

NAME EL CAJON

Job 224244 A81D#7

Class \_\_\_\_\_ Course \_\_\_\_\_ Party \_\_\_\_\_

X-Section

Warren, G. & G. Co., Inc.  
200 Broadway, N.Y.  
Eng. Dept.

1990

278

# FIELD NOTES

No. 403P

ESPECIALLY ADAPTED

TO THE USE OF

ENGINEERING STUDENTS

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**EUGENE DIETZGEN Co.**

MANUFACTURERS

**DRAWING MATERIALS**

**MATHEMATICAL AND SURVEYING INSTRUMENTS**

**MEASURING TAPES**

CHICAGO SAN FRANCISCO NEW YORK  
NEW ORLEANS PITTSBURGH



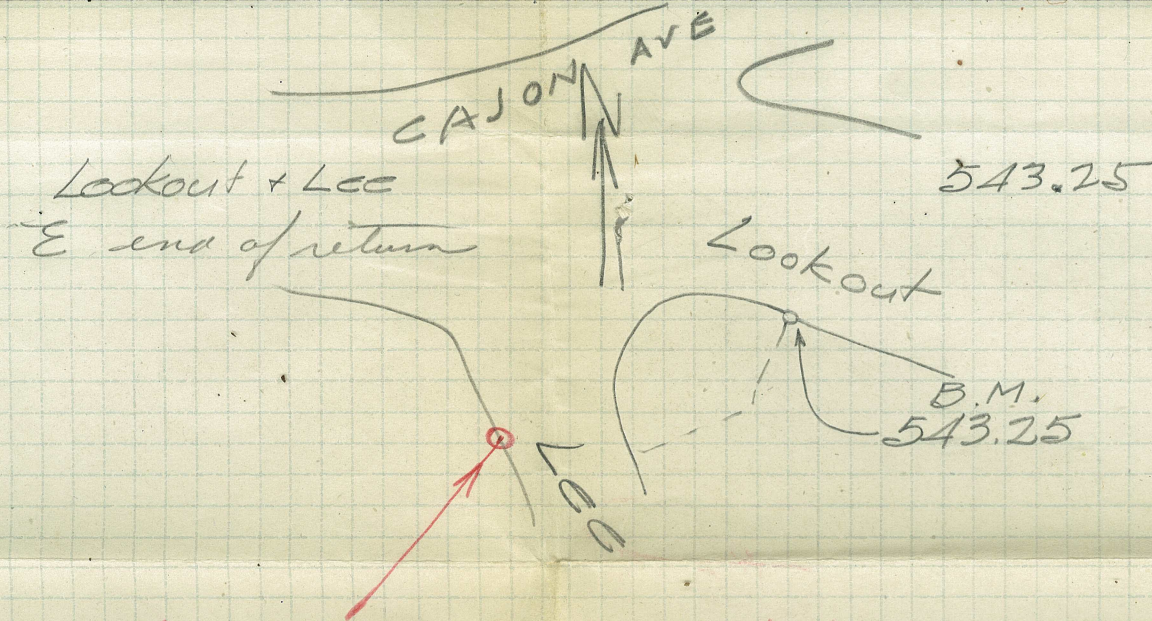
MICROFILMED

DEC 30 1964

INDEX

X Sec. El Cajon Blvd	1-8
Bench Levels	8-13
X Sec. El Cajon	14-16
Bench Levels	17





(Page 17-BK 278) Guy Pole - B.M. # N - 50' Rk. Sta. 125+00 - W. side Lee Ave.

$$\begin{array}{r}
 \text{Elev} = 543.437 \\
 \quad + 4.79 \\
 \hline
 \text{H.I.} = 548.227 \\
 \quad - 5.25 \\
 \hline
 542.977 \text{ Elev. Brass Plug}
 \end{array}$$

$$\begin{array}{r}
 543.250 = \text{Elev. La Mesa Datum.} \\
 - 42.977 = \text{" Coates Datum} \\
 \hline
 0.273 = \text{Diff.}
 \end{array}$$

Apr. 30, 1927

*og*



X-SECS EL CAJON BLVD

B<sub>w</sub>#1 268.72  
 1.59 A 1.50  
 0+00 396 469.34 469.4 ± Paxe

0-50 18" Chl?

0-100

0-150

B<sub>w</sub>#C 360 469.70 469.68

← Corrected Elev. — See Pg. 9

South										North					
64.8	66.7	67.1	66.95	69.20	69.31	69.52	469.0	469.1	69.58	67.4	68.1	67.9	68.3		
85	6A	6V	635	A.10	399	378	1.00	39	377	59	52	5A	50		
100	40	23	1A	135	75		75	15	125	13	28	40	75		
			Flax	Hawi	G.P.		EP		H.W.	Flax					
	67.3	67.4	69.5	69.64	69.85	69.62	69.8	68.1	68.8						
	60	59	38	365	345	368	45	52	45						
	20	21	11	75		75	15	16	20						
	67.9	68.4	69.2	69.2	69.90	70.11	69.90	69.8	68.9	68.5	70.0	69.8			
	5A	49	A.1	A.1	3A0	319	3A0	1.0	4A	45	33	35			
	40	36	20	16	75		75	15	16	29	35	40			

See Pg. 9

64.8  
55  
1.43

470.03  
1.25  
468.78

470.03  
469.68  
.35

468.72

Reduced 4-1-27 C.R.H.  
 Checked 4-1-27 C.R.H.



B.M. #1 5.55 474.27  
473.22

468.72

~~467.67~~  
See Page 5  
See Pg. 9

Blue = Cote 4/1/27

474.6  
4.9  
469.7

468.72  
5.55  
474.27  
4.9  
469.4

See Pg 18  
for Sta 2+84

4.60 475.30  
474.25 3.57

370.70  
469.65

0+00

0+50

1+00

1+50

2+00

2+25

2+50

3+00

3+50

3+80

4+00

X Sec. El Cajon Ave

1

LT Shoulder Edge Concrete ± Edge Concrete Shoulder

RT

Highway B.M. Nail in Porter Pole - 25' Rt. 579 0-30  
H.I. - ~~475.2~~

68.0 68.4 68.4 69.1 69.2 69.4 69.12 69.1 68.8 67.8 67.1 67.2 67.2  
6.3 5.9 5.9 5.1 5.1 4.9 5.15 5.2 5.5 6.5 7.2 7.1 7.1  
4.0 3.0 1.9 1.0 7.5 4.9 7.5 7.0 17 20 27 30 40

474.27

68.5 68.5 68.6 69.3 69.4 69.6 69.3 69.3 68.5 68.0 68.1 68.1  
5.8 5.8 5.7 5.0 4.9 5.0 5.0 5.8 6.3 6.2 6.2  
4.0 3.0 1.6 1.0 7.5 4.7 7.5 7.0 17 27 30 40

69.0 69.0 68.8 69.5 69.7 69.8 69.5 69.5 68.7 69.2 68.7 68.9  
5.3 5.3 5.5 4.8 4.7 4.5 4.8 4.8 5.6 5.1 5.6 5.4  
4.0 3.0 1.7 1.0 7.5 4.5 7.5 7.0 19 22 30 40

69.4 69.3 69.4 69.1 69.6 69.7 69.9 69.7 69.7 69.3 69.1 69.3 69.0  
5.0 4.9 5.2 4.7 4.6 4.4 4.6 4.6 5.0 5.2 5.0 5.3  
4.0 3.0 1.9 1.7 1.0 7.5 4.4 7.5 7.0 16 26 30 40

69.9 69.7 69.5 69.8 69.9 70.1 69.8 69.8 69.6 69.8 69.8  
4.4 4.6 4.8 4.5 4.4 4.2 4.5 4.5 4.7 4.5 4.5  
4.0 3.0 1.7 1.0 7.5 4.2 7.5 9 16 30 40

70.4 70.4 70.1 70.0 70.2 70.0 70.0 69.8 70.0 69.7 69.8  
3.9 3.9 4.2 4.3 4.1 4.3 4.3 4.5 4.3 4.6 4.5  
4.0 3.0 1.0 7.5 4.1 7.5 9 15 16 30 40  
Drive ↑

70.1 70.0 70.1 70.1 70.3 70.0 70.1 69.9 70.1 69.9 70.2  
4.2 4.3 4.2 4.2 4.0 4.3 4.2 4.4 4.2 4.4 4.1  
3.0 1.6 9 7.5 4.0 7.5 9 16 17 30 40

70.7 70.7 70.6 71.0 70.2 70.3 70.3 70.6 70.3 70.1 69.9 70.0  
3.6 3.6 3.7 3.3 4.1 4.0 4.0 4.0 4.0 4.2 4.4 4.3  
4.0 3.0 2.8 2.6 1.7 9 7.5 3.7 7.5 9 23 30 40

71.2 71.2 70.9 70.4 70.5 70.5 70.7 70.5 70.6 70.6 70.3 69.6 70.4 70.7  
3.1 3.1 3.4 3.9 3.8 3.8 3.6 3.8 3.7 3.7 4.0 4.7 3.9 3.6  
4.0 3.0 2.2 1.6 9 7.5 3.6 7.5 10 21 30 31 33 40

71.7 71.1 70.8 70.7 70.7 70.9 70.7 70.7 70.6 69.5 70.7 70.5 70.5  
2.6 3.2 3.5 3.6 3.6 3.4 3.6 3.6 3.7 4.8 3.6 3.8 3.8  
4.0 3.0 2.3 9 7.5 3.4 7.5 9 2.6 3.0 3.4 3.6 4.0  
Drive ↑

71.3 71.6 70.6 70.7 70.7 70.9 70.7 70.7 70.5 70.0 69.9 69.3 70.2 69.9  
3.0 2.7 3.7 3.6 3.6 3.4 3.6 3.6 3.8 4.3 4.4 5.0 4.1 4.4  
4.0 3.0 2.0 9 7.5 3.4 7.5 10 2.0 2.3 3.0 3.2 3.4 4.0

Measured 4-1-27 C.M.  
Checked 4-4-27 81376







475.30  
474.25

B.M. # 2

3.22

9400  
472.09  
471.03  
468.60  
467.55

3.07

475.15  
474.10

4.67

474.06  
473.01

5.76

469.39  
468.34

3.37

471.99  
470.94

5.44

468.67  
467.57

3.73

469.73  
468.68

5.99

466.00  
464.95

2.10

462.32  
461.27

9.51

460.22  
459.17

B.M. # A

5.50

456.82  
455.77

6.21

465.94  
464.89

2.59

459.73  
458.68

4.10

461.84  
460.79

	LT	±	RT
71.4	71.4	71.3	71.0
3.9	3.9	4.0	3.8
4.0	3.9	4.0	3.8
	19	16	10
	71.5	71.7	71.5
	3.8	3.6	3.8
	7.5	7.5	7.5
	3.9	3.9	3.9
	4.4	4.4	4.4
	3.8	3.8	3.8
	4.0	4.0	4.0
	3.9	3.9	3.9
	4.0	4.0	4.0

B.M. # 2 = Nail in Power Pole 30' Rt 9460 = 472.41  
471.03  
1.38

700' shot to Check B.M. # 1 = 467.67

Redwood 41-27 c2w

Checked 4-4-27 S.B.B.

