Job # 88

NAME Broadway Extension

Book # 8.

Class ..... Course ..... Party .....

"A" Line.

69

1966

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN CO.
MANUFACTURERS
DRAWING MATERIALS
MATHEMATICAL AND SURVEYING INSTRUMENTS
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CHICAGO SAN FRANCISCO NEW YORK
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BROADWAY EXTENSION

Massachusetts Ave.

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Property of
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508 Spreckles Bldg.
San Diego

— INDEX —

Survey of

MASSACHUSETTS AVE.
(Lemon Grove)

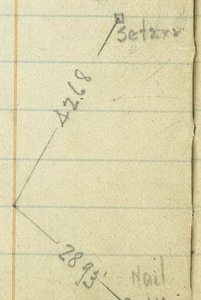
Sta.	Dist.	Angle Azimuth	Deflection	℄ Ties –
4+37.35 P.I.		160° 10' 320° 20'	19°50' Lt.	

5/21/26
Coote
Losey
Ball

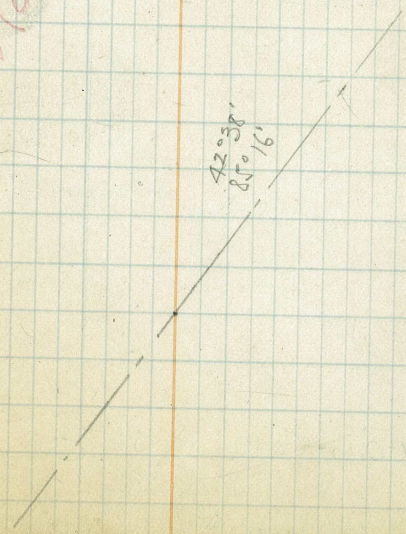
Field

0+00 =
76+74.6 ±
R.D.I.# 21

MASSACHUSETTS AVE.
— Line Change —



Field
Adopted Alignment
on P.S. 6

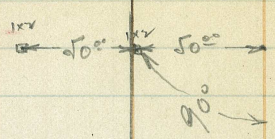


1

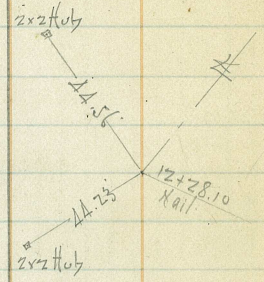
Sta. ↑ Dist. Angles- Azimuth Def. ℄ Ties-

18+88.60
15+51.10 =
↓

Equation



14+24.50
P.O.T.



12+28.10
P.I.

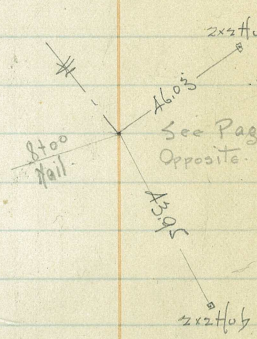
214° 18'
+ 68° 35'

34-18 RT ✓

8+00
P.I.

134° 22'
268° 45'

