

San Miguel

NAME Valencia St & Troy Ave

Job # 175

Class _____ Course _____ Party Book # 2

Alignment 0100 to 43+68.15

X- Sections, Pages - 12-21

Check Levels - 25-27

120

Alignment

1979

FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

VALENCIA ST. &

TROY AVE.

East from Golden Ave.

Alignment Book #2

This book contains
Cross Sections of
Line East from
Golden Ave.

MICROFILMED

DEC 30 1964

INDEX:

	Page
Alignment: 0+00 to 43+68.15 (East from Golden Ave.)	1 - 11
Cross Sections	17 - 24
Check Levels	25 - 27
Central Troy to LaMar	28 - 31
Bancroft Troy to Rosedale	32 - 34

Sta	Dist.	Angle Az.	Def.	Ties
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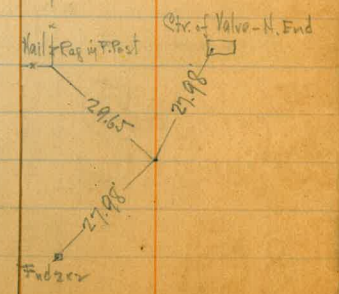
559.80

X- Sec Notes
on Pg. 12 this Book

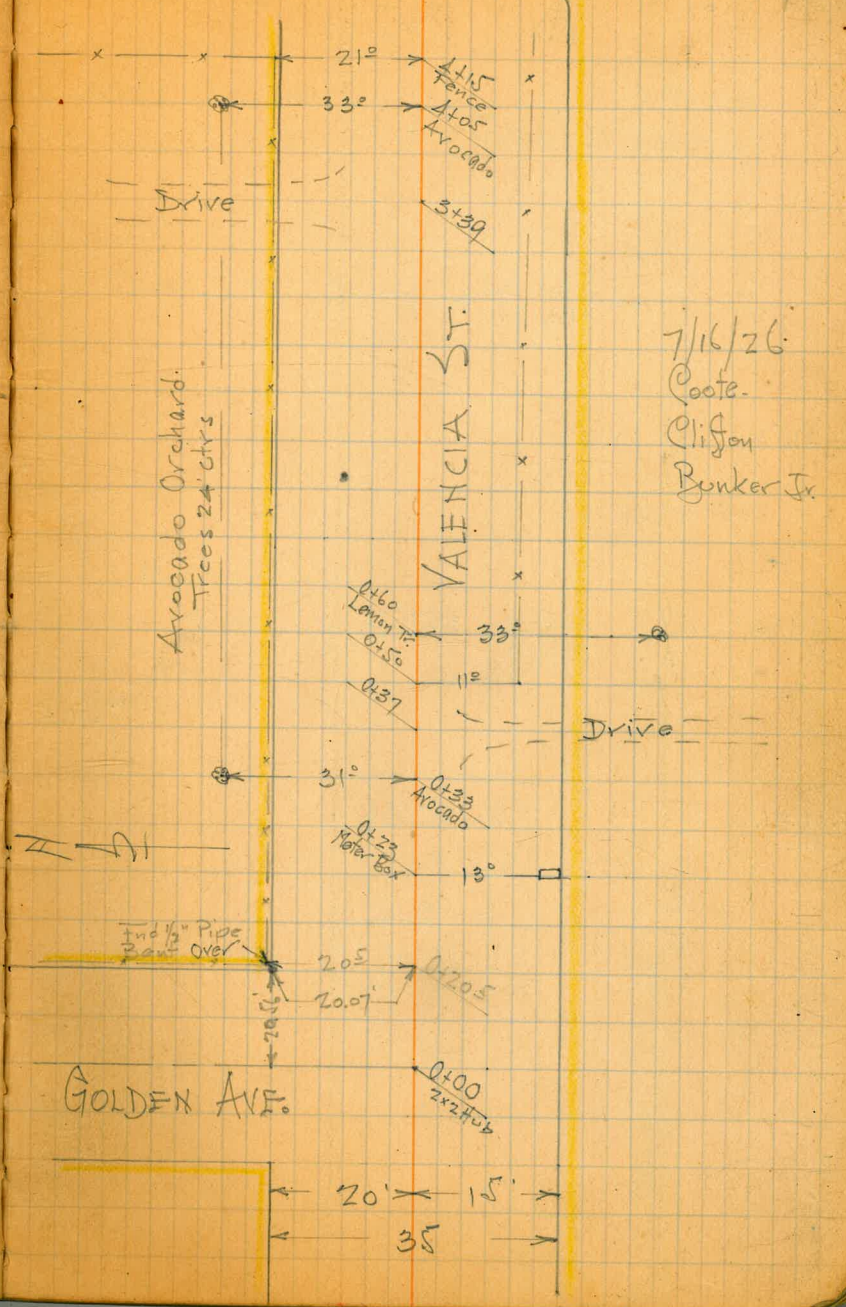
0+00 179°46' 0°14' Lt.
359°32'

4+53.09
BK#1, Pg 2

See Also Book # X Pg 1
#119



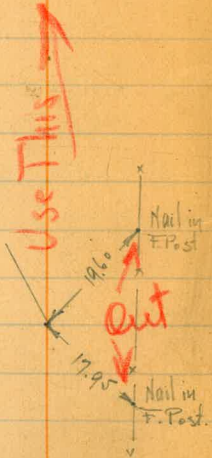
Topog



7/16/26
Coote.
Cliffon
Bunker Jr

Sta	Dist	Angle		Ties
		Az.	Def.	
				52.17
				50°
				50°
6447.52	722.89			Nail & Tin
				To Vent Pipe in Greenhouse
5459.80 PI		145°24'	34°36' L.	
		290°48'		
4166.36 PC	559.80			

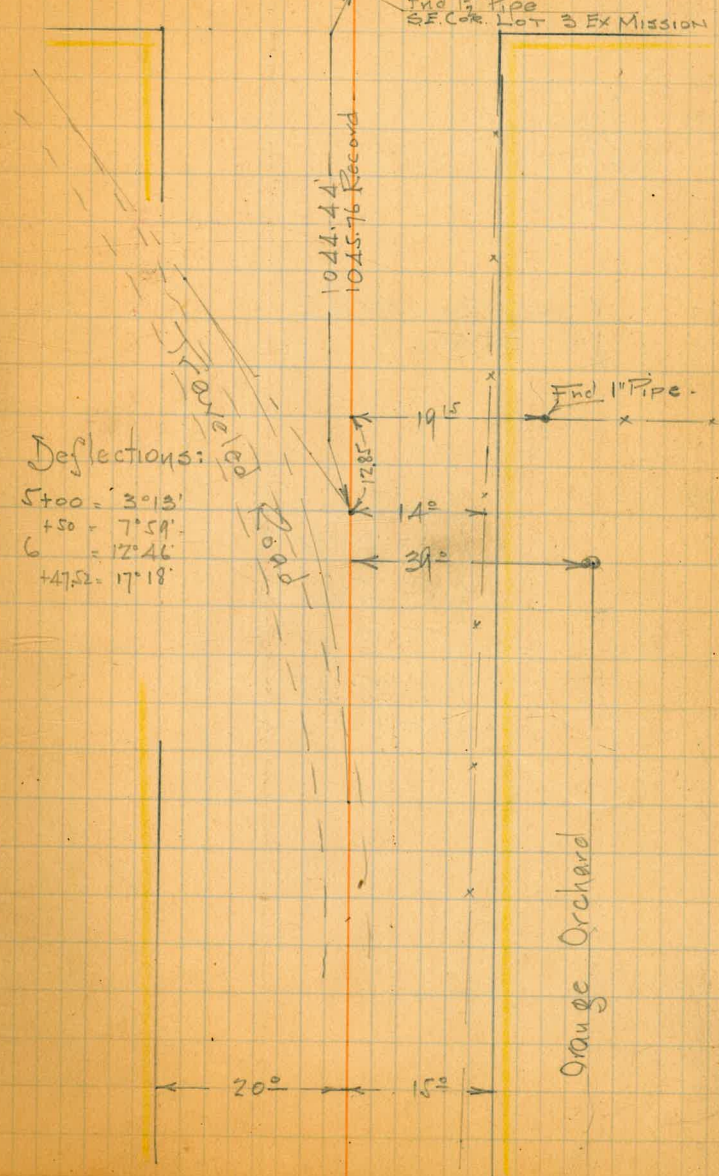
$\Delta = 34^{\circ}36'$
 $R = 300'$
 $T = 93.44'$
 $L = 181.16'$



SWEETWATER

ROAD

End 1 1/2" Pipe S.F. Co. Lot 3 Ex Mission



Deflections:

- 5+00 = 3°13'
- +50 = 7°59'
- 6 = 12°46'
- +47.52 = 17°18'

Orange Orchard

20° 15°

Sta. Dist. Angle Az. Def. Ties -

14+02.77
P.T.

365.35

12+76.97
P.I.