461.95

Nail in Pole 25' Lt Sta 31405 Elev = 456.95  
455.77  
1.18

B.M. - Iron Pipe Triangulation Sta Rolando # 1 - Elev 461.94  
460.79  
1.15



B.M. #2

3.42

475.56

475.83

472.14

472.41

See Pg. 18 For  
Extra Shots -

Catoctin Drive

4.60

474.22  
474.49 5.94

469.62  
469.89

LT

Shoulder

Edge

Core

4

Edge

Core

Shoulder

RT

4

Highway B.M. #2 - Nail in Power Pole 30' RT 570 960 See Pg. 9

4.1 = ~~4.75~~ 4.756

	Shoulder	Edge	Core	4	Edge	Core	Shoulder							
9+50	71.7 3.9 40	71.7 3.9 30	71.5 4.1 19	71.0 4.6 17	71.6 4.0 10	71.7 3.9 7.5	71.9 3.7	71.7 3.9 7.5	71.7 3.9 9	71.6 4.0 24	71.6 4.0 30	71.7 3.9 40		
10+00	71.8 3.8 40	72.1 3.5 30	71.7 3.9 19	71.5 4.1 17	71.3 3.8 10	71.8 3.8 7.5	72.0 3.6	71.7 3.9 7.5	71.8 3.8 9	72.1 3.5 15	71.3 3.8 30	71.9 3.7 40		
10+25		72.5 3.1 40	72.3 3.3 30	71.9 3.7 10	71.8 3.8 7.5	72.0 3.6	71.8 3.8 7.5	71.9 3.7 9	72.0 3.8 7.5	71.8 3.7 18	71.5 3.8 30	72.0 3.6 40		
10+50	71.8 3.8 40	71.9 3.7 30	72.1 3.5 25	71.9 3.7 23	71.9 3.7 9	71.8 3.8 7.5	72.1 3.5	71.8 3.8 7.5	71.8 3.8 9	71.6 4.0 17	71.5 4.1 22	72.0 3.6 30	71.8 3.8 40	
11+00	72.0 3.6 40	72.3 3.3 27	71.3 4.3 18	71.1 4.5 17	71.4 4.2 11	71.5 4.1 7.5	71.8 4.0	71.6 4.0 7.5	71.8 4.0 7.5	71.5 4.1 10	71.1 4.5 15	71.6 4.0 19	71.8 3.8 30	71.9 3.7 40
11+50	71.6 4.2 40	71.4 4.3 30	70.9 4.7 27	70.6 5.0 19	71.0 4.6 11	71.3 4.3 7.5	71.3 4.3 7.5	71.5 4.1	71.2 4.2 7.5	71.2 4.4 9	70.7 4.9 14	71.2 4.4 18	71.1 4.5 30	71.8 4.3 40
12+00	70.7 4.9 A0	70.4 5.2 30	70.2 5.4 17	71.0 4.6 10	71.1 4.5 7.5	71.3 4.3	71.3 4.3	71.1 4.5 7.5	70.9 4.7 10	70.4 5.2 20	70.8 4.8 30	70.6 5.0 40		
12+50		70.3 5.3 40	70.6 5.0 30	70.8 4.8 10	70.8 4.8 7.5	71.0 4.6	70.9 4.7 7.5	70.8 4.8 7.5	70.9 4.7 10	70.8 4.8 10	70.2 5.4 30	69.9 5.7 40		
13+00	70.7 4.9 40	71.0 4.6 30	71.6 4.4 28	70.6 5.0 28	70.0 5.6 17	70.2 5.4 11	70.4 5.2 10	70.5 5.1 7.5	70.7 4.9	70.4 5.2 7.5	70.4 5.2 10	69.9 5.7 20	69.5 6.1 30	69.3 6.3 40
13+50	70.0 5.6 40	70.5 5.1 30	69.9 5.7 28	69.9 5.7 16	70.0 5.6 10	70.1 5.5 7.5	70.3 5.3	70.1 5.5 7.5	70.0 5.6 11	70.0 5.9 12	69.7 7.2 24	68.4 7.2 30	68.8 6.8 40	
14+00	69.6 6.0 40	70.4 5.2 36	70.5 4.9 30	70.6 6.0 28	69.5 6.1 16	69.9 5.7 10	70.0 5.6 7.5	70.2 5.4	69.9 5.7 7.5	69.9 5.7 10	68.8 6.8 18	68.4 7.2 21	68.7 6.9 30	68.7 6.9 40

Revised 4-1-27 C.M.  
Checked - 4-4-27. E.B.R.



474.22  
~~474.49~~

Shoulder  
Edge  
Curb  
Edge  
Curb  
Shoulder

14+50	69.8 4.4 40	70.4 3.8 30	70.49 3.73 28	69.5 4.7 28	69.7 4.5 10	69.8 4.4 7.5	70.0 4.2 7.5	69.6 4.6 7.5	69.6 4.6 9	68.9 5.3 18	68.4 5.8 22	68.4 5.8 30	68.6 5.6 40	
15+00	69.7 4.5 40	70.1 4.1 30	70.31 3.91 28	69.8 4.9 17	69.4 4.8 10	69.5 4.7 7.5	69.7 4.5 4.5	69.5 4.7 7.5	69.4 4.8 10	69.2 5.0 17	68.8 5.9 25	68.1 6.1 30	68.7 5.5 40	
15+50	69.6 4.6 40	70.0 4.2 30	70.12 4.10 28	69.7 5.0 19	69.3 4.9 10	69.3 4.9 7.5	69.5 4.7 4.7	69.3 4.9 7.5	69.4 4.8 9	69.3 4.9 18	69.1 5.1 30	68.9 5.3 40		
16+00	69.8 4.4 40	69.9 4.3 30	70.08 4.14 28	69.1 5.1 17	69.3 4.9 10	69.3 4.9 7.5	69.6 4.6 4.6	69.4 4.8 7.5	69.4 4.8 9	69.2 5.0 15	69.7 4.5 18	69.3 4.9 30	69.3 4.9 40	
16+50	70.4 3.8 40	69.9 4.3 30	70.1 4.1 30	70.07 4.15 28	69.2 5.0 28	69.3 4.9 10	69.3 4.9 7.5	69.6 4.6 4.6	69.4 4.8 7.5	69.4 4.8 10	69.0 5.2 14	69.3 4.9 19	69.3 4.9 30	69.1 5.1 40
17+04 <sup>32</sup>	70.1 4.1 40	70.0 4.2 30	69.99 4.23 28	69.0 5.2 28	69.0 5.2 17	69.2 5.0 10	69.2 5.0 7.5	69.5 4.7 4.7	69.3 4.9 7.5	69.3 4.9 9	69.2 5.0 17	69.2 5.0 30	69.2 5.0 40	
17+50	69.8 4.4 40	69.8 4.4 30	69.91 4.31 28	68.9 5.3 28	69.1 5.1 10	69.2 5.0 7.5	69.4 4.8 4.8	69.2 5.0 7.5	69.1 5.1 9	69.2 4.9 19	69.3 4.9 30	69.2 5.0 40		
Choctaw Drive 17+88 <sup>26</sup>	69.6 4.6 40	69.2 5.0 30	68.8 5.5 26	69.1 5.1 23	69.1 5.1 9	69.1 5.1 7.5	69.3 4.9 4.9	69.0 5.2 7.5	69.0 5.2 10	68.9 5.3 16	69.1 5.1 17	68.9 5.3 30	68.6 5.6 35	68.6 5.6 40
18+00	69.0 5.2 40	69.0 5.2 30	68.9 5.3 25	69.0 5.2 25	69.0 5.2 10	69.0 5.2 7.5	69.3 4.9 4.9	69.0 5.2 7.5	69.1 5.1 10	68.9 5.3 18	68.6 5.6 23	69.0 5.2 30	68.6 5.6 35	68.9 5.3 40
18+50	69.2 5.0 40	69.6 4.6 35	69.8 4.4 30	69.88 5.4 28	68.8 5.5 16	68.9 5.3 10	69.0 5.2 7.5	69.3 4.9 4.9	69.2 5.0 7.5	69.2 5.0 10	68.8 5.4 20	69.0 5.2 25	68.6 5.6 30	69.0 5.2 40
19+00	69.2 5.0 40	69.9 4.3 35	69.8 4.4 30	69.74 5.4 28	68.8 5.5 18	68.9 5.3 10	69.0 5.2 7.5	69.2 5.0 5.0	69.1 5.1 7.5	69.1 5.1 9	68.9 5.3 20	69.1 5.1 30	69.5 4.7 33	69.0 5.2 40

74.22  
69  
69.32

RC.

