

NAME National Ave Ext.

Job bb
Class 123 Course _____ Party _____

B.M.'s - Line Chg.

RETURN TO
Watson, York & Co.
508 Broadway Bldg.
San Diego, Calif.

212

1904

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

MICROFILMED

DEC 30 1964

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Bws	1 -
X-Secs Linc Chg	3-16

Oct. 2, 1926.
M. H. Peterman.
Todd.
Spaulding.

1.

B.M. Levels.
+ H.I. - Elev.

B.M. #30			460.34	
	0.15	460.49		
			12.25	448.24
	11.28	459.52		
			2.20	457.32
	1.96	459.28		
T.P.			2.76	456.52
T.P.			9.67	449.61
	0.80	450.41		
			0.41	450.00
	11.34	461.34		
			0.68	460.66
	11.41	472.07		
B.M. (Est.)			2.77	469.30
B.M. (Est.)			3.07	469.00 Reset
	0.86	469.86		
B.M. }			11.81	458.05 } Out 0.07
B.M. }				458.12 }
	11.79	469.91		
B.M.			0.84	469.07
	6.72	475.79		
			6.49	469.30 Check.

Book 114, P. 10.

2x2 hub Sta. 240+50.00
@ 236+25

Rock. @ 232+10

2x2 hub P.T. 228+13.39
Set Red-head in Tel. Pole @ Mid-Point of Curve
#82456

Old P.T. 222+67.89 Elev. 458.12

In Power Pole (See Above).

P.T. 228+13.39 Elev. 469.30

10/4/26 Bright, Sun.

Party: Todd - N-Notes
Key - Rad.
Spaulding - "

Cont'd from Pg 16 this Bk

2

L

R

Sta.	+	T	-	EL.	B.M. Rec. elev. =
222+67 ⁸⁹					458.12
	4.63	462.75			
222+43 ⁸³					P.C.

222+64

+82

223+00

+19

+32

+50

+72

1.28 461.47

224+00

+20

+35

7.25 468.72

For X-Sections Sta.
220+43.27 to 222+67.89
See Pg. 15 this book

Alignment Notes
in Bk #

454.2	453.7	454.6	455.0	456.3	456.4
8 [±]	9 ^L	8 ^L	7 ⁸	6 [±]	6 [±]
30 [±]	25 [±]	0	10 [±]	26 [±]	30 [±]

454.4	454.8	457.5	458.1	457.2	455.7	453.5
8 [±]	8 [±]	5 [±]	4 ^L	5 [±]	7 ^L	7 [±]
30 [±]	25 [±]	12 [±]	6	9 [±]	18 [±]	30 [±]

458.3	456.9	456.1	456.7	456.6	459.7	458.0
4 [±]	5 [±]	6 ^L	6 ^L	6 ^L	3 ^L	4 [±]
40 [±]	30 [±]	25 [±]	0	15 [±]	30 [±]	30 [±]

458.0	457.4	457.4	457.5	458.4	458.6
4 [±]	5 [±]	5 [±]	5 [±]	4 [±]	4 [±]
40 [±]	30 [±]	0	10 [±]	18 [±]	30 [±]

458.2	459.5	460.6	459.5	460.1	460.2	458.5	458.2
4 [±]	3 [±]	2 [±]	3 [±]	2 ^L	2 [±]	4 [±]	4 [±]
40 [±]	30 [±]	21 [±]	7 [±]	0	12 [±]	25 [±]	30 [±]

459.0	459.4	459.6	460.2	460.2	460.3
3 [±]	3 [±]	3 [±]	2 ^L	2 [±]	2 [±]
30 [±]	24 [±]	0	11 [±]	19 [±]	30 [±]

461.1	460.8	459.6	459.0	460.3	461.4	462.1
1 ^L	2 [±]	3 [±]	3 [±]	2 [±]	1 [±]	0 ^L
40 [±]	30 [±]	12 [±]	0	16 [±]	30 [±]	40 [±]

