1147	1154	1174	120.0	121.1	120.8	121.1
86	79	59	33	22	25	22
<u>50</u>	<u>40</u>	<u>27</u>	<u>1</u>	<u>12</u>	<u>40</u>	<u>50</u>

1143	1155	1189	119.2	117.8	118.0
90	78	44	41	55	53
<u>50</u>	<u>40</u>	<u>15</u>	<u>1</u>	<u>40</u>	<u>50</u>

1139	1147	1155	114.8	114.5	114.5	114.9
94	91	78	85	88	88	84
<u>50</u>	<u>40</u>	<u>17</u>	<u>1</u>	<u>23</u>	<u>40</u>	<u>50</u>

118.85

106.8	107.3	107.7	109.5	110.8	112.1	113.1
120	115	111	93	80	67	57
<u>50</u>	<u>40</u>	<u>24</u>	<u>1</u>	<u>24</u>	<u>40</u>	<u>50</u>

R



118.85

7

+50

8

+28

0.67 108.09

11.43 107.42

+58

+83

Lt.

118.85

Rt.

14

104.7	105.4	108.0	108.8	111.8	113.6	115.5
$\frac{14.1}{50}$	$\frac{13.4}{40}$	$\frac{10.8}{15}$	$\frac{10.0}{-}$	$\frac{7.0}{28}$	$\frac{5.2}{40}$	$\frac{3.3}{50}$

103.5	105.3	110.1	112.0	113.8	115.3	116.5	117.0
$\frac{15.3}{50}$	$\frac{13.5}{40}$	$\frac{8.7}{19}$	$\frac{6.8}{13}$	$\frac{5.0}{-}$	$\frac{3.5}{15}$	$\frac{2.3}{40}$	$\frac{1.8}{50}$

103.4	104.9	107.4	109.2	110.4	111.7	111.5	111.7
$\frac{15.4}{50}$	$\frac{12.9}{40}$	$\frac{11.4}{19}$	$\frac{9.6}{13}$	$\frac{8.4}{-}$	$\frac{7.1}{14}$	$\frac{7.3}{40}$	$\frac{7.1}{50}$

105.6	106.3	108.7	109.3	109.3	108.7	109.1
$\frac{13.3}{50}$	$\frac{12.5}{40}$	$\frac{10.1}{18}$	$\frac{9.5}{-}$	$\frac{9.5}{20}$	$\frac{10.1}{40}$	$\frac{9.7}{50}$

108.09

99.7	100.6	103.1	104.8	104.5	104.3	104.7
$\frac{8.3}{50}$	$\frac{7.4}{40}$	$\frac{4.9}{14}$	$\frac{3.2}{-}$	$\frac{3.5}{14}$	$\frac{3.7}{40}$	$\frac{3.3}{50}$

94.3	94.8	99.7	97.0	98.4	100.2	100.6
$\frac{13.7}{50}$	$\frac{13.4}{40}$	$\frac{8.3}{14}$	$\frac{11.0}{-}$	$\frac{9.6}{23}$	$\frac{7.8}{40}$	$\frac{1.4}{50}$

B

B



9+21

108.09

"

On Angle of Draw

+50

+71

10

10.84

118.41

0.52

107.57

+25

B.

108.09

15

93.4	93.3	93.7	93.4	93.5	94.3	95.5	96.7
$\frac{14.6}{50}$	$\frac{14.7}{40}$	$\frac{14.3}{11}$	$\frac{14.6}{-}$	$\frac{14.5}{21}$	$\frac{13.7}{48}$	$\frac{12.8}{41}$	$\frac{11.3}{50}$

90.1	91.0	93.4	95.1	96.2	98.0
$\frac{18.0}{100}$	$\frac{17.1}{50}$	$\frac{14.6}{-}$	$\frac{12.9}{50}$	$\frac{11.8}{100}$	$\frac{10.1}{150}$

99.1	99.3	96.8	96.4	97.2	97.0	99.6
$\frac{9.0}{50}$	$\frac{8.8}{40}$	$\frac{11.3}{13}$	$\frac{11.7}{-}$	$\frac{10.9}{23}$	$\frac{11.1}{40}$	$\frac{10.4}{50}$

103.5	103.5	101.9	100.1	100.1	99.7	99.6
$\frac{4.6}{50}$	$\frac{4.6}{40}$	$\frac{6.7}{15}$	$\frac{8.0}{-}$	$\frac{8.0}{55}$	$\frac{8.4}{40}$	$\frac{8.5}{50}$

109.0	108.8	108.6	107.5	107.3	105.7	105.9
$\frac{11.0}{50}$	$\frac{10.8}{40}$	$\frac{10.6}{14}$	$\frac{0.6}{-}$	$\frac{0.8}{18}$	$\frac{2.4}{40}$	$\frac{2.2}{50}$

118.41

113.8	113.4	112.0	112.4	111.5	111.7
$\frac{4.6}{50}$	$\frac{5.0}{40}$	$\frac{6.4}{-}$	$\frac{6.0}{24}$	$\frac{6.9}{40}$	$\frac{6.7}{50}$



10+50

118.41

5.96

123.45

0.92 117.49

+81

11

+50

12

Bhw

+50

13

7.61

115.84

115.82

See Pg. 8

R

118.4

16

117.4	117.0	116.5	115.9	114.7	114.5	114.5
$\frac{10}{50}$	$\frac{15}{40}$	$\frac{19}{23}$	$\frac{25}{-}$	$\frac{37}{22}$	$\frac{39}{20}$	$\frac{39}{50}$

123.45

120.7	120.5	120.0	119.2	117.8	117.0	116.8
$\frac{27}{50}$	$\frac{30}{40}$	$\frac{35}{18}$	$\frac{42}{-}$	$\frac{57}{21}$	$\frac{65}{40}$	$\frac{76}{50}$

121.7	121.4	121.0	120.0	118.5	117.4	116.3
$\frac{18}{50}$	$\frac{21}{40}$	$\frac{24}{14}$	$\frac{35}{-}$	$\frac{50}{20}$	$\frac{60}{40}$	$\frac{71}{50}$

120.9	120.6	119.9	118.6	117.1	116.1	115.2
$\frac{26}{50}$	$\frac{29}{40}$	$\frac{36}{14}$	$\frac{49}{-}$	$\frac{64}{31}$	$\frac{74}{40}$	$\frac{83}{50}$

