

NAME EL Cerrito
Book # 3
Class _____ Course _____ Party _____

346 (1925)

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

W
123

MICROFILMED

DEC 30 1964

JUANITA ST.

BW#12

2.03 429.89

11.99 417.90

0.35 418.45

0-50

11.57 406.68

0.15 406.83

0+00

+17

+50

+73

TP

-0.01 395.80

11.04 395.81

R

Southerly from Ambassador.

Base Line = Prep. Line E. Side.

0+00 = PCC. Lot 1, Blk 22

Quixr Hub E. Side Ambassador at Juanita -
Lt. (E)

Pt. (W)

418.25

411.6

410.9

408.9

407.8

406.7

$\frac{6.6}{10}$

$\frac{7.3}{10}$

$\frac{9.3}{20}$

$\frac{10.4}{40}$

$\frac{11.5}{50}$

404.7

403.5

402.9

402.0

406.83

402.6

402.5

398.8

$\frac{2.1}{10}$

$\frac{3.3}{10}$

$\frac{3.9}{10}$

$\frac{3.8}{10}$

$\frac{4.2}{20}$

$\frac{6.3}{40}$

$\frac{8.0}{50}$

403.0

402.3

401.3

401.9

401.9

401.3

400.6

398.5

$\frac{3.8}{10}$

$\frac{4.5}{10}$

$\frac{5.5}{20}$

$\frac{4.9}{10}$

$\frac{4.9}{20}$

$\frac{5.5}{35}$

$\frac{6.2}{40}$

$\frac{8.3}{50}$

401.0

400.6

399.1

399.4

392.6

392.0

$\frac{5.8}{10}$

$\frac{6.2}{10}$

$\frac{4.7}{10}$

$\frac{7.4}{20}$

$\frac{9.2}{40}$

$\frac{9.8}{50}$

399.7

399.5

399.6

397.3

396.4

396.6

394.5

405.5

$\frac{7.1}{10}$

$\frac{7.3}{10}$

$\frac{7.2}{20}$

$\frac{9.5}{40}$

$\frac{10.8}{20}$

$\frac{10.7}{25}$

$\frac{12.3}{40}$

$\frac{13.8}{50}$

Quixr Hub Ret SE Cor Juanita & Alley

R

395.80

1+23

+80

2+30

11.40 384.40

0.62 385.02
B.C.

2+73

3+23

3/5

11.98 373.04

0.56 373.60

+73

4+13

11.47 362.13

0.22 362.35

+63

L.

R.

395.8

2

395.8 394.1 394.2 392.4 392.1 390.7 385.4 382.3

$\frac{00}{10}$ $\frac{17}{1}$ $\frac{16}{1}$ $\frac{34}{3}$ $\frac{37}{15}$ $\frac{5.1}{20}$ $\frac{10.4}{40}$ $\frac{13.5}{50}$

392.2 389.8 386.5 386.4 384.3 383.8 375.5 372.8

$\frac{36}{10}$ $\frac{6.0}{1}$ $\frac{9.3}{1}$ $\frac{9.4}{13}$ $\frac{11.5}{17}$ $\frac{12.0}{20}$ $\frac{20.3}{40}$ $\frac{23.0}{50}$

388.4 385.3 382.1 382.2 378.4 370.7 367.1

$\frac{7.4}{10}$ $\frac{10.5}{1}$ $\frac{13.7}{3}$ $\frac{13.6}{15}$ $\frac{17.4}{20}$ $\frac{25.1}{40}$ $\frac{28.7}{50}$

385.02

386.0 382.6 379.5 379.4 375.9 367.9 364.4

$\frac{+1.0}{10}$ $\frac{2.4}{4}$ $\frac{5.5}{4}$ $\frac{5.6}{15}$ $\frac{9.1}{20}$ $\frac{17.1}{40}$ $\frac{20.6}{50}$

383.4 380.1 377.6 377.3 373.2 365.9 362.2

$\frac{1.6}{10}$ $\frac{4.9}{1}$ $\frac{7.4}{3}$ $\frac{7.7}{13}$ $\frac{12.0}{20}$ $\frac{19.1}{40}$ $\frac{22.8}{50}$

373.6

376.5 374.6 371.8 371.2 365.8 362.5 356.3 362.1

$\frac{+4.9}{10}$ $\frac{+1.0}{1}$ $\frac{1.8}{3}$ $\frac{2.4}{13}$ $\frac{7.8}{20}$ $\frac{11.1}{40}$ $\frac{17.3}{40}$ $\frac{21.5}{50}$

372.6 367.8 364.8 365.0 361.6 350.8 347.4

$\frac{1.1}{10}$ $\frac{5.6}{1}$ $\frac{8.8}{3}$ $\frac{8.6}{13}$ $\frac{12.0}{20}$ $\frac{22.8}{40}$ $\frac{26.2}{50}$

365.1

342.35

361.8 359.0 358.7 355.7 349.7 346.4
 $\frac{+2.8}{10}$ $\frac{0.5}{1}$ $\frac{3.3}{2}$ $\frac{3.6}{13}$ $\frac{6.6}{20}$ $\frac{12.6}{40}$ $\frac{15.9}{50}$

362.35

5+3

11.93 350.42

0.74 351.16

+63

6/7

6+3

11.63 339.53

1.19 340.72

+63

7+2A

ES

T.P.

11.77 328.95

0.47 329.42

~~7+7~~

+77

2+2

8+20

2+2

0.47 328.95

0.22 329.17

Lt

Rt

3

362.35
357.2 339.5 352.0 352.3 360.3 349.5 344.2 341.7

5.1	7.8	10.3	10.0	12.0	12.8	18.1	20.6
<u>10</u>		<u>1</u>	<u>14</u>	<u>17</u>	<u>20</u>	<u>40</u>	<u>50</u>

351.16

349.7 347.9 345.5 345.9 344.7 344.1 340.8 339.1

1.4	3.4	5.6	5.2	6.1	7.0	10.3	12.0
<u>10</u>	<u>1</u>	<u>1</u>	<u>17</u>	<u>17</u>	<u>20</u>	<u>40</u>	<u>50</u>

344.2 342.6 340.5 340.9 339.1 338.6 336.5 335.0

6.1	8.5	10.6	10.7	12.0	12.5	14.6	16.1
<u>10</u>	<u>2</u>	<u>2</u>	<u>15</u>	<u>20</u>	<u>31</u>	<u>40</u>	<u>50</u>

