

1995

MEMORANDUM
FIELD BOOK

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

1995

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

1849

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page #69

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1 1/2 see inside of back cover.
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1844

Cross Sec Wabash Blvd Sec 47 109 to 219 1-47 37
" " 40th St. Lander to Highman 48-50 67
Levels Wabash Blvd Broadway to Market 51-52
Add. Levels 40th Lander to Highman 53-60
Wabash Blvd Sec 8 Line Change 5+92 to 9+48 61-64 54
Survey Lot 28 + 24 Block 5 San Diego Land to 65 66
Cross Sec Wetherby St La Jolla Blvd to Calif St 66-69 68
Prop Storm Drain University Ave 38th to 46th 70-74
Cross Sec 40th St " " North 75-77 91
5

Wabash "L" Line & Profile - Control Levels

Sept. 25, 1948
Sommer
McCoy
W. Moore
Bunch

112+00

111+50

111+42 For Profile 4.07 73.70
T.P.
111+31 1.66 77.77 12.35 76.11

111+00 This is last section in Field Book #1844

110+50

110+00

7.12

T.P.
109+80 7.12 88.46 - 81.34

Continued from BK #1844

Note: From Sta. 53+53.71 NORTH - RT & LT. ARC + ABOVE & - BELOW &

INDEXED

W.K.

OCT 4 1948

Oct. 21, 1948

X-sections
Sisson
Buckner
Bible
Clark
Garrett

RT.

1

69.8	66.6	68.5	69.3	69.5	69.07	61.7	100.2	119.3	122.5	131.2
+10	+0.3	-1.4	+1.0	+1.3	8.31	+1.4	+2.2	+2.1	+5.2	+6.76
105	92	90	90	93	16	22	23	25	26	116
100	77	67	48	8	77.77	119	42	66	97	108
-6.5	-6.7	-9.2	-7.1	-7.9	-12.35	+6.1	+7.2	+4.6	+5.2	+5.9
105	78	75	55	9	31	54	66	80	105	
					79.23					
					7.23					
					86.22					
					2.24					
					83.37					
					5.09					
					88.46					

115+00

114+50

114+00

113+50

113+00

112+50

77.77

14.8	16.3	16.8	16.0	75.95	16.3	19.6	92.0
-1.2	+0.3	+0.8	0.0	1.82	+0.3	+3.6	+16.0
103	84	52	24		30	72	110

12.6	14.3	13.7	15.3	15.02	14.8	14.8	87.3	107.8
-2.4	-0.7	-1.3	+0.3	2.75	-0.2	-0.2	+12.8	+32.8
104	86	48	38		33	34	86	124

71.0	71.3	73.4	73.6	73.41	73.8	72.5	87.4	107.6
-2.4	-2.1	0.0	+0.2	4.36	+0.4	-0.9	+19.4	+34.2
110	91	85	42		15	40	28	117

Bottom of wash

71.4	70.5	72.3	73.3	72.31	72.6	71.3	98.4	123.5
-0.9	-1.2	0.0	+1.0	5.46	+0.3	+5.0	+26.1	+51.2
107	96	70	40		40	76	86	137

Bottom of wash

71.4	70.0	71.9	72.6	71.07	72.0	81.9	102.3	130.2
+0.3	-1.1	+0.3	+1.4	6.70	+0.9	+10.8	+31.2	+59.1
117	74	68	30		28	38	85	142

Bottom of wash

70.4	69.6	71.2	71.6	71.64	71.0	70.8	76.4	96.5	116.8
-1.2	-2.0	-0.4	0.0	6.13	-0.6	-0.8	+6.2	+24.9	+52
103	74	58	22		10	28	33	60	73

Bottom of wash

77.77

131.7

118+00

117+50

117+00

116+50

116+00

T.P. 9.83 85.09 2.51 75.26

115+50

77.77

3

81.0	80.0	80.3	79.86	80.1	78.4	78.1	81.3	83.4
+1.1	+0.1	+0.4	5.23	+0.2	-1.5	-1.2	+1.4	+3.5
110	68	34		46	52	78	88	125

80.3	79.9	79.9	79.46	79.5	78.1	81.1
+0.8	+0.4	+0.4	5.63	0.0	-0.8	+2.2
108	74	37		40	70	104

78.2	79.1	78.9	79.11	78.8	79.4	79.1
-0.7	0.0	-0.2	5.98	-0.3	+0.3	+0.6
103	60	24		45	82	108

78.5	78.5	78.9	78.1	78.60	78.1	78.2	80.9
-0.1	-0.1	+0.3	-0.5	6.47	-0.5	-0.4	+2.3
105	90	66	30		43	81	108

78.4	77.9	78.2	77.3	77.93	77.1	78.2	87.7
+0.5	0.0	+0.3	-0.5	7.16	-0.2	+1.3	+2.8
102	84	50	23	85.49	40	86	107

77.1	77.5	77.3	76.5	75.26	76.6	75.3	80.4	80.6
+1.8	+2.2	+2.0	+1.2	2.51	+1.3	0.0	+5.1	+14.3
100	73	47	20		24	38	91	110

77.77

121+00
T.P. stake 12.89 107.42 1.29 94.62

121+00

120+50

120+00

T.P. 12.25 95.91 1.43 83.66

119+50 Stake + tack. Found in

119+00

118+50

85.09

4

85.1 85.3 88.1 93.07 98.0 99.3 108.1
-80 | -78 | -44 | 2.84+49 | +62 | +156
105 | 80 | 36 | 39 | 59 | 108

83.1 85.2 88.7 90.16 93.3 93.6 94.2 96.0
-65 | -50 | -15 | 5.75 | +34 | +34 | +40 | +58
103 | 62 | 28 | 37 | 59 | 94 | 102

84.1 83.6 84.7 81.0 87.72 89.0 88.8 89.5 90.5 91.0
-36 | -41 | -30 | -07 | 8.19 | +13 | +21 | +12 | +22 | +38
100 | 60 | 22 | 16 | 95.91 | 30 | 50 | 57 | 72 | 106

82.6 82.4 82.5 83.65 85.1 83.1 85.1 88.1
-12 | -13 | -12 | 1.44 | +14 | 00 | +12 | +60
106 | 75 | 32 | 30 | 33 | 68 | 106

81.7 80.0 81.5 81.70 81.9 83.9 82.1 88.1
00 | -12 | -02 | 3.37 | +02 | +22 | +02 | +70
107 | 75 | 28 | 30 | 47 | 50 | 109

80.9 79.1 79.6 80.61 80.8 78.6 80.8 85.3
+02 | -02 | -12 | 3.48 | +02 | -20 | +02 | +47
100 | 77 | 32 | 25 | 28 | 75 | 100

85.09

123+50

123+00

122+47³³ E.C. (Red on 1/2)
 T.P. rock 12.96 119.12 1.06 106.36

122+50

122+00

121+50

107.42

97.1 101.4 110.2 112.4 114.3 113.3 114.9
 -153 112 -22 6.71 +1.9 +0.9 +2.5
 108 61 31 43 47 76

94.1 97.2 102.6 107.9 109.38 112.1 113.4 114.9
 -153 122 -74 -24 9.14 +24 +32 +49
 106 79 53 26 34 68 105

92.1 97.1 105.9 108.22 111.1 112.0 114.4
 -155 114 -22 10.90 +22 +32 +62
 111 61 29 119.12 16 52 107

90.5 95.9 100.1 105.73 109.5 110.4 110.3
 -152 98 -52 1.69 +32 +42 +46
 109 62 28 22 40 107

88.8 91.0 94.7 98.6 100.37 107.5 107.9 112.8
 -122 102 -62 -24 6.45 +65 +62 +118
 105 63 35 15 33 39 107

84.6 87.8 91.4 94.33 101.1 107.0 107.6 108.6
 -112 86 -52 11.03 +42 +106 +112 +122
 104 60 28 21 48 66 106

107.42

126+00

90.6	90.3	91.4	101.6	113.00	119.2	121.5	128.4
-224	-227	-216	-114	6.12	+62	+85	+153
104	61	39	26		17	64	115

East Edge
of Wash

125+70 P.O.T. 1/2

89.8	89.9	90.5	101.7	115.38	119.0	119.8	123.6	126.1
-256	-255	-242	-137	3.74	+36	+44	+82	+102
150	72	49	27		8	30	82	112

East Edge
of Wash

125+50

88.0	90.9	91.7	95.3	110.6	113.23	118.0	120.8	125.1
-252	-223	-215	-172	-26	5.89	+48	+76	+112
102	79	57	50	10		22	54	106

125+00

89.6	102.6	112.7	114.5	116.82	118.4	121.7	123.1	125.4
-272	-142	92	-23	2.30	+16	+48	+63	+86
96	79	66	70		22	62	88	98

124+50

104.9	111.4	114.1	115.68	117.5	119.6	124.1
-108	+43	-16	3.44	+18	+39	+82
100	68	31		28	54	100

124+00

99.5	101.6	112.1	114.31	115.7	117.6	116.0	118.3
-148	+122	-22	4.81	+14	+32	+12	+40
106	82	32		33	64	69	100

119.12

119.12

Oct. 22, '48
 Sisson
 Beaker
 299
 Clark
 Garber

7-
 7

128+00

94.5	95.2	95.8	95.4	91.8	92.82	93.7	93.0	94.9	104.7	119.4
+17	+24	+32	+26	-12	5.40	+07	+03	+21	+119	+266
98	78	37	15	11		25	42	50	58	83
				West Edge of wash			East Edge of wash			132.8
										+40.2
										112

127+50

92.7	94.4	94.2	91.4	92.12	93.8	102.1	116.9	130.3
+06	+23	+21	-07	6.10	+13	+102	+242	+382
107	50	16	11		42	52	87	116
			West Edge of wash		East Edge of wash			

127+00 on rock (yellow crayon)

94.2	92.1	92.2	93.1	93.6	92.4	91.27	92.6	101.8	114.5	123.5
+29	+08	+02	+18	+23	+11	6.95	+13	+105	+232	+322
87	74	55	46	21	17		42	51	85	105
					West Edge of wash		East Edge of wash			
02	20.9									
107										

126+65

90.1	94.3	92.8	93.0	91.3	91.46	89.9	98.1	117.1	130.3
+02	+28	+13	+15	-02	6.76	-16	+66	+262	+382
104	91	52	30	38		34	39	83	116
				West Edge of wash		East Edge of wash			

126+40

91.0	92.1	92.7	90.1	89.9	88.39	98.6	104.8	118.2	129.3
+26	+31	+42	+12	+15	9.83	+102	+162	+292	+409
101	66	37	34	11		5	30	55	104
			West Edge of wash		East Edge of wash				
					98.22				

T.P. 4.40 98.22 12.86 94.12

T.P. 0.76 106.98 12.90 106.27

126+15

92.1	90.5	90.4	90.3	110.76	115.8	120.4	123.9	128.7
-187	-203	-204	-205	8.36	+52	+96	+131	+179
103	93	49	36		8	32	70	110
	West Edge of wash		East Edge of wash					

119.12

119.12

130+50

98.9	98.9	96.1	97.4	97.2	97.64	98.4	97.5	96.1	99.1	118.2
+1.3	+1.3	-0.2	-0.2	-0.2	5.74	+0.2	-0.1	-1.5	+1.5	+20.6
105	89	70	45	14		11	25	56	58	87
										122.9 +25.3
										107

130+00

98.0	98.2	97.4	96.0	95.3	95.31	95.0	96.5	93.9	100.0	111.3
+2.2	+2.2	+2.1	+0.2	0.2	8.07	-0.3	+1.2	-1.4	+9.2	+16.8
86	55	34	20	6		10	35	50	58	82
+2.6										122.2 +24.3
100										101
91.9										

129+50

97.6	98.5	98.1	97.6	95.9	96.17	95.4	94.1	94.5	104.4	113.7
+1.4	+2.3	+2.5	+1.1	-0.3	7.21	-0.8	-2.1	-1.7	+8.3	+17.5
105	63	30	16	10		25	28	50	62	78
										122.3 +26.1
										99

129+00

96.8	97.6	96.8	98.1	96.73	96.4	94.2	93.5	110.8	121.2	
+0.1	+0.9	+0.1	+1.1	6.65	-0.3	-2.5	-3.2	+14.1	+24.5	
103	58	34	17		5	13	44	61	85	
										134.3 +37.6
										114

103.38

T.P. stub 6.74 103.38 1.63 96.59

128+57

95.9	96.6	96.6	97.2	96.59	93.4	94.5	112.3	125.8		
-0.7	0.2	0.2	+0.6	1.63	-3.2	-2.1	+15.2	+29.2		
100	80	50	30		4	4.7	69	93		
										+37.6
										101

128+50

95.8	96.3	97.0	96.3	93.57	94.2	110.9	132.9	
+2.2	+2.2	+3.1	+2.2	4.65	+0.6	+17.3	+39.3	
101	61	15	3		4	68	109	
								98.22

98.22

T.P. 9.59 112.22 0.75 102.63

133+13

133+00

132+50

132+00

131+50

131+00

103.38

101.5	103.9	102.9	102.63	99.8	101.2	120.6	132.9
-11	+13	+03	0.75	-28	-14	+180	+303
104	62	26		9	50	78	101

101.4	103.5	102.9	101.5	99.91	99.0	101.0	121.6	137.4
+15	+35	+33	+16	3.47	-02	+11	+217	+375
99	60	30	3		12	42	76	103

103.2	102.1	101.4	100.6	98.5	99.19	100.1	107.8	116.0	127.7
+40	+22	+23	+14	-02	4.19	+02	+86	+168	+285
104	66	45	20	13		30	58	78	109

99.5	99.5	100.3	99.1	98.28	101.0	100.3	102.6	103.8	115.9
+12	+12	+22	+08	5.10	+22	+22	+43	+55	+174
105	95	40	26		7	33	42	57	87
									+256
									104

99.6	99.8	98.8	98.5	97.0	97.69	99.2	100.9	102.2	105.5	121.8
+18	+24	+14	+08	-02	5.69	+15	+32	+45	+78	+244
102	62	48	14	10		7	28	49	64	102

98.5	98.9	97.2	98.5	98.56	97.4	97.7	100.6	98.9	108.7
-01	+03	-14	-01	4.82	-12	-02	+20	+03	+101
100	68	60	48		6	32	44	60	71
									+271
									116

103.38

126.3+271

135+95

107.8	108.5	107.0	108.15	107.9	104.6	104.7	105.0	110.4
-0.4	+0.3	-1.2	1.07	-0.3	-3.6	-3.5	-3.2	+2.2
100	77	40		4	8	50	95	96
								1139+52
								100

135+50

108.9	106.0	106.3	107	106	103.5	104.7	104.0
+1.9	-1.0	-0.7	5.25	-1.0	-3.5	-2.3	-3.0
106	80	28		51	55	80	105

135+00

107.7	106.9	104.6	105.9	105.5	105.51	106.0	103.9	104.0	103.0
+2.2	+1.4	-0.2	+0.3	+1.2	6.71	+0.5	-1.6	-1.5	-2.5
100	80	57	28	6		50	57	90	112

134+50

106.8	105.3	104.3	106.1	106.2	105.07	106.0	102.5	103.0
+1.7	+0.2	-0.8	+1.2	+1.4	7.15	+0.2	-2.6	-2.1
97	70	52	45	8		47	55	115

134+06 1/2 P.O.T.

104.1	104.1	105.3	105.4	104.36	104.5	103.7	101.2	102.2
-0.3	-0.3	+0.2	+1.0	7.86	+0.1	-0.7	-3.2	-2.2
98	67	38	13		15	38	45	108

133+50

102.4	102.7	104.9	104.2	103.7	102.63	102.7	100.0	100.6	119.2
-0.3	0.2	+2.2	+1.5	+1.3	9.53	0.2	-2.7	-2.1	+1.65
140	78	70	46	15		16	25	70	101

112.22

112.22

T.P. 138+43 111.36 135.40 0.102 124.04

138+24

138+00

137+75

T.P. 12.39 124.06 0.55 111.67

137+50

137+00

136+50

136+00

112.22

Note: From Sta. 53+53.71 North - Rt & Lt. are + above & - below

109.4 108.8 106.4 106.7 105.0 105.92 106.4 105.0 105.5 111.6

+35 104 104 92 +22 92 +15 80 +18 71 -07 20 6.30 10 10 54 -09 54 -08 84 +57 90 +152 110

106.8 107.8 107.9 106.8 106.17 106.1 106.2 136.2

+16 100 100 85 +16 85 +17 92 +16 30 6.05 28 -01 28 02 80 +30 115

108.1 108.3 106.9 106.5 108.1 107.77 107.2 109.0 109.6 127.0

+03 100 100 77 +25 77 -09 65 -13 20 +23 15 4.45 10 -06 10 +12 30 +1.8 55 +19.2 98

106.9 106.7 109.2 108.3 110 109.98 111.3 127.3 139.6

-31 100 -33 72 -08 60 -17 25 2.24 28 +1.3 28 +17.3 64 296 100

108.2 109.1 109.2 109.8 111.9 114.42 122.8 131.4 141.7

-62 105 -47 95 -52 68 -46 34 -25 28 7.64 28 24 24 +8.4 24 +120 69 273 96

108.6 109.0 110.2 119.7 120.23 121.1 130.9 142.8

-146 100 -12 49 -100 28 -05 10 3.83 3 26 70.7 58 22.6 100

141+00 P.O.T. 1/4 Hub.