118.7	118.5	117.7	116.6	114.6	113.9	113.0
$\frac{48}{40}$	$\frac{50}{40}$	$\frac{58}{13}$	$\frac{69}{-}$	$\frac{89}{23}$	$\frac{96}{40}$	$\frac{99}{50}$

115.9	115.6	114.7	114.2	113.2	112.0
$\frac{76}{50}$	$\frac{79}{40}$	$\frac{88}{-}$	$\frac{93}{10}$	$\frac{103}{40}$	$\frac{115}{50}$

112.7	112.5	112.7	112.3	112.0	111.5	111.0
$\frac{108}{50}$	$\frac{110}{40}$	$\frac{108}{6}$	$\frac{112}{-}$	$\frac{115}{10}$	$\frac{120}{40}$	$\frac{125}{50}$

R



12345

11.60 11.85

0.37 11222

13450

14

+33

+50

+75

136 101.99

15

11.59 100.63

112.22

110.7	110.4	109.9	110.7	110.2	109.8	109.0	108.6	108.8
$\frac{15}{50}$	$\frac{18}{40}$	$\frac{23}{15}$	$\frac{15}{2}$	$\frac{20}{1}$	$\frac{24}{3}$	$\frac{32}{20}$	$\frac{36}{40}$	$\frac{34}{50}$

109.3	108.4	108.7	107.7	106.8	106.5
$\frac{29}{50}$	$\frac{38}{40}$	$\frac{38}{1}$	$\frac{15}{1}$	$\frac{56}{40}$	$\frac{57}{50}$

107.7	107.2	106.6	106.9	106.2	103.8	103.7
$\frac{45}{50}$	$\frac{50}{40}$	$\frac{56}{8}$	$\frac{53}{1}$	$\frac{60}{13}$	$\frac{84}{40}$	$\frac{88}{50}$

106.6	106.2	104.8	105.2	104.5	103.1	102.9	102.8
$\frac{56}{50}$	$\frac{60}{40}$	$\frac{14}{9}$	$\frac{70}{1}$	$\frac{77}{12}$	$\frac{91}{24}$	$\frac{93}{40}$	$\frac{94}{50}$

105.5	105.8	105.6	103.6	102.4	101.5	102.0	101.8
$\frac{67}{50}$	$\frac{64}{40}$	$\frac{66}{26}$	$\frac{86}{13}$	$\frac{98}{1}$	$\frac{107}{12}$	$\frac{102}{40}$	$\frac{101}{50}$

101.99

103.1	101.7	99.2	99.1	99.4	98.6	97.5
$\frac{11}{50}$	$\frac{03}{40}$	$\frac{28}{19}$	$\frac{30}{1}$	$\frac{26}{19}$	$\frac{34}{40}$	$\frac{44}{50}$



15+28

101.99

+70

16

+50

+69

17

6.65

99.93

8.71

93.28

R

18

101.99

98.5	97.1	96.6	97.1	96.3	95.2	99.0	93.5
<u>35</u>	<u>49</u>	<u>54</u>	<u>49</u>	<u>57</u>	<u>70</u>	<u>80</u>	<u>85</u>
50	40	7		12	30	40	50

92.4	92.5	90.6	91.2	92.4	93.6
<u>96</u>	<u>95</u>	<u>114</u>	<u>108</u>	<u>96</u>	<u>84</u>
50	40		16	40	50

91.8	89.6	88.0	90.4	91.4	92.3	93.8	94.8
<u>112</u>	<u>124</u>	<u>140</u>	<u>116</u>	<u>106</u>	<u>97</u>	<u>82</u>	<u>72</u>
80	40	23		3	21	40	50

85.8	86.8	89.4	92.1	92.2	93.7	95.4	99.2	100.6
<u>162</u>	<u>157</u>	<u>126</u>	<u>99</u>	<u>98</u>	<u>83</u>	<u>66</u>	<u>28</u>	<u>14</u>
50	40	22	3		4	18	4	50

86.6	87.5	89.7	92.9	93.4	95.1	97.2	100.2	101.2
<u>144</u>	<u>145</u>	<u>123</u>	<u>91</u>	<u>86</u>	<u>69</u>	<u>18</u>	<u>18</u>	<u>08</u>
50	40	23	3		5	30	40	50

99.9

85.6	86.7	89.1	92.6	93.2	94.2	95.3	99.4	100.7
<u>143</u>	<u>132</u>	<u>108</u>	<u>73</u>	<u>67</u>	<u>57</u>	<u>46</u>	<u>05</u>	<u>108</u>
50	40	24	4		2	11	40	50

R



9993

17+25

+50

18

+50

T.P.

4.24 101.16

3.01 96.92

19

+35

99.9

19

84.2	85.3	88.6	91.6	92.8	95.3	97.7	99.7
157	146	113	83	71	46	22	07
50	40	20	5	5	26	40	50

83.7	85.3	88.8	90.6	91.1	92.8	96.5	98.6
167	146	111	93	88	71	34	13
50	40	17	5	5	12	40	50

81.8	82.9	83.7	87.7	89.7	90.9	92.9	97.8	100.3
181	170	167	127	107	90	70	21	04
50	40	30	8	5	13	24	40	50

83.3	84.3	85.3	88.8	90.3	91.5	97.2	98.9
168	156	146	111	96	84	27	10
50	40	34	6	5	9	40	50

Spk in Ground 24' Rt. Sta. 18+67

87.1	89.7	92.9	96.3	96.6	96.5	98.9	99.3
140	114	82	48	15	44	27	18
50	40	24	5	5	12	40	50

89.4	91.7	93.0	94.8	96.1	96.8	97.1	98.2	98.5	98.6
117	94	81	63	50	43	40	29	26	25
50	40	33	11	6	5	9	21	40	50

R

R



19+85

101.16

20+25

~~76~~

+60

2.94

92.46

11.64

89.54

21

B-w

7.55

84.91

84.01

+25

101.16

20

91.3	93.0	93.7	93.8	94.6	95.5	96.2	96.1
$\frac{98}{50}$	$\frac{81}{40}$	$\frac{74}{31}$	$\frac{73}{9}$	$\frac{65}{7}$	$\frac{56}{16}$	$\frac{49}{40}$	$\frac{50}{50}$

