

NAME National Ave Extension

Job 123 Course _____ Party _____

Line change thru Reads.

1901

184

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

MICROFILMED

DEC 30 1964

X Sects

Line Change, Natl Ave
Thru Mr. Reeds Land

1-19

"G" Line BM's

20-22

" X-Secs

23-28

Line Chg. X-Secs

126+09.08 to 135+27.10=
134+69.58

29-32

Grade Stks at Potato Chip Factory

33

Sept. 30, 1926.
 Peterman
 Todd
 Spaulding
 Elev.

1.

Sta.	+ H.I.	- Elev.
B.M.		112.96
	0.85 113.81	
T.P.		11.75 102.06
	0.15 102.21	
B.M.		12.08 90.13
	5.37 95.50	

Left. W I Right.
 Nail in Power Pole 5' ± Sta. 8+11

H.I. = 95.50

0+00	4	92.3 3.33 200	41.7 3.80 1.50	41.6 3.92 1.00	41.9 3.62 .71	42.1 3.4 .50	41.9 3.6 .30	90.8 4.7	90.0 5.5 30	89.9 5.6 50	90.2 5.2 100	90.1 4.8 150	90.1 5.4 200
- 0+50													
- 0+67													
- 1+00													
- 1+50													
- 2+00													
- 3+00													

"Reversed"
 Left = Right
 etc.

Sta. + H.I. - Elev.

-0+29 95.50

0+11

0+15

0+50

1+00

1+50

2+00

2+50

3+00

Double 10"
Wood Culvert.

0.32 95.18

7.30(?) 102.48

Left. \$ Right.

88.6
6.95
13

89.4
6.10
8

91.7 91.3 91.0 90.9 90.3 90.3
3.8 4.2 4.5 4.6 5.2 5.2
150 100 50 30 30 30

91.0 90.9 90.5 90.1
4.5 4.6 5.0 5.4 ← Bldg.
30 21 23

91.3 91.3 91.7 91.9
4.2 4.0 3.8 3.6
30 20 30 30

93.2 93.7 93.1 93.1 92.2 93.9
2.3 1.8 2.4 2.4 1.3 1.6
30 20 19 5 30 30

(H.I. = 102.48)

95.7 95.7 95.1 95.3 94.8 95.7 96.5 97.2 95.7 95.7
6.8 6.8 7.4 7.2 7.7 6.8 6.0 5.5 6.8 6.8
30 21 18 13 4 3 4 12 30 30

97.1 97.0 96.6 96.8 96.3 97.5 97.7 97.0 97.1
5.4 5.5 5.9 5.7 6.2 5.0 4.8 5.5 5.4
30 23 19 13 3 2 12 30 30

96.0 98.4 98.5 99.3 99.4 97.0 97.4 96.8
Water } 6.5 4.1 4.0 3.2 3.1 5.5 5.1 5.7
Meter Box } 55 30 6 2 5 12 30

Sta + H.I. - Elev. Left ϕ Right.

3+25 102.48 ϕ 95.2 95.1 96.0 96.7 97.4 97.5 98.3 99.0
 7.3 7.4 6.5 5.8 5.1 5.0 4.0 3.5
 200 100 50 30 20 4 30

3+50 97.6 98.2 98.2 98.8 99.9 100.3
 4.9 4.3 4.3 3.7 2.6 2.2
 30 22 6 2 30

4+00 101.9 101.4 100.8 101.3 101.1 101.9 102.5
 0.6 1.1 1.7 1.2 1.4 0.6 0.0
 30 14 6 5 4 30

T.P. 0.44 102.04 (102.06)

(124.8)

12.24 114.30

1.34 112.96

4+50 105.1 104.7 103.6 104.7 105.2 105.1
 9.2 9.6 10.7 9.6 9.1 9.2
 30 15 7 5 30

5+00 109.1 108.0 107.0 108.2 108.3 107.7 108.6
 5.2 6.3 6.7 6.1 6.0 6.6 5.8
 30 22 6 5 18 30

5+50 110.3 109.1 109.0 107.9
 4.0 5.2 5.3 6.4
 30 21 30

6+00 111.9 110.7 110.1 109.2
 2.4 3.6 4.2 5.1
 30 23 30

6+34 112.5 112.4 111.6 111.2 108.9
 1.81 1.94 2.7 3.1 5.4
 55 30 30 30
 Curb Curbs
 Line Meridian Ave. Gutter

Sta. + H.I. - Elev.
114.30

6+50

6+86

B.M.

4.80 117.76

7+00

7+50

2.90 115.86

Curb 3.50 117.36 Stake 34, 30 Lt.

Gutter 4x 111.7

8+00

1/25/27
Cuts

Curb 4.5x 111.34 Stake 36, 30 Lt.

Gutter 5.0 110.9

Check on Curb Elev's Meridian Ave

+50

Left. ♀ Right.

111.8 111.2 109.3 107.4 107.0
2.5 3.1 5.0 6.9 7.3
50 30 30 50

111.7 111.2 110.6 109.3 108.8 107.0 106.0
2.64 3.07 3.7 5.0 5.5 7.3 8.3 112.8
50 30 30 20 5 30 Left { 1.50
Curb Gutter } 100
H.I. = 117.76

109.7 108.9 107.6 107.4 106.3
8.1 8.9 10.2 10.4 11.5
30 20 16 30

108.4 109.2 108.8 108.3 107.9
9.4 8.6 9.0 9.5 9.9
30 23 21 30

110.4 110.8 110.1 110.5 110.3 111.2 111.3
7.4 7.0 7.7 7.3 7.5 6.6 6.5
30 23 19 13 6 30

113.4 113.4 112.7 113.4 114.2 113.9 114.3
ΔΔ ΔΔ 5.1 ΔΔ 3.6 3.9 3.5
30 21 21 6 5 30

115.0 114.6 115.5 115.0 114.9 115.7 115.6 115.2
4.8 3.2 2.3 2.8 2.9 2.1 2.2 2.6
30 23 20 13 7 6 30

9

1/25/27

9+50 117.76
 095 116.81
 10 6.32 123.17
 Approx ± S± to North

+50
 11

+50

15

IP 1.57 121.60
 11.29 132.89
 B.M. 3.56 129.33 (129.31)
 3.56 132.87

12+50
 12+77

Lt. Rt. 5.

