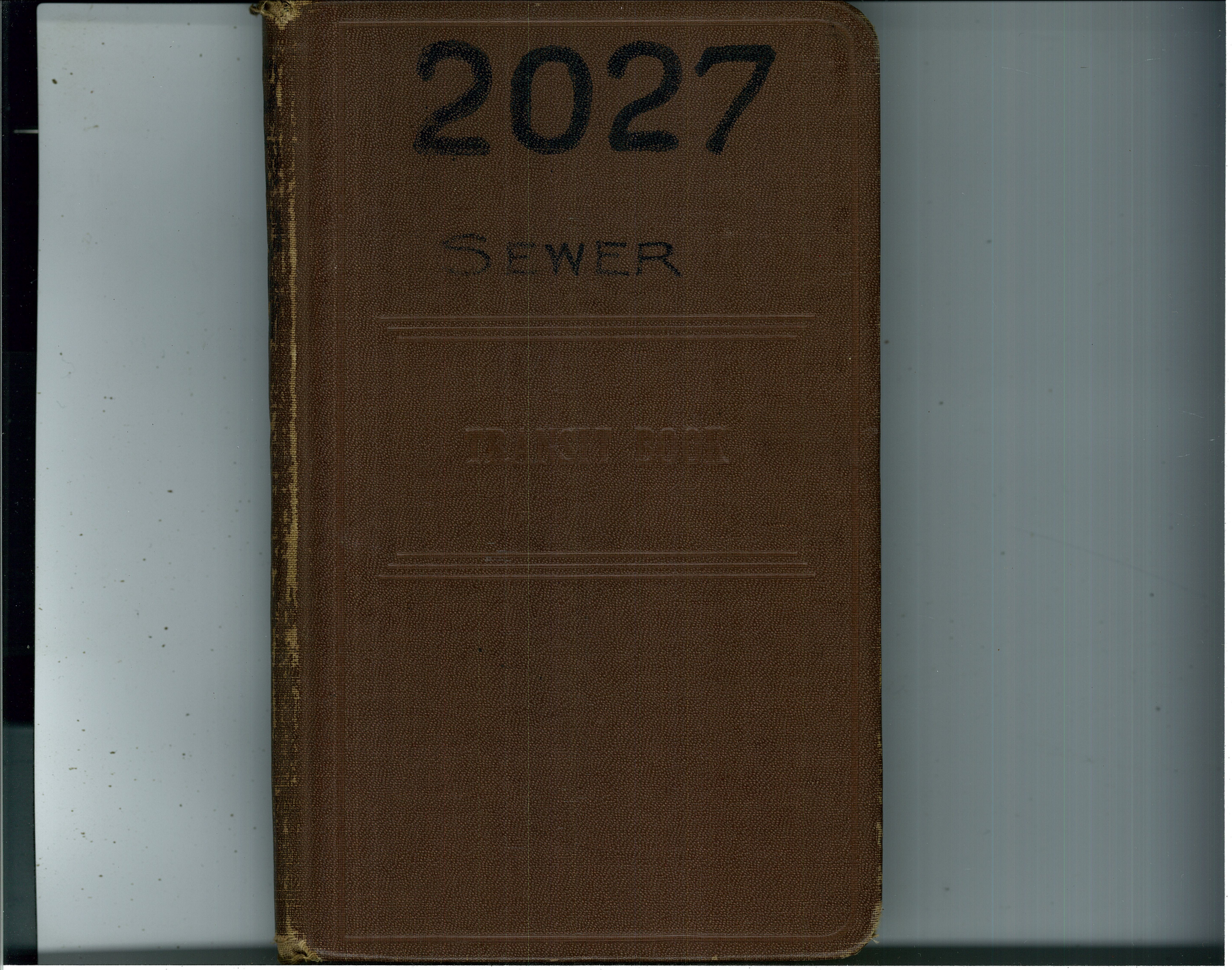
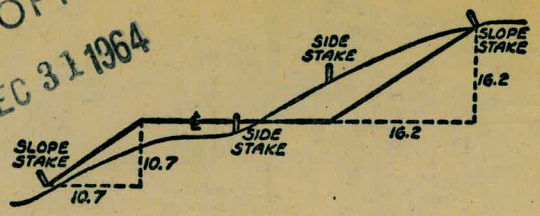

2027
SEWER



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

to page #59

Sewer Prelim 1

Torrey Road 23-26
~~East + West of St. Louis terrace~~ 20
Blk (Roseland S.W'ly) 21 & 27
La Jolla Hills (Lots 1 to 12) 29 & 22
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Roseland
Avenida Alamar } Line Change 45
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Newport & Abbott, X-Sec. for new cbs. 56
Kurtz & Riley, curbs & gutter levels 60
Nutmeg & Felton, Eastern Add. 64
Lots 566, Blk. 43, survey to extend culvert
Sewer Soledad Ave & Lots 45-56-57-60 La Jolla Hills } 67 ro

LOCATION PROPOSED SEWER
IN AMALFI STREET
And in LA JOLLA PARK WO 31720

Block L.

Walker
Johnson
Pope
Crawford
4-14-49

Levels - P.10 -

Proposed Sewer = ——

2+73.05 = P.O.T. = Intersection Semi Tangent

0+09.59 = P.O.T. Fd. Hub.

0+00 = Intersection Clints Line

Torrey Pines Road

(7+46.58 F.B. 597 24) Fd. Conc. Mon

68°21'45"

3+42.18 Set Hub

2

22°20'14"

111°38'15"

Fd. Conc. Mon

19.14'

(6+31.90 F.B. 597 24)

2+73.05 Set Hub = P.O.T.

See FB 2016 / 31 12/21/49

Proposed Sewer

Δ 28°24 F.B. 597 24

Fd. P.I. Hub.

(4+80.46 F.B. 597 24)

Fd. Conc. Mon. F.B. 597 24

111°18'45"

Ref. Point 50.00

Hub set 8+46.50

80°00

Ref. Pt. 50.00

89°20'30"

Fd. Hub

37.51

Fd. Conc. Mon

95.59'

6+40.35 F.B. 2019-58

0+00 Set Hub

3.72'