460.5	461.1	460.0	461.8	462.3	461.5
2 [±]	1 ^L	2 [±]	1 [±]	0 [±]	1 [±]
30 [±]	24 [±]	13 [±]	0	14 [±]	30 [±]

462.0	462.7	462.7	462.1	462.9	463.0	463.3
6 ^L	6 [±]	6 [±]	6 [±]	5 [±]	5 [±]	5 [±]
40 [±]	30 [±]	26 [±]	0	17 [±]	26 [±]	30 [±]

462.0	463.1	462.2	462.5		
6 ^L	5 [±]	6 [±]	6 [±]		
30 [±]	12 [±]	0	30 [±]		

462.2	462.9	464.2	464.1	463.3
6 [±]	5 [±]	4 [±]	4 [±]	5 [±]
30 [±]	0	15 [±]	30 [±]	40 [±]

Sta. + π - EL. B.M.s

224+50 468.72

+62

+78

0.05 468.67

6.09 474.76

225+15

+50

+80

226+00

+09

+31

+50

+75

5.63 469.14

Rec. EL. Notes
469.07
This EL. not
used.

Power Pole
#82456

3

469.7	464.3	463.3	465.7	465.7	464.6	464.2
$\frac{4^{\circ}}{40^{\circ}}$	$\frac{4^{\circ}}{30^{\circ}}$	$\frac{5^{\circ}}{22^{\circ}}$	$\frac{3^{\circ}}{0}$	$\frac{3^{\circ}}{10^{\circ}}$	$\frac{4^{\circ}}{23^{\circ}}$	$\frac{4^{\circ}}{30^{\circ}}$
464.9	464.5	464.4	466.4	466.4	465.0	466.0
$\frac{3^{\circ}}{40^{\circ}}$	$\frac{4^{\circ}}{30^{\circ}}$	$\frac{4^{\circ}}{20^{\circ}}$	$\frac{2^{\circ}}{0}$	$\frac{2^{\circ}}{11^{\circ}}$	$\frac{3^{\circ}}{27^{\circ}}$	$\frac{3^{\circ}}{30^{\circ}}$
466.3	464.9	466.1	465.7			
$\frac{2^{\circ}}{30^{\circ}}$	$\frac{3^{\circ}}{18^{\circ}}$	$\frac{3^{\circ}}{0}$	$\frac{3^{\circ}}{30^{\circ}}$			

467.6	469.2	469.1	467.5	467.5
$\frac{7^{\circ}}{30^{\circ}}$	$\frac{5^{\circ}}{70^{\circ}}$	$\frac{5^{\circ}}{0}$	$\frac{7^{\circ}}{19^{\circ}}$	$\frac{7^{\circ}}{30^{\circ}}$
469.6	468.2	468.8	469.2	469.3
$\frac{5^{\circ}}{40^{\circ}}$	$\frac{6^{\circ}}{30^{\circ}}$	$\frac{6^{\circ}}{22^{\circ}}$	$\frac{5^{\circ}}{0}$	$\frac{5^{\circ}}{30^{\circ}}$
468.1	468.2	470.8	470.5	469.0
$\frac{6^{\circ}}{30^{\circ}}$	$\frac{6^{\circ}}{10^{\circ}}$	$\frac{4^{\circ}}{0}$	$\frac{4^{\circ}}{12^{\circ}}$	$\frac{5^{\circ}}{30^{\circ}}$
468.8	467.5	467.5	469.1	468.6
$\frac{6^{\circ}}{40^{\circ}}$	$\frac{7^{\circ}}{30^{\circ}}$	$\frac{7^{\circ}}{24^{\circ}}$	$\frac{5^{\circ}}{0}$	$\frac{6^{\circ}}{15^{\circ}}$
467.6	467.6	469.5	469.8	468.7
$\frac{7^{\circ}}{30^{\circ}}$	$\frac{7^{\circ}}{23^{\circ}}$	$\frac{5^{\circ}}{8^{\circ}}$	$\frac{5^{\circ}}{0}$	$\frac{6^{\circ}}{15^{\circ}}$
	467.4	468.2	468.2	470.1
	$\frac{7^{\circ}}{30^{\circ}}$	$\frac{6^{\circ}}{0}$	$\frac{6^{\circ}}{28^{\circ}}$	$\frac{4^{\circ}}{40^{\circ}}$
468.0	468.0	469.8	470.9	470.5
$\frac{6^{\circ}}{30^{\circ}}$	$\frac{6^{\circ}}{25^{\circ}}$	$\frac{5^{\circ}}{13^{\circ}}$	$\frac{3^{\circ}}{0}$	$\frac{4^{\circ}}{18^{\circ}}$
467.9	469.5	468.8	468.5	469.2
$\frac{5^{\circ}}{30^{\circ}}$	$\frac{5^{\circ}}{24^{\circ}}$	$\frac{6^{\circ}}{12^{\circ}}$	$\frac{6^{\circ}}{0}$	$\frac{5^{\circ}}{23^{\circ}}$
				471.0
				$\frac{3^{\circ}}{40^{\circ}}$