116.5 116.7 116.2 116.5 116.3 116.8 116.8 116.4
 $\frac{1.3}{30}$ $\frac{1.1}{27}$ $\frac{1.6}{21}$ $\frac{1.3}{14}$ $\frac{1.6}{7}$ $\frac{0.9}{6}$ $\frac{1.0}{-}$ $\frac{1.4}{30}$

115.9 118.6 118.1 117.7 117.5 117.2 117.7 118.7
 $\frac{7.3}{200}$ $\frac{4.6}{130}$ $\frac{5.1}{100}$ $\frac{5.5}{50}$ $\frac{5.7}{30}$ $\frac{6.0}{6}$ $\frac{5.5}{-}$ $\frac{4.5}{30}$

116.6 117.6 117.6 117.2 118.8 119.1
 $\frac{6.6}{30}$ $\frac{5.6}{25}$ $\frac{5.0}{14}$ $\frac{6.0}{6}$ $\frac{4.4}{-}$ $\frac{4.1}{30}$

118.2 117.4 117.3 117.8 118.2
 $\frac{5.0}{30}$ $\frac{5.8}{20}$ $\frac{5.9}{5}$ $\frac{5.4}{-}$ $\frac{5.0}{30}$

117.8 118.2 117.8 118.3 119.2
 $\frac{5.4}{30}$ $\frac{5.0}{27}$ $\frac{5.4}{5}$ $\frac{4.9}{-}$ $\frac{4.0}{30}$

121.4 121.7 121.1 121.5 120.8 121.0 121.3
 $\frac{1.8}{30}$ $\frac{1.5}{21}$ $\frac{2.1}{19}$ $\frac{1.7}{11}$ $\frac{2.4}{4}$ $\frac{2.7}{-}$ $\frac{1.9}{30}$

On Water Pipe 25' ± Lt. 12+20
H.I. = 132.87

124.4 123.8 124.3 123.8 124.0 124.1
 8.5 9.1 8.6 9.1 8.9 8.8
 30 20 11 4 30

125.3 125.4 126.4 126.1 126.4 125.8
 7.6 7.5 6.5 6.8 6.5 7.1
 30 20 6 2 30

Sta. + H.I. - Elev.

Left. & Right.

13+00 132.87 & Upper St.

126.7	126.7	126.5	126.5	126.4	126.9	127.9	128.1
7.2	6.2	6.4	6.4	6.5	6.0	5.0	4.8
200	150	100	50	30		25	30

13+36 & Upper St.
18' wide.

128.6	128.1	128.4	128.2	128.3	122.4	126.6	122.1	117.7
4.3	4.8	4.5	4.7	4.6	5.5	7.4	10.8	15.2
50	24	15		22	50	100	150	200

13+50

128.1	127.7	127.8	127.5	128.1	129.8
4.8	5.2	5.1	5.4	4.8	3.1
-40	30		11	30	50

13+80

126.1	125.7	125.2	124.9	124.9	126.8	126.7
6.8	7.2	7.7	8.0	8.0	6.1	6.2
40	30	20		12	30	40

14+00 11.33 121.54

123.4	122.9	123.0	122.5	121.7	123.6	124.0
9.5	10.0	9.9	10.4	11.2	9.3	8.9
40	30	16		13	30	40

1.54 123.08

H.I. = 123.1

14+30

119.3	118.7	118.5	119.0	118.2	119.8	119.7
3.8	4.4	3.6	4.1	4.9	3.3	3.4
40	25	11		13	30	40

14+50

116.3	116.1	115.5	115.1	117.0	117.2
6.8	7.0	7.6	8.0	6.1	5.9
40	30		10	30	40

T.P. 11.17 110.91

0.28 ~~111.19~~
112.19 ck.

111.91 ck.

Sta. + H.I. - Elev.

14+90 ~~111.19~~
112.19

15+00

15+50

15+78

16+00

16+50

17+00

T.P.

17+42

0.95 ~~100.75~~
101.75 CK

11.39

~~100.50~~ CK.
99.80

Left.

112.19

±

Right.

110.3 110.7 109.9 109.0 111.6 112.0 111.9
1.9 1.5 1.3 3.2 0.6 0.2 0.4
40 30 19 14 30 40

110.0 109.0 109.6 108.3 110.0 110.2 110.1
2.2 3.2 2.6 3.9 2.2 2.0 2.1
50 36 22 19 30 40

104.2 103.3 102.9 101.9 101.2 100.6 100.9
Gully 8.0 8.9 9.3 10.3 11.0 11.6 11.3
50 40 30 15 22 30

104.0 102.7 99.1 97.8 97.9
8.2 9.5 13.1 14.4 14.3
40 30 30 40

106.3 104.7 99.9 96.7 95.7 96.2
5.9 7.5 12.3 15.5 16.5 16.0 ← Gully
40 30 30 33 40

106.1 105.3 102.1 100.4 98.2 97.6
6.1 6.7 10.1 11.8 14.0 14.6
40 30 16 30 40

99.9 99.7 101.1 101.1 100.8 101.1 101.5
12.3 12.5 11.1 11.1 11.4 11.1 10.7
40 30 10 11 30 40

H.I. = 101.75

91.9 94.2 94.5 96.9 92.9 98.2
9.9 7.6 7.0 4.9 3.9 3.6
40 23 7 30 40

Sta	+	H.I.	-	Elev.
17+50		100.75 101.75		
17+62				
18+50				
T.P.				111.91
	1.22	113.13 112.13		110.91
T.P.			12.03	101.10
	0.23	101.33 100.33		100.10
T.P.			12.02	89.31
				88.31
				96.23
	8.22	104.45 103.45	5.10	95.23
B.M. "Z"			0.61	103.84
				102.84
T.P.				89.31
	2.54	91.85 90.85		88.31
18+00				
18+15				

Left.	€	Right.
89.5 92.9 92.0 94.7 95.2 97.1		
12.3 9.9 9.0 7.1 5.6 4.7		
40 23 10		25 40
87.5 88.8 90.0 93.4 94.1		
14.3 13.0 11.2 8.4 7.7		
42 25		30 40
95.0 94.0 89.9 87.2 84.5 81.8		
6.8 7.8 11.9 14.6 17.3 20.0		← Gully
40 30		17 30 50

Rock in Mound; W. side big Gully.
 " ; E. " " "

Red-head in base of Eucalyptus at Potatoe-Chip Factory
 (H.I. = 91.85)

Gully →	82.0	82.8	83.1	83.2	83.9	84.9
	9.0	9.1	8.8	8.7	8.0	2.0
	60	45	23		23	50
	84.4	85.0	83.7	82.2	81.5	84.4
	7.5	6.9	8.2	9.7	10.4	7.0
	50	30	16		30	50

Sta.	+	H.I.	-	Elev.
T.P				96.23
		103.23		95.23
18+70	7.00	102.23		

18+70

19+00

Left

±

Right.

9.

100.5	99.2	95.5	95.0	92.6	90.9	84.9	82.9
2.7	4.0	7.7	8.2	10.6	12.3	18.3	20.8
44	30		8	23	30	50	75

(104.2)?	104.2	103.0	99.8	96.5	91.5		
-1.0	0.2	3.4	6.7	11.7			
40	25		32	50			

Oct. 1, 1926.

Peterman
Todd
Spaulding.

Elev.

~~103.84~~

102.84

See Sheet 8

10.