88.8	89.6	91.5	92.4	91.7	91.2	91.4	91.7	92.1
$\frac{123}{50}$	$\frac{115}{40}$	$\frac{96}{11}$	$\frac{87}{4}$	$\frac{94}{7}$	$\frac{99}{16}$	$\frac{97}{32}$	$\frac{94}{40}$	$\frac{90}{50}$

92.46

85.4	86.8	89.1	89.6	89.1	87.1	87.4	88.4
$\frac{70}{50}$	$\frac{56}{40}$	$\frac{33}{15}$	$\frac{28}{4}$	$\frac{33}{7}$	$\frac{53}{21}$	$\frac{50}{40}$	$\frac{40}{50}$

78.6	80.8	82.3	82.4	82.0	82.3	83.0
$\frac{138}{50}$	$\frac{116}{40}$	$\frac{101}{10}$	$\frac{100}{7}$	$\frac{104}{31}$	$\frac{101}{40}$	$\frac{94}{50}$

500 P 9

75.4	78.3	78.0	79.1	80.1	81.4	82.0
$\frac{170}{50}$	$\frac{161}{40}$	$\frac{144}{20}$	$\frac{138}{7}$	$\frac{123}{23}$	$\frac{110}{40}$	$\frac{104}{50}$

B

R



21+39 92.46

+75

22+15

2.18 91.40

+50

23

+30

+80

R

92.46 21

75.8	76.3	77.8	79.2	80.1	81.7	82.4
$\frac{16.6}{50}$	$\frac{16.1}{40}$	$\frac{14.6}{13}$	$\frac{13.2}{-}$	$\frac{12.3}{21}$	$\frac{10.7}{40}$	$\frac{10.0}{50}$

79.5	79.3	80.1	81.1	82.6	83.7	85.0	86.7
$\frac{12.9}{50}$	$\frac{13.1}{40}$	$\frac{12.3}{17}$	$\frac{11.3}{7}$	$\frac{9.8}{-}$	$\frac{8.7}{18}$	$\frac{6.8}{40}$	$\frac{5.7}{50}$

84.6	84.5	84.4	85.9	86.8	86.6	88.7	89.5
$\frac{7.8}{50}$	$\frac{7.9}{40}$	$\frac{8.0}{34}$	$\frac{6.5}{5}$	$\frac{5.6}{-}$	$\frac{5.8}{12}$	$\frac{3.7}{40}$	$\frac{2.9}{50}$

91.40

86.0	86.3	87.1	88.3	89.3	89.4	91.0	91.1
$\frac{5.4}{50}$	$\frac{5.1}{40}$	$\frac{4.3}{24}$	$\frac{3.1}{10}$	$\frac{2.1}{-}$	$\frac{2.0}{18}$	$\frac{0.4}{40}$	$\frac{0.3}{50}$

84.3	84.8	85.8	86.8	86.4	86.7	87.6	87.6
$\frac{7.1}{50}$	$\frac{6.6}{40}$	$\frac{5.6}{17}$	$\frac{4.6}{4}$	$\frac{5.0}{-}$	$\frac{4.7}{18}$	$\frac{3.8}{40}$	$\frac{3.8}{50}$

85.5	86.4	86.0	86.6	86.5	86.8	86.2	86.2
$\frac{5.9}{50}$	$\frac{5.0}{40}$	$\frac{5.4}{9}$	$\frac{4.8}{4}$	$\frac{4.9}{-}$	$\frac{5.4}{16}$	$\frac{5.2}{18}$	$\frac{5.2}{50}$

92.7	92.5	90.7	87.8	86.8	86.8	86.5	85.2	82.9	82.7
$\frac{+13}{50}$	$\frac{+11}{40}$	$\frac{0.7}{30}$	$\frac{3.6}{15}$	$\frac{4.5}{11}$	$\frac{4.6}{5}$	$\frac{0.9}{-}$	$\frac{6.2}{16}$	$\frac{8.5}{18}$	$\frac{8.7}{50}$



91.40

24

+50

1.57 81.55

+80

25+15

+43

26

+50

R

91.4

22

92.6	92.4	90.2	87.4	85.7	86.0	85.6	82.3	82.2	82.3
$\frac{+12}{50}$	$\frac{+10}{40}$	$\frac{12}{30}$	$\frac{40}{17}$	$\frac{57}{10}$	$\frac{54}{5}$	$\frac{58}{-}$	$\frac{91}{30}$	$\frac{92}{40}$	$\frac{91}{50}$

86.0	85.8	84.2	83.5	81.9	79.9	80.1	80.5
$\frac{54}{50}$	$\frac{56}{40}$	$\frac{72}{17}$	$\frac{89}{9}$	$\frac{95}{-}$	$\frac{120}{32}$	$\frac{113}{40}$	$\frac{109}{50}$

81.55

81.6	81.4	80.1	79.6	79.8	79.3	77.7	78.6	78.5	79.2
$\frac{+11}{50}$	$\frac{01}{40}$	$\frac{14}{24}$	$\frac{20}{12}$	$\frac{17}{4}$	$\frac{22}{-}$	$\frac{38}{12}$	$\frac{39}{22}$	$\frac{30}{40}$	$\frac{25}{50}$

74.6	74.5	75.8	75.3	75.6	75.7	76.0	77.0	77.8
$\frac{69}{50}$	$\frac{66}{40}$	$\frac{57}{20}$	$\frac{64}{11}$	$\frac{60}{-}$	$\frac{55}{7}$	$\frac{55}{17}$	$\frac{45}{40}$	$\frac{37}{50}$

71.7	72.1	73.2	74.6	75.3	75.9	76.9	77.5
$\frac{98}{50}$	$\frac{94}{40}$	$\frac{83}{17}$	$\frac{69}{-}$	$\frac{62}{13}$	$\frac{56}{28}$	$\frac{46}{40}$	$\frac{40}{50}$

71.0	71.7	73.1	74.8	75.2	76.7	77.3	77.7	77.8
$\frac{105}{50}$	$\frac{98}{40}$	$\frac{84}{16}$	$\frac{67}{7}$	$\frac{63}{-}$	$\frac{48}{16}$	$\frac{42}{38}$	$\frac{38}{40}$	$\frac{37}{50}$

72.9	71.8	73.6	74.0	74.6	75.6	75.8	75.7	75.7
$\frac{106}{50}$	$\frac{97}{40}$	$\frac{79}{12}$	$\frac{75}{-}$	$\frac{69}{5}$	$\frac{59}{19}$	$\frac{57}{-}$	$\frac{57}{40}$	$\frac{57}{50}$