340.72

340.0 338.6 337.0 337.1 335.9 335.3 333.6 332.3

0.7	2.1	3.7	3.6	4.8	5.4	7.1	8.4
<u>10</u>	<u>1</u>	<u>13</u>	<u>13</u>	<u>20</u>	<u>31</u>	<u>40</u>	<u>50</u>

335.7 334.8 334.9 334.0 334.1 333.5 333.2 330.9 330.1

5.0	5.9	5.8	6.7	6.6	7.2	7.5	9.8	10.8
<u>10</u>	<u>1</u>	<u>3</u>	<u>13</u>	<u>16</u>	<u>20</u>	<u>40</u>	<u>50</u>	

T.P. on 2x2 Hub NECor Piedmont

329.4

329.9 328.9 326.5 324.0 323.0

10.5	0.5	2.9	5.4	6.4
<u>10</u>	<u>1</u>	<u>20</u>	<u>40</u>	<u>50</u>

324.2 322.5 319.7 317.7 317.0

5.2	6.9	9.7	11.7	12.4
<u>10</u>	<u>1</u>	<u>20</u>	<u>40</u>	<u>50</u>

See Above

329.17

11.20 317.97

8+70 068 318.65

9+20

11.32 307.33

2.45 309.78

+65 P.I.

+89

10+09

On Line of Univ Ave - Curb

+09

11

- Gutter -

B.M. #2

7.04 302.69 302.81

Lt

317.7 315.9

0.9
10 2.7

312.2 311.0

6.4
10 7.6

307.3 306.0

2.4
10 3.7

303.0 302.3

6.7
10 7.4

302.1 301.9

7.6
10 7.86

301.3 301.2

8.4
10 8.54

RSek in N Side Pole $\frac{5}{22}$

Rt

318.65

313.7 311.1 310.6

4.9
20 7.5 8.0
4.0 5.0

309.0 307.3 306.1

9.6
20 11.3 12.5
4.0 5.0

309.78 301.4 301.2 300.8 300.7

304.1 8.3 8.5 9.0 9.07
20 3.4 4.0 5.0 5.7

301.5 301.4 300.6 300.8 300.8

8.2 8.38 9.14 8.98 9.01
20 2.7 3.2 4.0 5.0
Curb Gutter Curb

301.4 301.0 300.8

8.33 8.74 8.92
24 5.8 6.8

300.7 300.2 300.0

9.05 9.57 9.72
24 5.8 6.8

4

PIEDMONT PLACE-

B_m 2.79 331.74

328.95

0+00

+50

1

+A1

+63

11.82 342.89

0.67 331.07

Ⓚ

Fly from Juanita -

Base Line = Prop. Line on S. Side -

0+00 = S.E. Cor Piedmont & Juanita -

T.P. on 2x2 Hub N.E. Cor Piedmont

See Pg. 3

331.74

322.8	322.6	325.5	328.2	330.2
$\frac{10.9}{10}$	$\frac{9.1}{10}$	$\frac{6.2}{15}$	$\frac{3.5}{30}$	$\frac{1.5}{40}$
322.3	324.6	328.4	331.3	334.5
$\frac{9.4}{10}$	$\frac{7.1}{10}$	$\frac{3.3}{15}$	$\frac{0.4}{30}$	$\frac{+2.8}{40}$
323.8	326.5	329.2	333.0	335.0
$\frac{7.9}{10}$	$\frac{5.2}{10}$	$\frac{1.8}{15}$	$\frac{+1.3}{30}$	$\frac{+3.3}{40}$
328.1	328.7	332.9	336.5	338.5
$\frac{5.6}{10}$	$\frac{3.0}{10}$	$\frac{+1.1}{15}$	$\frac{+4.8}{30}$	$\frac{+6.8}{40}$
327.7	330.7	334.9	339.3	342.1
$\frac{4.0}{10}$	$\frac{1.0}{10}$	$\frac{+2.4}{15}$	$\frac{+7.6}{30}$	$\frac{+10.4}{40}$

Ⓚ

342.89

1+96

2+30 B.C.

+80

1.60 336.11

1.38 334.51

7.15 328.96 328.95 J.P. Pg 5

329.9

$\frac{130}{10}$

331.2

$\frac{117}{10}$

$\frac{114}{10}$

332.1

$\frac{108}{10}$

333.7

$\frac{95}{10}$

$\frac{87}{10}$

342.89

336.6

$\frac{63}{15}$

338.1

$\frac{18}{15}$

$\frac{45}{15}$

341.1

$\frac{18}{30}$

342.2

$\frac{0.7}{30}$

$\frac{0.0}{30}$

343.6

$\frac{0.7}{40}$

344.89

$\frac{1.3}{40}$

$\frac{1.53}{40}$

6

350.2

$\frac{1.96}{70}$

$\frac{1.14}{70}$

351.1

352.2

$\frac{1.87}{60}$

357.1

$\frac{1.14}{70}$

B

R

Alley - 20' -

Btw

9.61 205.42

39.581

T.P. on Ret. Hub SE. Cor. Juanita & Alley -
405.4

0-18

On line with 1/2 + Ret

398.5

397.6

396.8

395.8

395.4

$\frac{6.9}{10}$

$\frac{7.8}{10}$

$\frac{8.6}{10}$

$\frac{9.6}{20}$

$\frac{100}{30}$

395.4

394.4

392.9

391.6

390.4

0-41

"

$\frac{10.0}{10}$

$\frac{11.0}{10}$

$\frac{12.5}{10}$

$\frac{13.8}{20}$

$\frac{15.0}{30}$

399.6

399.1

398.5

397.6

396.6

0+00

Ret.

$\frac{5.6}{10}$

$\frac{6.3}{10}$

$\frac{6.9}{10}$

$\frac{7.8}{20}$

$\frac{8.8}{30}$

401.4

401.0

400.6

400.0

399.7

+40

BC.