℄ Clints Line

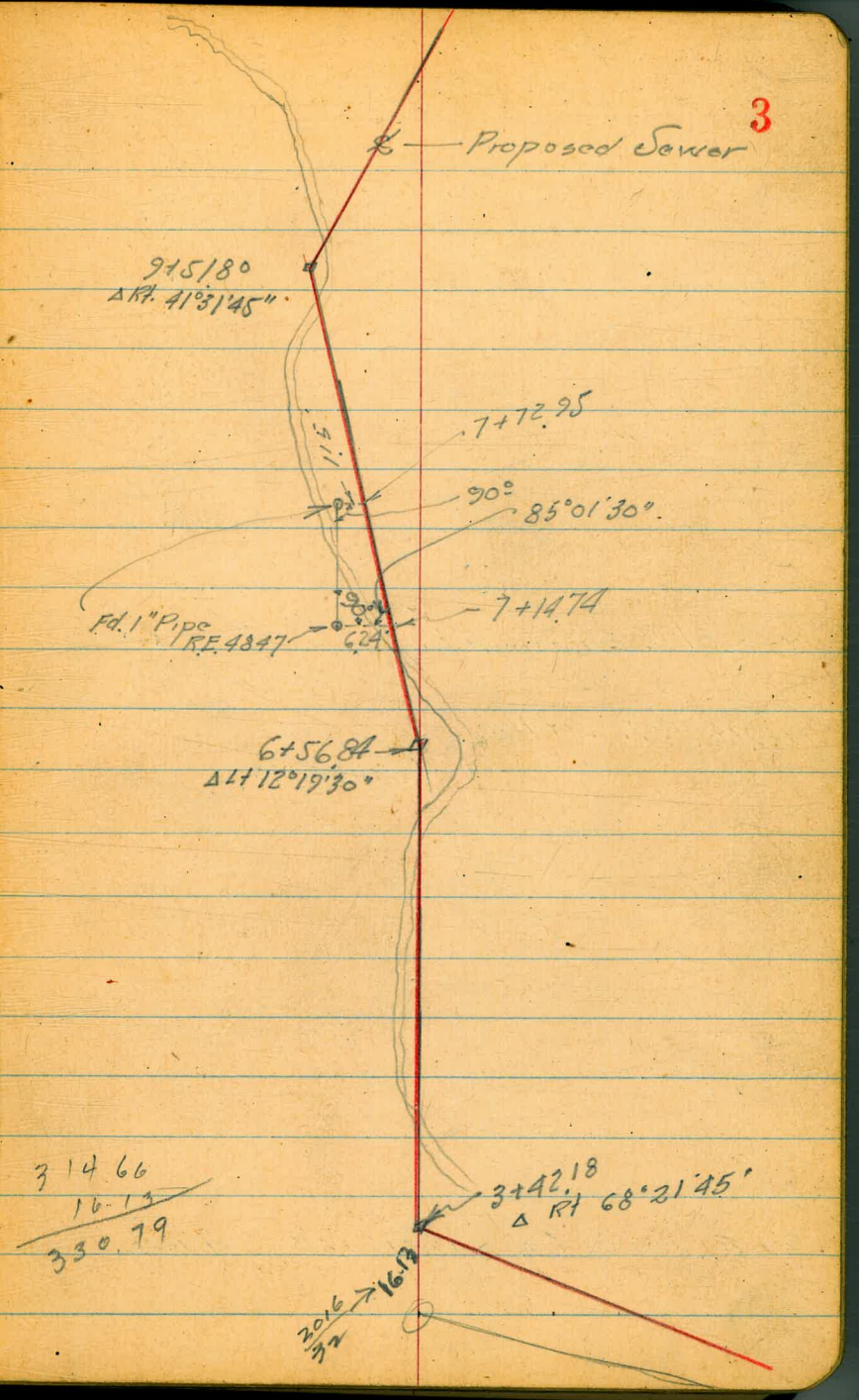
Location Proposed Sewer
in Loyola Park (Block Lx)

9+51.80 = Δ Rt 41°31'45"

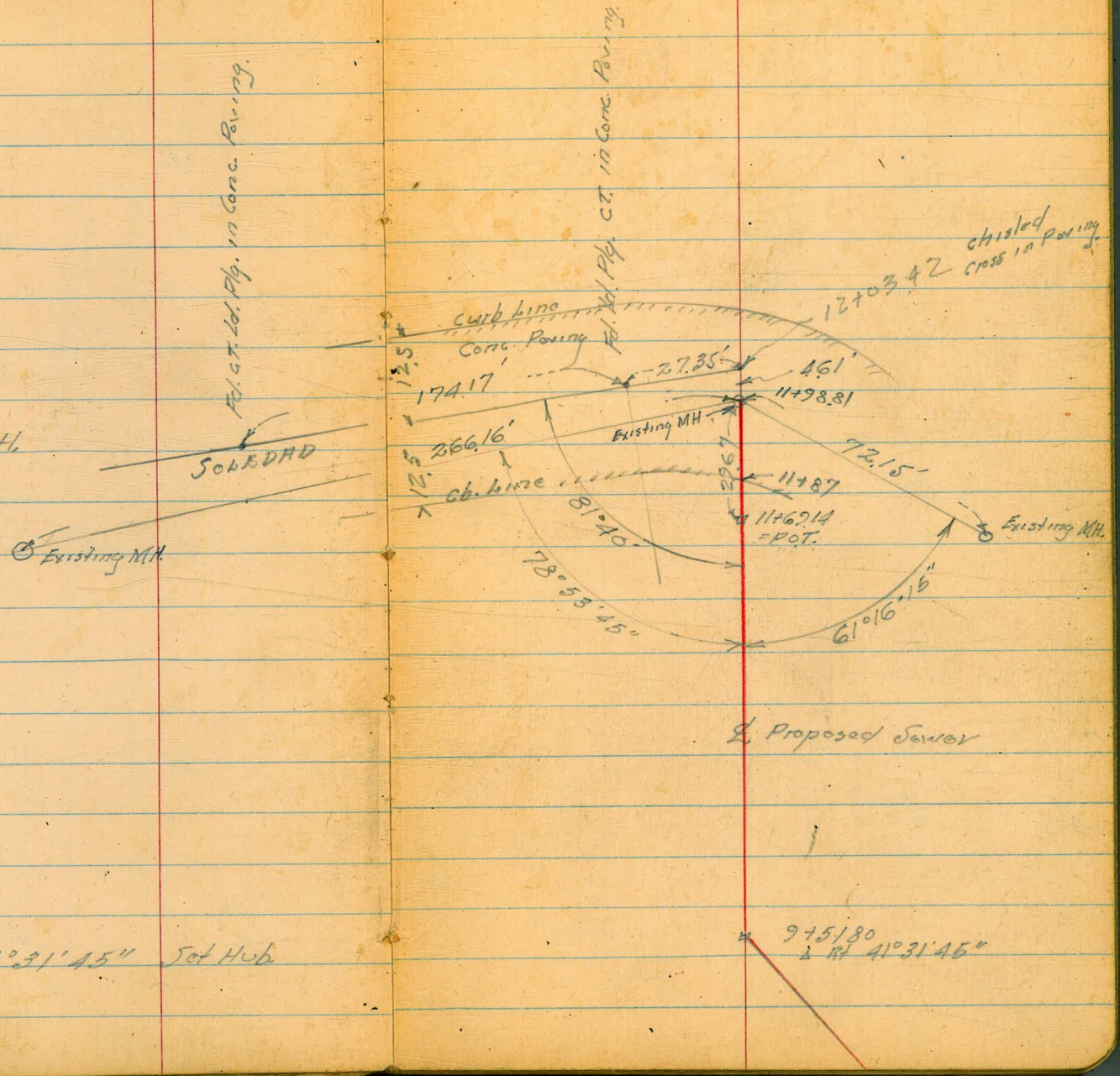
6+56.84 = Δ Lt. 12°19'30" Set Hub

3+42.18 = Δ Rt. 68°21'45" Set Hub.