TP □
140+93 2' Rt. 2.93 136.73 1.60 133.80

+50

140+00

139+50

139+00

138+50

135.40

112.8 112.8 115.3 135.0 142.1 149.0
-20.7 -20.7 -18.2 133.46 +1.4 +8.6 +15.5
98 68 38 3.27 23 68 96

136.73

112.8 114.7 128.7 131.7 134.1 139.7 151.5
-19.7 -17.8 -3.8 -0.8 132.52 +1.4 +7.2 +17.0
181 62 34 15 2.88 32 67 101

111.3 112.5 124.9 129.86 132.9 138.1 149.2
-18.6 -17.4 -5.0 129.86 +3.0 +8.2 +17.3
111 78 48 5.54 36 69 104

113.4 112.5 125.2 128.4 132.8 142.8 145.9
-15.0 -15.9 -3.2 128.4 +4.4 +14.4 +17.6
98 70 46 7.00 46 77 105

110.8 112.9 121.3 126.5 132.4 138.9 143.1
-15.7 -13.6 -5.2 126.5 +5.9 +12.4 +16.6
109 59 44 8.90 44 86 129

111.2 112.0 121.8 124.61 126.4 123.6 130.6 144.2
-13.4 -12.6 -2.8 124.61 +1.8 -1.0 +4.0 +17.6
111 47 20 10.79 24 36 54 103

135.40

143 + 0 =

143 + 87

T.P.

10.14 134.22 12.66 124.07

142 + 47 = B.C. Lt.

142 + 30

142 + 00

141 + 65

141 + 31

136.73

117.5	117.4	117.5	117.4		133.6	144.2	152.6
-36	-37	-34	-37	121.05	+12.5	+23	+31.5
114	95	60	30	13.17	28	68	95

134.22

116.9	116.9	116.4		136.0	139.3	145.2	151.2	152.2
-147	-147	-152	131.60	+44	+77	+136	+196	+206
110	80	35	5.13	10	42	64	87	99

113.5	117.2	115.7	118.3		132.60	134.9	142.8	146.8	150.2
-191	-154	-169	-143	132.60	+2.3	+132	+142	+176	
107	88	54	31	21.13	4	58	90	102	

112.7	117.0	115.1	116.8	116.7	120.0	135.6	141.5	153.0	
-152	-109	-128	-111	-112	-29	127.85	+37	+130	+251
102	97	84	50	30	15	8.88	17	59	103

112.4	111.4	115.0	114.1	115.8	117.1	135.3	140.7	144.7	155.0	
-124	134-98	-107	-90	-77	124.78	+105	+159	+199	+30.2	
95	87	78	58	55	23	11.95	16	60	78	112

112.9	114.2	117.4		128.12	134.6	141.7	143.0	152.1
-152	-139	-107		128.12	+6.5	+13.6	+14.9	24.0
100	49	28		8.61	10	40	73	98

136.73

T.R. 2 12.75 146.45 0.52 133.90
145+71

145+50

145+00

144+50

144+00

143+50

134.22

14

121.5 119.3 122.4 128.2 131.0 135.5 137.2 137.2 140.2 143.0
-12.2 -14.1 -11.3 -5.5 -2.7 133.70+1.8 +3.5 +3.5 +6.5 +9.3
101 | 63 58 40 23 0.52 12 36 52 | 78 104

121.1 119.4 125.5 129.3 134.5 141.4 150.9
-11.0 -12.7 -4.6 -2.8 132.13 +2.4 +9.8 +18.8
101 | 64 57 21 2.09 20 53 97 |

120.1 119.0 123.3 124.5 127.08 132.8 150.3 159.3
-7.0 -2.1 -3.8 -2.6 127.08 +5.7 +23.2 +32.2
100 | 78 | 60 18 7.14 17 62 99 |

121.0 121.1 121.5 126.2 134.4 141.9 155.7
-2.2 -2.1 -1.7 123.17 +3.1 +11.2 +18.7 +32.5
100 | 62 30 11.05 16 45 58 | 97

119.6 119.4 119.4 118.0 119.12 +8.6 +23.4 +38.1
70.5 | 74 30 10 15.1 31 71 | 110

117.9 118.0 118.22 120.6 136.4 144.6 152.3
-0.3 -2.2 16.0 +2.4 +18.2 +26.4 +34.1
103 | 76 16.0 10 39 68 | 96

134.22

148+50

148+00

147+50

147+00

146+50 1/2 P.O.C.

146+00

146.45

125.7	126.5	126.6	130.0	139.02	144.4	154.9	166.6	173.3	175.9	
-13 ² / ₁₀₄	-12 ⁵ / ₈₆	-12 ⁴ / ₅₇	-9 ⁰ / ₄₈	7.43	+5 ⁴ / ₁₃	+15 ² / ₃₈	+27 ⁶ / ₆₆	+34 ³ / ₈₉	+36 ⁹ / ₁₀₇	
122.4	124.0	129.4	132.2	138.5	146.2	168.1	175.5			
-16 ¹ / ₁₀₀	-14 ⁵ / ₅₈	-9 ¹ / ₄₅	-6 ³ / ₂₄	7.98	+9 ² / ₂₆	+29 ⁶ / ₇₀	+37 ⁹ / ₁₀₈			
123.5	123.4	121.6	128.8	130.6	140.41	150.5	168.7	172.5		
-16 ² / ₉₇	-17 ² / ₇₀	-18 ³ / ₄₆	-11 ⁶ / ₃₉	-9 ³ / ₂₆	6.04	+10 ¹ / ₂₄	+28 ³ / ₇₀	+32 ¹ / ₉₆		
121.2	122.2	121.2	129.0	131.2	137.59	142.3	156.7	163.7	169.6	
-16 ² / ₉₈	-15 ³ / ₇₂	-16 ³ / ₄₆	-8 ⁶ / ₃₈	-6 ⁴ / ₂₁	8.86	+12 ² / ₁₁	+19 ¹ / ₄₇	+26 ¹ / ₆₈	+32 ² / ₈₈	
121.5	121.9	122.9	124.0	130.9	142.55	157.2	162.3	166.8	169.5	
-21 ¹ / ₁₀₀	-20 ² / ₇₇	-19 ² / ₇₅	-18 ⁶ / ₅₀	-11 ² / ₂₇	3.90	+14 ⁶ / ₃₃	+19 ⁷ / ₅₃	+24 ² / ₈₀	+26 ² / ₁₀₅	
120.6	121.6	123.1	122.9	128.1	130.1	139.33	147.7	153.1	157.9	162.8
-18 ² / ₉₉	-17 ² / ₆₈	-16 ² / ₅₉	-16 ⁴ / ₄₅	-11 ² / ₃₈	-9 ² / ₂₃	7.12	+8 ⁴ / ₂₂	+13 ² / ₃₅	+12 ⁶ / ₅₆	+13 ⁵ / ₁₀₆

146.45

15.1+00

TP

2x2 Hub POC

150+50

5.23 162.56 048 157.30

150+70

+40

150+00

12.99 157.98 1.66 144.99

149+50

149+00

146.45

130.4 137.8 146.5
 -25.5 -18.1 -9.4
 105 | 80 29 155.93
 6.62
 162.55

164.1 174.6 186.6
 +8.8 +18.2 +30.2
 38 74 | 116

129.5 138.0 150.7 157.3
 -27.8 -19.3 -6.6 0.48
 104 | 64 24 457.3
 0.48
 128.6 130.1 147.9
 -28.8 -27.3 -9.5 157.38
 103 | 80 32 0.40 28 47 | 103

section Top obs
 Left out
 162.9 173.3 183.1
 5.6 +16.2 +25.8
 28 47 | 103

166.1 179.5 187.0
 +8.7 +22.1 +29.6
 39 87 | 120

127.4 127.3 129.5 140.0 151.73
 -24.8 -22.2 -11.3 157.78 +9.8 +21.2 +27.2
 107 | 64 35 32 66 | 103

127.4 126.5 124.9 128.9 140.7 144.79
 -17.8 -18.2 -19.2 -15.2 -4.1 1.66 +11.4 +18.8 +22.2 +24.2
 99 | 76 66 58 10 40 73 | 89 111

156.2 163.6 167.5 169.1
 161.5 172.9 178.9

125.2 125.0 127.3 127.4 132.1 134.7
 -16.5 -16.2 -14.2 -14.3 -9.6 -7.9
 103 78 | 73 56 46 29 4.73 +4.5 +19.2 +29.2 +35.8
 12 53 82 | 115

146.45

154+00

153+50

153+00

152+50

152+00

151+50

162.55

143.2	149.6	153.5	155.97	1620	171.7	183.6
-12.8	-6.4	-2.5	6.58	+6.2	+15.2	+27.6
104	91	71		41	80	120

151.0	153.4	154.64	159.2	172.4	183.9
-3.6	-1.8	7.91	+4.6	+17.2	+29.3
100	58		25	83	114

145.2	151.0	156.10	163.3	172.5	182.30
-10.2	-5.1	6.45	+7.2	+16.4	+26.2
104	57		46	85	115

141.8	143.0	146.6	152.2	155.21	162.1	165.6	176.7
-13.4	-12.2	-8.6	-3.0	7.34	+6.2	+10.4	+21.5
101	77	52	23		45	63	100

139.1	141.1	147.3	154.00	162.1	173.4	183.4
-14.9	-12.2	-6.7	8.55	+8.1	+19.4	+29.4
102	77	31		36	84	117

136.5	140.7	147.0	153.75	160.4	170.6	180.8
-17.3	-13.4	-6.2	8.80	+6.6	+16.2	+27.2
100	64	28		19	68	103

162.55

157+00

156+50

T. P. 6.09 163.29 5.35 157.20

156+00

155+50

155+00 Note windrow of dirt on this section. make allowance for

154+50

162.55

138.5	139.5	143.8	155.8	159.20	163.2	171.8	182.3
-20 1/2	-19 1/2	-15 1/2	-3 1/2	4.09	+4 1/2	+12 1/2	+23 1/2
107	91	72	39		35	67	135

135.8	138.5	149.8	155.2	158.18	160.9	163.7	169.4	178.8
-22 1/2	-20 1/2	-8 1/2	-3 1/2	4.81	+2 1/2	+4 1/2	+10 1/2	+20 1/2
107	95	59	35		28	35	63	101
163.29								

138.8	141.3	146.1	154.9	157.20	162.5	166.1	175.3
-18 1/2	-15 1/2	-11 1/2	-2 1/2	5.35	+5 1/2	+8 1/2	+18 1/2
100	90	75	38		39	57	100

137.2	140.5	155.2	156.90	159.8	164.0	172.3	178.8
-19 1/2	-7 1/2	-1 1/2	5.65	+2 1/2	+7 1/2	+15 1/2	+21 1/2
104	70	48		25	43	92	117

140.5	150.7	155.5	157.53	162.5	167.8	177.5
-17 1/2	-6 1/2	-2 1/2	5.02	+5 1/2	+10 1/2	+20 1/2
107	76	50		40	77	118

141.1	153.2	155.3	156.46	163.8	166.6	175.7
-15 1/2	-3 1/2	-1 1/2	6.09	+7 1/2	+10 1/2	+19 1/2
107	102	72	45	54	62	98

162.55

159+50

Outs

159+00

T.P. 1.69 151.97 13.01 150.28

158+75

158+50 P.O.C. 1/2 Hub.

158+00

157+50

163.29

142.6	143.0	140.9	141.6	143.62	157.0	166.3	176.4
-1.9	-0.4	-2.7	-2.0	8.35	+13.4	+22.7	+32.2
113	93	50	20		53	73	107

141.3	140.6	140.8	140.26	159.2	165.5	171.5	178.6
-8.0	-8.7	-8.5	2.71	+9.9	+15.2	+22.7	+29.3
108	78	25		31	50	79	106

151.97

140.5	140.0	145.2	155.02	160.4	169.6	180.4	
-14.5	-15.0	-9.8	8	27	5.4	+14.6	+25.4
100	67	37		15	75	109	

140.3	139.8	139.0	138.9	142.1	157.3	159.54	162.8	167.9	175.8	182.6
-19.2	-19.7	-20.5	-20.6	-17.4	-2.9	3.75	+9.9	+8.4	+16.7	+23.4
107	95	90	80	63	14		25	66	88	112

140.2	140.3	155.6	157.3	159.71	164.2	172.8	183.9
-19.5	-18.2	-4.2	-2.4	3.58	+4.5	+13.2	+24.2
103	95	60	50		37	81	111

139.8	140.9	149.2	156.0	160.14	162.5	173.8	182.5
-20.8	-19.7	-10.2	-4.1	3.15	+2.4	+13.1	+22.4
113	94	67	42		32	78	105

163.29

162+50

146.6	147.2	150.9	151.6	147.85	148.1	151.9	157.5
-13	-02	+32	+37	4.12	+02	+42	+96
100	67	52	14		40	70	109

162+00

145.2	146.6	146.3	146.60	147.0	151.2	164.2
-14	02	-03	5.37	+04	+46	+176
100	82	36		42	68	118

161+50

144.6	146.1	145.67	145.2	149.0	158.2	174.4
-14	+04	6.30	-05	+32	+125	+287
102	55		26	53	79	114

161+00

143.7	144.2	143.6	145.12	146.1	149.6	168.8	174.7
-14	-02	-15	6.85	+12	+45	+237	+296
102	60	20		32	48	88	108

160+50

143.1	142.5	142.5	142.7	144.07	143.4	149.0	154.6	172.7
-12	-16	-16	-14	7.90	-07	+42	+115	+286
107	91	57	8		23	40	63	104

160+00

141.6	142.1	142.4	140.9	142.92	147.3	155.8	174.5
-12	-02	-05	-22	9.05	+44	+127	+316
100	73	37	15		30	59	101

151.97

151.97

164+25

164+00 210 - P.O.C.

163+82

163+68

163+50

163+15

163+00

T.P. 11.66 162.19 1.44 150.53

162+58

151.97

Note: from Sta. 55+53.71 North - Right Hand are + above & ; - below &

21

150.5	153.1	154.9	157.43	159.6	159.2	162.2
-62	-43	-25	4.76	+22	+12	+42
110	167	40	47	89	118	

152.1	152.7	153.5	155.5	157.13	157.1	158.0	162.2	169.3
-52	-44	-34	-16	5.06	02	+02	+51	+122
112	77	50	21	18	42	83	117	

152.3	153.2	154.4	155.5	155.8	155.6	158.0	158.2	161.0	172.3
-35	-24	-14	-02	6.39	-02	+22	+24	+52	+165
98	80	65	33	17	27	46	78	112	

152.0	153.9	154.3	155.4	157.36	158.0	159.6	166.8
-54	-35	-34	-20	4.83	+06	+22	+94
104	80	68	35	33	78	104	

151.3	151.2	153.8	156.0	156.02	156.9	157.8	163.7
-42	-42	-22	02	6.17	+02	+12	+72
108	95	66	26	30	78	109	

149.8	152.8	154.4	154.48	154.5	155.4	154.5	157.7	152.5	155.1	159.1
-42	-12	-02	154.48	02	+02	02	-22	-22	+02	+42
110	57	31	7.71	16	40	53	57	74	78	109

149.0	151.8	153.4	153.8	152.9	149.3	152.2	157.6
-52	-32	-06	8.21	-11	-42	-12	+32
111	97	35	9	12	75	106	

162.19

146.6	147.1	151.3	151.8	150.53	148.5	149.5	153.9	159.8
-32	-34	+02	+13	1.44	-22	-12	+32	+92
102	75	48	10	6	56	80	106	

151.92

166+00

150.5
-2.8
107
150.1
-3.2
97

165+76

165+50

165+00

Sta 164+75 60' Lt Radial
Cross in
M.H. Rim 45' Lt. 2+60 P' Line
F.B. 1823 - P. 9

8.24 153.95

BM BK 1823-9

154.03

Low 0.25

2+30.59 "P" line
F.B. 1823 - P. 9

6.73 155.46

BM BK 1823-9

155.54

164+50

Power Pole # 2446 23' Lt Radial

162.19

156.8
+3.2
107
22
153.3 153.0 151.9 151.9 150.0 152.1 153.31 153.3 152.5 155.3 155.3 153.6 154.1

+0.2 -0.3 1.3 -1.3 -3.3 -1.2 8.88 +0.9 -0.8 +2.9 +2.9 +0.3 12.3
81 72 67 38 33 26 26 35 45 62 72 85

148.8 151.0 152.8 154.64 154.1 153.3 156.0 157.2
-5.8 -3.4 -1.8 7.55 -0.5 -1.3 +1.4 +2.6
100 166 40 72 62 82 112

148.1 151.6 151.8 153.5 153.97 155.1 156.4 158.1
-5.2 -2.4 -2.2 -0.5 8.22 +1.1 +2.4 +4.4
102 83 66 30 32 85 116

148.7 152.0 152.1 153.3 153.6 155.33 155.7 158.0 167.5
-7.2 -3.3 -3.2 -2.0 -1.2 6.86 +0.4 +2.7 +12.3
100 92 75 50 27 35 80 114

149.9 152.6 154.5 157.23 158.9 161.2 164.0
-7.3 -4.4 -2.2 4.96 +1.2 +4.0 +6.8
115 82 43 30 86 111

162.19

167+50 vtz - P.O.C.

T.P. 10.72 182.04 3.03 171.32

167+00 stub at 166+96 elevation O.R. for 167+00 cut

166+69

Rock 166+43

T.P. 12.99 174.35 0.83 161.36

F.W.