500 Pcs

Choctaw Drive

3.19

472.21  
472.48

5.20

469.02  
469.29

Reduced 4-1-27 CFW.  
Checked 4-4-27 CFW







472.21  
472.28

470.29  
470.56

5.97

466.24  
466.51

4.05

24+00

24+25

24+50

25+00

25+25

25+50

25+80

26+00

26+10

26+43

26+50

LT

Shoulder

Edge  
C&G

#

Edge  
C&G

Shoulder

RT

7

65.4	65.4	65.6	64.9	66.3	66.6	66.7	67.0	66.8	66.7	66.3	64.7	65.7	66.1
6.8	6.8	6.6	7.3	5.9	5.6	5.4	5.4	5.4	5.5	5.9	7.5	6.5	6.1
40	30	24	22	11	10	7.5	5.2	7.5	10	12	20	30	40

65.6	65.8	65.9	66.5	66.6	66.6	66.6	66.6	66.5	66.3	65.1	65.4	65.5	65.8
4.7	4.5	4.4	3.8	3.7	3.7	3.7	3.7	3.8	4.0	5.2	4.9	4.8	4.5
40	30	15	10	7.5	3.5	7.5	7.5	11	12	19	27	30	40

DRIVE →

65.3	65.9	65.7	64.6	66.3	66.3	66.7	66.4	66.3	65.3	65.5	65.5		
5.0	4.4	4.6	5.7	4.0	4.0	3.9	3.9	4.0	5.0	4.8	4.8		
40	30	30	20	10	7.5	3.6	7.5	11	17	20	40		

curb

65.1	66.0	65.7	65.7	66.1	66.1	66.4	66.2	66.2	65.7	65.3	65.7	65.6	
5.2	4.3	4.6	5.0	4.2	4.2	4.1	4.1	4.1	5.1	5.0	4.6	4.7	
40	30	30	16	10	7.5	3.9	7.5	11	17	27	30	40	

curb

65.6	65.8	66.0	66.0	66.0	66.0	66.2	66.0	65.8	65.3	66.4	65.7		
4.7	4.5	4.3	4.3	4.3	4.3	4.3	4.3	4.5	5.0	3.9	4.4		
40	30	10	7.5	7.5	4.1	7.5	7.5	10	21	30	40		

DRIVE →

66.0	65.7	65.8	65.8	65.8	65.8	65.8	65.7	65.4	66.1	65.5	66.0	66.1	
4.3	4.6	4.5	4.5	4.5	4.5	4.5	4.6	4.6	4.9	4.2	4.8	4.3	4.2
40	30	10	7.5	7.5	4.3	7.5	10	17	20	23	30	40	

65.8	66.1	65.7	65.7	65.7	65.7	65.7	65.7	65.4	65.8	65.9	66.0		
4.5	4.2	4.6	4.6	4.6	4.6	4.6	4.6	4.9	4.5	4.4	4.3		
40	30	10	7.5	7.5	4.4	7.5	10	16	19	30	40		

DRIVE →

66.1	66.1	66.1	65.5	65.5	65.5	65.7	65.4	65.3	65.2	66.2	66.3	66.4	
4.2	4.2	4.2	4.8	4.8	4.8	4.9	4.9	5.0	5.1	4.1	4.0	3.9	
40	30	23	14	10	7.5	4.6	7.5	10	16	20	30	40	

66.4	66.4	65.9	64.7	65.3	65.3	65.3	65.3	65.3	65.1	66.3	66.4	66.3	66.3
3.9	3.9	4.4	6.0	5.0	5.0	5.0	5.0	5.0	5.2	4.0	3.9	4.0	4.0
40	30	18	15	14	10	7.5	4.7	7.5	10	16	19	30	34

66.7	66.6	66.2	64.1	64.7	64.9	64.9	65.1	64.9	64.8	65.0	67.1	66.9	66.8
3.6	3.7	4.1	6.2	5.6	5.4	5.4	5.4	5.4	5.5	5.3	3.2	3.4	3.5
40	30	18	15	14	9	7.5	5.2	7.5	10	15	19	30	40

66.6	66.4	65.0	64.8	64.8	65.0	64.7	64.7	64.9	66.6	67.0	66.8		
3.7	3.9	5.3	5.5	5.5	5.3	5.6	5.6	5.4	3.7	3.3	3.5		
40	30	16	10	7.5	5.3	7.5	10	15	18	30	40		

DRIVE →

Reduced 7-1-27  
CWW

Checked 4-4-27 8376



470.79  
470.56

26+65

LT		Shoulder		Edge Conc.		E		Edge Conc.		Shoulder		RT	
66.6	66.8	66.9	67.1	64.0	64.6	4.5	4.5	4.1	4.1	64.5	64.8	67.1	67.0
3.7	3.5	3.4	4.6	6.3	5.7	5.8	5.8	6.4	6.4	5.8	5.5	3.2	3.3
40	30	24	17	15	12	7.5	7.5	5.6	7.5	10	15	19	30

26+93

66.9	67.0	66.7	64.1	63.8	63.9	6.4	6.4	6.3	6.3	6.4	6.4	6.2	6.2
3.4	3.3	3.6	6.2	6.5	6.4	6.4	6.4	6.4	6.4	6.4	6.2	3.3	3.0
40	30	20	17	10	7.5	7.5	7.5	7.5	7.5	10	14	18	30

27+10

65.7	64.7	62.6	62.3	62.6	63.5	6.3	6.3	6.3	6.3	6.3	6.4	6.3	6.6
4.6	5.6	6.7	7.0	6.7	6.8	6.8	6.8	6.8	6.8	6.8	6.3	4.0	3.4
40	30	15	13	7.0	7.5	7.5	7.5	7.5	7.5	10	16	18	40

P.T. 27+41.48  
27+12.26

64.9	64.6	62.9	62.8	62.6	62.7	6.2	6.2	6.3	6.2	6.2	6.3	6.5	6.5
5.4	5.7	6.4	7.5	7.7	7.6	7.5	7.5	7.5	7.4	7.2	7.3	5.2	4.6
40	30	27	13	12	10	7.5	7.5	7.2	7.5	12	18	20	40

27+25

64.9	64.5	63.8	62.7	62.4	62.6	6.7	6.7	6.7	6.7	6.7	6.2	6.3	6.3
5.4	5.8	6.5	7.6	7.9	7.7	7.6	7.6	7.6	7.6	7.6	7.7	7.2	6.9
40	30	22	13	11	10	7.5	7.5	7.4	7.5	10	18	30	40

27+50

64.3	63.6	62.1	62.2	62.2	62.2	6.2	6.2	6.2	6.2	6.2	6.2	6.3	6.3
6.0	6.7	8.2	8.1	8.1	8.1	8.1	8.1	8.1	8.1	8.1	7.6	7.3	7.3
40	30	12	10	7.5	7.9	7.9	7.5	7.9	7.5	10	22	30	40

464.02  
464.29

8.47  
7.11

461.82  
462.09  
456.91  
457.18

2.20

BM # 4

Nail in Pole 25' Lt Sta 31405 - Elev 456.95

Revised 4-1-27 C.W.  
Checked 4-11-27 S.B.D.

Cont'd on Pg. 14



Bench Levels  
Running Westerly

(Circuit #1)

Dietzgen Level # 10845

9

March 19-27  
Clark  
Culver  
Radler

B.M. #4	8.423	465.373	456.95	
Relando B.M.			3.375	461.998
	9.168	466.926	7.615	457.758
	5.682	471.418	1.190	465.736
B.M. "A"	3.438	473.874	0.982	470.436
	5.548	475.167	4.255	469.619
Highway B.M. #2			3.030	472.137
B.M. "B"			2.163	473.004
	3.033	476.037		
	4.261	474.972	5.326	470.711
Highway B.M. #1			6.25	468.72
B.M. "C"			5.294	469.678
	5.472	475.808	4.636	470.336
	3.200	475.075	3.933	471.875
	4.585	473.810	5.850	469.225
B.M. "A"			3.398	470.412
	3.004	471.486	5.328	468.482
	2.138	467.779	5.845	465.641
	4.542	462.216	10.105	457.674
Highway B.M. #4			5.325	456.891

Highway B.M. #4 Nail in Pole 25' Lt Sta. 31405  
On Iron pipe - Triangulation Sta Relando #1 - Elev = 461.94

Nail in easterly end of sign Board 60' Lt Sta 19450

Nail in pole 30' Rt Sta 9460 Elev = 472.41

Nail in pole 150' Lt Sta 10425

Nail in pole 25' Rt Sta 0-30 Elev 467.67

Nail in easterly end of sign board 135' Rt Sta 0-150

468.72

5.55

474.27

Checked  
4-1-27  
C.W.

Elev = 456.95



Bench Levels  
Running Easterly

(Circuit #2)

Dietzgen Level #10845

10

March-19-1927

Highway B.M. #4	5.310	462.260		456.95
	4.419	463.952	2.732	459.538
	1.397	453.375	11.974	451.978
	0.787	442.554	11.608	441.767
	1.243	431.981	11.816	430.758
B.M. "E"	11.432	440.271	3.142	428.839
	11.168	450.565	0.874	439.397
	11.813	462.115	0.263	450.302
B.M. "F"			3.147	458.968
	4.557	462.228	4.444	457.671
B.M. "G"			1.870	460.358
	0.868	455.028	8.068	454.160
	4.069	447.745	11.352	443.678
	11.185	448.384	10.546	437.199
	11.766	459.490	0.660	447.724
Highway B.M. #A	4.860	462.006	2.344	457.146
			5.040	456.968

B.M. #A	5.040	461.990		456.95
B.M. "D"			8.621	453.369

Nail in pole 25' Lt Sta 31405

Clark

Culver

Radier

428.94 Adj - to suit state Datum -  
Nail in Western End of sign board 50 Rt Sta 39485

459.07  
Nail in Tree 50 Rt Sta 42450

460.350  
Nail in pole 100' Rt Sta 46420

Calculations checked  
4-1-27 C.F.W.



Bench Levels

Circuit #3  
Adjusted  
Elev

B.M. "G"	4.547	464.897		460.350	Nail in pole 100' Rt Sta 46+20
	5.143	466.545	3.495	461.402	
	5.273	468.605	3.213	463.332	
B.M. H	4.596	467.597	5.604	463.001	<sup>+0.13</sup> 462.992 On N.E. Cor. Concrete. step "Casita" House - 75' Rt Sta 64+00
	7.766	471.560	3.803	463.794	
Highway B.M. #8			3.680	467.880	467.868 Elev = 468.06 - Nail in Pole 39' Rt Sta 70+25
	10.132	480.797	0.895	470.665	
B.M. - I			8.729	472.068	<sup>+0.13</sup> 472.055 On N.E. Cor. Conc. Step of house 70' Rt Sta 72+50
	8.903	485.992	3.708	477.089	
Highway B.M. #9			5.723	480.269	Nail in Pole 39' Rt Sta 79+74 Elev = 480.20
	9.140	494.227	0.905	485.087	
B.M. "J"			2.870	491.357	<sup>+0.15</sup> 491.337 Nail in southerly end of sign board 75' Lt Sta 84+50
	0.920	485.909	9.238	484.989	
	5.170	482.056	9.023	476.886	
	1.250	472.143	11.163	470.893	
	3.272	467.732	7.683	464.460	
	5.693	468.972	4.453	463.279	
B.M. "H"			5.950	463.022	
	5.064	468.233	5.803	463.169	
	4.365	466.193	6.405	461.828	
			5.803	460.390	

March 21-1927  
Clark  
Culver  
Rodier  
Dietzgen Level

checked  
4-1-27  
C.F.W.

