

NAME San Miguel #2

Class Alignment Course Party Job

257

RETURN TO
W. Leon Valle & Gough, Inc.
809 Broadway Bldg.
San Francisco

1980

335
FIELD NOTES

No. 403P

ESPECIALLY ADAPTED
TO THE USE OF
ENGINEERING STUDENTS

EUGENE DIETZGEN Co.

MANUFACTURERS

DRAWING MATERIALS

MATHEMATICAL AND SURVEYING INSTRUMENTS

MEASURING TAPES

CHICAGO SAN FRANCISCO NEW YORK
NEW ORLEANS PITTSBURGH

SAN MIGUEL #2

MICROFILMED
DEC 30 1964

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Alignment 100+74 ¹⁵ to 135+47 ⁸³ .	1-4
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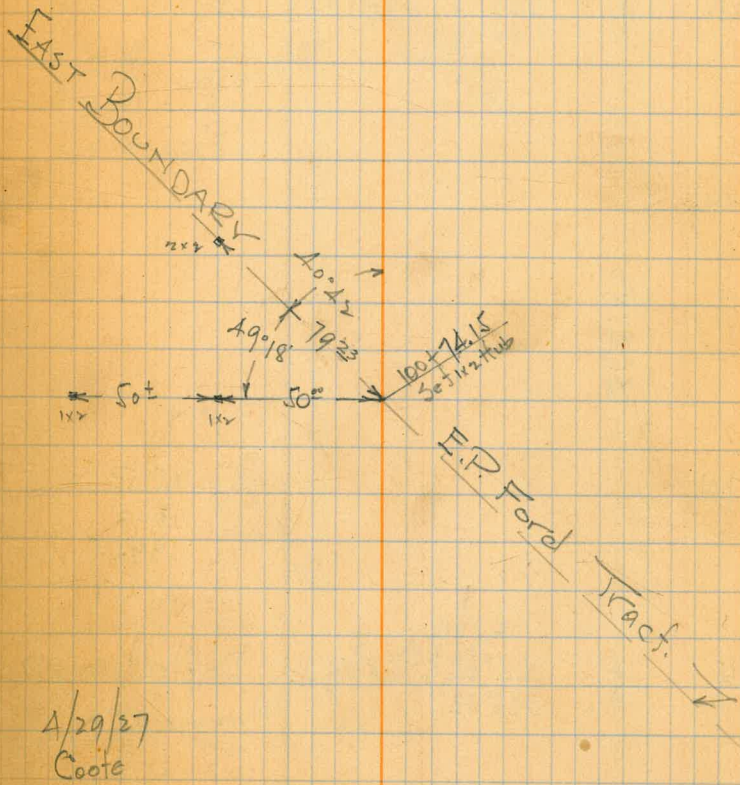
Sta. Dist. Angle
Az. Def.

245.00

100+74.15
PI

SAN MIGUEL

Unit # 2



4/29/27

Coote

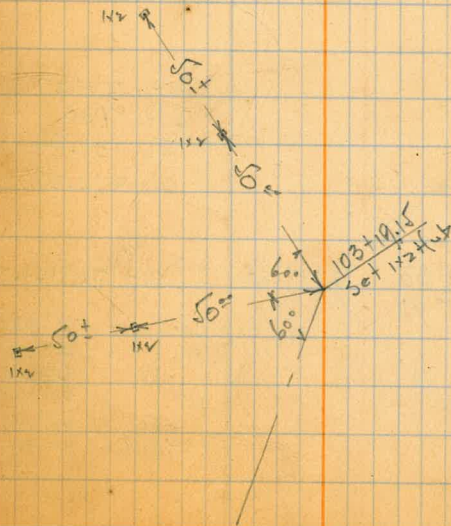
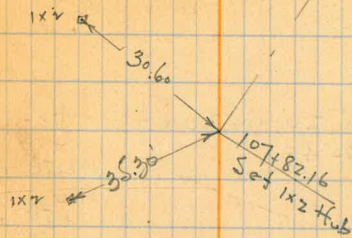
H. Thompson

Ryan-

Sta	Dist	Angle		Curve Data
		Az.	Def.	
108+87.58 P.T.	867.18			$\Delta = 42^{\circ}18'$ $R = 300'$ $T = 116.06$ $L = 221.48$
107+82.16 P.I.		$222^{\circ}18'$ $84^{\circ}36'$	$42^{\circ}18' R$	Deflections - $107 = 3^{\circ}14'$ $+50 = 8^{\circ}01'$ $108 = 12^{\circ}47'$ $+50 = 17^{\circ}34'$ $+87.58 = 21^{\circ}09'$
106+66.10 P.C.	464.80			

104+57.01 P.T.				$\Delta = 15^{\circ}54'$ $R = 1000'$ $T = 139.65$ $L = 277.51$
103+19.15 P.I.		$164^{\circ}06'$ $328^{\circ}12'$	$15^{\circ}54' L$	Deflections - $102 = 0^{\circ}35'$ $+50 = 2^{\circ}01'$ $103 = 3^{\circ}27'$ $+50 = 4^{\circ}53'$ $104 = 6^{\circ}19'$ $+50 = 7^{\circ}45'$ $+57.01 = 7^{\circ}57'$
101+19.50 P.C.	245.00			

≠ Ties -



Sta. Dist. Angle Az. Def. Curve Data

121+90.44
P.T. 574.88
 $\Delta = 15^{\circ}20'$
 $R = 1000'$
 $T = 134.61'$
 $L = 267.62'$

120+57.43
P.I. 195°20' 15°20' Rt
30°40'
Deflections -
119+50 = 0°47'
120 = 2°13'
+50 = 3°39'
121 = 5°05'
+50 = 6°31'
+90.44 = 7°40'

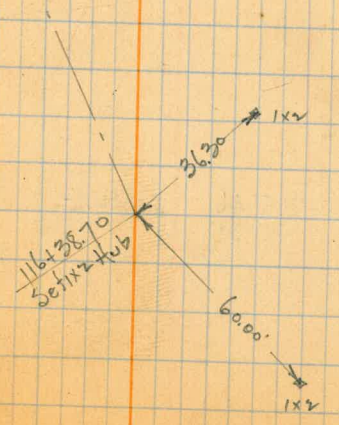
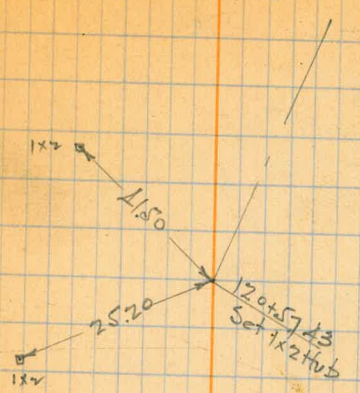
119+22.82
P.C. 422.29'