R



27 2.24 81.55 75.19 8.60 72.95

+35

+60

+90

B/W

28+30

+80

+84

8.24 66.95 66.94

8.24 66.95

1.19 68.14

1.40

(R)

7.5.19

87.2 28.0 70.9 71.2 72.2 72.3 72.0 71.9  
 8.0 7.2 4.3 4.0 3.0 2.9 3.2 3.3  
 50 40 10 19 9 19 40 50

60.3 61.1 63.3 66.5 66.7 66.7 65.3 65.7 66.3 66.9 67.0  
 14.9 14.1 11.9 8.7 8.5 8.5 9.9 9.5 8.9 8.3 8.2  
 50 40 14 7 2 6 16 19 40 50

60.4 60.8 62.6 65.7 65.7 65.5 64.4 66.0 66.7 67.3  
 14.8 14.1 12.6 9.3 9.5 9.7 10.8 9.2 9.5 7.9  
 50 40 14 8 6 16 32 40 50

63.8 65.3 66.2 66.9 66.9 67.2 67.6  
 11.4 9.9 9.0 8.3 8.3 8.0 7.6  
 50 40 24 27 40 50

See Pg. 9

61.4 63.5 66.4 67.2 66.9 67.4 68.7 69.0  
 13.8 11.7 8.6 8.0 8.3 7.8 6.5 6.2  
 50 40 24 8 4 40 50

68.14

56.8 58.7 62.0 64.6 65.3 65.2 66.1 66.8 68.34 68.64  
 13.0 9.4 6.1 3.5 2.8 2.9 2.0 1.3 10.7 10.5  
 50 40 24 19 10 3 6 40 50

7: Pt. au Conc Walk

(R)



68.14

29

+50

30

+50

+76

11.35

11.27 56.87

x 2.15 59.04

31

+50

Ⓜ

68.14

24

$\frac{110}{50}$  58.7 69.8 62.1 64.3 64.8 64.5 65.1 67.4 67.2  
 $\frac{94}{40}$  8.3 6.9 3.8 3.3 2.6 2.0 0.7 0.2  
 $\frac{28}{22}$   $\frac{15}{11}$   $\frac{4}{4}$   $\frac{40}{40}$   $\frac{50}{50}$

60.7 61.1 62.7 63.2 63.1 63.6 65.5 65.9  
 $\frac{74}{40}$   $\frac{70}{40}$   $\frac{54}{19}$   $\frac{49}{11}$   $\frac{50}{4}$   $\frac{45}{4}$   $\frac{26}{40}$   $\frac{22}{50}$

59.2 59.6 60.5 61.0 60.5 61.3 61.4 63.6 64.1  
 $\frac{89}{50}$   $\frac{85}{40}$   $\frac{76}{23}$   $\frac{71}{9}$   $\frac{76}{7}$   $\frac{68}{3}$   $\frac{67}{4}$   $\frac{45}{40}$   $\frac{41}{50}$

57.7 57.1 57.4 58.6 58.2 59.3 61.4 61.7  
 $\frac{114}{50}$   $\frac{110}{40}$   $\frac{102}{24}$   $\frac{95}{12}$   $\frac{99}{10}$   $\frac{88}{4}$   $\frac{67}{40}$   $\frac{64}{50}$

Conc Walk 29' Lt.

59.02

$\frac{94}{50}$  55.7 56.3 56.8 56.2 56.3 56.7 56.7 57.2 58.0 58.0  
 $\frac{42}{50}$   $\frac{35}{40}$   $\frac{27}{17}$   $\frac{22}{12}$   $\frac{28}{7}$   $\frac{27}{5}$   $\frac{21}{5}$   $\frac{23}{4}$   $\frac{16}{40}$   $\frac{10}{40}$   $\frac{10}{50}$

57.6 52.3 53.2 53.6 53.9 52.5 53.8 54.3 54.1 54.7 55.0  
 $\frac{84}{50}$   $\frac{67}{40}$   $\frac{18}{37}$   $\frac{54}{31}$   $\frac{51}{18}$   $\frac{45}{11}$   $\frac{52}{4}$   $\frac{47}{10}$   $\frac{44}{19}$   $\frac{43}{40}$   $\frac{40}{50}$

Ⓜ



32

59.02

+50

2.06

49.07

12.01

47.01

33

+50

34

+41

59.02

25

<u>49.8</u>	<u>49.9</u>	<u>50.3</u>	<u>50.3</u>	<u>49.9</u>	<u>50.5</u>	<u>50.3</u>	<u>50.8</u>	<u>57.0</u>
$\frac{92}{50}$	$\frac{91}{40}$	$\frac{87}{29}$	$\frac{87}{11}$	$\frac{91}{8}$	$\frac{85}{-}$	$\frac{87}{20}$	$\frac{82}{40}$	$\frac{80}{50}$

<u>46.8</u>	<u>46.5</u>	<u>46.5</u>	<u>47.2</u>	<u>46.9</u>	<u>47.9</u>	<u>47.4</u>	<u>47.9</u>	<u>48.2</u>
$\frac{122}{50}$	$\frac{128}{40}$	$\frac{128}{29}$	$\frac{118}{28}$	$\frac{121}{13}$	$\frac{116}{8}$	$\frac{116}{-}$	$\frac{111}{40}$	$\frac{110}{50}$

49.07

<u>46.2</u>	<u>45.6</u>	<u>45.9</u>	<u>45.5</u>	<u>45.7</u>	<u>45.2</u>	<u>45.6</u>	<u>45.8</u>
$\frac{30}{50}$	$\frac{34}{40}$	$\frac{31}{28}$	$\frac{35}{6}$	$\frac{33}{-}$	$\frac{38}{18}$	$\frac{34}{40}$	$\frac{32}{50}$

<u>44.3</u>	<u>44.5</u>	<u>44.5</u>	<u>44.7</u>	<u>44.1</u>	<u>43.6</u>	<u>43.7</u>	<u>44.1</u>
$\frac{47}{50}$	$\frac{48}{40}$	$\frac{48}{27}$	$\frac{43}{8}$	$\frac{49}{-}$	$\frac{54}{17}$	$\frac{51}{20}$	$\frac{49}{50}$

