

NAME San Miguel #2

Class \_\_\_\_\_ Course \_\_\_\_\_ Party Job #257

Cross Sections.

RETURN TO  
Watson, Valle & Gough, Inc.  
508 Spruce St.  
San Diego, Cal.

1981

**338**  
**FIELD NOTES**

No. 403 P

ESPECIALLY ADAPTED  
TO THE USE OF  
ENGINEERING STUDENTS

**EUGENE DIETZGEN Co.**

MANUFACTURERS

**DRAWING MATERIALS  
MATHEMATICAL AND SURVEYING INSTRUMENTS  
MEASURING TAPES**

CHICAGO SAN FRANCISCO NEW YORK  
NEW ORLEANS PITTSBURGH

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Cross Sections - 100+74 <sup>25</sup> to 135+47 <sup>83</sup>	1-14
X-Secs of Side Draws-	16-25

MICROFILMED  
DEC 30 1964

San Miguel #2  
X Sec.

B.M.	D-O	11.85	436.30	424.45	Sta
					100+74.5
					101+00
					101+50
					P.C. 101+79.40
					102+00
					102+50
0.20	425	.17	11.33	424.97	
					102+50
					103+00
					103+50
					104+00
0.55	414.06	11.66		413.51	

130.8  
33.3  
-----  
F.V.

12.55  
28.4  
-----  
101

116.7  
18.7  
-----  
Cup

107.5

1

2x7 hub  
50 Lt Sta 101+40 - Sec Book 163 Page A

	Lt	±	RT	
				H.I. 436.3
430.5	4321	435.5	439.1	440.2
5.8 40	4.2 30	0.8	+2.8 30	+3.9 40
428.5	429.7	432.3	436.8	437.9
7.8 40	6.6 30	3.0	+0.5 30	+1.6 40
429.5	425.8	429.1	432.3	433.5
11.8 40	10.5 30	7.2	4.0 30	2.8 40
422.9	424.0	426.7	430.4	431.6
13.4 40	12.3 30	9.6	5.9 30	4.7 40
421.3	422.4	425.4	429.1	430.2
15.0 40	13.9 30	10.9	7.2 30	6.1 40
			426.0	427.2
			10.3 30	9.1 40
				H.I. = 425.2
418.2	419.2	421.5		
7.0 40	6.0 30	2.7		
413.3	414.7	418.7	421.9	422.8
11.9 40	10.5 30	6.5	3.3 30	2.4 40
408.0	409.9	415.5	417.4	419.2
17.2 40	15.3 30	9.7	7.8 20	6.0 30
			414.9	416.1
			10.3 30	9.1 40

Apr 2-1927  
Clark  
Culver  
Radier

414.06

$$\begin{array}{r} 407.7 \\ 102 \\ \hline 27.5 \end{array}$$

Sta

104+00

104+50

P.T. 104+57.0

105+00

105+50

0.58 403.32 11.32 402.74

$$\begin{array}{r} 398.8 \\ 99.7 \\ \hline 29.9 \end{array}$$

106+00

2.44 393.80 393.60 11.96 391.36

$$\begin{array}{r} 390.7 \\ 90.6 \\ \hline 20.1 \end{array}$$

106+00

106+50

P.C. 106+66.0

106+74

RT

±

LT

H.I. = 414.1

402.5 409.2 410.2

$$\begin{array}{r} 11.6 \\ 40 \\ \hline 9.9 \\ 30 \\ \hline 3.9 \end{array}$$

398.3 400.2 402.1 400.6 402.9 403.9 404.6 410.4 411.4

$$\begin{array}{r} 15.8 \\ 40 \\ \hline 13.9 \\ 30 \\ \hline 12.0 \\ 16 \\ \hline 13.5 \\ 15 \\ \hline 11.2 \\ 45 \\ \hline 10.2 \\ 4 \\ \hline 9.5 \\ \hline 3.7 \\ 30 \\ \hline 2.7 \\ 40 \end{array}$$

398.2 399.5 403.8 409.9 411.1

$$\begin{array}{r} 15.9 \\ 40 \\ \hline 14.6 \\ 30 \\ \hline 10.3 \\ \hline 4.2 \\ 30 \\ \hline 3.0 \\ 40 \end{array}$$

395.2 396.3 399.7 404.0 405.7

$$\begin{array}{r} 18.9 \\ 40 \\ \hline 17.8 \\ 30 \\ \hline 14.4 \\ \hline 10.1 \\ 30 \\ \hline 8.4 \\ 40 \end{array}$$

390.0 391.8 395.1 399.0 400.4

$$\begin{array}{r} 24.1 \\ 40 \\ \hline 22.3 \\ 30 \\ \hline 19.0 \\ \hline 15.1 \\ 30 \\ \hline 13.7 \\ 40 \end{array}$$

H.I. = 403.3

495.9 397.4

$$\begin{array}{r} 7.4 \\ 30 \\ \hline 5.9 \\ 40 \end{array}$$

H.I. = 393.8

384.7 385.7 386.5 390.6

$$\begin{array}{r} 25 \text{ Wash} \\ \hline 9.1 \\ 40 \\ \hline 8.1 \\ 30 \\ \hline 7.3 \\ 15 \\ \hline 3.2 \end{array}$$

384.2 383.0 381.0 382.6 484.3 385.4 393.1 394.3

$$\begin{array}{r} 9.6 \\ 40 \\ \hline 10.8 \\ 30 \\ \hline 12.8 \\ 25 \\ \hline 11.2 \\ 20 \\ \hline 9.5 \\ \hline 8.4 \\ 8 \\ \hline 0.7 \\ 30 \\ \hline 10.5 \\ 40 \end{array}$$

383.6 383.1 381.7 379.2 381.5 382.4 389.3 390.1 393.1

$$\begin{array}{r} 10.2 \\ 40 \\ \hline 10.7 \\ 30 \\ \hline 12.1 \\ 13 \\ \hline 14.6 \\ 11 \\ \hline 12.3 \\ 8 \\ \hline 11.4 \\ \hline 9.5 \\ 70 \\ \hline 3.7 \\ 30 \\ \hline 0.7 \\ 40 \end{array}$$

384.2 383.2 382.0 380.0 381.5 383.6 388.7 392.5

$$\begin{array}{r} 9.6 \\ 40 \\ \hline 10.6 \\ 30 \\ \hline 11.8 \\ 10 \\ \hline 13.8 \\ 5 \\ \hline 12.3 \\ \hline 10.2 \\ 78 \\ \hline 5.1 \\ 30 \\ \hline 1.3 \\ 40 \end{array}$$

393.80  
393.60

106+79

106+84

107+00

107+24

107+31

107+38

107+50

107+75

B.M. - C-1

8.17

385.63  
385.43

B.M. - C-1 0.19

385.94

385.75

107+75

108+00

382.8  
79.1  
3.7

385.75

3

H.I. = 393.8

384.3 383.0 381.7 379.6 381.6 383.0 388.0 391.5

$\frac{9.5}{40}$   $\frac{10.8}{30}$   $\frac{12.1}{4}$   $\frac{14.0}{7}$   $\frac{12.2}{18}$   $\frac{10.8}{30}$   $\frac{5.8}{40}$   $\frac{2.3}{40}$

384.6 383.2 382.8 381.7 379.7 381.1 383.1 387.9 391.3

$\frac{9.2}{40}$   $\frac{10.6}{35}$   $\frac{11.0}{30}$   $\frac{12.1}{7}$   $\frac{14.1}{10}$   $\frac{12.7}{20}$   $\frac{10.7}{30}$   $\frac{5.9}{40}$   $\frac{2.5}{40}$

383.1 382.2 381.4 381.2 379.7 381.7 388.3 390.8

$\frac{10.7}{40}$   $\frac{11.6}{30}$   $\frac{12.4}{7}$   $\frac{12.6}{12}$   $\frac{14.1}{17}$   $\frac{12.1}{30}$   $\frac{5.5}{40}$   $\frac{3.0}{40}$

382.0 380.9 380.1 380.2 380.3 378.5 379.1 385.2 386.5 389.2

$\frac{11.8}{40}$   $\frac{12.9}{30}$   $\frac{13.7}{20}$   $\frac{13.6}{7}$   $\frac{13.5}{10}$   $\frac{15.3}{12}$   $\frac{14.7}{22}$   $\frac{8.6}{30}$   $\frac{7.3}{40}$   $\frac{5.6}{40}$