$\frac{4.0}{10}$

$\frac{4.4}{10}$

$\frac{4.8}{10}$

$\frac{5.4}{20}$

$\frac{5.7}{30}$

402.4

401.7

401.2

400.7

400.2

0+90

12/13

$\frac{3.0}{10}$

$\frac{3.7}{10}$

$\frac{4.2}{10}$

$\frac{4.7}{20}$

$\frac{5.2}{30}$

402.2

401.7

401.1

400.5

400.8

1+25

$\frac{3.7}{10}$

$\frac{3.7}{10}$

$\frac{4.3}{10}$

$\frac{4.9}{20}$

$\frac{4.6}{30}$

(R)

(R)

AD542

1460 13/14

2404 25.14

137

477 5/6

9.62 295.80 295.81

LH

400.2 400.2
 $\frac{53}{10}$ $\frac{54}{10}$

397.5 398.0
 $\frac{19}{10}$ $\frac{74}{10}$

394.4 395.9
 $\frac{11.0}{10}$ $\frac{9.5}{10}$

388.9 391.3
 $\frac{16.8}{10}$ $\frac{14.1}{10}$

RH

405.42
 $\frac{400.4}{10}$ $\frac{400.1}{10}$

398.5 399.1 399.0
 $\frac{69}{10}$ $\frac{63}{20}$ $\frac{64}{30}$

397.9 397.8 397.9
 $\frac{80}{10}$ $\frac{7.6}{20}$ $\frac{7.5}{30}$

393.5 394.7 395.5
 $\frac{11.9}{10}$ $\frac{10.7}{20}$ $\frac{9.9}{30}$

See T.P. Pg. 7

R

R

SEA BREEZE PLACE

B^m#13

1.22 364.22

11.60 352.62

0.61 353.23

11.33 341.90

0.67 342.57

0+00

+30 PRC

10.96 331.61

0.68 332.49

+80

+30

+73

37/

363.00'

W'y from Juanita.-

Base Line = Prop Line N. Side St.

0+00 = 5th 24/25, Blk 33

On 1/2 Hub E. Side Juanita at Sea Breeze

See Blk #339/7

Lt.

Rt.

342.57

342.1	345.3	349.2	342.7	340.1	338.6
+36 40	+28 30	+17 18	+07 15	24	39 10
338.5	337.7	336.7	335.7	335.2	
4.0 40	1.8 30	5.8 15	6.8 10	7.5 10	
334.5	330.8	332.29 330.5	329.9	329.5	
1.8 40	1.5 30	1.8 15	2.4 10	2.8 10	
326.7	326.4	325.3	324.9	325.0	
5.6 40	6.3 30	7.0 15	7.4 10	7.3 10	
323.0	322.7	321.8	321.9	321.9	
9.3 40	9.6 30	10.5 15	10.4 10	10.4 10	

R

2+00

332.29

11.15 321.14

1.43 322.57

.+33 PCC.

+58

On Line With PCC & 25/32

+70

9.30 313.27

2.29 315.56

B.M.#14

6.22 309.34 309.36

See Bk #359/8

B. 10

320.9	320.5	320.3	320.2	320.8	320.7
<u>11.4</u>	<u>11.8</u>	<u>12.0</u>	<u>12.1</u>	<u>11.5</u>	<u>11.6</u>
40	30	15	10	10	10

319.1	319.2	319.4	318.5	319.0	318.1	317.6
<u>3.4</u>	<u>3.3</u>	<u>3.1</u>	<u>4.0</u>	<u>3.5</u>	<u>4.4</u>	<u>4.9</u>
90	80	50	20	9	10	10

318.1	318.9	317.5	317.8	316.9
<u>4.4</u>	<u>3.6</u>	<u>5.0</u>	<u>4.7</u>	<u>6.1</u>
80	70	50	22	

316.7	317.0	317.6	316.1	316.0
<u>5.9</u>	<u>5.6</u>	<u>5.0</u>	<u>6.4</u>	<u>6.6</u>
70	50	25	9	

R

R

VICTORY PLACE.

Wily from Hacienda -
 Base Line = Prop Line N. Side St.
 0+00 = SEC. Cor Lot 8, Bk 34

Bm #14

309.36

0.94 310.30

See Bk # 339/8

310.3

303.1

302.2

300.9

300.1

299.5

$\frac{7.2}{40}$

$\frac{8.1}{30}$

$\frac{9.4}{15}$

$\frac{10.7}{10}$

$\frac{10.8}{10}$

0+00

300.1

299.9

299.6

298.9

298.3

296.7

296.6

297.2

$\frac{10.7}{40}$

$\frac{10.4}{30}$

$\frac{10.7}{23}$

$\frac{11.4}{15}$

$\frac{12.0}{7}$

$\frac{12.6}{6}$

$\frac{13.7}{10}$

$\frac{13.1}{10}$

+08

299.7

299.4

297.8

296.3

297.0

298.3

298.7

299.1

$\frac{10.6}{40}$

$\frac{10.9}{30}$

$\frac{12.5}{15}$

$\frac{14.0}{13}$

$\frac{13.3}{7}$

$\frac{12.0}{6}$

$\frac{11.6}{10}$

+13

309.2

300.3

301.3

302.1

303.8

$\frac{11.1}{40}$

$\frac{10.0}{30}$

$\frac{9.0}{15}$

$\frac{8.2}{10}$

$\frac{6.5}{10}$

+63

0.88 309.42

10.73 320.15

308.7

308.1

$\frac{320.5}{310.9}$

312.7

313.9

$\frac{11.4}{40}$

$\frac{11.0}{30}$

$\frac{9.2}{15}$

$\frac{7.4}{10}$

$\frac{6.2}{10}$

+03

316.5

311.2

313.2

$\frac{322.7}{322.7}$

320.5

321.5

$\frac{8.9}{40}$

$\frac{6.9}{30}$

$\frac{3.6}{15}$

$\frac{0.4}{10}$

$\frac{1.4}{10}$

+23

0.23 319.92

11.06 330.98

R

R

1+73 330.98

Bm - 11.31 341.60
2+23 0.69 330.29

0+
+58

3+08

+
+58

+ 11.38 330.22
1.23 331.45

0.72 320.49
11.68 319.77

1+5m#14 11.18 309.31 309.36

(K

12

321.0 322.9 325.3 328.1 330.4
9.9 8.0 5.6 2.8 0.5
10 30 15 1 10

319.4 321.6 322.8 329.6 332.4 335.7 338.2
2.22 1.48 1.20 0.92 5.9 3.4
100 50 30 15 10 10

322.8 329.7 332.9 335.7 339.4 341.6
5.5 1.88 1.19 0.92 5.9 2.2 0.0
30 100 50 35 20 10

340.9
0.7
15
343.2
+1.6
15

(E

CHARLOMA ST. (35' St.)

S'W'ly from City View -
Base Line = N'ly prop. line -
0+00 = B.C. lot 6

441.98w 1x2ftub SW Cor Paradise & City View -

B^m#11

2

1.21 443.19

11.75 431.44

0.73 432.17

0+00 P.R.C.