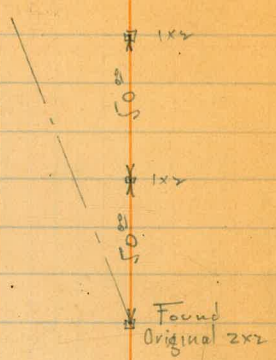


150° 30' 29' 30" Lt.
301° 00'

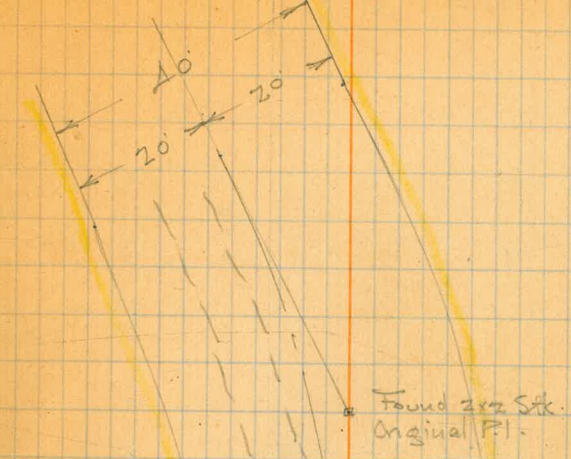
11+45.33
P.C.

722.89

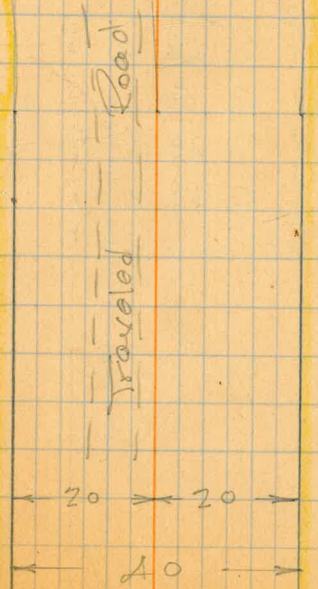
$\Delta = 29^{\circ} 30'$
 $R = 500'$
 $T = 131.64'$
 $L = 257.44'$



Topog - 3



Deflections -
11+50 = 0° 16'
12 = 3° 04'
15 = 6° 00'
13 = 8° 52'
15 = 11° 43'
14 = 14° 35'
102.77 = 14° 45'



Sta.	Dist.	Angle		Ties
		Az.	Def.	

17+10.36
P.T.

1598.21

16+36.48
P.I.

214°04' 64°04' Rt
+128°09'

15+42.63
P.C.

$A = 64^{\circ}04'$
 $R = 150'$
 $T = 93.85$
 $L = 167.73$

365.35

100
50
100
50

Orig. 200

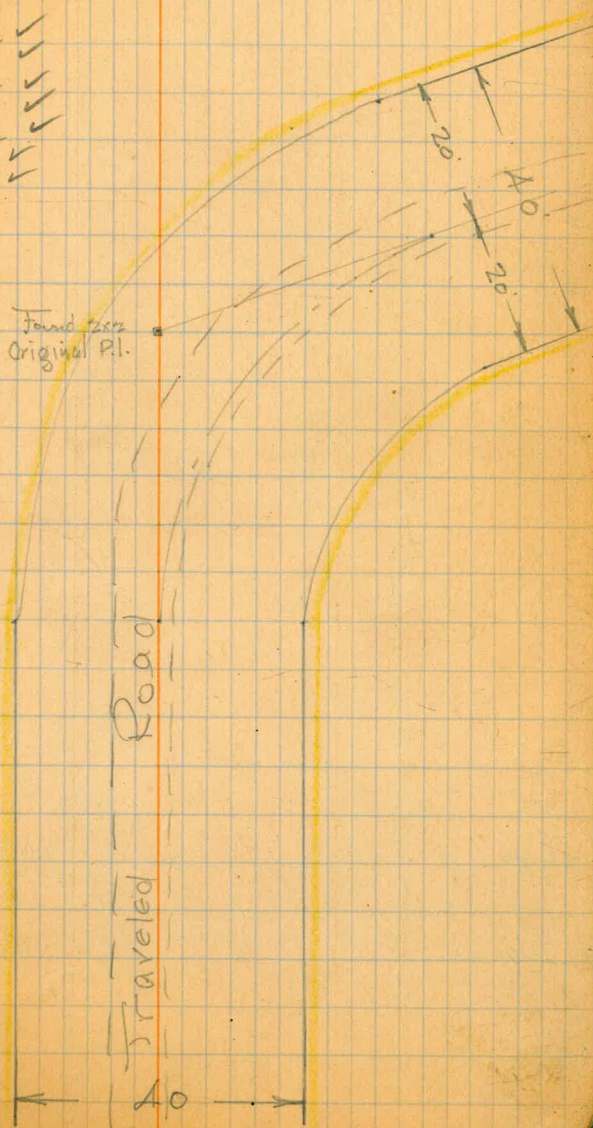
Topog-

4

Deflections-

15+50 = 1°24' ✓
16+75 = 6°11' ✓
16+50 = 10°57' ✓
17+25 = 15°44' ✓
17+50 = 20°30' ✓
17+75 = 25°17' ✓
17 = 30°03' ✓
10+36 = 32°02'

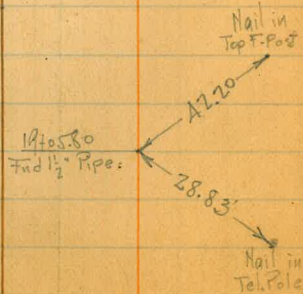
Found 200
Original P.I.



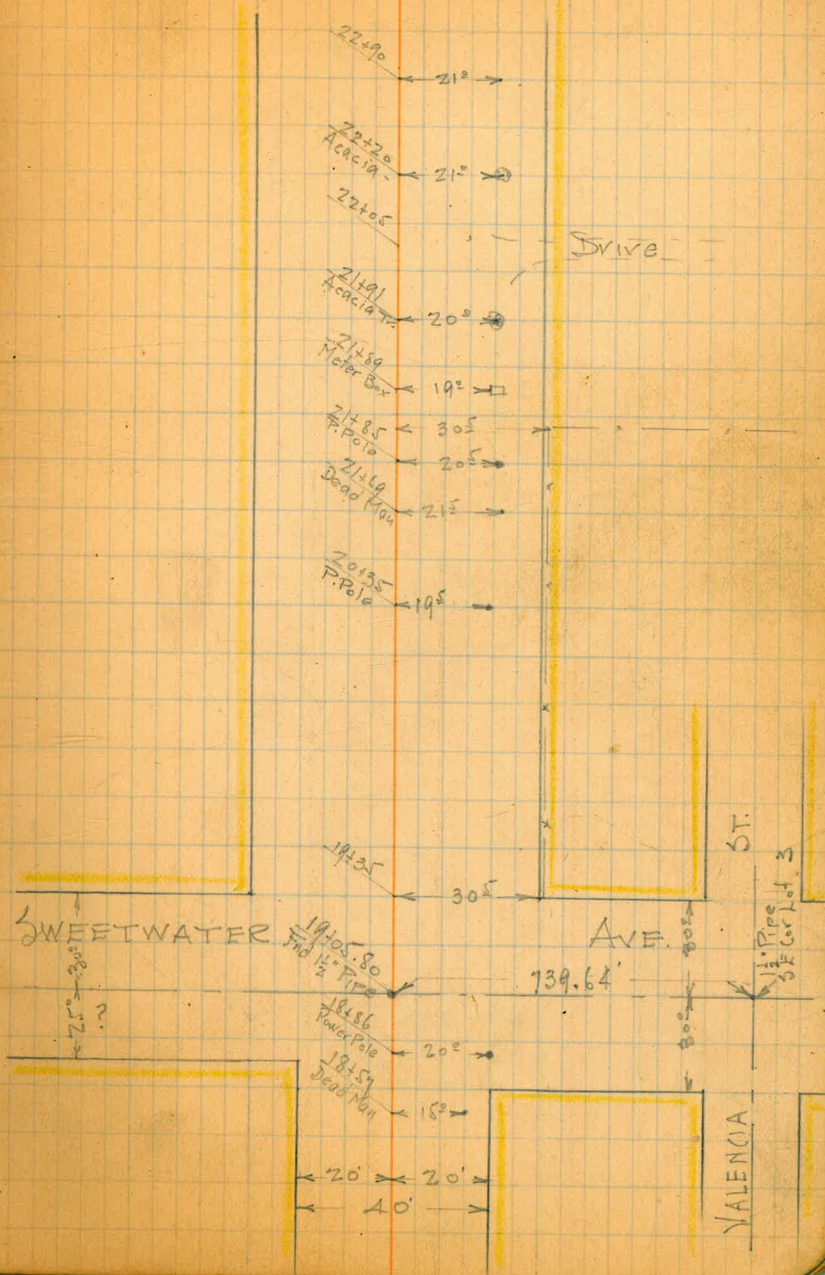
Sta.	Dist.	Angle Az. Def.	Ties
------	-------	-------------------	------

1598.21

1910.50
P.O.T.



Topog.