<u>43.6</u>	<u>43.9</u>	<u>43.7</u>	<u>43.7</u>	<u>43.0</u>	<u>43.9</u>	<u>42.6</u>	<u>42.7</u>
$\frac{54}{50}$	$\frac{56}{40}$	$\frac{53}{30}$	$\frac{53}{9}$	$\frac{60}{-}$	$\frac{66}{14}$	$\frac{64}{40}$	$\frac{63}{50}$

<u>43.2</u>	<u>43.2</u>	<u>43.6</u>	<u>42.8</u>	<u>41.2</u>	<u>41.6</u>	<u>40.9</u>	<u>41.6</u>	<u>41.5</u>
$\frac{48}{50}$	$\frac{58}{40}$	$\frac{54}{28}$	$\frac{67}{13}$	$\frac{78}{14}$	$\frac{74}{-}$	$\frac{81}{20}$	$\frac{75}{40}$	$\frac{75}{50}$

R

R



49.07

34+75

35

4.65 44.42

8.11 52.53

+50

+53

+68

118  
125

+81<sup>10</sup>

+89

+95

(B)

49.07

43.5	43.4	42.8	43.0	41.6	41.6	41.5	41.3
$\frac{55}{50}$	$\frac{56}{50}$	$\frac{62}{30}$	$\frac{60}{13}$	$\frac{74}{12}$	$\frac{74}{12}$	$\frac{75}{40}$	$\frac{77}{50}$

43.4	43.5	43.2	42.9	41.6	41.5	41.4
$\frac{56}{50}$	$\frac{55}{40}$	$\frac{58}{29}$	$\frac{61}{11}$	$\frac{74}{12}$	$\frac{75}{40}$	$\frac{76}{50}$

52.53

43.5	43.0	43.6	43.4	42.2	41.6	41.4	41.3	41.3
$\frac{90}{100}$	$\frac{95}{50}$	$\frac{95}{40}$	$\frac{91}{23}$	$\frac{10.3}{14}$	$\frac{10.9}{11}$	$\frac{11.1}{8}$	$\frac{11.2}{40}$	$\frac{11.2}{50}$

Flannel

57' Lt. Flow Line Culvert -  
48 " " "

41.5	41.2	42.7	43.1	41.7	41.2	40.6	40.5
$\frac{110}{50}$	$\frac{113}{40}$	$\frac{9.8}{39}$	$\frac{9.4}{19}$	$\frac{10.8}{11}$	$\frac{11.3}{11}$	$\frac{11.9}{40}$	$\frac{12.0}{50}$

43.0	43.0	39.7	40.7	43.0	42.8	41.7	40.9	40.9	40.8
$\frac{95}{50}$	$\frac{95}{45}$	$\frac{128}{40}$	$\frac{118}{20}$	$\frac{95}{15}$	$\frac{97}{4}$	$\frac{10.8}{11}$	$\frac{11.6}{18}$	$\frac{12.1}{40}$	$\frac{11.7}{50}$

43.0	39.5	40.5	39.8	40.0	39.5	39.3
$\frac{95}{47}$	$\frac{130}{40}$	$\frac{120}{50}$	$\frac{127}{12}$	$\frac{125}{12}$	$\frac{130}{40}$	$\frac{132}{50}$

Sot

(K)



36100 52.53  
An Angle of Wash

36+03

+07

+15

BW

+24

+74

2.99 49.54 19.52

0.82 51.69

9.13 60.82

(B)

52.53 27  
42.4 41.9 40.9 39.5 40.0 39.3 38.4 39.0  
 $\frac{10.1}{150}$   $\frac{10.6}{100}$   $\frac{11.6}{51}$   $\frac{13.0}{50}$   $\frac{12.5}{125}$   $\frac{13.7}{50}$   $\frac{14.1}{100}$   $\frac{13.8}{150}$

43.6 42.8 40.0 40.5 40.0 39.5 39.3  
504  $\frac{9.5}{40}$   $\frac{9.7}{30}$   $\frac{12.5}{24}$   $\frac{12.0}{13}$   $\frac{12.5}{12.5}$   $\frac{13.0}{40}$   $\frac{13.7}{50}$

43.6 42.7 42.7 42.4 43.1 43.2  
 $\frac{8.9}{50}$   $\frac{9.8}{40}$   $\frac{9.8}{1}$   $\frac{10.1}{17}$   $\frac{9.4}{40}$   $\frac{9.3}{50}$

47.0 48.0 48.0 43.4 43.1 43.2 43.1  
 $\frac{5.5}{50}$   $\frac{1.5}{40}$   $\frac{1.5}{36}$   $\frac{9.1}{8}$   $\frac{9.4}{1}$   $\frac{9.3}{40}$   $\frac{9.4}{50}$

See Pg. 9

47.9 49.0 48.6 48.4 47.7 47.1 46.0  
 $\frac{4.6}{50}$   $\frac{3.8}{40}$   $\frac{3.9}{14}$   $\frac{4.1}{1}$   $\frac{4.8}{11}$   $\frac{5.4}{40}$   $\frac{6.5}{50}$

60.8  
52.4 52.2 51.3 50.1 49.1 48.1  
 $\frac{8.4}{40}$   $\frac{8.6}{40}$   $\frac{9.5}{1}$   $\frac{10.7}{27}$   $\frac{11.7}{40}$   $\frac{12.7}{50}$

(R)



37+24

60.82

+74

38+24

00

+74

+77

39+24

+12.3

x section cont.  
on page 31.

Lt

60.8

Rt

28

54.9	55.1	54.7	53.8	55.8	51.2	50.2	44.5
<u>5.9</u>	<u>5.7</u>	<u>6.1</u>	<u>7.0</u>	<u>8.0</u>	<u>9.6</u>	<u>10.6</u>	<u>11.3</u>
50	27	40	13		27	10	50

57.5	57.2	57.1	55.3	52.6	52.7	52.5
<u>3.3</u>	<u>3.6</u>	<u>3.7</u>	<u>5.5</u>	<u>8.7</u>	<u>9.1</u>	<u>8.3</u>
50	40	31		35	40	50

R

R

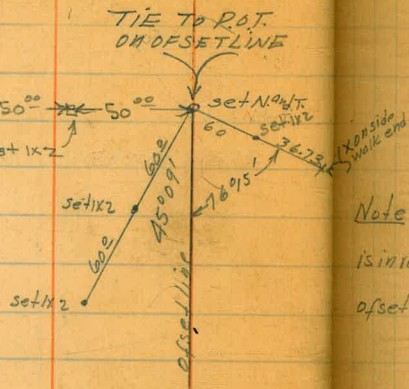


DIVISION ST  
LAUREL TO END OF JOB.