166+30 top of bank

166+25 Bottom of wash

166+20 Bottom of wash

162.19

153.2	153.5	156.1	167.4	173.27	175.2	178.0	158.9	157.9	160.3
-20 ²	-19 ²	-17 ²	-5 ²	8.77	+1 ²	+4 ²	-14 ²	-15 ²	-13 ²
115	71	57	25	<u>182.04</u>	12	54	85	95	102

151.9	153.3	153.8	156.6	167.8	168.50	171.0	172.3	159.7	150.1	157.0	157.3
-16 ²	-15 ²	-14 ²	-11 ²	-0 ²	5.85	+2 ²	+3 ²	-8 ²	-9 ²	-11 ²	-11 ²
102	90	60	43	16	6	28	73	90	93	103	

151.1	153.0	154.9	160.3	161.8	164.9	167.85	167.9	158.2	157.7	156.0	155.7
-16 ²	-14 ²	-13 ²	-7 ²	-6 ²	-3 ²	6.50	+0 ²	-9 ²	-10 ²	-11 ²	-12 ²
105	80	65	43	25	18	5	32	90	93	107	

174.35

151.3	154.0	155.8	156.6	158.16	156.1	155.1	156.5	154.2	155.8	156.7	156.7
-6 ²	-7 ²	-2 ²	-1 ²	4.03	-2 ²	-3 ²	-1 ²	-4 ²	-2 ²	-1 ²	-1 ²
101	84	47	22	17	25	67	71	85	93	110	

151.1	153.7	153.9	154.8	150.6	150.91	151.9	153.4	154.9	156.5	158.7	156.9
+0 ²	+2 ²	+3 ²	+3 ²	-0 ²	11.28	+1 ²	+2 ²	+4 ²	+5 ²	+7 ²	+5 ²
98	78	55	38	25	14	22	47	64	69	110	

162.19

170+00

169+62 = 202 Arb. P.O.C.

169+50

T.P. 4.31 185.40 0.95 181.09

169+00

168+50

168+00

182.04

$\begin{matrix} 158.1 \\ -19^{\circ} \\ 101 \end{matrix}$
 $\begin{matrix} 157.1 \\ -20^{\circ} \\ 96 \end{matrix}$
 $\begin{matrix} 157.3 \\ -19^{\circ} \\ 64 \end{matrix}$
 $\begin{matrix} 156.8 \\ -20^{\circ} \\ 38 \end{matrix}$
 $\begin{matrix} 158.0 \\ -19^{\circ} \\ 50 \end{matrix}$
 177.11
 $\begin{matrix} 184.9 \\ 8.29+7^{\circ} \\ 22 \end{matrix}$
 $\begin{matrix} 191.2 \\ +14^{\circ} \\ 80 \end{matrix}$
 $\begin{matrix} 193.7 \\ +16^{\circ} \\ 106 \end{matrix}$

$\begin{matrix} 156.5 \\ -27^{\circ} \\ 119 \end{matrix}$
 $\begin{matrix} 156.9 \\ -27^{\circ} \\ 86 \end{matrix}$
 $\begin{matrix} 156.2 \\ -27^{\circ} \\ 56 \end{matrix}$
 $\begin{matrix} 170.7 \\ -13^{\circ} \\ 28 \end{matrix}$
 183.35
 $\begin{matrix} 185.6 \\ 1.45+1^{\circ} \\ 8 \end{matrix}$
 $\begin{matrix} 185.4 \\ +1^{\circ} \\ 30 \end{matrix}$
 $\begin{matrix} 190.0 \\ +6^{\circ} \\ 77 \end{matrix}$
 $\begin{matrix} 192.5 \\ +8^{\circ} \\ 116 \end{matrix}$

$\begin{matrix} 159.1 \\ -24^{\circ} \\ 108 \end{matrix}$
 $\begin{matrix} 157.0 \\ -26^{\circ} \\ 81 \end{matrix}$
 $\begin{matrix} 157.2 \\ -26^{\circ} \\ 64 \end{matrix}$
 $\begin{matrix} 157.2 \\ -26^{\circ} \\ 55 \end{matrix}$
 $\begin{matrix} 163.7 \\ -19^{\circ} \\ 44 \end{matrix}$
 183.20
 $\begin{matrix} 185.8 \\ 2.20+2^{\circ} \\ 25 \end{matrix}$
 $\begin{matrix} 188.5 \\ +5^{\circ} \\ 70 \end{matrix}$
 $\begin{matrix} 191.2 \\ +8^{\circ} \\ 109 \end{matrix}$

$\begin{matrix} 154.7 \\ -21^{\circ} \\ 112 \end{matrix}$
 $\begin{matrix} 155.7 \\ -20^{\circ} \\ 90 \end{matrix}$
 $\begin{matrix} 155.3 \\ -21^{\circ} \\ 74 \end{matrix}$
 $\begin{matrix} 155.7 \\ -20^{\circ} \\ 48 \end{matrix}$
 $\begin{matrix} 154.7 \\ -21^{\circ} \\ 38 \end{matrix}$
 $\begin{matrix} 172.9 \\ -3^{\circ} \\ 20 \end{matrix}$
 176.39
 $\begin{matrix} 182.5 \\ 5.65+6^{\circ} \\ 31 \end{matrix}$
 $\begin{matrix} 187.2 \\ +10^{\circ} \\ 78 \end{matrix}$
 $\begin{matrix} 188.4 \\ +12^{\circ} \\ 110 \end{matrix}$

$\begin{matrix} 155.2 \\ -18^{\circ} \\ 113 \end{matrix}$
 $\begin{matrix} 155.9 \\ -18^{\circ} \\ 100 \end{matrix}$
 $\begin{matrix} 153.6 \\ -20^{\circ} \\ 80 \end{matrix}$
 $\begin{matrix} 152.7 \\ -21^{\circ} \\ 60 \end{matrix}$
 $\begin{matrix} 157.8 \\ -16^{\circ} \\ 42 \end{matrix}$
 $\begin{matrix} 172.0 \\ -2^{\circ} \\ 18 \end{matrix}$
 174.06
 $\begin{matrix} 176.5 \\ 7.78+2^{\circ} \\ 12 \end{matrix}$
 $\begin{matrix} 181.4 \\ +7^{\circ} \\ 41 \end{matrix}$
 $\begin{matrix} 183.6 \\ +9^{\circ} \\ 85 \end{matrix}$
 $\begin{matrix} 182.3 \\ +8^{\circ} \\ 105 \end{matrix}$

$\begin{matrix} 153.5 \\ -19^{\circ} \\ 113 \end{matrix}$
 $\begin{matrix} 153.8 \\ -18^{\circ} \\ 74 \end{matrix}$
 $\begin{matrix} 154.7 \\ -18^{\circ} \\ 60 \end{matrix}$
 $\begin{matrix} 170.2 \\ -2^{\circ} \\ 23 \end{matrix}$
 172.69
 $\begin{matrix} 179.6 \\ 7.35+6^{\circ} \\ 36 \end{matrix}$
 $\begin{matrix} 179.6 \\ +6^{\circ} \\ 63 \end{matrix}$
 $\begin{matrix} 161.0 \\ -11^{\circ} \\ 98 \end{matrix}$
 $\begin{matrix} 160.0 \\ -12^{\circ} \\ 109 \end{matrix}$

182.04

172+00

161.2
-2³/₁₀₇
161.1
-2³/₉₈
158.6
-4²/₉₂
160.2
-3²/₉₈
161.4
-2²/₅₈
161.7
-1²/₁₀
163.40
10.85
+3²/₂₀
166.7
+10²/₅₀
174.3
+19²/₇₀
183.0
+27²/₈₈
190.5
+44²/₁₁₈

171+50

159.7
-2⁴/₁₀₂
159.3
-2²/₈₃
160.2
-1¹/₈₀
160.3
-1²/₇₀
159.6
-1²/₆₀
160.6
-0²/₄₅
160.2
-1¹/₁₆
161.33
12.92
+3²/₂₀
165.1
+16²/₅₁
177.9
+32²/₇₅
184.1
+38²/₉₆
200.0

171+29²⁹ E.C. (on N.Y. Hub.)

158.8
-3¹/₁₀₂
159.1
-2²/₉₀
160.5
-1¹/₈₂
159.0
-2¹/₇₃
158.7
-3²/₆₆
160.5
-1²/₅₈
160.1
-1⁸/₃₃
159.0
-2²/₂₀
159.6
-2³/₇
161.93
12.32
+3²/₁₆
164.9
+20²/₅₄
182.6
+26²/₅₈
187.9
+33²/₇₉
194.9
+35²/₁₀₁

171+00

159.0
-7²/₁₀₈
160.4
-6³/₉₃
160.0
-6²/₈₈
159.5
-7²/₆₇
157.7
-9²/₅₆
159.4
-7²/₅₀
159.5
-7²/₃₃
160.0
-6²/₂₆
161.3
-5⁴/₁₅
166.69
7.56
+22²/₄₅
182.4
+27²/₈₅
194.2
+30²/₁₀₀
197.5

170+50

158.6
-11²/₁₀₂
157.9
-12²/₄₄
157.9
-12²/₃₁
160.9
-9²/₂₄
170.52
3.73
+17²/₂₂
187.9
+21²/₇₉
191.5
+25²/₁₀₁
195.7

T.P. =
170+25 0.72 174.25 11.87 173.53

158.3
-15²/₁₀₁
157.6
-15²/₄₉
157.0
-16²/₃₇
161.4
-12²/₂₇
174.25
173.53
+12²/₃₁
186.4
+18²/₈₅
192.0
+21²/₁₀₉
194.8

185.40

177+39.46 - P.O.T. - last stub set.

Smith, T.
Becker
Gamber
Clark

174+18

174+00

BM

13.17

176.73

→ 5.81

163.56

BY 1823-9,
Crisol X 1/4" Film
16" RT 10130" Plane

T.P. ²⁰

3.37

170.92

170.88

Low 2.1

173+50

173+00

172+80

172+50

174.25

Sept. 27, 1948

266

164.0	164.5	166.1	168.6	170.98	172.8	175.5	174.6	176.0	178.0	191.7
-7 ²	-6 ⁵	-4 ²	-2 ²	5.75	+1 ⁵	+4 ⁵	+3 ⁶	+5 ²	+8 ²	+20 ²
107	78	46	39		20	26	46	72	74	118

163.9	163.1	166.8	168.6	173.08	176.0	191.7	191.3	200.3
-9 ²	-10 ²	-6 ³	-4 ⁵	3.65	+2 ²	+8 ⁵	+18 ²	+27 ²
102	75	55	25		36	71	95	127

HI 176.73

163.6	163.0	161.5	165.4	166.7	168.5	170.88	172.9	190.7	209.1	212.4
-7 ²	-7 ²	-9 ¹	-5 ⁵	-4 ²	-2 ²	3.37	+2 ²	+19 ²	+38 ²	+41 ⁵
102	72	56	53	28	21		22	63	97	114

163.1	161.8	161.4	163.8	165.82	167.8	174.4	185.4	195.5	205.0	212.0
-2 ²	+4 ²	-4 ²	-2 ²	8.43	+2 ²	+8 ⁵	+19 ²	+29 ²	+39 ²	+46 ⁵
105	84	48	74		20	40	60	78	95	111

162.8	163.1	161.3	160.7	162.9	163.0	162.76	165.1	169.4	183.3	191.2	198.8	208.5
+0 ²	+0 ²	-1 ⁵	-2 ²	+0 ⁴	+0 ²	11.49	+2 ³	+6 ⁵	+20 ⁵	+28 ²	+36 ²	+45 ²
104	90	85	51	45	22		15	34	60	74	87	107

162.4	162.0	160.4	160.2	161.8	162.07	162.6	166.0	169.0	180.8	190.5	202.6
+0 ²	-0 ⁵	-1 ²	-1 ²	-0 ²	12.18	+0 ⁵	+3 ²	+6 ²	+18 ²	+28 ²	+40 ⁵
108	88	84	60	54		10	16	30	51	72	97

174.25

176+53
TP
176+43 10.80 185.92 1.61 175.12

176+35
save space

176+00

save space

175+50

175+00

174+97 £ Profile

174+70

174+52 POT Hub

17673

169.2
168.2
170.5
169.2
179.20
199.4
207.6
218.1
232.0
231.7
27
-10° -11° -8° -9° 6.64 120° +28° +38° +52° +51°
100 55 51 12 31 46 62 88 97

169.3
167.6
166.3
169.6
169.9
175.12
171.62
181.5
187.9
192.5
208.9
219.1
228.1
229.1
-2° -4° -5° -2° -1° 5.11 19° +16° +20° +37° +47° +65° +75°
107 90 75 64 8 12 26 40 55 71 89 100

169.1
168.5
169.1
168.9
167.92
168.6
181.6
195.6
230.7
+1° +0° +1° +1° 8.81 +0° +13° +27° +62°
100 90 45 4 9 24 49 108

167.2
167.2
168.3
167.5
169.1
168.15
168.0
181.8
195.6
216.4
218.2
-1° -1° +0° -0° +0° 8.58 -0° +13° +27° +48° +50°
104 47 60 27 14 18 34 57 90 105

166.4
165.7
166.5
166.7
165.3
166.8
167.05
171.4
173.1
187.9
196.2
194.2
-0° -1° +0° -0° -1° -0° 9.68 +4° +11° +20° +29° +27°
100 43 34 20 16 13 5 32 47 86 101

165.5
165.5
165.2
166.5
167.4
169.00
171.6
190.0
191.6
183.3
-3° +3° -3° -2° -1° 6.9 7.73 +2° +21° +22° +14°
105 80 55 40 8 10 43 73 103

165.0
165.6
166.3
166.0
167.4
174.99
180.3
186.6
185.6
182.0
180.1
-10° -9° -8° -9° -2° 1.74 +5° +11° +10° +7° +5°
100 70 44 21 11 21 49 76 95 105

17623

178+50

178+00

177+50

177+39⁴⁵ P.O.T.

^{Arch}
T.P. 177+25 403 200.22 0.71 196.19

^{cut A}
177+18

177+0

^{Arch}
T.P. 176+75 11.78 196.90 0.80 185.12

176+75

185.92

170.6 173.2 184.6 2
-20⁰ -17⁰ -6⁰ 9.66 +12⁰ +24⁰ +34⁰ +49⁰
103 59 31 30 58 81 110

171.1 171.7 179.2 184.1 192.34 198.4 213.6 229.6 244.2
-21⁰ -20⁰ -13⁰ -8⁰ 2.88 +6⁰ +21⁰ +37⁰ +51⁰
106 76 62 35 13 47 72 111

170.3 169.7 172.3 186.1 196.55 213.8 225.5 236.2 237.9
+26⁰ -26⁰ -24⁰ -10⁰ 3.67 +17⁰ +28⁰ +39⁰ +41⁰
100 69 64 23 35 63 88 100

171.1 170.2 174.3 182.2 197.29 213.6 224.2 233.0 234.9
+26⁰ -24⁰ -23⁰ -15⁰ 2.93 +16⁰ +26⁰ +35⁰ +37⁰
115 60 55 36 33 56 76 100

171.1 170.9 168.8 186.6 200.22 213.6 231.0 236.5
-24⁰ +24⁰ -26⁰ -0⁰ 1.68 +18⁰ +35⁰ +41⁰
105 97 57 22 34 67 103

170.1 168.4 170.7 189.05 209.4 223.8 231.3 236.8
-19⁰ -20⁰ -18⁰ 7.85 +20⁰ +34⁰ +42⁰ +47⁰
102 52 40 34 55 69 100

169.8 168.2 170.2 170.5 196.90 182.96 195.1 213.4 230.7 233.5
-19⁰ -14⁰ -12⁰ -13⁰ 2.96 +12⁰ +30⁰ +47⁰ +50⁰
102 52 46 26 20 50 75 101

185.92

181725

181700

TP 12.81 211.10 1.93 198.29

180750

180700

179750

179700

200 22

176.5
 $\frac{-24^2}{110}$

177.4
 $\frac{-23^2}{113}$

177.4
 $\frac{-23^2}{103}$

182.5
 $\frac{-18^2}{93}$

185.1
 $\frac{-16^2}{61}$

201.22
 9.83

208.8
 $+7^2$
 19

217.0
 $+15^2$
 34

220.4
 $+29^2$
 67

226.3
 $+35^2$
 85

232.3
 $+31^2$
 89

177.0
 $\frac{-23^2}{91}$

182.7
 $\frac{-18^2}{87}$

184.4
 $\frac{-16^2}{63}$

186.9
 $\frac{-13^2}{56}$

191.0
 $\frac{-9^2}{31}$

200.67
 10.43

216.4
 $+15^2$
 35

232.6
 $+31^2$
 64

235.5
 $+34^2$
 84

232.7
 $+32^2$
 91

232.7
 $+32^2$
 101

211.40

176.4
 $\frac{-21^2}{100}$

177.4
 $\frac{-20^2}{60}$

185.4
 $\frac{-12^2}{46}$

189.1
 $\frac{-9^2}{27}$

198.29
 1.93

208.8
 $+10^2$
 23

220.8
 $+21^2$
 47

234.1
 $+35^2$
 76

233.4
 $+35^2$
 87

230.4
 $+32^2$
 90

230.3
 $\frac{32^2}{100}$

176.4
 $\frac{-18^2}{101}$

175.9
 $\frac{-18^2}{44}$

187.3
 $\frac{-7^2}{31}$

194.38
 5.84

200.8
 $+6^2$
 22

206.6
 $+12^2$
 39

212.8
 $+18^2$
 54

231.6
 $+37^2$
 98

233.6
 $+39^2$
 108

175.2
 $\frac{-17^2}{104}$

174.0
 $\frac{-18^2}{93}$

174.5
 $\frac{-17^2}{33}$

189.4
 $\frac{-2^2}{16}$

192.22
 8.00

200.7
 $+8^2$
 32

208.9
 $+16^2$
 54

217.7
 $+25^2$
 72

221.9
 $+32^2$
 84

234.0
 $+41^2$
 100

174.2
 $\frac{-17^2}{100}$

173.1
 $\frac{-18^2}{93}$

172.4
 $\frac{-19^2}{45}$

175.5
 $\frac{-16^2}{34}$

185.5
 $\frac{-6^2}{30}$

191.75
 8.47

196.9
 $+5^2$
 23

205.5
 $+13^2$
 49

211.9
 $+20^2$
 64

221.2
 $+32^2$
 86

233.5
 $+41^2$
 108

200 22

183+10

183+00

cut 2.51

182+83.43 BCR

182+70

182+50

TP 182+17.91

2.61

213.20

0.51

210.59

182+00

181+50

211.0

30

181.3	182.8	191.3	193.5	190.6	187.95	191.2	196.3	202.4	227.0
-6.2	-5.2	+3.3	+5.5	+2.6	25.25	+3.2	+8.3	+14.3	+39.0
184.3	184.0	188.8	188.6	186.9	187.4	191.55	194.0	199.1	208.9
-7.3	-7.6	-2.2	-3.2	-4.2	-4.2	21.65	+2.2	+4.2	+7.5
179.3	182.0	186.7	187.4	193.5	195.15	205.23	209.8	210.3	218.3
-18.2	-16.3	-11.5	-10.2	-4.2	15.05	+8.3	+11.6	+12.2	+20.2
101	90	76	69	48	24	49	83	86	90

