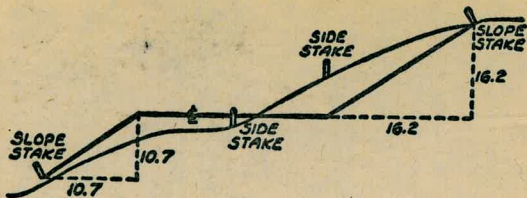


2019

INDEX



Johnston
7988 Roseland Dr

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| 0 | 0.00 | 0.10 | 0.20 | 0.30 | 0.40 | 0.50 | 0.60 | 0.70 | 0.80 | 0.90 | 0 |
| 1 | 1.00 | 1.10 | 1.20 | 1.30 | 1.40 | 1.50 | 1.60 | 1.70 | 1.80 | 1.90 | 1 |
| 2 | 2.00 | 2.10 | 2.20 | 2.30 | 2.40 | 2.50 | 2.60 | 2.70 | 2.80 | 2.90 | 2 |
| 3 | 3.00 | 3.10 | 3.20 | 3.30 | 3.40 | 3.50 | 3.60 | 3.70 | 3.80 | 3.90 | 3 |
| 4 | 4.00 | 4.10 | 4.20 | 4.30 | 4.40 | 4.50 | 4.60 | 4.70 | 4.80 | 4.90 | 4 |
| 5 | 5.00 | 5.10 | 5.20 | 5.30 | 5.40 | 5.50 | 5.60 | 5.70 | 5.80 | 5.90 | 5 |
| 6 | 6.00 | 6.10 | 6.20 | 6.30 | 6.40 | 6.50 | 6.60 | 6.70 | 6.80 | 6.90 | 6 |
| 7 | 7.00 | 7.10 | 7.20 | 7.30 | 7.40 | 7.50 | 7.60 | 7.70 | 7.80 | 7.90 | 7 |
| 8 | 8.00 | 8.10 | 8.20 | 8.30 | 8.40 | 8.50 | 8.60 | 8.70 | 8.80 | 8.90 | 8 |
| 9 | 9.00 | 9.10 | 9.20 | 9.30 | 9.40 | 9.50 | 9.60 | 9.70 | 9.80 | 9.90 | 9 |
| 10 | 10.00 | 10.10 | 10.20 | 10.30 | 10.40 | 10.50 | 10.60 | 10.70 | 10.80 | 10.90 | 10 |
| 11 | 11.00 | 11.10 | 11.20 | 11.30 | 11.40 | 11.50 | 11.60 | 11.70 | 11.80 | 11.90 | 11 |
| 12 | 12.00 | 12.10 | 12.20 | 12.30 | 12.40 | 12.50 | 12.60 | 12.70 | 12.80 | 12.90 | 12 |
| 13 | 13.00 | 13.10 | 13.20 | 13.30 | 13.40 | 13.50 | 13.60 | 13.70 | 13.80 | 13.90 | 13 |
| 14 | 14.00 | 14.10 | 14.20 | 14.30 | 14.40 | 14.50 | 14.60 | 14.70 | 14.80 | 14.90 | 14 |
| 15 | 15.00 | 15.10 | 15.20 | 15.30 | 15.40 | 15.50 | 15.60 | 15.70 | 15.80 | 15.90 | 15 |
| 16 | 16.00 | 16.10 | 16.20 | 16.30 | 16.40 | 16.50 | 16.60 | 16.70 | 16.80 | 16.90 | 16 |
| 17 | 17.00 | 17.10 | 17.20 | 17.30 | 17.40 | 17.50 | 17.60 | 17.70 | 17.80 | 17.90 | 17 |
| 18 | 18.00 | 18.10 | 18.20 | 18.30 | 18.40 | 18.50 | 18.60 | 18.70 | 18.80 | 18.90 | 18 |
| 19 | 19.00 | 19.10 | 19.20 | 19.30 | 19.40 | 19.50 | 19.60 | 19.70 | 19.80 | 19.90 | 19 |
| 20 | 20.00 | 20.10 | 20.20 | 20.30 | 20.40 | 20.50 | 20.60 | 20.70 | 20.80 | 20.90 | 20 |
| 21 | 21.00 | 21.10 | 21.20 | 21.30 | 21.40 | 21.50 | 21.60 | 21.70 | 21.80 | 21.90 | 21 |
| 22 | 22.00 | 22.10 | 22.20 | 22.30 | 22.40 | 22.50 | 22.60 | 22.70 | 22.80 | 22.90 | 22 |
| 23 | 23.00 | 23.10 | 23.20 | 23.30 | 23.40 | 23.50 | 23.60 | 23.70 | 23.80 | 23.90 | 23 |
| 24 | 24.00 | 24.10 | 24.20 | 24.30 | 24.40 | 24.50 | 24.60 | 24.70 | 24.80 | 24.90 | 24 |
| 25 | 25.00 | 25.10 | 25.20 | 25.30 | 25.40 | 25.50 | 25.60 | 25.70 | 25.80 | 25.90 | 25 |
| 26 | 26.00 | 26.10 | 26.20 | 26.30 | 26.40 | 26.50 | 26.60 | 26.70 | 26.80 | 26.90 | 26 |
| 27 | 27.00 | 27.10 | 27.20 | 27.30 | 27.40 | 27.50 | 27.60 | 27.70 | 27.80 | 27.90 | 27 |
| 28 | 28.00 | 28.10 | 28.20 | 28.30 | 28.40 | 28.50 | 28.60 | 28.70 | 28.80 | 28.90 | 28 |
| 29 | 29.00 | 29.10 | 29.20 | 29.30 | 29.40 | 29.50 | 29.60 | 29.70 | 29.80 | 29.90 | 29 |
| 30 | 30.00 | 30.10 | 30.20 | 30.30 | 30.40 | 30.50 | 30.60 | 30.70 | 30.80 | 30.90 | 30 |
| 31 | 31.00 | 31.10 | 31.20 | 31.30 | 31.40 | 31.50 | 31.60 | 31.70 | 31.80 | 31.90 | 31 |
| 32 | 32.00 | 32.10 | 32.20 | 32.30 | 32.40 | 32.50 | 32.60 | 32.70 | 32.80 | 32.90 | 32 |
| 33 | 33.00 | 33.10 | 33.20 | 33.30 | 33.40 | 33.50 | 33.60 | 33.70 | 33.80 | 33.90 | 33 |
| 34 | 34.00 | 34.10 | 34.20 | 34.30 | 34.40 | 34.50 | 34.60 | 34.70 | 34.80 | 34.90 | 34 |
| 35 | 35.00 | 35.10 | 35.20 | 35.30 | 35.40 | 35.50 | 35.60 | 35.70 | 35.80 | 35.90 | 35 |
| 36 | 36.00 | 36.10 | 36.20 | 36.30 | 36.40 | 36.50 | 36.60 | 36.70 | 36.80 | 36.90 | 36 |
| 37 | 37.00 | 37.10 | 37.20 | 37.30 | 37.40 | 37.50 | 37.60 | 37.70 | 37.80 | 37.90 | 37 |
| 38 | 38.00 | 38.10 | 38.20 | 38.30 | 38.40 | 38.50 | 38.60 | 38.70 | 38.80 | 38.90 | 38 |
| 39 | 39.00 | 39.10 | 39.20 | 39.30 | 39.40 | 39.50 | 39.60 | 39.70 | 39.80 | 39.90 | 39 |
| 40 | 40.00 | 40.10 | 40.20 | 40.30 | 40.40 | 40.50 | 40.60 | 40.70 | 40.80 | 40.90 | 40 |
| 41 | 41.00 | 41.10 | 41.20 | 41.30 | 41.40 | 41.50 | 41.60 | 41.70 | 41.80 | 41.90 | 41 |
| 42 | 42.00 | 42.10 | 42.20 | 42.30 | 42.40 | 42.50 | 42.60 | 42.70 | 42.80 | 42.90 | 42 |
| 43 | 43.00 | 43.10 | 43.20 | 43.30 | 43.40 | 43.50 | 43.60 | 43.70 | 43.80 | 43.90 | 43 |
| 44 | 44.00 | 44.10 | 44.20 | 44.30 | 44.40 | 44.50 | 44.60 | 44.70 | 44.80 | 44.90 | 44 |
| 45 | 45.00 | 45.10 | 45.20 | 45.30 | 45.40 | 45.50 | 45.60 | 45.70 | 45.80 | 45.90 | 45 |
| 46 | 46.00 | 46.10 | 46.20 | 46.30 | 46.40 | 46.50 | 46.60 | 46.70 | 46.80 | 46.90 | 46 |
| 47 | 47.00 | 47.10 | 47.20 | 47.30 | 47.40 | 47.50 | 47.60 | 47.70 | 47.80 | 47.90 | 47 |
| 48 | 48.00 | 48.10 | 48.20 | 48.30 | 48.40 | 48.50 | 48.60 | 48.70 | 48.80 | 48.90 | 48 |
| 49 | 49.00 | 49.10 | 49.20 | 49.30 | 49.40 | 49.50 | 49.60 | 49.70 | 49.80 | 49.90 | 49 |
| 50 | 50.00 | 50.10 | 50.20 | 50.30 | 50.40 | 50.50 | 50.60 | 50.70 | 50.80 | 50.90 | 50 |

INDEXED
completely.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE IX
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

| C | R | 30 | 28 | 26 | 24 | 22 | 20 | C | R | 30 | 28 | 26 | 24 | 22 | 20 |
|------|-------|------|------|------|------|------|------|----|-------|------|------|------|------|------|------|
| o | Feet | Inch | Inch | Inch | Inch | Inch | Inch | o | Feet | Inch | Inch | Inch | Inch | Inch | Inch |
| 0-20 | 17189 | .08 | .07 | .06 | .05 | .04 | .03 | 8 | 716.8 | 1.88 | 1.64 | 1.42 | 1.20 | 1.01 | .84 |
| 0-40 | 8594 | .16 | .14 | .12 | .10 | .08 | .07 | 9 | 637.3 | 2.12 | 1.84 | 1.60 | 1.35 | 1.14 | .94 |
| 1-0 | 5730 | .24 | .20 | .18 | .15 | .13 | .10 | 10 | 573.7 | 2.36 | 2.05 | 1.78 | 1.50 | 1.27 | 1.04 |
| 1-20 | 4297 | .31 | .27 | .23 | .20 | .17 | .13 | 11 | 521.7 | 2.59 | 2.26 | 1.95 | 1.65 | 1.39 | 1.15 |
| 1-40 | 3438 | .39 | .34 | .29 | .25 | .21 | .17 | 12 | 478.3 | 3.83 | 2.47 | 2.15 | 1.81 | 1.54 | 1.26 |
| 2-0 | 2865 | .47 | .41 | .35 | .30 | .25 | .20 | 13 | 441.7 | 3.05 | 2.66 | 2.30 | 1.96 | 1.66 | 1.36 |
| 2-20 | 2456 | .55 | .48 | .41 | .35 | .29 | .23 | 14 | 410.3 | 3.30 | 2.87 | 2.48 | 2.10 | 1.78 | 1.46 |
| 2-40 | 2149 | .63 | .55 | .47 | .40 | .33 | .27 | 15 | 383.1 | 3.54 | 3.08 | 2.68 | 2.26 | 1.91 | 1.57 |
| 3-0 | 1910 | .71 | .62 | .53 | .45 | .38 | .31 | 16 | 359.3 | 3.76 | 3.28 | 2.83 | 2.40 | 2.04 | 1.67 |
| 3-20 | 1719 | .78 | .68 | .59 | .50 | .42 | .35 | 17 | 338.3 | 4.00 | 3.48 | 3.02 | 2.57 | 2.16 | 1.78 |
| 3-40 | 1563 | .86 | .75 | .65 | .55 | .46 | .38 | 18 | 319.6 | 4.21 | 3.67 | 3.18 | 2.70 | 2.28 | 1.87 |
| 4-0 | 1433 | .94 | .82 | .71 | .60 | .50 | .42 | 19 | 302.9 | 4.45 | 3.89 | 3.36 | 2.86 | 2.41 | 1.98 |
| 4-20 | 1323 | 1.02 | .89 | .77 | .65 | .55 | .45 | 20 | 287.9 | 4.70 | 4.09 | 3.55 | 3.00 | 2.54 | 2.09 |
| 4-40 | 1228 | 1.10 | .96 | .83 | .70 | .59 | .48 | 22 | 262.0 | 5.16 | 4.44 | 3.84 | 3.30 | 2.80 | 2.29 |
| 5 | 1146 | 1.18 | 1.03 | .89 | .75 | .63 | .52 | 24 | 240.5 | 5.64 | 4.92 | 4.20 | 3.59 | 3.04 | 2.50 |
| 6 | 955.3 | 1.41 | 1.23 | 1.06 | .90 | .76 | .62 | 26 | 222.3 | 6.07 | 5.29 | 4.58 | 3.88 | 3.29 | 2.70 |
| 7 | 819.0 | 1.65 | 1.44 | 1.24 | 1.05 | .89 | .73 | | | | | | | | |

TABLE X
SHORT RADIUS CURVES

| Radius Feet | Chord Feet | Central Angle | Deflection Angle | Deflection for 1 Foot |
|-------------|------------|---------------|------------------|-----------------------|
| 35 | 10 | 16-26 | 8-13 | 49.3 |
| 45 | 10 | 12-46 | 6-23 | 38.3 |
| 50 | 15 | 17-16 | 8-38 | 34.5 |
| 60 | 15 | 14-22 | 7-11 | 28.8 |
| 75 | 15 | 11-30 | 5-45 | 23.0 |
| 100 | 20 | 11-30 | 5-45 | 17.3 |
| 120 | 20 | 9-34 | 4-47 | 14.3 |
| 150 | 20 | 7-39 | 3-49 | 11.5 |
| 190 | 25 | 7-32 | 3-46 | 9.15 |
| 200 | 25 | 7-10 | 3-35 | 8.6 |
| 225 | 25 | 6-25 | 3-12 | 7.7 |
| 240 | 25 | 5 58 | 2-59 | 7.2 |
| 250 | 25 | 5 44 | 2-52 | 6.9 |
| 275 | 25 | 5-12 | 2-36 | 6.2 |
| 288 | 50 | 9-58 | 4-59 | 6.0 |
| 300 | 50 | 9-32 | 4-46 | 5.7 |
| 350 | 50 | 8-12 | 4-06 | 4.9 |
| 376 | 50 | 7-40 | 3-50 | 4.6 |
| 400 | 50 | 7-10 | 3-35 | 4.3 |
| 410 | 50 | 7-00 | 3-30 | 4.2 |

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XI
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL.

| Slope | Horizontal Distance | Correction | Rise | Slope | Horizontal Distance | Correction | Rise |
|-------|---------------------|------------|-------|-------|---------------------|------------|-------|
| 0°00' | 100.000 | 0.000 | 0.000 | 8°00' | 99.027 | 0.973 | 0.139 |
| 15' | 99.999 | 0.001 | 0.004 | 15' | 98.965 | 1.035 | 0.143 |
| 30' | 99.996 | 0.004 | 0.009 | 30' | 98.902 | 1.098 | 0.148 |
| 45' | 99.991 | 0.009 | 0.013 | 45' | 98.836 | 1.164 | 0.152 |
| 1 00 | 99.985 | 0.015 | 0.017 | 9 00 | 98.769 | 1.231 | 0.156 |
| 15 | 99.976 | 0.024 | 0.022 | 15 | 98.700 | 1.300 | 0.161 |
| 30 | 99.966 | 0.034 | 0.026 | 30 | 98.629 | 1.371 | 0.165 |
| 45 | 99.953 | 0.047 | 0.031 | 45 | 98.556 | 1.444 | 0.169 |
| 2 00 | 99.939 | 0.061 | 0.035 | 10 00 | 98.481 | 1.519 | 0.174 |
| 15 | 99.923 | 0.077 | 0.039 | 15 | 98.404 | 1.596 | 0.178 |
| 30 | 99.905 | 0.095 | 0.044 | 30 | 98.325 | 1.675 | 0.182 |
| 45 | 99.885 | 0.115 | 0.048 | 45 | 98.245 | 1.755 | 0.187 |
| 3 00 | 99.863 | 0.137 | 0.052 | 11 00 | 98.163 | 1.837 | 0.191 |
| 15 | 99.839 | 0.161 | 0.057 | 15 | 98.079 | 1.921 | 0.195 |
| 30 | 99.813 | 0.187 | 0.061 | 30 | 97.992 | 2.008 | 0.199 |
| 45 | 99.786 | 0.214 | 0.065 | 45 | 97.905 | 2.095 | 0.204 |
| 4 00 | 99.756 | 0.244 | 0.070 | 12 00 | 97.815 | 2.185 | 0.208 |
| 15 | 99.725 | 0.275 | 0.074 | 15 | 97.723 | 2.277 | 0.212 |
| 30 | 99.692 | 0.308 | 0.078 | 30 | 97.630 | 2.370 | 0.216 |
| 45 | 99.657 | 0.343 | 0.083 | 45 | 97.534 | 2.466 | 0.221 |
| 5 00 | 99.619 | 0.381 | 0.087 | 13 00 | 97.437 | 2.563 | 0.225 |
| 15 | 99.580 | 0.420 | 0.092 | 15 | 97.338 | 2.662 | 0.229 |
| 30 | 99.540 | 0.460 | 0.096 | 30 | 97.237 | 2.763 | 0.233 |
| 45 | 99.497 | 0.503 | 0.100 | 45 | 97.134 | 2.866 | 0.238 |
| 6 00 | 99.452 | 0.548 | 0.105 | 14 00 | 97.030 | 2.970 | 0.242 |
| 15 | 99.406 | 0.594 | 0.109 | 15 | 96.923 | 3.077 | 0.246 |
| 30 | 99.357 | 0.643 | 0.113 | 30 | 96.815 | 3.185 | 0.250 |
| 45 | 99.307 | 0.693 | 0.118 | 45 | 96.705 | 3.295 | 0.255 |
| 7 00 | 99.255 | 0.745 | 0.122 | 15 00 | 96.593 | 3.407 | 0.259 |
| 15 | 99.200 | 0.800 | 0.126 | 15 | 96.479 | 3.521 | 0.263 |
| 30 | 99.144 | 0.856 | 0.131 | 30 | 96.363 | 3.637 | 0.267 |
| 45 | 99.087 | 0.913 | 0.135 | 45 | 96.246 | 3.754 | 0.271 |

For each foot take one one-hundredth of each reading.

TABLE XII
MINUTES IN DECIMALS OF A DEGREE.

| | | | | | | | | | | | |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|
| 0°30' | .00833 | 10°30' | .17500 | 20°30' | .34167 | 30°30' | .50833 | 40°30' | .67500 | 50°30' | .84167 |
| 1 00 | .01667 | 11 00 | .18333 | 21 00 | .35000 | 31 00 | .51667 | 41 00 | .68333 | 51 00 | .85000 |
| 30 | .02500 | 30 | .19167 | 30 | .35833 | 30 | .52500 | 30 | .69167 | 30 | .85833 |
| 2 00 | .03333 | 12 00 | .20000 | 22 00 | .36667 | 32 00 | .53333 | 42 00 | .70000 | 52 00 | .86667 |
| 30 | .04167 | 30 | .20833 | 30 | .37500 | 30 | .54167 | 30 | .70833 | 30 | .87500 |
| 3 00 | .05000 | 13 00 | .21667 | 23 00 | .38333 | 33 00 | .55000 | 43 00 | .71667 | 53 00 | .88333 |
| 30 | .05833 | 30 | .22500 | 30 | .39167 | 30 | .55833 | 30 | .72500 | 30 | .89167 |
| 4 00 | .06667 | 14 00 | .23333 | 24 00 | .40000 | 34 00 | .56667 | 44 00 | .73333 | 54 00 | .90000 |
| 30 | .07500 | 30 | .24167 | 30 | .40833 | 30 | .57500 | 30 | .74167 | 30 | .90833 |
| 5 00 | .08333 | 15 00 | .25000 | 25 00 | .41667 | 35 00 | .58333 | 45 00 | .75000 | 55 00 | .91667 |
| 30 | .09167 | 30 | .25833 | 30 | .42500 | 30 | .59167 | 30 | .75833 | 30 | .92500 |
| 6 00 | .10000 | 16 00 | .26667 | 26 00 | .43333 | 36 00 | .60000 | 46 00 | .76667 | 56 00 | .93333 |
| 30 | .10833 | 30 | .27500 | 30 | .44167 | 30 | .60833 | 30 | .77500 | 30 | .94167 |
| 7 00 | .11667 | 17 00 | .28333 | 27 00 | .45000 | 37 00 | .61667 | 47 00 | .78333 | 57 00 | .95000 |
| 30 | .12500 | 30 | .29167 | 30 | .45833 | 30 | .62500 | 30 | .79167 | 30 | .95833 |
| 8 00 | .13333 | 18 00 | .30000 | 28 00 | .46667 | 38 00 | .63333 | 48 00 | .80000 | 58 00 | .96667 |
| 30 | .14167 | 30 | .30833 | 30 | .47500 | 30 | .64167 | 30 | .80833 | 30 | .97500 |
| 9 00 | .15000 | 19 00 | .31667 | 29 00 | .48333 | 39 00 | .65000 | 49 00 | .81667 | 59 00 | .98333 |
| 30 | .15833 | 30 | .32500 | 30 | .49167 | 30 | .65833 | 30 | .82500 | 30 | .99167 |
| 10 00 | .16667 | 20 00 | .33333 | 30 00 | .50000 | 40 00 | .66667 | 50 00 | .83333 | 60 00 | 1.00000 |

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1

Sewer Prelim.

| | |
|---|-----------------------------|
| ✓ Calle de la Plata | } sketch 2-7 |
| ✓ Paseo Dorado | |
| ✓ Spindrift Drive | } Levels 8-17 |
| ✓ Princess St. | |
| ✓ St Louis Terrace | { sketch - 18 Levels 20- |
| Bench check | 19 |
| ✓ Viking way | 23-28 |
| ✓ Roseland Drive | 29 + 40 |
| ✓ Little St. | 30 + 40 |
| ✓ Hypatia Way DRIVE | 36 |
| ✓ AVENIDA ALAMAR | 42 - 48 |
| ✓ Torrey Rd. Charlotte pump station sly. | 49 + |
| Cowrie St. | 51 + and 66 |
| Villa Tract La Jolla Park Blks B+C - Map #1535 | 57 + to 65 |
| Alley Blk. 45 La Jolla Park | 75 to 79 |
| "Alternate line" " " " " | 50 + 80 |

For this area also see

book 2028 + BK 2027

Prelim Sewers
(S.E. La Jolla Shores) 4-1-49

WIO.#
31720 ✓

INDEXED

WIS
APR 29 1949

Sommermeier
Allen
Jones

Paseo Dorado - Spindrift Dr.
and Princess St.