117+74.06
P.T. $\Delta = 22^{\circ}27'$
 $R = 700'$
 $T = 138.92'$
 $L = 274.28'$

116+38.70
P.I. 157°33' 22°27' Lt
315°07'
Deflections -
115+50 = 2°03'
116 = 4°06'
+50 = 6°09'
117 = 8°12'
+50 = 10°14'
+74.06 = 11°13½'

114+99.78
P.C. 867.18'

* Ties -



Sta. Dist. Az. Def. Curve Data-

104+77± Broadway Ext.
135+47.83 =
San Miguel

933.73'

127+50.08
P.I.

A = 48° 46'
E = 300'
T = 135.98
L = 255.34

126+30.72
P.I.

228° 46'
97° 31' 48° 46' R.

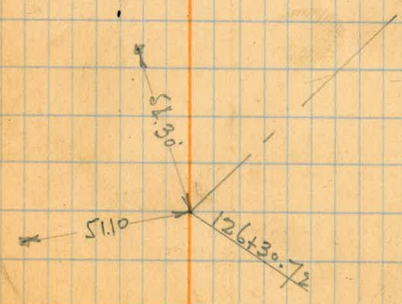
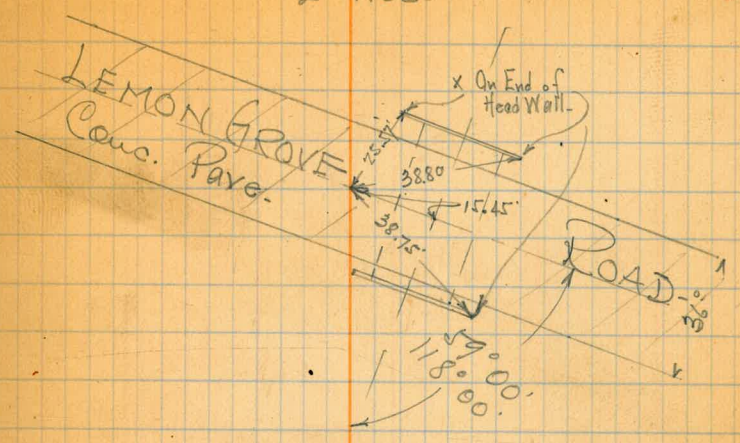
Deflections -
125 = 0° 30'
+50 = 5° 17'
126 = 10° 03'
+50 = 14° 49'
127 = 19° 36'
+50.08 = 24° 23'

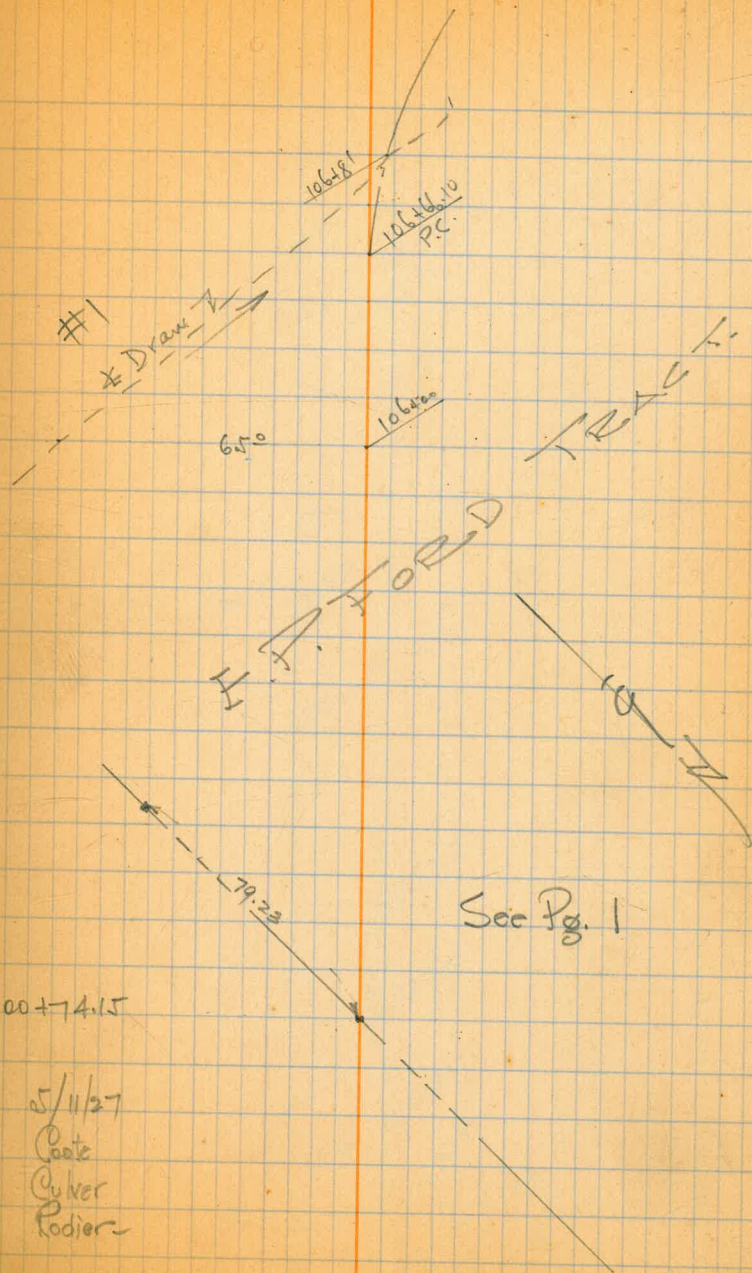
124+94.74
P.C.