11.65 420.52

0.20 420.72

3 +59

+91

2 1/2

11.64 409.08

1.28 410.36

1+41

B

+63

432.17

421.1 421.4 421.2 421.4

419.9 419.5

11.0 10.7 10.9 10.7
50 40 35 17.5

12.2 12.6
10

414.0 414.2 415.3 416.4 420.7 419.9 413.7 413.0 412.6

6.7 6.5 5.4 5.3 5.5 7.0 7.7 8.1
50 40 35 30 17.5 10 10 10

411.8 411.9 411.8 411.9 410.5 410.0 409.3

8.9 8.8 8.9 9.8 10.2 10.7 11.4
50 40 35 17.5 13 10 10

408.4 407.8 407.0 410.36 407.6 406.26 406.36

12.0 12.0 12.1 12.6 13.2 14.1 14.0
50 35 30 17.5 7 10 10

407.5 407.0 405.2 406.4 404.2 403.8

11.1 11.8 12.1 12.6 13.2 14.1 14.0
50 35 30 17.5 10 10

1488

A10.36

2408

730 PRC.

754

197 A01.23

777 Ret.

797

On Large Rad. Curve Produced

3+15

B_{hw}

11.10 399.26

A.02 397.21 397.18

T.P. on B.C. Hub - See Bk 343/24
58th St.

410.36

14

403.9	403.6	403.9	403.5	403.6	402.6
<u>6.5</u>	<u>6.8</u>	<u>6.5</u>	<u>6.9</u>	<u>6.8</u>	<u>7.8</u>
50	35	17.5	12		10

402.5	402.3	403.1	402.9	401.6	401.4	401.8
<u>7.9</u>	<u>8.1</u>	<u>7.3</u>	<u>7.5</u>	<u>8.8</u>	<u>9.0</u>	<u>8.6</u>
50	40	35	17.5	9		10

400.8	400.4	400.2	399.8	399.8	400.9	401.2
<u>9.5</u>	<u>9.9</u>	<u>10.1</u>	<u>10.5</u>	<u>10.6</u>	<u>9.5</u>	<u>9.2</u>
50	40	35	17.5	10		10

401.23

395.9	396.9	397.4	398.3	398.4
<u>5.3</u>	<u>4.3</u>	<u>2.8</u>	<u>2.9</u>	<u>2.8</u>
45	35	17.5		10

398.4	394.6	397.0	398.3	398.0
<u>7.8</u>	<u>6.6</u>	<u>4.2</u>	<u>2.9</u>	<u>3.2</u>
45	35	17.5		10

393.0	394.5	395.4	396.4	396.2	396.7
<u>8.7</u>	<u>6.7</u>	<u>5.8</u>	<u>4.8</u>	<u>5.0</u>	<u>4.5</u>
45	35	29	17.5		10

395.2	394.9	395.9	396.4	396.1	396.2
<u>6.0</u>	<u>6.3</u>	<u>5.3</u>	<u>4.8</u>	<u>5.1</u>	<u>5.0</u>
45	35	17.5	6		10

x

(K)

(B)

TROJAN ST.
30' St.

B₁#10

1.19 429.31

428.12

0-50

0.19 417.80

12.00 417.31

0+00 P.C.

+50

1+00

1.85 407.88

11.77 406.03

W'y from 58th St.

Base Line = Mix Prop Line -

0+00 = P.C., NW Cor Trojan & 58th.

1x2 tub AS E. 58th & Trojan -

(S) Lt

429.31

B₁(N)

420.2 420.1 419.0

418.3 417.8

9.1 9.2 10.3
50 30 15

11.0 11.5
10

415.8 415.6 415.5

414.6 413.9

2.0 1.4 1.3
50 30 15

3.2 3.9
10

412.4 412.1 411.9

411.0 409.9

5.4 5.7 5.9
50 30 15

6.8 7.9
10

410.8 410.0 409.7

418.0 417.5

8.5 9.3 10.6
50 30 15

11.3 11.8
10

407.88

1+50

1+79 2/5

2+29

+69 Ret-

2.28 398.14

+91

23
3+24

0.89 387.54

12.02 395.86

11.49 386.65

R

H

B¹⁶

407.88

402.88

405.73

405.08

404.18

50

402.2

$\frac{2.1}{50}$

$\frac{2.8}{30}$

$\frac{3.7}{15}$

$\frac{5.7}{10}$

409.2

401.7

402.0

401.6

401.2

$\frac{3.6}{50}$

$\frac{5.1}{30}$

$\frac{5.8}{15}$

$\frac{6.2}{10}$

$\frac{6.6}{10}$

400.0

399.1

398.5

398.3

397.9

$\frac{7.9}{50}$

$\frac{8.7}{30}$

$\frac{9.3}{15}$

$\frac{9.5}{10}$

$\frac{9.9}{10}$

397.8

396.6

395.8

395.3

394.3

$\frac{10.1}{50}$

$\frac{11.2}{30}$

$\frac{12.1}{15}$

$\frac{12.6}{10}$

$\frac{13.5}{10}$

398.14

395.7

394.6

394.5

393.5

392.3

$\frac{12.4}{50}$

$\frac{13.5}{30}$

$\frac{14.6}{15}$

$\frac{14.6}{10}$

$\frac{15.8}{10}$

393.6

391.6

389.8

387.7

386.0

$\frac{14.5}{50}$

$\frac{16.5}{30}$

$\frac{18.3}{15}$

$\frac{10.4}{10}$

$\frac{12.1}{10}$

R

387.54

3+59

35

+94

A.50 380.56

11.48 376.06

A+13

+29 B.C.

+58

+87

LH

387.54

R 17

387.5	384.4	381.7	379.0	377.6
<u>00</u>	<u>31</u>	<u>58</u>	<u>85</u>	<u>99</u>
50	30	15	10	10

380.3	372.0	375.7	374.0	373.6
<u>72</u>	<u>105</u>	<u>118</u>	<u>135</u>	<u>139</u>
50	30	15	10	10

380.56					
376.2	374.1	373.9	372.8	372.0	373.3
<u>43</u>	<u>64</u>	<u>71</u>	<u>77</u>	<u>86</u>	<u>72</u>
50	30	15	6	10	10

374.2	372.6	371.9	371.1	373.1	373.2
<u>63</u>	<u>79</u>	<u>86</u>	<u>94</u>	<u>74</u>	<u>73</u>
50	30	20	15	10	10

372.2	369.9	372.1	371.8	372.5	372.6	373.3
<u>83</u>	<u>106</u>	<u>84</u>	<u>87</u>	<u>80</u>	<u>79</u>	<u>72</u>
50	27	38	30	15	10	10

370.8	371.9	372.4	372.3	375.3
<u>97</u>	<u>86</u>	<u>81</u>	<u>67</u>	<u>52</u>
50	30	15	10	10

380.56

5+31 Car-St.