381.0 379.8 379.1 378.2 378.5 385.1 386.5 388.2

$\frac{12.8}{40}$   $\frac{14.0}{30}$   $\frac{14.7}{20}$   $\frac{15.6}{19}$   $\frac{15.3}{20}$   $\frac{8.7}{30}$   $\frac{7.3}{40}$   $\frac{5.6}{40}$

380.7 379.3 377.8 380.0 382.7 385.8 387.7

$\frac{13.1}{40}$   $\frac{14.5}{30}$   $\frac{16.0}{20}$   $\frac{13.8}{12}$   $\frac{11.1}{30}$   $\frac{8.0}{40}$   $\frac{6.1}{40}$

379.3 377.1 378.3 379.3 380.4 382.2 384.9 386.5

$\frac{14.5}{45}$   $\frac{16.7}{40}$   $\frac{15.5}{37}$   $\frac{14.5}{30}$   $\frac{13.4}{12}$   $\frac{11.6}{30}$   $\frac{8.9}{40}$   $\frac{7.3}{40}$

380.9 383.8 384.6

$\frac{12.9}{30}$   $\frac{10.0}{40}$   $\frac{9.2}{40}$

On 2x2 hub 70' RT Sta 109+00 Elev. = 385.75  
See 163 - Page 4

H.I. = 385.9

381.6 378.9 376.8 377.5 379.1

$\frac{4.3}{52}$   $\frac{10.0}{37}$   $\frac{9.1}{30}$   $\frac{8.4}{27}$   $\frac{6.8}{10}$

381.4 378.0 377.0 375.2 376.9 378.1 383.1 389.0

$\frac{4.5}{40}$   $\frac{7.9}{30}$   $\frac{8.9}{23}$   $\frac{10.7}{16}$   $\frac{9.0}{17}$   $\frac{6.8}{30}$   $\frac{2.8}{40}$   $\frac{1.9}{40}$

B

B

385.94

108+50

P.T. 108+87.58

109+00

109+45

110+00

110+39

6.45  $\frac{380.69}{370.69}$  11.70 374.24

P.O.T. 110+74.65

110+89

111+00

111+33

111+42

H. 385.9

383.0 380.0 375.7 374.3 380.2 381.4  
 $\frac{2.9}{40}$   $\frac{5.9}{30}$   $\frac{10.2}{7}$  11.6  $\frac{5.7}{30}$   $\frac{4.5}{40}$

382.6 374.3 374.5 373.6 373.0 374.5 374.7 381.2  
 $\frac{3.3}{40}$   $\frac{6.6}{30}$   $\frac{4.4}{7}$  12.3  $\frac{12.9}{3}$   $\frac{4.4}{7}$   $\frac{6.2}{30}$   $\frac{4.7}{40}$

383.1 380.0 376.2 374.3 373.4 373.0 374.7 374.3 380.7  
 $\frac{2.8}{40}$   $\frac{5.9}{30}$   $\frac{9.7}{18}$   $\frac{4.4}{2}$  12.5  $\frac{12.9}{8}$   $\frac{4.0}{8}$   $\frac{6.6}{30}$   $\frac{5.2}{40}$

381.2 380.0 379.5 373.6 371.1 372.5 373.8 377.2 380.1  
 $\frac{4.7}{40}$   $\frac{5.2}{30}$   $\frac{6.4}{25}$   $\frac{12.3}{2}$   $\frac{14.8}{2}$  13.4  $\frac{12.1}{4}$   $\frac{8.7}{30}$   $\frac{5.8}{40}$

378.8 377.5 372.4 370.3 372.3 374.9 376.1  
 $\frac{7.1}{40}$   $\frac{8.4}{30}$  13.5  $\frac{15.6}{3}$   $\frac{13.6}{9}$   $\frac{11.0}{30}$   $\frac{9.8}{40}$

372.4 375.9 374.7 372.0 370.0 372.1 372.4 374.2  
 $\frac{8.5}{40}$   $\frac{10.0}{30}$  11.2 13.9 15.4  $\frac{13.8}{20}$   $\frac{13.5}{30}$   $\frac{11.7}{40}$

H. = 380.7

476.2 375.6 373.7 373.1 371.0 370.7 369.6 371.3  
 $\frac{4.4}{40}$   $\frac{5.1}{30}$   $\frac{7.0}{15}$  7.6  $\frac{9.7}{30}$   $\frac{10.0}{35}$   $\frac{11.1}{37}$   $\frac{9.4}{41}$

378.6 378.1 373.5 372.6 371.5 369.5  
 $\frac{2.1}{40}$   $\frac{2.6}{30}$   $\frac{7.2}{10}$  8.1  $\frac{9.2}{30}$   $\frac{11.2}{40}$

378.4 377.9 374.0 371.9 371.1 370.2 369.0  
 $\frac{2.3}{40}$   $\frac{2.8}{30}$   $\frac{6.7}{16}$  8.8  $\frac{9.6}{30}$   $\frac{10.5}{39}$   $\frac{11.7}{40}$

377.5 375.6 370.6 368.1 368.6 367.3 367.7 368.5 370.1  
 $\frac{3.7}{40}$   $\frac{5.1}{30}$   $\frac{10.1}{15}$  12.6 12.1  $\frac{13.4}{20}$   $\frac{13.0}{30}$   $\frac{12.2}{40}$   $\frac{10.6}{41}$

377.0 374.8 370.6 367.9 366.5 368.5 368.8 370.1  
 $\frac{3.7}{40}$   $\frac{5.9}{30}$   $\frac{10.1}{20}$   $\frac{12.8}{6}$  14.2 12.2  $\frac{11.9}{30}$   $\frac{10.6}{40}$

$\frac{381.3}{336}$   
 $\frac{7.7}{7.7}$   
 ~~$\frac{380.2}{374.4}$~~   
 $\frac{6.5}{6.5}$

$\frac{377.9}{7.2}$   
 $\frac{6.5}{6.5}$

$\frac{374.9}{7.0}$   
 $\frac{4.8}{4.8}$

B

K

380.69  
370.69

111+61

111+85

112+00

112+13

112+35

112+50

113+00

Temp. B.M 0.66

372.96

367.96

8.39

372.30

367.30

568.9  
660  
F 4.9

365.7  
637  
F 2.1

5

H.I. = 380.7

374.7 369.1 367.3 366.4 367.5 369.2 371.7 373.4  
6.0 11.6 13.4 14.2 13.2 11.5 9.0 7.3  
40 30 23 18 14 30 40  
± Wash

371.0 376.1 365.9 366.8 367.0 368.0 373.5 375.2  
3.7 4.6 14.8 13.9 13.7 12.7 7.2 5.5  
50 44 30 26 8 30 40  
± Wash

376.8 373.6 366.0 366.2 367.2 372.7 374.9  
3.9 7.1 14.7 14.5 13.5 8.0 5.8  
50 38 30 5 30 40  
± Wash

374.3 371.2 368.4 366.5 365.3 365.5 369.7 372.1 374.1  
6.4 9.5 12.3 15.2 15.4 15.2 11.0 8.6 6.6  
40 30 18 15 11 18 30 40  
± Wash

372.2 370.4 369.7 366.0 365.8 365.2 364.1 371.4 374.9  
8.5 10.3 11.0 14.7 14.9 15.5 16.6 9.3 5.8  
40 30 20 10 16 20 30 40  
± Wash

370.8 369.5 366.4 365.6 364.9 363.0 367.0 370.3 374.2  
9.9 11.2 14.3 15.1 15.8 17.7 13.7 10.4 6.5  
40 30 12 7 7 20 30 40  
± Wash

368.7 367.6 364.0 361.9 363.8 372.3 375.2  
12.0 13.1 16.7 18.8 16.9 8.4 5.5  
40 30 17 30 40  
± Wash

On quinea 30' Rt Sta 113+00

H.I. = 373.0

366.4 365.2 362.3 361.8 360.4 361.8 370.4 373.3  
6.6 7.8 10.7 11.2 12.6 11.2 2.6 10.3  
40 30 7 4 7 30 40  
± Wash

364.5 363.3 361.6 360.4 361.9 366.2 369.1 371.1  
8.5 9.7 11.4 12.6 11.1 6.8 3.9 1.9  
40 30 4 7 12 30 40  
± Wash

363.5 362.0 361.4 360.7 360.3 362.5 363.7 367.2 368.9  
9.5 11.0 11.6 12.3 12.7 10.5 5.8 4.6  
40 30 13 13 7 30 40  
± Wash