202.72
10.48

180.0	187.2	192.1	194.1	207.6	208.15	214.0	223.2	229.9	233.9	228.8
-28.2	-21.2	-16.1	-14.2	-0.5	5.05	+5.2	+15.2	+21.2	+25.2	+20.4
100	89	57	54	6	29	61	85	97	97	105

180.9	184.9	186.8	190.8	195.0	213.20	210.59	220.2	230.4	237.1	240.0	232.0
-29.2	-25.3	-23.2	-19.2	-15.2	0.57	+9.2	+19.2	+26.2	+29.2	+21.2	+21.2
102	99	77	58	47	28	56	78	90	90	94	104

184.5	189.1	210.56	219.2	230.7	232.6	240.1	232.1
-26.2	-21.5	0.54	+8.2	+20.2	+28.2	+29.2	+21.2
100	59	24	52	78	86	84	104

182.9	185.9	193.2	201.4	205.55	216.4	230.1	239.2	231.2	230.9
-22.2	-19.2	-12.2	-4.2	5.55	+10.2	+29.2	+33.2	+25.2	+25.2
100	62	32	13	28	60	83	89	89	104

211.0

185400

184450

184420

TP ^{Arch} 184416 066 202.02 1184 201.36

184400 ^{Poc.}

183450

183435

213²⁰

Note: From Sta. 53+55.71 North - Rt & Lt are + above & - below

31

186.5	186.1	184.6	185.0	183.0	182.2	189.74	194.9	203.5	214.2	220.6	227.2
-32	-36	-51	-42	-62	-75	12.28	+52	+132	+242	+302	+372
100	73	66	28	15	6	9	27	44	62	85	93

184.1	183.7	183.9	181.9	182.4	186.1	190.87	198.0	203.7	208.5	220.3	227.1	225.0
-68	-72	-72	-92	-85	-42	11.5	+74	+128	+172	+292	+312	+342
73	58	43	31	21	10	10	21	38	69	89	92	102

184.2	183.2	182.6	182.5	183.9	196.4	199.62	208.8	215.1	221.3	226.6
-152	-164	-172	-171	-152	-32	2.40	+92	+152	+212	+272
110	75	60	34	32	9	40	63	87	105	

202.02

184.0	183.2	181.3	182.5	184.8	200.8	202.56	206.5	214.0	218.2	226.3
-182	-192	-213	-202	-172	-12	10.64	+32	+112	+152	+232
110	80	61	45	42	10	27	68	87	103	

181.6	180.9	180.9	183.0	183.5	200.3	202.12	207.1	209.4	203.7	205.7	224.8
-202	-212	-212	-192	-182	-12	11.08	+52	+42	+12	+32	+222
100	81	57	54	48	14	26	45	58	73	106	

180.6	180.5	180.1	200.0	202.44	203.9	202.6	200.2	222.6
-212	-212	-222	-212	10.76	+12	+102	-22	+202
100	97	62	78	21	43	67	108	

213²⁰

18750

18700

18650

18600 P.C.

18575

18550

T.P. ^{and} 18545

4,33

19340

12,95

189,07

202.02

191.0 191.0 189.8 192.9 192.4 190.1 190.36 193.6 191.7 206.3 223.9 247.2
 $+0^e$ $+0^e$ -0^e $+2^e$ $+2^e$ -0^e 3.04 $+3^e$ $+7^e$ $+15^e$ $+33^e$ $+56^e$
 /03 /86 /60 /53 /24 /19 /8 /18 /37 /49 /79 /178

192 190.2 189.0 187.4 191.8 191.0 188.5 189.16 189.1 192.5 204.9 224.7 246.6
 $+1^e$ -0^e $+1^e$ $+2^e$ $+1^e$ -0^e 4.24 -0^e $+3^e$ $+15^e$ $+35^e$ $+57^e$
 /79 /76 /42 /52 /18 /13 /24 /20 /30 /54 /85 /137

188.8 188.6 187.3 188.1 187.2 189.9 189.36 188.5 186.8 187.3 201.5 225.1 240.1
 -0^e -0^e -2^e -0^e -2^e $+0^e$ 4.04 -0^e -2^e -2^e $+12^e$ $+35^e$ $+50^e$
 /03 /70 /66 /50 /25 /22 /11 /15 /30 /45 /87 /113

187.0 185.5 187.6 187.1 186.5 185.3 187.1 187.12 185.8 189.3 199.3 203.3 220.1 230.3
 -0^e -1^e $+0^e$ $+0^e$ -0^e -1^e $+0^e$ 6.28 -1^e $+2^e$ $+12^e$ $+21^e$ $+33^e$ $+43^e$
 /08 /95 /85 /52 /27 /15 /12 /12 /15 /29 /44 /51 /87 /107

185.3 185.5 185.8 185.7 184.4 185.5 185.45 190.6 199.1 212.7 220.5 229.6 229.7
 -0^e $+0^e$ $+1^e$ $+0^e$ -1^e $+0^e$ 7.95 $+5^e$ $+13^e$ $+27^e$ $+44^e$ $+44^e$ $+44^e$
 /00 /87 /72 /19 /11 /10 /9 /27 /52 /78 /84 /100

187.9 187.9 184.5 185.3 186.2 185.8 184.1 184.2 184.24 193.0 200.4 210.1 231.7 226.7 227.1
 $+1^e$ $+1^e$ -1^e -0^e 0^e -0^e -2^e -2^e 7.16 $+6^e$ $+14^e$ $+23^e$ $+45^e$ $+40^e$ $+40^e$
 /02 /90 /85 /65 /60 /18 /13 /2 /11 /25 /42 /83 /90 /100

19340

189750

189700 POC

TP 13.06 213.58 2.49 200.52

188778

188766 v

188750

188725

TP 12.29 20301 2.68 19073

188700

19340

196.8 196.9 195.0 198.0 201.1
 -8^2 -8^2 -10^2 -6^2 -3^2 $+17^2$ 223.1 227.7 239.4 253.6 259.1
 112 80 78 53 20 205.13 79 57 78 101 113

195.7 194.7 195.5 202.64 205.0 223.6 224.9 245.1 250.1
 -6^2 -7^2 -7^2 1094 $+2^2$ $+21^2$ $+22^2$ $+42^2$ $+47^2$
 100 98 52 14 54 61 94 105

193.5 193.1 195.6 195.1 195.1 200.52 205.9 215.3 222.5 224.1 245.1
 -7^2 -7^2 -7^2 -5^2 -5^2 2.49 $+5^2$ $+14^2$ $+22^2$ $+23^2$ $+44^2$
 100 90 82 55 25 20 41 57 67 100

192.6 193.4 195.6 194.2 193 192.97 195.0 203.2 222.2 225.7 244.5
 $+0^2$ $+0^2$ $+2^2$ $+1^2$ 10.04 $+2^2$ $+10^2$ $+29^2$ $+32^2$ $+51^2$
 05 82 73 30 8 14 58 71 100

193.1 192.4 194.7 193.9 192.73 192.9 196.1 210.3 224.7 225.4 249.6
 $+0^2$ -0^2 $+2^2$ $+1^2$ 10.28 $+0^2$ $+3^2$ $+17^2$ $+32^2$ $+32^2$ $+54^2$
 103 63 57 22 12 21 33 66 72 131

192.0 192.6 193.3 192.1 194.3 194.6 193.73 191.0 191.3 208.9 223.9 227.2 246.3
 -1^2 -0^2 -1^2 $+0^2$ $+0^2$ 928 -2^2 -2^2 $+15^2$ $+30^2$ $+33^2$ $+53^2$
 100 90 75 54 52 40 10 20 39 61 77 113

191.9 192.0 190.4 190.7 194.5 193.1 190.72 192.0 197.6 207.5 223.9 225.1 246.9
 $+1^2$ $+1^2$ -0^2 $+0^2$ $+3^2$ $+2^2$ 2.68 $+1^2$ $+6^2$ $+16^2$ $+33^2$ $+34^2$ $+56^2$
 100 96 90 72 65 17 18 26 45 75 83 117

19340

192+00 P.O.C.

TP^{rod} 191+65 4.88 256.45 0.14 251.57

191+65

191+50 ✓

191+30

TP^{rod} 191+25 12.84 251.71 0.46 238.87

TP^{rod} 191+00 12.77 239.33 0.15 226.56

190+90

190+75 For Profile 4.2

190+69 " " 8.6

190+62 " " 3.1

190+46.89 P.O.C. Mid Point

TP^{rod} 190+05 13.18 226.74 0.05 213.53

wd. 1

190+00

213.58

changes

♀

34

203.0
 -49[±] / 30
 -49[±] / 94
 -40[±] / 80
 -27[±] / 58
 -19[±] / 32
 -15[±] / 15
 -3.56
 +12[±] / 25
 +19[±] / 75
 +23[±] / 101
 203.6
 212.6
 224.9
 233.7
 237.6
 252.59
 264.5
 272.2
 276.4

203.6
 -44[±] / 03
 -32[±] / 66
 -22[±] / 75
 -20[±] / 32
 -39[±] / 31
 -38[±] / 03
 -30[±] / 71
 -15[±] / 35
 -13[±] / 22
 256.45
 247.78
 244.78
 6.93
 245.41
 251.71
 258.9
 +11[±] / 29
 +14[±] / 50
 +19[±] / 82
 +21[±] / 100
 262.1
 266.9
 268.9
 +16[±] / 104
 +24[±] / 116
 +36[±] / 140
 264.9
 276.4

199.8
 -23[±] / 89
 -19[±] / 85
 -15[±] / 56
 -9[±] / 36
 -5[±] / 29
 +1[±] / 13
 3.85
 +19
 +17[±] / 53
 203.3
 207.4
 213.6
 217.6
 224.3
 222.86
 223.9
 240
 268.9
 +46[±] / 133

197.9
 -24[±] / 62
 -24[±] / 97
 -18[±] / 91
 -21[±] / 67
 -16[±] / 37
 4.67
 +1[±] / 6
 -0[±] / 20
 +14[±] / 53
 +32[±] / 88
 +37[±] / 99
 +51[±] / 133
 197.9
 197.9
 203.7
 200.2
 205.9
 222.04
 223.8
 221.7
 236.4
 254.5
 259.4
 273.3

197.2
 -13[±] / 100
 -15[±] / 93
 -13[±] / 90
 -13[±] / 89
 -5[±] / 18
 2.62
 +1[±] / 20
 +7[±] / 36
 +26[±] / 71
 +50[±] / 112
 226.74
 205.8
 210.96
 222.8
 220.6
 237.5
 261.4

213.58

194750

194725

TP. 242 238.51 1,143 236.09

194700

193750 MOC.

193700

TP. 184 247.52 10,77 245.68

192750

19

25645

210.6 210.6 215.7 220.0 £ 228.76 249.1 256.7 271.1 35
~~18²~~ ~~18²~~ ~~13²~~ ~~6²~~ 9.75 ~~20²~~ ~~27²~~ ~~42²~~ ~~53⁴~~
 105 67 41 17 42 55 82 106

210.5 210.4 209.7 215.7 233.55 240.0 251.7 268.2 283.1
~~23⁴~~ ~~23²~~ ~~22²~~ ~~17²~~ 4.96 ~~16⁴~~ ~~18⁴~~ ~~34⁶~~ ~~49⁵~~
 108 86 173 42 14 41 74 106

209.6 207.6 215.2 226.6 238.51 236.09 246.6 257.9 280.4 286.7
~~26⁵~~ ~~28⁵~~ ~~20²~~ ~~9⁵~~ 11.43 ~~10⁵~~ ~~12⁵~~ ~~144²~~ ~~50⁵~~
 100 78 52 21 22 44 90 108

207.6 207.6 207.9 221.5 239.59 257.0 275.6 287.7 289.3
~~32²~~ ~~32²~~ ~~31²~~ ~~15²~~ 7.93 ~~17²~~ ~~36²~~ ~~48²~~ ~~49²~~
 123 100 77 31 35 72 98 118

205.6 205.3 206.2 223.8 231.6 242.28 258.4 277.3 280.9 281.9 283.4
~~36²~~ ~~37²~~ ~~34²~~ ~~18⁵~~ ~~10²~~ 5.24 ~~16²~~ ~~35²~~ ~~38⁵~~ ~~39⁵~~ ~~41²~~
 103 90 72 49 20 28 64 77 87 102

204.5 205.2 220.4 231.6 247.58 245.68 255.6 270.7 273.2 277.5 279.3
~~42²~~ ~~40⁵~~ ~~25²~~ ~~11²~~ 10.77 ~~9²~~ ~~25²~~ ~~32⁵~~ ~~31⁵~~ ~~33⁵~~
 105 99 49 22 17 48 77 85 100

25645

Sept. 28, 1948

Becker T
Godfrey
Barber

197 + 00

196 + 50

196 + 00

195 + 70

P.O.C.
195 + 50

195 + 35

1
full

195 + 00

TP Prod
194185

0.62

226.53

12.60

225.91

238.51

36

216.4 216.5 214.6 216.0 217.8 216.8
 $\begin{matrix} -0^{\circ} \\ 100 \end{matrix}$ $\begin{matrix} -0^{\circ} \\ 90 \end{matrix}$ $\begin{matrix} -2^{\circ} \\ 83 \end{matrix}$ $\begin{matrix} -1^{\circ} \\ 77 \end{matrix}$ $\begin{matrix} +0^{\circ} \\ 52 \end{matrix}$ $\begin{matrix} -0^{\circ} \\ 38 \end{matrix}$ 7.33 219.3 227.1 241.9 256.2

215.0 214.1 215.4 216.5 215.2 215.4
 $\begin{matrix} -2^{\circ} \\ 103 \end{matrix}$ $\begin{matrix} -3^{\circ} \\ 85 \end{matrix}$ $\begin{matrix} -1^{\circ} \\ 82 \end{matrix}$ $\begin{matrix} -0^{\circ} \\ 53 \end{matrix}$ $\begin{matrix} -1^{\circ} \\ 50 \end{matrix}$ $\begin{matrix} -1^{\circ} \\ 30 \end{matrix}$ 9.43 +2² +4² +15² +29² +40²

214.1 213.3 213.9 214.4 215.4 217.5
 $\begin{matrix} -4^{\circ} \\ 103 \end{matrix}$ $\begin{matrix} -5^{\circ} \\ 90 \end{matrix}$ $\begin{matrix} -2^{\circ} \\ 76 \end{matrix}$ $\begin{matrix} -4^{\circ} \\ 41 \end{matrix}$ $\begin{matrix} -3^{\circ} \\ 27 \end{matrix}$ $\begin{matrix} -1^{\circ} \\ 21 \end{matrix}$ 7.87 +7² +22² +33² +50²

213.2 214.6 212.9 214.8 218.5
 $\begin{matrix} -9^{\circ} \\ 107 \end{matrix}$ $\begin{matrix} -8^{\circ} \\ 90 \end{matrix}$ $\begin{matrix} -9^{\circ} \\ 77 \end{matrix}$ $\begin{matrix} -7^{\circ} \\ 55 \end{matrix}$ $\begin{matrix} -4^{\circ} \\ 20 \end{matrix}$ 3.96 +3² +12² +23² +38²

213.2 212.7 214.4 218.5
 $\begin{matrix} -8^{\circ} \\ 108 \end{matrix}$ $\begin{matrix} -8^{\circ} \\ 83 \end{matrix}$ $\begin{matrix} -7^{\circ} \\ 54 \end{matrix}$ $\begin{matrix} -3^{\circ} \\ 21 \end{matrix}$ 221.50 233.8 251.9 261.0 266.9

211.6 211.7 215.8
 $\begin{matrix} -8^{\circ} \\ 107 \end{matrix}$ $\begin{matrix} -8^{\circ} \\ 77 \end{matrix}$ $\begin{matrix} -4^{\circ} \\ 34 \end{matrix}$ 220.47 232.9 246.6 266.1

211.9 211.8 213.7 216.4
 $\begin{matrix} -10^{\circ} \\ 104 \end{matrix}$ $\begin{matrix} -10^{\circ} \\ 65 \end{matrix}$ $\begin{matrix} -8^{\circ} \\ 48 \end{matrix}$ $\begin{matrix} -5^{\circ} \\ 22 \end{matrix}$ 221.89 234.7 255.0 273.9

226.53

238.51

200 + 35

200 + 00

199 + 50

199 + 13

199 + 00

198 + 50

T.P. VEC.