1598.21

6

25:40
Acacia 19°

70° $24:85$
Meter Box

24:56
Acacia 21°

72° $24:35$
Meter Box 19°

70° $24:36$ P Pole 70°

70° $24:15$
Acacia Trees 71°

$23:12$ 70°

$23:10$ P pole 30°

1598.21

7

29+14
Acacia → 21°

28+19
Grapes → 29°

ST

27+19
Grapes → 30°

TROY

26+19
F. Pine → 20°

24+20
Water Meter → 18°

26+21
Acacia → 21°

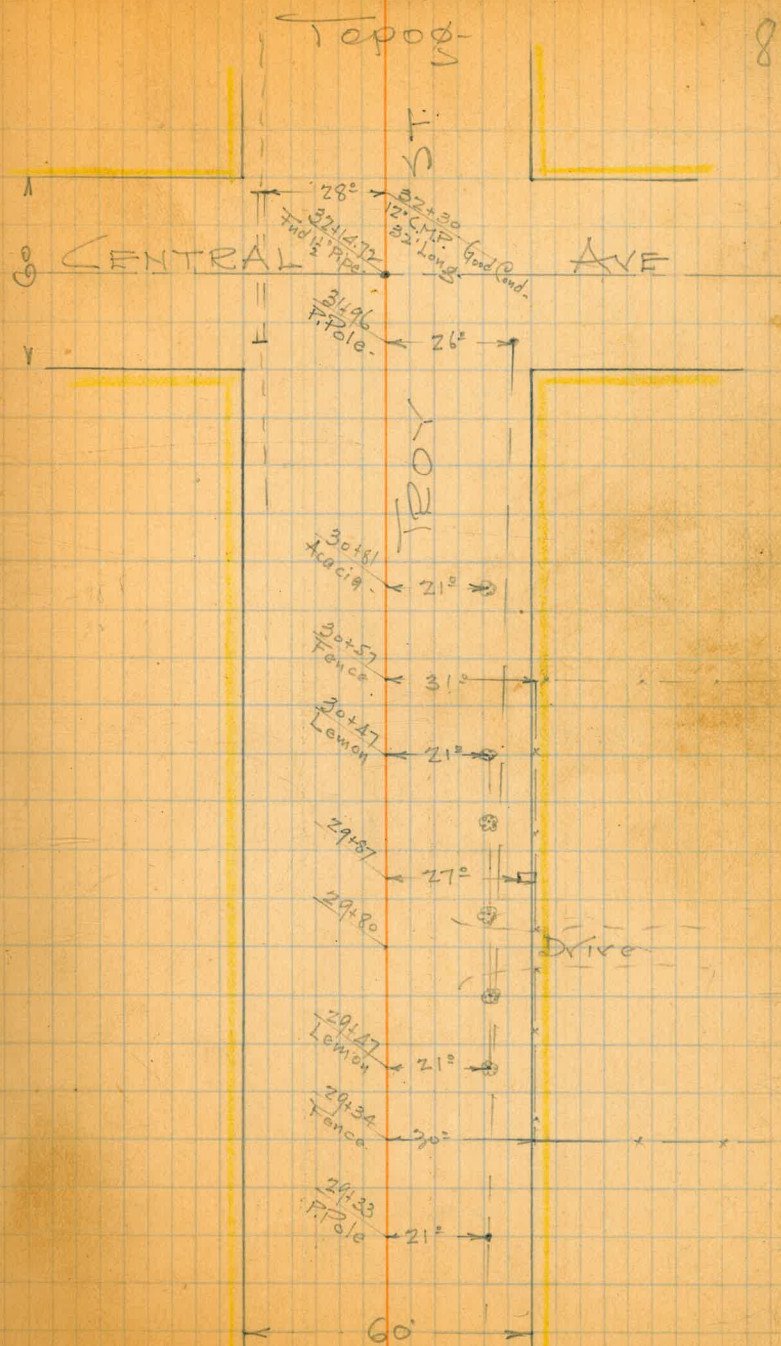
25+21
Acacia → 21°

25+16
Water Meter → 19°

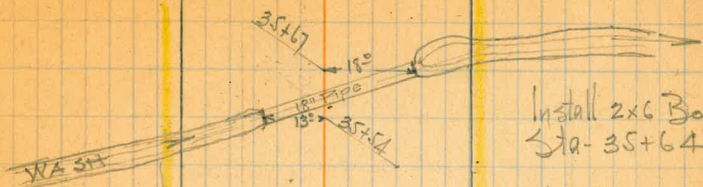
25+16
Fence → 20°

Sta	Dist.	Angle Az. Def.	Ties
32+14.7 P.I.		180°02' 360°03'	0°02' R.
	32+14.7		Found 1 1/2" Pipe
	36.23		Nail in Mail Box Post
	32.76		Nail in P. Pole

1598.21



1153.43



Install 2x6 Box
Sta-35+64

The pipe in place
is much too small -
In good condition.

35+19
Acacia → 21° →

35+41
Meter Box → 19° →

35+41
Acacia → 21° →

32+92
→ 30° →

DRIVE

34+64
→ 30° →

Garage
16

31+11
F.P.O. → 20° →

Ditch

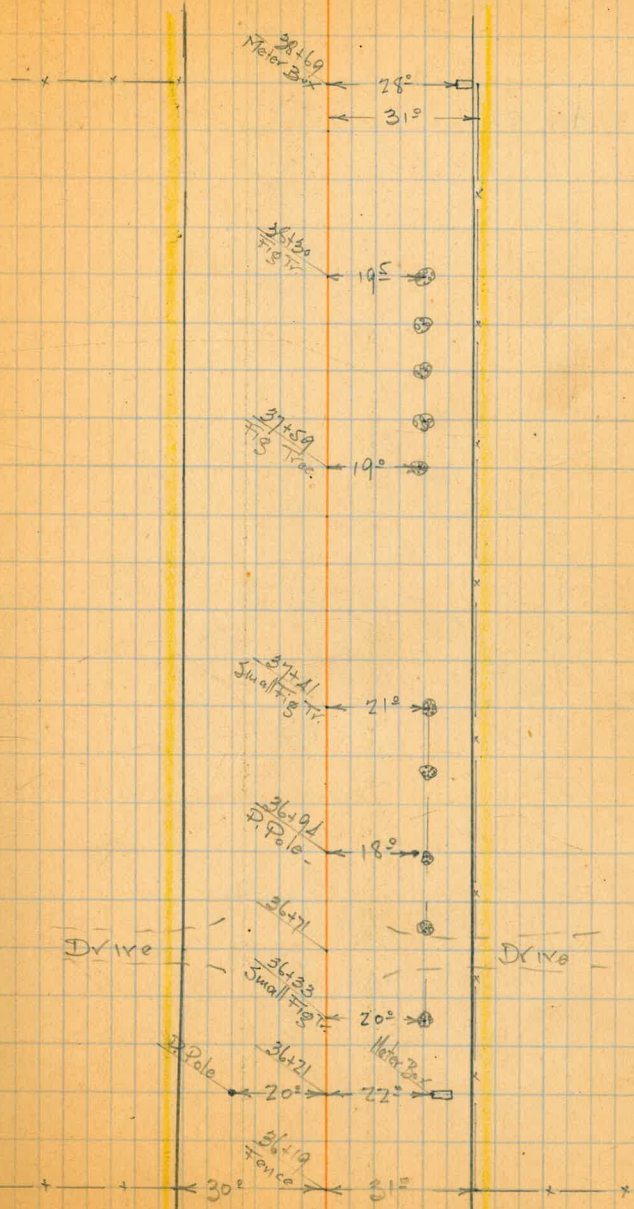
34+05
→

DRIVE

33+17
Meter Box → 19° →

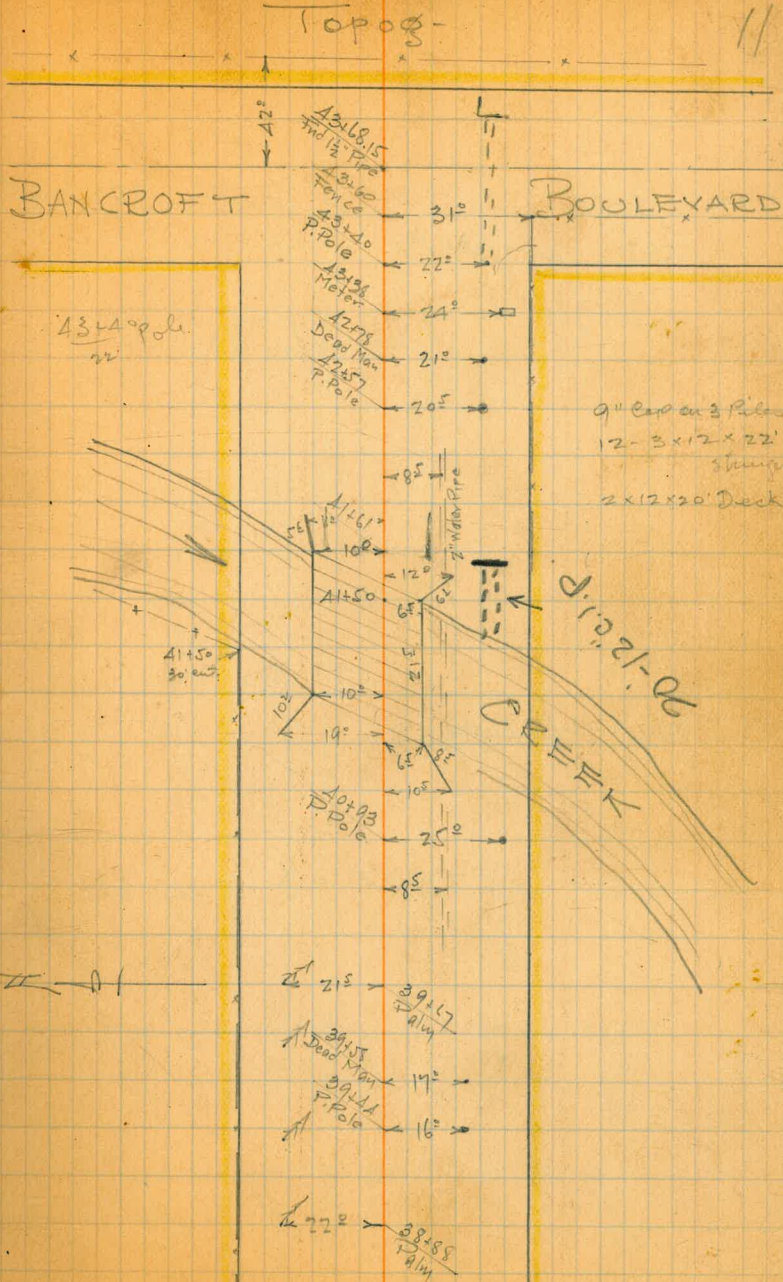
33+69
Fence → 30° →

1153.43



Sta	Dist.	Angle Az. Def.	Ties
43468.15			Found 1 1/2" Pipe
	45.40'		Mail m Pole

1153.43



3lu=1A

488 487.57

482.69

BK-121-P.3
Nail in Cor Fence Post 20' Lt 0+20
H-1 487.57

0+00

* Golden Ave.