114+00

(K)

372.96  
362.96

114+50

114+68

114+77

114 362.33 11.77 RC. 114+9928  
~~357.33~~ 361.19  
 351.19

$$\begin{array}{r} 362.8 \\ 6.1 \\ \hline F. 2.1 \end{array}$$

115+50

116+00

116+50

116+78

117+00

117+50

P.T. 117+74<sup>el</sup>

$$\begin{array}{r} 359.8 \\ 19.4 \\ \hline F. 7.4 \end{array}$$

H.I. = 373.0

$$\begin{array}{cccccccc} 359.7 & 360.6 & 359.6 & 359.6 & 362.7 & 363.6 & 363.1 & \\ \frac{13.3}{40} & \frac{12.4}{30} & 14.4 & \frac{13.4}{20} & \frac{10.3}{23} & \frac{9.4}{30} & \frac{7.9}{40} & \\ \text{Wash} & & & & & & & \end{array}$$

$$\begin{array}{cccccccc} 359.5 & 359.2 & 359.1 & 362.9 & 359.7 & 357.0 & 359.8 & 364.0 \\ \frac{13.5}{40} & \frac{13.8}{30} & \frac{13.9}{76} & \frac{10.1}{75} & 13.3 & \frac{16.0}{25} & \frac{14.2}{30} & \frac{9.0}{40} \\ \text{Wash} & & & & & \text{Wash} & & \end{array}$$

$$\begin{array}{cccccccc} 365.8 & 364.6 & 360.0 & 367.9 & 367.3 & 361.7 & & \\ \frac{7.2}{40} & \frac{8.4}{30} & 13.0 & \frac{15.6}{28} & \frac{15.7}{30} & \frac{11.3}{40} & & \\ \text{Wash} & & & \text{Wash} & & & & \end{array}$$

$$\begin{array}{cccccccc} 365.1 & 363.6 & 360.1 & 367.9 & 357.3 & 355.2 & 355.2 & \\ \frac{7.9}{40} & \frac{9.4}{30} & 12.9 & \frac{15.1}{30} & \frac{15.7}{35} & \frac{17.8}{35} & \frac{17.8}{40} & \\ \text{Wash} & & & & & & \text{Wash} & \end{array}$$

H.I. = 362.3

$$\begin{array}{cccccccc} 364.0 & 361.5 & 358.8 & 356.5 & 355.4 & 353.6 & 354.1 & \\ +1.7 & 0.8 & & 5.8 & 6.9 & 8.7 & 8.2 & \\ \frac{40}{40} & \frac{30}{30} & 3.5 & \frac{50}{50} & \frac{36}{36} & \frac{37}{37} & \frac{40}{40} & \end{array}$$

$$\begin{array}{cccccccc} 360.1 & 358.5 & 356.3 & 355.9 & 354.3 & 353.1 & 357.9 & \\ \frac{2.2}{40} & \frac{3.8}{30} & 6.0 & \frac{6.4}{17} & \frac{8.0}{30} & \frac{9.2}{40} & \frac{10.4}{42} & \\ \text{Wash} & & & & & & \text{Wash} & \end{array}$$

$$\begin{array}{cccccccc} 360.8 & 358.3 & 354.9 & 353.9 & 351.6 & 360.6 & 355.7 & 357.0 \\ \frac{1.5}{40} & \frac{4.0}{30} & 7.4 & \frac{8.4}{9} & \frac{10.7}{17} & \frac{11.7}{20} & \frac{6.6}{30} & \frac{5.0}{40} \\ \text{Wash} & & & & & \text{Wash} & & \end{array}$$

$$\begin{array}{cccccccc} 363.2 & 359.7 & 358.0 & 353.9 & 351.1 & 350.1 & 352.4 & 355.7 & 357.4 \\ +0.7 & \frac{2.6}{30} & \frac{4.3}{26} & 8.9 & \frac{11.2}{7} & \frac{12.2}{4} & \frac{9.9}{15} & \frac{6.6}{30} & \frac{4.9}{40} \\ \text{Wash} & & & & & & & & \end{array}$$

$$\begin{array}{cccccccc} 362.1 & 358.7 & 354.6 & 349.4 & 351.2 & 353.5 & 357.9 & \\ 0.2 & 3.6 & 7.7 & 12.9 & \frac{11.1}{7} & \frac{6.8}{30} & \frac{4.4}{40} & \\ \frac{40}{40} & \frac{30}{30} & \frac{4}{4} & \text{Wash} & & & & \end{array}$$

$$\begin{array}{cccccccc} 362.0 & 358.3 & 355.1 & 352.0 & 347.6 & 350.4 & 353.6 & 356.0 \\ 0.3 & \frac{4.0}{30} & \frac{7.2}{24} & 10.3 & \frac{14.7}{7} & \frac{11.9}{15} & \frac{8.7}{30} & \frac{6.3}{40} \\ \frac{40}{40} & & & & & & & \\ \text{Wash} & & & & & & & \end{array}$$

$$\begin{array}{cccccccc} 362.0 & 358.5 & 352.5 & 351.4 & 350.9 & 347.2 & 347.5 & 350.2 & 352.9 & 354.8 \\ 0.5 & 3.8 & 9.8 & 10.9 & 11.4 & \frac{13.1}{6} & \frac{14.8}{13} & \frac{12.1}{17} & \frac{7.4}{30} & \frac{7.5}{40} \\ \frac{40}{40} & \frac{30}{30} & \frac{19}{19} & & \frac{5}{5} & & & & & \\ \text{Wash} & & & & & & \text{Wash} & & & \end{array}$$

R

R



362.33  
352.33

352.8  
50.3  
+ 3.1

118+00

118+50

B.M. #1 (Established)

352.54  
1.48 347.54

6.25  
11.27  
350.7  
46.9  
F 3.8

356.08  
346.08  
351.06  
341.06

119+00

119+50

347.7  
43.0  
F 4.1

120+00

120+15

120+27

120+37

H.I. = 362.3

358.9 355.2 352.1 350.3 349.2 347.1 351.7 343.9 353.8  
3.4 7.1 10.2 12.0 13.0 15.2 10.6 8.9 6.5  
40 30 25 12.0 12 17 24 30 40  
2 Wash

352.9 350.3 348.7 347.6 345.8 348.10 351.0 352.3 355.7  
9.1 12.0 13.6 14.7 16.5 14.3 11.3 10.0 7.2  
40 30 13.6 6 17 22 30 40  
2 Wash

1X2 50' RT Sta 119+00

H.I. = 352.5

352.4 351.3 348.1 346.5 345.0 346.3 346.9 347.7 348.4 352.2  
0.1 1.7 4.4 6.0 7.5 6.2 4.8 4.1 0.2  
40 30 20 11 7 5.6 3 30 40  
2 Wash

351.1 349.2 347.4 346.5 344.7 345.8 345.6 345.9 347.7  
1.4 3.3 5.1 8.0 7.8 6.7 6.9 6.6 4.8  
40 30 20 19 12 6.7 30 37 40  
2 Wash

350.1 348.1 346.3 344.4 343.6 342.7 345.8 347.0 348.2  
2.4 4.4 6.2 9.1 8.9 9.8 6.7 5.5 4.3  
40 30 25 16 8.9 14 15 30 40  
2 Wash

353.2 347.5 349.3 348.4 346.8 342.6 343.1 342.4 345.6 346.2 347.8  
10.7 5.0 3.2 4.1 5.7 9.9 10.1 6.9 6.3 4.7  
40 30 20 40 30 22 9.4 17 19 30 40  
2 Wash from Lt  
2 Wash

351.6 356.5 358.0

0.9 + 4.0 + 5.5  
110 150 177

2 Wash from left - Approx 1000' to top ridge  
Drainage Area = 800± Wide

345.8 344.3 343.1 342.1 341.6 341.8 342.0 344.4 344.8 346.0  
6.7 8.2 9.1 10.4 9.9 10.7 10.5 8.1 7.7 6.5  
40 40 30 33 30 4 17 18 30 40  
2 Wash from Lt 2 Wash

350.0 349.0 342.2 341.9 341.5 342.5 342.0 344.3 346.5 347.1  
2.5 3.5 5.3 10.3 9.6 11.0 10.5 8.2 7.0 5.4  
40 33 30 26 14 8 12 13 30 40  
2 Wash