198 + 10.36 10.57 229.50 7.60 318.93

198 + 00

197 + 50

236.53

8.5
Bottom
of Wash

234.9 229.3 227.5 228.5 226.6 226.48 226.5 223.5 226.1 228.7 230.5 242.1 253.1
 +8² +2² +1² +2² +0² 3.02+0² 3² -0² +2² +4² +15² +26²
 16 83 50 26 20 3 9 18 46 62 72 72 120

237.3 232.1 228.4 227.2 224.70 226.0 223.2 223.6 220.8 252.9
 +12² +7² +3² +2² 4.80+1² -1² -1² +6² +28²
 110 87 58 27 12 21 32 60 113

231.3 228.8 228.5 226.5 225.1 224.22 224.1 221.7 229.3 233.6 245.6
 +7² +4² +4² +2² +0² 5.28-0² -2² +5² +9² +21²
 100 89 68 63 27 11 28 40 73 103

226.3 224.5 224.0 223.4 221.0 220.8 223.05 223.8 227.1 229.9 234.1 240.4
 +3² +1² +0² +0² -2² -2² 6.45+0² +4² +6² +11² +17²
 103 95 67 22 14 6 25 34 56 89 110

220.9 222.0 221.5 219.9 221.2 221.78 221.6 220.3 225.7 228.3 234.4 236.5
 -1² +0² -0² -1² -0² 7.72-0² -1² +3² +6² +12² +14²
 104 95 68 40 35 10 17 35 60 87 102

220.6 220.3 219.0 220.6 220.4 218.93 220.1 219.4 223.6 227.3 232.1 237.4
 +1² +1² +0² +1² +1² 10.57+1² +1² +0² +4² +8² +13² +18²
 102 75 46 30 8 2 16 28 61 93 107

220.2 219.9 218.9 219.6 219.0 229.50 219.6 223.0 226.8 231.1 239.0
 +1² +0² -0² +0² +1² 7.30+0² +3² +7² +11² +19²
 102 68 45 40 4 15 22 56 81 108

219.3 218.2 218.1 217.3 216.5 219.0 219.0 218.71 219.7 221.6 225.1 232.9 245.8
 +0² -0² -0² -1² -2² +0² +0² 7.82+1² +2² +6² +14² +27²
 102 95 75 68 58 52 23 25 31 51 77 109

536.53

STUB TACK
MYRTLE ST.
203+18

203+00

202+50

202+00

201+75

20453

25' Lt. M. Hole

201+50

T.P.V

201+00 11.21 237.41 3.30 226.20

200+50

229.50

38

234.1

3.31

not taken don't need

247.3 243.8 235.7 233.1
233.60 234.7 234.6 236.5 253.7

+18¹ +10² +2¹ -0⁵ 3.81 +1⁴ +1⁰ +2² +19⁵
106 99 60 23 25 50 66 111

249.3 241.1 232.9 233.4
231.78 230.4 232.3 233.1 233.8 242.0

+17⁵ +9³ +1⁴ +1⁵ 5.63 -1³ +0⁵ +1³ +2² +10³
110 189 55 25 10 20 50 80 108

250.1 235.4 232.8 231.1
231.56 231.1 229.3 231.0 232.1 234.2 235.7

+18⁵ +3⁸ +1³ -0⁵ 5.85 -0⁵ -2³ -0⁶ +0⁵ +2⁶ +4²
105 67 60 25 12 28 41 58 99 106

250.9 245.6 234.9 233.0 229.6 229.7
227.83 227.6 230.0 231.6 232.2 234.8

+23¹ +17² +7⁴ +5² +1⁸ +1⁴ 9.58 -0² +2² +3⁸ +4³ +7⁰
105 98 67 63 28 7 6 16 33 77 110

252.5 237.5 231.6 229.9 229.3 227.3
229.47 229.6 230.8 231.9 234.6 235.6

+24⁰ +9³ +3¹ +1⁸ +0⁸ -1² 8.94 +1⁴ +2³ +3³ +6² +7²
103 73 64 45 25 17 16 32 64 92 107

252.2 230.2 228.9 227.2 225.5 224.2 228.2 230.2 232.0 234.8 236.8

+26⁶ +4² +2² +1⁰ -0³ 11.21 +2² +4² +5⁸ +8⁶ +10⁵
110 170 43 13 8 5 32 61 89 120

240.7 228.8 227.6 228.3 227.0 237.4 224.26 226.5 228.3 231.1 242.8

+16³ +4⁵ +3⁸ +4² +2³ 5.24 +2² +4⁴ +6² +25⁵
103 83 47 23 9 8 33 62 124

229.50

205 + 50

205 + 00

P.O.T.

204 + 90

204 + 50

204 + 33

204 + 29

T.P. ↓

204 + 00 11.72 247.67 1.48 235.95

STAKE TACK
MYRTLE ST.

203 + 59

203 + 50

CHECK ON
HUB AT STATION

42 + 55

2.44 234.97 ^{BN 1823-10} 234.92

237.41

251.9 247.1 241.4 240.3 238.4 240.0 241.6 241.57 244.5 256.7 270.1 287.6 39

+102 +55 -02 -12 -32/16 02 6.10 +22 +152 +285 +462

1125 105 93 75 65 62 40 24 30 74 102

259.4 244.9 239.1 237.8 237.9 239.5

+192 +45 -04 -22 -12 -03 233.82

117 83 58 53 42 35 7.85

240.3 240.5 282.5

+05 +02 +422

25 51 118

239.54

8.13

Not needed

255.6 242.6 238.9 239.1 236.4 237.41 238.0 238.3 239.8 271.7

+183 +52 +15 +02 -12 10.26 +06 +02 +24 +342

109 77 50 18 16 11 42 62 110

253.2 238.1 237.6 237.0 235.95 236.0 235.0 236.4 239.4 260.4

+172 +21 +16 +10 11.72 02 -12 +04 +34 +244

110 70 27 2 9 13 30 62 101

247.67

234.71

3.70

Not needed

248.8 237.5 235.6 233.8 234.35 235.6 235.9 242.2 255.5

+144 +34 +12 -06 3.06 +12 +15 +78 +214

107 71 32 10 10 40 69 109

237.41

207+38
cut 1

207+00

T.P. ↓

206+96 13.60 289.63 0.15 271.03

206+67

206+45

T.P. Rock

206+40 12.37 271.18 0.51 258.81

206+25

206+00

T.P. Rock

205+93 12.60 259.32 0.95 246.72

205+80

247.67

257.0 258.1 268.1 272.6 291.1 296.8 301.2 305.2 310.6 40

216 -205 110 88 20 5.03 +125 +182 +122 +126 +1320

244.6 247.0 251.9 260.6 272.3 278.7 290.5 297.7 301 304.5

-272 -252 -208 -112 102 181 57 28 11.3 +64 +182 +125 +1202 +322

102 181 57 28 13 34 59 88 103

283.63

243.9 243.8 250.5 265.31 271.5 279.9 287.9 295.3 300.9

-214 -215 -148 5.87 +62 +146 +122 +1302 +356

105 81 42 17 35 55 77 103

244.2 243.6 245.5 255.0 260.36 264.9 272.8 283.3 291.7 300.4

-162 -162 -142 -54 10.82 +45 +124 +122 +1302 +40

113 83 56 15 15 38 62 80 112

271.18

243.7 243.3 246.0 253.45 259.7 267.9 281.7 291.8 299.6

-92 -102 -75 5.87 +62 +144 +122 +1382 +464

112 61 33 19 40 68 89 119

242.6 241.8 242.2 244.9 248.38 251.3 270.0 281.3 292.8

-64 -72 -62 -44 10.34 +124 +122 +1322 +432

103 82 77 13 24 52 73 100

259.32 241.7 259.8 242.3 241.4 243.39

-12 -36 -14 -20 4.28

105 92 61 35

247.67

251.3 271.9 285.4 290.5

+102 +128 +122 +174

29 65 84 101

208+82

T.P. Rock

208+60 12.75 306.84 0.22 394.09

208+50

208+06

P.O.T.

207+81.11

207+72

T.P. Rock

207+55 12.58 394.31 1.90 381.73

207+52

283.63

Note: From Sta. 58+53.71 North Rt. & Lt are + above & -, below

251.3	251.8	256.8	273.3	286.3	297.50
-462	-452	-402	-242	-112	9.34
117	100	185	44	19	

309.6	315.7	317.8	319.3
+124	+182	+202	+222
30	54	81	101

306.84

248.9	248.9	260.1	272.1	281.2	290.80	302.2
-412	+419	-302	-182	-92	3.51	+112+202+252+272
109	92	63	35	17		22 51 71 101

257.1	257.1	267.5	280.3A	297.9	307.2	308.6	312.4	314.4
-332	-382	-222	3.97	+72+132	+182	+182	+222	+242
112	70	45	17	40	65	88	103	

290.28

4.03

Not needed

248.6	249	270.0	281.1	290.68	299.1	305.2	306.8	311.7	313.5
-424	-412	-202	-92	3.62	+82	+142	+162	+212	+222
110	77	36	19	30	52	70	90	102	

394.31

283.42

0.31

Not needed

283.63

210 + 59

210 + 34

T.P. ROCK.

210 + 13 11.23 327.99 1.69 316.76

210 + 00

209 + 76

T.P.

209 + 28 13.00 318.45 1.39 305.45

209 + 00

306.84

42

256.9 271.1 282.5 297.1 307.1 318.4 318.6
 -635 -493 -372 -233 -122 -22 -12 9.61 +32 +42 +53
 150 108 85 61 42 16 3 30 69 100

258.3 266.3 295.8 308.6 318.84 319.6 322.3 324.4 324.8 325.7
 -605 -522 -232 -102 9.15 +02 +32 +56 +62 +72
 128 108 32 32 10 15 49 85 115

327.99

256.9 264.2 275.2 295.2 307.1 315.13 319.6 323.1 324.6
 -582 -502 -392 -192 -82 3.32 +42 +82 +95
 120 101 81 47 24 17 56 100

256.3 269.3 282.7 295.7 304.6 311.09 320.4 322.1 323.1 323.7
 -542 -412 -282 -152 -62 7.36 +92 +112 +122 +126
 111 80 55 33 19 30 58 90 102

255.1 251.1 264.3 278.0 288.1 305.45 313.9 317.6 320.7 320.7 321.7
 -502 -512 -412 -272 -172 12.00 +82 +122 +152 +152 +162
 121 106 84 55 34 26 44 67 88 100

318.45

252.2 257.7 264.5 270.3 280.5 290.4 300.52 312.4 317.7 320.1 322.0
 -482 -422 -362 -302 -202 -102 6.32 +112 +172 +192 +215
 122 106 72 36 36 18 33 62 82 100

306.84

212 + 50

212 + 00

211 + 70

211 + 40 103' RT westerly of wood frame house

211 + 15.5 19.5 RT Guy pole # D 29569T

211 + 05 1' ht Guy wire dead man

211 + 00 78' RT westerly of stucco house

tie in houses

INTERSECT. LANDS
7' LINE AND "L" LINE

P.O.T.

210 + 77.?

327.99

43

308.3	309.3	319.0	322.5	324.04	325.6	326.8	327.2	327.7
-15	-140	-50	-15	3.95	+1.6	+2.2	+3.2	+3.7
103	198	44	20		20	50	78	110

302.6	306.1	317.4	322.1	323.83	325.5	326.5	327.1	327.4
-21.2	-171	-62	-12	4.16	+1.2	+2.2	+3.3	+3.6
114	99	46	15		25	50	80	110

294.6	299.2	306.4	319.9	323.24	325.0	326.1	326.7	327.1
-28.4	-24.2	-14.2	-3.2	4.75	+1.2	+3.2	+3.5	+3.2
108	98	78	25		20	55	84	100

291.5	296.8	305.8	321.9	322.94	324.8	326.0	326.4	327.0
-31.4	-26.4	-14	-1.2	5.05	+1.2	+3.4	+3.5	+4.4
101	92	65	13		24	52	85	100

282.8	291.9	310.3	318.5	319.8	322.11	323.1	324.9	325.5	326.2
-39.3	-24.2	-11.2	-3.4	-2.2	5.88	+1.6	+2.2	+3.4	+4.4
102	72	45	24	8		7	35	65	78

321.97
6.02 Not Needed

321.44
6.55 Not Needed

327.99

215+00

T.P. OX. WATER PIPE

214+85 0.00 300.27 12.46 300.27

T.P.

214+50 1.20 312.73 16.83 311.53

214+00

T.P. ↓

BC. HUB. LT.

213+81.27 1.89 320.36 7.52 320.47

213+50

213+00

327.99

272.3 272.4 274.6 279.9 283.3 289.6
 242-246 -224 -174 -132 -74 3. 32.7125 309.5 325.7 327.7 327.14 326.5
 170 112 81 62 41 20 25 52 78 89 94 105

300.27

271.5 277.3 290.7 298.1 311.53 323.0 324.5 327.7 328.3
 -40° -34° -20° -13° 1.20 +11° +13° +16° +16°
 121 85 62 39 35 50 80 106
312.25

277.1 285.0 291.3 306.1 315.4 320.48 322.1 325.4 328.7 329.2
 -43° -35° -23° -14° -5° 1.88 +2° +4° +8° +8°
 120 102 76 56 15 25 60 81 119

279.1 290.3 305.8 316.2 320.47 324.1 327.9 328.7
 -41° -30° -14° -4° 1.89 +3° +7° +8°
 114 89 62 23 38 54 110

283.3 293.3 303.3 314.2 322.36 321.39 323.4 325.4 327.2 328.6
 -38° -28° -16° -7° 6.60 +8° +4° +5° +7°
 109 89 68 42 20 47 60 109

289.7 296.7 306.3 315.13 318.8 323.13 325.1 326.1 326.9 328.6
 -34° -26° -16° -8° -4° 4.86 +2° +3° +3° +5°
 112 98 76 54 37 22 42 68 100

327.99

217+00

216+95 47' RT & water valve box 3 1/2' x 3 1/2'

T.P.

216+72 13.50 293.63 7.32 281.13

216+53 1' RT & Sewer Manhole

7.45

216+50

216+20

216+00

T.P. ROCK

215+83 0.63 288.45 13.45 287.82

215+75 60' RT radial Hits westerly edge 40th St. Pool Bridge (Wood)

215+50

300.27

319.1

+282 118 +172 82 +125 163 +52 27 3.24

308.3

302.9

295.7

290.39

289.8

283.2

284.1

302

306

-62 17 -72 47 -62 15 +102 102 +102 115

315.7

297.6

290.5

282.2

280.3

281.3

280.5

280.5

280.5

282.6

285.5

304.4

304.6

+346 124 +165 93 +94 66 +11 31 -02 13 -12.50 10 -02 10 +15 33 +44 52 +232 65 +232 95 +232 109

315.3

293.4

282.4

219.4

278.6

293.63

280.67

280.9

286.9

293.4

307.7

308.5

316.7

+344 134 +122 96 +12 68 -12 48 -24 15 7.78 31 +02 48 +62 98 +122 68 +122 87 +122 101 +122 112

300.0

293.0

283.6

278.2

271.2

278.0

271.6

278.75

284.5

291.3

286.5

310.2

315.5

322.9

+212 125 +142 108 +12 92 -02 70 -12 59 -02 30 -12 6 9.70 12 +52 30 +122 45 +172 45 +312 94 +362 94 +452 106

293.6

290.0

278.3

276.4

277.1

278.4

281.0

285.41

293.8

299.7

308.3

313.7

319.0

325.1

+182 134 +46 118 -7 92 -20 85 -22 54 -22 23 -42 11 3.04 22 +82 41 +142 64 +222 77 +282 98 +332 117

288.45

284.1

280.1

276.1

277.4

279.9

228.3

292.8

299.3

305.7

310.5

319.3

322.3

323.1

-52 130 -92 118 -132 1102 -112 54 -92 23 11.14 10 +32 27 +102 46 +162 60 +212 77 +302 97 +332 103

276.5

274.6

274.6

277.2

280.6

285.1

290.64

304.4

315.6

321.3

328.4

-144 140 -16 122 -162 89 -132 59 -102 27 -52 13 9.63 29 +132 57 +282 75 +302 114 +372 114

300.27

218+11 126' Rt radial 2' dia con. storm culvert.

218+00

CONC. STOP
ON BRIDGE

217+80 12.06 328.31 0.02 316.25

217+55

T.P. ROCK

217+50 11.81 316.27 0.85 304.46

217+40

217+20

T.P. ROCK

217+08 12.76 305.31 1.08 292.55

293.63

329.5
 +113 172 +25 +23 10.09 -02 -202 -285 -304 -292 -232
 119 70 23 6 13 37 85 102 118 130
 289.0 289.1 287.6 298.4
 289.0 294.5

328.31

326.0 322.0 318.9 310.8 309.0
 +213 +172 +144 +62 +42 11.44
 11 25 46 16 8
 304.83
 -72 -182 -202 -174 -63 -55
 20 54 75 97 125 144

316.27

300.55

4.76 Not Needed

321.1 316.0 309.6 302.6 298.9
 +252 +205 +142 +71 +34 9.78 -45 -102 -124 -113 +45 +52
 112 89 51 24 12 13 35 64 80 110 133
 295.53 291.0 285.5 283.4 281.2 300.0 300.7

305.31

293.63

BRASS PLUG
N.W. CORNER LANDIS
AND 40 TH.