45-38 LT ✓



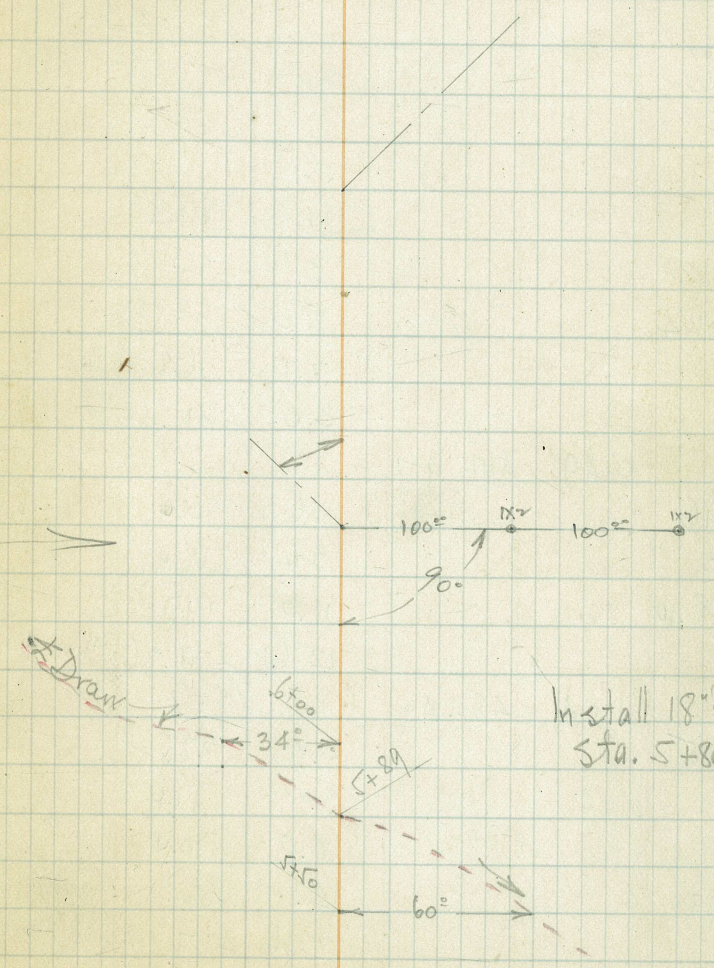
690.40

4+37.35

Continued from Pg 6

2

Contd in BK. # 7, Pg. 3



Install 18" Pipe
Sta. 5+89

Profile of Line Chg –

Bk #3				498.01
	6.48	504.49		
18+88.60				
15+51.10 =			9r	4953
15			6.6	47.9
14 +4r			3.1	01.4
+24			5.0	49.5
14			7.7	96.8
			13.01	491.48
	0.49	491.97		
13+16			1.6	90.4
13			3.6	88.4
12+28.10			11.3	80.7
			12.61	479.36
	1.04	480.40		
12+15			2.9	77.5
12			3.0	77.4
11			10.0.	70.4
10+78			14.1	66.3
			12.96	467.44
	0.54	467.98		

Transit notes
Pgs. 1 – 2
This Book

Cut 8 ft

		467.98		
10			6.1	61.9
9			12.3	55.7
			12.6✓	455.36
	1.26	456.62		
8+51			2.4	54.✓
Blu			5.39	451.23
8			6.7	44.5
			12.57	444.05
	0.10	444.15		
6+8			6.7	37.5
			8.8	35.4
			13.0✓	431.13
	0.58	431.71		
6			16.6	15.1
5+89			18.7	13.0
+40			9.6	22.1
↓			21	28.9
+68			1.0	30.7
			0.98	430.73
	0.90	431.63		

Ore Hub 15 W. 8+00

4 grade

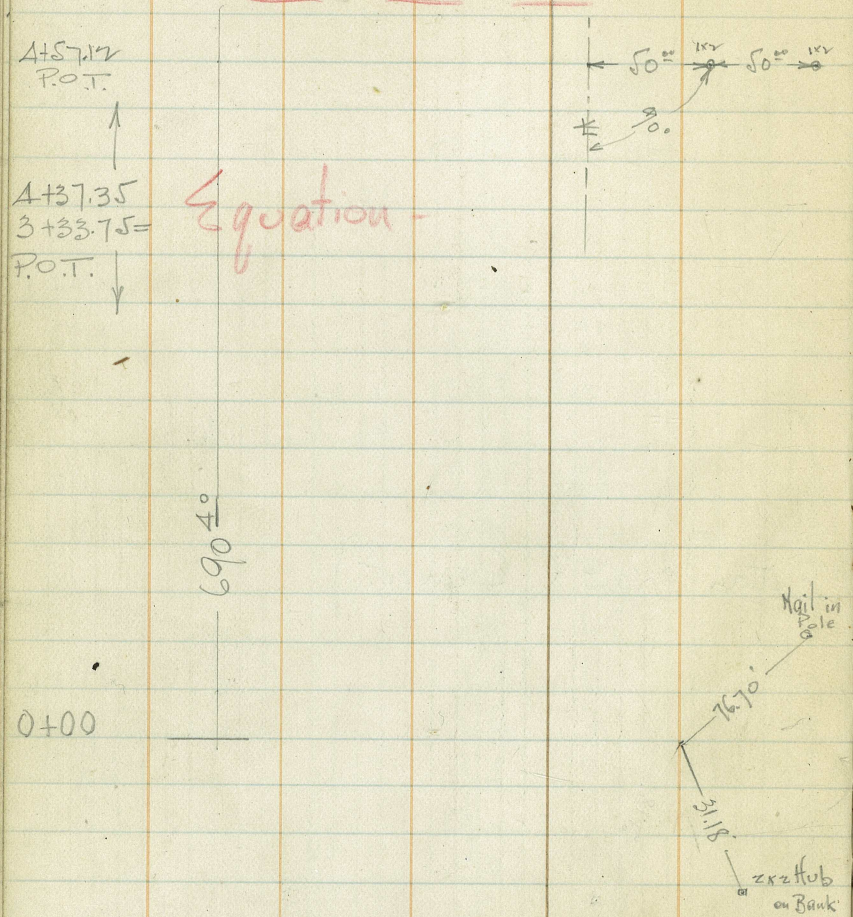
		431.63			
4+37.35			12.6	29.0	
4			5.5	26.1	
3+50			7.5	24.1	
			12.71	418.9 ✓	
	10.3	419.95			
3			3.C	16.4	
2+90			5.1	14.9	
+71			11.2	08.8	
			12.68	407.27	
	6.41	413.68			
2			8.4.	5.3	
1+21			7.3	6.4	
+17			10.0	3.7	
1			9.9	4.8	
0+98			7.3	6.4	
+75			6.6	7.1	
+64			9.4	4.3	
+43			9.2	4.5	
+32			4.9	8.8	
0+00=			4.8	8.9	
76+746					
RD1#21			3.41	410.27	
	6.80	417.07			
Blk#0			1.07	416.05	416.00