(Levels - p. 7)

Blue = change run 6/8/49
and 6/15/49

Set. N.E.B.P.
Calle de la Plata
+ Paseo Dorado

5.83 < 7.67 > = BM #2

T.P. 2.25 < 13.59 > 9.42 < 11.25 >

T.P. 0.05 < 20.67 > 12.43 < 20.62 >

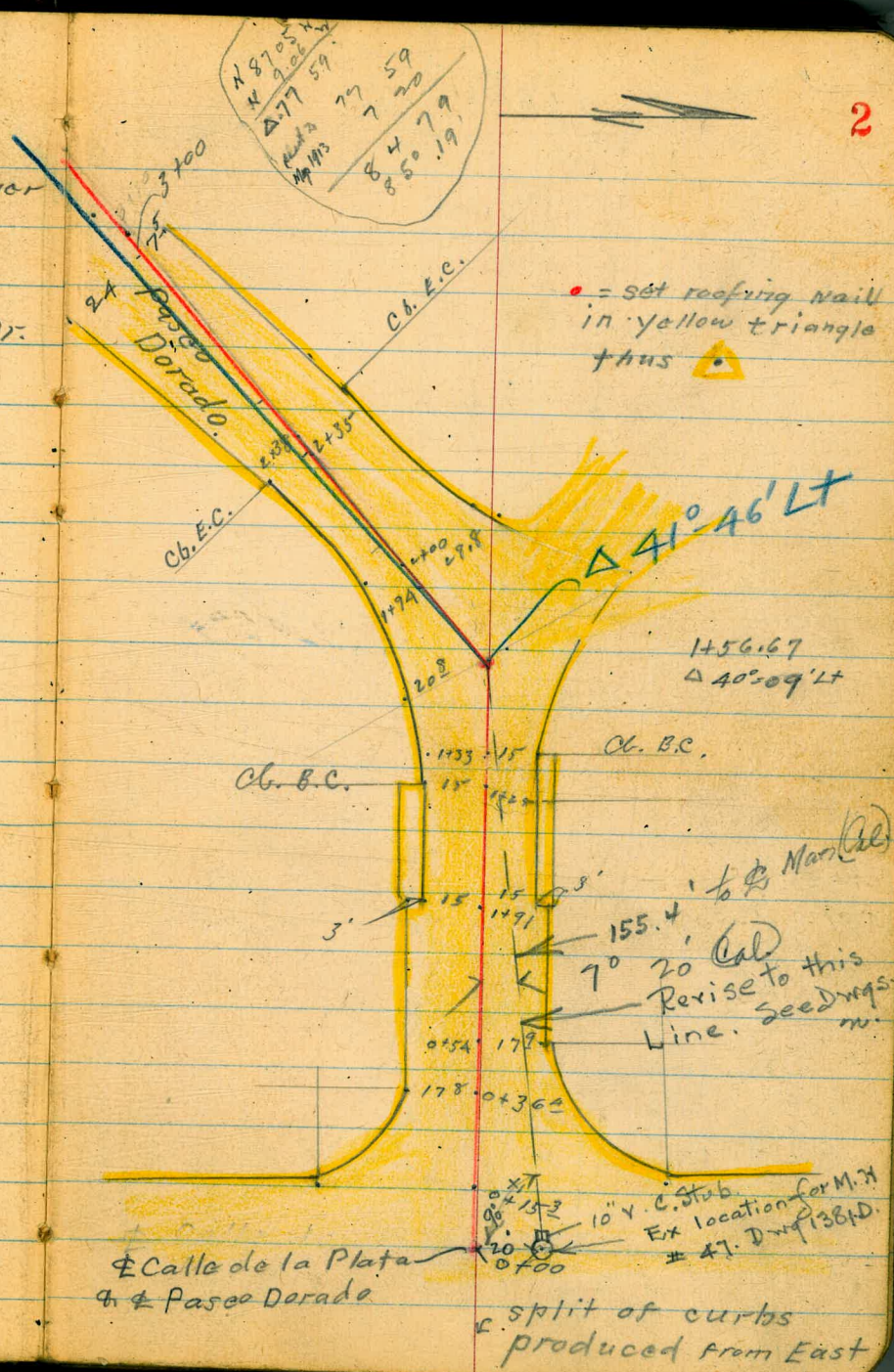
T.P. 0.25 < 33.05 > 12.46 < 32.80 >

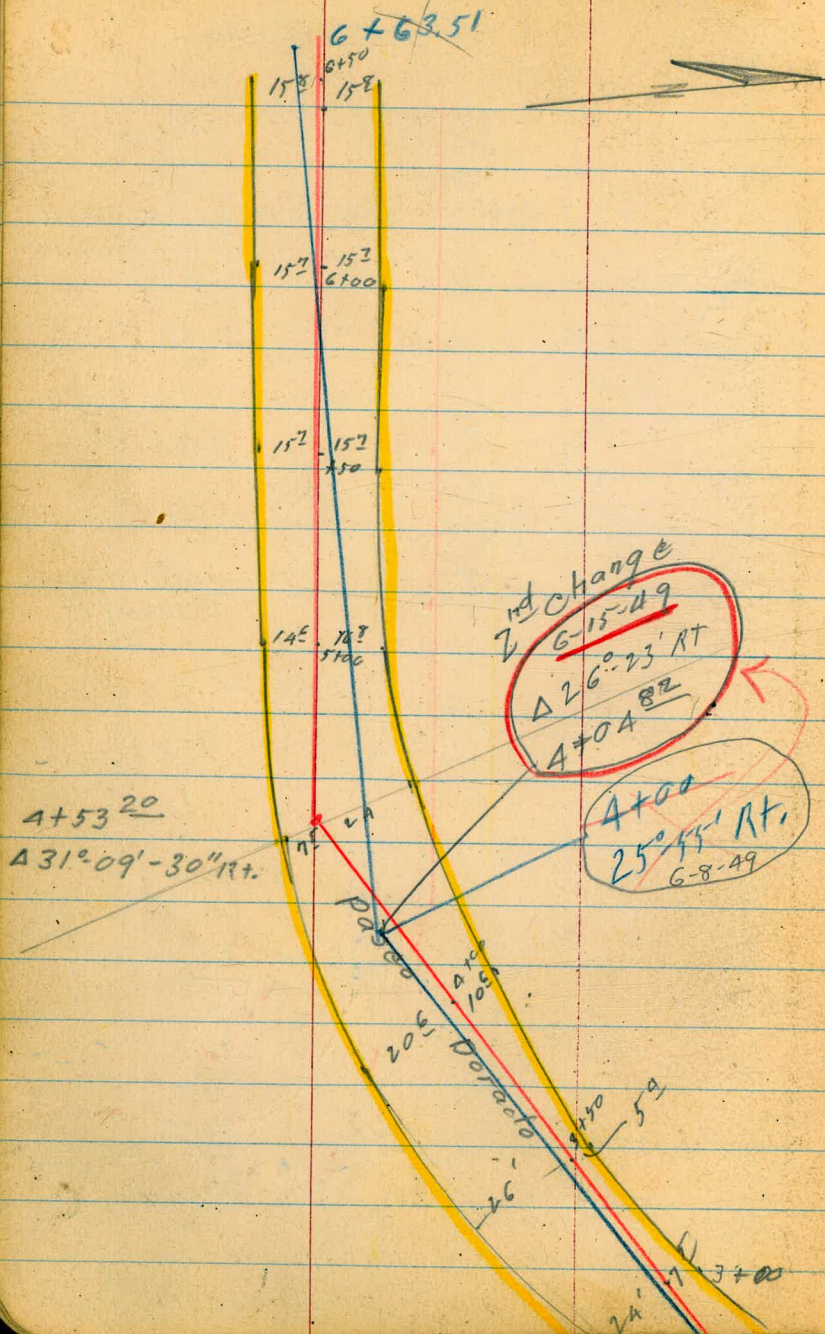
T.P. 0.36 < 45.26 > 12.39 < 44.90 >

N.E.B.P. Torrey Rd

+ Calle de la Plata

2.60 < 57.29 > - 54.69 BM #1





2028
38

Instrument

10+6966

3

Start std. ch.
End roll ch.

Note
 = 6+6409 Ahead }
 6+53⁵¹ back }

Dorado

Paseo

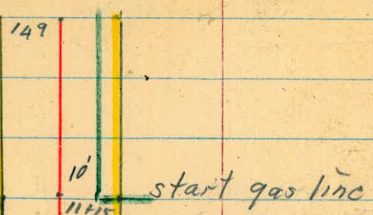
7+57²⁰
 $\Delta 20^{\circ}03'$ RT.

2nd Change
 6+64.09
 $\Delta 23^{\circ}24' - 30''$ RT
 $\Delta 23^{\circ}06' - 15''$ RT

6+6351
 $23^{\circ}55'$ RT
 6-8-49

6+66⁴³ - 0101
 Almarat 1180
 P.42

Red = Prop. Sewer.
 Green = Gas line
 Brown = water line

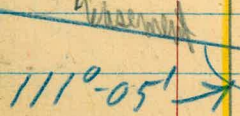


Paseo Dorado

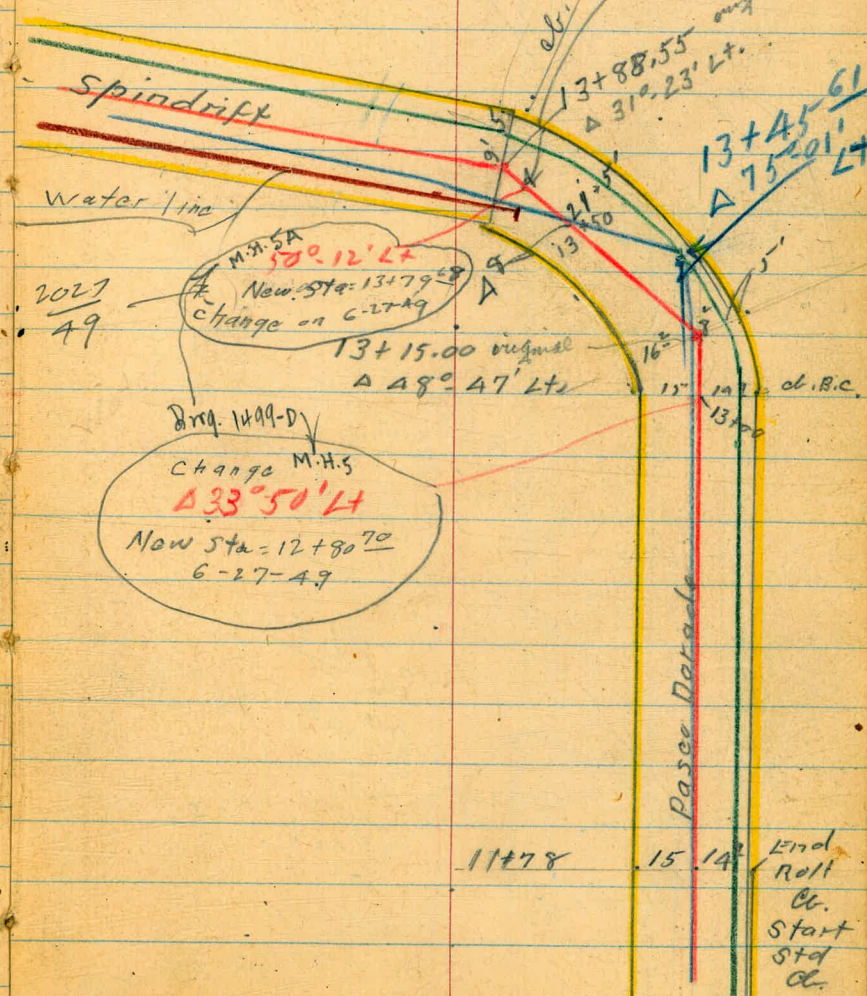
Levels F.B. 2027
 49

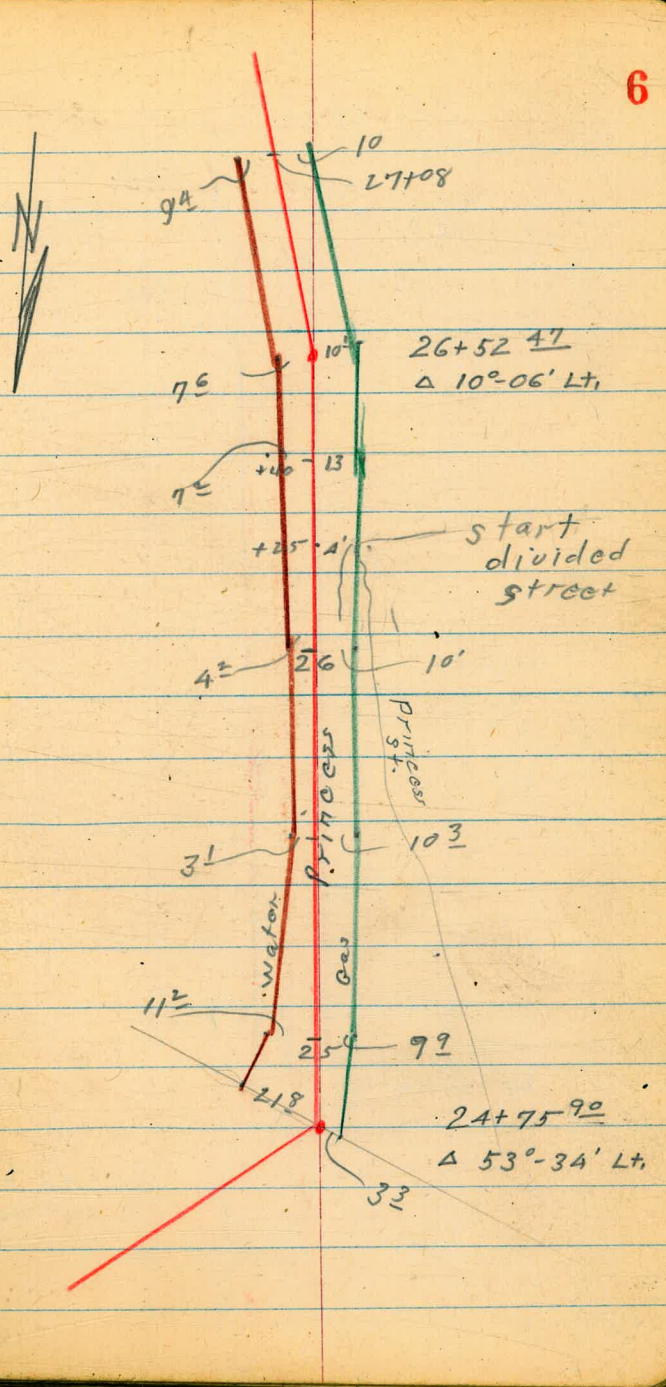
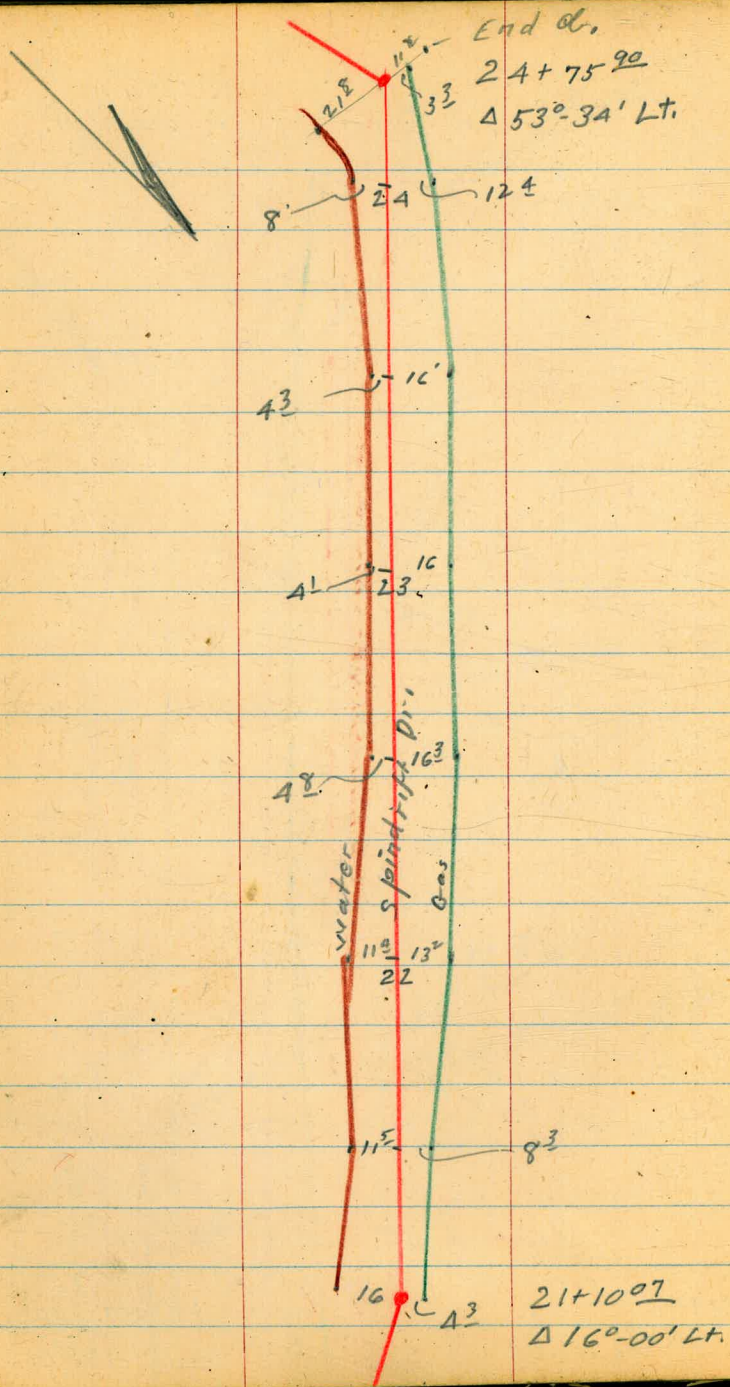
Change to
 $\Delta 4^{\circ} 37' RT$
 6-27-49

2028
 38

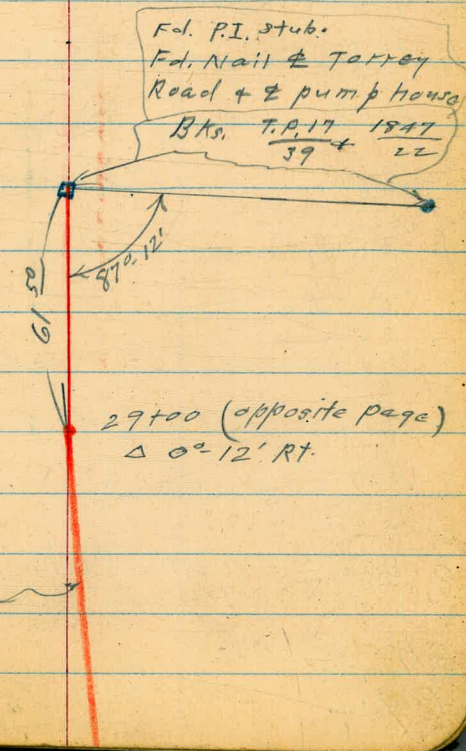
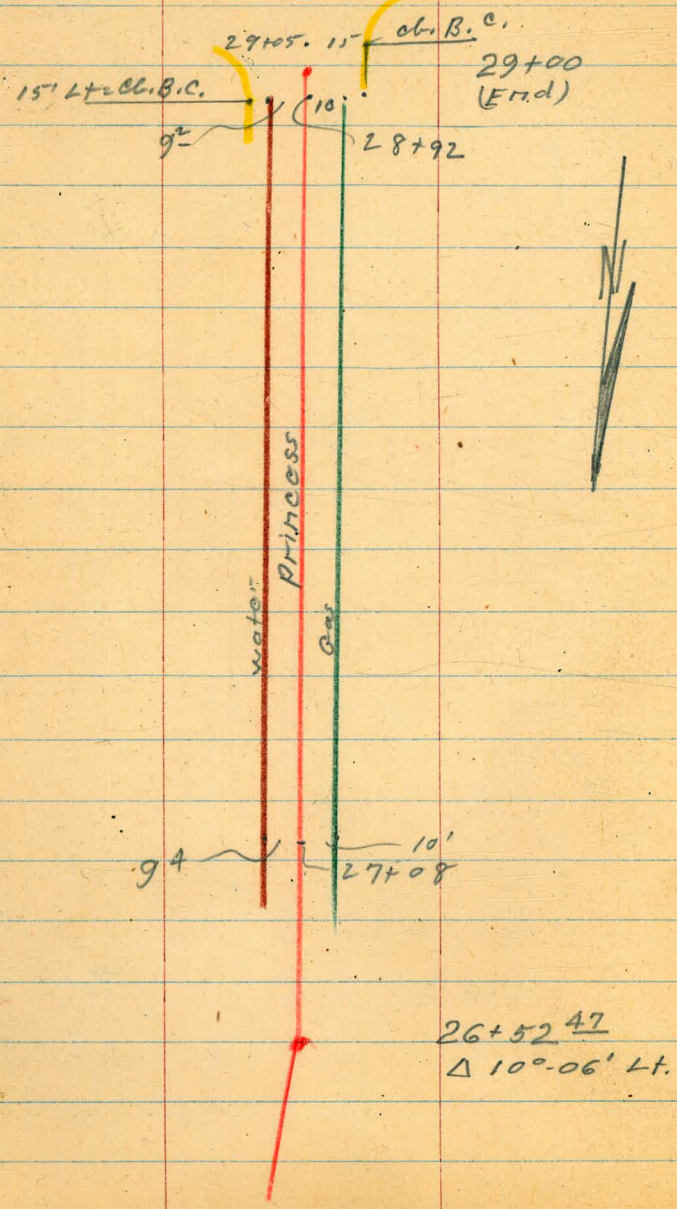


$14^{\circ} 15'$
 9+50





See opposite page for tie.



INDEXED

Paseo Dorado

Calle de la Plata

Wk
APR 29 1949

+4.15 <9.71x> - 4.96 <5.56> TP

2+50 15²LT=Cb. 16²RT=Cb.

2+38 18²LT=Cb. E.C.

2+35 12²LT=Cb. E.C.

2+00 9²LT=Cb. 25²RT=Cb

1+94 28²RT= start curb
on split of Δ

1+56² = Δ LT-20²LT=back with curb. 46²RT=edge PVT

1+33 15²RT= curb B.C.

1+25 15²LT= curb B.C.

1+00 18²LT+18²RT= curb

0+91 14²LT+14²RT= conc. parallel drain

0+5A 17²RT. = cb. Ret. E.C.

0+50

0+36² 17²LT. = cb. Ret. E.C.