Sta. + H.I. -

B.M. "Z"

2.73 106.57
105.57

19+35

19+50

19+77

20+00

20+20

20+25

20+40

20+50

Left

±

Right

<u>105.3</u>	<u>104.0</u>	<u>99.9</u>	<u>98.3</u>	<u>94.1</u>
1.3	2.6	6.7	8.3	12.5
43	30		30	50

<u>105.5</u>	<u>104.9</u>	<u>102.1</u>	<u>101.5</u>	<u>99.5</u>	<u>97.3</u>
1.1	1.7	4.5	5.1	7.1	9.3
40	30	12		36	50

<u>107.0</u>	<u>105.6</u>	<u>104.9</u>	<u>102.7</u>	<u>99.6</u>	<u>98.1</u>
W. edge Factory →	1.0	1.7	3.9	7.0	8.5
	45	22		30	40

<u>105.2</u>	<u>104.8</u>	<u>102.4</u>	<u>99.2</u>	<u>97.4</u>	
Bldg.	1.4	1.8	4.2	7.4	9.2
	22	10		30	45

<u>104.4</u>	<u>103.6</u>	<u>98.6</u>	<u>97.3</u>	<u>96.4</u>	
	2.2	3.0	8.0	9.3	10.2
	6		30	43	48

<u>104.4</u>	<u>103.6</u>	
E. edge Factory →	2.2	3.0
	6	

<u>106.6</u>	<u>106.6</u>	<u>104.3</u>	<u>103.6</u>	<u>102.4</u>	<u>100.5</u>	<u>99.9</u>	<u>88.1</u>
0.0	0.0	2.3	3.0	4.2	6.1	11.7	18.5
40	30	8		12	19	30	50

<u>106.3</u>	<u>104.7</u>	<u>103.3</u>	<u>103.1</u>	<u>102.1</u>	<u>99.6</u>	<u>99.8</u>	<u>88.0</u>
0.3	1.9	3.3	3.5	4.5	7.0	11.8	18.6
30	10	6		10	18	30	46

Sta. + H.I. - Elev.

~~106.57~~
105.57

20+60

20+79

20+90

21+10

21+50

22+00

22+15

22+30

T.P.

0.21

~~95.29~~
94.29

11.49

~~95.08~~
94.08

Left. ♀ Right

105.5 104.3 103.1 101.9 99.8 97.4 94.3 85.9
1.1 2.3 3.5 4.7 6.8 9.2 12.3 21.2
30 14 7 16 25 33 50

104.8 102.5 101.3 98.2 96.4 90.6 84.1
1.8 4.1 5.3 8.4 10.2 16.0 22.5
30 6 15 20 30 50

104.1 103.0 102.8 98.8 94.8 91.1 84.9
2.5 3.6 5.8 7.8 11.8 15.5 21.7
30 10 10 22 30 50

103.0 101.6 99.6 99.6 98.1 96.3 89.4 87.6
3.6 5.0 7.0 7.0 8.5 10.3 17.2 19.0
30 13 12 8 6 30 40

103.9 101.9 97.9 96.8 90.3 85.8
3.2 4.7 8.7 9.8 16.3 20.8
30 9 3 20 40

101.6 99.7 97.4 94.9
5.0 6.9 9.2 11.7
40 30 18 8

98.8 98.2 97.3
7.8 8.4 9.3
40 30 25

96.7 96.1
9.9 10.5
40 35

10.0 Left Sta 22+00

Sta. + H.I. - Elev.

Left.

±

Right.

22+00

95.29
94.29

92.5	85.1	83.3
2.8	10.2	12.0
	30	40

22+15

T.P.

88.82

11.73

83.56

~~82.56~~

Red-head Sta. 23+00.

91.1	89.6	86.7	83.3	81.8
4.2	5.7	8.6	12.0	13.5
	8	18	30	40

22+30

5.26

87.82

87.7	84.1	81.7	81.3	80.7	80.7	80.5	80.7	80.7
1.1	4.7	7.1	7.5	8.1	8.1	8.3	8.4	8.1
24	16	3		20	30	40	50	100

← Gully →

Gully

82.8	82.2	81.3
6.0	6.6	7.5
100	50	00

22+50

(94.5) 82.1
-5.7
50

87.8	83.4	81.6	81.2	82.3	82.3	82.3	83.7	83.2	82.9
1.0	5.4	7.2	7.6	6.5	6.5	6.5	5.1	5.6	6.4
40	30	20	7	6		3	6	30	40

23+00

Cont'd on Pg. 23

83.7	83.6	81.6	82.8	83.5	83.0
5.1	5.2	7.2	6.0	5.3	5.8
40	28	20	15		30

23+15³⁶

B.C.

83.9	83.4	80.7	82.3	83.6	83.2
4.9	5.4	8.1	5.5	5.2	5.6
40	30	22	20		30

23+50

Cont'd

84.2	84.3	82.8	82.7	83.5
4.6	4.5	5.0	5.1	5.3
30	3	2		30

Sta + H.I. - Elev.

24+00

~~88.82~~
87.82

24+30

fail

24+50

T.P.

11.90
98.67
~~97.67~~
2.05
86.77
~~85.77~~

24+77

25+00

T.P.

T.P.

6.86
91.81
90.81
97.17
~~96.17~~
1.50
107.72
~~106.72~~
10.55

25+50

fail

25+88

26+00

T.P.

0.09
107.63
~~106.63~~

Left. \$ Right

84.8 84.8 84.0 84.0 83.8
4.0 4.0 4.8 4.8 5.0
30 11 10 30

fail

85.3 84.3 84.9 85.8 85.8
3.5 4.5 3.9 3.0 3.0
30 20 30 40

85.3 84.8 85.6 87.8 86.6 86.0
3.5 4.0 3.2 1.0 -2.2 -2.8
30 13 12 30 40

Rock 8.0 Right of Sta. 24+50.

85.5 85.7 86.7 86.7 88.0 90.3 92.5 95.0 96.1
13.2 130 120 120 10.7 8.4 6.2 3.7 2.6
45 38 35 20 8 9 30 40

86.4 90.7 91.5 93.1 95.0 92.8 94.3 96.7
12.3 8.0 7.2 5.6 3.7 0.9 -0.6 -2.0
60 39 30 12 17 30 40

Red-head in top 2nd Post from Fence Corner.