Sta. + T - EL. B.M.s

227+00 474.76

+25

+50

+64

+78

228+00

4.74 470.02

3.17 473.19

3.83 469.36 469.30 1X2 h

+28

+50

+68

229+00

+50

9.99 463.20

L

Q

4.
R.

469.5 470.7 471.6 472.0 472.8 472.9
 $\frac{53}{40} \frac{41}{30} \frac{35}{21} \frac{48}{0} \frac{22}{25} \frac{24}{30}$

468.5 470.4 470.9 472.0 472.5 471.9
 $\frac{53}{40} \frac{41}{30} \frac{41}{19} \frac{48}{0} \frac{43}{30} \frac{34}{40}$

471.3 470.3 469.7 471.0 470.1 472.1
 $\frac{35}{40} \frac{45}{30} \frac{51}{25} \frac{38}{0} \frac{47}{19} \frac{47}{30}$

469.6 469.9 471.3 471.8 470.9 471.0
 $\frac{52}{30} \frac{42}{14} \frac{38}{0} \frac{30}{7} \frac{44}{24} \frac{38}{30}$

470.0 470.5 469.8 469.8 469.8
 $\frac{48}{30} \frac{43}{18} \frac{50}{7} \frac{50}{0} \frac{50}{30}$

471.2 470.5 469.8 469.8 471.7 471.2 470.1
 $\frac{36}{40} \frac{43}{30} \frac{50}{23} \frac{50}{0} \frac{34}{18} \frac{36}{30} \frac{47}{40}$

468.5 468.8 470.7 470.2 468.1 467.7
 $\frac{47}{53} \frac{44}{30} \frac{25}{13} \frac{30}{0} \frac{52}{16} \frac{55}{30}$

467.6 467.8 467.7 467.9 466.5
 $\frac{50}{30} \frac{51}{0} \frac{55}{25} \frac{58}{30} \frac{67}{40}$

468.0 468.1 468.8 466.1 466.9
 $\frac{52}{30} \frac{51}{12} \frac{64}{0} \frac{71}{8} \frac{68}{30}$

464.6 463.5 463.4 463.0
 $\frac{86}{30} \frac{92}{20} \frac{98}{0} \frac{102}{30}$

460.8 460.3 460.6 461.3 460.9
 $\frac{124}{30} \frac{123}{0} \frac{126}{13} \frac{119}{26} \frac{123}{30}$

Sta.	+	-	EL.	B.M.s
			463.20	
229+75	1.20	464.40		
+95				
230+00				
+25				
+44				
+70				
+88			11.69	452.71
	3.79	456.50		
231+08				
+25				
+41				
+60				
+77				

L.

E

R.

5.