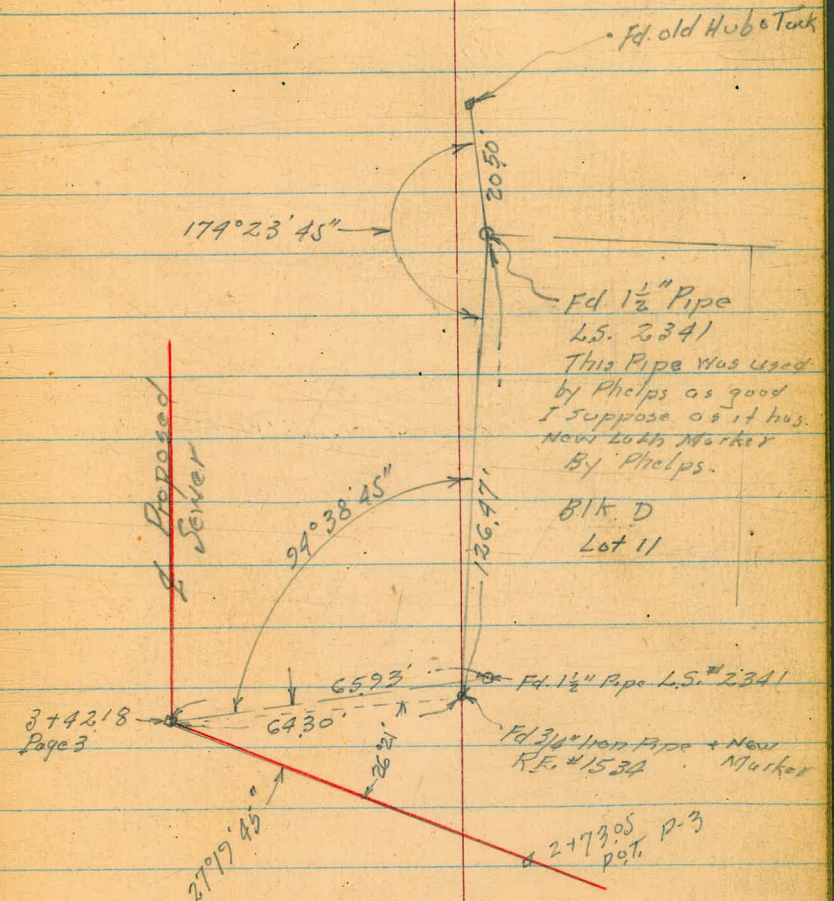
3 1 4 6 6



Location Proposed Sewer
in La Jolla Park



Property Ties To Proposed Sewer in Hacienda Park



Proposed Sewer in La Jolla Park

Location of Existing Culvert

3+15.63

277 111.64 108.57

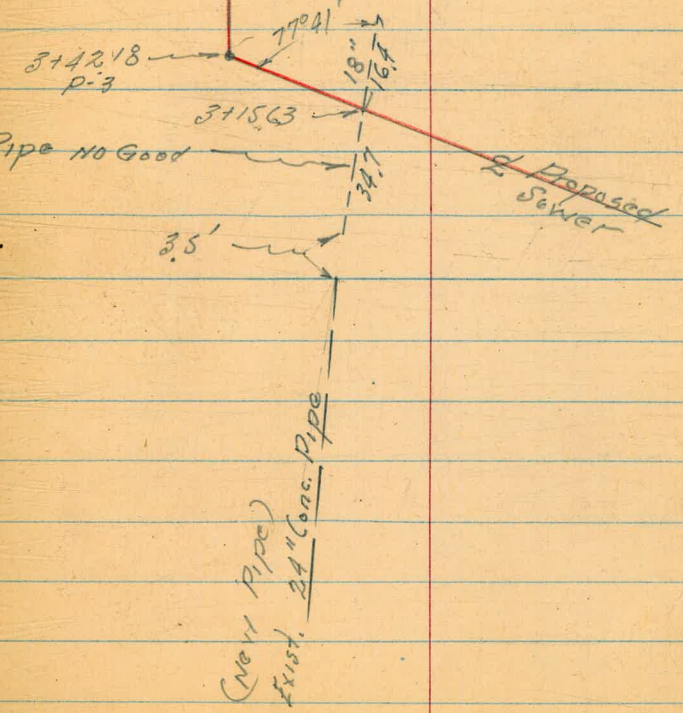
3+15.63 = P.O.T. = Intersection 18" Wooden Pipe

Lt. & Rt.

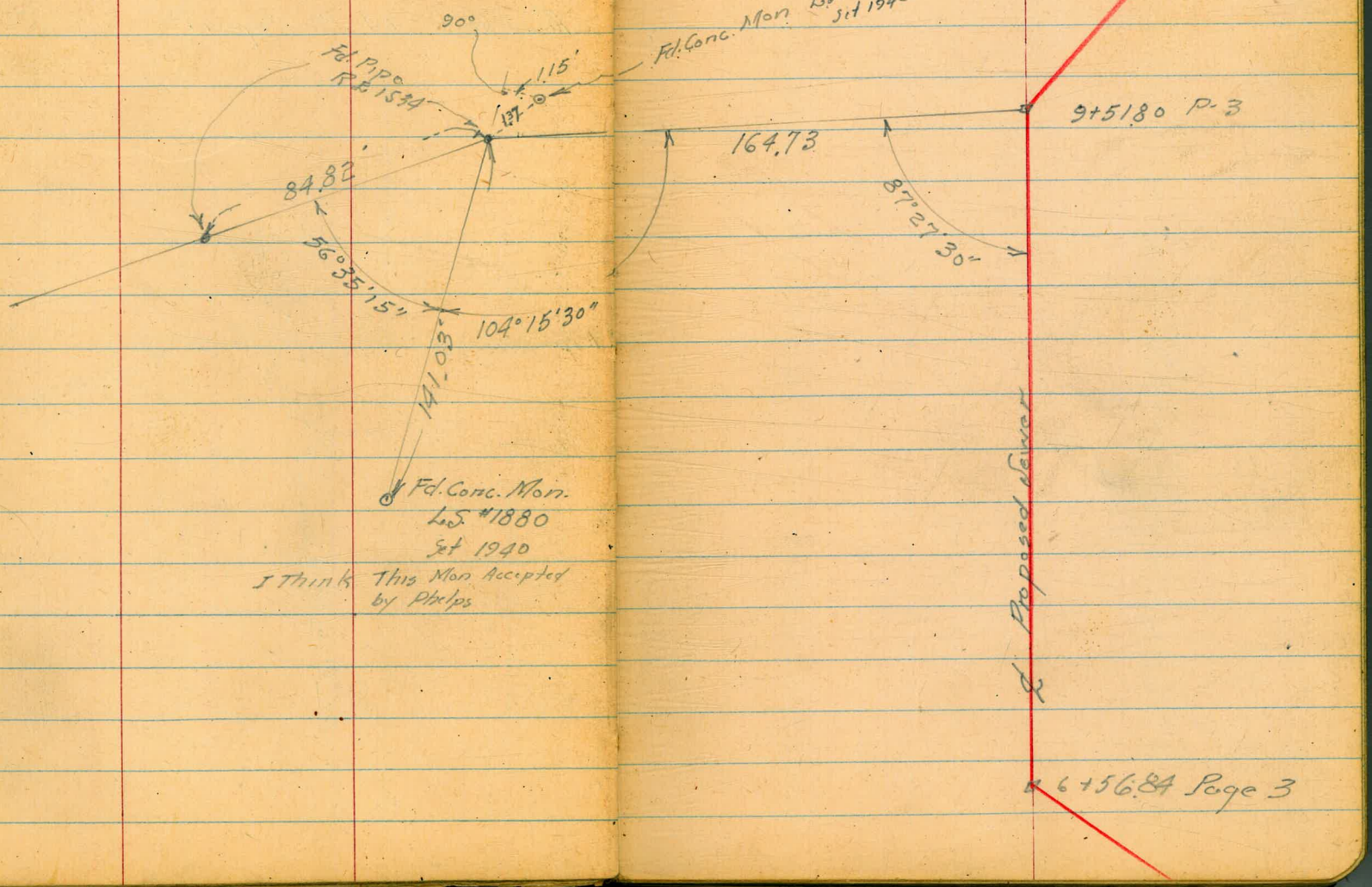
15.97
38.2
Flow 24" New Pipe

7.34
16.4
Flow 18"