Bottom Draw (Sewer)

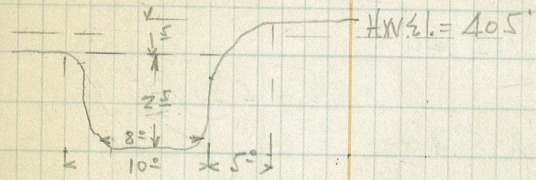
5/25/26
Coote
Losey
Spansel

Sta. | Dist | Angle Az. | Angle Def.

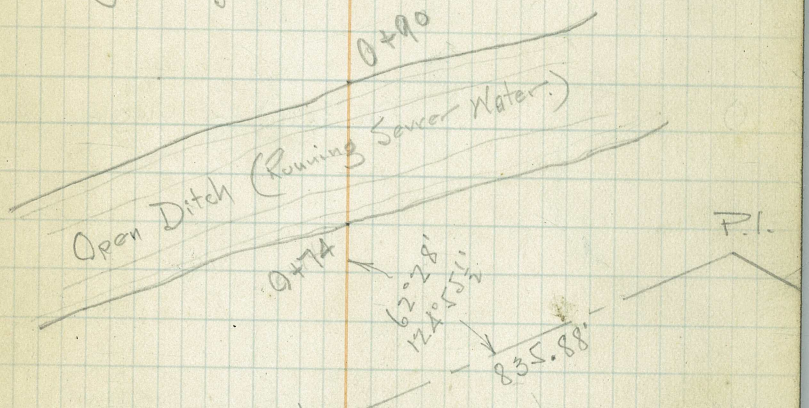
Cont'd on Pg. 2



MASSACHUSETTS AVE.
Change in Alignment



Cross Section of Ditch -



Use R = 200'

Level notes Pg. 7 this Bk.

117-37

BM					416.00
	1.50	417.50			
			6.68	410.82	
	4.67	415.49			
BM			1.02	414.47	
	1.43	415.90			
0+00			Along ℄ RD1 #21		
0			On split of angle		
+28					
+50					

Lt. Rt. 7

See Notes for RD1 #21 for description -

5/28/26
Coote
Dosey
Spansel

R.R. Spk. in Tel. Pole
HI = 415.90

8.4	8.2	7.7	7.0	6.9	
7.5	7.7	8.3	8.9	9.0	
100	50		50	100	

2.6	4.6	8.5	8.6	7.5	7.7	7.4
13.3	11.3	7.4	7.3	8.4	8.2	8.5
49	44	34	24	21		31

3.0	5.8	6.4
12.9	10.1	9.5
66	74	94

6.0	5.1	2.6	2.7	6.0	8.7	8.0	7.3	6.3
9.9	10.8	13.1	13.4	9.9	7.2	7.9	8.6	9.1
70	53	46	28	17		20	21	50

5.1	3.3	3.3	5.1	5.6	3.4	2.8	3.5	6.4	7.1	7.1
10.8	12.6	12.6	10.8	10.3	12.5	13.1	12.4	9.5	8.8	7.8
65	50	46	36	14	5		10	20	34	38 + 40

A15.90

0.+61

+74

10.75 A05.35

A.57 A09.72

+79

+88

HW.Elev = 404.9

+90

A.57 A05.35

6.18 A11.33

0.+83

* Wash on angle of same

1.+20

+66

2+. Rf 8

4.8 3.9 3.0 2.9 5.3 5.2 4.4 3.1 3.9 6.3 7.5
11.1 12.0 12.9 13.0 10.6 10.6 11.5 12.8 12.0 9.6 8.4
60 50 40 28 18 7 16 26 34 5