2.06 378.50

5.73 384.23

+81

6+81

7+81

Bm#23

5.73 378.50 378.50

See Bk #339/12

380.56

18

372.1

374.7

376.7

378.0

379.5

84

50

58

30

38

15

25

10

17

10

371.7

374.1

375.3

376.9

377.7

88

50

64

30

52

15

36

10

28

10

374.2

375.5

376.8

376.3

376.6

63

50

50

30

47

15

42

10

39

10

376.8

74

15

⊲

⊲

REGENT ST.
50'

Wily from 58th St.
Base Line = S'ly Prop. Line -
0+00 = PRC Lots

Bm# 9

0.31 405.73

0.28 394.03 11.98 393.75

0+00

0-40

T.P.

3.06 390.42

0+50

1+08 1/4

1+28 PRC

405.42^v

1x2 tub SECOR 58th & Meade -

ht

Rt
394.03

388.2	387.3	385.9	385.0	384.3	386.0	386.1	386.3
$\frac{55}{10}$	$\frac{67}{-}$	$\frac{81}{22}$	$\frac{9.0}{25}$	$\frac{9.7}{24}$	$\frac{9.0}{26}$	$\frac{1.9}{50}$	$\frac{7.7}{60}$

390.7	389.4	387.7	386.7	384.8	386.8	386.9	386.9
$\frac{3.1}{10}$	$\frac{4.6}{-}$	$\frac{6.3}{16}$	$\frac{7.9}{23}$	$\frac{9.2}{25}$	$\frac{7.2}{33}$	$\frac{7.1}{50}$	$\frac{7.1}{60}$

On 0+00 tub

386.3	385.8	386.3	390.42	384.6	382.3	384.5	384.9
$\frac{4.1}{10}$	$\frac{4.6}{-}$	$\frac{5.1}{15}$	$\frac{5.1}{25}$	$\frac{5.5}{43}$	$\frac{8.1}{46}$	$\frac{5.9}{50}$	$\frac{5.5}{60}$

385.0	384.5	384.0	383.9	383.8	383.1
$\frac{5.4}{10}$	$\frac{5.9}{-}$	$\frac{6.4}{6}$	$\frac{6.5}{25}$	$\frac{6.6}{50}$	$\frac{7.3}{60}$

384.3	383.9	383.7	383.5	381.4
$\frac{6.1}{10}$	$\frac{6.5}{-}$	$\frac{6.7}{25}$	$\frac{6.9}{50}$	$\frac{9.0}{60}$

390.42

1458

+89 4/6

10

2+29

+74 6/7

3.14 386.85

31

3+05

+39 7/8

Lt

382.8 383.5

$\frac{6.6}{10}$ $\frac{6.9}{-}$

384.6 383.4

$\frac{5.8}{10}$ $\frac{7.0}{-}$

387.5 386.1

$\frac{4.9}{10}$ $\frac{4.3}{-}$

388.4 387.3

$\frac{2.0}{10}$ $\frac{3.1}{-}$

388.2 386.0

$\frac{7.4}{10}$ $\frac{0.8}{-}$

387.7 385.4

$\frac{4.0}{10}$ $\frac{1.4}{-}$

382.7

$\frac{8.2}{14}$

382.2

$\frac{8.2}{14}$

383.7

$\frac{6.7}{11}$

386.4

$\frac{4.0}{6}$

383.3

$\frac{3.5}{17}$

383.2

$\frac{3.6}{14}$

Rt
390.42

20

383.1 381.6 382.9 383.4 380.5

$\frac{7.3}{25}$ $\frac{8.5}{31}$ $\frac{7.5}{39}$ $\frac{7.0}{50}$ $\frac{4.9}{6}$

382.4 380.6 381.5 382.1 381.8

$\frac{8.0}{25}$ $\frac{8.0}{31}$ $\frac{9.8}{39}$ $\frac{8.9}{44}$ $\frac{8.3}{50}$ $\frac{8.5}{60}$

381.7 381.8

$\frac{8.7}{50}$ $\frac{8.5}{60}$

389.6 380.7 380.2

$\frac{7.3}{25}$ $\frac{9.8}{40}$ $\frac{9.7}{50}$ $\frac{10.2}{60}$

386.85

382.7 380.5 379.5 379.3

$\frac{4.7}{25}$ $\frac{6.3}{37}$ $\frac{7.3}{50}$ $\frac{7.5}{60}$

380.9 378.3 378.3

$\frac{5.9}{25}$ $\frac{8.5}{50}$ $\frac{8.5}{60}$

R

R

386.85

3+89

230

4+39 Ret.

+89

Bk # 23

8.34 378.51 378.50^v

387.4 384.5 382.4 378.7 377.0 377.1

+ 0.6 2.3 4.4 9.1 9.8 9.7
10 8 25 50 60

386.2 384.8 378.9 376.9 375.9

0.6 2.4 8.1 10.9 10.9
10 8 25 50 60

386.6 384.0 377.7 377.2 374.9 374.6

0.2 4.8 7.1 9.6 12.1 12.2
10 8 16 25 50 60

See Bk # 339/12

CLAREMONT WAY.
(35 St.)

E'ly from 58th St.

Baseline = N'ly of St.
0+00 = P.R.C.

25

B. In

387.36 See Pg. 19 (T.P.)

11.61 398.97
10.58 408.74 0.81 398.16

408.7

398.4 398.6 399.5 400.9 401.4

0400

$\frac{10.3}{10}$ $\frac{10.1}{10}$ $\frac{9.2}{17.5}$ $\frac{7.8}{35}$ $\frac{7.3}{45}$

405.2 405.4 406.3 407.2 407.9

+52

$\frac{3.5}{10}$ $\frac{3.3}{10}$ $\frac{2.1}{17.5}$ $\frac{1.5}{35}$ $\frac{0.8}{45}$

11.67 419.18 1.23 407.51

419.18

408.4 409.6 410.5 412.4 414.1

+96 $\frac{7}{A}$ / $\frac{7}{B}$

$\frac{10.7}{10}$ $\frac{9.5}{10}$ $\frac{8.6}{17.5}$ $\frac{6.7}{35}$ $\frac{5.0}{45}$

35

412.8 413.5 415.2 417.0 419.2

141

$\frac{6.3}{10}$ $\frac{5.6}{10}$ $\frac{3.9}{17.5}$ $\frac{2.1}{35}$ $\frac{0.9}{45}$