574.88'

± Ties

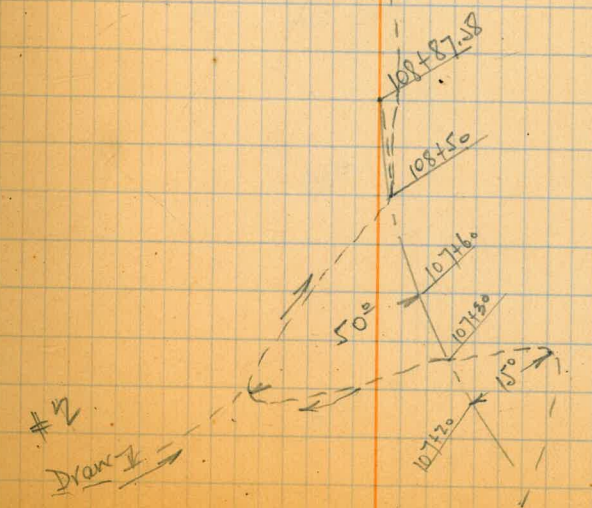
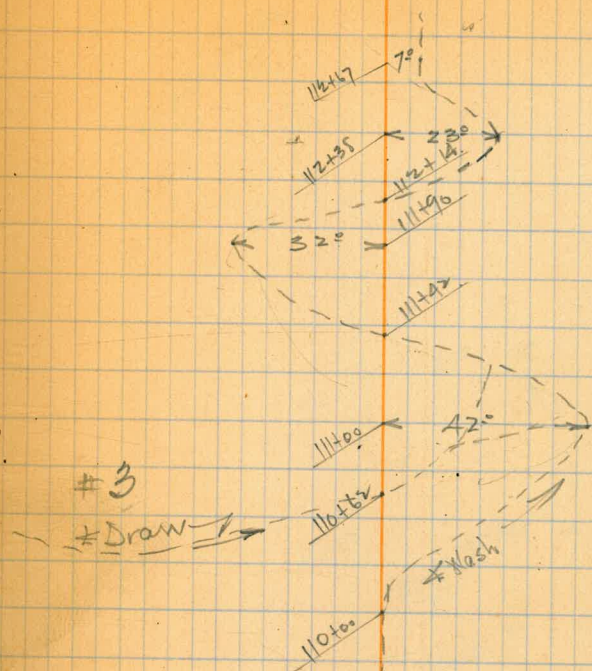
4