4.7 4.7 4.3 2.3 2.6 5.1 5.1 4.8 3.1
11.2 11.2 11.6 13.6 13.3 10.8 10.8 11.1 12.5
75 50 33 31 10 18 37 48

5.3 5.3 4.4 4.1 3.9 1.6 1.9 4.5 5.2 5.2 3.0
44 44 5.3 5.6 5.8 7.9 7.8 5.7 4.5 4.5 6.7
60 50 37 20 11 10 6 16 31 49

5.2 5.1 4.4 4.1 1.9 1.6 5.4 5.1
4.5 4.6 5.3 5.6 7.8 7.9 4.3 4.6
60 50 25 3 18 37 40

5.2 5.1 4.5 4.1 1.8 5.4 5.1
4.5 4.6 5.2 5.6 7.9 4.3 4.6
60 50 25 21 36 40

4.1 3.5 3.4 2.3 1.7 1.9 1.6 0.6
7.2 7.8 7.9 9.0 9.6 9.4 9.7 10.7
200 150 100 50 50 100 150

4.7 4.5 3.6 3.1 3.0 2.6
6.6 6.8 7.5 8.2 8.3 8.7
50 30 20 39 50

3.1 4.3 3.8 4.7 5.6 6.2 7.1
8.2 7.9 7.5 6.6 5.5 5.1 4.2
40 40 13 26 40 50

	411.33			
1+90				
		0.6	410.71	
	11.60	422.31		
2				
+23				
+50				
+86				
		0.87	421.44	
	11.60	433.04		
+81				
3+12				
+3375=				
4+37.35				

9.8 7.9 5.8 4.7 3.4
15 34 5.6 6.6 7.9
40 20 20 40

13.9 13.3 11.3 10.2 7.5 5.5 4.7
8.4 9.0 11.0 12.1 14.8 16.8 17.6
40 36 25 17 20 40

19.1 18.0 15.6 16.3 15.7 15.8 8.8 6.2
3.2 4.3 6.7 6.0 6.6 6.8 14.5 16.1
40 35 21 9 1 27 40

26.4 26.0 23.8 21.7 19.1 16.4 13.6 10.4
+4.1 +3.7 +1.5 0.6 3.2 5.9 8.7 11.4
40 35 21 7 15 30 40

25.8 24.8 23.2 22.4 20.7 18.9 16.9 15.6 13.6 11.3
+3.5 +2.5 +1.1 +0.1 1.6 3.4 5.5 6.7 8.7 11.0
40 32 22 10 1 14 23 34 40

25.6 27.2 26.1 24.8 23.8 22.6 20.6 19.6 16.5
4.4 5.6 6.9 8.2 9.2 10.4 12.4 13.4 16.5
40 33 23 13 8 20 29 40

32.8 31.0 29.4 28.4 25.7 24.5 23.6 21.6 20.8
0.2 2.0 3.6 4.6 7.3 8.5 9.4 11.4 12.2
40 29 20 14 12 24 36 40

34.0 30.6 28.9 28.0 24.9 22.3
+1.0 2.2 4.1 5.0 8.1 10.7
40 19 7 24 40

433.04

4+70

3.26 429.78

0.60 - 430.38

5

+50

11.91 418.47

2.24 420.71

+63

+89

± Draw

+89

On Angle of Draw

6

+16

0.20 420.51

11.31 431.82

36.0 33.7 30.3 27.3 24.1
+3.0 +0.7 2.7 5.7 8.9
40 20 20 40

33.7 31.5 28.4 25.4 23.6 21.9
+3.3 +1.1 1.5 4.6 7.6 8.5
40 20 19 30 40

26.7 24.2 19.6 16.2 20.9
3.7 6.2 10.8 14.2 9.5
40 20 20 40

24.1 20.2 16.4 15.5 13.9 12.4 10.8 9.8 10.7
+3.4 0.5 4.3 5.2 6.8 8.3 9.9 11.9 10.0
40 20 13 21 30 38 48 60
8 Draws

15.9 14.7 14.0 11.6 12.0 12.5 13.6
4.8 6.0 6.7 9.1 8.7 8.2 7.1 Same Slop
40 31 20 11 22 40 15