4.0 330.41 ^{0.13} 330.28 Elev. ^{Bench Mark}

HUB N.7 LINE LANDIS
E OF 40TH ST.

330.22

330.22
4.19

219+00

218+68.5

218+56 South curb line Landis St

F.P. ROCK

218+36 7.13 334.41 1.03 327.28

218+36

328.31

Note: From Sta. 53+53.71 North to Sta.
218+00 - Rt & Lt. are + above & ; -
below &.

329.8	329.8	329.4	329.8	329.3	329.4	328.6	327.7
50 00	04	4.58	05	02	12	21	
100 50	22		22	52	82	120	
30							
329.6	329.6	329.8	329.8	329.3	329.4	328.6	327.7
+02	-02	4.60	02	12	02	11	41
106	152	24	31	56	90	125	
329.6	329.9	329.4	328.0	321.1	320.9	316.1	312.3
+02	+05	+02	5.0	14	82	85	132
110	50	15		20	35	53	89
							115 145

334.41

331.2	329.2	326.1	326.3
+76	+56	+25	+22
115	103	27	11
			4.73

328.31

316.0	306.0	302.7	299.0	296.7
-76	-174	-212	-246	-262
20	40	88	126	156

Cross Section 4015 St. Landis St.
to W 19th main St.

Nov. 12, 48 Lt = 14

2

Pt = 5

48

+50

337.2 5.70 26.6	336.7 5.24 26.6	337.3 5.63 26.6	337.6 5.32 26.6	337.3 5.56 26.6	336.6 6.36 26.6	337.2 5.68 26.6
-----------------------	-----------------------	-----------------------	-----------------------	-----------------------	-----------------------	-----------------------

221+0

335.6 7.39 26.6	335.0 7.88 26.6	335.6 7.31 26.6	335.9 6.99 26.6	335.7 7.19 26.6	335.0 7.90 26.6	335.6 7.38 26.6
-----------------------	-----------------------	-----------------------	-----------------------	-----------------------	-----------------------	-----------------------

+50

334.0 8.91 26.6	333.5 9.11 26.6	334.0 8.85 26.6	334.3 8.53 26.6	334.0 8.92 26.6	333.4 9.15 26.6	334.0 8.89 26.6
-----------------------	-----------------------	-----------------------	-----------------------	-----------------------	-----------------------	-----------------------

220+0

332.4 10.50 26.6	331.8 11.09 26.6	332.4 10.45 26.6	332.7 10.19 26.6	332.5 10.38 26.6	331.8 11.10 26.6	332.4 10.55 26.6
------------------------	------------------------	------------------------	------------------------	------------------------	------------------------	------------------------

219+75.13 EC

331.7 11.23 26.6	331.0 11.85 26.6	331.5 11.35 26.6	331.9 11.01 26.6	331.7 11.20 26.6	331.1 11.81 26.6
------------------------	------------------------	------------------------	------------------------	------------------------	------------------------

219+3387 = 114 Landis = Sly HC. Paving

330.4 12.57 26.6	329.9 12.92 26.6	330.3 12.60 26.6	330.5 12.43 26.6	330.4 12.54 26.6	329.9 12.97 26.6	330.4 12.50 26.6
------------------------	------------------------	------------------------	------------------------	------------------------	------------------------	------------------------

RTV 12.50 342.91

330 4/ NWRP
Landis + 4031
330.38

342.91

TP 5.78 346.94 1.75 341.16

+50

223+0

+50

+25

222+0

221+75

342.91

Lt

Z

Rx

49

340.8 2.96 26-Cb	340.3 2.60 26-Gut	340.9 2.01 13	341.1 1.80	340.8 2.07 13	340.2 2.22 26-Gut	340.7 2.33 26-Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

340.5 2.38 26-Cb	340.0 2.02 26-Gut	340.6 2.01 13	340.8 2.12	340.5 2.07 13	339.8 2.10 26-Gut	340.4 2.52 26-Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

339.9 2.02 26-Cb	339.3 2.63 26-Gut	340.1 2.38 13	340.2 2.66	339.9 2.01 13	339.3 2.64 26-Gut	339.9 2.02 26-Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

339.4 2.54 26-Cb	338.8 1.10 26-Gut	339.6 2.32 13	339.8 2.11	339.5 2.42 13	338.8 1.09 26-Gut	339.4 2.49 26-Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

338.1 1.16 26-Cb	338.2 1.74 26-Gut	338.9 2.01 13	338.2 2.47	338.9 2.05 13	338.3 1.66 26-Gut	338.8 1.08 26-Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

338.1 1.82 26-Cb	337.5 5.47 26-Gut	338.1 1.82 13	338.5 1.44	338.2 1.34 13	337.4 5.47 26-Gut	338.0 1.86 26-Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

342.91

BM 0.68

H.M.B.P.
N. 1967 map
+ 90' S.E.

BM 13.18

H.M.B.P.
Londist 40

For check

BM 4.01 342.93

H.M.B.P.
N. 1967 map
+ 40' S.E.
343.09

+34 = South's Line of N. 1967 map

225+0

+50

224+0

346.94

L

S

R

50

342.3 1.57 26=Cb	341.8 5.11 26=Cut	342.3 1.54 13	342.4 1.50	342.0 1.89 13	341.3 5.62 26=Cut	341.9 5.02 26=Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

342 4.88 26=Cb	341.5 5.41 26=Cut	342.0 1.87 13	342.3 1.69	341.8 5.07 13	341.0 5.85 26=Cut	341.6 5.32 26=Cb
----------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

341.0 5.26 26=Cb	341.1 5.83 26=Cut	341.7 5.20 13	341.8 5.05	341.5 5.43 13	340.7 6.18 26=Cut	341.3 5.59 26=Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

341.2 5.69 26=Cb	340.7 6.20 26=Cut	341.3 5.63 13	341.5 5.40	341.1 5.77 13	340.4 6.51 26=Cut	340.9 5.90 26=Cb
------------------------	-------------------------	---------------------	---------------	---------------------	-------------------------	------------------------

346.94

Levols Habash Freeway P³
 Broadway to Market St
 #119, most 1822-74

BM 2.89 84.36 81.47

SIX BP
 Market St
 #35

4+	58.28 = F.L. 33rd St	3.29	81.1
5+		5.81	79.1
+50		7.73	76.7
6+		10.17	74.2
TP	1.84 73.90	12.30	72.06
+50		3.17	71.7
7+		4.87	69.2
+50		7.17	66.7
+82.28 A		8.83	65.1
8+		9.35	64.5
+25.7 = Gutter		10.42	63.5
+25.7 = Carb Top		9.79	64.1
+35 = 1/4 Conc Walk		10.04	63.9
+58		10.7	63.2
+69		17.3	56.6
9+		19.3	54.6
+30		19.5	54.4
+58		14.7	59.2
10+		11.0	62.9
+30		4.5	69.4
TP	10.24 81.30	2.84	71.06
+50		6.4	74.9

N.O 22008

81.30

Dec. 5-49
 Smith
 Becker
 Berger

51

10+	64	4.9	76.4
11+	0	5.2	76.1
+50		4.5	76.9
+68		4.1	77.2
+77		11.2	70.1
+84.8 = S.C. G.S.A.		11.83	69.5
" Gutter Conc.		12.67	68.6
12+06.54 = 2		11.7	69.6
+28.50 = Gutter		12.22	69.1
" = 1/4 C6		11.43	69.9
+36		10.8	70.5
+44		5.4	75.9
13+	0	5.6	75.7
+50		4.7	76.6
14+	0	3.9	77.4
+50		4.0	77.3
15+	0	3.8	78.5
+12.37 A		1.67	79.6
TP	11.82 91.45	1.67	79.63
+50		8.9	82.6
+87		6.3	85.2
16+04 = 1/4 Carb F.S.T.		6.33	85.2
" Gutter		6.97	84.5
+34.5		6.21	85.2

on top

on top

		91.45		
16+62	H Gutter	7.42	84.1	
"	H Cb of FSK	6.79	84.7	07 Top
+70		1.6	89.9	
17+0		1.1	90.4	
TP	8.17 98.85	0.77	90.68	
+50		7.8	91.1	
18+0		6.6	92.3	
+50		5.4	93.5	
+82		5.1	93.8	
+88		6.8	92.1	
19+0		7.0	91.9	
+37		8.1	90.8	
+50		5.0	93.0	
+60		2.6	96.3	
20+0		2.3	96.6	
+50		2.7	96.2	
TP	5.40 101.62	2.63	96.22	
+97.01	POT	4.87	96.7	07 Hab
21+50		4.5	97.1	
22+0		5.9	95.1	
+50		7.4	94.2	
+59		7.8	93.8	
+64		1.4	95.2	
23+0		6.5	95.1	
+50		6.7	94.9	

		101.62		
24+0		7.7	93.9	
+50		5.8	95.8	
TP	6.08 102.52	5.18	96.44	
25+0		6.6	95.9	
+38.00	4 43°39' Lt	5.84	96.7	
BM		3.09	99.43	07 Hab H & M Brooklyn 43°39' Lt 99.26
+90		6.1	96.4	
26+0		6.6	95.9	
+50		7.0	95.5	
27+0		9.0	93.5	
+50		12.0	90.5	
TP	2.49 92.16	12.85	89.67	
28+0		3.1	89.1	
+50		4.3	87.8	
+67.43	POT old F.C.	5.91	86.25	07 Hab

Additional Levels 40th St "L" Stationing
 Leads to right main
 Alignment #1823

220 +81

INDEXED
 MK.
 SEP 14 1950

+84 = Sty. Conc Wall on Lt.

+83

+77 = Solid Conc. Drive on Rt.

+72 = Conc. Walk + Steps on Lt.

219 + 34 = Sty. Curb on Rt.

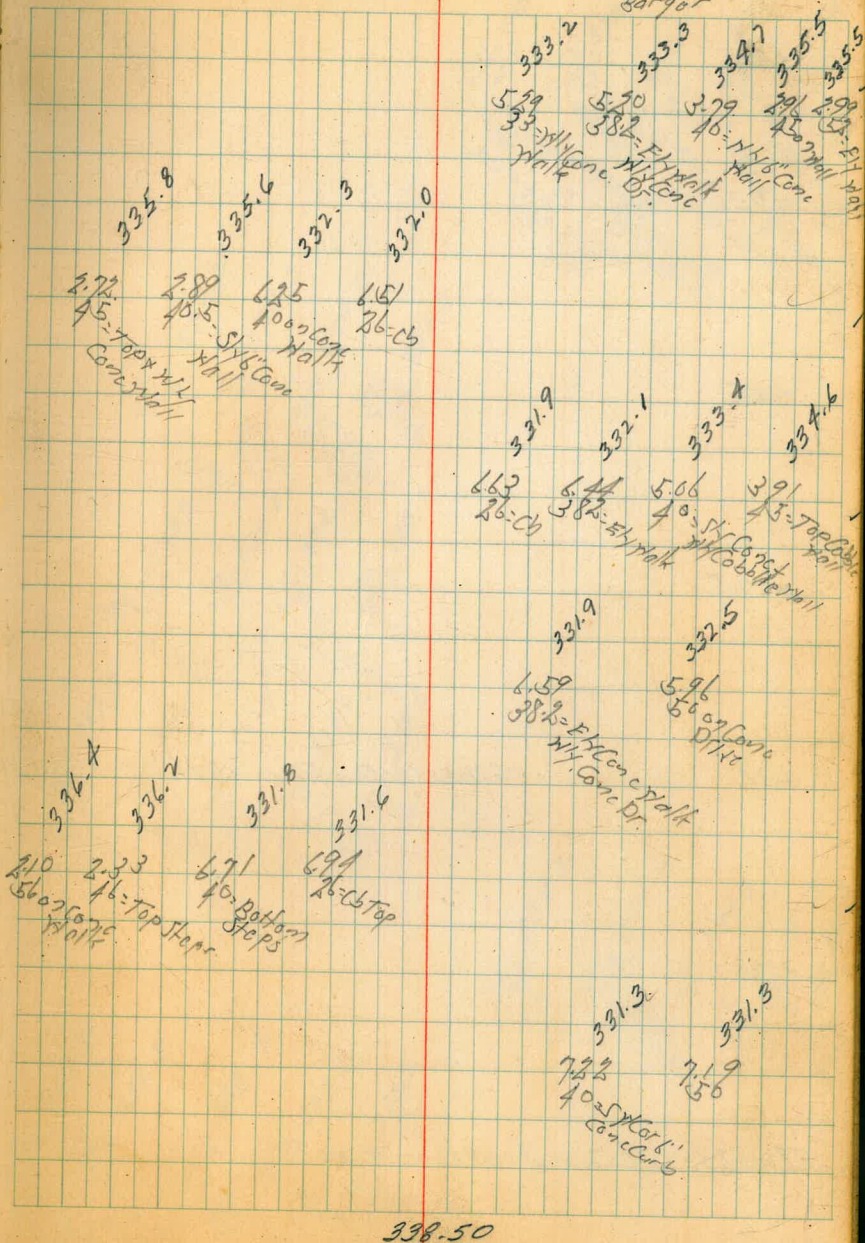
BY 8.09 23850 330.41 H.M.R.P.
 Leads to right
 page 47

Lt. West

L

May 9-49
 R.S. 5502
 Rt. E Roberts
 Barger

53



338.50

40th St. Landing to right man

+19.5 = 3.5 Conc. Steps + 6" Walls on Lt.

TP 810 345.72 0.88 337.62

+15 = 7' Solid Conc. On on Rt.

221+09

+97

+95

220+84 = 11 1/4 Conc. Wall on Lt.

338.50

Lt

Rt

Rt

55

337.6
611-00 Walk
339.3
615-00 Walk
908-00 Top
336.7
916-00 Top
336.6
920-00
336.3
944-00
345.72

336.2
235.8
33-00 Walk
336.4
210
382-00 Walk
337.9
0.60
445-00
338.9
+0.10
515-00
338-00

336.0
248
53-00 Walk
336.2
232
382-00 Walk
337.4
1.13
40-00 Conc
337.4
215-00 Conc

335.7
277
33-00 Conc
Walk
335.8
270
382-00 Walk
337.0
1.50
40-00 Conc
Walk
338.1
0.50
40-00 Conc
Walk

335.7
277
33-00 Conc
Walk
335.7
279
382-00 Walk
336.9
1.50
40-00 Conc
Walk
338.1
0.46
40-00 Conc
Walk

336.7
+0.16
41-00 Top
Walk
338.6
+0.11
41-00 Top
Conc. Wall
335.3
316
40-00 Conc
Walk
335.1
316
40-00 Conc
Walk
338.50

1015 St.

+84

+85

+715 = 2' Conc Walk on Rt.

+61

+57

+49 = 2' Steps & Walk on Rt.

221+345

34572

L

R

339.8
5.90
40.5
7.82
8.84
26-C6
338.6
7.33
26-C6
338.4
7.33
26-C6

338.3
7.33
26-C6
338.7
7.02
38.2
26-C6
340.2
5.57
5.00
Conc Walk

337.9
7.33
26-C6
338.2
7.40
38.2
26-C6
339.3
6.42
4.2
Conc Walk
339.7
6.50
Conc Walk

340.2
5.56
5.00
Conc Walk
340.2
5.56
44.5
340.1
5.58
7.45
340.1
5.90
40.5
339.8
7.82
10-Steps
339.7
7.82
339.7
7.91
339.7
8.23
26-C6
337.9
7.82
10-Steps
337.9
7.91
337.6
8.23
26-C6
337.6
8.10
26-C6
337.6
8.10
26-C6

337.2
8.48
26-C6
337.5
8.19
38.2
26-C6
337.6
8.16
40-Steps
339.2
6.50
43-Steps
339.2
6.50
43-Steps
339.2
6.50
43-Steps

339.7
6.00
8.57
38.2
26-C6
337.2
8.84
26-C6
336.8
8.84
26-C6

56

405 St. Louis to Nightman

+68

+49

+40

+38

222 + 13 = 9' Core Drive on Rt. Body Brakes

221 + 96.5

34572

4x

2

1x

57

341.9
388
390
500
391
415
515
465
340.6
382
515
465
340.5
382
515
465
340.2
382
515
465

339.9
585
465
340.2
557
382
465
340.8
490
450
382
465

340.0
577
382
465
339.9
583
333
465
339.1
663
465
338.9
685
465
338.0
606
333
465
339.7
685
465
338.9
685
465

338.6
713
465
339.4
635
382
465
339.4
635
382
465
338.8
696
465
339.0
672
382
465
340.1
513
465

34572

40+5 St.

+73

+16

+42

+19

223+064

222+885

34572

5

2

Rt.