11.56 429.48

1.26 417.92

R

B

429.48

456

$$\begin{array}{r} 420.3 \\ 9.1 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 422.0 \\ 14 \\ \hline \end{array}$$

429.48

23

$$\begin{array}{r} 424.6 \\ 1.8 \\ \hline 17.5 \end{array}$$

$$\begin{array}{r} 426.5 \\ 29 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 429.18 \\ 0.3 \\ \hline 50 \end{array}$$

481

$$\begin{array}{r} 428.1 \\ 3.3 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 427.3 \\ 21 \\ \hline \end{array}$$

$$\begin{array}{r} 428.0 \\ 0.5 \\ \hline 17.5 \end{array}$$

$$\begin{array}{r} 432.28 \\ 1.8 \\ \hline 30 \\ \text{Banjo} \end{array}$$

$$\begin{array}{r} 433.58 \\ 4.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 436.78 \\ 5.3 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 435.58 \\ 6.1 \\ \hline 70 \end{array}$$

2105

$$\begin{array}{r} 430.48 \\ 1.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 431.78 \\ 2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 434.28 \\ 1.8 \\ \hline 17.5 \end{array}$$

$$\begin{array}{r} 436.78 \\ 7.3 \\ \hline 35 \end{array}$$

$$\begin{array}{r} 438.38 \\ 8.9 \\ \hline 50 \end{array}$$

11.66 417.82

0.29 418.11

1.18 407.84 11.45 406.66

11.60 396.24

0.60 396.84

9.48 387.36 387.36 See T.P. Pg. 22

FRANCES WAY
(35')

Btw #22

1.32 432.33

0+00 P.I.

+20 Ret

11.67 420.66

2.64 423.30

+50

+90

431.01^v

Sly from Meade-

Base Line = Sly Prop Line

0+00 = P.I. of Ret - Lot #6

See Bk #339/13 -

	419.7	421.0	432.33	423.4	425.8	427.3
	<u>12.6</u>	<u>11.3</u>		<u>8.9</u>	<u>6.5</u>	<u>5.0</u>
	10			17.5	35	45

419.3
13.0

424.5
7.8
35

416.1 417.6
15.2 5.7
10

423.30
419.8
3.5
17.5

422.7 424.5
0.6 11.7
35 45

413.5 414.8
9.8 8.5
10

416.3 417.4 418.1 418.7
7.0 5.9 5.2 4.6
17.5 23 35 45

423.30

1415

3.54 414.98

11.86 411.44

185

77 BC

35

247

10.61 425.11

0.48 414.50

0.67 424.44

8.31 432.75

B7#22

1.76 430.99 431.01

25

423.3

411.5 412.4

$\frac{118}{10}$ $\frac{109}{10}$

414.3

416.1 417.1

$\frac{90}{17.5}$

$\frac{72}{35}$ $\frac{62}{45}$

414.44

407.44 412.8

$\frac{75}{10}$ $\frac{67}{10}$

409.58

411.38

412.68

413.78

$\frac{51}{17.5}$

$\frac{36}{35}$

$\frac{23}{50}$

$\frac{15}{60}$

405.98 406.08

$\frac{95}{10}$ $\frac{89}{10}$

407.38

409.18

410.68

412.58

413.78

$\frac{76}{17.5}$

$\frac{58}{35}$

$\frac{43}{52.5}$

$\frac{28}{70}$

$\frac{15}{80}$

402.08 402.28

$\frac{129}{10}$ $\frac{127}{10}$

403.58

404.28

405.98

$\frac{114}{17.5}$

$\frac{107}{35}$

$\frac{95}{50}$

56TH ST.

Sly from Meade-

2C

Base Line = E. Prop. Line
0+00 = P.I. S.E. Cor St

B_m#22

2.86 433.87

431.01

See 339/13

21 (E)

433.87 Pt. (W)

0+00 P.I.

424.27	424.27	424.07	424.27	423.57	424.17	423.87
$\frac{9.6}{10}$	$\frac{9.6}{10}$	$\frac{9.8}{10}$	$\frac{9.6}{20}$	$\frac{10.3}{24}$	$\frac{9.7}{37}$	$\frac{10.3}{50}$

0-50

425.5	425.3	425.2	424.9	423.8	424.7	423.9
$\frac{8.3}{10}$	$\frac{8.5}{10}$	$\frac{8.6}{10}$	$\frac{8.9}{20}$	$\frac{9.5}{27}$	$\frac{9.1}{33}$	$\frac{9.9}{50}$

0-150

425.5	425.1	424.9	424.5	423.8	423.9
$\frac{8.3}{10}$	$\frac{8.7}{10}$	$\frac{8.9}{10}$	$\frac{9.3}{20}$	$\frac{10.3}{31}$	$\frac{10.4}{50}$

0-200

0.85 425.84

11.85 427.02

$\frac{425.5}{8.3}$
422.84

0+50

422.7	422.6	422.6	422.4	421.6	422.4	421.7+
$\frac{0.1}{10}$	$\frac{0.2}{10}$	$\frac{0.2}{10}$	$\frac{0.4}{20}$	$\frac{1.2}{20}$	$\frac{0.7}{37}$	$\frac{1.1}{50}$

B

B

422.84

1400

+50

+74 14/15

0.49 411.81

2+34 15/16

+94 16/17

0.36 400.66

3+54 17/18

Lt.

422.84

Rt.

27

419.8 419.6

418.8 418.2 417.6 417.2 417.3 417.5

$\frac{30}{10}$ $\frac{3.2}{10}$

$\frac{40}{10}$ $\frac{46}{18}$ $\frac{52}{20}$ $\frac{56}{24}$ $\frac{55}{33}$ $\frac{53}{50}$

416.2 415.5

415.0 414.9 414.0 414.4 413.9

$\frac{66}{10}$ $\frac{73}{10}$

$\frac{78}{10}$ $\frac{81}{20}$ $\frac{88}{21}$ $\frac{84}{30}$ $\frac{89}{50}$

414.2 414.1

413.9 413.8 412.7 413.2 412.7

$\frac{86}{10}$ $\frac{87}{10}$

$\frac{89}{10}$ $\frac{90}{20}$ $\frac{101}{23}$ $\frac{96}{29}$ $\frac{101}{50}$

411.81

410.3 410.0

409.9 409.9 409.4 409.8 408.8

$\frac{15}{10}$ $\frac{18}{10}$

$\frac{19}{10}$ $\frac{19}{18}$ $\frac{24}{20}$ $\frac{20}{25}$ $\frac{30}{50}$

404.1 404.0

403.8 403.6 404.1 403.9

$\frac{77}{10}$ $\frac{7.8}{10}$

$\frac{80}{10}$ $\frac{82}{20}$ $\frac{77}{33}$ $\frac{79}{50}$

400.66

397.6 397.6

396.9 397.2 397.0 397.4

$\frac{31}{10}$ $\frac{31}{10}$

$\frac{38}{10}$ $\frac{35}{20}$ $\frac{37}{32}$ $\frac{33}{50}$

400.66

4+14 8/19

11.98 388.68

0.52 389.20

4+74 19/20

5+24

+74

5+990 P.I.