459.4	457.4	457.7					
5°	7°	6°					
30°	0°	30°					
458.9	458.3	458.0	456.4	458.7	458.9		
6°	5°	6°	8°	8°	5°	5°	
30°	17°	9°	0°	8°	21°	30°	
457.6	457.3	457.9	456.7	456.3	458.7	459.2	459.2
6°	7°	6°	7°	8°	5°	5°	6°
30°	24°	14°	5°	6°	18°	30°	40°
	456.7	455.4	455.0				
	7°	9°	9°				
	30°	0°	30°				
457.0	456.0	456.4	456.9	456.6	456.1	453.2	456.9
7°	8°	8°	7°	7°	8°	11°	8°
30°	19°	12°	0°	13°	21°	30°	40°
	455.9	453.5	453.3	452.9			
	9°	10°	11°	11°			
	40°	30°	0°	30°			
455.4	452.9	452.9	453.3	453.4	455.9	455.6	454.2
9°	11°	11°	11°	11°	8°	8°	10°
40°	27°	21°	8°	0°	13°	21°	30°
	453.3	453.3	453.0	453.2	452.8	452.1	
	3°	3°	3°	3°	3°	4°	
	40°	30°	0°	16°	30°	40°	
453.1	454.8	454.8	452.5	452.5	453.3	454.8	454.3
3°	1°	1°	4°	4°	3°	1°	2°
40°	30°	24°	3°	0°	7°	21°	30°
	451.3	451.5	451.5	452.1	451.7		
	5°	5°	5°	4°	4°		
	30°	22°	10°	0°	30°		
	450.9	450.6	452.5	453.3	453.2	451.1	
	5°	5°	4°	3°	3°	5°	
	30°	18°	5°	0°	12°	30°	
450.9	452.9	452.0	451.2	451.6	450.8		
6°	6°	6°	5°	4°	5°		
30°	27°	14°	0°	10°	30°		

Sta.	+	π	-	EL.	B.M.s
		456.50	6.42	450.08	T.P. EL. 450 not used.
232+00					
+17					
+50					
233+00					
+37					
			10.20	446.30	
+62	1.70	448.00			
234+00					
+37					
+60					
+83					
235+00					
+50					

L	φ	R
449.7 <u>6.3</u> 30°	9.5 <u>7.0</u> 17°	449.8 <u>6.7</u> 9°
	449.1 <u>7.4</u> 30°	450.2 <u>6.3</u> 30°
	447.8 <u>8.7</u> 30°	449.8 <u>6.7</u> 19°
	446.2 <u>10.3</u> 30°	446.7 <u>9.8</u> 30°
	446.1 <u>10.4</u> 30°	447.0 <u>9.5</u> 12°
		446.0 <u>10.5</u> 25°
		446.0 <u>10.5</u> 30°
	443.8 <u>4.2</u> 30°	443.8 <u>4.2</u> 30°
	442.2 <u>5.8</u> 30°	441.5 <u>6.5</u> 23°
	442.0 <u>8.2</u> 40°	443.2 <u>4.8</u> 0
	442.0 <u>6.0</u> 12°	441.3 <u>6.7</u> 0
	441.9 <u>8.6</u> 30°	441.7 <u>6.3</u> 30°
	442.2 <u>8.3</u> 30°	440.9 <u>7.6</u> 0
	440.2 <u>8.3</u> 30°	442.6 <u>5.4</u> 0
	440.3 <u>7.7</u> 30°	441.9 <u>6.1</u> 0
	442.9 <u>5.1</u> 30°	445.5 <u>2.5</u> 30°
		442.9 <u>4.7</u> 0
		445.0 <u>3.2</u> 30°

Sta.	+	-	EL.	B.M.s
			448.00	
235+75				
236+00				
		2.23	445.77	
	10.93	456.70	7.02	449.68
	+35			Reo. El. 449.61 Not used
	+50			
	+75			
237+00				
	+25			
			6.39	450.31

7

L.			R.		
444.7	445.5	445.7	444.6	446.2	447.2
33	25	23	34	18	08
40	30	19	10	0	18
			445.3	445.5	446.9
			22	25	16
			30	0	30
			446.3	447.1	449.8
			10	9	6
			30	15	0
			446.8	448.9	449.0
			9	8	7
			30	0	30
			449.7	448.7	448.7
			7	8	8
			40	30	23
			449.6	450.5	449.7
			7	6	7
			30	0	30
			451.4	452.5	452.9
			5	4	3
			30	0	10
					30

Oct. 5, 1926.
 M. H. Peterman
 Todd
 Chaulding.
 Elev. ✓
 450.31

Sta. + H.I. -
 T.P.