80.0	79.8	80.1	80.9	81.4	81.9	81.9	83.2	83.5
$\frac{7.6}{200}$	$\frac{7.8}{100}$	$\frac{7.5}{50}$	$\frac{6.7}{30}$	$\frac{6.2}{19}$	$\frac{5.7}{-}$	$\frac{5.8}{5}$	$\frac{4.4}{15}$	$\frac{4.1}{30}$

+50

82.0	82.0	82.1	82.4	82.2	83.4	83.7
$\frac{5.6}{30}$	$\frac{5.6}{20}$	$\frac{5.5}{13}$	$\frac{5.2}{-}$	$\frac{5.4}{4}$	$\frac{4.2}{14}$	$\frac{3.9}{30}$

1

2.67 484 90

83.6	83.7	83.4	83.7	83.4	83.7	83.9
$\frac{3.5}{30}$	$\frac{3.9}{20}$	$\frac{4.2}{10}$	$\frac{3.9}{-}$	$\frac{4.2}{3}$	$\frac{3.9}{10}$	$\frac{3.7}{30}$

+50

10.69 494.99

85.1	84.9	84.7	84.9	84.5	85.1	84.7
$\frac{9.9}{30}$	$\frac{10.1}{19}$	$\frac{10.3}{12}$	$\frac{10.1}{-}$	$\frac{10.5}{4}$	$\frac{9.9}{12}$	$\frac{10.3}{30}$

2

86.5	86.5	86.3	86.0	86.0	85.7	85.5
$\frac{8.5}{30}$	$\frac{8.5}{22}$	$\frac{8.7}{20}$	$\frac{9.0}{12}$	$\frac{9.0}{-}$	$\frac{9.3}{5}$	$\frac{9.5}{30}$

+50

87.9	87.9	87.6	87.4	87.8	87.4	87.7	86.1	87.1
$\frac{7.1}{30}$	$\frac{7.1}{20}$	$\frac{7.4}{15}$	$\frac{7.6}{10}$	$\frac{7.2}{-}$	$\frac{7.6}{5}$	$\frac{7.3}{7}$	$\frac{6.9}{15}$	$\frac{7.9}{30}$

3

89.4	90.4	90.1	89.5	90.0	89.4	89.7	89.4	89.3
$\frac{4.6}{30}$	$\frac{4.6}{21}$	$\frac{4.9}{13}$	$\frac{5.5}{11}$	$\frac{5.0}{-}$	$\frac{5.6}{7}$	$\frac{5.5}{8}$	$\frac{5.1}{16}$	$\frac{5.7}{30}$

X

494.99

3.50

4

0.07 494.92

4.91 499.83

±5.0

5

±5.0

6

±5.0

10.64 489.19

0.06 489.25

7

13

H.I - 494.99

93.0	92.3	91.6	92.0	91.3	91.6	91.3
2.0	2.7	3.4	3.0	3.7	3.5	3.7
30	20	9		6	12	30

95.0	94.5	94.0	93.3	94.6	94.1	93.5	94.9	94.0
0.0	0.5	1.0	1.7	1.0	0.9	1.5	0.1	1.0
30	18	13	11	7	7	7	9	30

H.I - 499.83

96.5	95.9	96.3	95.9	96.2	95.5
3.4	4.0	3.6	4.0	3.6	4.4
30	11	7	15	30	

96.1	97.8	97.1	97.7	97.3	97.7	96.9
1.8	2.1	2.8	2.2	2.6	2.2	3.0
30	16	14		8	15	30

97.8	96.9	95.3	95.9	95.8	95.2	94.4	93.9
2.1	3.0	4.5	4.0	4.1	4.7	5.5	6.0
30	18	14	4	5	19	30	

96.9	95.1	93.1	93.9	93.7	93.2	91.0	89.5	87.9	87.3
3.0	4.8	6.8	6.0	6.2	6.7	8.9	10.4	12.0	12.6
30	17	14	7		5	9	19	22	30

95.6	93.4	90.8	91.6	91.4	90.7	88.2	86.2	84.7
4.3	6.5	9.1	8.3	8.5	9.2	11.7	13.7	15.2
30	17	15	6	4	9	21	30	

H.I - 489.25

94.5	93.1	88.9	89.2	89.2	88.8	86.1	84.5
1.2	1.8	0.4	0.1	0.1	0.5	3.2	1.8
30	18	14	5		5	11	30

+

189.25

7+50

8

+50

9

0.25 477.85

11.65 477.60

+50

10

+50

0.39 466.54

11.70 466.15

11

Lt.

Rt.

14

92.5	94.8	95.9	86.9	86.7	86.3	83.4	78.0
+3.7	+0.5	3.4	2.4	2.6	3.0	5.9	11.3
<u>30</u>	<u>17</u>	<u>15</u>	<u>7</u>		<u>4</u>	<u>10</u>	<u>30</u>

89.1	86.7	83.7	84.1	83.9	83.3	80.6	78.0
0.2	2.6	5.2	5.2	5.4	6.0	8.8	14.3
<u>30</u>	<u>17</u>	<u>16</u>	<u>6</u>		<u>5</u>	<u>9</u>	<u>30</u>

86.7	83.6	80.6	86.0	80.8	80.3	76.6	71.6
2.6	5.7	8.7	8.3	8.5	9.0	12.7	17.7
<u>30</u>	<u>17</u>	<u>15</u>	<u>5</u>		<u>4</u>	<u>9</u>	<u>30</u>

84.1	80.6	77.5	78.0	77.7	77.1	73.2	68.2
5.2	8.1	11.8	11.3	11.6	12.2	16.1	21.1
<u>30</u>	<u>19</u>	<u>15</u>	<u>7</u>		<u>4</u>	<u>10</u>	<u>30</u>

H.I. 477.85

80.6	78.1	77.2	74.4	78.0	74.9	74.4	70.5	66.4
+2.8	+0.3	0.6	3.2	2.8	2.9	3.4	7.3	11.4
<u>30</u>	<u>20</u>	<u>18</u>	<u>15</u>	<u>9</u>		<u>4</u>	<u>11</u>	<u>30</u>

78.9	77.1	71.5	72.2	72.1	71.2	69.1	63.7
+1.1	0.7	6.3	5.6	5.7	6.0	8.7	14.1
<u>30</u>	<u>19</u>	<u>15</u>	<u>6</u>		<u>5</u>	<u>10</u>	<u>30</u>

69.9	71.7	68.1	68.8	69.3	68.9	68.4	65.3	61.0
2.9	6.1	9.7	9.0	8.5	8.9	9.4	12.5	16.8
<u>30</u>	<u>17</u>	<u>15</u>	<u>11</u>	<u>8</u>		<u>5</u>	<u>9</u>	<u>30</u>

H.I. 466.54

71.0	67.7	65.2	65.9	65.7	65.5	62.5	58.5
+4.5	+1.2	1.3	0.6	0.8	1.0	4.0	8.0
<u>30</u>	<u>16</u>	<u>15</u>	<u>5</u>		<u>4</u>	<u>10</u>	<u>30</u>

✓
X

1150

466.54

12

+50

11.60 454.94

Blu

0.23 455.17

4.50 450.67

4.50 455.17

+3

+50

14

+50

12.05 443.12

0.83 443.95

Lt.

H1- 466.54

Rt.