58

343.8
 192 500
 500
 Conc
 Walk

343.5
 218
 42
 500
 Conc
 Walk

341.6
 108
 70.5
 500
 Conc
 Walk

341.3
 141
 382
 500
 Conc
 Walk

341.0
 177
 26
 500
 Conc
 Walk

340.8
 489
 26
 500
 Conc
 Walk

341.1
 489
 382
 500
 Conc
 Walk

341.3
 442
 40
 500
 Conc
 Walk

342.4
 500
 41
 500
 Conc
 Walk

342.5
 500
 500
 Conc
 Walk

340.1
 540
 26
 500
 Conc
 Walk

340.9
 480
 43
 500
 Conc
 Walk

340.9
 480
 382
 500
 Conc
 Walk

341.8
 382
 40
 500
 Conc
 Walk

342.9
 285
 50
 42
 500
 Conc
 Walk

342.6
 315
 42
 500
 Conc
 Walk

340.9
 478
 70.5
 500
 Conc
 Walk

340.9
 182
 382
 500
 Conc
 Walk

340.6
 510
 26
 500
 Conc
 Walk

340.4
 528
 26
 500
 Conc
 Walk

340.7
 505
 382
 500
 Conc
 Walk

340.9
 480
 40
 500
 Conc
 Walk

341.6
 480
 40
 500
 Conc
 Walk

341.6
 480
 40
 500
 Conc
 Walk

339.9
 583
 26
 500
 Conc
 Walk

345.72
 583
 26
 500
 Conc
 Walk

401357

+84
TP 5.05 347.18 359 342.3

+71.5

+54

+34.5

+23

224+10.5

223+84

34572

LT

Z

343.3
1.41
50.00 Conc
Walk
343.7
2.03
42.5 Top Conc
Stop
342.1
3.15
38.2 NY Walk
341.8
3.91
26.00

347.18

341.5 PL
5.65
26.00
341.8
5.40
38.2 Fly Wall
343.7
3.76
Top NY
Cobble Wall
59

341.6
4.35
26.00
341.6
4.13
38.2 Fly Wall
Fly 15 Conc
Walk + Stop
341.7
4.05
26.00 Bolt Stop
342.8
4.88
26.00 Bolt Stop
342.9
5.00
26.00 Bolt Stop

343.30
2.10
24.00 NY Conc
Walk
341.9
3.84
38.2
341.6
4.15
26.00 Chalky
Conc Road
Walk + Cars

341.1
4.59
26.00
341.5
4.70
38.2 Fly Wall
Fly 10 Conc
Walk + Stop
341.5
4.35
26.00 Bolt Stop
342.6
3.19
24.00 Top Bolt

343.8
1.95
50.00 Walk
343.4
2.30
42.5 Top Stop
341.7
4.04
40.5 Bolt Stop
341.6
4.13
38.2 NY Walk
341.3
4.39
26.00 Cobble Fly
Conc Wall

342.9
2.87
34.00 NY Conc
Walk
341.5
4.13
38.2 NY Conc
Walk
341.7
4.57
26.00 Conc
340.9
4.26
26.00 Bolt Stop
341.3
4.46
38.2 Fly Conc
Walk
342.9
4.80
26.00 Top NY
Cobble Wall

34572

Wabash Boulevard Line Change

8+81.66 F.C. $4^{\circ}19.50'$

+50 $3^{\circ}25.07'$

$18^{\circ}39'$

R 1000

8+0 $1^{\circ}59.13'$

T 75.63

L 150.97

D 1.71887

+50 $0^{\circ}33.19'$

7+30.69 B.C. Lt.

5+92.24

Dec. 7-49
 F.S. 1000
 D. Smith
 Chas. C.
 Bunch
 M.O.

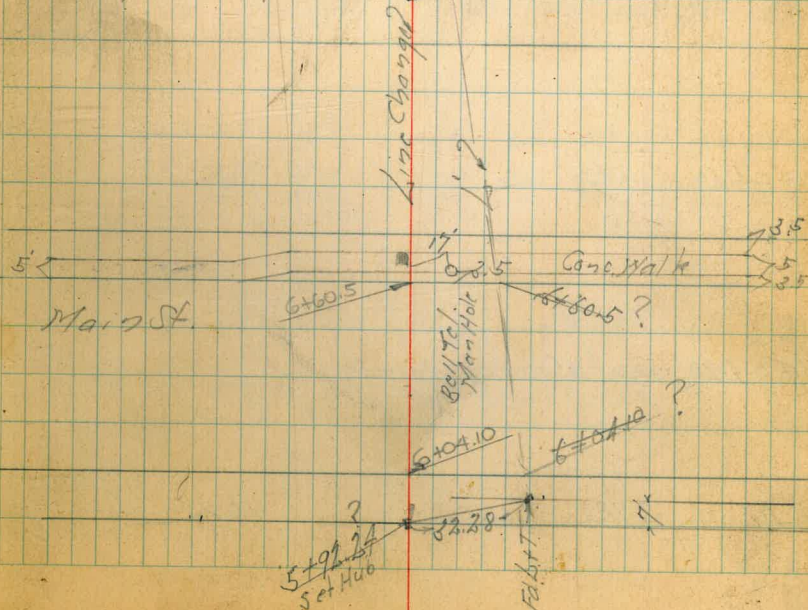
61

8+81.66 F.C.

$18^{\circ}39'$
 R 1000
 T 75.63
 L 150.97

19.1

7+30.69 B.C. Lt.



Cross Section Habash Blvd. Line Change

Alignment Page 61

6+60.5 Cont

6+60.5 = North Curb of Main St.

6+32.3 = $\frac{1}{2}$

6+04.10 Cont.

6+04.10 = South Curb of Main St.

BM 2.78 13.02 10.24

S. M. Cross Street
Top Curb
Main St +
Challier Street

Lt

R

Rt

62

8.6	9.3	5.5	4.9	5.8	5.2	5.3	6.1	5.6
4.38	5.74	7.46	8.10	7.22	7.80	7.68	6.87	7.55
200	200	100	100	150	150	200	250	250
Gut	cb	cb	Gut	cb	Gut	Gut	cb	Gut

1.6	8.7	6.7	6.8	5.5	6.1	5.0	5.5	4.9	5.5	4.8	5.5	4.5
5.47	4.82	6.72	6.18	7.47	6.90	8.00	7.50	8.09	7.52	8.15	7.50	8.25
175	100	100	100	50	50	100	150	50	50	100	150	200
cb	Gut	cb	cb	Gut	cb	Gut	cb	Gut	cb	Gut	cb	Gut

8.9	7.8	6.8	6.2	5.7	5.6	5.6	5.8	5.7	6.0
4.07	5.22	6.15	6.84	7.25	7.42	7.40	7.21	7.25	6.96
200	145	100	50	150	100	150	150	200	200
Gut	cb	cb	Gut	Gut	Gut	Gut	Gut	Gut	Gut

8.6	9.2	5.4	4.8	5.6	5.1	5.6	5.7	5.8
4.38	5.75	7.59	8.18	7.39	7.90	7.39	7.84	7.27
200	200	100	100	150	150	200	200	250
Gut	cb	cb	Gut	Gut	Gut	Gut	Gut	Gut

1.6	4.7	6.3	6.8	5.5	6.0	5.6	5.0	5.3	4.8	5.3	4.4
5.46	4.81	6.72	6.17	7.52	6.97	7.47	8.00	7.68	8.23	7.22	8.27
145	145	100	100	50	50	100	150	150	50	50	200
cb	Gut	cb	cb	Gut	cb	Gut	cb	Gut	cb	Gut	Gut

13.02

	4.5	4.2	6.8	6.8
+50	18.3	18.0	7.0	7.0
	210	195	177	158

	5.2	4.6	6.1	6.1
8+0	190	184	7.1	7.1
	300	173	163	143

TP 790 1378 7.14 5.88

			4.8
+50			18.2
			200

			5.3
7+30.69 BC Lt.			18.3
			200

	5.3	5.1	6.3	6.7
7+0	18.3	18.7	6.7	6.3
	200	159	137	118

6+72.5

13.02

4

5

9t.

63

10.1	11.9	11.3	11.9	9.5	10.5	10.4	8.8	8.1	1.8	1.1
3.7	1.9	2.5	1.9	1.3	5.3	3.4	5.0	5.7	6.0	6.6
150	126	100	77	50	37		30	50	75	100

10.0	10.6	9.5	1.3	6.6	5.9	5.6	1.1	8.6	4.7	4.6	1.3	5.4
3.8	3.2	4.3	6.5	7.2	7.9	8.2	6.1	5.2	9.1	9.8	6.5	8.1
133	112	100	77	50	25		13	37	66	88	88	100

13.78

4.6	1.3	6.6	11.7	9.5	5.1	5.1	5.9	9.6	5.3	4.7	1.1	5.7
18.4	5.7	6.1	1.3	5.5	7.9	7.3	7.1	5.4	7.7	8.2	5.3	7.8
176	150	131	116	85	32		7	19	38	75	89	105

5.0	7.4	1.2	11.5	6.8	5.1	8.3	5.1	5.0	4.6	7.6	5.0
18.0	5.8	5.8	1.5	6.2	7.3	7.7	7.3	8.0	8.4	5.4	8.0
166	143	124	114	50	24		19	50	84	97	107

9.8	9.5	7.6	7.9	8.1	6.4	5.8	5.1	5.0	7.1	5.5	5.4
3.2	3.5	5.4	5.1	4.3	6.6	7.2	7.3	8.0	5.9	7.5	7.6
108	84	74	50	20	12		50	98	100	106	150

AA	AB	5.5	6.0	5.8	5.1	6.0	7.3	7.5	5.6	6.0	5.1	6.1
18.6	18.2	7.5	7.0	7.2	7.3	7.0	5.7	5.5	7.1	7.0	7.2	5.9
200	150	135	100	50		21	50	98	105	150	200	260

water

13.02

Lt.

Z

Rt.

BM

9.39

4.39

on Herb 5
1374.56
439
1844.5

+18

+22

+13

9+0

8+81.66 FC

8+70

13.78

-4.9	-4.7	-2.5
18.7	18.15	18.3
225	200	150

-3.5	1.9	1.9	2.5
17.3	5.9	5.9	11.5
202	184	176	150

-5.5	5.0	1.9	1.1	1.6
19.3	18.8	5.9	6.1	6.7
230	210	189	150	138

-5.5	-2.3	1.1	6.8
19.3	17.1	6.1	7.0
229	208	192	150

1.2	11.1	8.4	8.3	1.6	1.3	6.4	6.5	6.5	6.4	6.4
6.6	2.1	5.4	5.5	6.2	5.5	7.4	7.3	7.3	7.4	7.4
10	178	100	85	50	30	74	25	30	25	100

6.9	1.1	11.9	11.7	10.8	10.4	9.5	9.5	9.4	8.8	8.9
6.9	6.9	19	16	30	24	43	43	4.4	5.0	19
184	130	150	100	50	25	43	35	50	75	100

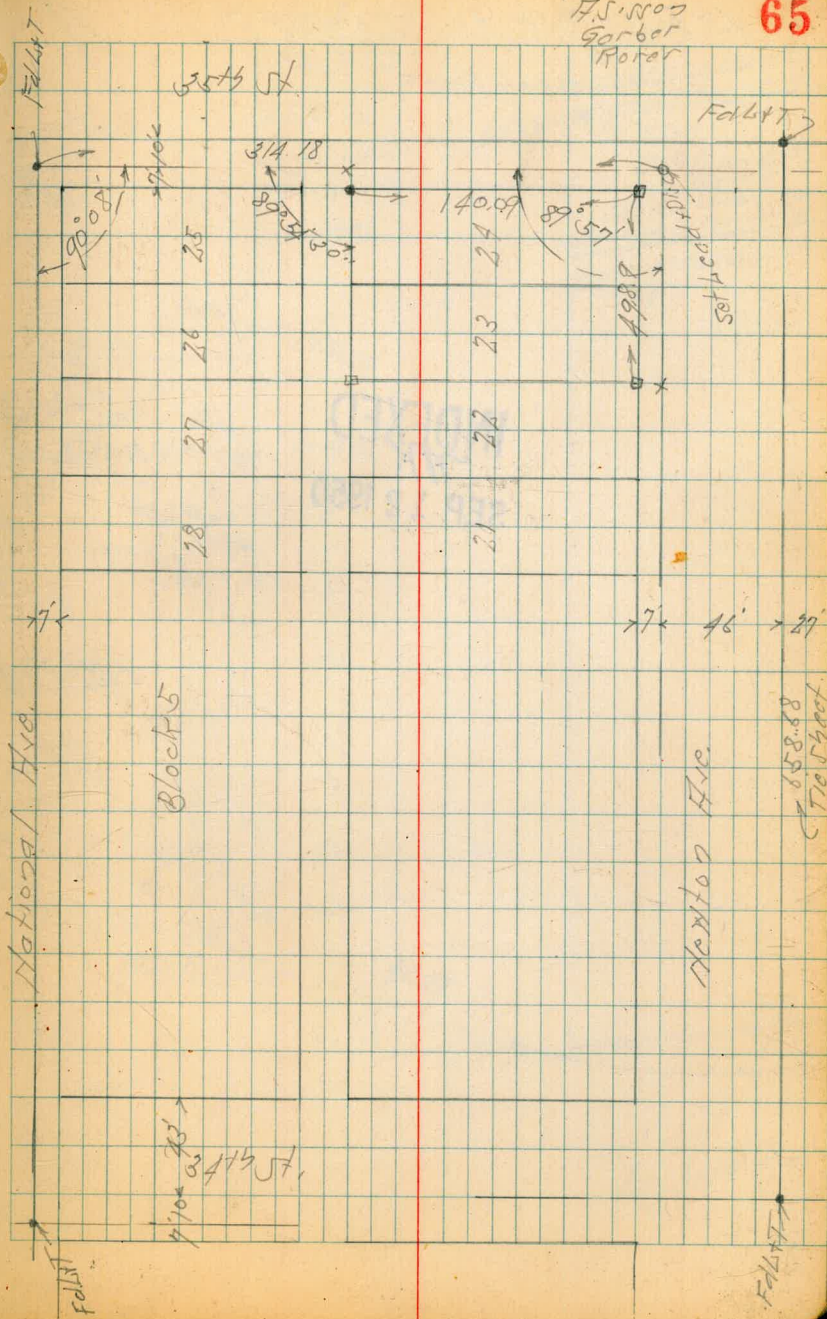
13.78

Survey Lot 23 + 24 Block 5
 San Diego Land + Town Co
 South Chollar Field

INDEXED
 MK
 SEP 14 1950

Sept. 6-50
 F.S. Mason
 Garber
 Porter

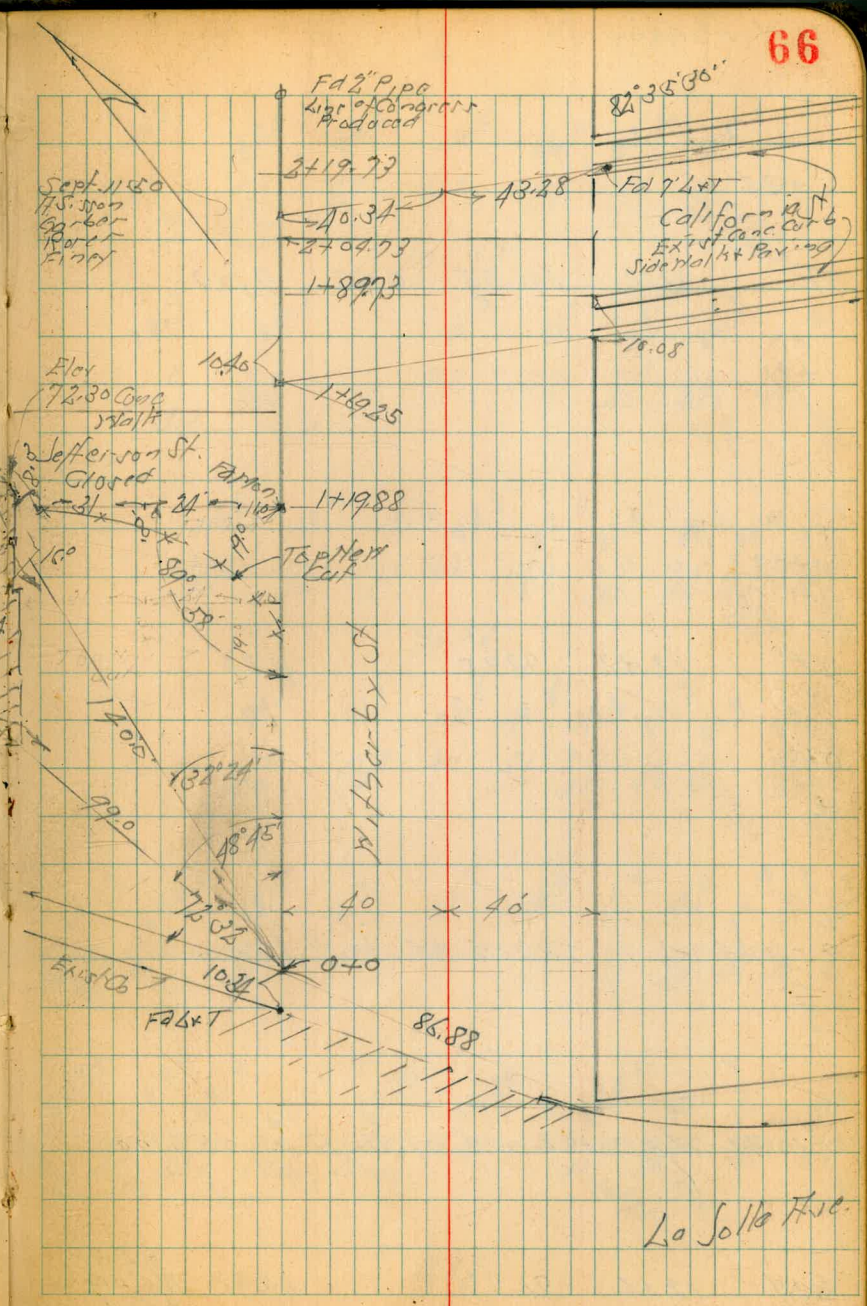
65



Gross Section Witherby St.
 La Solita Ave to California St.