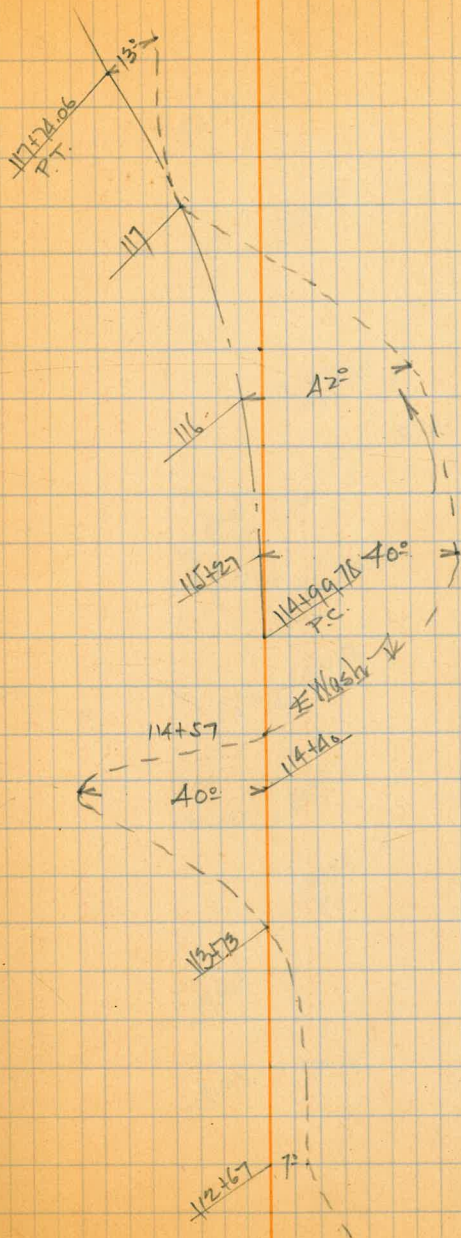


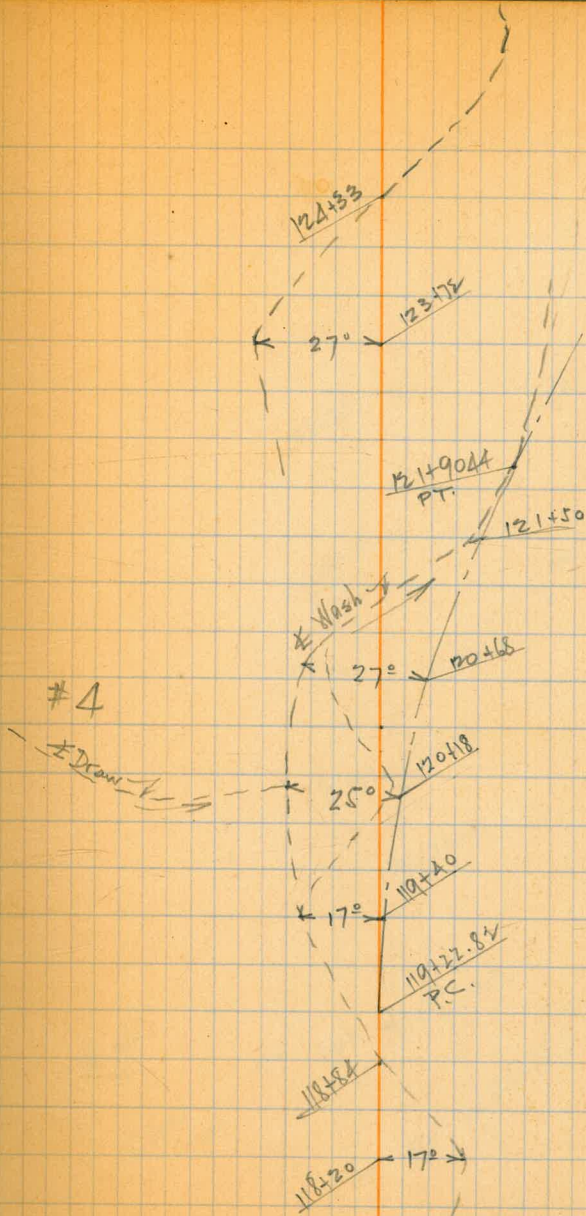


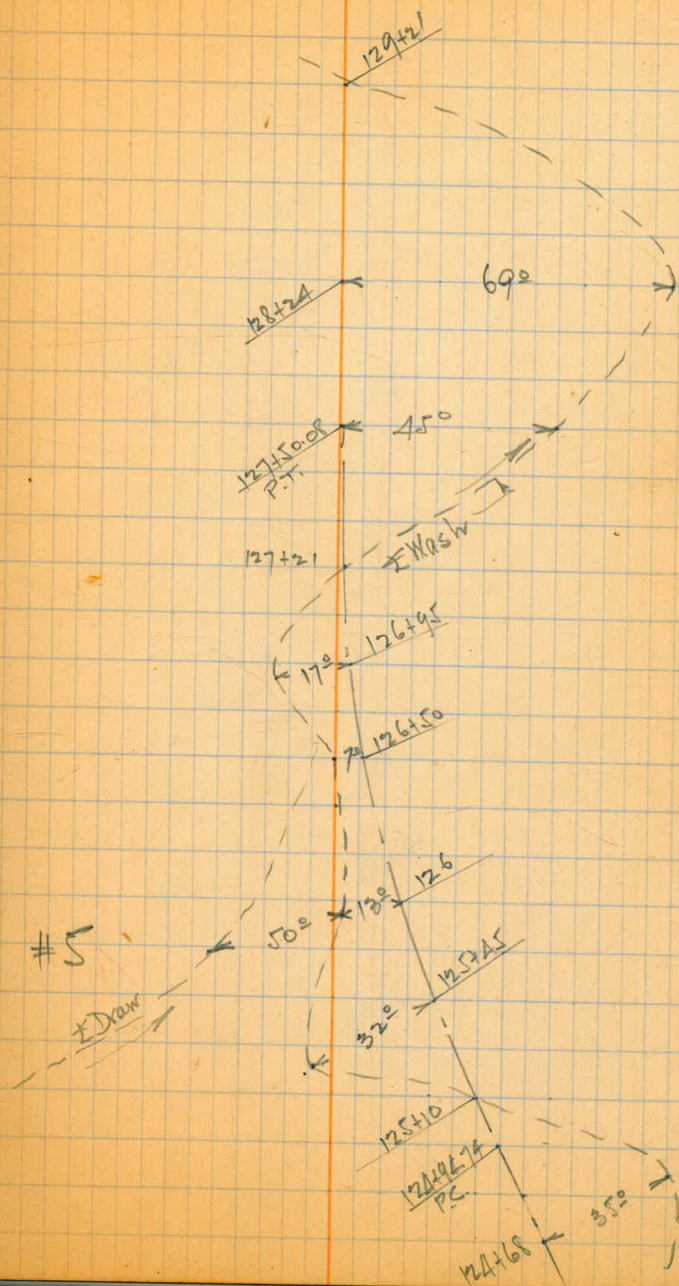
100+74.15

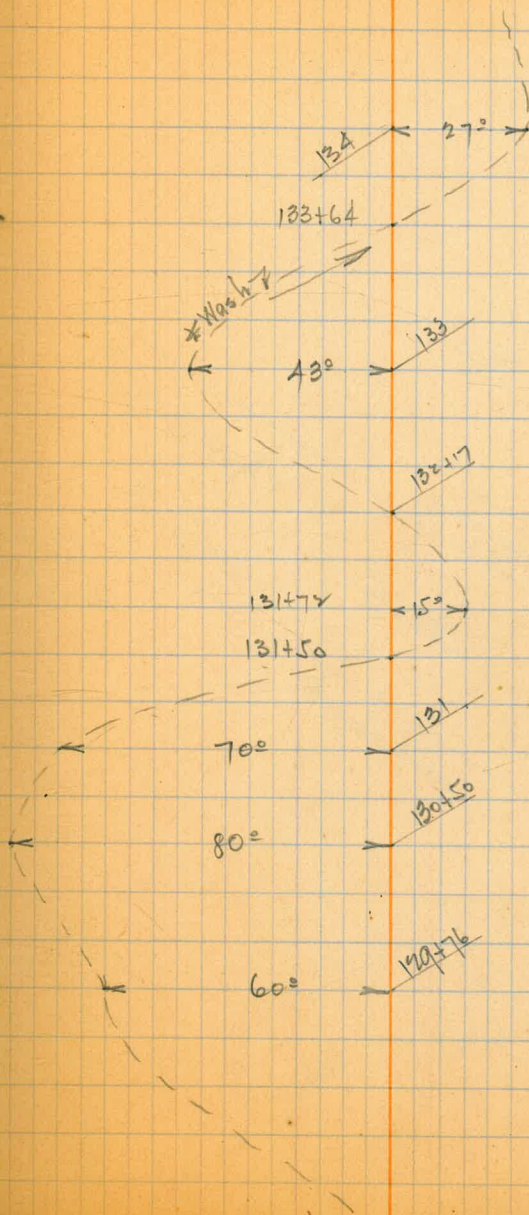
5/11/27
 Cook
 Culver
 Rodiers



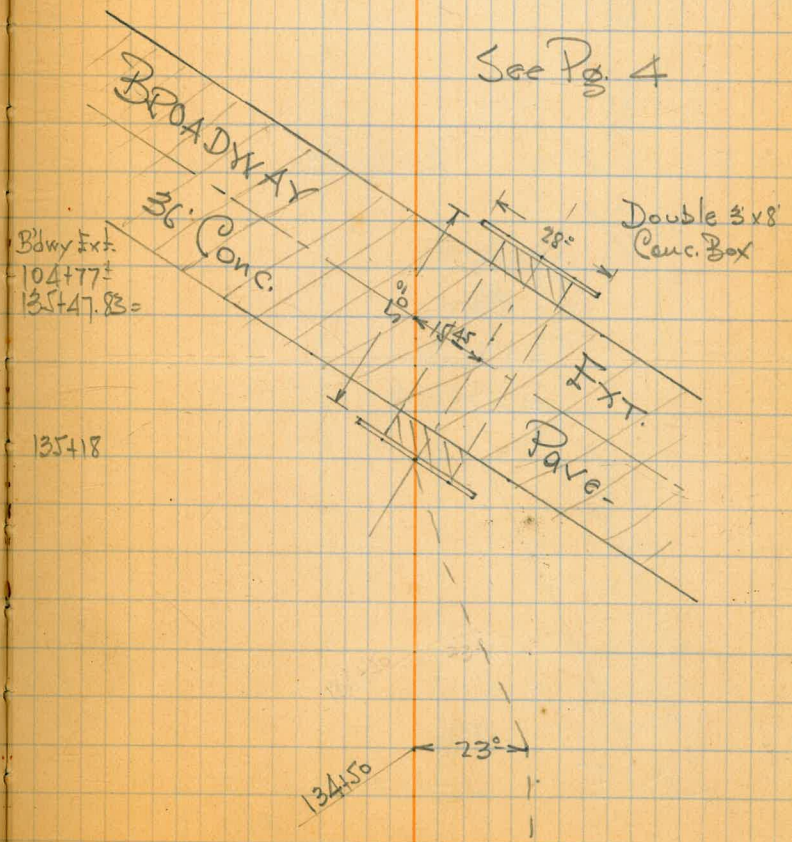








See Pg. 4



Sta.	Dist.	Angle Az. Def.	Bearing
------	-------	-------------------	---------

13

102+45.9
P.T.

584°55W

101+37.1
P.I.

43°10'P.

$$\Delta = 43^\circ 10'$$

$$P = 300$$

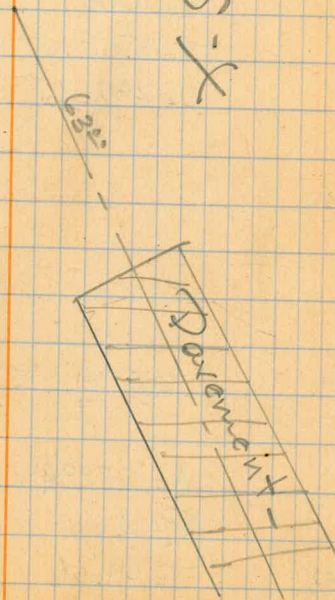
$$T = 120.20$$

$$L = 228.64$$

100+16.95
P.C.

541°15N

LINE CHANGE.



X-SECS on Pg. 16

Contd from Bk# 123/27

Cont'd in Bk # 119/25

Sta	Dist	Angle Az. Def.
111406.53 P.T.	Orig. Survey	
111411.95 P.I.		162° 55' 17° 05' Lt 325° 51'
10946175 P.C.		$\Delta = 17^{\circ} 05'$ $P = 1000'$ $T = 150.20$ $L = 298.16$
10643340 P.T.		
10544539 P.I.		205° 39' 25° 39' Rt 51° 17'
10445433 P.C.		$\Delta = 25^{\circ} 39'$ $P = 400'$ $T = 91.06$ $L = 179.07$

N86°31W

N69°26W

7- Secs -
Line Change

BW# D-0

1094 435.39

424.45

100+16.95

+50

+74

101

+50

Alignment on (D-0)

Sta 100+16.95 to

16

curvrtub 50' Lt 101+40

H.I. = 435.39

437.0 ^{438.0} 438.9 ^{438.2} 438.8 439.0 439.2 ^{438.9} 442.8 443.3 444.0

$\frac{+1.0}{20}$ $\frac{+2.6}{30}$ $\frac{+3.5}{18}$ $\frac{+3.8}{15}$ $\frac{+3.4}{10}$ $\frac{+3.6}{-}$ $\frac{+3.8}{50}$ $\frac{+3.5}{12}$ $\frac{+7.4}{15}$ $\frac{+7.9}{30}$ $\frac{+8.6}{40}$

436.0 436.4 436.8 436.8 436.9 436.7 436.8 436.9 438.9 440.3 441.4