87.9 91.4 95.4 99.4 101.8 106.0 108.2 109.8
19.8 16.3 12.3 8.3 5.9 1.7 -0.5 -2.1
50 35 24 10 18 30 40

87.4 89.9 97.7 103.6 107.5 111.5 113.7 117.3
20.3 17.8 10.0 4.1 0.2 -3.8 -6.0 -9.6
55 45 30 17 15 30 48

88.9 96.5 99.7 103.7
18.8 11.2 8.0 4.0
48 30 24 16

fail

Sta.	+	H.I.	-	Elev.
T.P.				107.63 106.62
	8.92	116.55 115.55		
26+25				
26+50				
28+00				
28+50				
T.P.				104.42
	1.00	105.42 104.42	12.13	103.42
		95.40		94.85
	0.55	94.40	10.57	93.85
			3.43	91.97 90.81 (T.P.) (90.97) 91.97
B.M. "Z"				103.84 102.84 See Sheet 8
	0.14	103.98 102.98		
T.P.			8.87	95.11 94.11 (94.08 Sh. #11)
	1.79	96.90 95.90		
T.P.			10.05	86.85 85.85 (85.77 Sh. #13)
	5.23	92.08 91.08		
T.P.			0.19	91.89 90.89 (90.81)

Left

Left @ Right

89.6	90.0	109.9	105.8	114.6	116.1
27.0	26.6	12.2	10.7	2.4	0.5
50	42	7		24	40

99.9	106.9	112.1	114.7
16.7	9.7	4.5	1.9
22	35	50	

106.8	110.6	111.6
9.8	6.0	5.0
16	30	40

105.6	109.6
11.0	7.0
22	40

Left

Red-head in Fence Post. Set. See Sh. # 13.

Sta + H.I. - Elev.
 T.P. 6.21 98.10 90.89
 T.P. 1.08 97.10 97.02
 26+50 96.02

Left. & Right.

89.4 87.7 87.8 87.8 95.2
 8.7 10.4 10.3 10.3 2.9
 40 25 22 18 13

(Handwritten scribble)

27+00
 27+50 12.07 109.09 108.09 108.13 107.13
 T.P. 0.96

90.1 90.1 87.9 87.8 92.6 99.4 96.5 (100.0) (107.8)
 8.0 8.0 10.2 10.3 5.5 3.7 1.6 -2.5 -9.7
 40 24 17 14 8 8 22 40

90.7 90.7 88.1 88.1 90.8 97.1 (99.3) (107.0) (108.0)
 7.4 7.4 10.0 10.0 7.3 1.0 -1.2 -8.9 -10.5
 50 41 38 32 29 7 30 40

28+00

91.6 91.8 93.8 99.1 101.0 108.1 (110.9) (114.7)
 17.5 17.3 15.3 10.0 7.5 1.0 -1.8 -2.6
 50 40 30 12 21 33 40

28+50

94.0 96.6 102.4
 15.1 12.5 6.7
 49 30

29+00

100.1 98.3 97.0 95.1 95.1 96.4 99.3 105.5 108.0
 9.0 10.8 12.1 14.0 14.0 12.7 9.8 3.6 1.1
 40 30 22 20 16 14 30 40

29+45

(Gully)

92.3 95.1 97.3 98.3 100.9
 16.8 14.0 11.8 10.8 8.2
 100 50 50 100

29+50

108.1 107.3 98.8 92.3 100.4 103.0 105.6
 1.0 1.8 10.3 11.8 8.7 6.1 3.5
 40 30 7 13 30 40

(Handwritten scribble)

Sta. + H.I. - Elev.

30+00

~~109.09~~
~~108.09~~

30+50

11.78 ~~118.91~~
119.91

T.P.

0.17 ~~118.74~~
119.74

30+50

30+75

31+00

31+09

(Gully)

31+50

10.93 ~~129.67~~
130.67

T.P.

0.95 ~~128.72~~
129.72

31+75

Left e Right.

~~111.6~~ 109.1 105.0 101.3 103.0 98.7 103.3 106.6
-2.5 0.0 4.1 7.8 6.1 10.4 5.8 2.5
40 30 8 12 26 34 50

109.1 107.0 103.5 102.9 103.7 106.0
0.0 2.1 5.6 8.2 5.4 3.1
16 30 38 43 50

116.6 112.5 112.1
3.3 7.4 7.8
40 24 20

fold

119.1 117.2 115.4 112.3 105.9 103.3 105.3
0.8 2.7 4.5 7.6 14.0 16.6 14.6
40 30 22 30 34 38

118.9 115.9 114.1 111.8 110.5 111.5 112.0
1.0 4.0 5.8 8.1 9.4 8.4 7.9
40 26 10 8 30 40
Gully

115.9 115.2 112.0 108.3 104.9 100.9
4.0 4.7 7.9 11.6 15.0 18.0 (Intersection
40 25 26 28 60 of Gully
29+45.

116.4 116.7 117.9 119.2 118.8 117.9
3.5 3.2 2.0 0.7 1.1 2.0
30 10 14 30 40

Hub - P.C. 33+52.71.

118.1 118.3 121.2 122.3 122.6 120.8 119.7
12.6 12.4 9.5 8.4 8.1 10.0 11.0
40 30 12 15 30 40

Sta. + H.I. - Elev.

~~130.67~~
129.67

32+00

119.4	120.3	122.1	123.1	121.2	120.0
11.3	10.4	8.6	7.6	9.5	10.7
40	30	15		30	40

32+50

125.6	125.5	125.1	124.7
5.1	5.2	5.6	8.0
30		32	50

33+00

fail

126.7	126.2	126.7	128.0	127.1
4.0	4.5	4.0	2.7	3.6
40	30		30	40

33+52.4

139.24
9.52 ~~138.30~~

B.C.

129.2	129.7	129.8	129.6
1.5	1.0	0.9	1.1
30	20		30

33+75

fail

132.1	132.0	130.8	130.8	131.2	130.2
7.1	7.2	8.4	8.4	8.0	9.0
40	30	10		16	30

34+00

130.8	130.7	130.8	130.0
8.4	8.5	8.4	9.2
30		20	30

34+50

fail

130.6	130.9	130.8
8.6	8.3	8.4
30		30

35+00

131.0	133.0	132.7	133.0	134.8	134.4
8.2	6.2	6.5	6.2	4.4	4.8
38	16		13	35	45

Sta. + H.I. - Elev.

35+25

39.24
138.30

35+50

35+75

36+00

36+50

37+00

37+23

37+50

T.P.

134.50
4.74 133.56

Left. ϕ Right.

132.0 132.4 133.5
7.2 6.8 5.7
30 30

132.8 133.6 135.2 134.3 134.9 134.8
6.4 5.6 4.0 4.9 4.3 4.4
40 30 13 25 35

133.7 134.7 136.2 136.2
5.5 4.5 3.0 3.0
30 21 30

134.0 134.8 135.6 136.2 135.6
5.2 4.9 3.6 3.0 3.6
30 11 10 30

134.4 134.2 134.2
4.8 5.0 5.0
30 30

135.0 135.2 134.4 134.9
4.2 4.0 4.8 4.3
30 18 30

135.1 134.7 136.2
4.1 4.5 3.0
30 30

134.6 135.2 136.8 136.9
4.6 4.0 2.4 2.3
30 10 30

Red-head Sta. 37+00

Sta.	+	H.I.	-	Elev.
T.P.		141.88		134.50 133.56
	7.38	140.94		137.26
B.M. "X"			4.62	136.32

37+65

38+00

38+50

38+65 = EQUATION
22+65

CONTINUED BOOK #82 p 8

19.