STA DIST

41+51.60

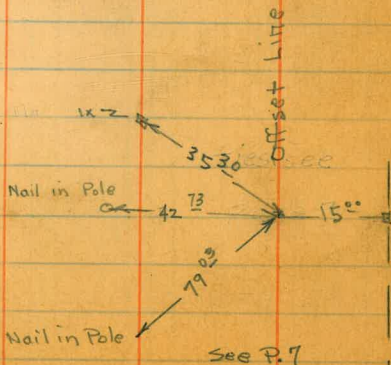
P.O.T. on 15' offset line



570.50

35+81.10

& LAUREL ST.



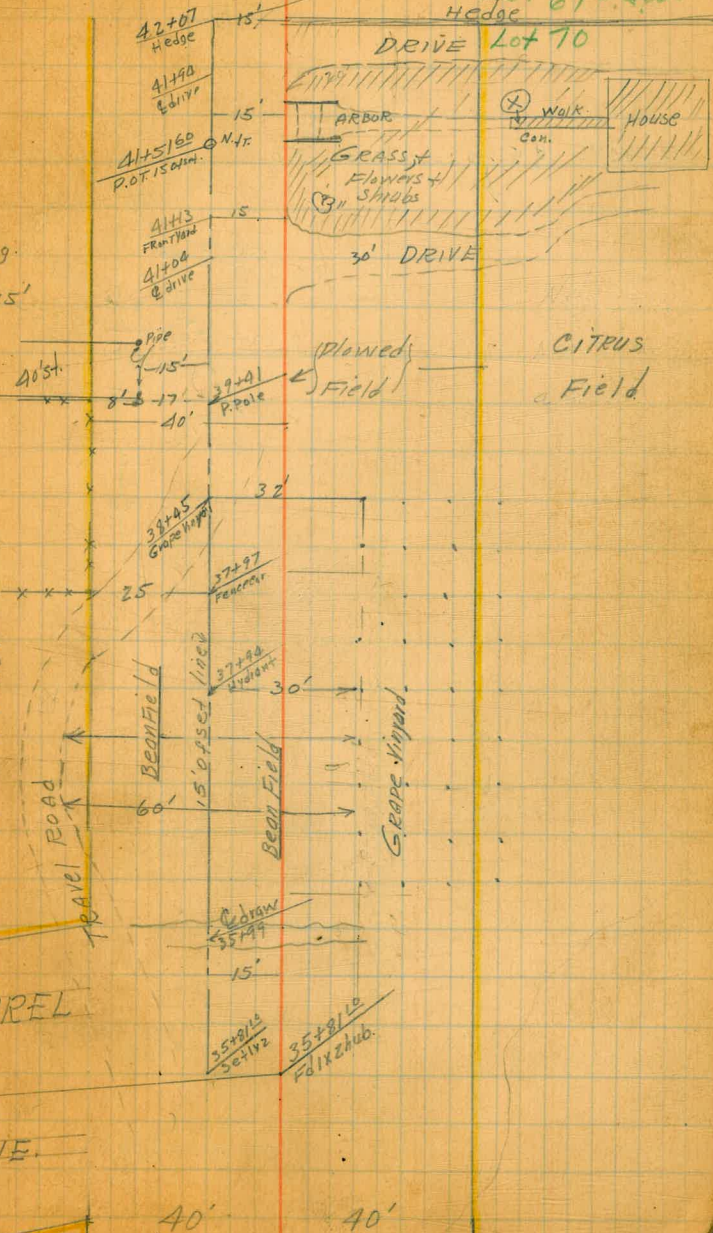
Note topog.  
is in ref to 15'  
offset line

Note ST has lot  
state 30' from door  
both sides.

July 28, 1927  
- G.T. Treadwell -  
0110

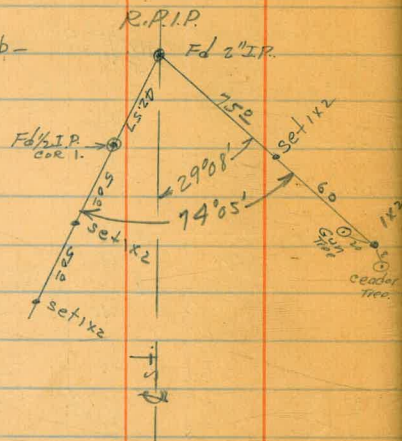
29

Lot 69 c. 200.





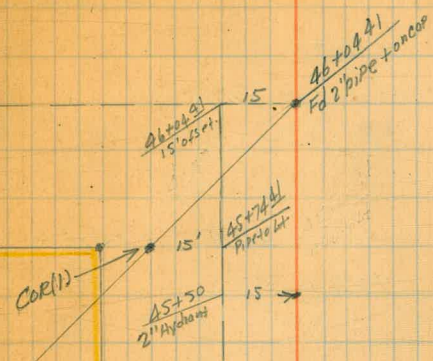
46+04.41  $\phi$  st to South end of Job -



452.81

Ties

46+00  
2" Hydrant



45+50  
2" Hydrant

45+74.41  
Pine tree

ST

45+50  
Hydrant

17'

DIVISION

44+15  
Willow tree

43+60  
Gum tree

15'

15'

Q

43+10  
Gum tree

15'

42+80  
Gum tree

15'

Beon Field



July 28, 1927.  
G. T. Freedwell. 31  
Rt.

X SECTIONS.

STA			ELEV.
B.M.			49.52.
	11.17	60.69	
X sections cont. from page 28			
38+00			
		0.14	60.55
	12.56	73.11	
+50			
+78			
39+00			
		0.20	72.91
	12.73	85.64	
+50			
40+00			
+50			
		0.66	84.98
	5.13	90.11	
41+00			
+50			

OK

Lt. see page 9.