{41²LT. = cb. Ret. B.C.

0+15² - 51²RT. = cb. Ret. B.C. Along cb. line
of Calle de la Plata

0+00 = E³ Calle de la Plata atid
Paseo Dorado.

B.M. #2

Page 2.

2.85 <10.52>

7.67

4

8

5.68✓

4.84

15²
Cb

16²
Cb

5.91✓

4.61

9²
Cb

25²
Cb

5.19✓

4.73

46²
Edge Pavt
No curb

5.5A✓

4.98

5.91✓

4.61

7.08✓

3.44

<10.52>

Paseo Dowado
Calle de la Plata

8+00

20° 03' RT
7+57²⁶ Δ RT on split of Δ

+4.40 <6.79> -7.32 <2.39> TP

7+00

14² LT = cb - 16² RT = cb

6+50 = Curb B.C.

15² LT = cb - 15² RT = cb

6+00

15² LT = cb - 15² RT = cb

5+50

14² LT = cb - 16² RT = cb

Pipe = 15 X 0.8 Rectangle

5+26

14² LT = 1.2 X 1.2 drain - 14² RT = 1.2 X 1.2 drain

5+00

14² LT = cb - 16² RT = cb

4+53²⁰

31° 09' RT

= Δ RT. 7² LT = cb - 24² RT = cb on split of Δ

4+00

20² LT = cb - 10² RT = cb

3+50

26² LT = cb - 5² RT = cb

3+00

24² LT = cb - 7² RT = cb

9

13²
cb

1.59 ✓
5.20

17²
cb

80
cb

1.93 ✓
4.86

23²
cb

<6.79> ✓

2.31 ✓

7.40

14²
cb

2.58 ✓

16²
cb

15²
cb

7.13

2.96 ✓

15²
cb

15²
cb

6.75

3.41 ✓

15²
cb

14²
cb

6.30

16²
cb

1.71 ✓
8.00
14²
FLOWLINE

3.61 ✓
6.10
GRTC

3.70 ✓
6.01

2.82 ✓
6.89
GRTC

1.02 ✓
8.69
14.4
FLOWLINE

3.94 ✓

5.77

14²
cb

16²
cb

4.31 ✓

5.40

7²
cb

4.43 ✓

24²
cb

20²
cb

5.28

4.67 ✓

10²
cb

26²
cb

5.04

5.16 ✓

5²
cb

24²
cb

4.55

7²
cb

<9.71> ✓

Paseo Dorado
Calle de la Plata

⊕

10

+5.62

⟨ 7.15 π ⟩ -5.26 ⟨ 1.53 ⟩ TP

11+00

142
cb

1.59 ✓
5.20

156
cb

10+50

142
cb

1.55 ✓
5.24

156
cb

10+00

142
cb

1.46 ✓
5.33

156
cb

9+50

142
cb

1.42 ✓
5.37

156
cb

9+00

142
cb

1.35 ✓
5.44

156
cb

8+85 14.5 RT = 1/2 of 15' x 8' catch basin containing
27-8" pipes draining North
do NOT Cross Road

0.90 ✓
5.89
grate

-0.20 ✓
6.99
14.5
FLOWLINE
WEST END
BOX

8+50

156
End roll
cb.

142
START STD. cb.

1.28 ✓
5.51

152
cb

drain
8+37 3/4 = 15' x 0.2

142 RT = 1/2 12' x 12' Grate for drain

142 RT = 1/2 12' x 12' Grate for drain

-0.43 ✓

1.22 ✓

1.33 ✓

0.78 ✓

-0.73 ✓

7.22

5.57

5.46

6.01

7.52

142
FLOWLINE

142
Grate

142
Grate

142
FLOWLINE

⟨ 6.79 π ⟩

Parque Dorado
Calle de la Plata

(W = water line)

12+72 - 6° LT. = start water line

T.P. 11.81 <17.46> 1.50 <5.65>

+ 50

Δ 48°-47' LT

13+15: Δ LT at 90° to Fwd Tang.

13+00 15° LT: Curb B.C. - 14° RT: Curb 130

12+50

12+00

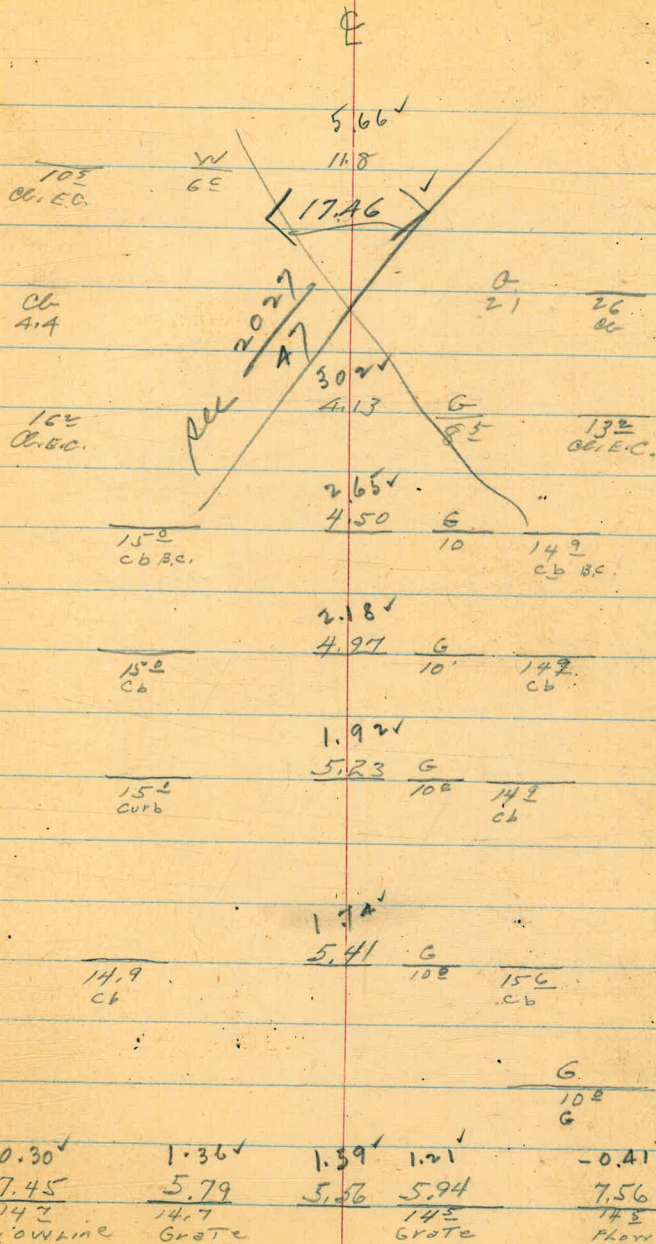
11+78 15° LT: Curb - 14° RT: Face 3rd Curb - 15° BK Roll Cb

11+50

11+15 10° RT: Start Gas Line

2-8" pipes - Catch Basins - 12x12 Grates

11+00: Catch Basins North & South Curb



<7.15 T>

Spindrift

12

16+41

16+00

T.P. 12.66 $\left\langle \begin{array}{l} \downarrow \\ 29.63 \\ \downarrow \end{array} \right\rangle$ 0.47 $\left\langle \begin{array}{l} \downarrow \\ 16.97 \\ \downarrow \end{array} \right\rangle$

15+66 - 15^E Lt. = ob. Ret. E.C.

+
15+54 - 27' Lt. = start ob. Return

+50

+22 - 25^E Lt. = End. ob. Ret.

15+16 - 15^E Lt. = B.C. ob. Ret.

15+00

+50

14+00

(5^E Rt. on split of A = ob. E.C.)

13+88^{EE} = Δ 31^E 23' Lt. (90° to Fwd Tang.)

$\left\langle \begin{array}{l} \downarrow \\ 17.46 \\ \downarrow \end{array} \right\rangle$

16^E ob. B.C. $\frac{W}{10}$ $\frac{G}{83}$ 13^E ob. B.C.

16^E $\frac{W}{11.7}$ 8.12 $\frac{G}{84}$ 13^E ob.

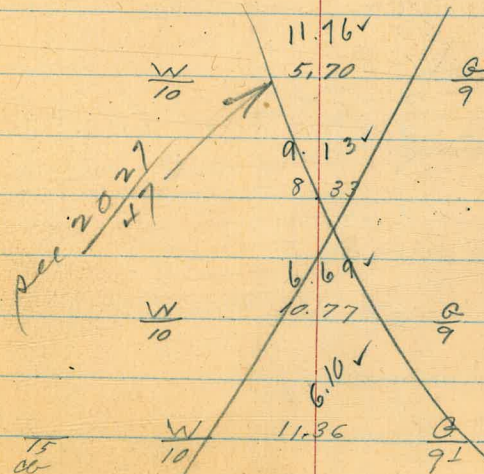
21.51^v
 $\left\langle \begin{array}{l} \downarrow \\ 29.63 \\ \downarrow \end{array} \right\rangle$

$\frac{W}{10.6}$ $\frac{G}{9}$

16.31^v
11.07

$\frac{G}{9}$

14^E ob.



$\left\langle \begin{array}{l} \downarrow \\ 17.46 \\ \downarrow \end{array} \right\rangle$

Spindrift

125' RT = House
 19+17 - 13' Lt = cl. B.C.
 17' RT }
 13' Lt. Also = Return E.C.

on split W of St Louis Terrace
 17+89⁴² Δ 12' 48" Lt. 64' RT = House

+50

17+26 }
 11' RT } = cl. E.C.
 19' Lt }

17+00

+9A

T.P. 11.63 $\langle 40.50 \rangle$ 0.76 $\langle 28.87 \rangle$

17+50

16+77¹⁰ Δ 36-19' RT
 on split of Δ

16+42

16+50

$\langle 29.63 \rangle$

37.53[✓]
 2.97 $\frac{W}{82}$ $\frac{G}{112}$ $\frac{17}{26}$ $\frac{32.9}{7.6}$ $\frac{32.6}{7.9}$ **13**
 13' cl. E.C. Floor Ord.

36.70[✓]
 3.80 $\frac{W}{10}$ $\frac{G}{92}$ $\frac{1.45}{26}$ $\frac{32.4}{8.1}$ $\frac{31.6}{8.9}$
 Floor Ord.

34.94[✓]
 5.56 $\frac{W}{112}$ $\frac{G}{72}$ 125' cl.

19' cl. $\frac{W}{118}$ $\frac{G}{52}$ 11' cl. E.C.

30.85[✓]
 9.65 $\frac{W}{12}$ $\frac{G}{45}$ 13' cl.

$\langle 40.50 \rangle$ $\frac{G}{38}$
 148 ft. Intert. zero. 7' River between lower bank

29.15
 0.48 $\frac{W}{65}$ $\frac{G}{82}$ 19' cl.
 Ed. 26^o Street

26.72
 2.91 $\frac{W}{92}$ $\frac{G}{85}$ 14' cl.

$\langle 29.63 \rangle$

Spindrift

TP Stub 105 Rt 20+70 -6.55 Elev. 40.31
20+50 +1.97 746.86 -10.31 44.89
20+100 +0.56 755.20 59.64

T.P. 11.54 <63.77> 0.59 <52.23>

+50

20+00

+70

Newhouse
Rt. = N. Ely cor. House

+50

19+25 60' Rt. = double Bar.

19+00

T.P. 13.02 <52.82> 0.70 <39.80>

18+50

SE. B.P.
St Louis Terrace
+ Spindrift

3.08 <37.42> +0.02

<40.50>

20+50

46.86

3.62
19.5
Floor
of New House

See Profile
Grade (Sewer)
at 20+50

14' oc. W 9 51.57 1.25 G 12' oc 16' oc

10' oc W 5' 48.47 4.35 G 14' oc 19' oc

38.3' E of present sewer. straight out
-4.8 below floor
110W.

43.1
10.4 G 9.7
6' oc 62' Floor
Ord.

8' oc W 4 45.56 7.26 G 17' oc 21' oc

Home further west by sea 40 lower than Garage
40.1'
12.7
60' Floor

8' oc W 4 42.41 10.41 G 16' oc 21' oc

<52.82>

17' oc W 11 39.35 1.15 G 72' oc 72' oc

<40.50>

Spindrift

+50

21+00 110' RT = House

+50

23+00 98' RT = House

+50

T.P. 9.82 $\left\langle \begin{array}{c} \nearrow \\ 73.08 \\ \searrow \end{array} \right\rangle$ 0.51 $\left\langle \begin{array}{c} \nearrow \\ 63.26 \\ \searrow \end{array} \right\rangle$

22+00

+50

21+10⁰⁷ A 16⁰² Lt (on split.)

21+00

$\left\langle \begin{array}{c} \nearrow \\ 63.77 \\ \searrow \end{array} \right\rangle$

193⁰⁶

W
14

68.6⁰⁰
4.46

G

85

129⁰⁶

123⁰⁶

W
8

68.36⁰⁰
4.72

G

122

172⁰⁶

12.2

130⁰⁶

110⁰⁶

Floor + Drive

56⁰⁰ = Lowest
Sewer out lot

92⁰⁶

W
43

67.79⁰⁰
5.29

G

16

22⁰⁶

8⁰⁶

W
41

66.49⁰⁰
6.59

G

16

22⁰⁶

63.0⁰⁰

64.0⁰⁰

9.7

9.1

98⁰⁶

98⁰⁶

Ordn.

Floor

82⁰⁶

W
48

64.08⁰⁰
9.00

G

162

213⁰⁶

$\left\langle \begin{array}{c} \nearrow \\ 73.08 \\ \searrow \end{array} \right\rangle$

114⁰⁶

W
7

60.99⁰⁰
2.78

G

132

185⁰⁶

100⁰⁶

Ordn.

16⁰⁶

W
115

57.5⁰⁰
6.25

G

82

14⁰⁶

52.4⁰⁰

118⁰⁶

145⁰⁶

Ordn.

21⁰⁶

W
16

54.64⁰⁰
9.13

G

43

88⁰⁶

54.16⁰⁰
9.61

G

52

10⁰⁶

199⁰⁶

W
142

$\left\langle \begin{array}{c} \nearrow \\ 63.77 \\ \searrow \end{array} \right\rangle$

Spindrift also Princess

Lower floor 16

Wyman's sewer complaint 1-9-51
See 2009 for check on sewer + house elev

26+52⁴⁷ = Δ 10° 06' Lt. 41' Rt. = start house

| | | | | |
|----|-----|-------|-----|-------------|
| | | 69.70 | | 12.5 |
| | | 5.17 | Gas | 15 cl. |
| 17 | W | | | 2.5 |
| cl | 182 | | | 412 |
| | | | | House Floor |

26+34 = Cross water line

26+25 = 4' Rt. = End divided street.

26+00

| | | | | |
|------|---|-------------------|-----|----|
| | | 69.4 ^v | | |
| | | 5.45 | Gas | |
| 12.4 | W | | | |
| cl | 4 | | | 11 |

+50

| | | | | |
|------|----|--------------------|-----|------|
| | | 69.11 ^v | | |
| | | 5.70 | Gas | |
| 10.7 | W | | | |
| cl | 34 | | | 10.1 |

one level.

25+00 Cont. bottom floor stepped up, not on
75' Rt. = approx. ctr. of front of house

| | | | | |
|------|----|-------------------|-------------------|-------------------|
| | | 62.3 ^v | 59.4 ^v | 64.4 ^v |
| | | 12.55 | 15.7 | 10.5 |
| cl. | W | | | |
| 19.2 | 11 | 46.8 | 7.5 | 7.5 |
| | | cl | lower level | upper level |
| | | | Floor 1 | |

28' Rt. = N.W. Edge Pave. Princess St.
25+00 10° Rt. = Edge Pave. +

| | | | | | | |
|--|--|--------------------|--------------------|-------------------|-------------------|-------------------|
| | | 69.03 ^v | 68.77 ^v | 68.7 ^v | 62.5 ^v | 61.9 ^v |
| | | 5.84 | 6.10 | 6.2 | 12.4 | 13.0 |
| | | 9 | 10.5 | 12 | 2.8 | 4.6 |
| | | 74.87 | 10.5 | 12 | 2.8 | 4.6 |
| | | | 10.5 | 12 | 2.8 | 4.6 |
| | | | | | | 30.0 |
| | | | | | | Enter |

T.P. Nail 25+00 5.84 $\langle 74.87 \rangle$ 4.05 $\langle 69.03 \rangle$

24+75^v = Δ 53° 34' Lt (on split of Δ)

| | | | | |
|------|-----|--------------------|---|------------|
| | | 68.58 ^v | | |
| | | 4.50 | G | End of cl. |
| 28.3 | W | | | |
| cl | 218 | | | 11.8 |

$\langle 73.08 \rangle$

$\langle 73.08 \rangle$

Princess

see page 19 for check on levels.

S.W. B.R. Princess
& Spindrift

12.84 $\overset{-0.18}{\langle 68.88 \rangle}$ (69.06)

29+05 15' Lt. = cb. Ret. B.C. Torrey Pines
Road & Princess

29+00

82.3 ✓
+ 0.6 Gas
 $\frac{W}{9}$ 10

28+92, 15' Lt. = cb. Ret. B.C. Princess
Torrey Pines Road

15' $\frac{W}{92}$ Gas
10

28+50

19.62 ✓
2.10 Gas
 $\frac{W}{9}$ 10

28+00

T.P. 7.22 $\langle 81.72 \rangle$ 0.37 $\langle 74.50 \rangle$ T.P.#1
+50

16.80 ✓
4.92 ✓
 $\langle 81.72 \rangle$ Gas
10
73.98 ✓
0.89

27+00 15' Lt. = Approx. cb. F.C.

71.44 ✓
3.43 Gas
 $\frac{W}{9}$ 95 15' cb.

$\langle 74.87 \rangle$

$\langle 74.87 \rangle$

St. Louis Terrace

4-11-49

Sommermeier
Allen
Jones

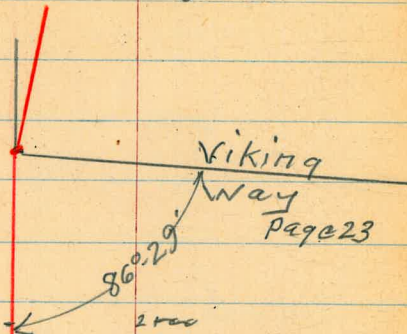
INDEXED

WIK

APR 29 1949

$2+4687$
 $\Delta 11^{\circ}52' Rt.$

Viking
Way
page 23



Rough oil
& rock pave.

1+00

$85^{\circ}06'$
0+00

Spindrift
Line - $17+8942$
(P. 5)



St. Louis Terrace

See 2027
20

2027
20 5+72 18

5+57
End.

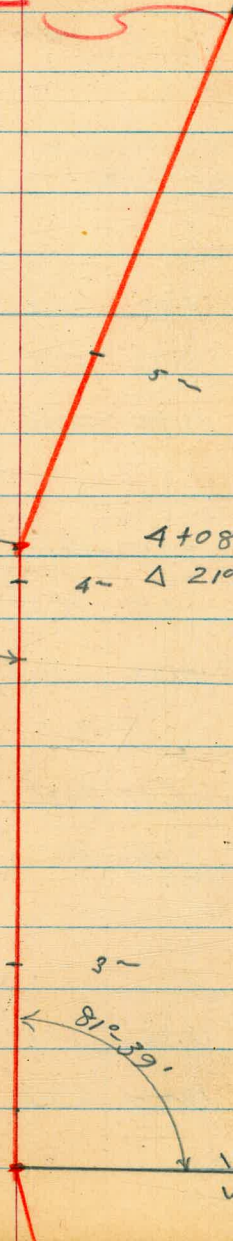
End. (Tie in Δ to
End of line off
Rose land = $17^{\circ}11' Lt.$)

Hypatia
Drive.
(A36)

4+0857

4- $\Delta 21^{\circ}28' Rt.$

$101^{\circ}46'$



$2+4687$
 $\Delta 11^{\circ}52' Rt.$

Viking
way



Check on benches

N.E. B.P.
 Torrey Road + Calle de la
 Orig. B.M. (R2) Plata. 5.83 +0.03 54.72 ✓ (54.69)

T.P. 3.66 60.55 ✓ 12.06 56.89 ✓

T.P. 0.47 68.95 ✓ 1.52 68.48 ✓

Set spike
 Pole # P181
 Roseland
 + Little St. 11.82 70.00 ✓ 7.15 58.18 B.M. #3

T.P. 0.14 65.33 ✓ 12.86 65.19 ✓

T.P. 0.51 78.05 ✓ 13.01 77.54 ✓
 N.W. B.P. Little
 + Torrey Rd. 0.38 90.55 ✓ 6.69 90.17 ✓ (90.11) +0.06 B.M. #2

T.P. 4.71 96.86 ✓ 8.74 92.15 ✓

T.P. 2.53 100.89 ✓ 0.81 98.36 ✓
 N.W. B.P. Torrey Rd.
 + Viking Way 2.83 96.34 ✓ (96.32) B.M. #1 +0.02

T.P. 12.36 99.17 ✓ 0.31 86.81 ✓

T.P. #1-P17. 12.62 87.12 ✓ — 74.50 ✓

St. Louis Terrace
(Sketch - P. 18)

4-13-49

20

2+40

2+27 RT. = Ob. Ret. B.C. (Viking Way)

2+00

T.P. 12.74 $\left\langle \begin{array}{l} \downarrow \\ 61.75 \\ \downarrow \end{array} \right\rangle$ 0.35 $\left\langle \begin{array}{l} \downarrow \\ 49.01 \\ \downarrow \end{array} \right\rangle$

1+50

1+45 9^E Lt. = Ob. B.C.

1+40 20^E Lt. = Ob. B.C.

1+00

G = gas.
W = water
Ob. = Curb

0+50

0+28 = Cross Fire Hydr. Service

+26 - 9^E Lt } = curb return E.C.

0+23 - 21^E RT }
= "T" on water line

0+10 = Cross water line. Also A-Lt.