B.M. #G?



Bench Levels

(Circuit #4)

94+75

12.

March 21-1927

	+	π	-	
B.M. "J"	0.563	491.900		491.337
	4.442	487.660	8.682	483.218
	8.873	493.318	3.215	484.445
B.M. "K"			0.542	492.77 <sup>6</sup>
	7.190	498.664	1.844	491.474
	9.440	507.458	0.646	498.018
Highway B.M. #11			5.705	501.753
B.M. "L"			1.493	505.965
	4.149	504.146	7.461	499.997
	11.923	514.520	1.549	502.597
	11.880	525.724	0.676	513.844
	9.175	534.028	0.871	524.853
Highway B.M. #1		535.028		525.853
			6.130	527.898
B.M. "M"			3.828	528.898
	6.283	537.410		530.200
		538.410	2.901	531.200
	3.157	533.861		531.127
		534.861	6.706	532.127
	9.740	537.942		530.704
		538.942	5.659	531.704
	10.877	547.309		528.202
		548.309	1.510	529.202
B.M. "N"			3.872	536.432
	1.225	538.765		543.437
		539.765	9.769	544.437
	7.200	535.626		537.540
		536.626	10.339	538.540
	4.331	536.383		528.426
		537.383	3.574	529.426
	0.870	529.834		532.052
		530.834	7.419	533.052
	1.987	520.269		528.962
		521.269	11.552	529.962
				518.282
				519.282

Dietzen Level #

Nail in tree 60 Lt. Sta 94+75

Nail in brace post 20' Lt Sta 100+16 Elev- 501.89

Nail in 18" Eucalyptus tree 50' Lt Sta 100+75

Nail in tree 21' Rt Sta 110+30 Elev- 528.01

Nail in pole 50' Rt Sta 113+50 - W. Side Park Ave. El 530.34

Nail in guy pole 50' Rt Sta 125+00 - W. Side Lee Ave



	520.269		
	<del>521.269</del>		
1.429	509.834		508.405
	<del>510.834</del>	11.864	<del>509.405</del>
6.542	505.856		499.314
	<del>500.856</del>	10.520	<del>500.314</del>
	500.939		500.756
0.183	<del>445.939</del>	5.100	<del>445.756</del>
	493.664		492.281
1.383	<del>488.664</del>	8.658	<del>487.281</del>
	488.355		484.012
4.343	<del>487.355</del>	9.652	<del>478.012</del>
	492.602		483.098
9.504		5.257	<del>477.098</del>
			491.284
		1.318	

B.M. "J"

Elev- 491.337

Checked 4-1-27  
J.W.



# Cont'd from Pg. 8

14

Highway  
BM #A

7.86

464.81

456.95

6K

See Pg. 22

Lt | | | Rt

H.I. = 464.81

28+00	62.5 2.3 35	62.8 2.0 30	62.6 2.2 24	62.3 2.5 18	61.7 3.6 13	61.5 3.3 10	61.4 3.1 7.5	61.0 3.2 7.5	61.38 3.43 7.5	61.48 3.33 9	61.2 3.6 14	61.6 3.2 17	61.9 2.9 30	62.1 2.7 40
28+50	61.5 3.3 40	61.4 3.4 30	61.3 3.5 19	60.5 4.3 15	60.5 4.2 10	60.5 4.2 7.5	60.7 4.0 4.09	60.44 4.3 7.5	60.52 4.29 10	60.5 4.3 16	60.8 4.0 17	60.75 4.1 19	60.5 4.3 22	60.5 4.1 30
29+00	55.7 9.6 40	56.7 9.1 30	55.5 9.3 21	58.5 6.3 15	58.9 5.9 12	59.41 5.4 10	59.39 5.4 7.5	59.42 5.39 7.5	59.45 5.36 10	59.4 5.4 14	59.5 5.3 16	57.2 7.6 22	56.3 8.5 30	55.7 9.1 35
29+19	58.0 11.8 40	53.3 4.5 30	53.1 4.6 20	54.8 10.0 14	58.0 6.8 11	58.4 6.4 9	59.0 6.7 7.5	58.96 6.8 7.5	58.92 6.8 10	58.9 6.8 10	58.9 6.8 15	55.9 10.5 18	54.2 8.4 21	55.3 9.5 30
29+54	51.5 13.3 40	52.2 12.6 30	51.9 11.9 22	59.3 7.5 15	58.32 6.4 10	58.32 6.4 7.5	58.55 6.4 6.26	58.37 6.4 7.5	58.32 6.4 10	58.3 6.5 17	56.4 8.4 21	56.5 8.3 26	57.1 7.7 30	57.5 7.3 35
30+00	52.9 11.9 40	53.6 11.2 30	54.2 10.6 21	57.3 7.5 15	57.91 6.9 10	57.89 6.9 7.5	58.16 6.6 6.65	57.90 6.9 7.5	57.90 6.9 10	57.3 7.5 20	57.7 7.1 30	57.7 7.1 40	57.7 7.1 40	57.7 7.1 40
30+50	51.2 13.6 40	52.7 12.1 30	53.6 11.2 19	59.0 7.8 14	57.78 7.0 10	57.68 7.1 7.5	57.94 6.8 7.5	57.67 7.1 7.5	57.70 7.1 10	57.3 7.5 17	57.5 7.3 21	57.6 7.2 30	57.5 7.3 40	57.5 7.3 40
31+00	54.9 7.6 40	55.4 7.1 35	54.8 7.7 30	55.6 6.9 20	56.9 5.6 15	57.49 5.0 10	57.48 5.0 7.5	57.74 4.7 4.76	57.49 5.0 7.5	57.54 4.9 10	57.8 4.7 30	58.0 4.5 40	58.0 4.5 40	58.0 4.5 40
31+50	57.4 5.1 40	57.7 4.8 34	58.3 4.2 30	57.5 5.0 24	57.3 4.9 15	57.44 5.0 10	57.42 5.0 7.5	57.62 4.8 4.88	57.43 5.0 7.5	58.0 4.5 30	58.2 4.3 37	58.5 4.0 40	58.5 4.0 40	58.5 4.0 40
32+00	58.2 4.3 40	58.5 4.0 30	58.3 4.2 20	57.7 4.8 16	57.6 4.9 14	57.28 5.2 10	57.29 5.2 7.5	57.25 5.2 5.01	57.25 5.2 7.5	57.2 4.8 30	57.7 4.8 37	58.4 4.1 38	58.5 4.0 40	58.5 4.0 40

± Culvert.

R.T.

H.I. = 462.50

Revised 4-1-27 CSW  
Checked 4-4-27 RBH







464.30 ✓

36+00

36+50

1.29

453.58 ✓

12.01

452.29 ✓

37+00

0.67

442.31 ✓

11.94

441.64 ✓

37+50

1.54

433.00 ✓

10.85

431.46 ✓

38+00

B.M. "E"

4.29

428.71 ✓

428.84

P.T. ~~38+57.50~~  
38+36.47

Nail in Westerly end sign board Elev 428.84 Page 10

Cont'd on Pg. 19

Lt. H.I. = 464.3 ✓ RT

59.1	59.1	59.1	56.1	55.85	55.5	455.66	55.70	53.45	55.27	55.4	58.5	59.2	59.3
5.2	5.2	5.2	8.2	8.65	8.75	8.64	8.6	8.85	9.03	8.9	5.8	5.1	5.0
40	30	12	8	6	4	4	4	7	15	20	30	35	40

Pavement 5

58.4	58.5	66.8	59.0	58.2	57.1	459.70	54.8	54.2	54.30	54.02	53.98	54.3	58.2
5.9	5.8	5.5	5.3	6.1	5.2	4.6	9.5	10.09	10.00	10.28	10.27	10.0	6.1
50	40	30	19	17	13	4.6	6	10	19	28	30	35	47

Pav 5

54.1	54.9	56.6	55.8	55.1	46.0	57.5	58.1	58.2	53.2	52.18	52.03	52.09
10.2	9.4	7.7	8.5	9.2	8.3	6.8	6.2	6.1	11.1	12.12	12.27	12.21
50	40	15	8	2	7	7	7	21	28	5	40	46

H.I. 453.6 ✓ Pav 5

43.8	44.3	44.8	44.60	45.6	46.4	47.9	48.5	48.9	49.5
9.8	9.3	8.8	7.6	8.0	7.2	5.7	5.0	4.7	4.1
50	40	15	7.6	70	74	27	37	40	50

H.I. - 442.31 ✓

33.1	33.3	433.4	33.9	34.1	35.6	34.2	35.0
9.2	9.0	8.9	8.4	8.2	6.7	8.1	7.3
50	40	8.9	20	35	40	44	50

Top 16" Water Main

H.I. - 433.0 ✓

23.6	23.7	24.1	425.6	25.4	26.3	28.0	28.4
9.4	9.1	8.9	7.4	7.6	6.7	5.0	4.6
50	40	35	7.4	17	30	40	50

Revised 4-1-27  
C.F.W.