60.69T									
60.6	59.4	58.1	58.2	57.5	56.4	55.3	55.0		
$\frac{0.1}{50}$	$\frac{1.3}{40}$	$\frac{2.6}{33}$	$\frac{2.5}{20}$	$\frac{3.2}{00}$	$\frac{4.3}{10}$	$\frac{5.4}{40}$	$\frac{5.7}{50}$		
73.11T									
64.2	64.6	64.1	63.3	64.0	65.3	66.6	67.3		
$\frac{8.9}{50}$	$\frac{8.5}{40}$	$\frac{9.0}{15}$	$\frac{9.8}{14}$	$\frac{9.1}{00}$	$\frac{7.8}{20}$	$\frac{6.5}{40}$	$\frac{5.8}{50}$		
68.5	68.7	69.6	69.3	68.2	68.4	69.2	70.2	70.6	
$\frac{4.6}{50}$	$\frac{4.4}{40}$	$\frac{3.5}{28}$	$\frac{3.8}{15}$	$\frac{4.9}{11}$	$\frac{4.7}{00}$	$\frac{3.9}{13}$	$\frac{2.9}{40}$	$\frac{2.5}{50}$	
70.8	71.7	71.7	71.4	70.5	70.4	71.0	70.4	72.0	
$\frac{2.3}{50}$	$\frac{1.4}{40}$	$\frac{1.4}{35}$	$\frac{1.7}{15}$	$\frac{2.6}{11}$	$\frac{2.7}{00}$	$\frac{2.1}{20}$	$\frac{1.7}{40}$	$\frac{1.1}{50}$	
85.64T									
75.1	75.2	75.4	74.7	73.6	74.6	75.6	76.0		
$\frac{10.5}{50}$	$\frac{10.4}{40}$	$\frac{10.2}{20}$	$\frac{10.9}{00}$	$\frac{12.0}{30}$	$\frac{11.0}{50}$	$\frac{10.0}{40}$	$\frac{9.6}{50}$		
80.4	80.3	79.9	78.7	78.4		78.3	78.6		
$\frac{5.2}{50}$	$\frac{5.3}{40}$	$\frac{5.7}{30}$	$\frac{6.9}{50}$	$\frac{7.2}{00}$		$\frac{7.3}{40}$	$\frac{7.0}{50}$		
85.2	85.2	85.1	83.7	82.9	81.9	81.3	80.7	80.6	80.4
$\frac{0.4}{50}$	$\frac{0.4}{40}$	$\frac{0.5}{33}$	$\frac{1.9}{22}$	$\frac{2.7}{70}$	$\frac{3.7}{00}$	$\frac{4.3}{07}$	$\frac{4.9}{21}$	$\frac{5.0}{40}$	$\frac{5.2}{50}$
90.11T									
87.3	87.3	87.1	85.2	84.1	83.5	83.4	83.3		
$\frac{2.8}{50}$	$\frac{2.8}{40}$	$\frac{3.2}{31}$	$\frac{4.9}{00}$	$\frac{6.0}{20}$	$\frac{6.6}{30}$	$\frac{6.7}{40}$	$\frac{6.8}{50}$		
86.8	87.1	87.2	86.7		85.8		85.6		
$\frac{3.3}{50}$	$\frac{3.0}{40}$	$\frac{2.9}{31}$	$\frac{3.4}{00}$		$\frac{4.3}{40}$		$\frac{4.5}{50}$		



Division Cont.

32

sta	elev
4200	90.11
+50	
43100	
+50	

L+	Q	R+
85.4 4.7 50	85.5 4.6 20	85.7 4.4 29
83.1 7.0 50	83.2 6.9 40	83.4 6.7 37
80.5 9.6 50	80.8 9.3 40	81.1 9.0 30
78.0 1.2 50	78.3 1.8 40	78.8 1.3 30

1202 78.09

44100	0.44	78.53
+50		
45100		

74.8 8.7 50	75.8 2.7 40	76.1 2.0 28	76.3 2.2 7.0	78.53 M 72.7 6.0	77.5 1.3 20	77.6 0.7 40	78.0 0.5 50
72.6 5.9 50	73.1 5.4 40	73.3 5.2 27	73.2 5.3 40	74.2 4.3 0.0	73.6 4.9 5.0	73.9 4.6 40	74.2 4.3 50
68.3 10.2 50	68.5 10.0 40	69.4 9.1 25	69.5 9.0 2.0	70.9 8.1 0.0	70.1 8.4 6.0	70.0 8.5 28	69.3 9.2 40

45+50	0.69	67.05
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65.6 12.9 50	65.8 12.7 40	65.8 12.7 22	66.7 12.8 4.0	66.1 10.2 0.0	65.4 13.7 8.0	64.8 13.7 26	63.9 14.2 40	62.2 16.3 50	59.5 19.0 70
--------------------	--------------------	--------------------	---------------------	---------------------	---------------------	--------------------	--------------------	--------------------	--------------------

45+74.91 West side 60' STREET.

67.05 M										
52.5 14.1 200	53.6 14.0 150	54.0 13.9 150	60.3 10.8 100	60.9 10.7 100	63.6 10.3 100	63.7 10.3 100	63.5 10.2 100	64.0 10.1 100	64.2 10.0 100	63.5 10.0 100

46+04.91 Q 60' STREET.

52.4 14.6 200	53.9 14.1 150	56.5 12.5 100	60.5 10.5 50	61.8 10.3 30	62.5 10.2 0.0	62.0 10.0 18	59.8 10.0 40	58.4 9.8 50	59.4 10.0 70
---------------------	---------------------	---------------------	--------------------	--------------------	---------------------	--------------------	--------------------	-------------------	--------------------

46+34.91 East side 60' street.

51.4 15.3 200	52.0 15.0 150	52.7 14.3 100	57.6 10.0 50	57.8 9.2 40	62.0 10.0 0.0	62.3 9.7 12	60.5 10.0 40	59.4 10.0 50	55.2 11.8 66	57.7 16.3 85
---------------------	---------------------	---------------------	--------------------	-------------------	---------------------	-------------------	--------------------	--------------------	--------------------	--------------------



46+50 Box to Lt. elev on top 18x18" con Box  
67.05

46+65

492

47+27

262 57.28

+35

Box to Lt. 18x18" con. 2" walls

+50

+60

WASH-

+87

Bottom of wash-

48+00

+28

+50

48+64

49+00

10.50 66.93

12.19 77.25

0.85 56.43

1.87 65.06

0.52 76.73

Lt.

¢

Rt.