Levels next Page

INDEXED
 MK
 SEP 12 1950



82°35'30"

Sept. 11 1950
 15.00
 30.00
 45.00
 60.00

F42 Pipe
 43.28
 40.37
 27.04.73
 1+89.73

F47 Let
 California St
 EXIST CONC CUT 6
 SIDE WALK PAV 100

Elev
 72.30 Conc
 74.17

Jefferson St. Paved
 Closed
 1+19.88

TOP NEW CUT

WITHERBY ST

LA SOLITA AVE.

Witberby St.

+55

TP 1312 106.75 0.32 9363

+21

+09

TP 1332 9395 0.24

0+0

0-1034 Taken 90° to Witberby

0-1034 = H.E. Curlew at La Jolla Ave. 02 D 109

BM 12.04 81.87 69.83 H.E.B.P. Witberby + La Jolla Ave.

LF

S

RT

67

71.3 53.5 M.O. 40- Cut	93.5 132 38 40- Cut	94.0 128 30	94.8 120	96.2 106 20	95.2 116 40	95.1 117 50 D.H.E.P. Top Cut
106.75						
70.7 23.3 40- Bot Cut	84.7 93 20.5 Top Cut		85.3 87	86.5 75 17	86.1 80 40	86.3 77 45.0 Top Cut
16.0 18.0 38.0- Bot Cut						
70.6 23.8 40	73.7 21.3 20	78.4 15.9 8	77.5 16.5 8.0	82.0 10.7 40	83.3 9.5 40	84.5 8.6 45.0 Top Cut
93.95						
70.3 11.6 40	71.1 10.8 4	73.8 8.1	79.8 7.1 10	79.6 2.3 30	80.3 1.6 40	80.9 1.0 45.0 Top Cut
12.2 5.7 54.0- Bot Cut						
69.19 12.68 40- Cut	69.53 12.04 40- Cb	69.5 12.4 39.0	70.3 11.6 13	70.8 11.1	74.9 7 16	75.9 6.0 38
78.0 2.9 29						
77.1 1.1 45						
78.8 1.1 45						
72.9 1.9 30- Bot Cut						
68.74 13.12 80- Cut	69.38 12.52 80- Cb	69.19 12.68 34.4 50- Cut	69.53 12.04 34.4 Cb	69.30 12.57 30- Fl.	69.38 12.49	69.53 13.34 30- Cut
70.22 11.65 30- Cut						
71.74 13.02 30						
71.60 11.37 30- Cb						
81.87						

W. Derby St

2+04.73 = 2 Calif 0219f

+89.73

TP 10.41 140.79 136 136.38

+69.25

Taken 90° off W. Derby

+45

TP 13.24 131.74 0.55 118.50

1+19.88

89.7

294
106

TP 12.78 119.05 0.48 106.27

0+92

106.75

67.

2

pt.

68

117.0	118.5	129.9	132.4	134.3	134.5	135.40
23.8 79.0	22.2 59.0	10.9 70.1	8.4 70.1	6.5	6.3 70.1	5.39 70.1
115.7	117.5	126.6	129.6	132.5	134.2	134.88
25.1 80.4	23.3 57.0	14.1 70.1	11.3 70.1	8.3	6.6 70.1	5.91 70.1
113.6	115.6	121.1	125.2	127.2	127.6	129.5
18.1 84.0	16.1 58.0	10.8 70.1	6.5 70.1	4.5	4.3 70.1	3.4 70.1
111.5	113.0	116.0	118.6	119.8	119.7	119.9
20.2 86.0	18.7 59.0	15.7 70.0	13.1 70.0	11.9	12.0 70.0	11.8 70.1
98.9	102.6	108.2	110.4	111.8	112.4	112.4
21.2 75.0	16.5 58.0	10.9 70.1	8.7 70.1	7.3 70.1	6.7	6.7 70.1
71.1	98.1	99.3	102.4	103.8	104.6	104.1
25.7 56.0	8.7 70.1	7.5 70.1	4.4 70.1	3.8 70.1	2.2	2.7 70.1

106.75

Lt.

L

Rt

69

BM

470 136.09

N.F. Lt+Tie
Buck
W. L. Borby
Col. R. St.
136.09

2+19.73 = Corb. line of Calif. on Rt

140.79

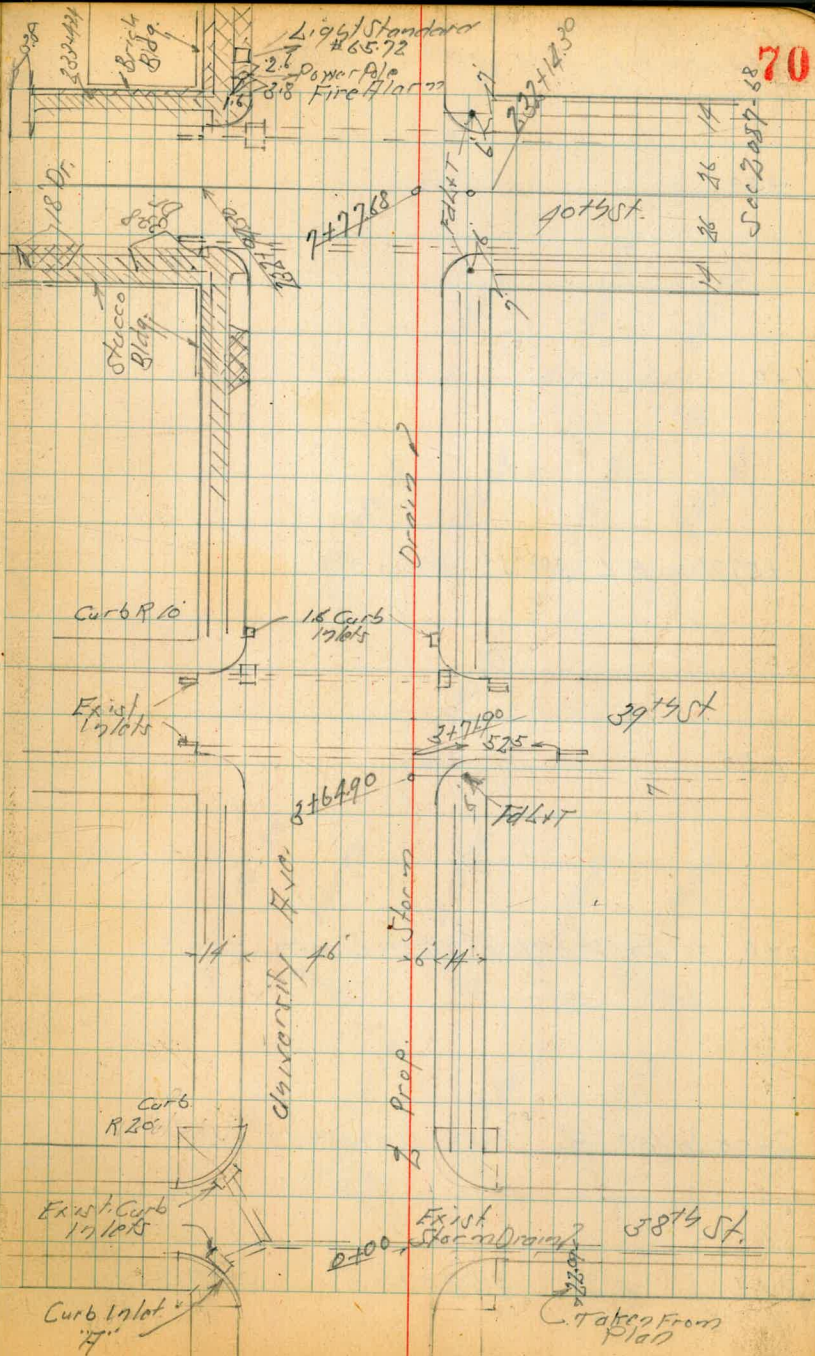
118.4	119.5	133.2	135.7	137.8	137.0	138.6	136.04	135.6
22.4	21.3	26	51	30	28	22	175	51.8
73.0	630	40	30		30	33	10.14	10.00
2.3							0.16	0.16

140.79

Proposed Storm Drains
University Ave. 38th to 40th St.

Jan. 27. 51
F. Simon
Garber
Parker
Papp.

1965
238492
25



70
Sec 2089-68

C. Taken From
Plan

Levels Proposed Storm Drain
University Ave. 38th to 40th St

+50

+10

+57.91 = E.L. 38th St.

+50

0+0 = Existing Storm Drain

Curb Inlet "A" N.W. Corner + 38th St.

B.M.

487

352.13

347.24
N.W. B.P. University
+ 39th St.

Lt.

Z

Rt.

71

345.94
6.19

345.72
6.11

346.15
5.98
10.0

345.69
6.44

345.79
6.34

346.30
5.83
20.00 H.C.

345.99
6.14
10.00 H.C.

345.59
6.54
Top Curb
5' Return

345.56
6.57
6.07 H.C.

344.78
7.35
6.07 H.C.

352.13

345.40
6.73
6.50
6.50

345.04
7.09
6.35
6.35

345.73
6.40
6.06

345.63
6.50
6.35
6.35

345.43
6.70
6.07 H.C.

344.99
7.14
6.07 H.C.

337.78
14.35
14.35
5' Return

+97.9

+71.9 = Hart Curb Line 38' 1/2 St

TP 547 352.71 489 347.24 NW 8P Unit 38' 1/2 St

+50

3+0

+50.

3+0

352.13

4x

2

PT

72

513 347.58
10
525 347.46
523 347.48
10

346.30
541 347.19
59.5 544 347.57
1510 59.5 567 347.04
59.5 59.5 591 346.80
1510 20 on RC 717 344.75
59.5 59.5 717 345.54
1510 6 on RC 717 5 TOP
59.5 59.5 6 on RC 717 5 TOP
1510 6 on RC 717 5 TOP

352.71
346.73
540

346.51
562

347.03
510 346.31
20 582 6.12 345.95
6.64 5.78 346.35
6.56

346.17
5.96

352.13

6+0

+50

5+0

TP 6.16 353.88 4.99 347.72

+50

+38 = 16 Carb Inlets R/L

4+23.9 = East Carb Line of 38 1/2 ft

352.71

Lt.

Z

Rt.

73

348.21
5.67
347.78
6.10
6-9cut
5.63
6-c6
348.25

347.62
6.28

347.20
6.58
347.07
6.86
6-5cut
6.48
6-c6
347.40
353.88

347.26
5.95

346.55
5.30
46-c6
347.41
6.83
16-FL-11
Carb Inlet
346.48
347.38
4.91
12-TP
347.80
5.33
12-TP
346.93
5.78
7.8
346.30
6.41
6-FL-11
Carb Inlet
5.65
6-c6
347.06
346.03
6.80
6-5cut
347.05
5.66
20-Top In.
345.94
6.10
6-FL-11
Carb Inlet

352.71

JP 506 354.72 422 349.66

SE. 6' 2 1/2 T
497 v. 400% St

+7768 = 1/2 40 1/2 St.

+50

7+0

6+50

353.88

H.

S

St.

74

598 349.90

711 349.44

946
10 349.42

497 348.91

515 348.43
6.64

503 348.85
6.66

348.57

501

353.88

Cross Section 40th St.
University Ave. North

Sketch Page 90

233+24.7 = N 1/4 Conc Dr. on Lt

+99.3 = N 1/4 Inlets & Grades Rt & Lt

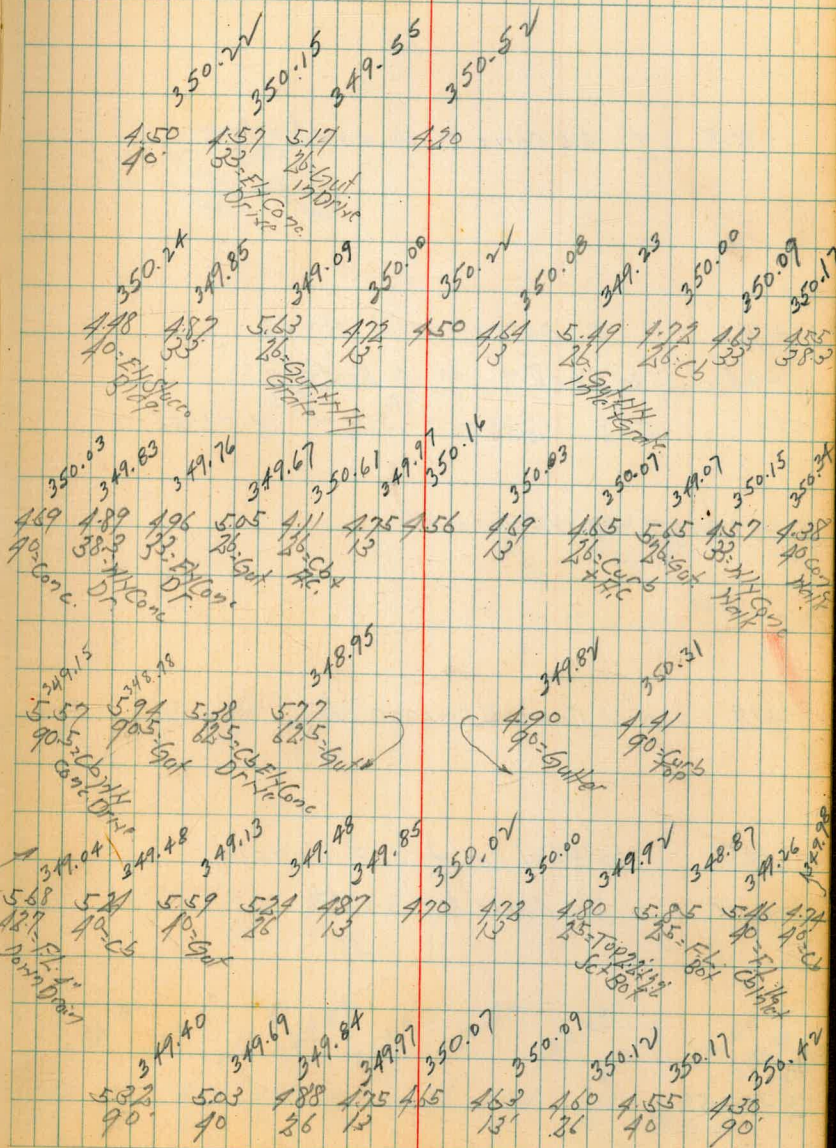
+94.3 = North Line University Ave

+80.3

232+80.3 = North Curb Line University Ave

232+67.3 = North 1/4 of University Ave

354.72 Bl. Ford
Page 94



354.72

+96.5 = 2' Conc. Walk on Lt.

+96 = 1' Down Drain on Lt.

+94 = 30' Lt of 1/2 = 1/2 18 Acacia

TP 5.15 356.71 3.16 351.56

+61.5 = 2' 3/8 Walk on Lt.

+69 = 1/4 Conc. Drive on Lt.

+57 = 30' Pt of 1/2 = 1/2 10" Acacia

+54 = 1/4 Conc Dr on Lt.

2334.50

Lt

Rt

Pt

5.79 5.43
51' Conc. Walk
38.3' FY 1/2 1/2
Conc. Walk

6.30
28' FY 1/4"
Down
Drain
356.71

4.50 4.00 3.90 3.88
26' Gut 26' Gb 23' 1/2 Conc
Walk 350' Walk

4.02 4.02 4.13 4.55
41' Conc Floor 26' Gut

4.16 4.24 4.76
40 33 26' Gut

350.50 350.47 350.33 349.89 350.69 350.86 350.69 350.07 350.54 350.91
4.22 4.25 4.39 4.53 4.13 3.86 4.03 4.65 4.18 3.81 4.0
40' FY 1/2 1/2 Walk 26' Conc 26' Gut 26' Gut 26' Conc Walk
354.72

BM 569 347.25 NW 8 P
 CIVIL 391 347.24

TP 3.28 352.94 7.05 349.66 SE 6 1/2 P
 CIVIL 404 349.66

- +50
- +41 30' Rt of L = Z 9" Palm Tree
- +23 30' Rt of L = Z 9" Palm Tree
- +21 = Z Walk on Lt 3.7 + 5.0

- +18.5 30' Lt of L = Z 12" Acacia Tree
- +13.5 = Z 4' Conc Walk on Rt
- +0.5 30' Rt of L = Z 9" Palm Tree
- 234+0

351.63

47 469 5.08 548 476 148 468 5.00 478 480 46

46 383 26.06 26.50 13 26.50 26.50 26.50

352.23

351.41

351.93

519 519 519 519

38 38 38 38

351.00

351.75

251.75

351.56

54 544 5.76 6.20 5.46 5.45 5.35 5.94 5.48 5.17 5.0

46 383 26.06 26.50 13 13 26.50 26.50 383 40

356.71

A ledger page with a grid of 20 columns and 20 rows. A single vertical red line is positioned between the 10th and 11th columns. The grid is formed by light blue horizontal and vertical lines.

A ledger page with 5 columns and 20 rows. A single vertical red line is positioned between the 1st and 2nd columns. The grid is formed by light blue horizontal and vertical lines.

95
52

43

118.22
10592

6.30

155.5A
2+30.69

154.03
2+00 - 45' 1/2

9822
9146
676
90 66 93
8
46

9823
9

73°10
68
49°10
50 high
406

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16)÷2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.