$\frac{0.6}{20}$ $\frac{+1.0}{30}$ $\frac{+1.4}{18}$ $\frac{+0.4}{15}$ $\frac{+1.0}{10.5}$ $\frac{+1.3}{-}$ $\frac{+1.4}{6.5}$ $\frac{+1.0}{12}$ $\frac{+3.5}{14}$ $\frac{+4.9}{30}$ $\frac{+6.0}{40}$

432.6 433.7 433.8 434.4 434.9 435.0 434.9 437.4 439.7 441.1

$\frac{2.8}{20}$ $\frac{1.7}{30}$ $\frac{1.6}{18}$ $\frac{1.0}{14}$ $\frac{0.5}{-}$ $\frac{0.4}{3}$ $\frac{0.5}{8}$ $\frac{+2.0}{12}$ $\frac{+4.3}{30}$ $\frac{+5.7}{40}$

429.1 430.9 433.2 434.0 435.4 438.9 440.0

$\frac{6.3}{20}$ $\frac{4.5}{30}$ $\frac{2.2}{17}$ $\frac{1.4}{-}$ $\frac{0.0}{6}$ $\frac{+3.5}{30}$ $\frac{+4.6}{40}$

427.3 428.3 430.4 432.3 434.4 437.3 438.7

$\frac{9.1}{20}$ $\frac{7.1}{30}$ $\frac{5.0}{13}$ $\frac{2.9}{-}$ $\frac{1.0}{13}$ $\frac{+1.9}{30}$ $\frac{+3.3}{40}$

435.39

102

445.59
P.T.

7.39 44x36 0.42 434.97

103

150

104

Lt.

Rt.

17

435.39

427.6	428.8	432.6	437.6	439.5
<u>7.8</u>	<u>6.6</u>	<u>2.8</u>	<u>+2.2</u>	<u>+4.1</u>
40	30		30	40

428.6	429.7	433.8	438.4	439.4
<u>6.8</u>	<u>5.7</u>	<u>1.6</u>	<u>+3.0</u>	<u>+4.0</u>
40	30		30	40

H.I. = 442.36

430.8	432.0	436.7	439.6	440.8	441.6
<u>11.6</u>	<u>10.3</u>	<u>5.7</u>	<u>2.8</u>	<u>1.6</u>	<u>0.7</u>
40	30		18	30	40

431.8	432.8	436.0	439.4	440.3
<u>10.5</u>	<u>9.6</u>	<u>6.3</u>	<u>3.0</u>	<u>2.1</u>
40	30		30	40

433.0	434.0	436.6	438.1	439.0
<u>9.4</u>	<u>8.4</u>	<u>5.7</u>	<u>4.2</u>	<u>3.3</u>
40	30		30	40

B

R

A12.38

104+36

+54.33
P.C.