15

67.0	64.3	61.9	62.5	62.3	62.0	59.6	56.0
+0.5	2.2	4.6	4.0	4.2	4.5	6.9	10.5
<u>30</u>	<u>18</u>	<u>15</u>	<u>7</u>	<u>7</u>	<u>3</u>	<u>8</u>	<u>30</u>

62.9	60.9	58.7	59.4	59.2	59.0	56.7	52.3
3.8	5.6	7.8	7.1	7.3	7.5	9.8	14.2
<u>30</u>	<u>18</u>	<u>16</u>	<u>7</u>	<u>7</u>	<u>3</u>	<u>7</u>	<u>30</u>

60.5	58.5	55.7	56.6	56.3	55.9	48.7
6.3	8.0	10.8	9.9	10.2	10.6	17.8
<u>30</u>	<u>19</u>	<u>16</u>	<u>7</u>	<u>4</u>	<u>30</u>	

H1. 455.17

On Pl. Hub Sta 12+76.97

58.3	56.4	53.0	54.1	53.8	53.6	51.1	46.2
+3.1	+1.7	2.2	1.1	1.4	1.6	4.1	9.0
<u>30</u>	<u>19</u>	<u>15</u>	<u>7</u>	<u>4</u>	<u>8</u>	<u>30</u>	

56.0	53.0	50.2	51.1	50.7	50.5	47.6	43.4
+0.8	2.2	5.0	4.1	4.5	4.7	7.6	11.8
<u>30</u>	<u>18</u>	<u>15</u>	<u>7</u>	<u>4</u>	<u>8</u>	<u>30</u>	

52.5	50.4	47.2	46.2	48.1	47.7	45.4	42.2
2.7	4.8	8.0	7.0	7.1	7.5	9.8	13.0
<u>30</u>	<u>17</u>	<u>15</u>	<u>7</u>	<u>3</u>	<u>5</u>	<u>9</u>	<u>30</u>

48.9	47.4	44.7	45.5	45.4	44.8	43.5	40.7
6.3	7.8	10.5	9.7	9.8	10.4	11.7	14.5
<u>30</u>	<u>18</u>	<u>16</u>	<u>6</u>	<u>7</u>	<u>7</u>	<u>9</u>	<u>30</u>

443.95

15

+50

16

+50

17

+50

18

+50

Btu

0.39 432.34

12.00 431.95

0.99 423.90

9.13 422.71

H.1 443.95

16

44.9	43.5	41.5	42.3	41.9	41.7	40.7	38.9
<u>10.9</u>	<u>0.5</u>	<u>2.5</u>	<u>1.7</u>	<u>2.1</u>	<u>2.3</u>	<u>3.3</u>	<u>5.1</u>
30	19	15	5		6	9	30

40.3	39.7	38.6	39.1	38.7	36.1
<u>3.7</u>	<u>4.3</u>	<u>5.4</u>	<u>4.9</u>	<u>5.3</u>	<u>7.9</u>
30	18	13	6		30

35.4	36.2	36.3	35.9	34.5	34.8	34.2
<u>8.6</u>	<u>7.8</u>	<u>7.7</u>	<u>8.2</u>	<u>9.5</u>	<u>9.2</u>	<u>9.8</u>
30	10	5		10	15	30

31.7	31.8	32.7	33.2	33.3	32.1	31.4
<u>12.3</u>	<u>12.2</u>	<u>11.3</u>	<u>10.8</u>	<u>10.7</u>	<u>11.9</u>	<u>12.6</u>
30	18	12	7		9	30

H.1 432.34

29.2	30.0	30.1	29.6	29.5
<u>3.1</u>	<u>2.3</u>	<u>2.2</u>	<u>2.5</u>	<u>2.8</u>
30	5		11	30

27.7	27.5	27.4	27.3	27.3	27.6
<u>4.6</u>	<u>4.8</u>	<u>4.5</u>	<u>5.0</u>	<u>4.5</u>	<u>4.5</u>
30	11		11	16	30

26.3	26.4	25.3	25.8	25.3	26.3	26.3
<u>6.0</u>	<u>5.9</u>	<u>7.0</u>	<u>6.5</u>	<u>7.0</u>	<u>6.0</u>	<u>6.0</u>
30	16	9		11	16	30

23.9	24.0	23.0	23.6	22.9	24.4	24.6
<u>8.4</u>	<u>8.3</u>	<u>9.3</u>	<u>8.8</u>	<u>9.4</u>	<u>9.9</u>	<u>7.7</u>
30	15	12		11	16	30

Mail in Pale SW Cor Troy & Sweetwater

423.70

18+83

+88

19+080

± Sweetwater Rd.

+50

11.60 117.10

0.37 117.47

20

+50

21

11.58 400.84

0.63 401.52

+50

L+ H.I. 423.70 R+

17

21.1	21.4	20.2	21.6	20.9	21.0	22.7	22.8
<u>2.6</u>	<u>2.3</u>	<u>3.5</u>	<u>2.1</u>	<u>2.8</u>	<u>2.7</u>	<u>1.8</u>	<u>0.9</u>
30	17	13		9	13	15	30

18.6	19.2	21.2	20.5	20.1
<u>5.1</u>	<u>4.5</u>	<u>2.5</u>	<u>3.2</u>	<u>3.6</u>
30	18		15	30

10.4	17.3	18.9	19.4	19.8	20.3	20.7	20.6	16.7
<u>13.3</u>	<u>6.4</u>	<u>4.8</u>	<u>4.3</u>	<u>3.9</u>	<u>3.4</u>	<u>3.0</u>	<u>3.1</u>	<u>7.0</u>
200	100	50	30		30	50	100	200

15.3	15.5	14.9	16.0	15.6	15.9	16.7
<u>8.4</u>	<u>8.5</u>	<u>8.8</u>	<u>7.7</u>	<u>8.1</u>	<u>7.8</u>	<u>7.0</u>
30	19	14		14	16	30

H.I. 412.47

9.9	10.3	9.9	11.0	10.1	10.6	10.6
<u>2.6</u>	<u>2.2</u>	<u>2.0</u>	<u>1.5</u>	<u>2.4</u>	<u>1.9</u>	<u>1.9</u>
30	19	16		14	19	30

5.4	5.5	5.0	5.9	6.1	5.2	5.5	5.9
<u>7.3</u>	<u>7.0</u>	<u>7.5</u>	<u>6.0</u>	<u>6.4</u>	<u>7.3</u>	<u>7.0</u>	<u>6.6</u>
30	19	15	7		17	19	30

99.9	00.2	99.9	0.7	0.9	0.1	1.5	0.8
<u>2.6</u>	<u>2.3</u>	<u>2.6</u>	<u>1.8</u>	<u>1.6</u>	<u>2.4</u>	<u>1.9</u>	<u>1.7</u>
30	19	16	8		12	13	30

H.I. 401.52

95.4	95.7	95.1	95.8	96.0	95.1	95.3	95.8
<u>6.1</u>	<u>5.8</u>	<u>6.4</u>	<u>5.7</u>	<u>5.5</u>	<u>6.4</u>	<u>6.2</u>	<u>5.7</u>
30	20	15	9		11	18	30

22

401.52

11.97 389.55

+50

0.96 390.51

23

+50

24

11.39 379.12

0:39 379.51

+50

25

+50

12.03 367.18

0.03 367.51

H.1- 401.52

18

91.5	91.7	91.2	91.9	92.0	91.3	91.0
100	9.8	10.3	9.6	9.5	10.2	10.5
30	21	15	9		14	30

H.1. 390.51

88.6	88.3	87.7	88.4	88.6	88.4	87.5	88.0	87.7
19	22	2.8	2.1	19	21	3.0	2.5	2.8
30	19	16	10		7	13	21	30

88.4	88.6	84.8	85.6	88.7	88.3	84.7	84.0	84.6
5.1	4.9	5.7	4.9	4.8	5.2	5.8	6.5	5.9
30	19	16	10	23	7	13	20	30

82.5	82.5	81.8	82.5	82.8	82.2	81.6	81.9
8.0	8.0	8.7	8.0	7.7	8.3	8.9	9.6
30	19	15	10		10	14	30

79.2	78	79.0	78.6	79.3	79.3	79.1	78.5	78.9	78.9
11.3	11.7	11.5	11.9	11.2	11.2	11.4	12.0	11.6	11.6
30	18	21	15	9		8	13	22	30

H.1- 379.51

75.8	75.7	74.9	75.7	75.7	75.1	74.4	75.1	74.5	75.2	75.2	75.9
4.0	3.8	4.5	3.8	3.8	4.4	5.1	4.4	5.0	4.3	4.3	3.6
30	20	15	9		9	12	13	15	20	29	30

71.2	71.4	70.7	71.3	71.8	71.3	70.5	71.5	71.2	71.5
8.3	8.1	8.8	8.2	7.7	8.2	9.0	8.0	8.3	7.0
30	19	16	11		9	13	21	29	31

66.7	67.5	66.6	67.4	67.9	67.5	67.0	67.4	67.8
12.8	12.0	12.9	12.1	11.6	12.0	12.5	12.1	11.7
30	19	16	11		9	18	29	30

✓
+

26

367.51

+50

27

11.76

355.75

+50

1.11

356.86

28

+50

29

+50

Lt.

Rt.