Checked B.P.H. 4-4-27



Bench Levels  
Cont from Page 13

Circuit #5

17

BM "N"	5.935	549.372	543.437
	1.832	539.935	11.269 538.103
	3.702	535.586	8.051 531.884
	0.823	527.416	8.993 526.593
	4.581	520.313	11.684 515.732
	1.444	510.154	11.603 508.710
	12.057	521.501	0.710 509.444
	11.939	532.729	0.711 520.790
	11.971	543.691	1.009 531.720
	5.345	548.201	0.835 542.856
	1.922	541.233	8.890 539.311
	5.843	540.285	6.791 534.447
U.S.G.S.-BM		0.525	539.760
	6.090	541.009	5.366 534.919
	9.022	548.369	1.662 539.347
	1.588	544.295	5.662 542.707
	0.526	533.032	11.789 532.506
	1.290	522.327	11.995 521.037
	0.487	510.980	11.834 510.493
	10.949	516.953	4.976 506.004
	11.365	527.319	0.999 515.954
	9.522	535.511	1.330 525.989
	7.910	540.125	3.296 532.215
	10.070	548.990	1.205 538.920
BM "N"		5.569	543.421 ✓

Nail in guy pole 50' Rt Sta 125+00 - W. Side Lee Ave

← Brass cap in wall of Bldg 4' ± above sidewalk  
near SW Cor Hero Dr + Lookout St Elev. 540.06  
La Mesa -

OK 4-1-27  
C. J. W.

Elev = 543.437



B<sup>m</sup>#B

2.80

475.86

473.004

See Pg. 9

12+30 E

1.73 471.07

5.5 470.3

5.8 470.0

4.75 471.05

5.8 470.0

5.8 470.0

5.3 470.5

5.03 470.97

See Pg. 4

Along ≠ Catoctin Dr.  
≠ Pave -

50' North ≠ St.

90 " " "

" " Curb Rt.

100 " "

150 " "

184 " "

" " Curb Rt.

Revised 4-1-27  
C.F.W.Checked 4-4-27  
81576B<sup>m</sup>#4

3.39

475.53

472.14

See Pg. 9

7+50

1.02 471.51

71.5 ✓

≠ Pave -

5.0 470.5

5.2 470.3

5.3 470.4

4.5 471.0

100' South on ≠ Huron Dr.

200 " "

300 " "

400 " "

See Pg. 2

2+84

5.38 470.15

On Man Hole Cover 14' Lt of ≠

Revised 9-1-27  
C.F.W.Checked 4-4-27  
81576



Cont'd from Pg. 16

E. P. Chittor  
J. Thompson  
W. Bunker  
3-31-1927

19

Cont from Page 16

428.84 <sup>✓</sup> B.M.

Nail in Westery. end of signboard 50 ft 39+85

T. 429.45 - 429.5

0.61 429.45 <sup>✓</sup>

38+50

8.0	20.7	21.8	423.3	24.9	27.4	
60	80	70	60	40	20	19
	40	15		20	20	60

38+67

17.4	18.4	420.0	21.1	22.7	23.8	24.3
12	11	95	80	60	50	50
75	40		20	40	40	75

38+85

15.5	16.6	418.3	19.3	22.4	21.0
14	12	110	100	70	85
75	40		40	60	75

Top 16" Water Main  
Disregard for quantities

38+92

16.4	15.5	16.0	416.3	16.9	18.1	20.1
13	14	13	130	12	11	90
75	60	40	40	40	50	75

39+00

16.2	17.0	16.7	17.4	16.4	17.6	19.0
13	12	12	12	13	11	10
75	40	40	40	75	40	100

39+20

17.5	17.9	418.5	19.0	18.7	22.2
12	11	110	10	10	70
75	40		40	75	75

Top 16" Water Main

39+40

22.1	21.0	420.1	20.4	20.9
70	85	90	90	80
75	40		40	75

39+70

21	28.1	425.5	23.8
60	10	40	50
	40		40

0.61 428.84 <sup>✓</sup>

Reduced 7-1-27

checked 4-4-27 8376



11.27 440.11 ✓  
39+90

π 440.11 ✓  

$$\begin{array}{r} 31.8 \\ 83 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 30.6 \\ 95 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 429.1 \\ 110 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 285 \\ 116 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 26.2 \\ 132 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 15.7 \\ \hline 60 \end{array}$$

40+15

$$\begin{array}{r} 35.1 \\ 50 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 433.7 \\ 84 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 32.8 \\ 73 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 31.8 \\ 83 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 87 \\ \hline 60 \end{array}$$

40+50

$$\begin{array}{r} 439.7 \\ 04 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 4381 \\ 20 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 377 \\ 24 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 36.6 \\ 33 \\ \hline 40 \end{array}$$

0.68 439.43 ✓

Top fence post 25' Lt 40+15

C. P. Chilton  
3-31-1927

0.15 439.58 ✓  
B<sub>W</sub>

11.80 427.78 ✓ 427.87

State B<sub>W</sub> 68' Lt Sta. 39+64 en 1x2 Hub

11.80 439.67 ✓  
B<sub>W</sub>\*F

10.71 428.96 ✓ 428.84

See Pg. 10

0.15 439.52 ✓

12.81 452.33 ✓

41 452.3

$$\begin{array}{r} 46.7 \\ 56 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 46.4 \\ 59 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 46.7 \\ 56 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 446.4 \\ 59 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 45.3 \\ 110 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 45.1 \\ 113 \\ \hline 40 \end{array}$$

A1

1.92 450.41 ✓

41.462.5

12.05 462.46 ✓

$$\begin{array}{r} 54.3 \\ 64 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 452.0 \\ 85 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 453.0 \\ 95 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 452.8 \\ 97 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 52.2 \\ 103 \\ \hline 40 \end{array}$$

45.0

$$\begin{array}{r} 57.3 \\ 52 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 57.1 \\ 54 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 457.0 \\ 55 \\ \hline 11 \end{array}$$

$$\begin{array}{r} 56.9 \\ 56 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 56.7 \\ 58 \\ \hline 40 \end{array}$$

A2

Cont'd on Pg. 23

Revised 4-1-27  
Checked 4-4-27 E.B.K.



3<sup>th</sup> A

3.39

473.83

470.44

See Pg. 9

17+88<sup>26</sup>

POT

4.51

169.3<sup>✓</sup>69.3<sup>✓</sup>

≠ Pave

3.9

69.9

50' N. on Choctaw Dr.

3.98

369.85

Rt Curb

3.90

369.93

Lt "

3.4

70.4

150' N on St.

3.66

370.17

" 15' Rt. Curb

3.63

370.20

" 15' Lt. "

500  
See Pot3<sup>th</sup> A

2.68

473.12

470.44

See Pg. 9

21+42.47

4.84

68.30

68.31<sup>✓</sup>

≠ Pavement

4.6

68.5

37' N on Art St - End Ret.

4.22

468.90

" 15' Lt. on Curb

4.9

68.2

100' N on St

4.67

468.45

" 15' Lt. - Curb

5.3

67.8

250' N on St

5.40

467.72

" 15' Rt - Curb

5.38

467.74

" 15' Lt "

500  
See Pot

Reduced 4-1-27 C. J. M.

Checked 4-4-27 B. B. B.



3 1/2 #4

10.56 467.51

456.95 See Pg. 9

28+00.76

5.69 467.82

± Pavement

3.3 64.2

100' South end Seminole -

14 66.1

200 " "

See Pg. 9

27+55

4.82 462.69

24' Rt. of ± On Gas Valve Cover =

Checked 4-11-27

SBH



Cont'd from Pg. 20

462.46

42+50

BW#F

3.38 459.08 <sup>9.07</sup> 458.97

See Pg. 10

43

+50

4.11

462.47

4.10 458.36

44

+50

45

+50

46

4.1. 462.46 = 462.5

23

58.2 58.2 457.8 57.5 57.5  
 $\frac{4.3}{40}$   $\frac{4.3}{25}$   $\frac{4.7}{-}$   $\frac{5.0}{25}$   $\frac{5.0}{40}$

58.4 58.4 457.8 57.7 57.3  
 $\frac{4.1}{40}$   $\frac{4.1}{25}$   $\frac{4.7}{-}$   $\frac{4.8}{25}$   $\frac{5.2}{40}$

458.4 458.4 458.4 57.7 57.4  
 $\frac{4.1}{40}$   $\frac{4.1}{25}$   $\frac{4.1}{-}$   $\frac{4.8}{25}$   $\frac{5.1}{40}$

462.5

58.2 58.1 457.6 57.2 57.2  
 $\frac{4.3}{40}$   $\frac{4.4}{25}$   $\frac{4.9}{-}$   $\frac{5.3}{25}$   $\frac{5.3}{40}$

57.7 57.7 457.4 457.4 57.3  
 $\frac{4.8}{40}$   $\frac{4.8}{25}$   $\frac{5.1}{-}$   $\frac{5.1}{25}$   $\frac{5.2}{40}$

57.9 57.8 457.7 57.8 57.9  
 $\frac{4.6}{40}$   $\frac{4.7}{25}$   $\frac{4.8}{-}$   $\frac{4.7}{25}$   $\frac{4.6}{40}$

58.4 58.8 458.7 58.6 58.7  
 $\frac{4.1}{40}$   $\frac{3.7}{25}$   $\frac{3.8}{-}$   $\frac{3.9}{25}$   $\frac{3.8}{40}$

59.4 59.4 459.6 59.5 59.5  
 $\frac{3.1}{40}$   $\frac{3.1}{25}$   $\frac{2.9}{-}$   $\frac{3.0}{25}$   $\frac{3.0}{40}$

Checked 4-4-27 5877 Reduced 4-1-27 C.F.W.