0.13 435.92

6.57 435.79

105

+50

106

+3340
P.T.

R

Lt.

Rt.

18

442.36

433.5	434.4	436.7	437.4	436.4	436.6
$\frac{8.8}{40}$	$\frac{7.9}{30}$	$\frac{5.6}{40}$	$\frac{4.9}{10}$	$\frac{5.9}{30}$	$\frac{5.7}{40}$

433.8	435.3	436.0	435.5	436.7	435.8
$\frac{8.5}{40}$	$\frac{7.0}{30}$	$\frac{6.3}{40}$	$\frac{6.8}{21}$	$\frac{6.6}{30}$	$\frac{6.5}{40}$

H.I. = 435.92

434.5	434.9	434.8	434.3	434.8	433.2	432.6
$\frac{1.4}{40}$	$\frac{1.0}{30}$	$\frac{1.1}{4}$	$\frac{1.6}{40}$	$\frac{1.1}{13}$	$\frac{2.7}{30}$	$\frac{3.3}{40}$

434.2	434.4	432.9	433.1	432.0	430.2	429.7
$\frac{1.7}{40}$	$\frac{1.5}{32}$	$\frac{3.0}{30}$	$\frac{2.8}{9}$	$\frac{3.9}{40}$	$\frac{5.7}{30}$	$\frac{6.2}{40}$

430.9	430.4	430.1	427.5	427.0	426.2
$\frac{5.0}{40}$	$\frac{5.5}{30}$	$\frac{5.8}{40}$	$\frac{8.4}{19}$	$\frac{8.9}{30}$	$\frac{9.7}{40}$

427.5	427.1	426.9	425.4	424.3
$\frac{8.4}{40}$	$\frac{8.8}{30}$	$\frac{9.5}{40}$	$\frac{10.4}{20}$	$\frac{11.6}{40}$

R

106+67 = 435.92

0.75 425.52 11.15 424.77 ✓

107

+33

+55

+80

0.69 414.40 11.81 413.71 ✓

R

Lt.

Rt.

19

435.92

423.6	423.2	423.7	422.2	422.0
$\frac{12.3}{40}$	$\frac{12.7}{30}$	$\frac{12.2}{30}$	$\frac{13.7}{30}$	$\frac{13.9}{40}$

H.I. = 425.52

420.3	421.0	422.7	422.6	420.1	419.6	419.3
$\frac{5.2}{40}$	$\frac{4.5}{30}$	$\frac{2.8}{21}$	$\frac{2.9}{-}$	$\frac{5.4}{15}$	$\frac{5.9}{30}$	$\frac{6.2}{40}$

417.5	417.2	416.1	415.3	414.3
$\frac{8.0}{40}$	$\frac{8.3}{30}$	$\frac{9.4}{-}$	$\frac{10.2}{30}$	$\frac{11.2}{40}$

416.1	415.5	416.2	415.1	413.5	413.2	412.7
$\frac{9.4}{40}$	$\frac{10.0}{30}$	$\frac{9.3}{17}$	$\frac{10.4}{-}$	$\frac{12.0}{8}$	$\frac{12.3}{30}$	$\frac{12.8}{40}$

416.8	415.1	412.9	414.1	411.4	410.9	411.0
$\frac{8.7}{40}$	$\frac{10.4}{30}$	$\frac{12.6}{17}$	$\frac{11.4}{-}$	$\frac{14.1}{22}$	$\frac{14.6}{30}$	$\frac{14.5}{40}$

H.I. =

R

414.40

108

+23

+50

+75

109

0.00 402.91

11.49 402.91

+30

R

414.4

20

413.3	413.0	411.8	410.9	410.2	410.8	409.8
<u>11</u>	<u>14</u>	<u>2.6</u>	<u>3.5</u>	<u>4.8</u>	<u>3.6</u>	<u>4.6</u>
40	30	20		20	30	40

411.1	410.3	410.4	412.2	411.3	409.0	410.1	410.8	409.4
<u>3.3</u>	<u>4.1</u>	<u>4.0</u>	<u>4.2</u>	<u>3.1</u>	<u>5.4</u>	<u>4.3</u>	<u>3.6</u>	<u>5.0</u>
40	30	26	12		10	23	30	40

409.4	409.1	407.6	409.2	406.9	407.3
<u>5.0</u>	<u>5.3</u>	<u>6.8</u>	<u>5.2</u>	<u>7.5</u>	<u>7.1</u>
40	30		16	30	40

407.9	409.2	409.3	405.9	405.4	404.6	404.2
<u>6.5</u>	<u>5.2</u>	<u>5.1</u>	<u>8.5</u>	<u>9.0</u>	<u>9.8</u>	<u>10.2</u>
40	30	26	10		30	40

405.7	406.5	404.3	406.5	405.9	405.7	400.9	400.5	399.7
<u>8.7</u>	<u>7.9</u>	<u>10.1</u>	<u>8.9</u>	<u>8.5</u>	<u>8.7</u>	<u>13.5</u>	<u>13.9</u>	<u>14.7</u>
40	30	16	8		5	25	30	40

11.49 = 402.91

403.3	402.5	400.2	399.4	399.1	397.2	395.0
-------	-------	-------	-------	-------	-------	-------

<u>0.4</u>	<u>0.4</u>	<u>2.7</u>	<u>3.5</u>	<u>3.8</u>	<u>5.7</u>	<u>7.9</u>
40	30	9		17	30	40

R

40291

109+44

+61.75
PC.