352.54  
342.54

120+41

120+70

121+00

121+38

121+75

P.T. 121+90.4

122+50

	363.51		352.05
11.46	353.51	0.49	342.05
	371.45		361.89
9.56	361.45	1.62	351.89
			370.54
B.M.-B-3		0.91	360.54

B.M.-B-3	0.91	371.50	370.59
	0.57	359.98	12.09
	0.95	349.37	11.56
B.M.#2 (Established)		11.69	337.68

H.I. = 352.5

350.5      345.2      342.6  
 349.1      341.6      341.2      341.6      342.2      343.5      345.4      346.8  
 2.0      3.4      7.3      10.9      9.9      11.3      10.9      10.3      9.0      7.1      5.7  
 40      35      30      28      19      17      10.9      4      5      30      40

351.0      347.3      342.5      339.8      341.9      342.4      344.3      345.6  
 1.5      5.2      10.0      12.7      10.6      10.1      8.2      6.9  
 50      38      30      25      20      10.1      30      40

346.2      343.9      339.3      340.3      341.3      343.0      344.7  
 6.3      8.6      13.2      12.2  
 40      30      23      16      11.2      9.5      7.8  
 40

341.5      341.5      339.4      338.2      340.3      341.7      347.4      350.3  
 11.0      11.0      13.1      14.3      12.7      10.8      5.1      2.2  
 40      30      10      10      5      18      30      40

339.9      339.6      338.3      337.8      337.5      338.7      341.4      345.5      348.9  
 12.6      12.9      14.2      14.7      15.0      13.8      11.1      7.0      3.6  
 40      30      8      14.7      8      8      23      30      40

339.3      339.3      337.1      336.8      340.7      346.2      349.7  
 13.2      13.2      15.4      15.7      11.8      6.3      2.8  
 40      30      2      20      30      40

337.6      337.3      336.7      335.3      337.0      338.1      340.8      345.5      348.4  
 14.9      15.2      15.8      17.2  
 40      30      15      10      15.5      14.4      11.7      7.0      4.1  
 40

2x2 - 125' Rt Sta 120+00 Elev 370.59  
 See book 163 - Page 3

1x2 - 60' Rt Sta 124+08

(B)

(E)

Lt.

Rt.

9

337.68 EM 2

60 Rt 124108.

335 341.03

128400

338.7  
36.0  
F v.7

341.0  
336.1 335.9 335.1 336.0 338.5 339.6 343.0  
48 51 52 50 25 19 23  
40 30 15 50 25 30 40

337.4 338.8 334.3 334.1 335.3  
58 73 62 62 52  
40 30 30 40

338.9 337.0 335.1 331.7 333.3 333.1 332.5 333.2  
21 42 52 93 71 79 85 78  
40 30 23 20 10 30 40

12400

B/W #54

336.7  
33.1  
F v.6

337.68

153 334.41

124424

+20  
40

340.3 337.1 334.4 332.9 331.8 331.8 332.7 331.8 333.5  
+11 15 48 63 74 74 65 74 57  
36 3 23 10 6 2 4 30 40

+30

342.0 339.2 337.6 334.9 332.8 332.5 331.7 331.3 331.3 332.0 332.0 331.9 333.5  
+38 0.0 17 43 64 67 75 19 19 72 72 73 57  
40 30 26 23 15 5 3 3 4 14 30 40

+36

342.4 339.6 337.7 334.3 332.4 332.2 331.3 330.8 331.9 331.7 332.0 333.0  
+32 104 15 49 68 70 79 84 73 75 72 62  
40 30 25 20 14 70 2 5 6 20 30 40

+73

342.4 338.4 335.7 333.2 329.6 330.4 330.6 330.8 329.1 331.1 332.6  
+32 0.8 35 60 96 88 86 84 95 81 66  
40 30 20 18 14 10 80 30 30 40 44

R

R

1249474  
PC

339.21

332.8  
29.0  
F 3.8

125109

+22

6.48 335.68 10.01 329.20

+50

126

329.5  
26.9  
-2.7

+50

+78

127

5.05 328.68

326.5  
21.1  
-2.5  
12.05 323.63

(8)

Lt.

Rt.

343.7 335.9 333.7 332.1 329.9 329.0 329.6 330.1 329.1 328.4 327.8 329.8 321.1  
145 33 55 71 93 102 96 91 95 101 94 94 81  
40 30 25 16 9 2 7 13 24 30 35 40

336.8 333.1 328.8 328.4 328.1 328.5 330.1 332.0  
24 61 104 108 111 107 91 72  
40 30 11 4 30 40

335.8 332.4 329.0 327.5 327.2 327.1 329.0 329.0 331.0 331.8  
34 68 102 117 120 115 102 102 82 74  
40 30 25 15 9 4 4 30 40

332.6 330.6 325.5 326.7 328.0 327.5 328.5 329.0 330.5 332.4  
31 51 102 90 77 82 72 67 52 33  
40 33 30 22 23 12 18 30 40

327.3 327.3 325.9 326.0 325.0 325.1 326.4 26.9 328.2 331.4 334.3  
84 84 98 97 107 106 93 88 75 43 14  
40 30 25 16 15 9 8 20 30 40

325.6 324.6 325.1 324.9 323.4 323.3 323.9 324.7 27.4 326.8 329.3 331.2  
161 11 100 108 123 124 118 110 103 89 64 45  
40 26 30 11 10 6 3 2 15 30 40

326.0 324.8 324.3 324.4 322.4 323.2 324.8 324.6 325.3 327.4 329.1  
97 109 114 113 133 125 109 11 104 83 60  
40 30 24 14 11 6 5 20 30 40

326.4 324.8 323.7 321.4 321.7 323.8 324.1 323.6 324.6 327.1  
93 109 120 143 140 119 116 121 111 86  
40 30 20 18 15 12 18 30 40

(8)

328.68

127+14

+21

+5008  
P.T.

128

$\frac{3236}{21.1}$   
2.5

+50

129

2.81 320.10 11.39 317.29

$\frac{3206}{17.2}$   
184

+40

130

$\frac{3175}{146}$   
2.2

+

⊕

Lt.

Rt.

11

$\frac{3252}{38}$   $\frac{3243}{44}$   $\frac{3231}{56}$   $\frac{3216}{71}$   $\frac{3223}{64}$   $\frac{3235}{52}$   $\frac{3231}{56}$   $\frac{3237}{50}$   $\frac{3251}{36}$   
40 30 15 13 2 14 30

$\frac{3252}{38}$   $\frac{3243}{44}$   $\frac{3236}{51}$   $\frac{3224}{63}$   $\frac{3215}{72}$   $\frac{3216}{71}$   $\frac{3217}{70}$   $\frac{3229}{58}$   
40 30 21 12 15 30 40

$\frac{3253}{34}$   $\frac{3243}{44}$   $\frac{3228}{59}$   $\frac{3230}{57}$   $\frac{3225}{62}$   $\frac{3209}{78}$   $\frac{3204}{83}$   
40 30 12 30 34 40

$\frac{3226}{61}$   $\frac{3222}{65}$   $\frac{3219}{68}$   $\frac{3211}{76}$   $\frac{3215}{72}$   $\frac{3210}{77}$   $\frac{3209}{78}$   
40 30 15 17 30 40

$\frac{3217}{70}$   $\frac{3214}{73}$   $\frac{3195}{92}$   $\frac{3195}{92}$   $\frac{3200}{87}$   $\frac{3190}{97}$   $\frac{3192}{95}$   
40 30 22 11 30 40

$\frac{3197}{90}$   $\frac{3184}{103}$   $\frac{3172}{115}$   $\frac{3170}{117}$   $\frac{3170}{117}$   $\frac{3171}{110}$   $\frac{3190}{97}$   
40 30 13 22 30 40

$\frac{3145}{56}$   $\frac{3153}{48}$   $\frac{3157}{44}$   $\frac{3158}{43}$   $\frac{3165}{36}$   $\frac{3167}{33}$   $\frac{3185}{16}$   $\frac{3205}{104}$   $\frac{3246}{45}$   
40 30 22 2 17 26 30 40

$\frac{3151}{50}$   $\frac{3151}{50}$   $\frac{3146}{55}$   $\frac{3142}{59}$   $\frac{3155}{46}$   $\frac{3176}{25}$   $\frac{3229}{25}$   
40 30 14 25 30 40

⊕

320.10

130+50

131

314.5  
11.1  
---  
3.2

+38

+65

5.76 314.20

11.66 308.44

+90

132

311.5  
.061  
---  
5.4

+35

Lt.