B.M. on Hub 3+42.18 Page 11



Property Ties - Proposed Sewer in La Jolla Park



Walker
Johnson
Pope
Crawford
4-24-49

Levels - Proposed Sewer -
in Loyola Park
Location P-2-4

				Lt	℄	Rt
2+50				101.3 / 5.7 / 10	101.1 / 5.9	100.9 / 6.1 / 7 — 101.7 / 5.3 / 8 — 101.2 / 5.6 / 10
2+00				96.6 / 10.9 / 10	96.7 / 10.3	96.5 / 10.5 / 10
T.P.	11.85	⟨106.98⟩	0.14		⟨106.98⟩	
1+50				91.9 / 3.4 / 10	91.9 / 3.4	91.9 / 3.4 / 10
1+00				88.1 / 7.2 / 10 — 87.7 / 7.6 / 8 — 87.1 / 8.2 / 7	87.4 / 7.9	87.5 / 7.8 / 10
0+50				85.1 / 10.2 / 10 — 84.1 / 11.2 / 8	84.3 / 11.0	84.1 / 11.2 / 8 — 85.0 / 10.3 / 10
0+00 - Hub	12.76	⟨82.51⟩		83.0 / 12.3 / 10	82.9 / 12.4	82.8 / 12.5 / 7 — 83.1 / 12.2 / 10
	12.64	⟨95.27⟩	⟨82.63⟩	F.B. 2019-38 BM. 6+40.35		⟨95.27⟩

Levels Proposed Sewer
in La Jolla Park

	Lt	℄	Rt
4+50	113.6 ✓ 2.9 10	113.1 ✓ 2.0 8	112.6 ✓ 3.4
4+38 = ℄ Elec. Pole #PC #1759 5' Rt.			114.4 ✓ 1.8 7
			117.6 ✓ +1.6 10
			Toe Slope (Natural)
4+00.	111.9 ✓ 4.1 10	109.9 ✓ 6.1 4	109.4 ✓ 6.6
			109.4 ✓ 6.6 10
3+57		108.4 ✓ 7.8	
3+54.5 Elec. Pole 4.2' Rt #P-1757			
3+45	109.4 ✓ 6.6 10	109.2 ✓ 6.8	108.0 ✓ 8.0 10
3+42.18 = Δ Rt 68°21'45"		108.57 ✓ 7.42 on Hub	
T.P. 934 ⟨115.99⟩ ✓		⟨115.99⟩ ✓	
033 ⟨106.65⟩ ✓			
3+00	105.5 ✓ 1.5 10	105.7 ✓ 1.3	105.5 ✓ 1.5 5
			106.3 ✓ 0.7 10
⟨106.98⟩ ✓		⟨106.98⟩ ✓	

Proposed Sewer in Apollo Park

~ Levels ~

					Lt.	℄	Rt.
5+80							
T.P.	13.87	(132.48)	1.92	(125.61)			
					124.6	127.9	133.1
					14.9	11.6	6.4
					8=Toe slope		10
					6' wash		
						(139.48)	
5+50					121.5	120.2	121.4	127.0
					5.5	6.8	5.6	0.0
						4		10
						in wash = Toe slope		Side Hill
5+00					117.4	116.2	117.2	123.1
					9.6	10.8	9.8	3.3
					10	2	Toe	10
						in wash	Nat. slope	on Side Hill
4+88						115.0		
						12.0		
						in hole		
						in wash		
4+74					115.0	117.6	123.2
					12.0	9.4	3.6
					10	Toe slope	10
T.P.	12.04	(127.03)	1.00	(114.99)		(127.03)	
					116	114.2	119.7
4+60					1.8	1.6	+3.7
					10		10
		(115.99)				(115.29)	

Levels · Proposed Sewer in Lafollette Park

	Lt.	℄	Rt.
on Pipe PE 4847			
T.P.	12.24 (150.27) ✓	1.45 (138.03) ✓	
7+12 = Int Wash	137.9 ✓ 1.6 10	135.9 ✓ 3.6	137.9 ✓ 1.6 10
6+82	139.9 +0.4 10	135.8 ✓ 3.7	131.9 ✓ 7.6 16 in Wash
6+56.84 = Δ Lt. 12°19'30" Section on Bisector	140.9 ✓ +1.4 10	136.5 ✓ 2.97 on Hub.	131.9 ✓ 130.7 ✓ 134.5 ✓ 7.6 8.8 8.0 10 13 20 Bank Edge Wash Edge Wash
6+38		134.1 ✓ 5.4	
6+25 = ~~End~~ edge of Wash = Toe Bank	134.6 ✓ 4.9 10 Side Hill	128.6 ✓ 10.9 Edge Wash = Toe Slope	128.3 ✓ 11.2 10 edge wash = Toe Slope
5+97 = Beg. Wash (139.48) ✓	126.6 ✓ 12.9 8 Wash	126.3 ✓ 13.2 (139.48) ✓	131.3 ✓ 8.2 10 Side Hill

Levels Proposed Sewer
La Jolla

	Lt.	℄	Rt.
8+18		150.0 ✓ 11.8	
T.P.	12.22 (161.83) ✓	0.66	(149.67) ✓
		(161.83) ✓	
8+05	150.8 ✓ +0.5 10	150.3 ✓ 0.0 8	148.8 ✓ 1.5
	148.3 ✓ 2.0 3 Bottom Wash	148.6 ✓ 1.7 7	149.8 ✓ 0.5 10
7+97	149.6 ✓ 0.7 10	147.5 ✓ 2.8 4	146.6 ✓ 3.7 Bottom Wash
	147.1 ✓ 3.2 7	149.9 ✓ 0.4 10	
7+73		145.2 ✓ 5.1	
7+64	143.5 ✓ 6.8 10	142.7 ✓ 7.6 8 ± 2' Wide Wash	143.8 ✓ 6.5 6
	144.3 ✓ 6.0 1	145.0 ✓ 5.3	150.3 ✓ 0.0 10
7+29	137.8 ✓ 12.5 10 Bottom of Wash	138.8 ✓ 11.5	143.2 ✓ 7.1 10
	(150.27) ✓	(150.27)	

Levels - Proposed Sewer
Lapolla Park

				Lt.		℄		Rt.	
				160.3	160	160.0	160.2	165.0	
				11.0	11.1	11.3	11.1	6.3	
				10	3		2 Wash	10	
8+25									
T.P.	11.71	⟨171.35⟩	2.19	⟨159.64⟩		⟨171.35⟩			
						159.1			
8+85						2.7			
				157.9	157.5	157.1	157.1	158.8	
				3.9	4.3	4.7	4.7	3.0	
8+76				10	5		4	10	
						156.2			
8+58						5.6			
8+54 = Pole 16.8 Lt. Tel. ≠ J.P.C. 1787									
				155.5		154.5	154.6		
				6.3		7.3	7.2		
8+50				10			10		
				152.7	152.7	151.0	151.6	150.3	
				2.1	2.6	10.8	10.2	11.5	
8+33				10	8		4	10	Bottom Wash
	⟨161.83⟩					⟨161.83⟩			

Levels - Proposed Sewer
in La Jolla Park

Lt. | ℄ | Rt.