+83

0.23 391.89

11.25 391.66

110+11

+34

+65

Ⓚ

402.9

21

402.2	400.7	399.4	398.9	398.0	395.1	393.6
$\frac{0.7}{40}$	$\frac{2.2}{30}$	$\frac{3.5}{20}$	$\frac{4.0}{-}$	$\frac{4.9}{9}$	$\frac{7.8}{30}$	$\frac{9.5}{40}$

410.2	398.6	395.1	392.8	392.6	391.3
$\frac{2.7}{40}$	$\frac{4.3}{30}$	$\frac{7.8}{-}$	$\frac{10.1}{26}$	$\frac{10.3}{30}$	$\frac{11.6}{40}$

397.0	396.3	396.1	393.6	393.1	391.9	388.1	385.9
$\frac{5.9}{40}$	$\frac{6.6}{30}$	$\frac{6.8}{19}$	$\frac{9.3}{4}$	$\frac{9.8}{-}$	$\frac{11.0}{17}$	$\frac{14.8}{30}$	$\frac{17.0}{40}$

H = 391.89

395.0	394.0	388.9	382.9	380.6
$\frac{+3.1}{40}$	$\frac{+2.1}{30}$	$\frac{3.0}{-}$	$\frac{9.0}{30}$	$\frac{11.3}{40}$

393.0	392.7	392.8	391.0	387.7	384.9	380.0	377.8
$\frac{+1.1}{40}$	$\frac{+0.8}{30}$	$\frac{+0.9}{24}$	$\frac{0.9}{10}$	$\frac{4.2}{-}$	$\frac{7.0}{9}$	$\frac{11.9}{30}$	$\frac{14.1}{40}$

391.1	387.6	382.5	379.1	377.9	375.6	372.9
$\frac{0.8}{40}$	$\frac{4.3}{30}$	$\frac{9.4}{-}$	$\frac{12.8}{14}$	$\frac{14.0}{24}$	$\frac{16.3}{30}$	$\frac{19.0}{40}$

Ⓚ

110+87

391.89

0.32 380.42

11.79 380.10 ✓

111+16

+35

+60

0.16 368.69

11.89 368.53 ✓

+75

391.89

22

386.3 383.8 384.7 379.9 377.6 377.8 371.9 368.8

$\frac{5.6}{40}$ $\frac{6.1}{30}$ $\frac{7.2}{21}$ $\frac{12.0}{8}$ $\frac{14.3}{8}$ $\frac{17.1}{20}$ $\frac{20.0}{30}$ $\frac{23.1}{40}$

H.I. = 380.42

385.4?

375.4 381.2 375.2 374.9 373.4 370.0 368.1 363.9

+30
 $\frac{5.0}{40}$ $\frac{7.08}{30}$ $\frac{1.2}{19}$ $\frac{5.5}{9}$ $\frac{7.0}{9}$ $\frac{10.4}{25}$ $\frac{12.3}{30}$ $\frac{16.5}{40}$

381.4 381.2 377.8 373.2 368.6 362.1 361.1

$\frac{+1.0}{40}$ $\frac{+0.8}{30}$ $\frac{2.6}{14}$ $\frac{7.2}{15}$ $\frac{11.8}{15}$ $\frac{18.3}{30}$ $\frac{19.3}{40}$

379.8 377.0 369.2 365.7 358.5 355.4

$\frac{0.6}{40}$ $\frac{3.4}{30}$ $\frac{11.2}{13}$ $\frac{14.7}{13}$ $\frac{21.9}{30}$ $\frac{25.0}{40}$

H.I. = 368.69

379.9 375.1 371.0 367.5 360.1 355.6 352.7

$\frac{+9.2}{40}$ $\frac{+6.4}{30}$ $\frac{+2.3}{16}$ $\frac{1.2}{14}$ $\frac{8.6}{14}$ $\frac{13.1}{30}$ $\frac{16.0}{40}$

R

R

115

368.69

+36

1.66

359.05

11.30

357.39

+599
P.T.

2.6

57.5

9.8

1.5

(R)

368.69

23

375.8	374.2	364.7	361.3	353.1	352.5	347.7
$\frac{+7.1}{40}$	$\frac{+55}{30}$	$\frac{10}{11}$	$\frac{7.4}{11}$	$\frac{15.6}{23}$	$\frac{16.2}{30}$	$\frac{21.0}{40}$

373.0	367.8	361.5	356.9	350.3	346.9	344.3
$\frac{+4.3}{40}$	$\frac{0.9}{30}$	$\frac{7.2}{14}$	$\frac{11.5}{14}$	$\frac{18.4}{14}$	$\frac{21.9}{30}$	$\frac{24.8}{40}$

359.05

369.0	364.5	352.2	348.7	345.7	343.1	341.0
-------	-------	-------	-------	-------	-------	-------

$\frac{+10.0}{40}$	$\frac{+55}{30}$	$\frac{6.8}{14}$	$\frac{10.3}{9}$	$\frac{13.3}{24}$	$\frac{15.9}{30}$	$\frac{18.0}{40}$
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old P.T.

RH 100' ahead old P.T.

20' "

(R)

Rough Grades

Sta.		± Grade	Header Grade
100+16.9	PC 0-00	724 ^	
100+25	0-46	776 v 2592 ^ 24.08 v	38.60 38.54
+50	3-09		36.60 36.54
+75	5-32		34.67 34.59
101+00	7-55.4		33.17 33.09
+25	10-18.6		32.32 32.24
+50	12-42		32.08 32.00 (22)
+75	15-05		32.43 32.35 789
102+00	17-28		33.08 33.00
+25	19-51.5	21.32 ^ 19.86 v	33.73 33.65
102+45.9	P.T.	21.50	34.28 34.20
102+75			34.97 34.89