Rt.

12

313.3 313.4 312.6 312.6 312.7 313.7 318.6 324.6  
6.8 6.7 7.5 7.5 7.4 6.4 1.5 +4.5  
40 30 23 23 14 21 30 40

311.9 311.7 311.0 311.1 311.3 313.1 316.4 321.0  
8.7 8.4 9.1 9.0 8.8 7.0 3.7 +0.9  
40 30 14 13 21 30 40

308.8 308.7 308.2 309.5 309.6 313.0 316.4 320.6  
11.3 11.4 11.9 10.6 10.5 7.1 3.7 +0.5  
40 30 3 1 21 30 40

309.6 309.1 309.0 308.8 309.0 308.3 306.9 307.5 313.2 315.4 320.1  
10.5 11.0 11.1 11.3 11.1 11.5 13.2 12.5 6.9 4.7 0.0  
40 30 25 7 5 14 22 25 30 40

309.4 308.6 307.5 308.1 308.2 307.1 306.6 307.2 311.6 215.0 318.6  
4.8 5.6 6.7 6.1 6.0 7.1 7.6 7.0 2.6 +0.8 +4.4  
40 30 26 23 2 10 19 22 30 40

309.0 308.8 307.0 307.7 307.8 306.5 306.1 306.7 309.6 311.5 314.4 318.3  
5.7 5.4 7.2 6.5 6.4 7.7 8.1 7.5 4.6 2.7 +0.2 +3.9  
40 30 27 19 4 3 16 18 23 30 40

307.0 306.6 305.0 305.0 305.7 305.2 306.6 306.9 307.2 309.1 312.2 313.8 317.7  
17.76 9.7 9.7 8.5 9.0 7.6 7.3 7.0 5.1 2.0 0.4 +3.5  
40 24 24 16 9 6 11 20 27 30 40

R

R

314.20

132+50

133

307.4  
5.5  
F 1.9

+50

+63

+86

10.46 303.74

134

5.73 309.47

302.3  
2.1  
@ 0.5

+50

Lt.

Rt.

13

$\frac{306.2}{80}$	$\frac{304.7}{95}$	$\frac{304.2}{100}$	$\frac{304.7}{97}$	$\frac{305.2}{90}$	$\frac{306.1}{81}$	$\frac{306.9}{73}$	$\frac{306.4}{78}$	$\frac{307.3}{69}$	$\frac{309.3}{49}$	$\frac{312.1}{2.1}$	$\frac{317.0}{2.8}$
40	38	37	30	27	14	7	7	13	24	30	40

$\frac{303.5}{10.7}$	$\frac{304.5}{9.7}$	$\frac{304.5}{9.7}$	$\frac{305.5}{8.7}$	$\frac{306.3}{7.9}$	$\frac{308.1}{6.1}$	$\frac{311.6}{2.6}$
40	30	19	16	30	40	

$\frac{303.5}{10.7}$	$\frac{303.4}{10.8}$	$\frac{303.5}{10.7}$	$\frac{302.2}{12.0}$	$\frac{301.3}{12.9}$	$\frac{301.7}{12.5}$	$\frac{303.5}{10.7}$	$\frac{303.5}{10.7}$	$\frac{306.5}{7.7}$	$\frac{308.6}{5.6}$
40	30	27	26	11	3	15	30	40	

$\frac{303.3}{10.9}$	$\frac{302.8}{11.4}$	$\frac{302.9}{11.3}$	$\frac{300.6}{13.6}$	$\frac{300.8}{13.4}$	$\frac{302.1}{11.5}$	$\frac{305.1}{8.5}$	$\frac{307.9}{6.3}$
40	30	10	16	20	30	40	

$\frac{304.0}{10.7}$	$\frac{303.3}{10.9}$	$\frac{303.6}{10.6}$	$\frac{302.5}{11.7}$	$\frac{301.6}{12.6}$	$\frac{300.5}{13.7}$	$\frac{303.3}{10.9}$	$\frac{305.3}{8.9}$	$\frac{306.9}{7.3}$
40	30	20	17	6	26	30	32	40

$\frac{303.5}{6.0}$	$\frac{303.1}{6.4}$	$\frac{302.8}{6.7}$	$\frac{302.3}{7.7}$	$\frac{301.2}{8.3}$	$\frac{300.3}{9.2}$	$\frac{299.9}{9.6}$	$\frac{302.3}{7.2}$	$\frac{304.8}{4.7}$	$\frac{306.5}{3.0}$
40	30	6	18	20	27	30	35	40	

$\frac{302.0}{1.5}$	$\frac{301.8}{1.7}$	$\frac{301.8}{1.7}$	$\frac{301.5}{8.0}$	$\frac{301.2}{8.3}$	$\frac{299.9}{9.6}$	$\frac{299.7}{10.3}$	$\frac{299.2}{8.7}$	$\frac{300.8}{5.4}$	$\frac{307.1}{2.5}$	$\frac{307.0}{2.5}$	$\frac{306.7}{2.8}$
40	20	24	8	15	22	30	31	40	60	80	

(B)

(R)

309.17

135

3000  
2969  
F 11

+18

135+4783=  
104+77

9.30 300.17

1.22 308.45

11.70 319.95

0.39 319.56

11.08 330.64

1.20 329.44

10.09 339.53

BW

2.60 336.93 337.00

R

301.8 303.5 302.3 300.8 300.0 299.6 297.9 297.9 297.4 299.4 297.8 300.15  
 0.7 5.7 7.2 8.7 9.5 9.9 10.1 11.6 12.1 10.1 9.7 9.32  
 60 50 46 40 30 5 3 14 21 30 40

305.7

Sum  
Stop  
20

3.6  
68

303.2 300.0 299.1 297.8 297.8 296.8 297.7 301.11 300.1 300.3 300.3  
 6.3 9.5 10.4 0.7 11.7 12.7 11.8 8.36 9.35 9.24 9.33  
 55 40 30 10 9 2 \* H. Wall Pavement Pavement Pavement Pavement

\* Pavement

H. Wall  
Pavement

2x2 Hub in E.P. Ford Tr. Rectangle -

R

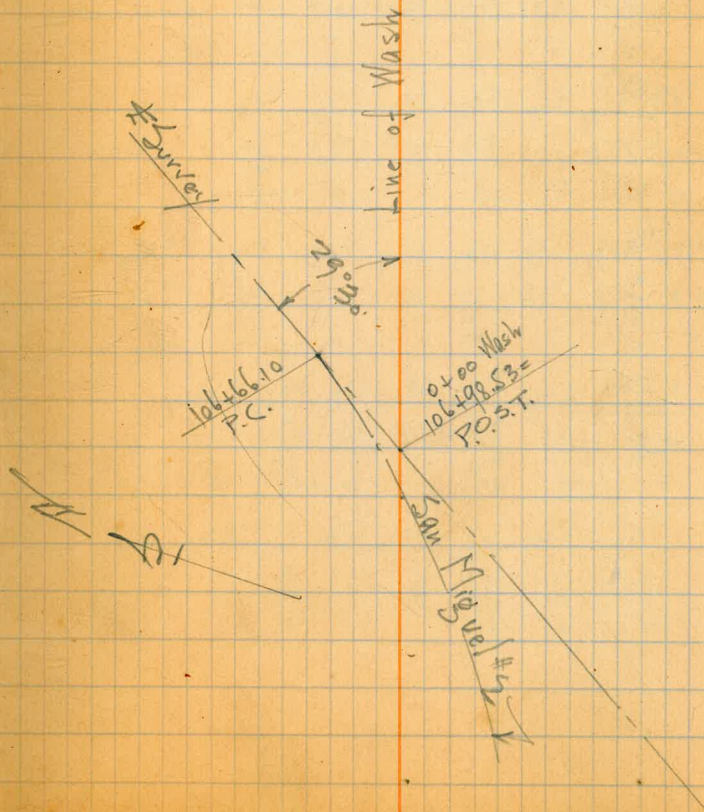




## DRAW #1

Alignment up main Wash  
from intersection with  $\pm$  of  
San Miguel #2

X-Sec. on Pg. 17



# DRAW #1

BW

112 392.6

381.4

100 382.6 382.4

0+00

+16

Alignment on Pg. 16

≠ Wash

+50

2

≠ Wash

+50

\* Sta 107 See Pg. 3

± 106 + 66

Lt.