33

16.5	49.0	51.0	52.5	67.05	62.2	60.4	59.0	57.8
127	18.0	16.0	14.5	62.0	4.8	6.6	8.0	12.2
	70	50	40	70	24	40	50	70
	43.5	49.5	56.8	58.5	59.3	59.0	58.9	51.5
	18.5	17.5	12.2	8.5	7.7	8.0	12.1	15.5
	50	40	90	13	30	40	50	70
43.6	43.5	45.6	49.7	51.9	57.8	50.3	48.0	
20.4	23.5	21.9	17.3	18.1	13.2	16.7	19.0	
60	50	33	00	19	40	50	70	
				14.5				
				50				

11.2  
00

18.8  
27

2.0  
00

17.8  
00

16.6  
00

64  
50

11.5  
00

2.7 Bottom wash  
50

16.6  
00

15.7  
00

set BM. ON R.R. P.P OUT 75' 40' Rt. sta 46+40



			elev.
1184	88.57		76.73
		5.39	83.18
0.41	83.59		
		10.71	72.88
0.30	73.18		
		12.95	60.23
0.49	60.72		
		11.23	59.49
			59.52

BM. Page 9 —



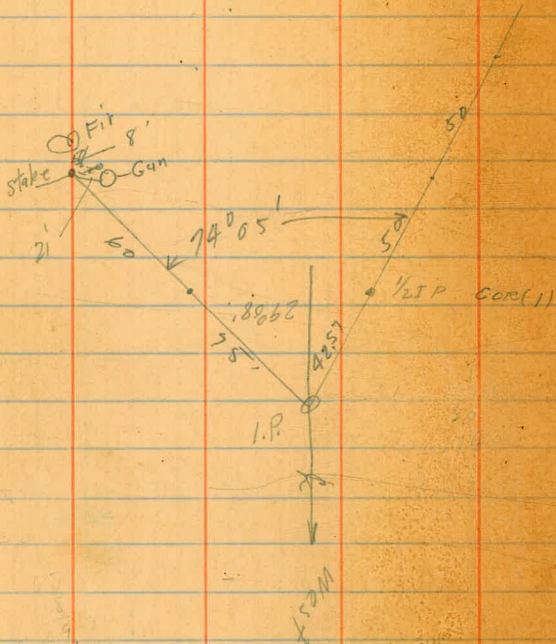
35



46404.41  
30  
45799.1

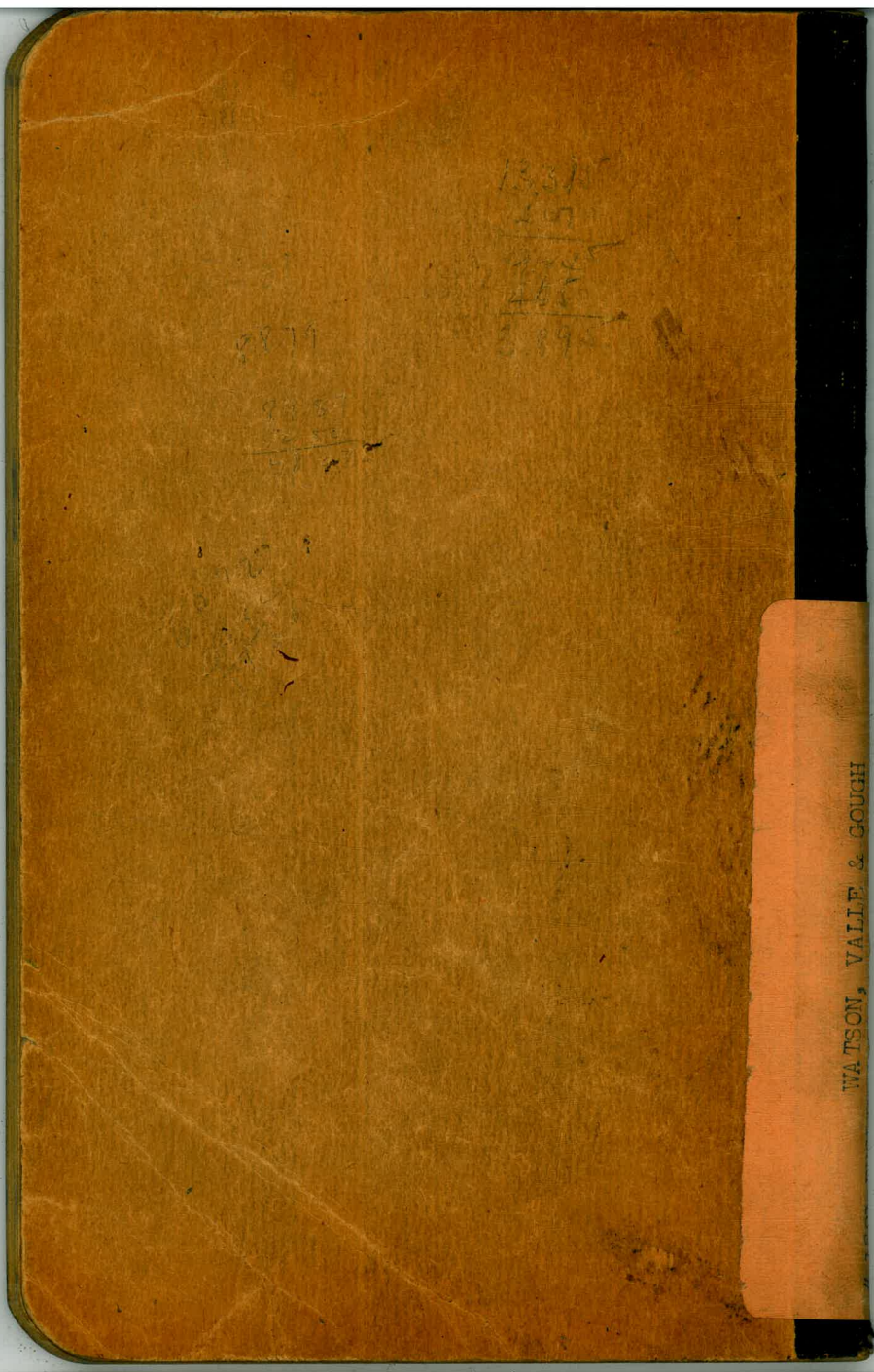
# DIVISION

46404.41  
91 + 51.60  
45281



35481.10  
28 + 58.79  
174431





2879

1351  
20  
205  
265  
339

WATSON, VALLE & GOUGH