Left. & Right.

E.C. $38+65^{26} = 22+65^{44}$

135.2	135.9	137.7
67	60	4.2
30		30

135.4	136.7	135.9	137.4
6.5	5.2	6.0	4.5
30	16		30

135.7	136.6	136.8
6.2	5.3	5.1
30		30

	+	H.I	-		
B.M. #12	0 ⁶⁶	104 ⁵⁰		103 ⁸⁴	Nail in Eucalyptus Tree at potato chip Factory
T.P	5 ¹²	97 ¹⁸	12 ⁴⁴	92 ⁰⁶	
B.M	10 ²⁰	99 ⁵¹	8 ⁵⁷	88 ⁶¹	B.M. in Cor. fence post. 5' L. Sta. 26+30
T.P	12 ⁹³	111 ⁸³	0 ⁶¹	98 ⁹⁰	
T.P	11 ⁸³	123 ⁴²	0 ²⁴	111 ⁵⁹	
T.P	8 ⁹⁴	131 ⁸⁴	0 ⁵²	122 ⁹⁰	
B.M	0 ⁴⁴	131 ⁷⁰	0 ⁵⁸	131 ²⁶	B.M. 50' L. Sta. 34+90
				131 ³⁶ 13 ²⁸	
T.P	5 ⁵³	124 ⁴⁰	12 ⁸³	118 ⁸⁷	
T.P	7 ⁶³	130 ⁷⁴	1 ²⁹	123 ¹¹	
T.P	6 ⁷⁵	133 ⁹²	3 ⁵⁷	127 ¹⁷	
B.M.	12 ⁴⁵	141 ²⁵	5 ¹²	128 ⁸⁰	B.M. on P.I. Hub. Sta. 44+64 ⁴⁷
				128 ⁹⁴ Bk 230 ^{1/2}	

+ H.I -

T.P 11⁵⁰ 141²⁵ 150⁶¹ 2¹⁴ 139¹¹ ✓

T.P. 6¹⁴ 156⁰³ 0⁷² 149⁸⁹ ✓

B.M. 10⁰⁸ 165⁸⁸ 0²³ ~~155⁸⁰~~ 155.98
Bk 230/5

B.M. 40'R. P.I. Sta. 54+15¹⁵

B.M. 12⁴² 177⁷⁵ 0⁵⁵ ~~165³³~~ 165.54
Bk 230/6

on P.I. Hub Sta. 58+71¹³

T.P. 12²⁹ 187⁸⁰ 2²⁴ 175⁵¹ ✓

T.P. 12³⁴ 199⁷⁶ 0³⁸ 187⁴² ✓

T.P. 12¹⁴ 211⁴⁸ 0⁴² 199³⁴ ✓

B.M. 12²³ 223⁵⁶ 0¹⁴ ~~211²⁴~~ 211.46

B.M. on P.I. Hub Sta. 65+14¹⁴

T.P. 11⁴³ 234⁶⁶ 0³⁹ 223¹⁷ ✓

T.P. 12⁷⁶ 247¹⁰ 0³² 234³⁴ ✓

T.P. 12⁴² 259⁴² 0¹⁰ 247⁰⁰ ✓

+ H.I -
259.42

T.P 12⁰⁰ 270⁷⁰ 0⁷² 258⁷⁰ ✓

T.P 12²⁸ 282⁴³ 0⁵⁵ 270¹⁵ ✓

T.P 7⁹³ 288²⁸ 2⁰⁸ 280²⁵ ✓

B.M 7³¹ 291⁴⁶ 4¹³ ~~284¹⁵~~ 284.34

B.M. 50' R. Sta. 76+00

T.P 9⁶⁰ 298²⁴ 2¹² 289³⁴ ✓

B.M. #9 4⁵⁶ 294³⁸ 294.57
294.57
19

On Hub at Fence Cor. H. Sta. 69+40

G LINE

X-Sections-

B/W

~~8.23 96.84~~

~~88.61~~

~~See Pg. 20~~

~~13.20 83.62 83.56~~

~~TP on Sta. 23~~

~~Pg. 12~~

~~9.97 86.87 86.77~~

~~TP on Sta. 24~~

~~See Pg. 13~~

B/W

0.64 104A8

103.84

B/W #2 - See Pg. 8

12.44 92.04

4.44 96.48

7.89 88.59 88.61

B/W See Pg. 20

7.89 96.50

23+50

$\frac{84.3}{12.2}$
 $\frac{30}{30}$

$\frac{84.3}{12.2}$
 $\frac{3}{3}$

$\frac{83.8}{12.7}$

$\frac{83.5}{13.0}$
 $\frac{30}{30}$

2A

$\frac{85.0}{11.5}$
 $\frac{30}{30}$

$\frac{84.5}{12.0}$

$\frac{84.1}{12.4}$
 $\frac{30}{30}$

450

$\frac{85.6}{10.9}$
 $\frac{30}{30}$

$\frac{85.3}{11.2}$

$\frac{85.5}{11.0}$
 $\frac{16}{16}$

$\frac{88.6}{7.9}$
 $\frac{30}{30}$

479

$\frac{85.7}{10.8}$
 $\frac{30}{30}$

$\frac{85.7}{10.8}$
 $\frac{6}{6}$

$\frac{85.2}{10.3}$

$\frac{86.9}{9.6}$
 $\frac{11}{11}$

$\frac{88.8}{7.7}$
 $\frac{20}{20}$

$\frac{92.2}{4.3}$
 $\frac{30}{30}$

12/14/26

Route
Dittan
Key

23

⊕ ✓

25+07

96.50

+23

+50

+78

26+00

9.99

98.60

7.89

88.61

+37

+64

+67

26+50

Lt.

Rt.