462.47

46+50

B<sub>1</sub> + G

4.24 164.72

1.99 460.48 460.50 See Pg. 10

B<sub>1</sub> W

5.78 458.94 458.96 State B<sub>1</sub> W - On P.C. Hub Sta. 46+98.02

HD 462.5

59.1	59.7	459.5	594	593
<u>34</u>	<u>28</u>	<u>20</u>	<u>31</u>	<u>32</u>
40	25		25	40

H2464.72

59.3	59.4	459.6	59.71	59.20
<u>54</u>	<u>53</u>	<u>51</u>	<u>501</u>	<u>552</u>
40	25		25	40
			at base	at base

47

+08

On Angle of Alice St.  
For drainage - not quantities -

57.1	58.6	59.6	459.7	59.26	58.72	56.92
<u>76</u>	<u>61</u>	<u>51</u>	<u>50</u>	<u>536</u>	<u>600</u>	<u>780</u>
200	100	50		50	100	200

+50

59.7	60.49	460.64	460.28	59.4	59.6	59.7	60.34
<u>50</u>	<u>423</u>	<u>408</u>	<u>444</u>	<u>53</u>	<u>51</u>	<u>50</u>	<u>441</u>
40	21	8	pare	11	19	40	conc base of pump

48

59.7	60.0	61.0	61.14	61.27	460.74	60.4	59.7	59.6
<u>50</u>	<u>47</u>	<u>37</u>	<u>355</u>	<u>343</u>	<u>398</u>	<u>43</u>	<u>50</u>	<u>51</u>
40	34	27	8.8	10		4	25	40

+50

61.4	60.6	60.8	61.27	61.53	461.39	61.10	60.6	60.0
<u>36</u>	<u>41</u>	<u>39</u>	<u>345</u>	<u>319</u>	<u>333</u>	<u>362</u>	<u>41</u>	<u>47</u>
40	27	16	11.8	4		4	9	40

49

61.6	61.4	61.1	61.27	61.48	461.73	61.44	61.0	60.4	60.3
<u>37</u>	<u>33</u>	<u>36</u>	<u>325</u>	<u>322</u>	<u>299</u>	<u>328</u>	<u>37</u>	<u>43</u>	<u>44</u>
40	20	18	12.8	12.8		7.5	11	33	40

Reduced 4-1-2 Egn  
E



↑  
49+26.29=  
54+6.85  
↓

461.72 ✓

4.61 466.05 ✓ 3.35 461.37 ✓

+50

37m

2.51 463.54 ✓ 463.51 ✓

55

+50

+50

Colvert Data

56

+50

I.P.

3.92 467.87

2.10 463.95 ✓

H. 1.464.72

25

61.3	61.3	61.3	461.62	461.87	61.58	61.0	60.6
$\frac{24}{40}$	$\frac{26}{22}$	$\frac{24}{12}$	$\frac{310}{75}$	$\frac{285}{EP}$	$\frac{314}{75}$	$\frac{37}{14}$	$\frac{41}{.40}$

H. 3466.05

61.3	61.2	61.1	61.6	61.76	462.12	61.90	61.2	60.9	60.7
$\frac{28}{40}$	$\frac{29}{27}$	$\frac{50}{16}$	$\frac{45}{11}$	$\frac{429}{75}$	$\frac{383}{EP}$	$\frac{415}{75}$	$\frac{49}{12}$	$\frac{52}{19}$	$\frac{54}{40}$

State B'm - Nail in Pepper Tree 52 ft 54+76

61.4	61.0	60.6	61.6	61.0	61.6	61.84	462.22	61.88	61.5	61.4	61.0	60.9	60.9
$\frac{27}{50}$	$\frac{51}{40}$	$\frac{55}{39}$	$\frac{45}{17}$	$\frac{51}{16}$	$\frac{45}{12}$	$\frac{421}{75}$	$\frac{383}{EP}$	$\frac{417}{75}$	$\frac{45}{11}$	$\frac{47}{17}$	$\frac{51}{23}$	$\frac{52}{40}$	$\frac{52}{50}$

61.4	61.1	60.1	60.7	61.5	61.7	61.76	462.22	61.89	61.8	61.5	61.1	60.7
$\frac{42}{50}$	$\frac{50}{40}$	$\frac{60}{21}$	$\frac{54}{20}$	$\frac{46}{14}$	$\frac{44}{11}$	$\frac{429}{75}$	$\frac{383}{EP}$	$\frac{416}{75}$	$\frac{43}{11}$	$\frac{46}{17}$	$\frac{50}{28}$	$\frac{54}{50}$

460.92	541.67	461.35	459.60
$\frac{613}{50}$	$\frac{438}{35}$	$\frac{470}{75}$	$\frac{625}{65}$
Flower	H. Nail	H. Nail	Flower

61.9	61.8	61.6	61.9	62.09	462.37	62.12	61.8	61.3	61.1	60.7	61.1
$\frac{42}{50}$	$\frac{43}{35}$	$\frac{45}{17}$	$\frac{42}{11}$	$\frac{390}{75}$	$\frac{368}{EP}$	$\frac{393}{75}$	$\frac{43}{12}$	$\frac{48}{17}$	$\frac{50}{23}$	$\frac{54}{40}$	$\frac{50}{50}$

62.7	62.2	62.6	62.1	62.2	62.38	462.57	62.33	62.1	61.5	61.3
$\frac{33}{50}$	$\frac{38}{24}$	$\frac{28}{20}$	$\frac{40}{15}$	$\frac{39}{12}$	$\frac{367}{75}$	$\frac{348}{EP}$	$\frac{372}{75}$	$\frac{40}{11}$	$\frac{46}{21}$	$\frac{48}{50}$

Nail in Pole Joint 56+40

Reduced 4-1-27  
C.W.







60+585

168.90

Culvert Data -  
Drainage - hot particles

Lt.

Rt.

27

Reverse  
this section.

462.9	463.3	463.5	463.7	463.90	463.70	463.7	463.1	462.4	462.2
65	66	74	65	520	8.3	6.8	7.5	8.7	
65	4x	16	15		15	48	150	250	
		Flow	#Wall		Flow				

61

462.7	462.7	462.3	462.7	462.1	462.3	462.3	462.5	462.4	462.6	462.5	462.5
67	67	56	57	56	548	522	545	57	59	55	63
50	36	18	15	11	78	EP	75	11	15	17	21
					EP		EP				50

+50

463.3	463.3	462.1	462.2	463.4	463.5	463.66	463.5	463.4	463.1	463.9	463.2	463.1	462.6
56	56	48	47	55	544	522	542	55	58	50	57	58	51
50	36	19	15	15	75	EP	75	10	14	16	21	24	50
					EP		EP						

62

462.9	462.9	462.1	463.5	463.1	462.9	463.5	463.73	463.5	463.3	463.1	462.1	463.5	462.0	462.3
59	49	48	57	58	55	540	417	545	56	58	48	34	39	45
50	20	21	16	15	10	75	EP	75	10	15	15	18	21	50
						EP		EP						

+50

462.7	462.7	462.3	462.9	463.1	462.9	463.5	463.75	463.5	463.3	463.2	463.6	463.8	462.5
42	42	44	50	58	55	540	515	543	56	57	57	43	41
50	35	19	13	13	10	75	EP	75	11	12	15	18	45
						EP		EP					50

63

462.4	462.1	462.4	463.9	463.1	462.9	463.5	463.76	463.6	463.9	463.2	462.1	463.5	462.1	464.3
45	48	45	50	50	55	541	514	550	55	57	48	47	48	45
50	7	16	12	13	10	75	EP	75	11	15	15	20	34	50
						EP		EP						

+50

462.4	462.6	462.5	462.1	462.0	463.0	463.4	463.6	463.6	463.9	463.5	462.9	463.1
45	43	54	48	49	59	55	538	515	533	55	54	60
50	26	52	20	14	13	10	75	EP	75	11	15	33
							EP		EP			50

64

462.0	462.1	462.3	462.6	462.5	462.1	463.3	463.5	463.77	463.5	463.9	462.6
49	48	56	49	48	49	57	56	543	513	536	58
50	38	33	30	21	16	15	11	75	EP	75	10
								EP		EP	50

+05

6.17

in Cam. NK 50' Rt.

Red. 4-4-27 8876

R



Bw\*H

468.90

584

463.06

463.12

See P. 11

A.57

167.69

64+50

$\frac{462.4}{53}$   $\frac{463.1}{20}$   $\frac{463.9}{16}$   $\frac{463.1}{15}$   $\frac{463.5}{11}$   $\frac{463.6}{10.9}$   $\frac{467.69}{38.8}$   $\frac{463.6}{10.9}$   $\frac{463.4}{4.3}$   $\frac{463.3}{4.4}$   $\frac{462.9}{4.8}$   $\frac{462.8}{4.9}$   
 $\frac{464.5}{50}$   $\frac{461.3}{33}$   $\frac{461.9}{23}$   $\frac{462.9}{18}$   $\frac{463.5}{10}$   $\frac{463.5}{11.6}$   $\frac{463.76}{39.3}$   $\frac{463.5}{4.1}$   $\frac{463.4}{4.3}$   $\frac{463.2}{4.5}$   $\frac{462.8}{4.9}$   $\frac{462.5}{5.3}$   $\frac{462.4}{5.0}$

+70

$\frac{464.5}{50}$   $\frac{461.3}{33}$   $\frac{461.9}{23}$   $\frac{462.9}{18}$   $\frac{463.5}{10}$   $\frac{463.5}{11.6}$   $\frac{463.76}{39.3}$   $\frac{463.5}{4.1}$   $\frac{463.4}{4.3}$   $\frac{463.2}{4.5}$   $\frac{462.8}{4.9}$   $\frac{462.5}{5.3}$   $\frac{462.4}{5.0}$

+75

$\frac{459.1}{86}$   $\frac{459.8}{70}$   $\frac{461.9}{58}$   $\frac{461.6}{67}$   $\frac{462.7}{50}$   $\frac{463.4}{4.3}$   $\frac{463.5}{4.20}$   $\frac{463.71}{39.8}$   $\frac{463.5}{4.1}$   $\frac{463.3}{4.4}$   $\frac{462.9}{4.8}$   $\frac{462.4}{5.3}$   $\frac{461.4}{6.3}$   $\frac{461.1}{6.5}$   
PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20 PT 2.20

+83

$\frac{462.7}{50}$   $\frac{462.3}{24}$   $\frac{463.4}{10}$   $\frac{463.5}{4.20}$   $\frac{463.74}{39.4}$   $\frac{463.5}{4.1}$   $\frac{463.4}{4.3}$   $\frac{462.6}{5.1}$   $\frac{462.1}{16}$   $\frac{462.3}{17}$   $\frac{462.3}{17}$

65719

\* Victoria St.