19

63.1	63.3	62.3	62.7	63.6	63.8	63.4	62.9	62.9	63.3	63.3
4.4	4.2	4.2	4.8	3.9	3.7	4.1	4.7	4.5	4.2	4.5
$\frac{30}{30}$	$\frac{27}{27}$	$\frac{18}{18}$	$\frac{17}{17}$	$\frac{9}{9}$		$\frac{9}{9}$	$\frac{14}{14}$	$\frac{16}{16}$	$\frac{22}{22}$	$\frac{30}{30}$

59.5	59.6	59.3	59.8	60.3	59.9	59.3	59.8	59.7
8.0	7.7	8.2	7.7	7.2	7.6	8.2	7.7	7.8
$\frac{30}{30}$	$\frac{19}{19}$	$\frac{16}{16}$	$\frac{10}{10}$		$\frac{9}{9}$	$\frac{13}{13}$	$\frac{21}{21}$	$\frac{30}{30}$

57.4	57.4	56.8	57.3	57.5	57.1	56.3	56.9	56.5
10.1	10.1	10.7	10.2	10.0	10.4	11.2	10.5	11.0
$\frac{30}{30}$	$\frac{20}{20}$	$\frac{16}{16}$	$\frac{9}{9}$		$\frac{9}{9}$	$\frac{14}{14}$	$\frac{16}{16}$	$\frac{30}{30}$

H-1 356.86

55.6	55.0	55.7	55.8	55.6	54.4	54.7
1.3	1.9	1.2	1.1	1.3	2.5	2.2
$\frac{30}{30}$	$\frac{14}{14}$	$\frac{5}{5}$		$\frac{7}{7}$	$\frac{15}{15}$	$\frac{30}{30}$

54.4	53.9	53.3	54.1	54.3	54.1	53.0	53.1
2.5	3.0	3.6	2.8	2.6	2.8	3.9	3.8
$\frac{30}{30}$	$\frac{20}{20}$	$\frac{13}{13}$	$\frac{6}{6}$		$\frac{7}{7}$	$\frac{14}{14}$	$\frac{30}{30}$

52.6	52.0	51.4	52.6	52.6	52.4	51.6	52.4	52.2
4.3	4.9	5.5	4.3	4.3	4.5	5.3	4.5	4.7
$\frac{30}{30}$	$\frac{17}{17}$	$\frac{15}{15}$	$\frac{4}{4}$		$\frac{7}{7}$	$\frac{13}{13}$	$\frac{20}{20}$	$\frac{30}{30}$

51.2	50.5	50.5	49.6	50.7	50.8	50.5	49.7	50.1	50.4
5.7	6.2	6.4	7.3	6.2	6.1	6.4	7.2	6.8	6.5
$\frac{30}{30}$	$\frac{27}{27}$	$\frac{17}{17}$	$\frac{13}{13}$	$\frac{5}{5}$		$\frac{5}{5}$	$\frac{17}{17}$	$\frac{18}{18}$	$\frac{30}{30}$

46.1	46.3	46.8	47.1	46.1	46.6	46.9	46.6	47.9	48.5
8.8	8.6	8.4	9.5	8.8	8.3	8.0	8.3	9.0	8.4
$\frac{30}{30}$	$\frac{23}{23}$	$\frac{17}{17}$	$\frac{10}{10}$	$\frac{8}{8}$		$\frac{8}{8}$	$\frac{6}{6}$	$\frac{12}{12}$	$\frac{30}{30}$

356.86

30

11.13 345.73

1.25 346.98

+50

31

+50

32

+15

± Central Ave.

+30

Btu

0.00 341.33

5.65 341.33

L+

R+

20

44.6	45.7	46.0	45.4	46.5	46.7	46.5	45.6	46.0	46.3
12.3	11.7	10.9	11.5	10.4	10.2	10.4	11.3	10.9	10.6
<u>30</u>	<u>28</u>	<u>17</u>	<u>14</u>	<u>6</u>	<u>1</u>	<u>5</u>	<u>12</u>	<u>15</u>	<u>30</u>

H.1 346.98

44.1	42.5	44.3	44.2	43.4	44.7	44.8	44.6	44.0	44.2
2.4	4.5	2.7	2.8	3.6	2.3	2.1	2.4	3.0	2.8
<u>30</u>	<u>24</u>	<u>21</u>	<u>16</u>	<u>14</u>	<u>5</u>	<u>1</u>	<u>6</u>	<u>12</u>	<u>30</u>

42.5

44.5	44.7	44.4	41.3	42.1	43.2	43.2	43.0	42.4	42.7	42.8
5.7	4.5	4.6	5.7	4.9	3.8	3.8	4.0	4.6	4.3	4.2
<u>24</u>	<u>26</u>	<u>24</u>	<u>16</u>	<u>14</u>	<u>13</u>	<u>5</u>	<u>5</u>	<u>12</u>	<u>14</u>	<u>30</u>

41.2	40.5	41.0	41.2	40.3	41.6	41.9	41.6	41.0	41.4	41.2
5.8	6.5	6.0	5.8	6.7	5.7	5.1	5.4	6.0	5.6	5.8
<u>30</u>	<u>28</u>	<u>26</u>	<u>17</u>	<u>15</u>	<u>6</u>	<u>1</u>	<u>6</u>	<u>12</u>	<u>21</u>	<u>30</u>

40.1	38.4	40.4	40.0	40.5	40.5	39.8	39.6
6.9	8.0	6.6	7.0	6.5	6.5	7.2	7.4
<u>30</u>	<u>28</u>	<u>26</u>	<u>14</u>	<u>5</u>	<u>1</u>	<u>12</u>	<u>30</u>

F.1
Central

41.7	40.4	39.8	40.0	40.0	40.1	40.2	40.4	40.5
5.3	6.6	7.2	7.0	7.0	6.9	6.8	6.6	6.5
<u>200</u>	<u>100</u>	<u>50</u>	<u>30</u>	<u>1</u>	<u>30</u>	<u>50</u>	<u>100</u>	<u>20</u>

39.6	37.3	38.6	39.0	39.3	39.0	38.8
8.2	9.75	8.7	8.0	7.7	8.0	8.2
<u>30</u>	<u>27</u>	<u>24</u>	<u>11</u>	<u>1</u>	<u>17</u>	<u>30</u>

F.1
Central

Mail in Pole (S. side) SW Cor Central Ave.

x

H.I. 341.33

2/

341.33

32+50

36.9	36.4	36.7	37.7	36.3	36.7	36.9	36.5	37.9	38.3	36.4
2.4	4.4	4.7	3.6	2.0	2.6	2.5	2.8	3.4	3.0	2.9
31	30	29	27	8	5	7	7	15	16	30

33

37.3	35.0	36.0	36.1	37.4	37.3	37.0	36.3	36.8	37.0
4.0	6.3	5.3	5.2	4.1	4.0	4.3	5.0	4.5	4.3
30	24	24	17	5	7	7	16	19	30

+50

35.9	33.8	34.7	34.7	35.4	35.9	35.7	35.0	35.4	35.4
5.4	7.5	6.6	6.6	5.7	5.4	5.6	6.3	5.9	6.1
30	29	27	17	10	7	7	16	19	30

34

33.3	33.4	34.1	34.1	33.1	33.9	33.8	33.8
8.0	7.9	7.2	7.2	8.2	7.4	7.5	7.5
30	18	11	11	14	18	26	30

+50

31.7	32.4	32.0	32.3	32.6	32.3	32.5	31.9	32.0
9.6	9.1	9.3	9.0	9.7	9.0	9.8	9.4	9.3
30	22	15	8	7	6	17	20	30

3.44

335.02

9.75

331.55

H.I. 335.02

35

31.3	31.3	30.6	31.4	31.6	31.2	30.5	30.8	30.7
3.7	3.7	4.4	3.6	3.4	3.8	4.5	4.2	4.3
30	17	15	9	7	11	16	19	30

+50

27.6	28.6	28.8	29.9	30.3	30.5	29.9	29.1	30.2	29.8
1.4	6.4	6.2	5.1	4.7	4.5	5.1	5.9	4.8	5.2
34	27	21	19	10	7	12	17	18	30

+64

29.7	30.1	29.9	30.4	29.8	29.6	29.3	29.1
5.3	4.9	5.1	4.6	5.2	6.4	5.9	5.9
30	15	12	12	13	16	21	30

+

335.07

35764

On line of wash

+76

36

+56

37

3.45 331.57

5.58 337.15

+50

38

+50

Lt. H. I 335-02 R. t.

22

28.7	27.9	27.5	27.8	27.5	27.9	30.4	29.8	27.3	26.7	27.3	27.3	26.9	26.8	26.3
$\frac{6.3}{200}$	$\frac{7.1}{100}$	$\frac{7.5}{50}$	$\frac{7.7}{30}$	$\frac{7.55}{15}$	$\frac{5.1}{10}$	$\frac{4.6}{10}$	$\frac{5.2}{70}$	$\frac{7.7}{73}$	$\frac{8.35}{20}$	$\frac{7.7}{30}$	$\frac{7.7}{50}$	$\frac{8.1}{100}$	$\frac{8.5}{50}$	$\frac{8.7}{20}$

F.L.
CulvertF.L.
Culvert

30.4	30.3	30.2	30.4	29.5	27.5	27.3
$\frac{4.6}{30}$	$\frac{4.7}{16}$	$\frac{4.8}{11}$	$\frac{4.6}{10}$	$\frac{5.5}{14}$	$\frac{7.5}{23}$	$\frac{7.7}{30}$

31.0	30.5	29.8	30.4	30.1	29.4	30.5	30.2
$\frac{4.0}{30}$	$\frac{4.5}{16}$	$\frac{5.2}{14}$	$\frac{4.6}{10}$	$\frac{4.9}{7}$	$\frac{5.2}{17}$	$\frac{4.5}{20}$	$\frac{4.8}{30}$

31.3	30.9	30.4	31.0	31.3	30.4	30.9	30.9
$\frac{3.7}{30}$	$\frac{4.1}{19}$	$\frac{4.6}{17}$	$\frac{4.0}{9}$	$\frac{3.7}{14}$	$\frac{4.6}{18}$	$\frac{4.1}{18}$	$\frac{4.1}{30}$

31.4	31.3	30.9	31.5	30.6	31.1	31.2
$\frac{3.6}{30}$	$\frac{3.7}{19}$	$\frac{4.2}{16}$	$\frac{3.5}{10}$	$\frac{4.4}{14}$	$\frac{3.9}{17}$	$\frac{3.8}{30}$