14.0 15.5 13.4 11.6 9.0 6.3
2.7 5.2 7.3 9.1 11.7 14.4
150 100 50 50 100

14.8 14.4 12.4 14.1 13.8 13.8 15.1
Same Slope 5.9 6.3 8.3 6.6 6.9 6.9 5.6 Same Slop
20 50 44 40 25 20 40 10

17.0 16.9 16.3 16.9 16.8 17.6 19.3 19.2 18.1 19.2
3.7 3.8 4.4 3.8 3.9 3.1 1.4 1.5 2.6 1.5
50 40 37 20 10 20 32 40 50

A31.8 r

6+50

+68

0.37 A31.45

12.11 A43.56

+79

7

+20

X 1.0r A42.54

11.61 A54.35

+46

8+00 On split of angle -

B.M. 2.96 A51.29 A51.23

+50

26.3 25.4 26.3 26.6 26.3 26.0
5.5 6.4 5.5 5.r 3.5 3.8
A0 28 18 2r A0

31.r 29.9 30.6 31.r 31.7 33.3 33.5
0.6 1.9 1.0 0.6 0.1 +1.5 +1.7
20 28 17 15 3r A0

33.7 33.3 35.4 35.6 34.6 35.4
9.9 10.3 8.r 8.0 9.0 8.2
A0 18 11 23 A0

37.r 36.4 37.4 37.4 37.9 37.7 38.4
6.4 6.8 6.r 6.r 5.7 5.9 5.2
A0 37 23 15 58 A0

40.r 40.6 40.7 31.6 40.r 40.7 41.0
3.4 2.8 2.9 A.1 3.4 2.9 2.6
50 A0 33 21 21 A0

43.9 43.4 43.1 43.4 44.8 44.0 44.7 44.6 44.4
10.5 11.2 11.3 11.0 9.6 10.4 9.7 9.5 10.0
60 50 A5 A0 20 1r 1A 30

44.1 45.4 47.5 46.4 50.1 51.4
10.3 9.0 6.9 5.6 4.3 3.0
15 5.r A0 26 20

On Hub 15' West 8+00 (See Pg. 4)

46.9 47.9 46.6 51.4 52.0 53.6 54.4 54.6 55.5 58.r
7.5 6.5 5.8 3.0 2.A 0.8 0.0 +0.A +1.1 +3.8
60 50 A7 34 2r 13 19 20 A0

454.35

6 0.33 454.02

11.14 465.16

9

+29

+50

10

0.70 464.46

10.95 475.41

+50

+75

11

52.3 53.4 55.9 55.9 56.7 58.0 58.8
12.9 11.4 9.3 9.3 8.5 7.2 6.4
40 32 13 15 26 40

54.3 55.0 56.1 57.1 57.9 59.3 60.9 61.5 61.4
10.9 10.2 9.1 8.1 7.3 5.9 4.3 3.7 3.8
40 34 27 10 14 24 37 40

56.5 56.6 56.1 61.0 63.0
8.7 8.6 6.1 4.2 2.2
40 27 26 40

59.2 60.2 62.0 62.1 63.1 64.0 65.5
6.0 5.0 3.2 3.1 2.1 1.2 +0.3
40 28 16 21 35 40

61.8 63.2 64.9 65.6 66.2 67.4 68.4
13.6 12.3 10.5 9.8 9.2 7.5 7.0
40 27 10 27 34 40

64.0 64.4 64.8 66.2 68.8 71.5 71.5
11.4 11.0 10.6 9.2 6.6 3.9 3.9
40 35 16 27 37 40

64.8 68.2 67.5 70.4 71.9 74.1 74.9
10.6 9.7 7.9 5.0 3.5 1.3 0.5
40 35 15 15 33 40

475.41

11+50

0.54 474.87

11.24 486.11

12

+28.10

On split of angle—

+56

0.47 485.64

10.31 495.95

T.P.

1.29 491.66

9.00 500.66

13

+22

+70

68.4 69.8 71.5 72.2 73.7 74.2 77.1 78.1 79.2
7.0 5.6 3.9 3.2 1.7 1.2 +1.7 +2.7 +3.8
40 30 23 16 3 14 32 40

73.0 73.4 75.0 76.6 78.5 80.4 81.7 82.6
13.1 12.7 11.1 9.5 7.6 5.7 4.4 3.5
40 31 9 9 23 35 50