9+97

T.P. 12.45 (183.80) 000 (171.35)

9+97 = Tel Pole 18' Lt #300347-H

9+77

170.6	170.7	171.0	170.8	173.0
13.2	13.1	12.8	13.0	10.8
10	3		2	10

(183.80)

168.4	168.0	170.0
2.9	3.4	1.4
10	Wash	10

9+51.80 = Δ Rt 41°31'45"

166.[illegible]	166.40	167.0	166.4
5.1	4.95	4.4	4.2
10	on Hub.	5	10

9+36.

165.6
5.7

9+20

163.3	163.5	164.1	166.3	169.0
8.0	7.8	7.2	5.0	2.3
10	7	3		10
	Wash			

9+06

161.0	161.3	163.0	167.7
10.3	10.0	8.3	3.6
10	6		10
Wash 3' wide			

(171.35)

(171.35)

Levels - Proposed Sewer
in La Jolla Park

11+07

~~11+07~~

T.P. 13.03 (208.05) 0.26 (195.02)

10+94

10+78

T.P. 12.79 (195.28) 1.31 (182.49)

10+56

10+43

10+08 (183.80)

Lt.	℄	Rt.
199.6	196.6	198.7
8.4	11.4	9.3
10		10
	(208.05)	
	192.8	
	2.8	
185.8	186.3	187.1	188.6
3.5	2.0	8.2	6.7
10	4.0		10
	(195.28)	
180.2	179.1	181.8
3.6	4.1	2.0
10		10
179.6	179.4	178.8	178.1
4.2	4.4	5.0	5.7
10	5		10
173.0	174.2	174.1	174.6
10.8	9.6	9.7	9.2
10	5	(183.80)	10

11+63 (Section not in regular order)

11+69.14 ± P.O.T.

11+55

T.P. 13.08 (2.21.09) 0.04 2080.1

11+50

11+39

11+28

11+16 (2080.5)

Lt		℄	Rt.	
212.8	215.1	215.2	215.6	216.4
8.3	6.0	5.2	5.5	4.7
10	4		7	10
215.5		216.45	216.6	
5.6		4.64	4.5	
10		on Hub.	10	
		211.6		
		9.5		
		(2221.09)		
203.0		206.0	208.0	
5.0		2.0	0.0	
10			10	
201.0	204.7	205.2	206.2	
7.0	3.3	2.8	1.8	
10	3		10	
		200.4		
		7.6		
194.1		197.2	199.7	
13.9		10.8	8.3	
10		(2008.05)	10	

Levels - Proposed Sewer

Lo/olla Park

Lt ℄ Rt. 19

.004

1"x1" Paving Stake 180.62

Check 0+00 FB. 2019/57 5.12 (180.66) ✓

T.P. 2.24 (185.78) ✓ 13.05 (182.84) ✓

T.P. 0.39 (195.89) ✓ 12.80 (195.50) ✓

T.P. 0.01 (208.30) ✓ 12.80 (208.29) ✓

12+03.42

11+98.81

11+87 = Int. Curb Line

(221.09) ✓

216.87 ✓

4.22

27.75

on Ld. Plg.

in Conc. Paving

216.79 ✓ 209.04 ✓

4.30 12.05

on Rim MH 0

on Flow Line

216.79 ✓ 216.36 ✓

4.30 4.73

on 0

curb on Conc. Paving

(221.09) ✓

Torrey road
St. Louis Terrace (East + West)

6-9-49

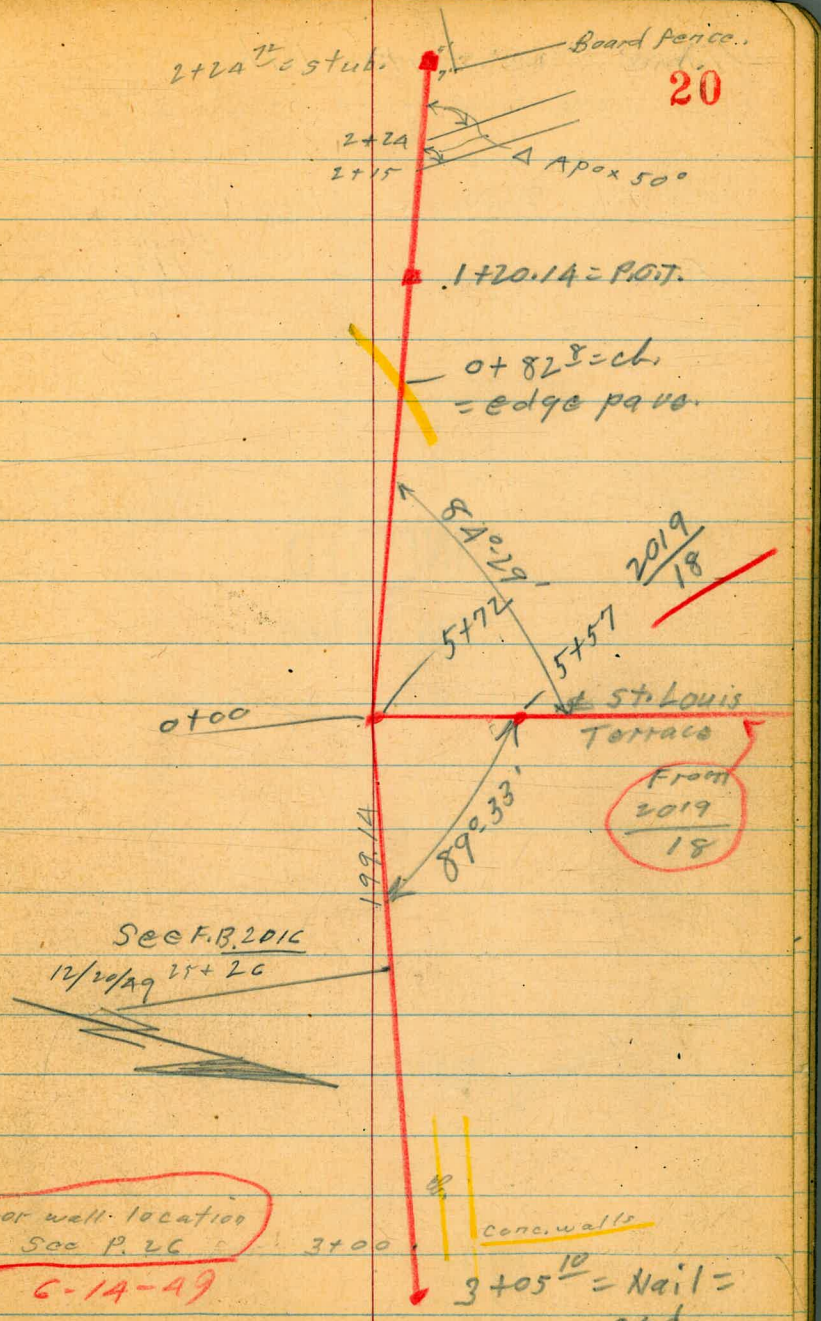
Sommermeyer
McCoy
Allen

Levels page 23 to 26

See P. 24 for fence opposite 2+23 & 2+24½ on line to west.