Left

Right

Headings

$$-\frac{11}{25} \text{ (-0.02)}$$

$$+\frac{4.6}{25} \text{ (-0.35)}$$

$$-\frac{13}{25} \text{ (+0.08)}$$

$$+\frac{4.5}{25} \text{ (-0.38)}$$

$$-\frac{30}{28} \text{ (+0.10)}$$

$$+\frac{3.6}{25} \text{ (-0.07)}$$

$$-\frac{3.9}{30} \text{ (-0.49)}$$

$$+\frac{3.4}{25} \text{ (-0.29)}$$

$$-\frac{4.2}{3.1} \text{ (-0.07)}$$

$$+\frac{2.6}{25} \text{ (-0.54)}$$

$$\frac{4.0}{31} \text{ (-0.05)}$$

$$+\frac{2.2}{25} \text{ (-0.51)}$$

$$-\frac{4.2}{31} \text{ (-0.46)}$$

$$+\frac{3.2}{25} \text{ (-0.72)}$$

$$\frac{3.6}{30} \text{ (+0.04)}$$

$$+\frac{4.2}{25} \text{ (-0.55)}$$

Rough Grades

Sta.		Header Grade	Header Grade		Left	Right
103		35.45	35.37	(487)	$\frac{-2.7}{28}$ (-0.10)	$\frac{+4.3}{25}$ (-0.38)
+25		35.82	35.74	(450)	$\frac{-2.3}{28}$ (-0.21)	$\frac{+3.7}{25}$ (-0.3)
+50		36.08	36.00	(424)	$\frac{-2.8}{28}$ (-0.20)	$\frac{+2.3}{25}$ (-0.33)
+75		36.28	36.20	(404)	$\frac{-2.3}{28}$ (-0.08)	$\frac{+1.5}{25}$ (-0.46)
104		36.35	36.27	(397)	$\frac{-1.7}{27}$ (-0.12)	$\frac{+1.3}{25}$ (-0.20)
+25		36.16	36.08	(416)	$\frac{-1.1}{27}$ (-0.56)	$\frac{+1.5}{25}$ (+0.02)
104+54.33.P.C.	21241 20101	35.59	35.51	(473)	$\frac{+0.3}{25}$ (-0.42)	$\frac{-0.2}{25}$ (-0.23)
+75	1-303 2569 2431	35.01	34.93	(531)	$\frac{0.0}{25}$ (-0.47)	$\frac{+0.1}{25}$ (-0.09)
105	3-177 "	34.18	34.10	(448)	$\frac{+0.4}{25}$ (-0.33)	$\frac{0.0}{25}$ (+0.14)
+25	5-05 "	33.34	33.26		$\frac{+0.7}{25}$ (-0.48)	$\frac{-1.6}{27}$ (+0.08)
+50	6-225 "	32.33	32.25		$\frac{+0.6}{25}$ (-0.30)	$\frac{-1.4}{27}$ (-0.11)
+75	8-40 "	31.01	30.93		$\frac{-0.3}{25}$ (-0.42)	$\frac{-2.3}{28}$ (-0.22)

Rough Grades

Sta.		Grade	Healer Grade		Left	Right
106	10-275 34.31 22.49	29.34	29.26	(22)	+1.0/ 25 (-0.40)	-1.8/ 29 (+0.09)
106.733-40	12-49.5 F.T.	26.65	26.57	(4.81)	+0.1/ 25 (-0.34)	-1.0/ 27 (+0.18)
+50		25.19	25.11	(6.27)	0.0/ 25 (-0.57)	-1.2/ 27 (+0.10)
107		20.87	20.79		+0.9/ 25 (-0.22)	-1.1/ 27 (+0.31)
+50		16.55	16.47	(3.67)	-0.4/ 25 (-0.57)	-1.7/ 27 (-0.15)
108		12.23	12.15	(7.99)	0.0/ 25 (-1.11)	-1.2/ 27 (-0.33)
+50		07.91	07.83		+0.9/ 25 (-0.60)	+0.2/ 25 (+0.12)
109		03.59	03.51	(4.55)	+3.0/ 25 (-0.60)	-2.1/ 28 (+0.03)
+25		01.23	01.15	(6.91)	+0.8/ 25 (-0.71)	-3.0/ 28 (+0.06)
+50		398.47	+98.39	(9.67)	+0.5/ 25 (-0.68)	-3.5/ 30 (+0.04)
+61.75 P.C.	0-00 13.39 13.11	97.60	96.92	(11.14)	+0.5/ 25 (-0.67)	-4.7/ 31 (+0.13)
+75	0-22.5	95.32	95.25	(14.6)	+0.9/ 25 (-0.62)	-6.5/ 33 (+1.27)

Rough Grades

Sta		Grade	Header Side	Left	Right
110	1-05	$\frac{25.27}{24.67}$ 91.77	91.69	$\frac{+24}{25} - 0.14$	$\frac{-7.6}{36} + 0.38$
+50	2-31	$\frac{100.55}{99.45}$ 84.27	84.19	$\frac{+54}{25} - 0.90$	$\frac{-89}{36} + 0.51$
111	3-57	"	76.77	$\frac{+58}{25} - 0.81$	$\frac{-5.5}{32} + 0.11$
+50	5-03	"	69.27	$\frac{+7.1}{25} - 0.62$	$\frac{-11.3}{40} - 0.07$
111+75	6-06	$\frac{25.27^A}{24.67}$ 65.52	65.44	$\frac{+7.1}{25} - 0.71$	$\frac{11.4}{40} - 0.34$
112	6-49	"	61.59	$\frac{+9.4}{25} - 0.11$	$\frac{-13.8}{41} + 0.24$
+25	7-31	"	57.84	$\frac{+9.7}{25} + 0.69$	$\frac{-14.8}{46} + 0.94$
+50	8-15	"	56.33	$\frac{+8.2}{25} - 0.27$	$\frac{100}{40}$ No stake set
112+59.91 P.T.	8-32.5	$\frac{100.2^A}{9.80}$ 55.54	55.52	$\frac{+6.7}{25} - 0.62$	$\frac{-14.7}{48} - 0.31$
Equation identical					
111+06.53 P.T.					
+50			52.10	$\frac{+7.3}{25} - 0.68$	$\frac{-11.7}{48} - 0.33$
112			48.10	$\frac{+8.8}{25} - 0.13$	$\frac{-9.1}{40} - 0.35$

Headers - West Side
- of Intersections -

Sta.

130
413+79.77

30

Header dopo
2' offset

$$\Delta = 54^{\circ} 53'$$

$$R = 154.50$$

$$L = 148'$$

$$\text{Curve} = 37.085$$

$$1' \text{ arc} = 0^{\circ} 11.125'$$

103+19.15
1 39.65
101+79.50 PC

135+47.83
27+50.08

7 97.75
1 35.98
9 33.73

126+30.72
21+90.44
46.28

134.60
574.88

130+57.43
17+74.06
4 83.37
1 88.92
474.79

116+38.70
108+87.58

751.12
116.05
867.18

107+82.16
4+57.01
3 45.15
1 39.65
464.80

103+19.15
100+74.15
445.00

Broadway + San Miguel Ave

336" CAMP

45' ahead P.C. + 61' N

50' across Road @ 90°

21' So to Other End Camp

Sept 25 1927