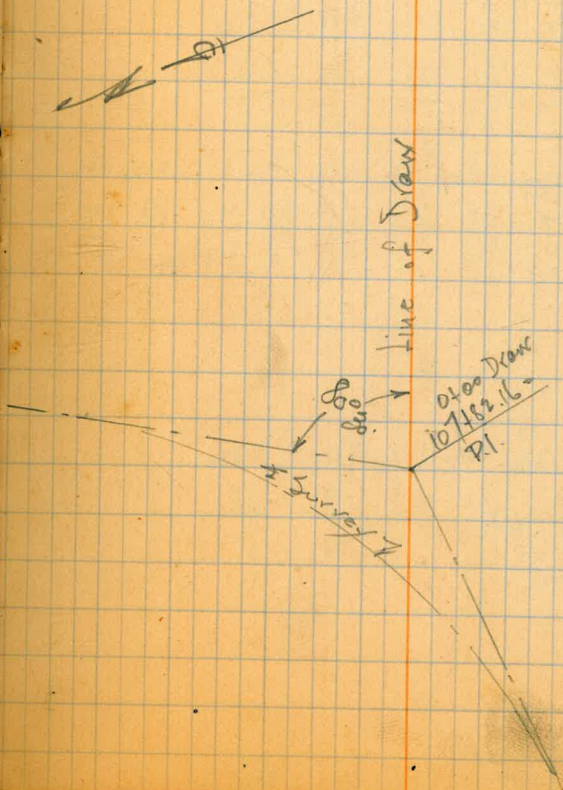
Rt.

	385.5	382.7	381.6	379.8	381.6	381.6	381.5	381.5	382.4
	$\frac{7.1}{30}$	$\frac{9.9}{22}$	$\frac{11.0}{16}$	$\frac{12.8}{11}$	$\frac{11.0}{8}$	$\frac{11.0}{11}$	$\frac{11.1}{12}$	$\frac{11.1}{23}$	$\frac{10.2}{30}$
	385.1	383.1	382.8	381.0	382.7	383.6	385.0		
9.0 = H. Water 0+16	$\frac{7.5}{30}$	$\frac{9.5}{12}$	$\frac{9.8}{6}$	$\frac{11.6}{11}$	$\frac{9.9}{2}$	$\frac{9.0}{21}$	$\frac{7.6}{3}$		
	387.0	385.7	384.4	383.7	381.0	382.8	386.4		
	$\frac{5.7}{30}$	$\frac{6.9}{15}$	$\frac{8.2}{8}$	$\frac{8.9}{8}$	$\frac{10.8}{13}$	$\frac{9.8}{16}$	$\frac{6.2}{30}$		
	389.9	387.7	386.9	385.6	384.8	383.1	384.4	385.5	
	$\frac{2.7}{30}$	$\frac{3.9}{22}$	$\frac{5.7}{6}$	$\frac{7.0}{9}$	$\frac{7.5}{9}$	$\frac{9.5}{15}$	$\frac{8.2}{18}$	$\frac{4.1}{30}$	
	391.6	387.4	386.1	384.3	385.7	389.6	390.2		
	$\frac{1.0}{30}$	$\frac{5.2}{13}$	$\frac{6.5}{4}$	$\frac{8.3}{8}$	$\frac{6.9}{2}$	$\frac{3.0}{15}$	$\frac{2.4}{30}$		
	387.9	386.7	387.3	388.0	389.8	390.9	392.5		
	$\frac{4.7}{30}$	$\frac{5.9}{27}$	$\frac{5.3}{22}$	$\frac{4.6}{16}$	$\frac{2.5}{16}$	$\frac{1.7}{26}$	$\frac{0.1}{30}$		

DRAW # 2

Alignment up side Draw -

X-Sec. on Pg. 19



DRAW #2

3<sup>th</sup>

7.8 390.0

382.2 \* Sta 107+50

11.0 379.0 379.1 \* Sta 108

0

+43

Across Mouth of Draw

11.7 =  
High Water @ Sta 107+50

381.3	378.5	376.7	379.5	382.9	386.0
$\frac{8.7}{2}$	$\frac{11.5}{3}$	$\frac{13.3}{4}$	$\frac{10.5}{5}$	$\frac{7.1}{11}$	$\frac{4.0}{23}$

8.8 =  
High Water @ Sta 108

387.2	383.6	381.0	379.7	382.4	384.6
$\frac{2.8}{27}$	$\frac{6.4}{10}$	$\frac{9.0}{5}$	$\frac{10.3}{8}$	$\frac{7.6}{2}$	$\frac{3.4}{21}$

+38

Alignment out to 18

389.3	385.2	381.9	383.1	383.2	384.4	385.2	388.6
$\frac{0.7}{38}$	$\frac{4.8}{30}$	$\frac{8.2}{27}$	$\frac{6.9}{22}$	$\frac{6.8}{10}$	$\frac{5.6}{9}$	$\frac{4.8}{9}$	$\frac{1.4}{21}$

+58

387.0
$\frac{3.0}{30}$

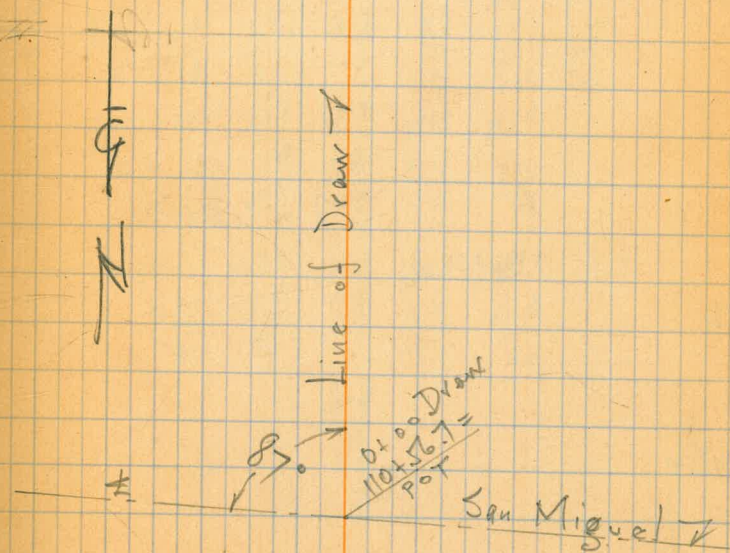
+84

388.4	385.4	383.1	386.4	388.2	389.6
$\frac{1.6}{20}$	$\frac{4.6}{2}$	$\frac{6.9}{7}$	$\frac{3.6}{7}$	$\frac{1.8}{13}$	$\frac{0.4}{25}$

DRAW # 3

Alignment up side draw.

X-Sections on Pg. 21



DRAW # 3

B.W

116 384.7

373.1  $\neq$  110+74

129 371.8 371.9  $\neq$  111+00

Lt. R

0

From this draw  
 $\frac{10.7}{HW \frac{61}{0.25}}$

+50

R.S.  
 H.W. 61  
 0.25

	373.6	374.6	373.5	373.3	372.8	
	$\frac{111}{30}$	$\frac{10.1}{15}$	$\frac{112}{13}$	$\frac{114}{13}$	$\frac{119}{30}$	
	391.0	377.5	377.4	374.9	375.9	377.2
	$\frac{3.7}{30}$	$\frac{5.2}{14}$	$\frac{7.3}{6}$	$\frac{9.8}{3}$	$\frac{8.8}{3}$	$\frac{7.5}{21}$
	374.3	380.1	378.8	379.3	381.0	382.4
	$\frac{9.4}{15}$	$\frac{4.6}{5}$	$\frac{5.9}{2}$	$\frac{5.4}{1}$	$\frac{3.7}{5}$	$\frac{2.3}{19}$
	370.7	385.9	385.0	386.1	389.0	
	$\frac{2.7}{20}$	$\frac{7.5}{7}$	$\frac{8.4}{1}$	$\frac{7.3}{10}$	$\frac{4.4}{20}$	
			$\frac{387.8}{56}$			
			& Wash			