6-14-49

INDEXED
JUN 19 1950



Thru easement Blk
Bet Roseland Dr + St Louis Ter.

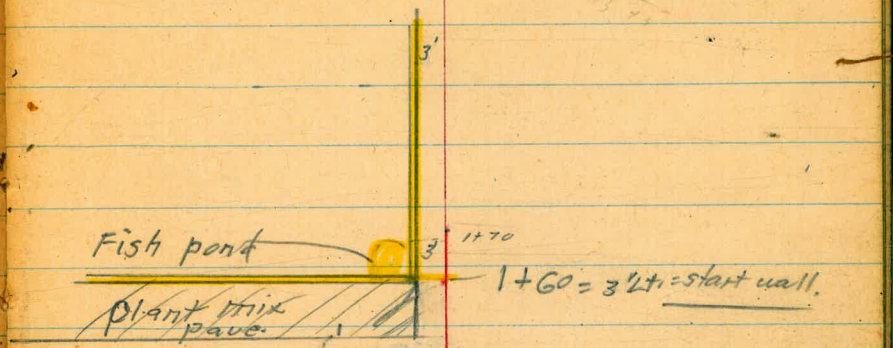
S. Wly. from Roseland

6-10-49

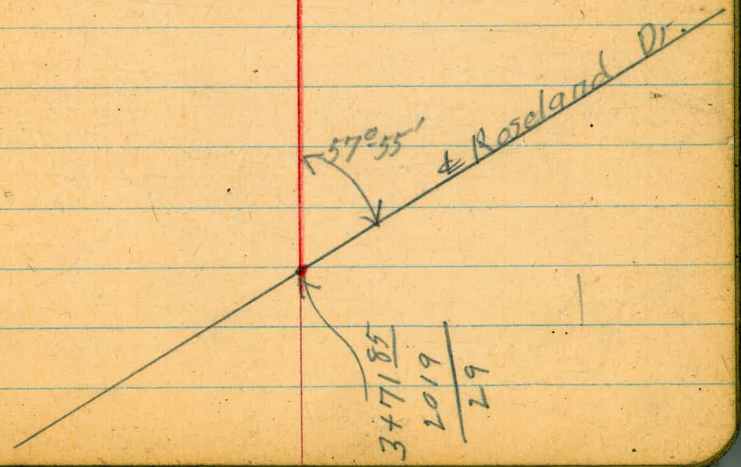
Sommermeyer
McCoy
Allen

INDEXED
MK
JUN 19 1950

Levels - P. 27



1+21 43 P.O.T.



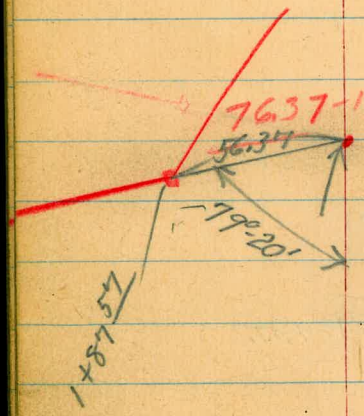
Prelim. Sewer La Jolla Hills (Lots 1-12)

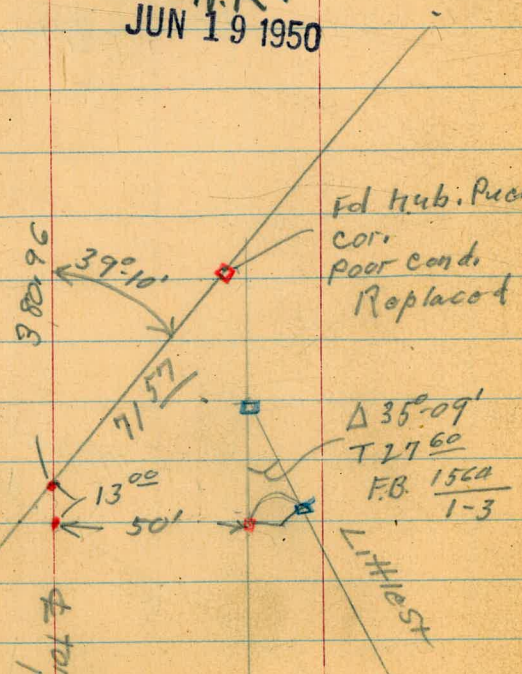
Torrey Rd. - Sly. - between Hillside + Lookout

6-9-49

Sommermeyer
McCoy
Allen

Levels
P. 31





Torrey Road
West from St. Louis Terrace

sketch - P. 20

T.P	8.12	(96.78) ✓	0.36	(88.66) ✓
1+00				
0+82.8 Cont.	Top. cl.			
0+82.8	Leave	Pave.		
+50				
+25				
+13				
0+00 (P. 20) = St. Terrace extended to Sta. Page no 2019/22				
B.M. = 5157 F.B. 2019/22	12.02	(89.02) ✓ . —		77.0 ✓

96.78 ✓

88.7
0.3

85.0
4.0

84.5
4.5
G

80.7
8.3

7.4 / 9E / cl	7.9 / 9E / G	9.0 / 11 / G	8.5 / 11 / cl

18.2 ✓
10.8

77.6 ✓
11.4

77.2 ✓ ✓
11.8

11.2 / 5 / Top cl	11.7 / 5 / G

89.02

Torrey Road

West of St. Louis Terrace

2+24.72 = stub end

at aprox. Δ of 50° - See P. 19
outlet can come out from house

2+24 shot in yard at point sewer

2+24.72 5' Rt. = fence
2+23 - 7.3 Rt. = Cor. of fence
see sketch P. 20

} 6-14-49

2+15 shot in yard Δ aprox 50°-

2+14 Top rock & grout wall

2+13.7

1+73 { 9' Rt. = 6' wide N. & S. Cedar hedge
{ 9.5 Lt. = 14" diam. eucalyptus

1+50

1+20

96.78

91.2
5.6

91.2 87.5
5.6 9.3
50.
Grd. in yard

91.1 87.8
5.7 9.0
45
Grd. level over septic tank

91.1
5.7

90.3
6.5

91.2
5.6

89.7
7.1

96.78

Torrey Road

East of St. Louis Terrace

2+47 { Ord. along house to left. (100' Lt. / 60' Lt.) } Ord. over sewer outlets

2+30. 110' = Grd. over septic tank.

T.P. 8.52 〈95.69〉 0.58 〈87.17〉

2+00

1+67 3' Lt. = △ in ch. line of house.