2x

<u>86.0</u>	<u>86.3</u>	<u>88.9</u>	<u>90.7</u>	<u>92.6</u>	<u>93.8</u>	<u>96.1</u>
<u>10.5</u>	<u>10.2</u>	<u>7.6</u>	<u>5.8</u>	<u>3.9</u>	<u>2.7</u>	<u>0.4</u>
<u>30</u>	<u>22</u>	<u>6</u>	<u>1</u>	<u>14</u>	<u>22</u>	<u>30</u>

<u>86.2</u>	<u>86.6</u>	<u>88.8</u>	<u>90.6</u>	<u>92.3</u>	<u>96.6</u>
<u>10.3</u>	<u>9.9</u>	<u>7.7</u>	<u>5.9</u>	<u>4.2</u>	<u>0.1</u>
<u>30</u>	<u>22</u>	<u>8</u>	<u>1</u>	<u>13</u>	<u>30</u>

<u>86.5</u>	<u>86.1</u>	<u>86.8</u>	<u>87.0</u>	<u>87.8</u>	<u>88.8</u>	<u>95.0</u>
<u>10.0</u>	<u>10.4</u>	<u>9.7</u>	<u>9.5</u>	<u>8.7</u>	<u>7.7</u>	<u>1.5</u>
<u>30</u>	<u>21</u>	<u>18</u>	<u>9</u>	<u>1</u>	<u>9</u>	<u>30</u>

<u>86.9</u>	<u>86.5</u>	<u>86.7</u>	<u>87.8</u>	<u>87.6</u>	<u>87.0</u>	<u>90.5</u>	<u>92.9</u>
<u>9.6</u>	<u>10.0</u>	<u>9.8</u>	<u>8.7</u>	<u>8.9</u>	<u>9.5</u>	<u>6.0</u>	<u>3.6</u>
<u>30</u>	<u>26</u>	<u>13</u>	<u>4</u>	<u>1</u>	<u>15</u>	<u>25</u>	<u>30</u>

<u>87.1</u>	<u>86.6</u>	<u>87.5</u>	<u>88.0</u>	<u>87.2</u>	<u>88.5</u>
<u>9.4</u>	<u>9.9</u>	<u>9.0</u>	<u>8.5</u>	<u>9.3</u>	<u>8.0</u>
<u>30</u>	<u>21</u>	<u>4</u>	<u>1</u>	<u>20</u>	<u>30</u>

<u>88.0</u>	<u>87.5</u>	<u>86.4</u>	<u>86.5</u>	<u>87.4</u>	<u>88.5</u>	<u>88.6</u>
<u>10.6</u>	<u>11.1</u>	<u>12.1</u>	<u>12.1</u>	<u>11.2</u>	<u>10.1</u>	<u>10.0</u>
<u>30</u>	<u>14</u>	<u>11</u>	<u>1</u>	<u>3</u>	<u>14</u>	<u>30</u>

<u>87.9</u>	<u>88.6</u>	<u>86.1</u>	<u>87.1</u>	<u>87.3</u>	<u>86.7</u>
<u>10.7</u>	<u>10.0</u>	<u>14.5</u>	<u>11.5</u>	<u>11.3</u>	<u>11.9</u>
<u>30</u>	<u>4</u>	<u>1</u>	<u>8</u>	<u>26</u>	<u>20</u>

<u>88.0</u>	<u>88.6</u>	<u>88.4</u>
<u>10.6</u>	<u>10.0</u>	<u>10.2</u>
<u>30</u>	<u>1</u>	<u>30</u>

81.6	82.1	81.9	82.5	81.0	82.2	83.2	81.4	81.4	83.0	83.7
87.7	88.2	88.0	86.6	87.1	88.2	87.3	87.5	87.5	89.1	87.8
<u>10.9</u>	<u>10.4</u>	<u>10.6</u>	<u>12.0</u>	<u>11.5</u>	<u>10.3</u>	<u>9.3</u>	<u>11</u>	<u>11</u>	<u>9.5</u>	<u>9.8</u>
<u>50</u>	<u>25</u>	<u>7</u>	<u>4</u>	<u>1</u>	<u>22</u>	<u>61</u>	<u>64</u>	<u>68</u>	<u>74</u>	<u>100</u>

for
Box
colvert.

98.60

27

+29

+50

060. 98.00

12.02 110.02

+75

28

+23

+46

+82

Lt.

98.60

Rt.

25

88.6	88.1	88.4	89.0	89.4	88.9
<u>10.0</u>	<u>10.5</u>	<u>10.2</u>	<u>9.6</u>	<u>9.2</u>	<u>9.7</u>
30	10		16	24	30

90.4	90.5	90.9	90.4
<u>8.4</u>	<u>8.1</u>	<u>7.7</u>	<u>8.2</u>
30	30	13	30

95.7	95.9	95.3	93.8	93.3	92.4
<u>4.9</u>	<u>2.7</u>	<u>2.3</u>	<u>1.8</u>	<u>5.3</u>	<u>6.2</u>
30	13		10	22	30

110.0

103.2	101.6	98.2	95.5
<u>6.8</u>	<u>8.4</u>	<u>11.8</u>	<u>14.5</u>
30	19		30

106.6	104.5	101.8	99.1	98.0
<u>3.4</u>	<u>5.5</u>	<u>8.4</u>	<u>10.9</u>	<u>12.0</u>
30	14		18	30

109.8	107.9	105.0	103.7	100.6	99.5
<u>0.2</u>	<u>2.1</u>	<u>5.0</u>	<u>6.3</u>	<u>9.4</u>	<u>10.5</u>
30	17		8	24	30

114.1	112.3	108.0	100.1
<u>1.1</u>	<u>2.3</u>	<u>2.0</u>	<u>9.9</u>
30	18		30

114.6	111.9	105.6	102.8	98.8	98.0
<u>1.6</u>	<u>1.9</u>	<u>1.1</u>	<u>1.2</u>	<u>11.2</u>	<u>12.0</u>
30	17		9	27	30

⊗

29

110.07

+30

10.40 99.62

+50

8.73 108.35

+86

30+15

+21

+68

+73

9.44 98.91 98.90

Lt

Rt

26

(110.0)

109.8	107.4	104.6	102.7	100.9	99.2	97.4
<u>0.2</u>	<u>2.6</u>	<u>5.4</u>	<u>7.3</u>	<u>9.1</u>	<u>10.8</u>	<u>15.6</u>
<u>30</u>	<u>23</u>	<u>6</u>		<u>10</u>	<u>18</u>	<u>30</u>

105.6	101.2	97.6	94.1	93.0	91.0
<u>4.4</u>	<u>5.8</u>	<u>14.4</u>	<u>15.9</u>	<u>17.0</u>	<u>19.0</u>
<u>30</u>	<u>14</u>		<u>16</u>	<u>28</u>	<u>30</u>

103.5	96.0	94.4	93.5	91.4	93.6
<u>1.9</u>	<u>12.4</u>	<u>14.0</u>	<u>14.9</u>	<u>17.0</u>	<u>14.8</u>
<u>30</u>		<u>6</u>	<u>19</u>	<u>26</u>	<u>30</u>

102.8	102.0	94.4	94.2	93.2	92.1	94.3
<u>5.6</u>	<u>6.4</u>	<u>14.0</u>	<u>14.2</u>	<u>15.2</u>	<u>16.3</u>	<u>14.1</u>
<u>30</u>	<u>20</u>		<u>17</u>	<u>19</u>	<u>27</u>	<u>28+30</u>

101.0	95.4	94.3	92.9	94.8	94.9
<u>7.4</u>	<u>13.0</u>	<u>14.1</u>	<u>15.5</u>	<u>13.6</u>	<u>13.5</u>
<u>30</u>	<u>11</u>		<u>6</u>	<u>14</u>	<u>30</u>