10.68 460.99

237+43

237+63

237+78

237+92

238+06

238+25

238+50

238+66

Left. ♀ Right.

(4610)

451.5 455.3 455.5 453.4 454.4 454.2
 9.5 5.7 5.5 7.6 6.6 6.8
 40 16 16 35 40

452.7 453.0 453.2
 8.3 8.0 7.8
 30 30

455.5 455.0 453.4 453.2 459.0
 5.5 6.0 7.6 7.8 7.0
 40 30 18 30

454.0 454.7 455.0 456.3 456.3
 7.0 6.3 6.0 4.7 4.7
 30 16 30 40

454.3 456.5 455.6 455.1
 6.7 4.5 5.4 5.9
 30 16 30

454.4 455.3 456.0 457.5 457.4
 6.6 5.7 5.0 3.5 3.6
 30 6 16 30

455.0 456.5 457.1 455.1 455.9
 6.0 4.5 3.9 5.9 5.1
 40 30 20 30

455.4 455.2 457.2 457.9
 5.6 5.8 3.8 3.1
 30 16 30

Sta. + H.I. - Elev.

238+90

460.99

239+00

239+25

239+50

239+75

240+00

240+25

240+50

T.P.

4.41 456.58

Left.

¢

Right

456.0 456.8 457.6 455.7 456.2
 5.0 4.2 3.4 5.3 4.8
 40 30 17 30

456.2 456.8 456.1 456.8 456.9
 4.8 4.2 4.9 4.2 4.1
 30 17 14 30

458.3 457.5 456.3 456.5 457.0 458.7 457.5
 2.7 3.5 4.7 4.5 4.0 2.3 3.3
 40 30 20 10 25 40

456.7 458.3 458.6 458.4 457.0 456.7
 4.3 2.7 2.4 2.6 4.0 4.3
 30 16 10 20 30

458.2 457.3 456.6 456.5 456.8
 2.8 3.7 4.4 4.5 4.2
 40 30 25 30

456.8 457.7 458.3 458.6 458.0 457.2 457.7 456.7
 4.2 3.3 2.7 2.4 3.0 3.8 3.3 4.3
 40 30 25 10 8 30 40

456.8 456.6 457.2 456.7 457.3 457.9
 4.2 4.4 3.8 4.3 3.7 3.1
 30 15 20 30 40

457.1 457.4 456.5 456.6 455.8
 3.9 3.6 4.5 4.4 5.2
 30 25 15 30

Sta. + H.I. - Elev.
T.P. 456.58

1.14 457.72
240+75

Left. € Right.

456.9 456.5 455.7 455.6
0.8 1.2 2.0 2.1
30 5 30

241+00

455.0 454.9 455.4 454.3
2.7 2.8 2.3 3.4
30 10 30

241+35

453.6 454.4 454.4 453.6 451.7
4.1 3.3 3.3 4.1 6.0
30 15 15 30

241+60

453.2 450.8 449.3
4.5 6.9 8.4
30 30

241+80

451.3 451.6 450.9 450.0 447.7
6.4 6.1 6.8 7.7 10.0
30 15 22 40

242+00

452.3 449.6 448.9 446.8
5.4 8.1 8.8 10.9
40 25 30

T.P. 11.17 446.55
1.18 447.73

242+50

447.7 445.0 442.9
0.0 2.7 4.8
30 30

Sta + H.I. - Elev.

447.73

242+75

243+00

243+35

244+00

T.P.

T.P.