2.7 385.0

114 393.4

2

+50

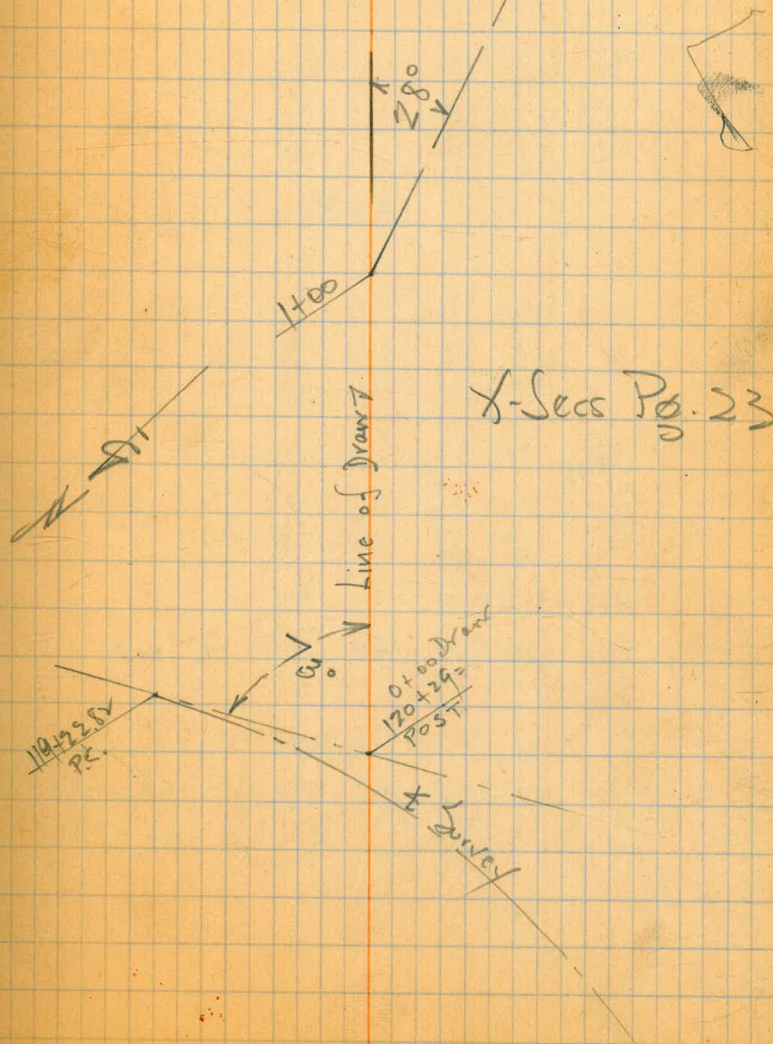
Alignment on Pg. 20

DRAW # 4

DRAW # 4

27

Alignment up side draw-



X-Section Page 23



# DRAW # 4

3m 10.7 354.3 343.6  
 11.2 43.1  
 13.3 41.0 341.3  
 8.5 345.8 458 ✓

0  
 +12 10.2  
 +30  $\frac{104}{H.W. Sta + 30}$

+70 0.8 353.5  
 10.5 364.0  
 1+00 on split of angle

+50  
 2 Alignment on P.S. 22

R

# Sta 120+00  
 +41 Lt. Pt.  
 121  
 119+50  
 343.5 343.6 342.2 341.2  
 $\frac{108}{30}$   $\frac{10.7}{14}$   $\frac{12.1}{14}$   $\frac{12.1}{14}$   
 343.0 342.2  
 $\frac{11.3}{16}$   $\frac{12.1}{30}$

## H. Water & Main Wash

348.0 347.1 343.9 342.9 343.7 349.5 350.3  
 $\frac{6.3}{30}$   $\frac{7.2}{10}$   $\frac{10.4}{6}$   $\frac{11.4}{2}$   $\frac{10.6}{14}$   $\frac{4.8}{14}$   $\frac{4.0}{20}$

355.9 355.2 348.9 346.5 348.8 353.0 354.8 356.1  
 $\frac{11.6}{22}$   $\frac{10.9}{13}$   $\frac{5.4}{4}$   $\frac{7.8}{14}$   $\frac{5.5}{4}$   $\frac{1.3}{9}$   $\frac{10.5}{12}$   $\frac{1.8}{20}$

361.5 360.0 351.2 350.5 351.0 354.6 556.6  
 $\frac{2.5}{23}$   $\frac{4.0}{18}$   $\frac{12.8}{3}$   $\frac{13.5}{14}$   $\frac{13.0}{1}$   $\frac{9.4}{5}$   $\frac{7.4}{16}$

367.0 364.0 356.3 354.3 356.0 357.7 362.1 365.9  
 $\frac{13.0}{22}$   $\frac{8.0}{14}$   $\frac{7.7}{4}$   $\frac{9.7}{2}$   $\frac{8.0}{14}$   $\frac{6.3}{5}$   $\frac{1.9}{11}$   $\frac{1.9}{20}$

366.1  
 +2.1



DRAW #5

B/W

8.5 335.4

326.9

10.0 325.4 325.4

0

7.9

9.3

+50

Alignment on  
Pg 24

1

+50

3.7

Sta. 156

~

Lt.

~

126+50

Rt.

324.5	326.3	325.5	326.9	326.6	325.4	325.5	327.2
109	91	99	85	88	100	99	82
<u>30</u>	<u>25</u>	<u>12</u>	<u>5</u>	<u>—</u>	<u>10</u>	<u>23</u>	<u>30</u>

H. Water = 0+00

||

10' Lt Sta 126+12  
Main Wash

332.4	329.3	328.1	327.4	328.1	328.1	329.3	330.4	333.7
30	6.1	7.3	8.0	7.3	7.3	6.1	5.0	1.7
<u>30</u>	<u>19</u>	<u>9</u>	<u>5</u>	<u>3</u>	<u>4</u>	<u>17</u>	<u>22</u>	<u>30</u>
335.4	329.6	328.6	328.0	328.8	328.7	331.7		
0.0	5.8	6.8	7.4	6.6	6.5	3.7		
<u>19</u>	<u>4</u>	<u>4</u>	<u>4</u>	<u>7</u>	<u>11</u>	<u>25</u>		
331.9	330.7	329.7	329.0	329.9	330.4	333.3		
0.5	4.7	5.7	6.4	5.5	5.0	2.1		
<u>11</u>	<u>4</u>	<u>—</u>	<u>3</u>	<u>6</u>	<u>12</u>	<u>24</u>		

High Water = 1+50

Add'l X-Sec's at Intr'n

C/1/27

26

SAN MIGUEL <sup>9 3/4</sup> BROADWAY -

B.M.

337.00

See Pg. 14

0.87 337.87

0.32 326.82 11.37 326.50

0.69 315.75 11.76 315.06

1.07 304.95 11.87 303.88

3.83 301.12 301.11

4.77 300.18 300.17

Head Culvert ±

Sta 135+47.83 ± Pave.

B.M.

3.85 301.10

X On N. End of W. Headwall of Culvert.  
Pt.

134+68

$\frac{4.2}{10}$   $\frac{4.0}{30}$   $\frac{4.1}{-}$   $\frac{4.6}{12}$   $\frac{6.0}{14}$   $\frac{6.4}{23}$   $\frac{6.7}{27}$   $\frac{4.7}{30}$   $\frac{4.4}{38}$   $\frac{4.4}{50}$

$\frac{2.7}{70}$   $\frac{3.1}{72}$   $\frac{5.2}{75}$   $\frac{4.9}{77}$   $\frac{4.66}{84}$   
E.P.

148

$\frac{4.0}{40}$   $\frac{4.2}{30}$   $\frac{4.7}{4}$   $\frac{3.9}{-}$   $\frac{4.3}{10}$   $\frac{6.6}{15}$   $\frac{6.9}{23}$   $\frac{5.2}{27}$   $\frac{4.1}{30}$   $\frac{4.2}{50}$

$\frac{5.2}{53}$   $\frac{4.8}{56}$   $\frac{4.70}{62.48}$

304.95

Lt.

Rt.

27

135+27

0A	60	66	60	48	484
<u>70</u>	<u>46</u>	<u>79</u>	<u>21</u>	<u>18</u>	<u>±</u>

+4783 ± Broadway

+6.3	25	47	61	507	478
<u>90</u>	<u>73</u>	<u>58</u>	<u>47</u>	<u>32</u>	<u>5P</u>

+56

+80	24	45	61	526	483	485
<u>100</u>	<u>70</u>	<u>61</u>	<u>58</u>	<u>46</u>	<u>13</u>	<u>±</u>
				EP	Plan	

+76

64	507	524	507	50
<u>90</u>	<u>50</u>	<u>26</u>	<u>12</u>	<u>±</u>
Gutter		Plan	EP	

+4783

4.78

± Pave.

4.88

Edge Pave 18' Lt.