100.8	95.5	94.6	92.6	95.1	94.9
<u>7.6</u>	<u>12.9</u>	<u>13.8</u>	<u>15.6</u>	<u>13.3</u>	<u>13.5</u>
<u>30</u>	<u>12</u>	<u>6</u>		<u>6</u>	<u>30</u>

101.2	95.8	95.4	93.2	93.4	95.4	95.3	95.8
<u>7.2</u>	<u>12.6</u>	<u>13.0</u>	<u>15.4</u>	<u>15.0</u>	<u>13.0</u>	<u>13.1</u>	<u>12.6</u>
<u>30</u>	<u>15</u>	<u>7</u>		<u>5</u>	<u>6</u>	<u>23</u>	<u>30</u>

100.8	95.7	95.5	93.3	93.2	95.4	95.9
<u>7.6</u>	<u>12.7</u>	<u>12.9</u>	<u>15.1</u>	<u>15.2</u>	<u>13.0</u>	<u>12.5</u>
<u>30</u>	<u>14</u>		<u>7</u>	<u>11</u>	<u>14</u>	<u>30</u>

@ld TP B₂₀

(x) ✓

108.35

31

+30

1.84

106.51

10.17

116.68

+74

32

+50

1.70

114.98

12.44

127.42

33

+27

+50

(108.35)

104.9	98.2	96.3	96.0	93.8	93.8
<u>35</u>	<u>102</u>	<u>121</u>	<u>124</u>	<u>146</u>	
<u>20</u>	<u>10</u>		<u>20</u>	<u>25 + 20</u>	

106.9	102.8	100.1	98.0	97.1	93.8
<u>15</u>	<u>56</u>	<u>83</u>	<u>104</u>	<u>113</u>	<u>146</u>
<u>30</u>	<u>17</u>		<u>11</u>	<u>24</u>	<u>30</u>

(116.68)

116.1	112.3	108.8	107.0	102.8	102.0
<u>0.6</u>	<u>4.4</u>	<u>7.9</u>	<u>9.7</u>	<u>13.9</u>	<u>14.7</u>
<u>30</u>	<u>17</u>		<u>7</u>	<u>23</u>	<u>30</u>

119.4	117.8	114.2	112.4	109.8	107.9	106.3
<u>27</u>	<u>11</u>	<u>25</u>	<u>43</u>	<u>6.9</u>	<u>8.8</u>	<u>10.4</u>
<u>30</u>	<u>24</u>	<u>9</u>		<u>13</u>	<u>21</u>	<u>30</u>

125.1	123.7	119.9	111.1
<u>8.4</u>	<u>7.0</u>	<u>43.7</u>	<u>56</u>
<u>30</u>	<u>13</u>		<u>30</u>

(127.42)

122.9	118.4	116.8	118.9
<u>15</u>	<u>9.0</u>	<u>10.6</u>	<u>8.5</u>
<u>30</u>		<u>19</u>	<u>30</u>

123.3	122.4	122.5	121.7	120.5	121.8
<u>4.1</u>	<u>5.0</u>	<u>14</u>	<u>5.7</u>	<u>6.9</u>	<u>5.6</u>
<u>30</u>	<u>13</u>		<u>7</u>	<u>17</u>	<u>30</u>

125.1	125.0	123.1	122.7	122.6	124.6
<u>23</u>	<u>24</u>	<u>43</u>	<u>4.7</u>	<u>4.8</u>	<u>2.8</u>
<u>30</u>	<u>25</u>	<u>9</u>		<u>9</u>	<u>30</u>

(+) ✓

33+71 127.42

0.48 126.94

+90 6.12 133.06

34

+41

+79

B hr

1.70 131.36 131.26

Cont'd in Bk # 230/0

28

1251	124.9	1266	127.4	126.9	125.4	125.3
23	25	08	06	05	20	21
30	19	5		9	24	30

133.06						
126.8	126.4	127.3	127.1	126.0	126.0	
63	67	58	68	71	71	
30	9		8	17	30	

1273	126.4	126.4	126.2	126.1	
58	67	67	69	70	
30	16		8	30	

1287	127.6	127.4	128.2	127.5	
44	55	57	49	56	
30	9		19	30	

129.4	129.9	129.9	129.3	127.6	
37	34	34	38	55	
30	15		14	30	

See Pg. 20

(x)

Cross Sections -

LINE CHANGE

Sta 126+09.08 to 135+27.40 =
134+69.58

B.M.# 15 386.68
0.15 386.83

124+50

12/17/26

125

Alignment in
Bk# 124/32

Coote
Clifaw
King

+50

126

0.15 386.68

+50

12.06 398.74

Cont'd from Bk# 109/6

29

Nail in Tel. Pole 20' Rt Sta. 126+05
See Also Bk# 109/6

74.4	74.3	73.2	70.6	70.9	70.5	68.6	66.2
12	12.6	13.7	16.1	16.1	16.4	18.3	20.7
30	28	16	9	10	16	30	

74.1	74.0	75.0	75.2	74.3	72.9	72.7
7.8	8.9	11.9	11.7	12.6	14.0	14.2
30	16	7	15	22	30	

82.9	81.5	80.5	80.1	79.6	79.1	78.9	79.5
3.9	5.3	6.3	6.7	7.0	7.7	7.9	7.3
30	16	12	6	11	23	30	

88.6	88.6	88.1	84.4	85.1	80.5
1.8	1.2	1.7	2.0	1.7	0.3
30	7	9	11	30	

95.3	94.5	92.7	91.0	91.6	91.4	90.6
3.3	4.2	6.0	7.7	7.1	7.3	8.1
30	22	12	7	8	13	30

X

126+75

398.74

127+13.27
P.F.

1.81 396.93

+73

11.94 408.87

128

+50

129

+50

130

T.P.