B-#23

1.19 379.69

10.68 378.52 378.50

6+29 Boundary

<u>392.1</u>	<u>392.0</u>	<u>392.7</u>	<u>391.8</u>	<u>391.8</u>	<u>391.1</u>
<u>86</u>	<u>87</u>	<u>80</u>	<u>89</u>	<u>89</u>	<u>96</u>
<u>10</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>32</u>	<u>50</u>
<hr/>					
<u>389.20</u>					

<u>388.6</u>	<u>387.8</u>	<u>387.9</u>	<u>387.8</u>	<u>387.2</u>
<u>0.6</u>	<u>1.4</u>	<u>1.3</u>	<u>1.4</u>	<u>2.0</u>
<u>10</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>50</u>

<u>385.1</u>	<u>384.7</u>	<u>384.6</u>	<u>384.5</u>	<u>384.7</u>
<u>4.1</u>	<u>4.5</u>	<u>4.6</u>	<u>4.7</u>	<u>4.5</u>
<u>10</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>50</u>

<u>380.2</u>	<u>380.8</u>	<u>381.2</u>	<u>381.6</u>	<u>381.8</u>	<u>381.8</u>
<u>9.0</u>	<u>8.4</u>	<u>8.0</u>	<u>7.6</u>	<u>7.4</u>	<u>7.4</u>
<u>10</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>50</u>

<u>377.4</u>	<u>378.1</u>	<u>378.4</u>	<u>379.0</u>	<u>379.1</u>	<u>379.1</u>	<u>380.3</u>
<u>11.8</u>	<u>11.1</u>	<u>10.8</u>	<u>10.2</u>	<u>10.1</u>	<u>9.5</u>	<u>8.9</u>
<u>10</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>37</u>	<u>50</u>
<hr/>						
<u>379.69</u>						

<u>373.5</u>	<u>374.6</u>	<u>374.9</u>	<u>375.5</u>	<u>376.6</u>	<u>377.5</u>
<u>6.2</u>	<u>5.1</u>	<u>4.8</u>	<u>4.2</u>	<u>3.1</u>	<u>2.2</u>
<u>10</u>	<u>10</u>	<u>10</u>	<u>20</u>	<u>31</u>	<u>50</u>

379.69

6+9.0

$$\begin{array}{r} 368.8 \\ 10.9 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 368.4 \\ 11.3 \\ \hline \end{array}$$

$$\begin{array}{r} 368.7 \\ 10.8 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 368.7 \\ 10.8 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 367.9 \\ 9.5 \\ \hline 50 \end{array}$$

7+4.0

$$\begin{array}{r} 371.8 \\ 7.9 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 370.3 \\ 9.4 \\ \hline \end{array}$$

$$\begin{array}{r} 369.5 \\ 10.2 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 368.8 \\ 10.9 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 367.6 \\ 9.1 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 368.1 \\ 11.6 \\ \hline 50 \end{array}$$

+9.0

$$\begin{array}{r} 381.7 \\ 12.0 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 380.5 \\ 10.8 \\ \hline \end{array}$$

$$\begin{array}{r} 378.4 \\ 13 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 376.3 \\ 3.4 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 370.7 \\ 9.0 \\ \hline 50 \end{array}$$

8+4.0

$$\begin{array}{r} 385.3 \\ 15.6 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 384.2 \\ 14.5 \\ \hline \end{array}$$

$$\begin{array}{r} 384.1 \\ 14.4 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 383.6 \\ 13.9 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 379.2 \\ 0.5 \\ \hline 50 \end{array}$$

Bm#23

1.19 378.50 378.50

CAMPBELL DR.

S' E'ly from Meade

Base Line = N. Easterly Prop. Line -
0+00 = P.I. S.E. Cor. St -

30

Btmc

10.93 465.90

454.97" See Bk# 339/6 465.9

0+00

462.3	462.2	461.5	460.6	461.2	362.0
$\frac{3.6}{10}$	$\frac{3.7}{10}$	$\frac{4.4}{28}$	$\frac{5.3}{47}$	$\frac{4.9}{48}$	$\frac{1.7}{50}$
				$\frac{3.9}{60}$	

+35

463.1	462.9	462.8	462.7	461.7	461.1
$\frac{2.8}{10}$	$\frac{3.1}{10}$	$\frac{3.1}{25}$	$\frac{3.0}{34}$	$\frac{4.5}{50}$	$\frac{4.8}{60}$

+59 Ret.

464.4	464.2	463.5	462.8	462.1	462.4
$\frac{1.5}{10}$	$\frac{1.7}{10}$	$\frac{2.4}{3}$	$\frac{3.1}{25}$	$\frac{3.8}{50}$	$\frac{3.5}{60}$
464.7	464.5	463.6	464.3	464.3	463.1
$\frac{1.0}{10}$	$\frac{1.4}{10}$	$\frac{2.3}{4}$	$\frac{1.6}{25}$	$\frac{1.6}{33}$	$\frac{2.8}{50}$
					$\frac{3.4}{60}$

33
+92

1.28 464.64

470.28

5.66 470.28

1+33

464.9	464.7	464.0	463.0	463.3	462.7	462.8
$\frac{5.4}{10}$	$\frac{5.4}{10}$	$\frac{6.3}{25}$	$\frac{7.2}{34}$	$\frac{6.9}{46}$	$\frac{1.5}{50}$	$\frac{1.4}{60}$

R

R

47028

1462 1/2

15

2407

141 2/6

+91

3421

156 REC.

31

470.28

469.9	464.6		469.8	464.4	463.5	462.6
5.4	5.7	465.2	5.5	5.9	6.7	7.6
<u>10</u>	<u>11</u>		<u>25</u>	<u>41</u>	<u>50</u>	<u>60</u>

465.8	465.3	465.2	464.1	464.3
4.8	5.0	5.1	6.2	6.0
<u>10</u>	<u>11</u>	<u>25</u>	<u>50</u>	<u>60</u>