0+00 St. Louis Terrace line

17+89 1/2 (P. 18) =

S.E.P. Spindrift

St. Louis Terrace 11.96 $\left\langle \begin{array}{l} \downarrow \\ 49.36 \\ \downarrow \end{array} \right\rangle$ - 37.40 Page 14

⊕

53.5 ✓
8.5

$\frac{22.2}{Ob.}$

$\frac{18}{W}$

51.2 ✓
10.6
 $\left\langle \begin{array}{l} \downarrow \\ 61.75 \\ \downarrow \end{array} \right\rangle$

$\frac{G}{LE}$

$\frac{Ob}{7E}$

$\frac{21.2}{Ob.}$

$\frac{16}{W}$

47.0 ✓
2.4

$\frac{G}{5L}$

$\frac{Ob}{8E}$

$\frac{Ob}{13E}$

$\frac{W}{7E}$

42.9 ✓
6.5

$\frac{G}{11}$

$\frac{Ob}{16E}$

$\frac{W}{6E}$

38.9 ✓
10.5

$\frac{Gas}{12E}$

37.1 ✓
12.3

$\frac{W}{4E}$

$\frac{Gas}{16}$

36.6 ✓
12.69

$\left\langle \begin{array}{l} \downarrow \\ 49.36 \\ \downarrow \end{array} \right\rangle$

#

T.P. 6.60 $\langle 80.81 \rangle$ 0.20 $\langle 74.21 \rangle$
 5+00

$\frac{cb}{162}$ $\frac{W}{12}$ 72.8 ✓
 1.6 $\frac{G}{76}$ $\frac{cb}{13}$

4+50

$\frac{cb}{15}$ $\frac{W}{10}$ 68.5 ✓
 5.9 $\frac{G}{93}$ $\frac{cb}{149}$

4+25 - 12² Lt. = E.C. Cb. Ret. (Hypatia Dr.)

4+08⁵⁷ = Δ 21° 28' Rt. (Hypatia Drive)

64.57 ✓
 $\frac{W}{45}$ 7.84 $\frac{G}{135}$ $\frac{cb}{192}$
 Nail
 Δ

3+91 - 13⁸ Lt. = B.C. Cb. Ret. Hypatia Drive

T.P. 13.20 $\langle 74.41 \rangle$ 0.54 $\langle 61.21 \rangle$

$\frac{cb \text{ B.C.}}{138}$ $\frac{W}{84}$ $\langle 74.41 \rangle$ $\frac{G}{11}$ $\frac{cb}{165}$

3+50

$\frac{cb}{175}$ $\frac{W}{135}$ 60.3 ✓
 1.5 $\frac{G}{45}$ $\frac{cb}{108}$

3+00

$\frac{cb}{22}$ $\frac{W}{17}$ 56.3 ✓
 5.5 $\frac{G}{26}$

2+80 Rt. = Cb. P.C.C. (End Cb. Ret.)

$\frac{cb}{215}$ $\frac{W}{165}$ 55.1 ✓
 6.7 $\frac{G}{33}$ $\frac{cb \text{ P.C.C.}}{85}$

2+67 = Cross Viking way water line

2+46⁸⁷ = Δ 11° 52' Rt. (Viking Way)

54.13 ✓
 $\frac{cb}{195}$ $\frac{W}{14}$ 2.62 $\frac{G}{47}$
 Nail
 Δ

$\langle 61.75 \rangle$

$\langle 61.75 \rangle$

Torrey Pines Road
East from
St. Louis Terrace

2+30

26.41
14.0
80
Low. Ground

89.9
8.0
75
Floor
in Back

83.1
9.24
62

clean out (92.41)

2032
25

2+45

NW.
B.P.B.M.#4
Torrey Pines
+ Little

2.30

92.41

90.11

5+72

See 2027
20.

set chiseled B

B.M. Back cor. N. Wly. Ret. walk.

St. Louis Terrace

4 Torrey Road.

3.56 77.25 B.M.#4

+60

77.0 ✓
3.8

.5157: Approx wly. of line lower Torrey road

77.0 ✓
3.8

5+47 15' RT. }
192.41 } = B.C. of Returns Torrey Road.

of. B.C.
148

W
95

76.8 ✓
4.0

G
94

of. B.C.
15

80.81 ✓

80.81 ✓

Viking Way

INDEXED

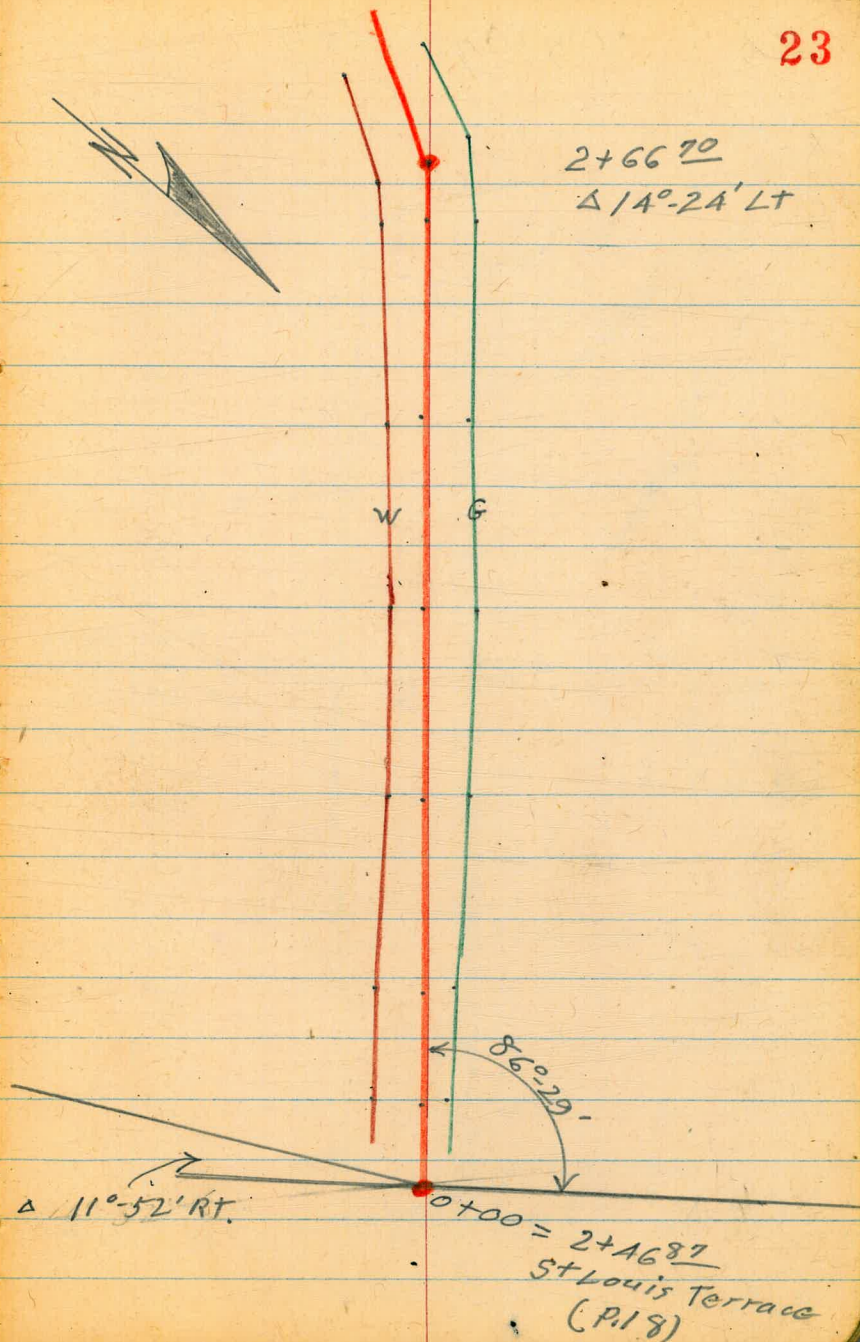
WK
APR 29 1949

A/19/49

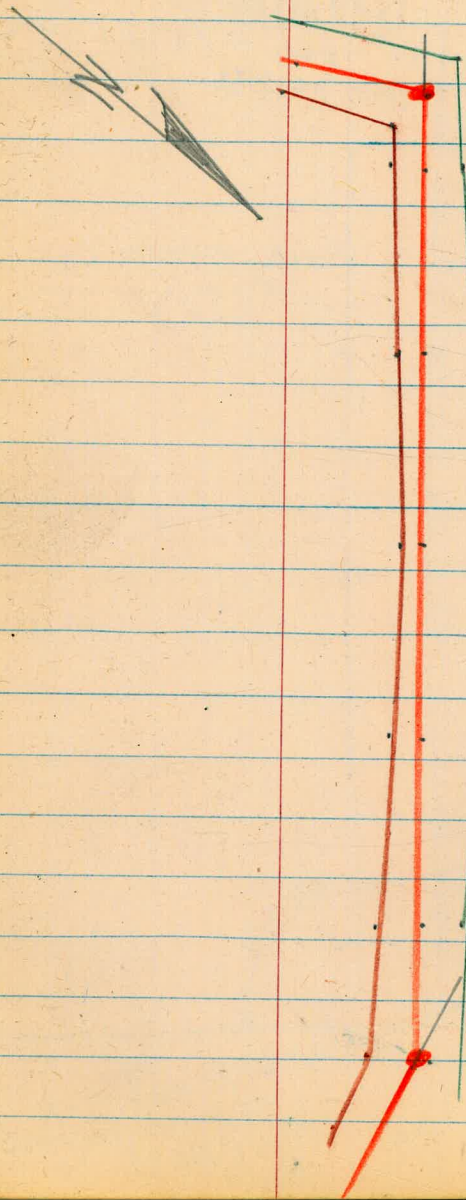
Sommermeier
McCoy
Allen
Jones

23

● = Roofing fact
— = water
— = Gas.



Viking Way

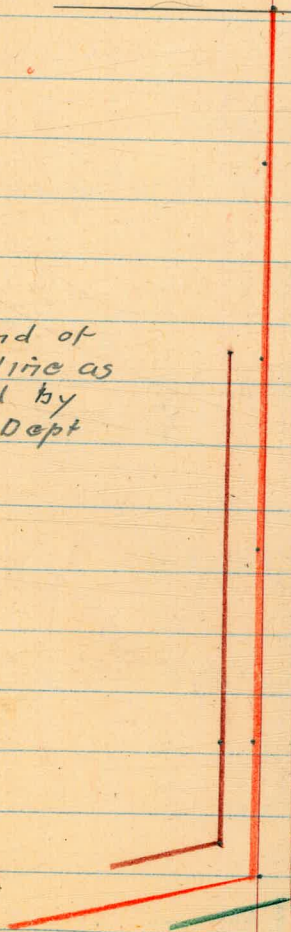


5+16.93
 $\Delta 79^{\circ}-42'-30''$ Lt.

2+66.70
 $\Delta 14^{\circ}-24'$ Lt

6+50 End of
Water line as
located by
Water Dept

7+41.5 = ~~E~~ Torrey Road



Gas line
is 5' off
curb.
Information
by Gas. Co.

5+16.93
 $\Delta 79^{\circ}-42'-30''$ Lt.

Viking Way
Levels (Sketch P. 23+24)

25

1+40

68.9 ✓
10.4

1+20

67.4 ✓
11.9

T.P.

12.85

79.33 ✓

0.31

66.48 ✓

79.33 ✓

1+00

$\frac{cl}{132}$

$\frac{W}{8}$

65.3 ✓
1.5

$\frac{G}{11}$

$\frac{cl}{165}$

0+50

$\frac{cl}{172}$

$\frac{W}{107}$

58.9 ✓
7.9

$\frac{G}{65}$

$\frac{cl}{132}$

0+23 - 20' Lt. = Cl. Ret. E.C.

$\frac{cl}{20}$

$\frac{W}{13}$

$\frac{G}{5}$

0+21 - 10' Rt. = Cl. Ret. E.C.

$\frac{W}{13}$

55.0 ✓
11.8

$\frac{G}{5}$

$\frac{cl}{10}$

0+11

53.8 ✓
13.0

= 0+00

2+46.87 Δ (PZI)

12.56

66.79 ✓

54.13

99.21

54.13 ✓
12.66

66.79 ✓

3+60 110' Rt. = S.E. Cor. of Car. (House at 3+05)

T.P. 11.40 $\langle 90.21 \rangle$ 0.52 $\langle 78.81 \rangle$

3+50

3+05 - 55' Rt. = N.E. Cor. house

3+00 (Gas is supposed to be 5' off. cl.)

2+66⁷⁰ Δ 14² 24' Lt. (on split of Δ)

2+50 - 50' Rt. = \pm house

2+00

1+58 - 42' Rt. = N.E. Cor. House

1+50

$\langle 79.33 \rangle$

\pm

71.9[✓]

18³
110
Floor

$\langle 90.21 \rangle$

77.6[✓]

cl
12²

w
6²

1.7

cl
18²

74.5[✓]

75.9

4.8
5.3
Ord

3.4
5.3
Floor

75.5[✓]

cl
16²

w
10⁵

3.8

cl
14²

74.0[✓]

cl
20²

w
14⁵

5.3

cl
10²

73.3[✓]

cl
18²

w
12

6.0

cl
12

71.9[✓]

71.9[✓]

7.4
4.2
Ord

7.4
4.2
Floor
OF Car

71.5[✓]

cl
14²

w
9.

7.8

cl
16

69.9[✓]

71.1[✓]

9.4
4.2
Ord.

8.2
4.2
Floor

69.3[✓]

cl
13²

w
7

10.0

cl
12²

cl
17²

$\langle 79.33 \rangle$

6+50 End of located water line

T.P. 11.82 $\leftarrow 101.22 \rightarrow$ 0.81 $\leftarrow 89.40 \rightarrow$

92.3 ✓
8.9 ✓
 $\frac{cl}{15}$ $\frac{W}{94}$ $\leftarrow 101.22 \rightarrow$ $\frac{cl}{15}$

6+00

88.8 ✓
1.4 ✓
 $\frac{cl}{15}$ $\frac{W}{94}$ $\frac{cl}{15}$

5+50

5+36 15' Lt. = cl. E.C.

85.5 ✓
4.7 ✓
 $\frac{cl}{15}$ $\frac{W}{93}$ $\frac{cl}{15}$

Curb E.C. (10' Radius)

5+17 15' Rt. = cl. = About 6' East of

$\frac{15}{cl}$

5+16⁹³ Δ 79° 42' 30" Lt. (Taken on split of Δ)

83.9 ✓
6.3 ✓
 $\frac{cl}{215}$ $\frac{\Delta IN}{12}$ $\frac{cl}{158}$

4+98 13^E Lt. = cl. Ret. B.C.

83.6 ✓
6.6 ✓
 $\frac{cl}{135}$ $\frac{W}{8}$ $\frac{cl}{164}$

4+50

81.7 ✓
8.5 ✓
 $\frac{cl}{11}$ $\frac{W}{42}$ $\frac{100}{194}$

4+00 Shot on Gar. floor. (Future plumbing)
93' Rt. = N.W. Cor. Comb. house + Gar.

79.5 ✓
10.7 ✓
 $\frac{cl}{104}$ $\frac{W}{39}$ $\frac{cl}{205}$ $\frac{16.1}{93}$
Gar. Floor

$\leftarrow 90.21 \rightarrow$ ✓

$\leftarrow 90.21 \rightarrow$ ✓

Viking Way

28

Bench Book - 96.32
P-19 = 96.34

N.W. B.R. Torrey Road
& Viking Way (P.19)

4.88 <96.34> x

7+41^E = & Torrey Road + Viking Way

97.8 ✓
3.4

7+35 = Intersect. New trunk sewer

97.8 ✓
3.4

7+25

97.5 ✓
3.7

7+17^E - 15' Rt. = cl. Ret. B.C. Right

7+14^E 15' Lt. = cl. Ret. B.C. Left

7+00

95.8 ✓
5.4

6+96^E = Nail P.O.T.

<101.22>

<101.22>

Roseland Drive
Spindriff to Little

1/2/49

2+75

Levels
P.30

INDEXED

WK

2~ APR 29 1949

Sommermeier
McCoy
Allen
Jones

Ely line Roseland

←25'→

←81°27'→

= 0+00
15+37

Spindriff Dr.
P.5

29

5+87.95
Δ 4°35' RT.

4~

3~

Ely line Roseland

←25'→

3+71.85

←57°55'→

See 201/21

4/8/49

line.
5+93 = Cross Water

Hypatia
Way.

70°06'

2+75

Roseland Drive

Little Street

30

See page 40

8+45⁰⁰
45°-08' Lt.

Little St.

134.52'

90°-30'

8-

7+12
Δ 14°-07'-30" Rt.
7-

Levels @ 35

2+50

22

Also see
Page 40

Fd
Hub.

22⁴²

1420²¹

1-

Fd
Hub

20.15 + 10 + 19.56

= 0+00 for Little St.
8+45⁰⁰ (Roseland).
892.30' Rt.

90°-30'

1+70 35' Lt. = double Gar.

18.8
 $\frac{11.7}{35}$
 Floor

1+50

20.9 ✓
 9.6
 $\frac{W}{9}$

T.P. 12.55

30.51 ✓

0.40

17.96 ✓

30.51 ✓

1+00

18.7 ✓
 0.2
 $\frac{W}{9}$

0+50

15.9 ✓
 2.5
 $\frac{W}{8}$

0+29 - 15' Rt. = Cl. Rot. E.C.

0+23 - 15' Lt. = Cl. Rot. E.C.

14.84 ✓
 3.52

0+10⁵ L

W = water line

$\frac{W}{43}$

= 0+00
 15+37 - P5

15.18 ✓
 3.18

13+88.55

P. 12

12.26

18.36 ✓

+

6.10 ✓

18.36 ✓

Roseland Drive

4+50

T.P.

12.60

54.17

0.83

41.57

4+00

4+50

3+37 63' Lt. = £ House

3+00

T.P.

12.08

42.40

0.19

30.32

2+50

G = gas line

2+25

Cross Gas Service

2+00

55' Lt. = £ House

30.51

37. ✓
17.0
60
Ord.
vacant lot

42.7 ✓
11.5

54.17 ✓

39.7 ✓
2.7

$\frac{G}{10}$

36.2 ✓
6.2

33.6 ✓ 33. ✓
8.8 Floor 63
7.2 Ord 63

32.2 ✓
10.2

$\frac{G}{10}$

42.40

28.1 ✓
2.4

$\frac{G}{10}$

$\frac{G}{106}$

22.0 ✓ 22.9 ✓
8.5 Floor 55
55 Grd

24.2 ✓
6.3

$\frac{W}{73}$

30.51

Floor Level.
of house, Plumbing on lower

6+30 52' Lt. = house 87' Lt. = back

40.8 ✓ 46.7 ✓ 47.5 ✓ 50.6 ✓
13.4 ✓ 5.5 ✓ 6.7 ✓ W 3.6 ✓
87 ✓ 52 ✓ 52 ✓ 132 ✓
Floor ✓ Ord ✓ Floor ✓ Ord ✓

This facade
seems in basement
at end of same

5+93 = Cross Hypatia way water line.

5+87²⁵ = Δ 4°-35' RT. (Also = 0+00 Hypatia Drive
line)

W
83

49.03 ✓
5.14
4 Nail

G
10

5+80 10' RT = Gas line T

Gas T
10

5+50

47.5 ✓
6.7

5+32 15' Lt. = start conc. cb.

45.2 ✓

5+00

W
10

9.0

G
10

A+87 Cont. 153 Lt. = back of house.

48.7 ✓
25.5 ✓

30.9 ✓
24 ✓

outlet
pipe

Ord.
Back of house

38.6 ✓

37.5 ✓

44.6 ✓

15.6 ✓

16.7 ✓

9.6 ✓

103

100

Floor
(top floor)

Ord

54.17 ✓

54.17 ✓

A+87 - 103' Lt. = E house (See above.)

= 0+00 Little Street. (Cont. P. 35)

8+45 = Δ $89^{\circ}30'$ to Little St. Line
 + $45^{\circ}08'$ Lt. to Continuation
 Roseland See. page 40)

8+34. 11' Lt = Δ in water line

8+00

7+48 (on extension of Back Line from 7+12)

7+50 - A^S Rt. = End of marked Gas line

7+50

7' below floor.
 sewer outlet at back of house

7-22 - 45' Lt. = Δ house

Δ 7+12⁰⁰ Δ $14^{\circ}07'30''$ Rt.

T.P. on Nail Δ 11.35 $\langle 64.60 \rangle$ 0.92 $\langle 53.25 \rangle$

7+00

6+67 - 21^A Lt. = End Cono. Cl.

6+50

$\langle 54.17 \rangle$

W ditch
 1 A^E
 on split of Δ

7.93

Nail

56.6[✓]

8.0

W
 11

56.0[✓]

8.6

W
 13

54.5[✓]

10.1

G
 4E

53.6[✓]

52.8[✓]

11.0

11.8

45

45

Floor

End

8+45 = 56.67
 1.90
 57.57
 7.60 310

Joint in Floor
 Sewer Outlet

53.25[✓]

11.35

W
 14
 Approx.

$\langle 64.60 \rangle$

G
 5

52.5[✓]

1.7

W
 15
 Approx.

G
 4A

51.7[✓]

2.5

W
 16

G
 4

51.2[✓]

3.0

$\langle 54.17 \rangle$

Little St.

35

INDEXED

WK

B.M. #2, P. 19

APR 29 1949

3.36

90.19

B.M. #2
P. 19
90.17

T.P.

6.42

93.55

1.74

87.13

2+50

W
8

83.0 ✓
5.9

T.P.

11.96

88.87

0.13

76.91

88.87 ✓

2+00

W
7.5

76.1 ✓
0.9

1+50

W
7

70.8 ✓
6.2

1+00

W
6.5

66.0 ✓
11.0

T.P.

12.87

77.04

0.43

64.17

77.04 ✓

0+50

(water dept. spotted water
line 12' Left. Trench shows
up as indicated at right.)

W
6?

61.0 ✓
3.6

= 0+00

8+45 Δ 89°-30' Rt. P. 30+35

W
6

56.67 ✓
7.93

64.60 ✓

64.60 ✓

Hypatia Way DRIVE
Roseland Dr. to St. Louis Terrace

36

INDEXED
WK
APR 29 1919

Sommermaier
McCoy
Allen
Jones

2+28³³
Δ 9° 25' RT.



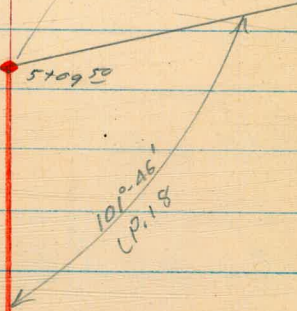
Roseland Dr.

= 0+00
5+87²⁵ (P. 29)



5+09⁵⁰

4+08⁵⁷
St. Louis Terrace
Line



101° 26'
LP. 18

A~

3+24⁶⁰
Δ 17° 11' RT.