5.22 409.43

1.66 404.51

Lt

Rt

30

97.9 08 30	95.2 35 21	95.8 29 16	94.4 43	92.6 61 14	91.9 6.8 30
------------------	------------------	------------------	------------	------------------	-------------------

100.3 +16 30	98.4 0.3 20	95.3 21	93.8 5.2 17	92.5 6.2 30
--------------------	-------------------	------------	-------------------	-------------------

408.87		
99.9 9.0 30	97.0 11.9	94.8 14.1 30

00.5 8.4 30	97.7 11.2	95.5 13.4 30
-------------------	--------------	--------------------

2.9 6.0 30	0.6 8.3	97.6 11.3 30
------------------	------------	--------------------

6.7 2.2 30	5.2 3.7 20	2.8 6.1	99.8 9.1 30
------------------	------------------	------------	-------------------

9.0 +0.1 30	4.7 1.2	1.6 7.3 30
-------------------	------------	------------------

6.9 2.0 30	6.2 2.7 20	4.6 1.3	3.6 5.4 17	2.9 6.0 20	2.9 6.0 30
------------------	------------------	------------	------------------	------------------	------------------

Out Hub ≠ Sta 130 + 20.60

X

130+30

409.43

131

150

132

14734
BC

133

750

6.32

407.45

8.30

401.13

H

409.43 Pt

31

4.6	4.2	3.6	3.8	3.4
<u>4.6</u>	<u>5.2</u>	<u>4.8</u>	<u>5.1</u>	<u>6.0</u>
30	9		13	30

2.0	3.3	4.6
<u>7.4</u>	<u>6.1</u>	<u>4.8</u>
30		30

1.1	1.9	3.2	5.4
<u>8.3</u>	<u>7.5</u>	<u>6.3</u>	<u>4.0</u>
30	15		30

0.4	0.5	2.7	5.7
<u>9.0</u>	<u>8.9</u>	<u>6.7</u>	<u>3.7</u>
30	24		30

399.0	1.9	4.5	5.7
<u>10.4</u>	<u>7.5</u>	<u>4.9</u>	<u>3.7</u>
30		21	30

97.2	1.3	5.5
<u>12.2</u>	<u>8.1</u>	<u>3.9</u>
30		30

96.1	0.8	5.6
<u>13.3</u>	<u>8.6</u>	<u>3.8</u>
30		30

x

134

407.45

+50

135

Check

9.45 399.00 398.9

Contd in Bk # 109/8

Lt 407.45 Pt

cu

95.5	0.5	57
<u>12.0</u>	<u>7.0</u>	<u>1.8</u>
30		30

95.4	0.2	5.0
<u>12.1</u>	<u>7.3</u>	<u>2.5</u>
30		30

95.3	98.0	99.6	1.0	2.7	4.3
<u>12.2</u>	<u>9.5</u>	<u>7.9</u>	<u>6.5</u>	<u>4.8</u>	<u>3.7</u>
30	12		11	19	30

± Sta 135 + 27.40 = 134 + 69.58

x

Grade Stks at Potato Chip Factory

	+	Hl.	-	Grade St
Bhw	4.06	107.90 106.90		102.84 103.84
19+00			19.6 18.57	88.33
19+55			20.0 19.01	87.89
	2.40	98.52 97.52	11.78	96.12 95.12
18+43			8.7	88.79
			2.40	95.12
Bhw	8.68	103.80	0.97	102.83

1/25/27 (Payday)
Coots

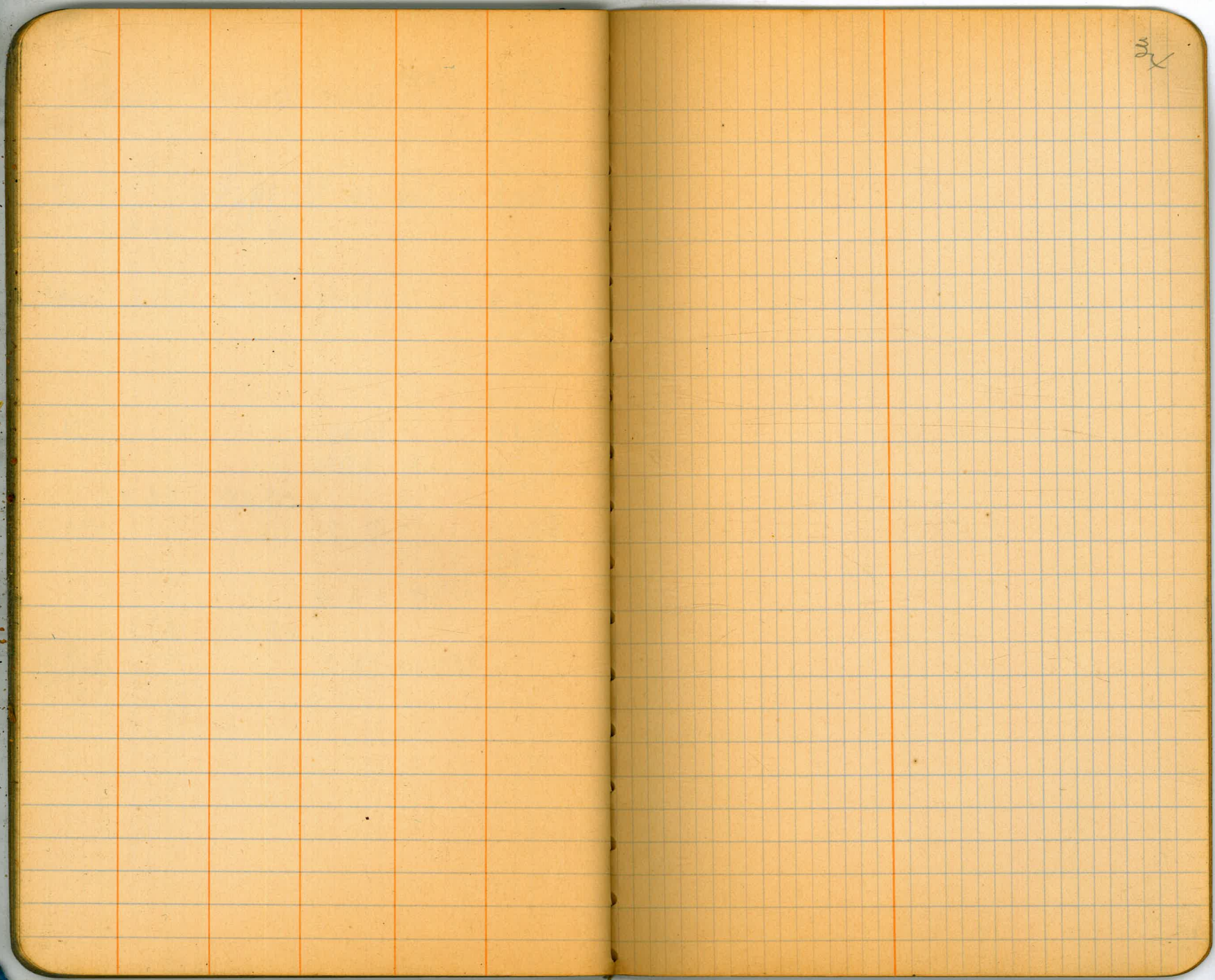
Nail in Gum Tree * Sta 19+80

45
 $\frac{14.1}{30 \text{ out}}$ c15^s

3.0
 $\frac{16.0}{30 \text{ out}}$ c17^s

7.1
 $\frac{1.6}{30 \text{ out}}$ c2^s

~~e13~~



20

58

0.00
2.76

14.76
2.67

14.09
+ 4.65

16.74

19
17.50 150 1.20

89.20

12

55

440

19+55

50

19+05

81
88.00 8tu 19

44
87.56 +55

93

5

724

19+55

75
18+80

37

18+43

89.20

74

88.46