77.8 80.4 80.8 74.9 80.7 82.5 83.3
8.3 5.7 5.3 6.2 5.4 3.6 2.8
28 17 13 26 50 60

82.9 83.5 83.1 83.8 83.8 84.7
3.3 2.6 3.0 2.3 2.3 1.4
40 24 24 43 50

On Rock 2' Lt. 13+20

88.9 88.4 88.4 88.7 84.9 86.1 86.1
11.7 12.2 12.2 11.9 10.7 12.5 12.5
40 20 5 21 34 40

90.7 91.0 91.1 90.3 91.1
9.9 9.6 9.5 10.3 9.5
40 20 20 40

94.8 93.7 93.6 94.2 94.1
5.8 6.9 7.0 6.4 6.1
40 20 20 40

500.66

14

1.20 499.46

5.87 505.33

1 +24

+ +54

+ 15

+51.10= Equation
18+88.60

Bkw#3 7.23 498.10 498.01 On 2x2 Hub 1' Rt. Sta 15+00

Contd in Bk 7, Pg. 17

95.7 96.3 96.8 97.0 99.2 97.6
4.9 4.3 3.8 3.6 2.4 2.7
/40 /20 /10 /25 /40

97.7 98.3 99.5 99.7 00.2 1.1 0.8
7.6 7.0 5.8 5.6 5.1 4.2 4.5
/40 /19 /10 /17 /28 /40

99.0 99.6 0.6 2.1 1.5 0.7 1.2 0.8
6.3 5.7 4.5 3.2 3.8 1.6 4.1 4.5
/40 /31 /18 /7 /22 /35 /40

99.1 98.2 98.0 97.9 97.2
6.2 7.1 7.3 7.4 8.1
/40 /20 /20 /40

96.4 97.0 95.2 94.2 93.0
6.9 8.3 10.1 10.8 12.3
/40 /20 /20 /40

	+	H.I	—		
B.M.	2.82	417.29		414.47	R.R. Spk in Tel. Pole -
T.P.	11.67	427.91	1.05	416.24	
T.P	11.59	439.11	0.39	427.52	
T.P	11.86	450.62	0.35	438.76	
T.P	9.84	460.29	0.17	450.45	
			5.88	454.41	Sta 8+00 P.I
			5.40	454.89	
#1 B.M.	7.95	463.62		455.67	Ref to Book #68. P. 12.
T.P	1.41	456.88	8.15	455.47	
T.P	3.70	448.94	11.64	445.24	
T.P	10.22	455.99	3.17	445.77	
B.M.			6.14	449.85	Sta 8+00 P.I.
			5.65	450.34	B.M. on R.P. Hub. 100 ft Rt Sta 8+00 P.I.

	+	H.I	−	
B.M	5.74	456.08		450.34
T.P.	12.00	467.89	0.19	455.89
T.P	11.52	479.22	0.19	467.70
T.P.	11.56	489.77	1.01	478.21
T.P	10.05	498.22	1.60	488.17
B.M	2.16	491.48	8.90	489.32
T.P	0.77	480.52	11.73	479.75
T.P	0.47	469.28	11.71	468.81
T.P	1.24	459.98	10.54	458.74
B.M.			9.64	450.34
				450.34

See. Page 15

B.M. 100 ft R. Sta 12+00

B.M. on R.R. Hub. 100' Rt. Sta 8+00

Check Levels - on Grade Stakes -

MASSACHUSETTS AVE.

	+	HI	Lt. on 5' Offset Hubs	Rt.
B.Mk.	2.78	453.12		
				450.34 On R.P. Hub 100' Rt. P.I. Sta 8+00
				See Pg. 15
7+50			10.6	7.3
8			5.40	
			0.41	45r.71
	10.63	463.34		
+50			12.1	8.8
9			8.1	4.2
+50			5.2	
			0.63	46r.71
	10.76	473.47		

Lt. Rt.

(4½) = on D Hub

D = C 3.1 / 21.6 Out F = C 2.5 D = C 4 / Out 22 F = C 4.5

D = C 3.4 / 21.7 F. C 3.4 D = C 5.0 / 22.5 F. C 5.0

D = C 3.0 / 21.5 F = C 2.7 D = C 5.0 / 22.5 F = C 5.0

D = C 2.8 / 21.2 F = C 2.4 D = C 5.0 (4½) F = C 5.1

D = C 0.3 / 20.2 ✓ F = Grade

C 3.7 / 21.8 C 3.9 / 22.2

Set 10/23/26

On 5' Offset Hubs

+	H.I.	Lt	Rt
	473.47		
10		11.8	9.8
+50		10.9	6.1
11		7.5	
		0.6r	47r.55
	9.45	48r.30	
11			8.9
+50		10.0	4.r
12		6.4	0.7
		0.69	481.61
	11.43	493.04	
Bchr		3.73	489.31 489.32
+50		9.3	