Hypatia Way DRIVE

37

T.P. 5.84 $\langle 77.10 \rangle$ 3.01 $\langle 71.26 \rangle$

2+28³³ $\Delta 9^\circ 25'$ Rt. (P. 37)

2+00

1+50

T.P. 12.50 $\langle 74.27 \rangle$ 0.12 $\langle 61.77 \rangle$

1+00

0+50

0+13

0+10 3.5 Rt. = Gas. 'T'

= 0+00

5+87⁹⁵ $\langle 61.89 \rangle$
 P. 33

$\langle 49.03 \rangle$

71.26 ✓
 $\frac{W}{6}$ 3.01 $\frac{G}{9}$

69.5 ✓
 $\frac{W}{9}$ 4.8 $\frac{G}{52}$

65.1 ✓
 $\frac{W}{11}$ 9.2 $\frac{G}{3}$

$\langle 74.27 \rangle$

59.9
 $\frac{W}{10}$ 2.0 ~~$\frac{G}{22}$~~

53.6
 $\frac{W}{82}$ 8.3 $\frac{G}{22}$

49.5 ✓
 12.4

49.03
 12.86

$\langle 61.89 \rangle$

A+89^E 10' L. } start Ob. returns.
 10' R. }

+50

A+00

+50

3+24^E Δ 17' 11" Rt.

3x10⁰ *con lincis in dist. ground.*
 This house need not be considered as
 there is a wide easement between
 property of Calloway + I. B. Davis (Roll 6101)

2+95 175' Rt. = Ely Face House

2+90± = wly line private way

2+70± = Ely line private way to North

77.10

Ob. end
10

W
45

64.6[✓]

12.5

G
55

Ob. end
10

66.7[✓]

10.4

G
44

69.0[✓]

8.1

G
4

70.9[✓]

6.2

G
53

71.65[✓]

5.45

G
8

65.4[✓]

11.9
175
Ord

66.5[✓]

10.6
175
Floor

72.2[✓]

4.9
50

72.2[✓]

4.9
50

65.7[✓]

11.4
150

62.2[✓]

14.9
200

72.3[✓]

4.8
9

72.0[✓]

5.1
50

65.1[✓]

11.4
150

61.7[✓]

15.4
200

77.10

Hypatia Way DRIVE

39

5+09⁵⁰ = (4+08⁵⁷ (Page 18) St. Louis Terrace.)

4197

64.63[✓] (64.57 - P. 21)
12.47

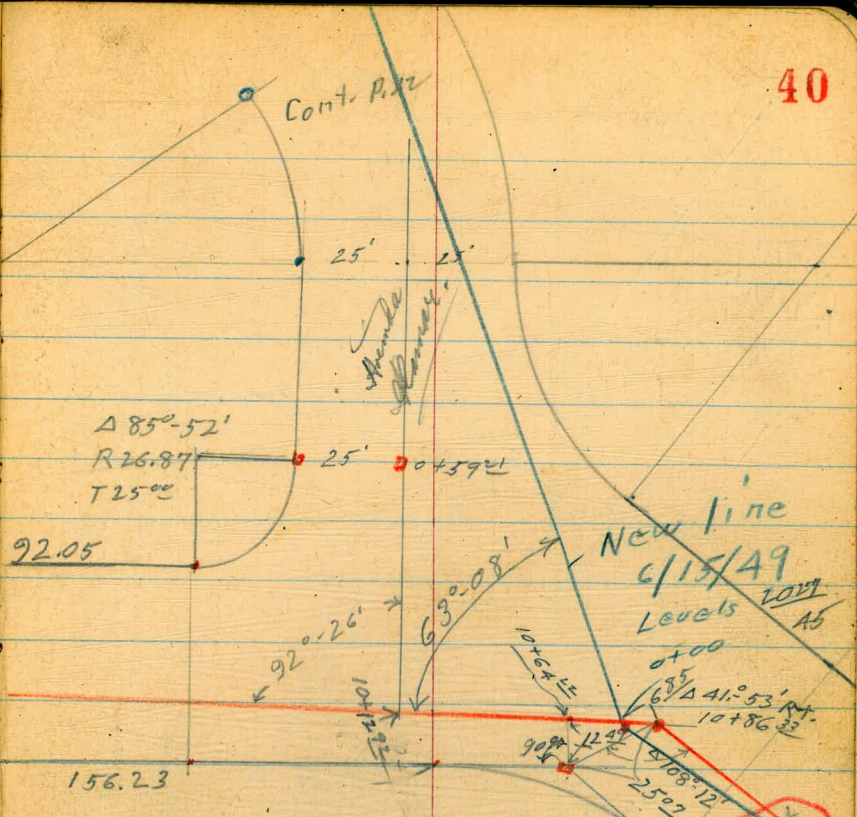
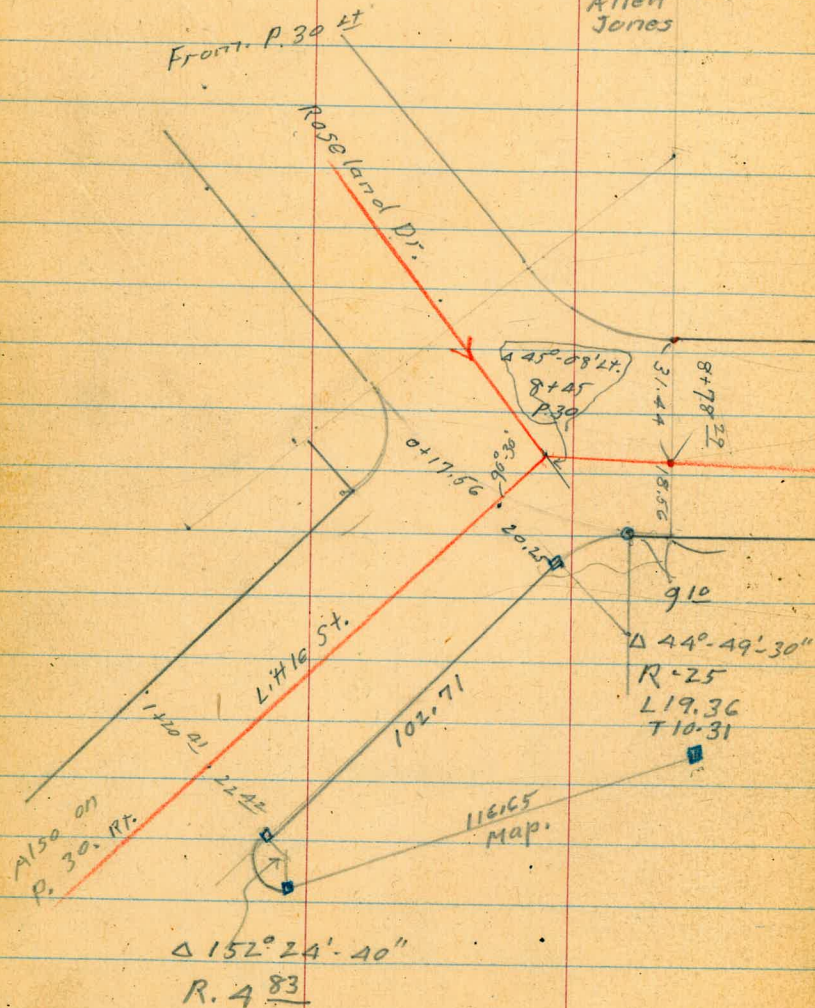
63.9[✓]
13.2
 $\frac{W}{45}$ $\frac{Q}{55}$

77.10[✓]

Little St.
Portion of Roseland Drive

4-28-49

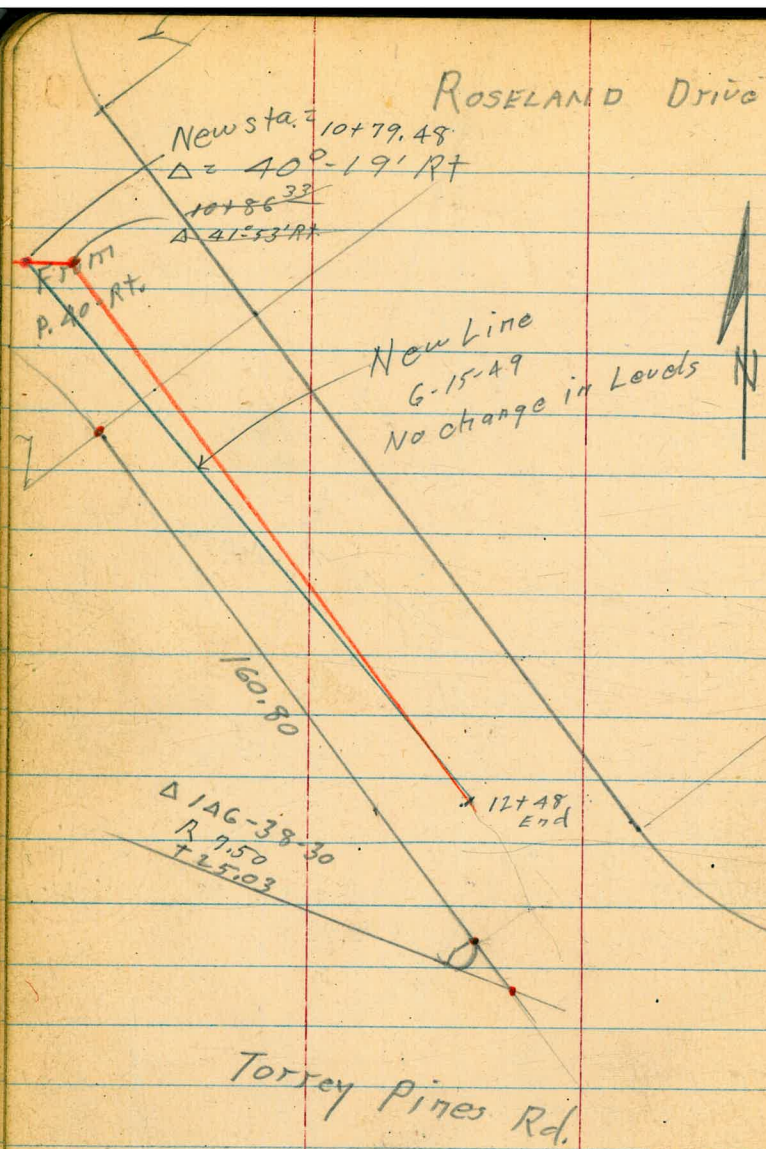
Sommermeier
McCoy
Allen
Jones



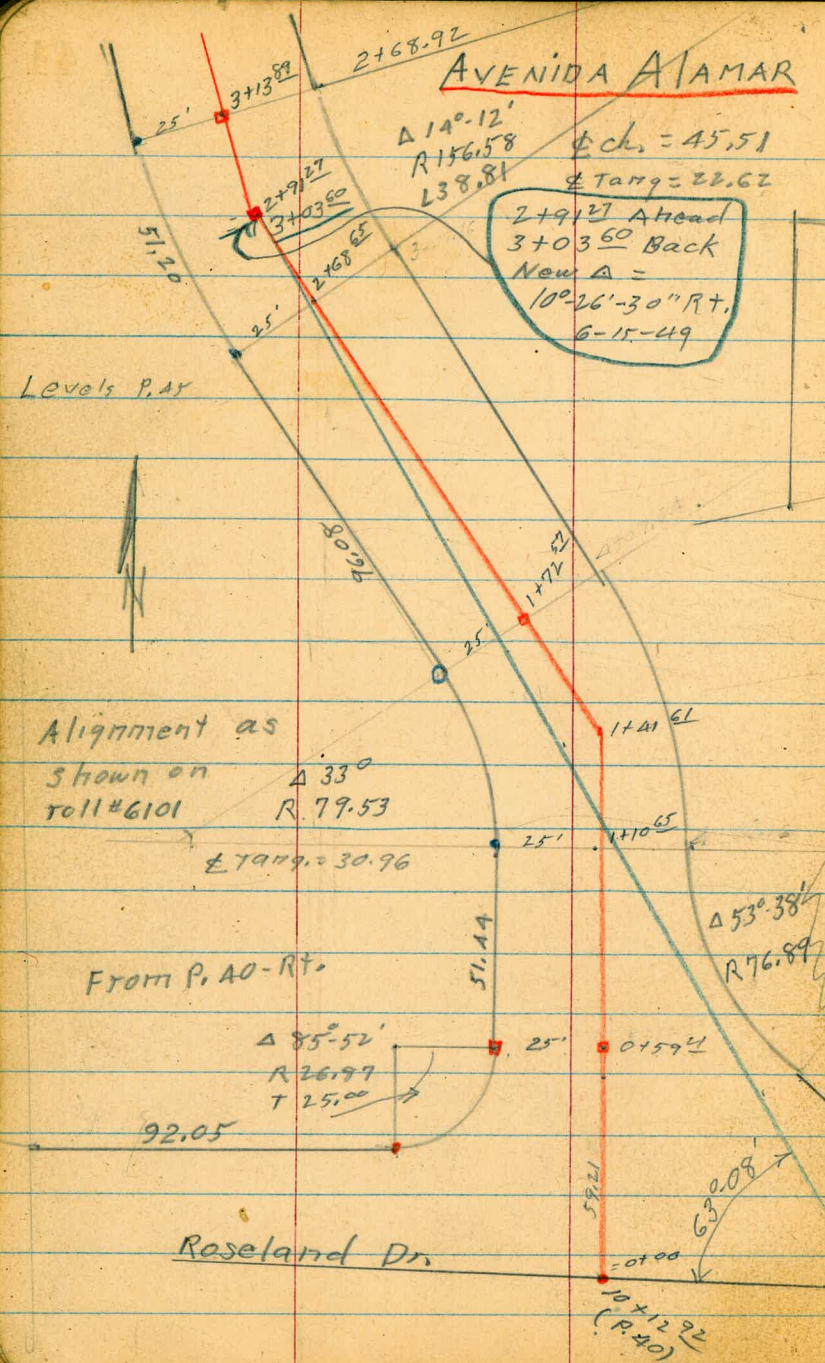
Alignment as shown
on Roll #6101

- Fd. Pit
- Fd. Pipe
- Fd. Hub
- Fd. Man.
- Set Nail
- Hub or stub.

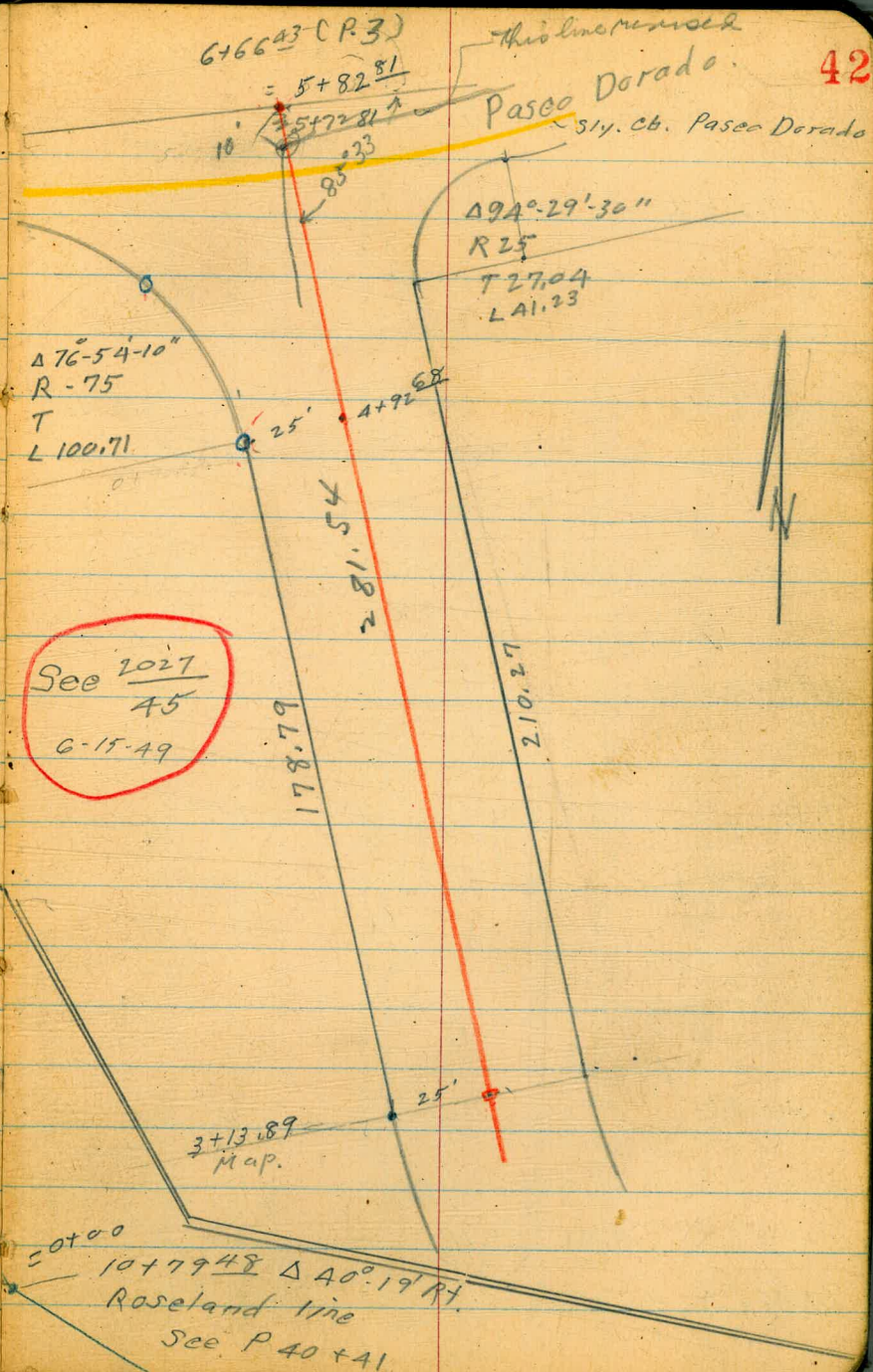
Δ 40° 30'
R 93.72
T 34.58
L 66.25



AVENIDA ALAMAR



6+6643 (P. 3)



Levels From P. 34

Roseland Dr. Cont.

Sketch P. 40

10+72 = Cross gas line

10+50

10' RT of Sta. 10+13

Set Nail B.M. Pole # 7985

oiled road

999 $\langle 44.75 \rangle$

B.M. #4

W
135

42.9 ✓
12.4

10+12⁹² = (0+00 Avinida Alamar line)

W
18

42.76 ✓
11.98
Nail

10+00

roads on
these

T.P.

9.78

$\langle 54.74 \rangle$

12.15

$\langle 44.96 \rangle$

43.2 ✓
11.5

$\langle 54.74 \rangle$

+50

W
19

47.1 ✓
10.0

9+00

52.2 ✓
4.9

8+78²⁹

W
165

54.6 ✓
2.5

B.M.C

0.44

$\langle 57.11 \rangle$

$\langle 56.67 \rangle$

8+45 = Δ 45°-08' Lt. El. = From P. 34

$\langle 57.11 \rangle$

Roseland Drive

orig B.M. (8745 P 43)

3.93 $\langle 56.68 \rangle$ $\langle 56.67 \rangle$

12+74 intersect water line

58.6 ✓
2.0

12+48

$\frac{W}{63}$

56.9 ✓
3.7

T.P.

6.14 $\langle 60.61 \rangle$

0.27 $\langle 54.47 \rangle$

$\langle 60.61 \rangle$

12+00

$\frac{W}{12}$

53 ✓
1.5

+50

$\frac{W}{10}$

48.9 ✓
5.8

11+00

$\frac{W}{72}$

44.7 ✓
10.0

10+86³³ = Δ 41°-53' RT.

5.8

43.9 ✓
10.8

$\frac{W}{\text{split of } \Delta}$

$\langle 54.74 \rangle$

$\langle 54.74 \rangle$

Avenida ALAMAR

Sketch P 42

20' Lt. of 1+41⁶¹

T.P. Pole 7955 0.30

$\left\langle \begin{matrix} 33.02 \\ 12.86 \end{matrix} \right\rangle \left\langle 32.72 \right\rangle$

1+41⁶¹ = Δ 33° Lt

INDEXED

WK

APR 29 1949

1+10⁶⁵ 25' Rt. = P.R.C.

25' Lt. = B.C.

1+00

+59⁴¹ = B.C. on Lt.

+50

+47 Cross gas line

+27

+23 End oil

+18 = Cross water line

0+00 (P. 42)

B.M. # 4
P. 43

0.83
4.83

$\left\langle \begin{matrix} 45.58 \\ 47.58 \end{matrix} \right\rangle$

$\left\langle 44.75 \right\rangle$

$\begin{matrix} 31.0 & 31.4 & 28.4 & 31.8 & 31.8 \\ \hline 1.6 & 1.2 & 1.2 & 1.8 & 1.8 \\ 20 & 10 & 6 & 3 & \end{matrix}$

$\begin{matrix} 33.5 & 33.4 & 30.8 & 34.4 & 35.0 \\ \hline 12.1 & 11.7 & 14.8 & 11.2 & 10.6 \\ 10 & 2 & & 5 & 20 \end{matrix}$

$\begin{matrix} 34.4 & 31.6 & 34.7 & 34.4 \\ \hline 11.2 & 14 & 10.9 & 11.2 \\ & 5 & 10 & 20 \end{matrix}$

$\begin{matrix} 38.4 & 38.4 & 35.0 & 37.6 & 37.6 \\ \hline 7.2 & 7.4 & 10.6 & 8.0 & 8.0 \\ & 8 & 10 & 13 & 20 \end{matrix}$

$\begin{matrix} 39.1 \\ \hline 6.5 \end{matrix}$

$\begin{matrix} 41.9 \\ \hline 3.7 \end{matrix}$

$\begin{matrix} 41.8 \\ \hline 3.8 \\ 15 \end{matrix}$

$\begin{matrix} 42.0 \\ \hline 3.6 \\ \text{oil} \\ \text{Road} \end{matrix}$

$\begin{matrix} 42.8 \\ \hline 2.8 \\ \text{oil} \\ \text{Road} \end{matrix}$

$\left\langle 45.58 \right\rangle$

3400

21.48 T

TR 5106 R+91.27

0.65 21.48 T 12.19

20.83

R+91.27

Δ HUR RT

10° 26'

30 RT 6.15-49 Hots

R+68.65

25 L.F.C

R+50

+28

+18

R+00

+74

+72

+64

1+516

33.02 T

¢

19.0 ✓

2.5

21.48 T

20.83 ✓

12.19

5706

22.34 ✓

10.68

5706

23.6 ✓

9.4

25.3 ✓

7.7

8

24.0 ✓

9.0

3

35.9 ✓

7.1

7

27.2 ✓

5.8

5

25.3 ✓

7.7

24.0 ✓

9.0

24.9 ✓

8.1

5

25.4 ✓

7.6

5

26.1 ✓

6.9

2

27.5 ✓

5.5

5

29.1 ✓

3.9

8

26.4 ✓

6.6

4

29.3 ✓

3.7

27.3 ✓

5.7

29.3 ✓

3.7

29.7 ✓

3.3

10

26.8 ✓

6.6

31.0 ✓

2.0

30.0 ✓

3.0

3

31.2 ✓

1.8

5

29.6 ✓

3.4

10

28.2 ✓

4.8

3

33.02 T

5+00

6.01 ✓
4.58
10.0
Edge oil drive

5.8 ✓
4.8

TP

160 $\langle 10.59 \pi \rangle$ -12.49 $\langle 8.99 \rangle$

$\langle 10.59 \pi \rangle$

4+50

9.53 ✓
11.95
8.5
Edge oil drive

9.8 ✓
11.7

4+00

13.41 ✓
8.07
13.3
Edge of parallel
oil drive
Drive 9.7 wide

13.4 ✓
8.3

+76

Edge oil drive

16.09 ✓

3+54

5.39
Leave oil drive
17.39 ✓
2.11

17.46 ✓
4.02
7
Edge oil drive

+50

oil drive

17.64 ✓
3.90
oil

+39.6

Edge oil drive

18.04 ✓
3.40
Enter oil drive

+32

18.39 ✓
3.09
17
Edge oil drive

18.3 ✓
3.2

3+13⁸⁹ 25' RT BC.