466.0	465.7	465.0	464.4	464.7	464.7
4.3	4.6	5.3	5.9	5.6	5.5
<u>10</u>	<u>11</u>	<u>25</u>	<u>49</u>	<u>50</u>	<u>60</u>

465.6	465.3	465.0	464.9	465.2	464.7
4.7	5.0	5.3	5.4	5.1	5.6
<u>10</u>	<u>11</u>	<u>25</u>	<u>49</u>	<u>50</u>	<u>60</u>

465.7	465.2	465.0	464.1	464.4	464.3
4.6	5.1	5.3	6.2	5.9	6.0
<u>10</u>	<u>11</u>	<u>25</u>	<u>49</u>	<u>50</u>	<u>60</u>

465.6	466.1	466.4	466.3	465.8	465.2	464.7	464.6	464.7
4.7	4.2	3.9	4.0	4.5	5.1	5.6	5.7	6.1
<u>10</u>	<u>11</u>	<u>5</u>	<u>21</u>	<u>25</u>	<u>34</u>	<u>49</u>	<u>50</u>	<u>60</u>

R

R

47028

470.28

32

3+73 6h

465.4	465.4	465.4	465.4	464.9	464.3
$\frac{19}{10}$	$\frac{19}{10}$	$\frac{19}{25}$	$\frac{19}{20}$	$\frac{54}{50}$	$\frac{60}{60}$

39
4+12

465.1	465.3	465.9	466.0	465.2	464.8	464.5
$\frac{52}{10}$	$\frac{50}{10}$	$\frac{44}{16}$	$\frac{43}{25}$	$\frac{51}{37}$	$\frac{55}{50}$	$\frac{58}{60}$

43
4+55

463.6	463.8	464.2	464.8	464.3	464.6	464.5
$\frac{67}{10}$	$\frac{65}{10}$	$\frac{61}{25}$	$\frac{55}{43}$	$\frac{60}{47}$	$\frac{57}{50}$	$\frac{58}{60}$

483 7/8

460.1	460.9	462.8	463.9	463.8	464.2	464.1
$\frac{10.7}{10}$	$\frac{94}{10}$	$\frac{7.5}{25}$	$\frac{64}{35}$	$\frac{65}{47}$	$\frac{61}{50}$	$\frac{62}{60}$

1.00 461.82

9.46 460.82

Rock near 7/8

5+33

461.58	462.48	467.18	467.88	469.68	470.48	470.78
8.7	7.4	3.1	0.4	0.6	10.2	10.5
$\frac{8.7}{10}$	$\frac{7.4}{10}$	$\frac{3.1}{25}$	$\frac{0.4}{25}$	$\frac{0.6}{47}$	$\frac{10.2}{50}$	$\frac{10.5}{60}$

T.P.

0.42 454.57

7.67 454.15

Tap Hub 9/12 So. Side Lt.

454.57

5+66

<u>458.0</u>	<u>452.2</u>	<u>453.4</u>
<u>46</u>	<u>24</u>	<u>12</u>
<u>10</u>		<u>18</u>

+98

<u>445.6</u>	<u>447.4</u>
<u>9.0</u>	<u>72</u>
<u>10</u>	

6+27 EC.

11.87 AA2.70

0.52 AA3.42

+77

<u>443.0</u>	<u>444.5</u>	<u>445.7</u>	<u>449.7</u>	<u>451.4</u>	<u>452.7</u>	<u>454.2</u>
<u>16</u>	<u>105</u>	<u>89</u>	<u>19</u>	<u>32</u>	<u>19</u>	<u>04</u>
<u>10</u>		<u>10</u>	<u>25</u>	<u>42</u>	<u>50</u>	<u>60</u>

443.22

7+27

11.49 A31.73

0.46 A32.19

+50

<u>437.5</u>	<u>439.4</u>	<u>440.2</u>	<u>442.7</u>	<u>445.1</u>	<u>446.7</u>	<u>448.2</u>
<u>57</u>	<u>38</u>	<u>30</u>	<u>05</u>	<u>19</u>	<u>35</u>	<u>50</u>
<u>10</u>		<u>7</u>	<u>25</u>	<u>42</u>	<u>50</u>	<u>60</u>

<u>430.1</u>	<u>431.7</u>	<u>435.9</u>	<u>440.1</u>	<u>441.0</u>
<u>13</u>	<u>11.5</u>	<u>7.3</u>	<u>3.1</u>	<u>2.2</u>
<u>10</u>		<u>25</u>	<u>50</u>	<u>60</u>

432.19

<u>427.5</u>	<u>430.3</u>	<u>431.9</u>	<u>432.6</u>	<u>435.9</u>	<u>436.3</u>
<u>17</u>	<u>19</u>	<u>03</u>	<u>10.4</u>	<u>37</u>	<u>1.1</u>
<u>10</u>		<u>25</u>	<u>30</u>	<u>50</u>	<u>60</u>

454.57

33

R

432.19

8+00

<u>423.9</u>	<u>424.8</u>	<u>427.0</u>	<u>428.4</u>	<u>431.3</u>	<u>433.0</u>
<u>8.3</u>	<u>7.4</u>	<u>5.2</u>	<u>3.8</u>	<u>0.9</u>	<u>+0.8</u>
<u>10</u>	<u>-</u>	<u>19</u>	<u>28</u>	<u>50</u>	<u>60</u>

423.2

9.0

+50

0.23 431.96

11.97 443.93

11.65 455.05 0.53 443.40

11.36 465.49 0.92 454.13

5.22 469.62 1.09 464.40

0.43 461.63 8.42 461.20

BW#6

6.67 454.96 454.97

See Bk#339/6

Profile MEADE Ave - East from 60th St - = 0+00 on E

BW#6 9.54 464.51

454.97

0 16.7 447.8

+50 10.4 454.1

1 4.6 459.9

+50 2.2 462.3

2 0.9 463.6

+50 0.4 464.1

3 0.0 464.5

8

Profile of
MEADE AVE
West from 58th St.

0+00 = West line Meade on E

BM#9			405.42
	11.47	416.89	
0		5.2	411.7
+50		1.5	412.4
1		5.1	411.8
+50		3.9	413.0
	11.06	427.33	0.62 416.27
2		8.6	418.7
+50		1.5	425.8
	11.53	438.47	0.39 426.94
3		6.5	432.0
+50		4.0	434.5
4		5.4	433.1
+50		7.0	431.5
BM#22		6.45	432.02 431.01

cked. - by JVB

June 3-4-6-1927

Regent St 0-6

Clarendon 0-7

Frances 0-2

56th 1000'