Lt. Rt 19

D = C 1° / 20.5 F = C 0 3

D = C 2° / 21° F = C 2 1

D = F 3 3 / 25 F = F 3 7

D = C 1° / 20.5 F = C 1 5

D = F 3 8 / 25.7 F = F 4 4

D = C 4° / 22.0 F C 4 5

D = F 2 5 / 23.7 (9.6) F = F 2 8

D = C 3 6 / 21.7 F = C 4 1

D = F 3 7 / 24.8 (5.9) F = F 3 7

D = C 3 3 / 21.7 F = C 3 3

D = C 0 3 / 20 1 F = C 0 1

C 1.6 / 20.8 C 1.6 / 21.8

Set 10/23/86 Eve.

		493.04		
13			2.8	
	10.81	503.11	0.74	499.30
+34.1			10.3	10.8
14			7.3	
+50			1.27	501.84
	0.29	501.13		
15			4.1	4.5
19			4.7	
			7.93	494.90
	1.46	495.66		
			10.15	485.51
	1.34	486.85		
			11.31	475.54

Lt. Rt. 20

D = C 25 / 21.3 F = ? 23

C 26 / 21.3 C 24 / 26.3 Set 10/23/26

D = C 20 / 21.0 F = C 3 D = C 20 F = C 20

C 3.5 / 9.0

D = C 24 / 21 F = C 21

C 38 / 21.9 C 38 / 26.9 Set 10/23/26

C 44 / 22.2 C 44 / 27.7 Set 10/23/26

D = C 24 / 21.3 (4.2) F = C 23 D = C 20 / 21 (4.3) F = C 18

D = C 33 / 21.6 (5.1) F = C 36

			475.54	
	1.00	476.54		
			7.57	468.97
	1.37	470.34		
Bkw#4			6.31	464.03	464.09

Outfub 65' Rt. Sta. 26+50

10/22/26
Coote Notes
Clifton ⊼
Draner ϕ

D= Dauchys Marking on Stake -
F= Foremans " "
A number in a circle (44) indicates a reading on Dauchys original hub, most of which have been destroyed.

Mass. Ave. X-Sections

March-8-27
O.S. Thompson

Note We 11

0+00 = Intersection ℄ Univ. Ave & ℄ Mass.
Stationing = ℄ Chaining from Univ. Southerly
and is continuous to 3+33.75 Bk = 4+37.35 Fwd = Equation
From Station 4+37.35 to 5+ 21+50 = Continuous without
any other Station Equations — March. 8-27 — O.S. Thompson
The Plane of the Finished Pav. = Datum for each Station = 0.0±

Station	Left			℄	Right			Areas Cut	Areas Fill
1+94		0.0/25	-.01/15	.00	-.01/15	-1.0/22	-5.8/31		
2+50	+1.09/32	.00/20	.00/15	.00	.00/15	0.0/30	-1.0/36		
2+60	+.10/31	.00/18	.00/15	.00	.00/25				
3+00	+11.6/26	.00/20	.00/15	.00	.00/15	+.02/24	+4.9/27		
3+33.75 ↑	+13.5/30	.09/21.	.00/15	0.0	.00/15	.00/22	+5.3/28		
4+37.35 ↓									
4+50	+13.5/31	.00/20	.00/15	.00	.00/15	.00/27	+5.8/28		
5+00	+8.6/29	.00/20	.00/15	.00	.00/15	.00/23			
5+40		.00/25	.00/15	.00	.00/15	.00/20	-12.0/39		

From - 5+40 to 6+85 = Fill
Sections not taken

Mass. Ave. X-sections

Sta.	Left	℄	Right	Areas Cut	Areas Fill
6+85	-5.0/30 00/20	0.0	00/15 00/21		
7+25	00/20 00/15	00	00/15 00/20	+2.5/27	
7+50	+0.6/23 00/20 00/15	00	00/15 00/20	+4.1/27	
8+00	+2.1/23 00/20 00/15	00	00/15 00/20	+4.7/27	
8+50	+2.5/22 00/20 00/15	00	00/15 00/20	+4.5/26	
9+00	+1.4/23 0/20 0/15	00	0/15 0/22	+4.3/27	
9+50	+0.6/21 0/19 0/15	00	0/15 0/22	+2.9/25	
10+00	0/20 0/15	00	0/15 0/20	+0.7/22	
10+50	-3.8/29 0/20	00	0/15 0/21	+1.1/24	
11+00	-3.8/29 0/21	0/15 00	0/15 0/20	+3.1/22	
11+50	+2.1/24 0/20	0/15 00	0/15 0/20	+2.8/23	
12+00	-3.9/27 0/20	0/15 00	0/15 0/19	+2.3/23	