19.6 ✓
1.90
Stub

$\langle 21.48 \pi \rangle$

$\langle 21.48 \pi \rangle$

£

Paseo Dorado line (P33) 49

TP = 7+57.20

-8.63

193

1.96 ✓

New Sta: 5+72.31
6-19-49

∠ 85°33' IN NE

5+82.81

Tie Paseo Dorado line

2.50 ✓

8.09

5+67.6

Gutter

2.44 ✓

8.15

5+67.1

Top roll type curb

2.78 ✓

7.81

5+50

3.3 ✓

7.3

<10.59 A> ✓

<10.59 T> ✓

TORREY Road,
Charlotte St. S'y.

5/5/49

INDEXED
WK
MAY 19 1949

- = Set Disk
- = Set. Stub.
- = " Nail
- X = Cut Cross
- = Fdr. Hub.
- = Fdr. Disk.

Sammermeyer
McCoy
Allen
Jones

2+25

Levels P 53

Sec 2016
 37
 12-22-49

1+46.40
Δ 82°-17' Lt.

■ 8' curb

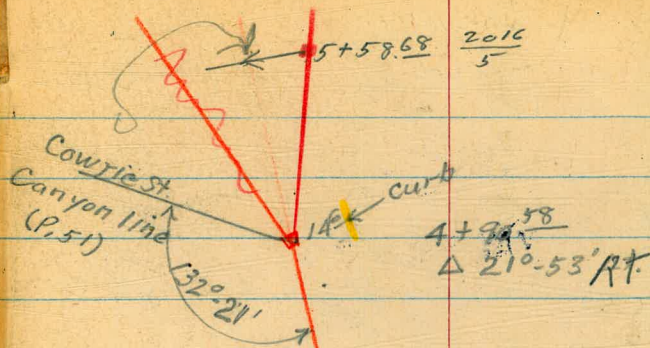
Use line in FB 2016
 42



RO.T. 0+14



Pump station
under Const.
(Charlotte St.)



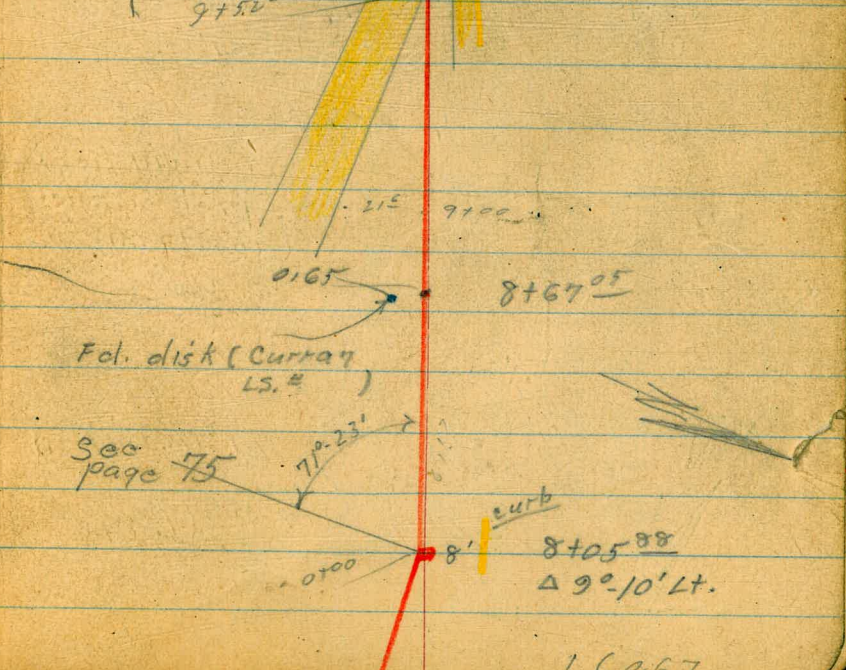
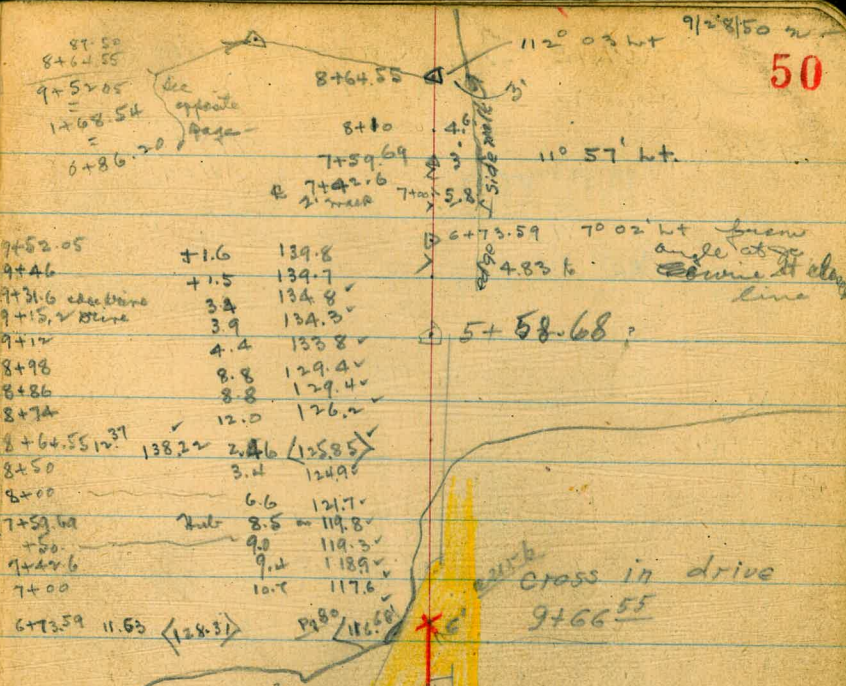
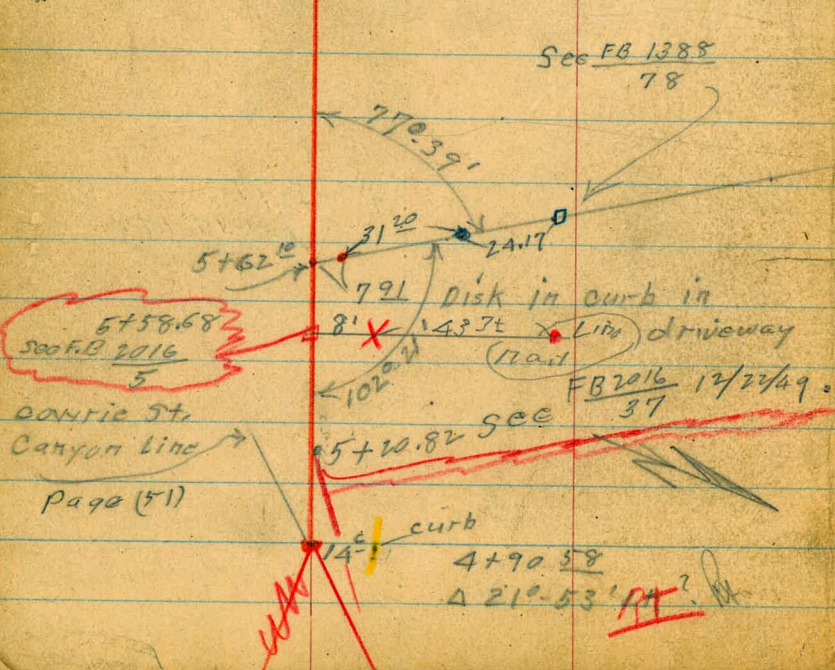
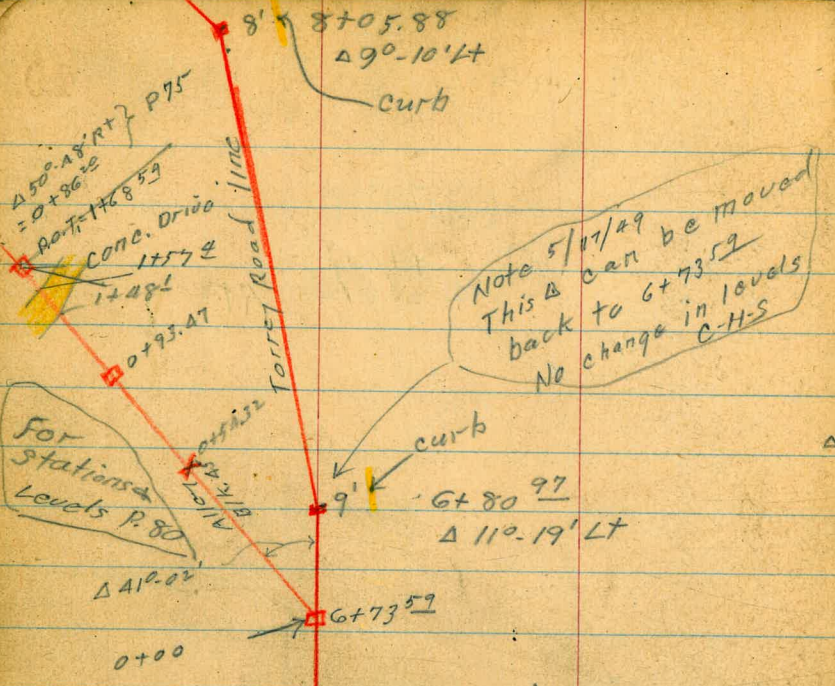
Levels - P 53

163.45

7' curb
3+27.10
Δ 10°-17' Lt

180.7

2+25



COWRIE ST Canyon 11110
(Cowrie St. is closed)

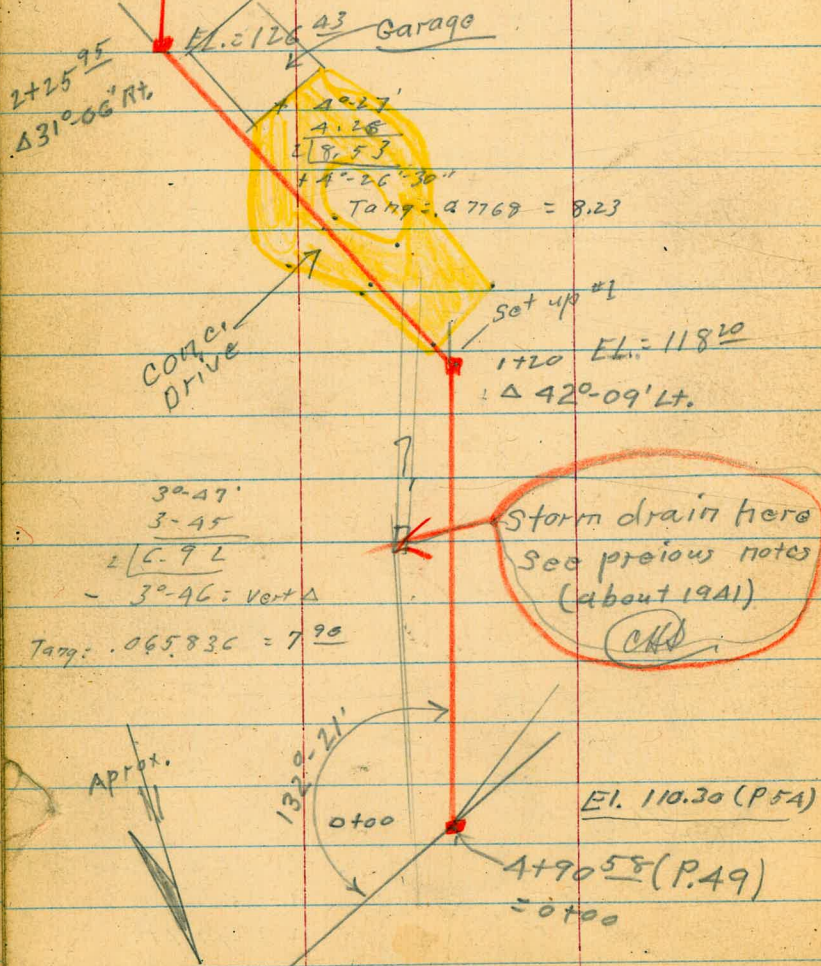
4-10-49

INDEXED

MAY 19 1949

W.K. Sommermeyer
M. McCoy
Allen
Elevation by stadia
distances - chained

Vert. A = $\frac{\text{down}}{\text{up}}$ Δ Right side up + Δ Upside down
Z



Levels - P.66

5+30

11.43 Rod
3.98 Foot
15.41 - Level reading
- 4.75 = Δ at Set up #7
+ 10.66 = Net diff. in EL.

EL. = 144.44

4+60.00
 $\Delta 16^{\circ}27' \text{ RT}$

+ $\Delta 4^{\circ}16'$
4.15
2 | 8.31
Vert. = 4-15-30
Tang. = .07224 = 6.26'

EL. = 138.15

Set up #2
3+75.73
 $\Delta 13^{\circ}01' \text{ LT}$

- 4-31
4-27
2 | 8.60
4-30 = Vert. A
Tang. = .07970 = 11.75

APPROX.

See
2016
5-15
12-15-49

Note

2+25.95
 $\Delta 31^{\circ}06' \text{ RT}$

COWRIE ST. CANYON LINE.

206.38 = El. T.P. (on right)

1.11
207.49
12.96
194.53
0.37
194.92
7.02

187.90 = N.W. B.P. Virginia Way + Prospect Place

194.92
13.07
181.85
54

182.37
12.69
169.70
11

169.81
12.09
157.72
1.84

159.54 EL = 167.56

7.30
152.24 = S.E. L+T.
Prospect & Torrey Rd
(see page 56)

APPROX.



25° 12'
5-11
110-23
5-11-30 = vert. A.
Tang. = .109086 = 12.46'

setup #3 $\times 4^{25}$

EL = 155.10
5+69 93
11° 45' RT.

+ 18° 38'
18-36'
36-74
+ 18-37 = vert. to T.P. set. 52.8 from setup #4 **52**
Tang. = .33686 17.79 (Δ direct to T.P.)
5.13 = \times
22.92
183.46 = El. setup #4
206.38 = El. T.P.

APPROX.



EL = 183.46
8+54 65 P.O.T. setup #4. $\times 5^{13}$

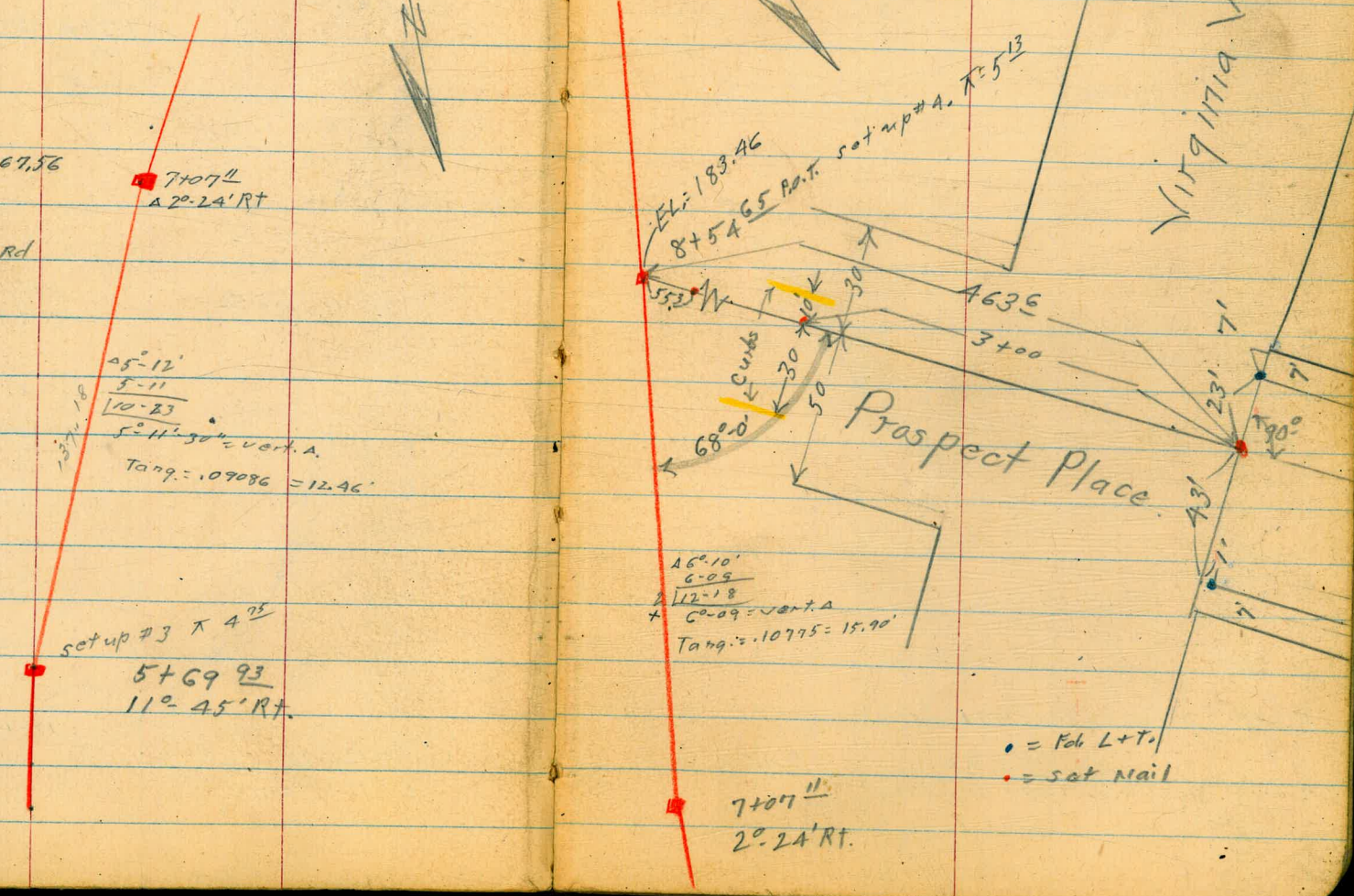
4635
3+00
Prospect Place

45° 10'
6-09
112-18
6-09 = vert. A
Tang. = .10775 = 15.90'

7+07 11.
2° 24' RT.

• = Fds L+T.
• = set nail

Virginia Way



Torrey Road (Charlotte side)

2/7/29

(Sketch P. 49)

Sommermeier
McCoy
Allen

2+50

INDEXED
WK
MAY 19 1949

2+00

T.P.

12.01

106.93

0.16

94.92

1+50

1+46²⁵ Δ 8°-17' Lt.

1+00

0+50

0+20

0+00 (dug out. Pump house under Const.)

10.84 95.08

84.24

B.M. on Ch. 3A.51 R.P. to pump house

G-250

101.0 ✓

5.9

99.11 ✓

7.82

85
00

96.7 ✓

10.2

95.69 ✓

11.24

84
00

106.93

92.5 ✓

2.6

92.2 ✓

2.9

91.89 ✓

3.19

8
Top. 00

89.2 ✓

5.9

89.9 ✓

7.2

87.0 ✓

8.1

95.08

Torrey Road

54

5+50

114.0 ✓
2.0

5+43

inside edge of walk
2nd Rt. = start. 5' Comb cl. + walk
M.H. 4' wide inside walls = 0.5 ft thick.

5+26

3rd Rt. = Ctr. telephone Co. M.H.

~~Cont. from FB 2016 - P. # 44~~

5+00

110.7 ✓
5.3
110.30 ✓
111.06 ✓
4.94
125.00

4+90⁵⁸ Δ

21°-53' Lt. (Canyon line P. also = 0+00 - Courier St)

5.70

110.80 ✓
5.20
114.00

4+70 - 5' Lt. = Pole # 307920 H

4+50

110.4 ✓
5.6

109.55 ✓
6.45
138.00

4+05 7' Rt. = Pole # No. number. Buy pole.

4+00

108.8 ✓
7.2

107.10 ✓
8.30
131.00

3+50

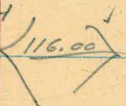
107.2 ✓
8.8

105.5 ✓
10.48
92.00

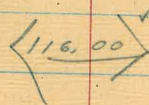
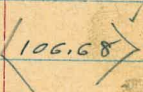
Nail in Pole # 307921 H

T.P.

9.32



0.25



3+27¹⁰ Δ 10°-17' Lt.

105.0 ✓
1.9

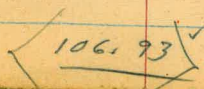
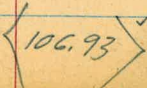
104.27 ✓
2.66
7.00

3+19 - 3' Rt. = Pole # 307921 H

3+00

104.1 ✓
2.8

102.43 ✓
4.50
8.00



Torrey Road

T.P. 12118 $\langle 138.16 \rangle$ 0.51 $\langle 125.98 \rangle$

8+50

8+05⁸⁸ $\Delta 9^\circ 10' \text{ Lt.}$ 8' Rt. = Apex. Cl. E.C.

8+00

7+50

7+00

6+80⁹⁷ $\Delta 11^\circ 19' \text{ Lt.}$

6+50

6+34 10' Rt. = Cl. B.C.

T.P. 11126 $\langle 126.49 \rangle$ 0.77 $\langle 115.23 \rangle$

6+00

5+96 - 3^E Rt. = Fifo Hydt.
 $\langle 116.00 \rangle$

E

125.0 ✓

1.5 ✓

$\frac{122.12}{574.6}$ EL.

121.96 ✓
 $\frac{4.53}{8 \text{ cl.}}$

121.8 ✓

4.7

119.2 ✓

7.3

119.14 ✓
 $\frac{7.35}{12.5 \text{ cl.}}$

117.6 ✓

8.9

117.64 ✓
 $\frac{8.85}{11.3 \text{ cl.}}$

117.0 ✓

9.5

116.95 ✓
 $\frac{9.54}{9' \text{ cl.}}$

116.7 ✓

9.8

115.85 ✓
 $\frac{10.66}{10.2 \text{ cl.}}$

~~114.17~~
 $\langle 126.49 \rangle$

115.32 ✓
 $\frac{11.17}{10.3 \text{ cl.}}$

114.7 ✓

1.3

114.29 ✓
 $\frac{1.71}{9.4 \text{ cl.}}$

$\langle 116.00 \rangle$

Torrey Road

56

S.W. B.P. Torrey Rd.
& Coast Blvd.