0+50 South

5.16

±

5.36

EP

1+00 "

5.97

±

6.04

EP

1+50 "

6.51

±

6.62

EP

30495

0+50 North

4.69

±

4.82

E.P. 18' R.

1+00 "

4.60

±

4.67

E.P.

1+50 "

4.48

±

4.58

E.P.

8.74

East End North Box - N. Side

8.69

" " S. "

8.73

" South Box N. "

8.69

" " S. "

B<sup>W</sup>

3.85 301.10 301.10

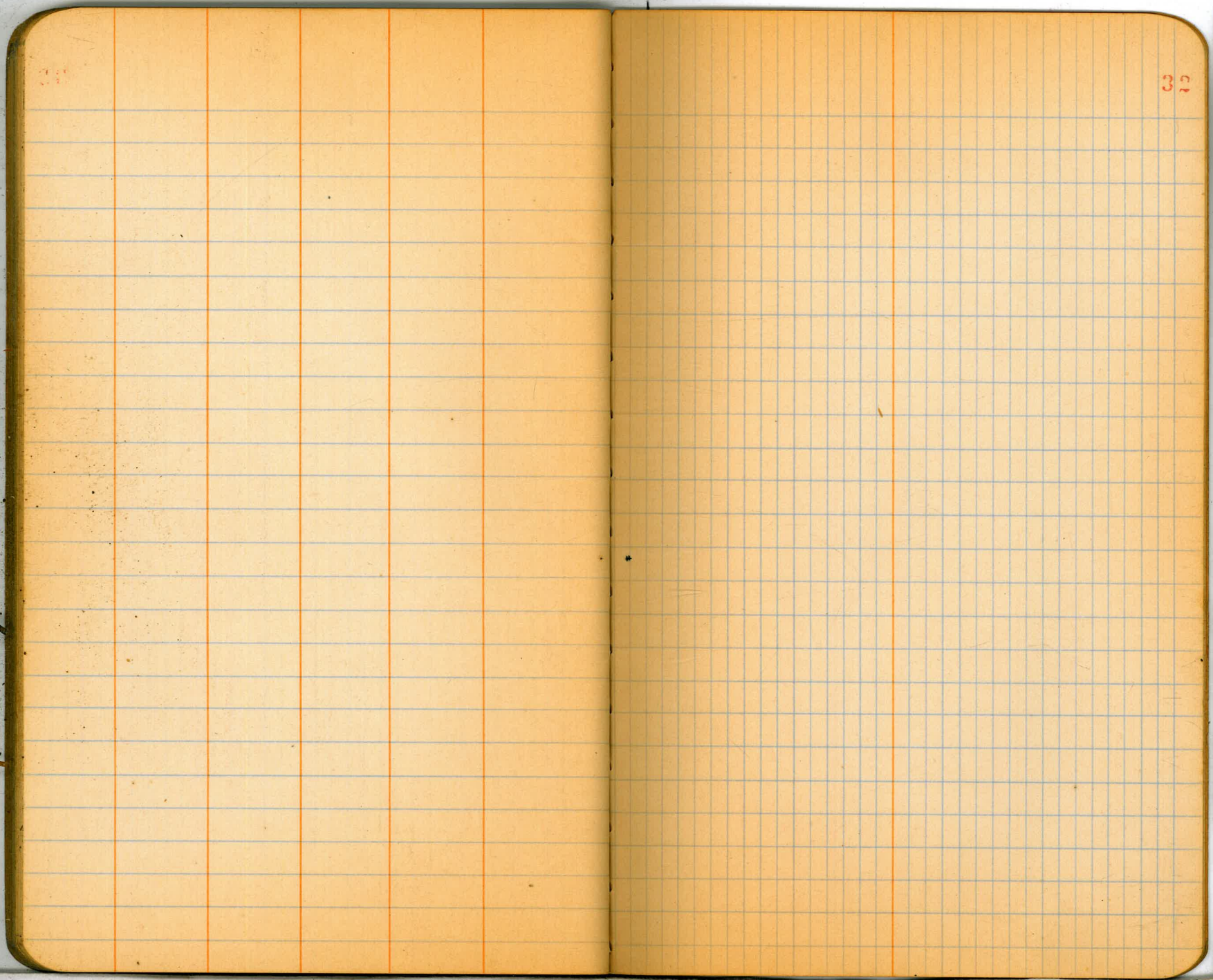
See Pg. 26



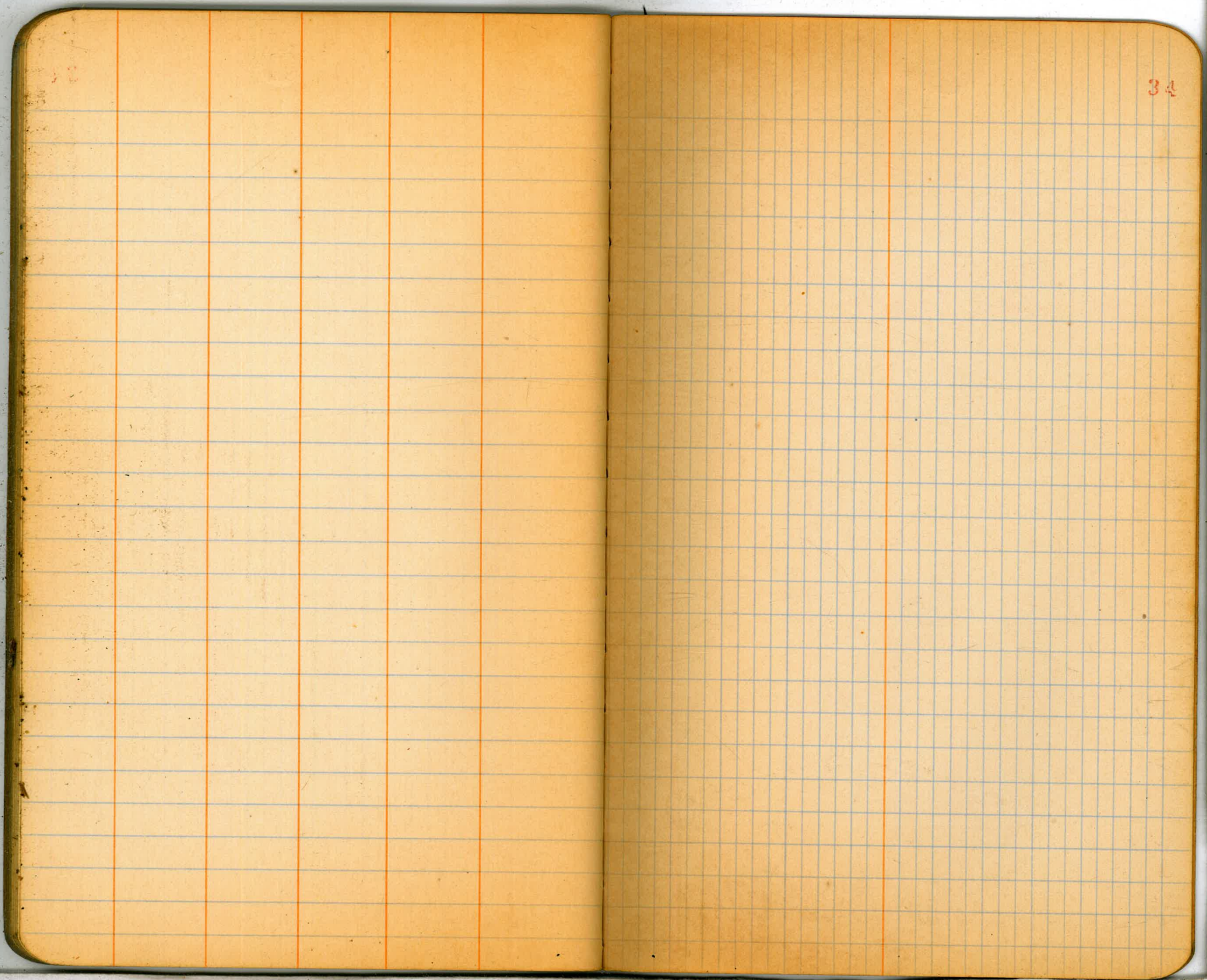












468.97

98<sup>no</sup>

Hub 35' Lt 1+045 Brdwy  
Elev 301.87

B.M. #12 San Miguel 2x2 hub 40' Lt  
~~140700~~ Elev 392.91  
107400

304.95

4.50

300.45

309.47

300.15

9.32