3.43 439.31

244+35

244+42

Gully

244+50

245+00

Left. ϕ Right

445.3 444.1 443.5 442.5
2.4 3.6 4.2 5.2
30 20 30

443.5 442.4 441.4 439.9
4.2 5.3 5.3 7.8
30 30 50

442.1 442.3 441.3 440.0 438.6
5.6 5.4 6.4 7.7 9.1
30 15 10 30

436.3 435.7 433.9
11.4 12.0 13.8
30.0 30

433.7 432.1 430.2
5.6 7.2 9.1
30 30

438.9 433.9 431.1 428.9 427.3 425.0 416.7
0.4 5.4 8.2 10.4 12.0 14.3 22.6
150 100 50 50 100 150

435.3 434.3 432.8 431.1 431.1
4.0 5.0 6.5 8.2 8.2
30 10 8 30

439.2 437.2 435.0 432.3 424.2
0.1 2.1 4.3 7.0 5.1
30 28 35 40

Sta. + H.I. - Elev. Left. Right

245+45 439.31 Gully &

436.6 432.8 428.8
 2.7 6.5 10.5
 50 100

245+30

437.9 435.8 435.8 436.8 437.3 436.9 438.3
 1.4 2.5 3.5 2.5 2.0 2.4 1.8
 8 12 20 25 30 40

T.P. 446.82 (Sh. #11)

6.68 453.50

245+30

440.5
 13.0
 30

245+50

441.4 439.5 437.1 439.0 439.5
 12.1 14.0 16.4 14.5 14.0
 30 10 5 30

245+75

443.2 442.2 440.0 441.8 442.2 443.0 442.1
 10.3 11.3 13.5 11.7 11.3 10.5 11.4
 30 15 10 5 13 30

246+00

443.3 443.6 443.6
 10.2 9.9 9.9
 30 30

246+25

444.7 446.9 446.9 446.6 445.5 445.2
 8.8 6.6 6.6 6.9 8.0 8.3
 30 7 17 25 30

Sta. + H.I. - Elev.

246+44¹² B.C. 453.50

246+85

247+10

T.P.

10.12 462.77

B.M. #30

247+25

2.41 460.36 460.34

247+50

247+85

248+10

248+35

Left.

4

Right.

446.0 446.8 447.0
7.5 6.7 6.5
300 30

449.0 449.5 449.6 449.5
4.5 4.0 3.9 4.0
30 15 30

452.3 452.0 453.1 451.9 452.8
1.2 -0.5 0.4 1.6 0.7
30 8 10 30

247+15

Book 114, P.10.

452.7 453.3 455.0
10.1 9.5 7.8
30 30

454.0 454.2 456.2 456.9 456.2 455.3 456.5
8.8 8.6 6.6 6.4 6.6 7.5 7.3
30 23 7 10 15 30

455.6 455.1 455.5 456.4
7.2 7.7 7.3 6.4
30 20 30

456.7 458.4 457.9 457.4 457.7
6.1 4.4 4.9 5.4 5.1
30 10 12 30

456.9 456.9 458.5 459.4 460.1
5.9 5.9 4.3 3.4 2.7
30 12 8 30

Sta. + H.I. - Elev.

463.17

248+50

248+65

249+00

249+15

249+50

250+00

250+50

250+804 = E.C.

249+39.33 = B.C.

see book # 113 page 18

Left.

±

Right.

^{462.77}
~~456.9~~ 458.1 ~~458.3~~ 458.8 458.5
 5.9 4.7 4.5 4.0 4.3
 30 12 20 30

459.3 459.9 ^{459.4} 458.3 458.7
 3.5 2.9 3.4 4.5 4.1
 30 12 10 30

458.7 459.6 ^{460.4}
 4.1 3.2 2.4
 30 30

460.3 459.8 ^{461.6} 461.2 460.2 460.5
 2.5 3.0 1.2 1.6 2.6 2.3
 30 15 15 20 30

461.0 461.6 460.1 461.7
 1.8 1.2 2.7 1.1
 30 20 30

461.8 461.8 460.9 462.0 461.3 462.2
 1.0 1.0 1.9 0.8 1.5 0.6
 30 22 14 20 30

460.7 462.4 462.5 461.1 461.2
 2.1 0.4 0.3 1.7 1.6
 30 15 25 30

460.8 460.8 462.3 462.4 461.3 461.6
 2.0 2.0 0.5 0.2 1.5 1.2
 30 22 8 20

Cont'd from Bk # 116/25

Lt.