3.00 $\langle 113.55 \rangle$ (113.82)
 $\frac{F.B. 1655}{10}$

4+90⁵⁸
(P. 54

6.25 $\langle 116.55 \rangle$

$\langle 110.30 \rangle$

S.E. Lt. Torrey Rd. + Prospect. 1.61 152.24 (152.65)

T.P. 4.90

$\langle 153.85 \rangle$

1.09

$\langle 148.95 \rangle$

T.P.

12.52 $\langle 150.04 \rangle$

0.64

$\langle 137.52 \rangle$

9+66⁵⁸ x in driveway

9+52² = intersect Conc. drive

9+50

+55 - 1' Rt. = 12" diam. tree.

+20 4' Lt. = 20" diam. tree

+04 5' Lt. = 6" diam. tree

9+00- 21⁶ Lt. = N.W. ly line Conc. Drive

$\langle 138.16 \rangle$

133.91 ✓
 $\frac{4.25}{15}$
 S. Ely. edge
 Drive

133.80 ✓
 4.36

133.46 ✓
 $\frac{5.00}{6' \text{ of gutter}$
 1N. Drive

133.24 ✓
 4.92

132.9 ✓
 5.3

132.17 ✓
 $\frac{5.99}{63' \text{ of}}$

128.5 ✓
 9.7

128.40 ✓
 $\frac{9.76}{75' \text{ of}}$

$\langle 138.16 \rangle$

Sewer
 BIKs. C + B. - Map # 1535
 Villa Tract, La Jolla Park

5-11-49

- = Fd. Man.
- = Fd pipe + Disk
- = Fd Hub.
- ▣ = set stub
- = Fd. Nail.

INDEXED

WK
 MAY 19 1949

Sommernayer
 14th Coy
 Allen

0.00 - Elevation
 established by angle
 (tang. x dist.)

From Δ #4
 191' @ +Δ 12° 30'
 6' boot on red

From Δ #4
 Stadia 227' @ +Δ 12° 30'
 4' boot on red

0-1A¹⁷ - Nail
 Set 12/14/49

See FB 2016
 21

259' @ 14° 02' vert. Δ
 = 251.27 + Δ.

EL 155.0

EL 163

EL 150.62

Ctr. M.H. at
 pump

Sly Lind
 Salsalad Ave

Δ 61° 26'
 R-119'
 Map

BIK
 E

Levels - P. 59

57

Chained from "A." 1/4 x 3

Dist: 299.3 @ Δ 3° 27' = 298.86

EL: 298.86 (tang 3° 27') = 19.24
 above "A"

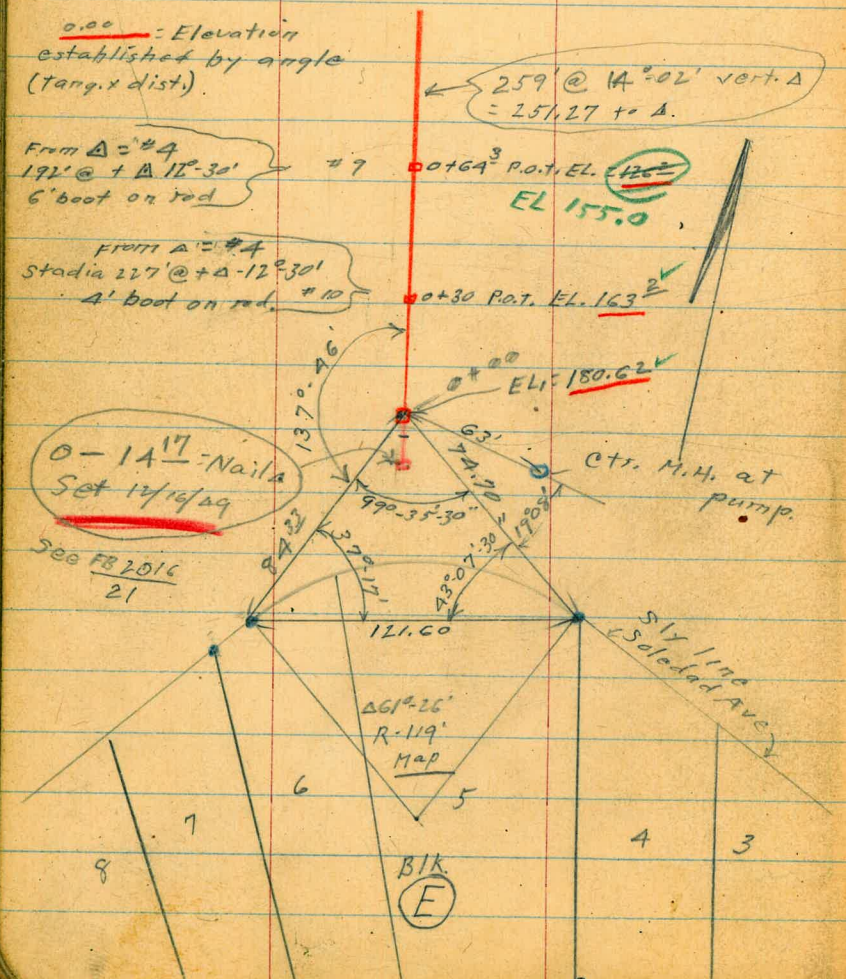
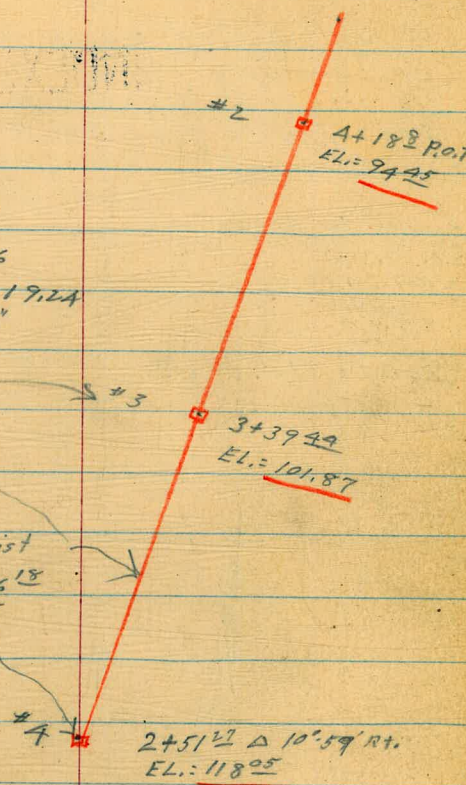
From Δ #4

89.77 @ 10° 50' = 88.17 = Dist
 EL 88.17 @ -Δ 10° 24' = 16.18

Above #3

From Δ #4

76' @ +Δ 12° 44'
 4' boot on red.



Results B + C. x 69.0%
 Levels BIK C + D. Villa Tract.
 La Jolla Park

Ground around pump house is all torn up because of pump house construction. No use showing present elevations. See opposite page for ties to this point.

x-on ch. for Pump house:

B.M. (G-250)
 84.24
 3.46
 87.70
 5.07

82.63 = stub. 6+40.35

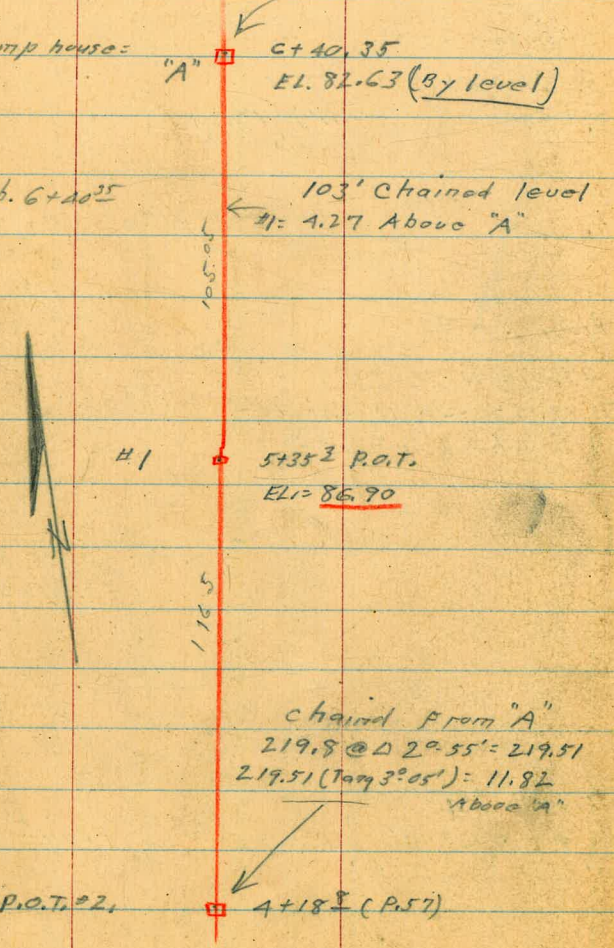
"A" \square C+40.35
 EL. 82.63 (By level)

103' Chained level
 H1 = 4.27 Above "A"

H1 \square 5+35.3 P.O.T.
 EL. = 86.90

Chained from "A"
 $219.8 @ \Delta 2^{\circ} 55' = 219.51$
 $219.51 (\text{Tan } 3^{\circ} 05') = 11.82$
 Above "A"

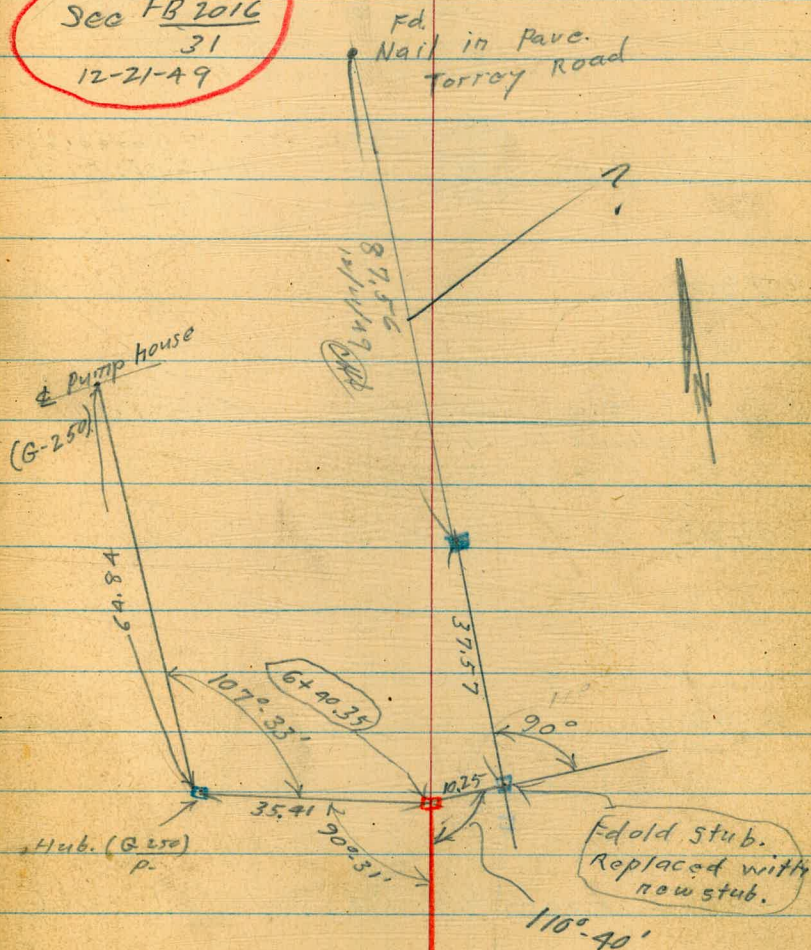
P.O.T. #2 \square 4+18.8 (P.57)



125.13
 37.57
 87.56

58

See FB 2016
 31
 12-21-49



W.O. 31720

B/Ks. C+D 69

Villa Tract La Jolla Park

Sommermeier
McCoy
Allen

0+83

0+64 dead

use green 12/7/50

w = bottom of wash

0+50 EL: 157.5

5.00 ~~160.0~~
131.2
Hard level

✓ (0+64.3)
176.2 (P. 57)
155.0 ↓

0+30

5.0 168.2
(Hard level.)

✓ (0+30)
163.2 (P. 57)

0+02

0+00

0-03² = Face Nly. Cb. Soledad road

0.00 ~~180.62~~

180.62
(0+00 P. 57)

59

W

9.3

155.0

12.0
6
w

154.3
5.7
5
W

8.0
8
W

570
0.0

131.2

160.9

163.2 ✓

5.0

168.2

180.3 ✓
0.3

180.6 ✓
0.0

180.57 ✓
0.05

180.62

Bkts. C.+B. #69
Villa Tract

60

1+50

7.0 138.0
Hand level

131.0 P.O.T. #25
P.57

131.3 ✓

6.7

138.00 ✓

1+30

141.5
18.5
w

1+20

144.3
~~12.5~~
15.7
2
w

146.6
13.4
12.2

1+10

145.0
15.0
2
w

144.3
~~14.0~~
12.0

0+95

147.0
~~11.8~~
13.0 ✓
6
w

148.0
149.9
~~11.1~~
10.1 ✓

v = red ok.

0+85

151
9.0
5

147
11.3 ✓
w

~~13.0~~
8.2
5

153.0 ~~131.2~~ Hand level

150.8
160.0
131.2

Bkts. C. + B + 69
Villa Tract

61

3+25

10 0.1 ✓
17.4

2+75

10 6. ✓
11.7

2+72

10 8.1 ✓
9.4

2+51²] = Δ 10° 59' RT. (P. 57.

See 2027
48

0.05 118.1 ✓

Hand level

118.05 P. 57 ✓
P. 57, #A

111.7 ✓
6.4
13
W

118.1 ✓
0.0
118.10

2+15

115.3 ✓
22.7
6
W

123.3 ✓
14.7
118.9 ✓
19.1
W

1+96 El. on ♀ figures rod of 19¹
cannot get rod in place.

1+77

131.0 ✓
7.0

122.5 ✓
15.5
8
W.

{ 138.0 } Hand level

138.00

Bks. C+D x.69
Villa Tract.

62

4+18.8

See $\frac{2027}{48}$

89. ✓
8.8
5
w

94.56 ✓
3.55

4+10

3.55 98.00
Hand level

94.45 P.O.T.#2
P.57

89. ✓
8.8
5
w

95.2 ✓
2.8
98.00 ✓

3 +90

93.2 ✓
11.8
7
w

99.8 ✓
5.2

+65

3.13 105.00

101.87 #3
P.57

94.5 ✓
10.5
7
w

100.0 ✓
5.0
105.00 ✓

3+40

0.03 101.9
Hand level

101.87 #3
P.57

101.9 06.9 100.9
0.0 5 1 0.0
10 5 3 101.9 ✓
w

3+30

See $\frac{2027}{48}$

103.1 ✓
14.4

118.10 ✓

Bks. C+B 69
Villa Tract

63

+99

85.1 ✓
9.9
W

+90

89.7 ✓
8.8

+75

90.7 ✓ 88.9 ✓
7.3 9.1
 3
 W

+57

91.6 ✓
6.1

+55

89.4 ✓
8.6
W

+53

91.8 ✓
6.2

+35

98.0 Hand Level

88.5 ✓ 93.0 ✓
9.5 5.0
7 98.00 ✓
W

131ks. C+B+69
Villa Tract

64

+59

82.6 ✓
5.4
W

+50

82.8 ✓
5.2
4
W

85.1 ✓
2.9

5+44

82.8 ✓
5.2
5
W

86.1 ✓
1.9

+41

13' L.T. = outlet 18" Ely + Wly, Drain

83.0 ✓
5.0
13
Ord.

86.0 ✓
2.0
13
invert

82.0 ✓
6.0
4
W

83.4 ✓
4.8
W

+38

86.6 ✓
1.4

5+35

1.1 88.00

by hand level

86.90 #1-P.58

82.5 ✓
3.5
3
W

86.9 ✓
1.1
88.00 ✓

5+00

87.5 ✓
10.5
W

88.5 ✓
2.5

4+96

98.0 Hand Level

90.1 ✓
7.9
98.0 ✓

6+40³⁵ (P. 58) = stub.

6+35

82.8 ✓
5.2

6+22

10' L. = start old iron pipe
culvert.

75.4 ✓
12.6
10
w

79.0 ✓
9.0

6+02

Revised
Oct 1950

78.1 ✓
9.9
8
w

79.6 ✓
8.4

6+00

See 2016
57

78.6 ✓
9.4
w

+87

82.4 ✓
5.6

81.2 ✓
6.8
15
w

5+80

see

2017
48

5+67

80.0 ✓
4.0

82.3 ✓
5.7
6
w

88.00 ✓

Cowie St. Canyon line

sketch P. 51

Sommermeier

McCoy

Allen

5-1649

INDEXED

WIK
MAY 19 1949

0+97

0+88

4' RT. = 16" diam Eucalyptus

5.3 123.50

118.20 (#1-P.51)

(was located about 1941 or 1942)
(check for details I believe this)
cleanout, for 24" drain. in 18" out

0+79 2' RT. = ctr. 2' x 2' grate over

0+75

Levels taken off
As by hand level

0+60

0+50

0+26 - 3' Lt. = 10" diam Eucalyptus

0+10 #

0+00 (P.51)

0.4 116.70

110.30

110.30

66

117.9 ✓
5.6

114.8 ✓
8.7

123.50 ✓

114.3 ✓
2.4

114.3 ✓
2.4

109.6 ✓
7.1

Grate invert

113.8 ✓
2.9

110.5 ✓
6.2

111.7 ✓
5.0

109.3 ✓
2.4

111.9 ✓
2.8

110.1 ✓
6.6

110.5 ✓
6.4
studs

116.70 ✓

Cowrie St. Canyon

67

1+78
 10^s Lt. = Edge of drive
 31' Rt. = Edge of drive
 12' Rt. = End of Ctr. Island

T.P. 2.1 - 128.5 126.43 - $\frac{2+25.95}{P.51}$

1+67
 12' Lt. } Right side of Circle Not shown
 23' Rt. } = Edge of drive

1+55
 Shrubs in Conc. Circle Dr
 10' Rt. = start Ctr. Island of

1+50
 Rads on drive

1+29³ = start Conc. Drive

1+20 = Δ 42°-09' Lt

123.50

127.1[↓]
 6.1
 10^s
 Edge Dr

127.2[↓]
 6.3
 12
 End Circle Island

127.3[↓]
 6.3
 12
 End Circle Island

127.0[↓]
 5.5
 31
 Edge of Drive

128.50[↓]

127.5[↓]
 1.0
 12

127.0[↓]
 1.5

121.9[↓]
 1.6
 22

121.0[↓]
 2.5
 10

119.3[↓]
 4.2
 4
 Edge of Dr.

121.0[↓]
 2.5

120.6[↓]
 2.2
 10

121.4[↓]
 2.1
 30
 Edge of Dr.

119.6[↓]
 3.9
 0.4
 Lt.
 Cor. Dr.

119.6[↓]
 3.9

118.9[↓]
 4.6
 8

120.3[↓]
 3.2
 25
 Cor. of Dr.

118.2[↓]
 5.3

123.50

Cowrie St. Canyon

68

2+46

127.8[✓]
7.5

(This flume is approx. 2' wide)

2+44 9^E (Cross conc. flume)
Rt. = 20" diam Eucalyptus

126.3[✓]
9.0
Bottom of flume.

2+30 4^E Lt. = 14" diam Eucalyptus

8.87 135.30[✓] 2+25⁹⁵
126.43 P. 51

135.30[✓]

Conc. storm drain (Flume in fair condition.)
Also start open conc.

2+25⁹⁵ = Δ 31°-06' Rt. 3' Rt. = intake for

126[✓] 127[✓] 125.5[✓]
2.1 5.8 3.0
3' 3'

2+22^E 4^E Rt. = End garage

Estimated
Drain invert

2+15

124[✓]
4.2

Gar. is 22' wide

4^E Rt. = Cor. of drive (End of Dr.)

2+04 3^E Rt. = N.W. Cor. 2 car. Gar.

123[✓] 123.5[✓]
5.3 5.0
42
DRIVE +
Gar. floors

1+93^E End of drive on T

123[✓]
5.4

128.50[✓]

128.50[✓]

31
3+90

| | | |
|--------------------|--------------------|--------------------|
| 138.5 [✓] | 135.3 [✓] | 137.9 [✓] |
| $\frac{4.0}{3}$ | 7.0 | $\frac{4.4}{3}$ |
| W | W | W |

3+80

138.3[✓]
7.0

3+75²² = Δ 13²⁰¹ Lt.

| | | |
|--------------------|--------------------|--------------------|
| 134.4 [✓] | 137.3 [✓] | 138.2 [✓] |
| $\frac{8.1}{6}$ | $\frac{5.0}{4}$ | 4.1 |
| W | W | W |

3+58 - 2' Lt. = 5" diam. eucalyptus.

3+50 (W = wash)

| | | |
|--------------------|--------------------|--------------------|
| 133.1 [✓] | 136.7 [✓] | 136.5 [✓] |
| $\frac{9.2}{8}$ | $\frac{5.6}{6}$ | 5.8 |
| W | W | W |

3+44 5⁵ Lt. = 10" diam. eucalyptus

3+25 12' Lt. = ♀ wash

T.P. 4.12 142.30

3+75.73
138.18 P.51

| | | |
|--------------------|--------------------|--------------------------|
| 133.0 [✓] | 134.9 [✓] | 134.7 [✓] |
| $\frac{9.3}{12}$ | $\frac{7.4}{8}$ | 7.6 |
| W | W | W |
| | | <u>142.3[✓]</u> |

3+00 16' Lt. = End of Conc. flume.

| | | |
|--------------------|--------------------|--------------------|
| 131.1 [✓] | 132.3 [✓] | 132.5 [✓] |
| $\frac{4.2}{16}$ | $\frac{3.0}{14}$ | 2.8 |
| ♀ Flume | ♀ Flume | ♀ Flume |

2+50 16' Lt. = End of conc. P

| | |
|--------------------|--------------------|
| 127.1 [✓] | 127.8 [✓] |
| $\frac{8.2}{2}$ | 7.5 |
| ♀ Flume | ♀ Flume |

135.30[✓]

135.30[✓]

5+10

5+07

4+90

4+84

T.P.

4+60 Δ 16°-27' Lt.