Mass. X-sections

Sta.	Left	℄	Right
12+50	+1.0/20 0/17	0/15 00 0/15	0/20 +2.4/24
13+00	+2.2/24 0/20	0/15 00 0/15	0/20 +2.6/23
13+50	+1.1/23 0/20	0/15 00 0/15	0/21 +1.7/23
14+00	+2.0/27 0/23	0/15 00 0/15	0/23 +5.0/30
14+50	+2.3/25 0/20	0/15 00 0/15	00/21 +2.5/24
15+00	+1.7/22 00/19	01/15 00	0/30
15+50	+3.4/24 0/19	0/15 00	00/20 Fill = Waste 40' out
16+00	+4.6/24 0/19	0/15 00	0/20 Fill = " 20' out
16+50	+5.3/23 0/19	0/15 00	0/20 Fill = Waste for 20' out
17+00	+5.3/25 0/19	0/15 00	0/15 0/20 -3.1/25
17+50	+3.8/24 0/19	0/15 00	0/15 0/19 -3.5/25
18+00	+1.1/21 0/19	0/15 00	0/15 0/19 -5.1/26

Areas

Cut	Fill

Mass. X-sections

Sta	Left	℄	Right	Cut	Fill
18+50	0/20	0/15 00	0/20	4.8/28	
19+00	+0.8/22 0/19	0/15 00	0/15 0/19	2.3/25	
19+50	+2.5/21 0/19	0/15 00	0/20	1.2/22	
20+00	+3.0/22 0/19	0/15 00	0/15 0/18	1.5/26	
20+50	+2.0/21 0/19	0/15 00	0/15 0/20	1.3/26	
21+00	00/21	0/15 00	0/15 0/18	1.7/24	
21+50	-1.0/21 0/19	0/15 00	0/15 0/19	1.5/23	

	Hl.	Grd Rod		
			4.11.0	4.11.6
C 1.6 / 409.7 / 410.3				
			Gutter fr. 409.7	Prof.
1+50	407.8 +	1.3	409.1	409.7
1+00		0.0	408.0	408.6
4.5				
B Lw.				450.1
	8.6	458.7		
8+00		13.4	445.30	446.30
+50		8.7	450.0	451.00
9		4.0	454.7	455.7

Lt. Rt. 34

2+00 Lt. twkd C 1.6 / 20.8 Set C 2.9 / 25.8

Set Rt. F 7.2 / 30.8 F 8.5 / 35.8

F 5.7 / 28.5 F 6.0 / 33.5 Rt. F 6.2 / 29.3 F 6.6 / 34.3

F 4.8 / 27.2 F 4.7 / 32.2

* Sta. 8+00 (P.1.)

10.7 / C 4.7 twk C 3.4

8.1 / C 5.3 twk C 5.2

7.2 / C 1.5 twk C 2.7

3.8 / C 4.9 twk C 5.0

3.2 / C 0.8 twk C 2.4

+0.4 / C 4.6 twk C 5.1

5' off Lt = ℄ 9.0
Lt Stk tuked ℄ 8.6
5+00 Rod + 1.6
10.2
— 7.7
tuked ℄ 2.5 ℄ 1.5 Stk on Rt.
5' off = ℄ 1.9

3+33.75= Lt tuked ℄ 14.0 — 5' off = ℄ 14.3
4+37.15 HI = ℄ 14.0
Rt. ℄ 7.7
23½
7.7
5.5
℄ 5' off

3+00 Lt tuked ℄ 13.4 — 5' off ℄ 14.2
Rt ℄ 6.0 5' " ℄ 5.2
12.3

2+50 Rt tuked Syr. 5' off F 1.4
HI = +12.0
Lt = ℄ 9.0 5' " ℄ 10.4
21.4½ 22.9½

Blk #3

498.01
416.00

409.7
4.8
404.9

76+74.6
167.3
75+07.3
123

3+33.75
3+53.52
19.77
4+37.35
4+57.12

333.75
362.65
696.40

8+00.00
1+37.35
6+62.65

18+88.60
18+07.98
80.62

96.5
94.8
Grd = 1.7 higher

0.2
1.7
0.7

WATSON, VALLE & GOUGH