Rt.

15

Blev
1.89 460.01

258.12

On Hub ± 222 + 67.89 See Bk # 116/27

220 + 43.27

45.7
14.3
30

47.9
12.1

449.1
100
25

429.5
102
30

+67

10/6/26
Coote
Glover
Cliffan-

447.8 451.0
12.2 9.0
30 15

450.7
9.3

448.3 449.6
11.2 10.4
14 30

+88

448.2
11.8
30

448.3
11.7

448.6 451.1
11.4 8.9
13 30

22407

447.2
12.8
30

449.1
10.9

449.8
10.2
30

+26

450.0
10.0
30

452.7
7.3
15

452.4
7.6

451.1 451.4
8.9 8.6
13 30

+45

448.8
11.2
30

450.6
9.4

451.8 453.1 454.7
8.2 8.0 5.1
9 25 30

LH.

Rt.

16

A6001

221+60

$$\begin{array}{r} 452.0 \\ \underline{100} \\ 30 \end{array} \quad \begin{array}{r} 451.2 \\ \underline{8.8} \\ 13 \end{array} \quad \begin{array}{r} 451.0 \\ \underline{9.0} \\ 1 \end{array} \quad \begin{array}{r} 453.5 \\ \underline{6.5} \\ 30 \end{array}$$

+79

$$\begin{array}{r} 452.8 \\ \underline{7.2} \\ 30 \end{array} \quad \begin{array}{r} 452.1 \\ \underline{7.9} \\ 25 \end{array} \quad \begin{array}{r} 454.3 \\ \underline{5.7} \\ 16 \end{array} \quad \begin{array}{r} 454.1 \\ \underline{5.9} \\ 1 \end{array} \quad \begin{array}{r} 452.0 \\ \underline{8.0} \\ 13 \end{array} \quad \begin{array}{r} 452.9 \\ \underline{7.6} \\ 30 \end{array}$$

+95

$$\begin{array}{r} 452.0 \\ \underline{8.0} \\ 30 \end{array} \quad \begin{array}{r} 452.7 \\ \underline{7.3} \\ 23 \end{array} \quad \begin{array}{r} 453.1 \\ \underline{6.9} \\ 1 \end{array} \quad \begin{array}{r} 452.8 \\ \underline{7.2} \\ 14 \end{array} \quad \begin{array}{r} 454.3 \\ \underline{5.7} \\ 25 \end{array} \quad \begin{array}{r} 454.1 \\ \underline{5.9} \\ 30 \end{array}$$

222+14

$$\begin{array}{r} 453.5 \\ \underline{6.5} \\ 30 \end{array} \quad \begin{array}{r} 455.8 \\ \underline{4.2} \\ 16 \end{array} \quad \begin{array}{r} 455.6 \\ \underline{4.4} \\ 1 \end{array} \quad \begin{array}{r} 454.3 \\ \underline{5.7} \\ 10 \end{array} \quad \begin{array}{r} 454.8 \\ \underline{5.2} \\ 30 \end{array}$$

+34

$$\begin{array}{r} 454.4 \\ \underline{5.6} \\ 30 \end{array} \quad \begin{array}{r} 452.6 \\ \underline{6.4} \\ 25 \end{array} \quad \begin{array}{r} 454.2 \\ \underline{5.8} \\ 1 \end{array} \quad \begin{array}{r} 457.3 \\ \underline{2.7} \\ 19 \end{array} \quad \begin{array}{r} 459.1 \\ \underline{2.9} \\ 30 \end{array}$$

+A3

+5x6
5A3w[#]

190 458.11 458.12

Cont'd on Pg 2 this Book-

17

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See. Bln Bk 116/27