$\frac{463.5}{2.2}$   $\frac{463.4}{4.3}$   $\frac{463.4}{4.3}$   $\frac{463.7}{4.0}$   $\frac{463.5}{4.15}$   $\frac{463.71}{39.8}$   $\frac{463.5}{4.15}$   $\frac{463.3}{4.4}$   $\frac{463.3}{4.4}$   $\frac{462.2}{5.5}$   $\frac{461.5}{6.2}$   $\frac{461.0}{6.7}$   $\frac{460.3}{7.4}$   
200 100 50 11 85 80 65 60 70 30 50 100 150

+50

$\frac{462.3}{50}$   $\frac{461.9}{18}$   $\frac{462.2}{55}$   $\frac{463.3}{4.4}$   $\frac{463.5}{4.19}$   $\frac{463.73}{39.6}$   $\frac{463.5}{4.25}$   $\frac{463.3}{4.4}$   $\frac{462.7}{5.0}$   $\frac{461.8}{5.9}$   $\frac{461.3}{6.4}$   $\frac{461.2}{6.5}$

66

$\frac{462.4}{53}$   $\frac{462.3}{17}$   $\frac{462.9}{15}$   $\frac{463.5}{4.2}$   $\frac{463.6}{4.12}$   $\frac{463.77}{39.2}$   $\frac{463.4}{4.25}$   $\frac{463.2}{4.5}$   $\frac{462.5}{5.2}$   $\frac{461.6}{6.1}$   $\frac{461.2}{6.5}$   $\frac{461.5}{6.2}$   $\frac{462.3}{5.9}$   $\frac{462.0}{5.7}$

Red. U-4-27 8876.

R



66+24

467.69

Convert-

+50

67

+50

7.51

470.94

4.26

463.43

68

+50

69

+50

$\frac{463.2}{50}$   $\frac{463.7}{43}$   $\frac{463.0}{21}$   $\frac{461.4}{6.3}$   $\frac{463.0}{4.65}$   $\frac{463.4}{4.3}$   $\frac{467.69}{4.7}$   $\frac{463.76}{39.3}$   $\frac{463.5}{4.15}$   $\frac{462.3}{4.4}$   $\frac{461.0}{4.7}$   $\frac{461.3}{4.69}$   $\frac{461.5}{4.7}$   $\frac{461.3}{4.69}$   $\frac{461.5}{4.7}$

$\frac{463.3}{50}$   $\frac{463.1}{24}$   $\frac{462.1}{20}$   $\frac{463.1}{17}$   $\frac{462.8}{16}$   $\frac{463.3}{11}$   $\frac{463.5}{8.5}$   $\frac{463.66}{4.03}$   $\frac{463.4}{4.2}$   $\frac{463.2}{10}$   $\frac{461.9}{7}$   $\frac{463.5}{31}$   $\frac{461.6}{50}$

$\frac{463.3}{50}$   $\frac{463.4}{43}$   $\frac{462.9}{27}$   $\frac{463.4}{18}$   $\frac{463.6}{17}$   $\frac{463.5}{12}$   $\frac{463.7}{8.5}$   $\frac{463.70}{39.3}$   $\frac{463.4}{4.2}$   $\frac{463.3}{4.4}$   $\frac{463.4}{4.5}$   $\frac{461.3}{16}$   $\frac{461.5}{26}$   $\frac{461.3}{30}$   $\frac{461.5}{37}$   $\frac{462.1}{40}$

$\frac{463.3}{50}$   $\frac{463.4}{43}$   $\frac{462.9}{27}$   $\frac{463.4}{18}$   $\frac{463.6}{17}$   $\frac{463.5}{12}$   $\frac{463.7}{8.5}$   $\frac{463.82}{39.3}$   $\frac{463.5}{4.2}$   $\frac{463.5}{4.4}$   $\frac{463.5}{4.5}$   $\frac{461.7}{16}$   $\frac{461.5}{26}$   $\frac{461.3}{30}$   $\frac{461.5}{37}$   $\frac{462.8}{40}$

$\frac{464.2}{50}$   $\frac{463.6}{43}$   $\frac{463.8}{27}$   $\frac{463.9}{18}$   $\frac{463.4}{17}$   $\frac{463.8}{12}$   $\frac{470.94}{8.5}$   $\frac{464.19}{6.75}$   $\frac{463.9}{6.96}$   $\frac{463.8}{7.1}$   $\frac{463.0}{7.9}$   $\frac{463.8}{7.1}$   $\frac{462.9}{8.0}$   $\frac{464.5}{6.4}$   $\frac{464.9}{6.0}$

$\frac{464.2}{50}$   $\frac{464.4}{43}$   $\frac{464.6}{27}$   $\frac{463.8}{18}$   $\frac{464.4}{17}$   $\frac{464.7}{12}$   $\frac{464.93}{6.01}$   $\frac{464.6}{6.2}$   $\frac{464.5}{6.4}$   $\frac{464.2}{5.9}$   $\frac{464.7}{6.2}$   $\frac{464.3}{6.6}$   $\frac{464.0}{6.4}$   $\frac{464.5}{6.4}$   $\frac{464.9}{6.0}$

$\frac{464.6}{50}$   $\frac{464.4}{43}$   $\frac{464.6}{27}$   $\frac{464.7}{18}$   $\frac{464.3}{17}$   $\frac{464.5}{12}$   $\frac{465.77}{6.23}$   $\frac{465.5}{6.4}$   $\frac{465.4}{6.4}$   $\frac{465.6}{5.9}$   $\frac{466.0}{6.2}$   $\frac{466.0}{6.6}$   $\frac{467.7}{6.0}$   $\frac{467.9}{6.0}$

$\frac{464.7}{50}$   $\frac{464.6}{43}$   $\frac{464.2}{27}$   $\frac{464.8}{18}$   $\frac{464.7}{17}$   $\frac{464.9}{12}$   $\frac{466.49}{6.25}$   $\frac{466.2}{6.4}$   $\frac{466.3}{6.4}$   $\frac{466.4}{5.9}$   $\frac{466.0}{6.2}$   $\frac{466.3}{6.6}$   $\frac{467.5}{6.0}$   $\frac{467.7}{6.0}$

Red. 4-4-27. E.B.H.





70

470.94

+50

71

+50

B.M. #8

2.96

471.02

2.96

467.98

468.06

State B.M.

- See Pg. 11. (Inst. out of adjustment.)

T.P.

5.98

475.47

1.53

469.49

On C.H.C. Monument SW Cor. E1 Cajon & Lois

71+99.12 =

71+99.62

4.75

470.74

marked

469.74

Station Pole NE Cor. Lois

72+50

$\frac{473.4}{2.1}$   $\frac{471.9}{3.6}$   $\frac{470.9}{1.6}$   $\frac{471.3}{4.2}$   $\frac{470.6}{4.9}$   $\frac{470.4}{5.14}$   $\frac{475.47}{4.91}$   $\frac{470.56}{5.13}$   $\frac{470.4}{5.2}$   $\frac{470.3}{5.4}$   $\frac{470.4}{5.1}$   $\frac{470.4}{5.1}$   $\frac{470.4}{5.1}$   $\frac{469.0}{6.5}$   
 $\frac{150}{50}$   $\frac{100}{50}$   $\frac{50}{38}$   $\frac{15}{15}$   $\frac{8}{8}$   $\frac{8}{8}$   $\frac{7}{7}$   $\frac{10}{10}$   $\frac{14}{14}$   $\frac{10}{10}$   $\frac{100}{100}$   $\frac{200}{200}$

$\frac{470.9}{4.6}$   $\frac{470.9}{4.6}$   $\frac{470.8}{4.7}$   $\frac{470.9}{4.55}$   $\frac{471.6}{4.37}$   $\frac{470.9}{4.52}$   $\frac{470.8}{4.7}$   $\frac{471.2}{4.5}$   $\frac{471.5}{4.04}$   
 $\frac{50}{50}$   $\frac{16}{16}$   $\frac{10}{10}$   $\frac{7}{7}$   $\frac{8}{8}$   $\frac{7}{7}$   $\frac{10}{10}$   $\frac{50}{50}$

Red. 4-11-27. E.B.F.

(15)

$\frac{466.9}{0.1}$   $\frac{466.4}{2.1}$   $\frac{466.0}{1.9}$   $\frac{466.7}{1.1}$   $\frac{466.9}{2.9}$   $\frac{470.94}{3.74}$   $\frac{466.9}{3.95}$   $\frac{466.8}{4.1}$   $\frac{466.0}{4.9}$   $\frac{466.1}{4.8}$   $\frac{466.1}{4.9}$   $\frac{467.4}{3.5}$   $\frac{467.5}{3.0}$   
 $\frac{467.3}{3.0}$   $\frac{466.6}{4.3}$   $\frac{467.6}{3.3}$   $\frac{467.8}{3.13}$   $\frac{468.03}{2.9}$   $\frac{467.7}{3.15}$   $\frac{467.6}{3.3}$   $\frac{466.6}{4.3}$   $\frac{466.5}{4.4}$   $\frac{467.2}{3.7}$   $\frac{467.4}{3.5}$   
 $\frac{467.6}{3.3}$   $\frac{467.6}{3.3}$   $\frac{467.7}{3.2}$   $\frac{468.4}{3.5}$   $\frac{468.6}{2.3}$   $\frac{468.86}{2.58}$   $\frac{468.6}{2.28}$   $\frac{468.5}{2.0}$   $\frac{467.1}{3.8}$   $\frac{466.9}{4.0}$   $\frac{467.6}{3.3}$   $\frac{467.6}{3.3}$   
 $\frac{468.3}{2.6}$   $\frac{469.2}{2.7}$   $\frac{468.7}{2.2}$   $\frac{469.1}{1.8}$   $\frac{469.3}{1.57}$   $\frac{469.61}{1.33}$   $\frac{469.3}{1.57}$   $\frac{469.3}{1.6}$   $\frac{468.9}{2.0}$   $\frac{467.9}{3.0}$   $\frac{468.0}{2.9}$   $\frac{468.4}{2.7}$   $\frac{468.7}{2.0}$



73

475.47

+50

2.13 473.34

8.20 481.54

74

+50

75

+50

76

+50

L.

R.