1+18. 50' Lt. = shot in yard back

1+00

0+50

0+00

5+77. +B 2019 2/4 10.75 〈87.75〉 — 77.0

See 2019 2/4

8.2 / 13.0 / 100 — 8.3 / 14.0 / 6" / 60 — 8.1 / 7 / C in drive — 8.7 / 8.6 — 8.5 / 8.2

7.7 / .18 / 110 — 8.7 / 9.0 — 〈95.69〉

8.3 / 3.9 / 3.7 ch — 8.3 / 4.4 / 3.7 C — 8.3 / 4.4

7.3 / 10.4 / 50 Grd — 8.1 / 6.6 / 15 — 8.3 / 6.4 / 7 ch — 8.0 / 6.8 / 7 C — 8.1 / 6.6

8.0 / 7.4

7.8 / 9.4 / 12' ch. — 7.8 / 9.8 / 12' C — 8.1 / 9.6 — 8.2 / 9.5 / 7 9 C — 8.8 / 8.9 / 7 9 ch

7.7 / 10.55

8.5 / 2.7

8.3 / 4.4

8.1 / 6.6

87.75

Torrey Road
East of St. Louis Terrace

3+05 End

3+00 { else = ℄ N.4S. conc. wall.
15 Lt. : face E+w. conc. wall
9 Lt. : Cb. face } 4-10-49

2+75

90.7 ✓
5.0
50
Ord.

90.4 ✓
5.5

88.9 ✓
6.8

95.69

Thru Easement
Bet Roseland Dr + 24 L. Terrace.

1+38 3' Lt. = start plant mix pave.

1+25

1+00

T.P. 11.93 (59.67) ✓ 1.16 (47.74) ✓

+50

+33

+28

+20 end oil + rock pave.

0+00 (See page 21)

Nail 3+50
2019
3.2
EL: 36.2

12.70 (48.90) ✓ 36.2 ✓

Sketch P. 21

58.7 58.0 57.8 ✓
1.0 1.7 1.9
3 2
oil pave.

56.0 ✓
3.7

52.4 ✓
7.3

(59.67) ✓

44.5 ✓
4.4

41.8 ✓
7.1

38.0 ✓
10.9

36.9 ✓
12.0

37.8 ✓
11.1

(48.90) ✓

Δ · 3+24.60
(2089/38)

5.46 ⟨71.67⟩ (71.65)