4+23

4+00

7.62 145.80

✓ 4+60
144.44 P. 51

✓ 3+75²³
138.18 P. 51

144.1 ✓
8.5
2
w

147.3 ✓
5.3

144.0 ✓
8.6
w

142.6 ✓
10.0
w

142.5 ✓
10.1
4
w

145.4 ✓
7.2

152.6 ✓

140.2 ✓
5.6
8
w

144.1 ✓
1.7
4

144.4 ✓
1.4

137.4 ✓
8.4
5
w

140.3 ✓
5.5
1

140.3 ✓
5.5

138.8 ✓
7.0
3

135.3 ✓
10.5
w

138.3 ✓
7.5
4

145.8 ✓

Cowrie St Canyon line

71

6+46
 T.P. 5.64 173.20 ✓
 167.56 P.52 ✓ 7+07.11

6+35

6+31 Δ in wash

5+88

5+83

5+69.93 Δ 11° 45' RT.

8.07 167.10 ✓
 155.10 ✓ 5+69.93 P.52

162.5 ✓
 10.7 ✓
173.20 ✓

161.9 ✓
 11.3 ✓
6
 153.0 ✓
 20.2 ✓
13
 W

161.4 ✓
 1.7 ✓
6

155.9 ✓
 7.2 ✓
6

161.4 ✓
 1.7 ✓
3

155.4 ✓
 7.7 ✓
W

160.5 ✓
 2.6 ✓
8

158.1 ✓
 5.0 ✓
4

152.9 ✓
 10.2 ✓
W

156.1 ✓
 5.0 ✓
3

152.1 ✓
 10.4 ✓
2
 W

151.4 ✓
 5.7 ✓

152.8 ✓
 10.3 ✓
11
 W

156.2 ✓
 6.9 ✓
9

~~154.9~~ ✓
 6.2 ✓

should be $\frac{155}{8.0}$

146.0 ✓
 15.1 ✓
18
 W

154.0 ✓
 9.1 ✓
16

143.1 ✓

Cowrie St. Canyon line

72

7+55

167.8 ✓
9.8
 W

7+53

173.1 ✓ 167.6 ✓
4.5 10.0
 3
 W

7+35

171.9 ✓ 171.4 ✓ 164.6 ✓
5.7 6.2 13.0
 10 12
 W

7+20

169.6 ✓ 169.7 ✓ 162.3 ✓
8.0 8.4 15.3
177.6 ✓ 7 9
 W

T.P. 10.04 177.6 ✓

✓ 7+07 11
 167.56 B.52

5.6

7+07 11 Δ 2'-2A' RT.

7+00

166.7 ✓ 166.6 ✓ 158.0 ✓
6.5 6.6 15.2
 3 10
 W

6+65

164.0 ✓ 155.7 ✓
9.2 17.5
 7
 W

173.20 ✓

173.20 ✓

Cowrie St. Canyon line

73

8+54⁶⁵ P.O.T. + Tie in point P. 52

183.5 ✓
2.9

8+39

180.9 ✓
5.5
2
W
182.1 ✓
4.3

8+33

181.7 ✓
4.7
1
180.7 ✓
5.7
W
182.0 ✓
1.4
2

8+26

182.1 ✓
4.3
182.0 ✓
4.4
2
177.4 ✓
9.0
6
W

T.P.

2.94

186.4 ✓

183.46 ✓
point #4
P. 52

186.4 ✓

7+93

177.6 ✓
0.0
2
174.8 ✓
2.8
5
W

7+9.2

177.6 ✓
0.0
2
174.6 ✓
9.0
W
174.7 ✓
2.9
8
W
177.6 ✓
0.0
10

177.6 ✓

177.6 ✓

Cowrie St. Canyon line

74

9+00

187.0[✓]
2.5

8+90

185.3[✓]
4.2

783

184.1[✓]
5.4

8+80

185.4[✓]
4.3

T.P.

6.04 189.5[✓]

183.46[✓] point #4
P.52

189.5[✓]

Alley
BIK, 45 La Jolla Park

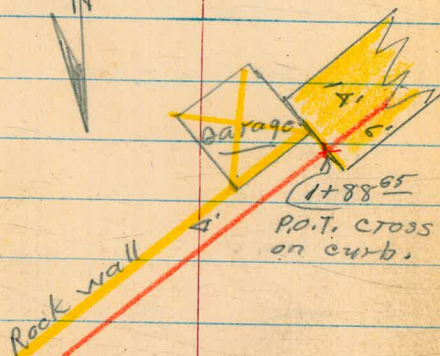
75

5-16-49
wo 31720

Sommermeier
McCoy
Alley

INDEXED
WK
MAY 19 1949

APPROX.
N



$\Delta 50^\circ-48'$ RT.

0+86.20

See page 50

0+67.6

0+89

0+75

Conc. Drive

$87.40 @ 92.30'$ vert. Δ
= 86.20

$77^\circ-23'$

0+00

8+05.88 $\Delta 9^\circ-10'$ Lt

Torrey Pines Road line
= 0+00 (P50)

APPROX.
N

Prospect Place

Ely. line Prospect.
3+88.9

& Prop. Sewer
is 6' off. RT. side
pavement
header board
which is still
in place.

See alley
construction plans
for location of
improvements.

They also should
show drain
details.

14' x 6'

Clean out + grate.
 $1+96 = \Delta$ Lt. = Ctr. 2/13'

12" Conc. Drain

1+88.65 = P.O.T.
Cross in curb

5-16-49
W.O. 31720
+76

Alley BIK. 45
La Jolla Park

+75 Leave Conc. Dr. (Sly edge)

0+67^e Cross Conc. Drive (Nly. edge.)

T.P. 11.78 <146.20> 0.55 <134.42>

+53

+44

0+30

+15

0+14 7 1/2" Lt. = 8" acacia

0+00

4+05.88

12.85 134.97

<122.12> 8+05.88
P.55

see lands page 50
for line as finally
located

135.1 ✓
11.1

135.04 ✓
11.16

134.74 ✓
11.46

<146.20>

132.4 ✓
2.6

127.9 ✓
7.1

125.7 ✓
7.3

122.8 ✓
12.2

122.12 ✓
12.85
stub

134.97 ✓

Alley BIK, 45
La Jolla Park.

77

1+85

154.5 ✓
3.0

+71 2' Lt. = 12" diam. Accacia

1+68 3' Lt. = 10" diam. "

1+65

150.3 ✓
2.2

1+50

T.P. 1153 $\langle 157.53 \rangle$ 0.20 $\langle 146.00 \rangle$

149.2 ✓
8.3
 $\langle 157.53 \rangle$

1+16

146.0 ✓
0.2

0+89 A' Lt. = start rock wall

140.7 ✓
5.5

0+86²⁰ Δ 90°

139.64 ✓
6.56

0+79

137.8 ✓
8.4

$\langle 146.20 \rangle$

Alley B/k. 45
La Jolla Park

78

2+50

159.37 ✓
7.49

T.P.

11.87

168.86 ✓

0.54

156.99 ✓

168.86 ✓

details of Improvements
(See alley plans for

2+00

155.84 ✓
1.69

1+76

{ also = cross 12" culvert
Clean out:
4' Lt. = ctr. 2x3 grate over

✓ ✓
152.00 ✓ 155.20 ✓ 155.5 ✓
8.51 2.33 2.0
4 4
invert grate

1+88²

gutter.

155.67 ✓
1.86
pave

(Conc. Pave
alley pavement (8" curb.)

1+88⁸⁵ = Face of cross curb start of

156.1 ✓
1.40

1+88

4' Lt. = End rock wall.

155.5 ✓
2.0

157.53 ✓

157.53 ✓

Alley BLK. 45
La Jolla Park

Alternate line on Page 80

SE. 1/4 Lt. Prospect
+ Torrey Road

7.98

152.23

152.24
P 56

T.P.

3.47

160.21

12.23

156.74

?

3+88[±] = N.E. 1/4 line Prospect.

T.P.

11.43

168.97

132

167.54

3+50

3+00

168.86

Also see Page 80

79

157.5

1.0

158.48

?

165.71

3.15

162.50

6.36

168.86

Sketch P. 50
Alley Bk. 45 - La Jolla Parks

= Δ 0+86.20 (P. 50)

1+68.57A P. 07, =

139.67 ✓
4.60

A/ 1+57.4 = End Conc. Dr.

135.14 ✓
9.13

1+48.1 start. Conc. Dr.

134.97 ✓
9.30

144.27 ✓

SE. 1/4

+ Tor

T.P. 9.25 (144.27)

1+08 - 15 ft. Ctr. 18" Locust

0+98 - 8 ft. = 18" Evergreen

2.16 (135.02)

T.P.

T.P. 0+93.47

12.10 (137.18)

0.86 (124.78)

Cross 18" Conc. walk

122.15 ✓

3+88 0+54.32 & Walk

3.49

T.P.

0+34

122.9 ✓
2.7

3+50

+13 start small trees

11.6 ✓
8.0

0+00:

6+73.57 P. 50:

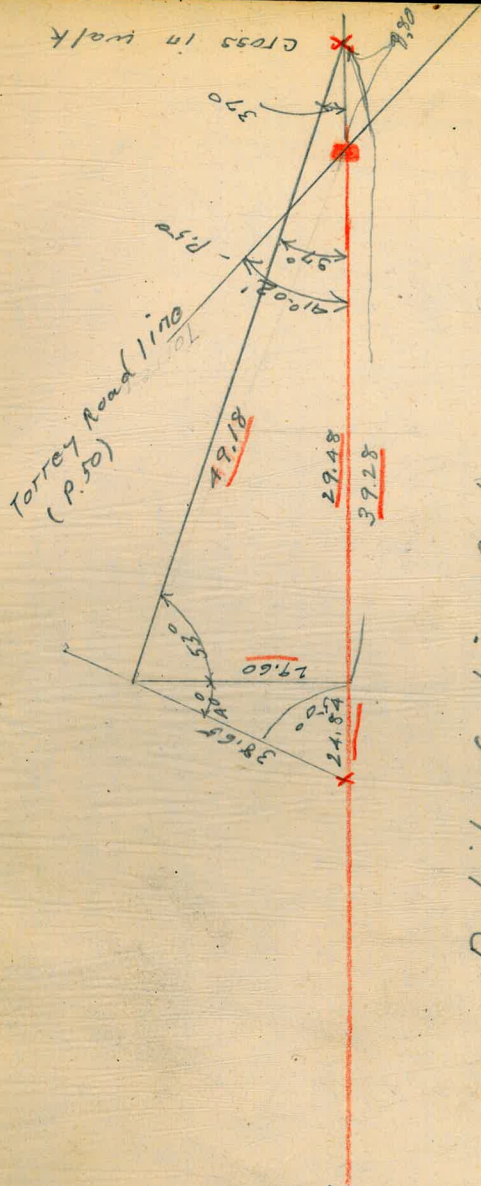
116.68 ✓
8.96

3+00

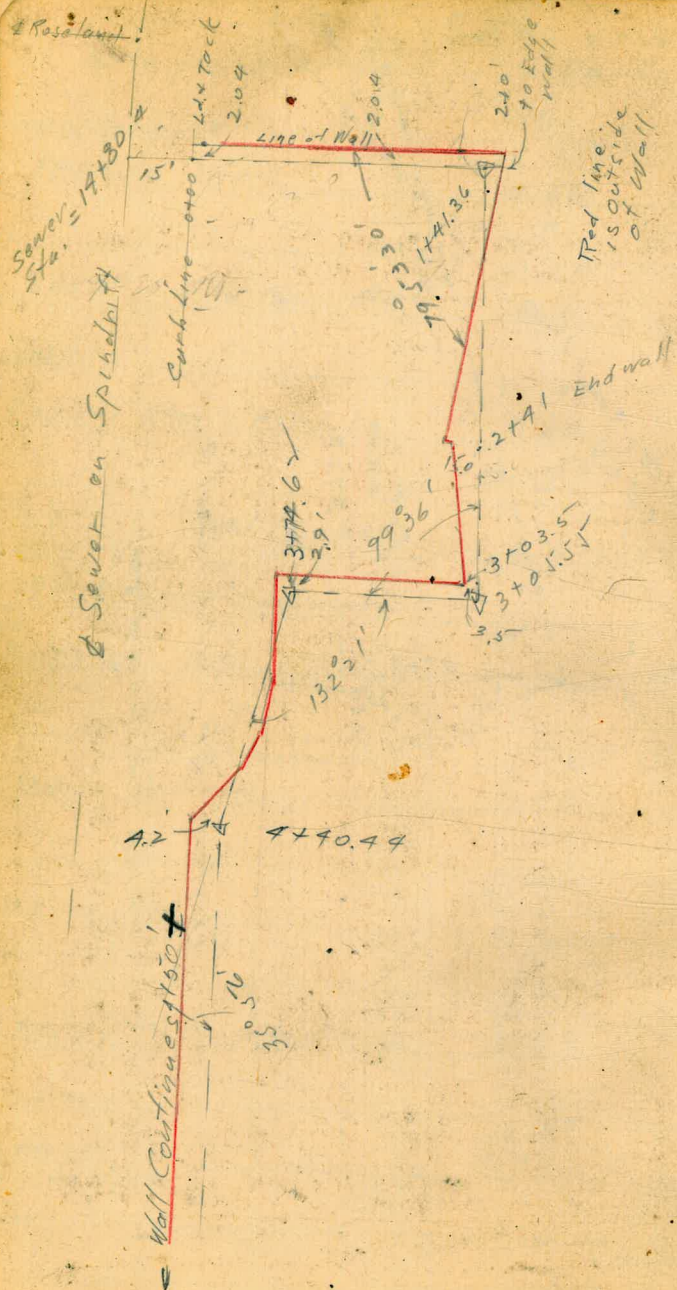
3.52 (125.64)

122.12 P. 55

oppo = Calc.



Detail of line Calc. on P. 50
(Also on Page 50)



SE. 1/4
* TOT

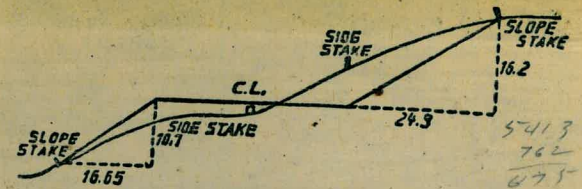
T.P.

3+8

T.P.

3+50

3+00



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1/2 TO 1. ROADWAY OF ANY WIDTH.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| 0 | 0.00 | 0.15 | 0.30 | 0.45 | 0.60 | 0.75 | 0.90 | 1.05 | 1.20 | 1.35 | 0 |
| 1 | 1.50 | 1.65 | 1.80 | 1.95 | 2.10 | 2.25 | 2.40 | 2.55 | 2.70 | 2.85 | 1 |
| 2 | 3.00 | 3.15 | 3.30 | 3.45 | 3.60 | 3.75 | 3.90 | 4.05 | 4.20 | 4.35 | 2 |
| 3 | 4.50 | 4.65 | 4.80 | 4.95 | 5.10 | 5.25 | 5.40 | 5.55 | 5.70 | 5.85 | 3 |
| 4 | 6.00 | 6.15 | 6.30 | 6.45 | 6.60 | 6.75 | 6.90 | 7.05 | 7.20 | 7.35 | 4 |
| 5 | 7.50 | 7.65 | 7.80 | 7.95 | 8.10 | 8.25 | 8.40 | 8.55 | 8.70 | 8.85 | 5 |
| 6 | 9.00 | 9.15 | 9.30 | 9.45 | 9.60 | 9.75 | 9.90 | 10.05 | 10.20 | 10.35 | 6 |
| 7 | 10.50 | 10.65 | 10.80 | 10.95 | 11.10 | 11.25 | 11.40 | 11.55 | 11.70 | 11.85 | 7 |
| 8 | 12.00 | 12.15 | 12.30 | 12.45 | 12.60 | 12.75 | 12.90 | 13.05 | 13.20 | 13.35 | 8 |
| 9 | 13.50 | 13.65 | 13.80 | 13.95 | 14.10 | 14.25 | 14.40 | 14.55 | 14.70 | 14.85 | 9 |
| 10 | 15.00 | 15.15 | 15.30 | 15.45 | 15.60 | 15.75 | 15.90 | 16.05 | 16.20 | 16.35 | 10 |
| 11 | 16.50 | 16.65 | 16.80 | 16.95 | 17.10 | 17.25 | 17.40 | 17.55 | 17.70 | 17.85 | 11 |
| 12 | 18.00 | 18.15 | 18.30 | 18.45 | 18.60 | 18.75 | 18.90 | 19.05 | 19.20 | 19.35 | 12 |
| 13 | 19.50 | 19.65 | 19.80 | 19.95 | 20.10 | 20.25 | 20.40 | 20.55 | 20.70 | 20.85 | 13 |
| 14 | 21.00 | 21.15 | 21.30 | 21.45 | 21.60 | 21.75 | 21.90 | 22.05 | 22.20 | 22.35 | 14 |
| 15 | 22.50 | 22.65 | 22.80 | 22.95 | 23.10 | 23.25 | 23.40 | 23.55 | 23.70 | 23.85 | 15 |
| 16 | 24.00 | 24.15 | 24.30 | 24.45 | 24.60 | 24.75 | 24.90 | 25.05 | 25.20 | 25.35 | 16 |
| 17 | 25.50 | 25.65 | 25.80 | 25.95 | 26.10 | 26.25 | 26.40 | 26.55 | 26.70 | 26.85 | 17 |
| 18 | 27.00 | 27.15 | 27.30 | 27.45 | 27.60 | 27.75 | 27.90 | 28.05 | 28.20 | 28.35 | 18 |
| 19 | 28.50 | 28.65 | 28.80 | 28.95 | 29.10 | 29.25 | 29.40 | 29.55 | 29.70 | 29.85 | 19 |
| 20 | 30.00 | 30.15 | 30.30 | 30.45 | 30.60 | 30.75 | 30.90 | 31.05 | 31.20 | 31.35 | 20 |
| 21 | 31.50 | 31.65 | 31.80 | 31.95 | 32.10 | 32.25 | 32.40 | 32.55 | 32.70 | 32.85 | 21 |
| 22 | 33.00 | 33.15 | 33.30 | 33.45 | 33.60 | 33.75 | 33.90 | 34.05 | 34.20 | 34.35 | 22 |
| 23 | 34.50 | 34.65 | 34.80 | 34.95 | 35.10 | 35.25 | 35.40 | 35.55 | 35.70 | 35.85 | 23 |
| 24 | 36.00 | 36.15 | 36.30 | 36.45 | 36.60 | 36.75 | 36.90 | 37.05 | 37.20 | 37.35 | 24 |
| 25 | 37.50 | 37.65 | 37.80 | 37.95 | 38.10 | 38.25 | 38.40 | 38.55 | 38.70 | 38.85 | 25 |
| 26 | 39.00 | 39.15 | 39.30 | 39.45 | 39.60 | 39.75 | 39.90 | 40.05 | 40.20 | 40.35 | 26 |
| 27 | 40.50 | 40.65 | 40.80 | 40.95 | 41.10 | 41.25 | 41.40 | 41.55 | 41.70 | 41.85 | 27 |
| 28 | 42.00 | 42.15 | 42.30 | 42.45 | 42.60 | 42.75 | 42.90 | 43.05 | 43.20 | 43.35 | 28 |
| 29 | 43.50 | 43.65 | 43.80 | 43.95 | 44.10 | 44.25 | 44.40 | 44.55 | 44.70 | 44.85 | 29 |
| 30 | 45.00 | 45.15 | 45.30 | 45.45 | 45.60 | 45.75 | 45.90 | 46.05 | 46.20 | 46.35 | 30 |
| 31 | 46.50 | 46.65 | 46.80 | 46.95 | 47.10 | 47.25 | 47.40 | 47.55 | 47.70 | 47.85 | 31 |
| 32 | 48.00 | 48.15 | 48.30 | 48.45 | 48.60 | 48.75 | 48.90 | 49.05 | 49.20 | 49.35 | 32 |
| 33 | 49.50 | 49.65 | 49.80 | 49.95 | 50.10 | 50.25 | 50.40 | 50.55 | 50.70 | 50.85 | 33 |
| 34 | 51.00 | 51.15 | 51.30 | 51.45 | 51.60 | 51.75 | 51.90 | 52.05 | 52.20 | 52.35 | 34 |
| 35 | 52.50 | 52.65 | 52.80 | 52.95 | 53.10 | 53.25 | 53.40 | 53.55 | 53.70 | 53.85 | 35 |
| 36 | 54.00 | 54.15 | 54.30 | 54.45 | 54.60 | 54.75 | 54.90 | 55.05 | 55.20 | 55.35 | 36 |
| 37 | 55.50 | 55.65 | 55.80 | 55.95 | 56.10 | 56.25 | 56.40 | 56.55 | 56.70 | 56.85 | 37 |
| 38 | 57.00 | 57.15 | 57.30 | 57.45 | 57.60 | 57.75 | 57.90 | 58.05 | 58.20 | 58.35 | 38 |
| 39 | 58.50 | 58.65 | 58.80 | 58.95 | 59.10 | 59.25 | 59.40 | 59.55 | 59.70 | 59.85 | 39 |
| 40 | 60.00 | 60.15 | 60.30 | 60.45 | 60.60 | 60.75 | 60.90 | 61.05 | 61.20 | 61.35 | 40 |
| 41 | 61.50 | 61.65 | 61.80 | 61.95 | 62.10 | 62.25 | 62.40 | 62.55 | 62.70 | 62.85 | 41 |
| 42 | 63.00 | 63.15 | 63.30 | 63.45 | 63.60 | 63.75 | 63.90 | 64.05 | 64.20 | 64.35 | 42 |
| 43 | 64.50 | 64.65 | 64.80 | 64.95 | 65.10 | 65.25 | 65.40 | 65.55 | 65.70 | 65.85 | 43 |
| 44 | 66.00 | 66.15 | 66.30 | 66.45 | 66.60 | 66.75 | 66.90 | 67.05 | 67.20 | 67.35 | 44 |
| 45 | 67.50 | 67.65 | 67.80 | 67.95 | 68.10 | 68.25 | 68.40 | 68.55 | 68.70 | 68.85 | 45 |
| 46 | 69.00 | 69.15 | 69.30 | 69.45 | 69.60 | 69.75 | 69.90 | 70.05 | 70.20 | 70.35 | 46 |
| 47 | 70.50 | 70.65 | 70.80 | 70.95 | 71.10 | 71.25 | 71.40 | 71.55 | 71.70 | 71.85 | 47 |
| 48 | 72.00 | 72.15 | 72.30 | 72.45 | 72.60 | 72.75 | 72.90 | 73.05 | 73.20 | 73.35 | 48 |
| 49 | 73.50 | 73.65 | 73.80 | 73.95 | 74.10 | 74.25 | 74.40 | 74.55 | 74.70 | 74.85 | 49 |
| 50 | 75.00 | 75.15 | 75.30 | 75.45 | 75.60 | 75.75 | 75.90 | 76.05 | 76.20 | 76.35 | 50 |

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