H. I 337.15

31.9	31.7	31.1	31.5	31.8	31.2	31.5	31.5
$\frac{5.3}{30}$	$\frac{5.5}{19}$	$\frac{6.1}{17}$	$\frac{5.7}{10}$	$\frac{5.4}{14}$	$\frac{6.0}{17}$	$\frac{5.7}{17}$	$\frac{5.7}{30}$

32.4	32.0	31.5	31.7	32.2	31.4	31.9	31.8
$\frac{4.8}{30}$	$\frac{5.2}{19}$	$\frac{5.7}{16}$	$\frac{5.7}{9}$	$\frac{5.0}{10}$	$\frac{4.6}{15}$	$\frac{5.3}{18}$	$\frac{5.4}{30}$

32.6	32.3	31.7	32.7	31.8	32.1	31.9
$\frac{4.6}{30}$	$\frac{4.4}{19}$	$\frac{5.1}{17}$	$\frac{4.5}{15}$	$\frac{5.4}{13}$	$\frac{5.1}{10}$	$\frac{5.3}{30}$

39

337.15

+50

40

+50

41

5.32 339.99

+32

+44

+44

2.48 334.67

Angle of Wash

H.1 337.15

23

32.6	32.4	31.6	32.6	32.6	31.9	31.8
$\frac{4.6}{30}$	$\frac{4.8}{20}$	$\frac{5.4}{16}$	$\frac{4.1}{10}$	$\frac{4.6}{10}$	$\frac{5.3}{15}$	$\frac{5.4}{30}$

33.0	32.6	32.3	32.7	32.9	32.4	32.2	31.9	30.0
$\frac{4.2}{30}$	$\frac{4.4}{20}$	$\frac{4.9}{16}$	$\frac{4.8}{10}$	$\frac{4.5}{10}$	$\frac{4.8}{12}$	$\frac{5.0}{15}$	$\frac{5.3}{26}$	$\frac{7.2}{31}$

33.1	32.6	32.9	32.7	32.8
$\frac{4.1}{30}$	$\frac{4.6}{16}$	$\frac{4.3}{10}$	$\frac{4.5}{14}$	$\frac{4.4}{30}$

33.0	33.6	33.2	33.8	33.4	33.2	33.2
$\frac{4.2}{30}$	$\frac{3.6}{18}$	$\frac{4.0}{16}$	$\frac{3.4}{5}$	$\frac{3.4}{10}$	$\frac{4.0}{19}$	$\frac{4.0}{30}$

34.0	34.1	33.7	34.3	34.5	33.5	34.1	34.0
$\frac{3.2}{30}$	$\frac{3.1}{23}$	$\frac{3.5}{18}$	$\frac{2.9}{13}$	$\frac{2.7}{10}$	$\frac{3.7}{14}$	$\frac{3.1}{17}$	$\frac{3.2}{31}$

Mail in end S.W. wing 11 Pt. 41+20

34.4	34.9	34.9	30.0	30.4
$\frac{5.6}{30}$	$\frac{5.2}{10}$	$\frac{5.2}{6.5}$	$\frac{100}{8}$	$\frac{9.6}{30}$

31.5	30.2	29.8	30.0	29.5	35.0	35.0	35.0	28.7	28.4	28.8	28.2	27.8	
$\frac{8.5}{200}$	$\frac{9.5}{100}$	$\frac{10.2}{50}$	$\frac{100}{30}$	$\frac{10.5}{11}$	$\frac{5.0}{10}$	$\frac{5.0}{10}$	$\frac{5.0}{10}$	$\frac{5.0}{6.5}$	$\frac{11.5}{7}$	$\frac{11.6}{30}$	$\frac{11.5}{50}$	$\frac{11.8}{100}$	$\frac{12.2}{200}$

41+55

339.99

+73

42

+50

43

+50

+68.15

Blu.

1.41 338.58

H.1 339.99

21

30.6	30.1	29.6	30.0	30.1	30.0	30.4	30.9
<u>94</u>	<u>99</u>	<u>104</u>	<u>5.00</u>	<u>49</u>	<u>5.0</u>	<u>56</u>	<u>5.1</u>
30	24	11	10	800	11	16	30
				Foot			

35.1	35.4	34.6	35.3	35.0	34.3	34.7	35.0
<u>49</u>	<u>46</u>	<u>54</u>	<u>47</u>	<u>5.0</u>	<u>5.7</u>	<u>5.3</u>	<u>5.0</u>
30	20	15		17	17	20	30

35.5	35.0	35.4	35.0	34.3	35.0	35.5
<u>45</u>	<u>5.0</u>	<u>46</u>	<u>5.0</u>	<u>5.7</u>	<u>48</u>	<u>4.5</u>
30	18		11	17	14	30

36.7	35.3	35.3	36.0	35.8	35.1	36.0	36.0	37.6
<u>3.3</u>	<u>4.7</u>	<u>4.7</u>	<u>4.0</u>	<u>4.2</u>	<u>4.9</u>	<u>4.0</u>	<u>4.0</u>	<u>2.4</u>
30	27	16		7	16	18	27	30

36.2	36.0	35.4	36.2	36.7	36.2	36.5	36.8	37.2
<u>38</u>	<u>4.0</u>	<u>4.6</u>	<u>3.8</u>	<u>3.3</u>	<u>3.8</u>	<u>3.0</u>	<u>3.2</u>	<u>1.8</u>
30	21	19	17		13	18	27	30

36.1	36.2	37.4	36.7	37.3	37.3
<u>3.9</u>	<u>3.8</u>	<u>2.6</u>	<u>3.3</u>	<u>2.7</u>	<u>2.7</u>
30	18		15	27	30

37.3	36.6	36.6	36.8	36.4	37.1	37.4	37.2	37.8	39.7	43.3	
<u>2.7</u>	<u>3.4</u>	<u>3.4</u>	<u>3.5</u>	<u>3.6</u>	<u>2.9</u>	<u>2.6</u>	<u>2.8</u>	<u>2.4</u>	<u>2.2</u>	<u>0.3</u>	<u>+3.3</u>
15	10	50	30	27	14		21	30	50	100	200

Nail in Power Pole 22 ft. Sta 43+40

X

CHECK LEVELS

				338.58	
1.21	339.99				
		5.32	334.67	334.67	On End of SW Wing of Bridge -
2.39	337.06				
		5.79	331.27		
7.69	338.96				
		0.13	338.83		
10.68	349.51				
		8.23	341.28	341.33	Nail in Pole SW Cor. Central
		0.19	349.32		
11.52	360.86				
		0.17	360.69		
11.53	372.42				
		0.43	371.79		
11.24	383.03				
		0.52	382.51		
12.02	394.53				
		0.15	394.38		
11.78	406.16				
		0.02	406.14		
11.89	418.03				
		0.18	417.85		
11.67	429.52	6.84	422.68	422.71	Nail in Pole SW Cor Sweetwater.

Check Levels Cont'd.

26

	429.52			
		0.34	429.18	
11.44	440.67			
		0.60	440.07	
10.87	450.89			
		0.46	450.43	
11.60	462.03			
		0.15	461.88	
11.29	473.57			
		0.03	473.54	
11.29	484.83			
		0.00	484.83	
11.17	495.97			
		0.52	495.45	
5.15	500.60			
		8.57	492.03	
0.23	492.26			
		9.73	482.53	482.69

482.69

Nail in Cor F Post Lt O+20

7.79 490.48

0.13 490.35

10.83 501.18

7.59 493.59

0.48 494.07

11.83 482.24

0.14 482.38

11.46 490.92

0.14 471.06

11.39 459.67

0.76 460.43

9.76 450.67 450.67

11.49 448.94

1.05 449.99

11.34 438.65

0.89 439.54

11.47 428.07

2.07 430.12

7.47 422.67 422.91

Nail in Pole SW Cor Sweetwater

7+39³⁰ Central =
Lamar St P.I.#7



LAMAR ST

x x x x

Fence

SWEETWATER AVE.

1940.880
Est. 1/2" Pipe

7+39³⁰ P.I

28

30.5	7+10	Fence
17.5	7+10	Power Pole
2+6.4		20°
1+5.7		
5	6+90	2" Acacia
6+77		20°
6+50		20°
6+22		21°
5+97		21°
5+48		21°
5+22		21°
5+07		21°
Water Meter		
4+90	4+90	2" Acacia
4+65		Power Pole
4+59		21°
4+00		21°
3+70		3+70
3+34		Fence
3+20		20°
3+13		20°
2+20		2+20
1+70		Power Pole
1+29		21°
1+6		21°
0+27		2" Acacia
0+00		Ed 1/2" Iron Pipe

{ Aug 7-26
David
Anderson
Jobless

32+1.476 Troy Ave =
0+00 Central Ave



TROY ST.

Aug 7-1926
Dorval
Anderson
de la Vaux

29

X Sec Central Ave Troy St to

Lamar St.

B.M.

341.33

5.60 346.93

Start in S. Side Pole JW cor Troy & Central

H-1 346.93

0+00 Along E. Troy St.