$\begin{array}{r} 471.1 \\ 38 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 471.6 \\ 39 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 471.5 \\ 40 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 470.9 \\ 46 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 471.7 \\ 38 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 471.8 \\ 37 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 475.47 \\ 471.92 \\ 355 \\ \hline 471.7 \\ 376 \\ \hline 471.5 \\ 40 \\ \hline 471.3 \\ 37 \\ \hline 471.8 \\ 34 \\ \hline 472.1 \\ 30 \\ \hline 50 \end{array}$

$\begin{array}{r} 473.8 \\ 17 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 473.3 \\ 21 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 472.8 \\ 27 \\ \hline 45 \end{array}$ 
 $\begin{array}{r} 472.5 \\ 30 \\ \hline 16 \end{array}$ 
 $\begin{array}{r} 472.0 \\ 35 \\ \hline 14 \end{array}$ 
 $\begin{array}{r} 472.5 \\ 30 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 472.6 \\ 256 \\ \hline 7 \end{array}$ 
 $\begin{array}{r} 472.78 \\ 269 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 472.5 \\ 298 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 472.6 \\ 29 \\ \hline 10 \end{array}$ 
 $\begin{array}{r} 472.4 \\ 31 \\ \hline 12 \end{array}$ 
 $\begin{array}{r} 473.2 \\ 23 \\ \hline 15 \end{array}$ 
 $\begin{array}{r} 473.9 \\ 16 \\ \hline 19 \end{array}$ 
 $\begin{array}{r} 473.9228 \\ 22 \\ \hline 25 \end{array}$

Door sill

$\begin{array}{r} 473.8 \\ 7.1 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 473.9 \\ 7.6 \\ \hline 37 \end{array}$ 
 $\begin{array}{r} 473.5 \\ 8.0 \\ \hline 15 \end{array}$ 
 $\begin{array}{r} 473.3 \\ 8.2 \\ \hline 9 \end{array}$ 
 $\begin{array}{r} 473.3 \\ 8.20 \\ \hline 7 \end{array}$ 
 $\begin{array}{r} 481.54 \\ 473.51 \\ 8.03 \\ \hline 8.50 \end{array}$ 
 $\begin{array}{r} 473.3 \\ 8.2 \\ \hline 11 \end{array}$ 
 $\begin{array}{r} 473.3 \\ 8.2 \\ \hline 13 \end{array}$ 
 $\begin{array}{r} 474.1 \\ 7.5 \\ \hline 15 \end{array}$ 
 $\begin{array}{r} 474.9 \\ 6.5 \\ \hline 21 \end{array}$ 
 $\begin{array}{r} 474.5 \\ 7.0 \\ \hline 37 \end{array}$ 
 $\begin{array}{r} 474.5 \\ 7.0 \\ \hline 50 \end{array}$

$\begin{array}{r} 476.5 \\ 12 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 475.3 \\ 62 \\ \hline 37 \end{array}$ 
 $\begin{array}{r} 475.2 \\ 63 \\ \hline 33 \end{array}$ 
 $\begin{array}{r} 474.5 \\ 70 \\ \hline 12 \end{array}$ 
 $\begin{array}{r} 474.1 \\ 74 \\ \hline 12 \end{array}$ 
 $\begin{array}{r} 474.1 \\ 73.6 \\ \hline 7 \end{array}$ 
 $\begin{array}{r} 474.39 \\ 71.5 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 474.1 \\ 73.5 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 474.2 \\ 73 \\ \hline 11 \end{array}$ 
 $\begin{array}{r} 474.3 \\ 72 \\ \hline 13 \end{array}$ 
 $\begin{array}{r} 475.0 \\ 6.5 \\ \hline 14 \end{array}$ 
 $\begin{array}{r} 475.7 \\ 5.5 \\ \hline 26 \end{array}$ 
 $\begin{array}{r} 475.9 \\ 5.5 \\ \hline 31 \end{array}$ 
 $\begin{array}{r} 475.6 \\ 5.0 \\ \hline 50 \end{array}$

$\begin{array}{r} 478.2 \\ 3.3 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 478.0 \\ 3.5 \\ \hline 23 \end{array}$ 
 $\begin{array}{r} 477.3 \\ 4.2 \\ \hline 15 \end{array}$ 
 $\begin{array}{r} 475.2 \\ 6.3 \\ \hline 12 \end{array}$ 
 $\begin{array}{r} 474.9 \\ 6.59 \\ \hline 7 \end{array}$ 
 $\begin{array}{r} 475.19 \\ 6.35 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 474.9 \\ 6.57 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 475.0 \\ 6.5 \\ \hline 13 \end{array}$ 
 $\begin{array}{r} 476.0 \\ 5.5 \\ \hline 14 \end{array}$ 
 $\begin{array}{r} 477.0 \\ 4.5 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 477.0 \\ 4.5 \\ \hline 35 \end{array}$ 
 $\begin{array}{r} 476.6 \\ 4.9 \\ \hline 50 \end{array}$

$\begin{array}{r} 4800 \\ 1.66 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 479.9 \\ 1.6 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 479.8 \\ 1.7 \\ \hline 35 \end{array}$ 
 $\begin{array}{r} 478.8 \\ 2.7 \\ \hline 19 \end{array}$ 
 $\begin{array}{r} 477.5 \\ 4.0 \\ \hline 13 \end{array}$ 
 $\begin{array}{r} 475.8 \\ 5.7 \\ \hline 12 \end{array}$ 
 $\begin{array}{r} 475.6 \\ 5.9 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 475.88 \\ 5.6 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 475.6 \\ 5.9 \\ \hline 8 \end{array}$ 
 $\begin{array}{r} 475.8 \\ 5.7 \\ \hline 13 \end{array}$ 
 $\begin{array}{r} 476.5 \\ 5.0 \\ \hline 14 \end{array}$ 
 $\begin{array}{r} 476.9 \\ 4.6 \\ \hline 19 \end{array}$ 
 $\begin{array}{r} 476.5 \\ 5.1 \\ \hline 30 \end{array}$ 
 $\begin{array}{r} 476.0 \\ 5.5 \\ \hline 50 \end{array}$

$\begin{array}{r} 478.8 \\ 2.69 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 478.6 \\ 2.9 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 478.3 \\ 3.2 \\ \hline 38 \end{array}$ 
 $\begin{array}{r} 476.2 \\ 5.3 \\ \hline 11 \end{array}$ 
 $\begin{array}{r} 476.4 \\ 5.13 \\ \hline 7 \end{array}$ 
 $\begin{array}{r} 476.65 \\ 4.89 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 476.4 \\ 5.16 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 476.4 \\ 5.1 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 475.8 \\ 5.5 \\ \hline 35 \end{array}$ 
 $\begin{array}{r} 475.5 \\ 6.0 \\ \hline 50 \end{array}$

$\begin{array}{r} 477.8 \\ 3.7 \\ \hline 50 \end{array}$ 
 $\begin{array}{r} 476.9 \\ 4.6 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 476.9 \\ 4.6 \\ \hline 15 \end{array}$ 
 $\begin{array}{r} 477.1 \\ 4.39 \\ \hline 7 \end{array}$ 
 $\begin{array}{r} 477.34 \\ 4.20 \\ \hline 28 \end{array}$ 
 $\begin{array}{r} 477.1 \\ 4.5 \\ \hline 16 \end{array}$ 
 $\begin{array}{r} 477.0 \\ 4.5 \\ \hline 16 \end{array}$ 
 $\begin{array}{r} 476.5 \\ 5.0 \\ \hline 20 \end{array}$ 
 $\begin{array}{r} 475.3 \\ 6.2 \\ \hline 25 \end{array}$ 
 $\begin{array}{r} 475.0 \\ 6.5 \\ \hline 50 \end{array}$

Red. 4-4-27. 8B26.

Ⓚ



76+87

481.54

77

8.32 485.71

+50

+68

6.60 479.1

78

+50

78+20

7.22 478.5

BW# 9

5.23 480.48 480.42

Cont'd in Bk# 310/1

Lt.

Rt.

$\frac{33}{50}$	$\frac{42}{31}$	$\frac{60}{24}$	$\frac{45}{20}$	$\frac{44}{16}$	$\frac{393}{7}$	$\frac{481.54}{477.86}$	$\frac{388}{8}$	$\frac{472}{16}$	$\frac{63}{16}$	$\frac{66}{36}$	$\frac{62}{50}$	$\frac{78}{750}$
Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow

$\frac{36}{50}$	$\frac{44}{31}$	$\frac{43}{15}$	$\frac{37}{27}$	$\frac{384}{27}$	$\frac{478.1}{477.5}$	$\frac{475.7}{475.6}$
Flow	Flow	Flow	Flow	Flow	Flow	Flow

$\frac{72}{50}$	$\frac{78}{34}$	$\frac{79}{16}$	$\frac{75}{15}$	$\frac{697}{7}$	$\frac{676}{8}$	$\frac{698}{8}$	$\frac{72}{12}$	$\frac{89}{26}$	$\frac{90}{50}$	$\frac{849}{50}$
Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow

43' left of ± - Conc Walk

50  
Conabase  
of Gas pump.

$\frac{58}{50}$	$\frac{67}{15}$	$\frac{615}{7}$	$\frac{595}{60}$	$\frac{479.6}{610}$	$\frac{479.4}{63}$	$\frac{477.7}{80}$	$\frac{477.9}{78}$
Flow	Flow	Flow	Flow	Flow	Flow	Flow	Flow

$\frac{480.34}{517}$	$\frac{480.3}{541}$	$\frac{480.2}{515}$	$\frac{478.8}{69}$	$\frac{478.7}{70}$
Flow	Flow	Flow	Flow	Flow

50' Rt = Conc Walk

See Pg. 11 Gradually lowered -  
u.b.

Red. 11-11-27. EBB

(\*)



# Ax4 Box Culvert

Sta - 38+97

~~BM# E 428.94~~

See Pg. 10 -

~~0.34 429.78~~

~~7.32 425.01 11.59 417.69~~

~~Stk. El. Grd El.~~

~~"A" 9.00 416.01 416.50~~

~~B 7.73 417.48 415.00~~

~~8.25 416.76~~

≠ Elev - on hub -

BM# E 428.94

See Pg. 10

0.31 429.45

3.76 425.93 7.08 422.17

"A" 10.05 415.88 415.00

B 8.51 417.42 416.50

3.16 422.77

7.21 429.98

10.3 428.95 428.94

BM# E.



46972

540.06

Brass cap in wall of Bldg 4<sup>±</sup>  
above side walk near S W Cor  
New Drive + Lookout

B<sup>th</sup> El = 427.87

142 hrs on f. line 68' Lt. 39+64

B<sup>th</sup> El = 458.84

On 4<sup>th</sup> floor Lt. 35+58.02

B<sup>th</sup> El = 458.96

on last 6' under (P. 1. 56 46+98.02)

B<sup>th</sup> El 463.51

Nail in S Side Pepper 52' Lt 54+76  
2'± above pipe

40.06  
39.76  
30