42.7	41.4	40.8	340.0	38.9	38.4	36.8
42	55	62	42	82	85	102
30	50	20		30	50	100

+27

40.7	40.4	39.7	38.4	40.2	39.8	38.1	37.2	37.2	37.1
62	65	82	85	60	71	82	92	92	98
30	20	19	17	10		15	16	17	30

Flowline 12" Cor. Iron Pipe Culvert

+30

40.7	40.4	39.1	40.2	40.0	38.8	37.6	39.0	38.9
62	65	78	62	62	82	92	72	82
30	20	18	15		10	18	19	30

+50

40.4	39.0	39.4	39.7	38.6	38.1	38.0
65	72	75	72	82	82	82
30	18	15		15	17	30

+100

40.4	40.0	39.5	40.2	38.6	39.1	39.0
65	62	72	66	82	78	72
30	18	15		15	18	30

+50

40.9	40.4	39.7	40.5	38.9	39.4	39.2
62	65	72	62	80	75	72
30	17	15		15	18	30

6.45 340.48

5.40 345.88

X 345.9

2+00

41.1	40.4	39.8	40.6	38.3	39.7	39.3
42	55	62	52	62	62	60
30	18	15		15	18	30

X

345.88

2+50

3+00

4+50

4+00

4+50

5+00

TP

5.98

347.82

4.04 34.84

5+50

6+00

6+50

H1 345.9

30

41.1	40.9	40.1	40.6	39.4	39.7	39.7
48	52	58	52	65	62	62
30	18	15		15	19	30

41.4	41.0	40.0	41.2	39.7	40.3	40.0
45	49	52	47	62	56	59
30	19	16		16	19	30

41.6	41.4	40.6	41.6	40.1	40.7	40.4
47	45	52	43	58	52	55
30	18	16		16	20	30

42.3	41.9	41.1	42.0	40.4	41.0	40.6
36	40	48	32	55	42	53
30	18	15		16	18	30

42.7	42.4	41.3	42.5	40.9	41.4	41.1
32	35	46	32	50	45	48
30	19	15		15	19	30

43.5	42.7	41.9	43.1	41.5	41.9	42.2
22	32	42	22	42	40	32
30	18	16		16	19	30

347.82
Top Water Meter 21' R Sta 5+02 - 76.32

43.6	43.1	42.2	43.2	41.6	42.2	42.2
42	47	50	46	62	50	50
30	19	15		17	19	30

44.0	43.4	42.6	43.6	42.6	42.6	42.1
38	42	50	43	52	52	52
30	19	16		16	20	30

34782

6+50

7+00

1+23

131 along E Lamar St.

BM. 2.96 344.86

Check Levels

BM. 344.86

2.02 346.88

6.13 346.75

7.11 347.86

BM. 6.53 341.33 OK

H.I. 347.82

31

43.4	43.6	42.8	43.8	42.3	42.8	42.8
39	42	50	40	55	50	50
30	18	15		15	18	30

44.4	43.7	43.6	43.8	42.6	43.1	43.0
38	41	42	40	52	47	40
30	18	15		16	17	30

44.0	43.4	43.6	42.7	42.1
38	41	43	51	51
30	16		17	30

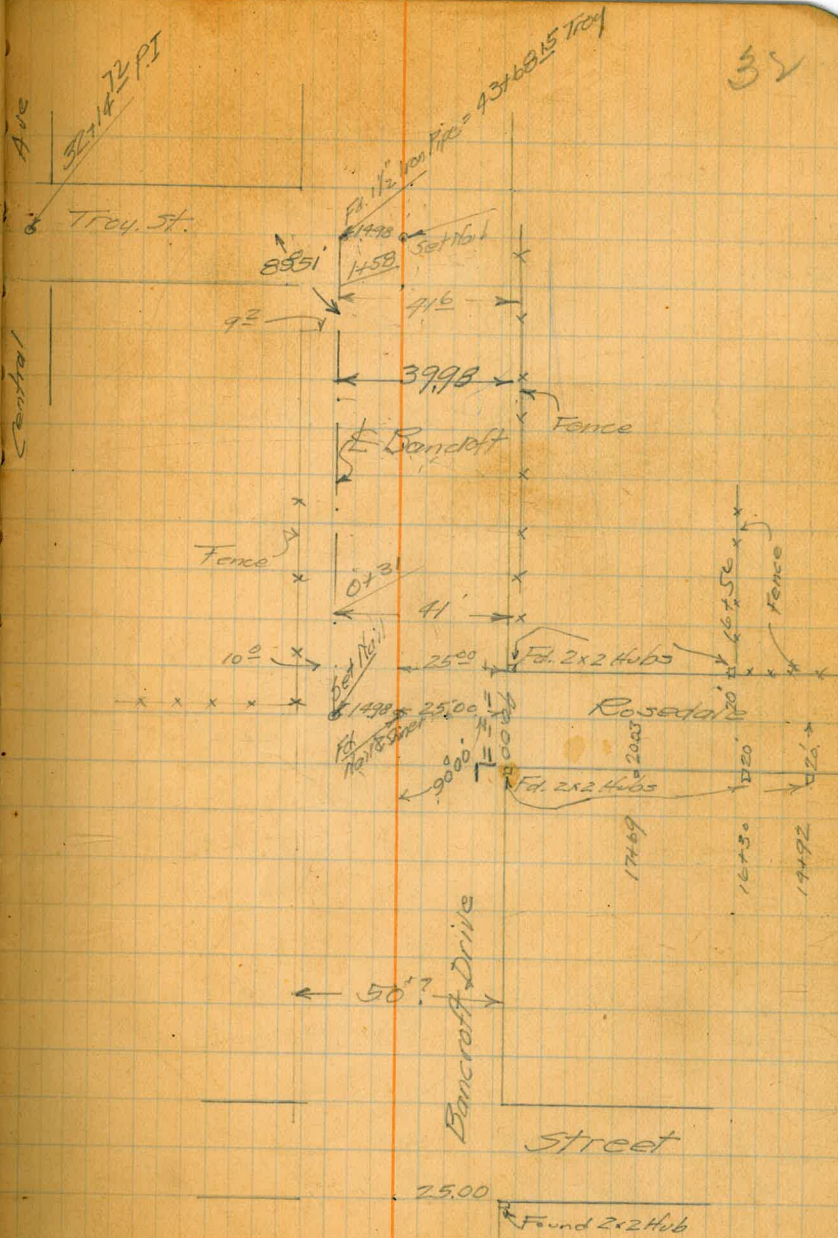
47.0	45.5	44.7	44.0	42.9	42.0	39.7
08	23	31	38	42	58	81
100	50	30		30	50	100

Nail in Pole (East side) S.W. Cor Lamar & Central

Nail in S. Side Pole S.W. Cor Central & Troy.

1490³⁵ Bancroft =
13+68¹⁵ Troy St.

0400 Bancroft =



x-See Bancroft St. Tray to Rosedale

BM 344.73

2.10 346.44

0100 Bancroft on Rt. along to Rosedale

0106 Top 3" Iron Pipe → 3⁶⁵

0450

1400

4.30

342.32

8.97 38.04

1750

160

190

On Left Along to Tray

BM

3.76 338.58

2.09 336.59

701

33

aug 7-1976

Dorval
Anderson
de la Vaux

Nail in Pole N. Side Bancroft St. Line Rosedale

H-1 346.99

43.0	42.9	42.7	43.0	42.6	44.0	46.1
40	4	4 ³	4 ²	4 ²	30	08
30		9	15		40	90

42.7	42.4	41.9	41.6	41.2	41.3	40.9	40.4	40.9	40.7	41.2	41.6
4 ³	4 ⁶	5 ¹	5 ²	5 ²	5 ²	6 ¹	6 ⁶	6 ¹	6 ²	5 ²	5 ²
30	26	23	8	6		8	9	17	25	20	40

42.6	42.1	41.4	40.4	40.1	39.8	39.4	39.9	39.2	39.3	39.0	40.8
4 ²	4 ²	5 ⁶	6 ⁶	6 ²	8 ²	7 ⁶	7 ¹	7 ²	7 ²	6 ²	6 ²
30	18	8	6		11	19	34	36	36	37	10

Top 3" Pipe Top 2" Pipe

342.32

39.8	38.8	38.4	37.8	37.5	37.1	37.7	37.0	37.5	38.2
2 ⁵	3 ⁵	3 ²	4 ⁵	4 ⁸	5 ²	4 ⁶	4 ³	4 ⁵	4 ¹
30	15	7	6		6	15	20	36	40

37.7	37.7	37.6	37.2	37.0	37.6	37.8	37.2	38.2
4 ⁶	4 ⁶	4 ²	5 ¹	5 ³	4 ²	4 ⁵	5 ¹	4 ¹
30	15	9	4		15	20	36	40

36.3	36.9	37.2	37.4	37.5	37.7	36.6	36.9
6 ⁶	5 ²	5 ¹	4 ⁹	4 ⁸	4 ⁶	5 ¹	5 ²
100	58	30		15	21	37	40

Nail in Pole SW Cor Tray to Bancroft

B.M.	376	344.34		338.58
	701	347.70	2.09	340.75
B.M.			1.53	344.73

34
Nail in Pole SW Cor Tray & Bancroft

Nail in Pole J. Line Parodale W side Bancroft.

35

16.51
2.01
14.10
4.84
8.94

30000
1500

48.54
6

5000
25000
15

50
625
117.5

21000

500
5000

30

50000

30

200

15

100

179 42

89 51

7739²⁰

578
540
560
1.698
1345
3.53

301.33
3.53
304.86

496
604
645
1.365

75 44

Nailin Post 51.72 elev.

Nailin^{tele} Post sta 21+50 11/5 elev 441.29