T.P 5.92 ⟨77.13⟩ 1.01 ⟨71.21⟩

T.P. 12.82 ⟨72.22⟩ 0.27 ⟨59.40⟩

1+75

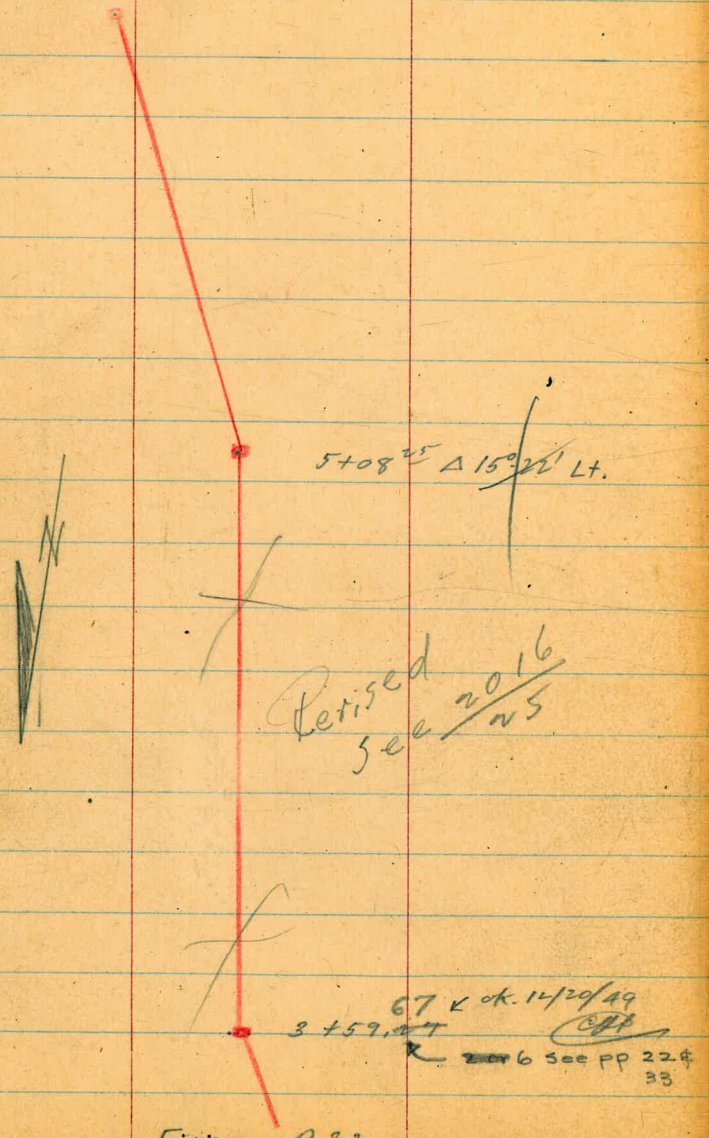
1+60 3'Lt. = start tile wall

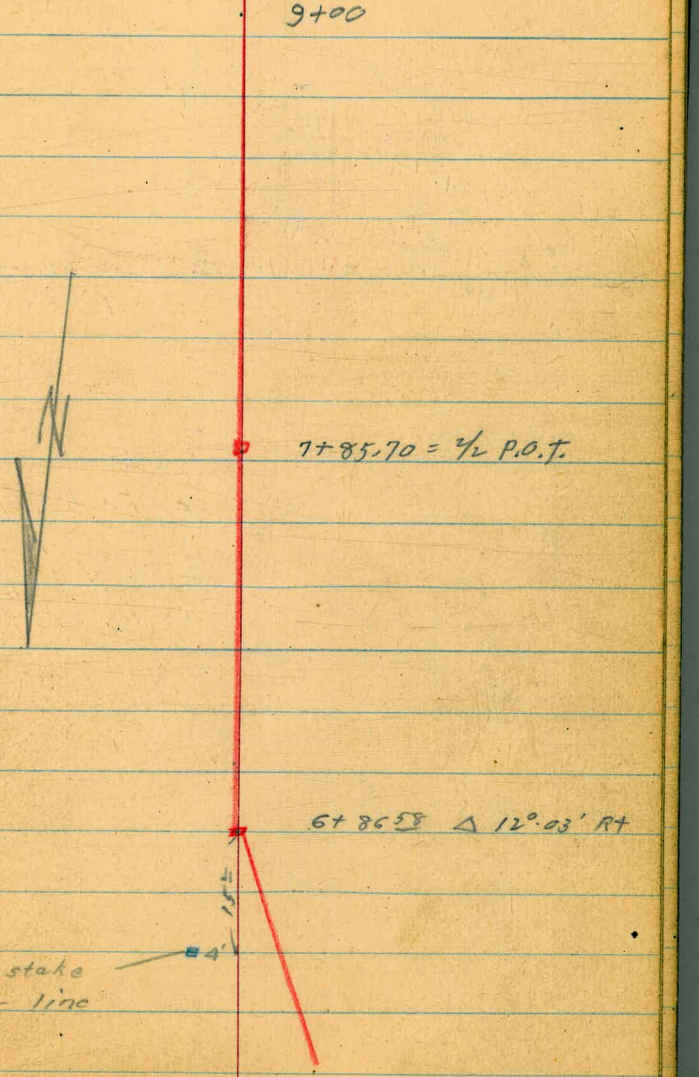
⟨59.67⟩

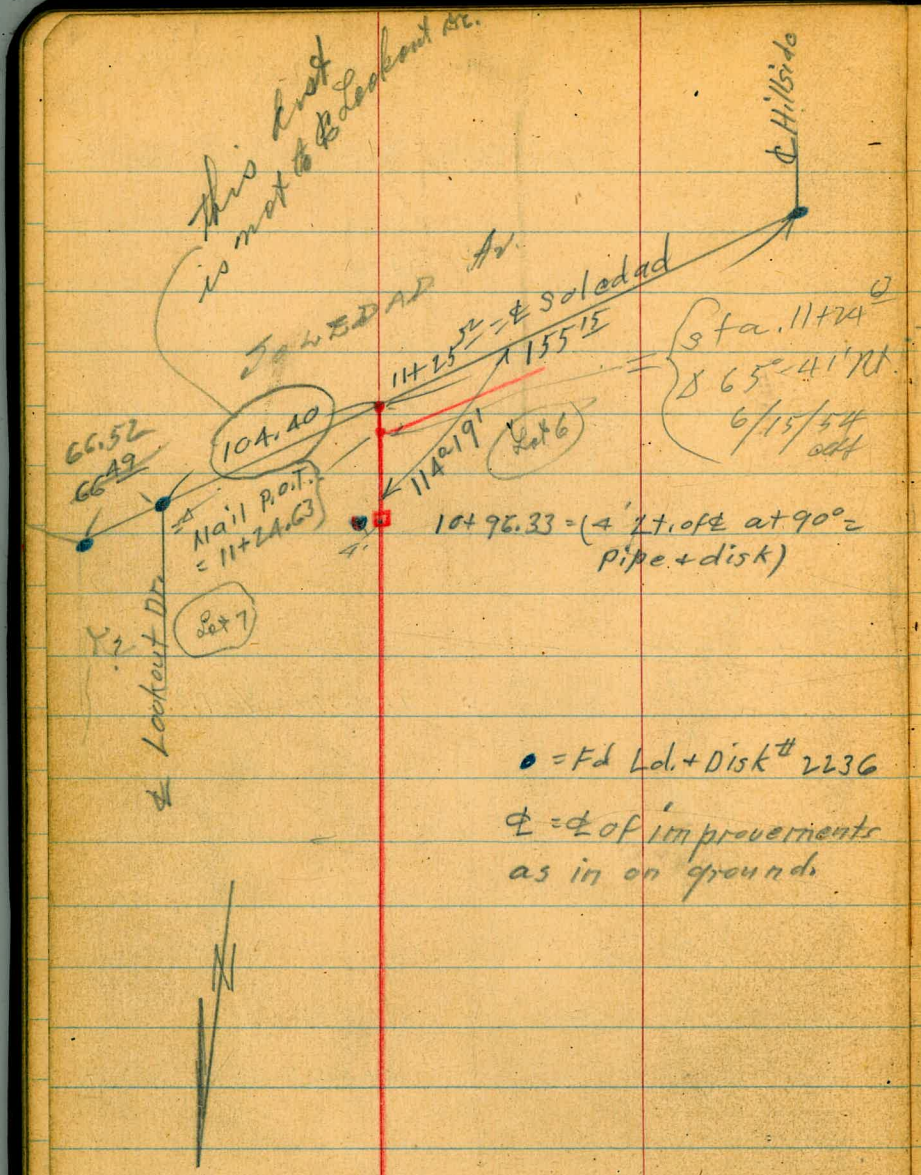
59.7
0.3/3 0.5
58.4
40/3 1.3

⟨59.67⟩

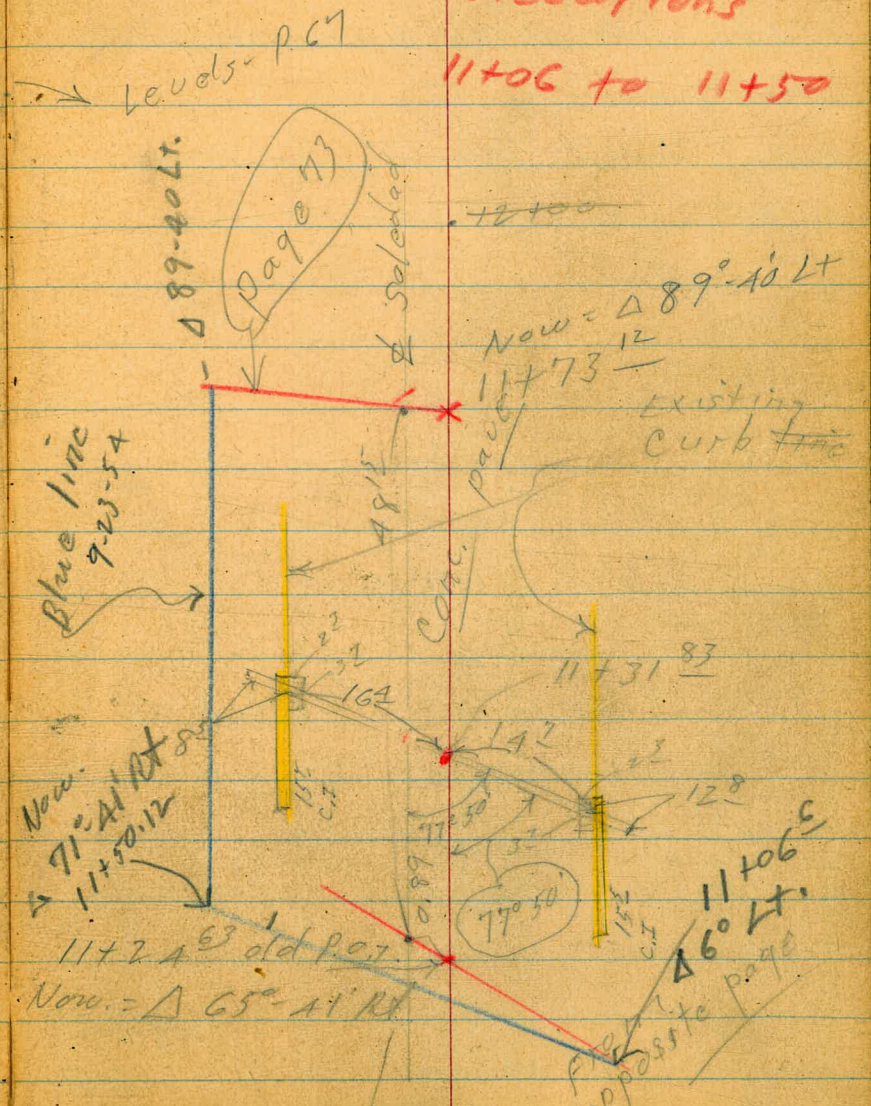
Prelim. Sewer La Jolla Hills.
Lots 1-12
So. of Torrey Rd. Between Hillside & Lookout.







See page 75 for Elevations 11+06 to 11+50



La Jolla Hills Lots 1 to 12
Sketch P22+29

1+84 5E Lt.= 12" diam eucalyptus

1+50

1+00

+83

+75

+64.5 Edge of Paving

0+32 ℄ Torrey Pines Rd

0+00±

0+00= Exist M.H. (P.22)

8.72 98.89

90.17 B.M.#2 FB 2019 19

N 77° 58' W Little Torrey Pines Rd

E W

94.0 94.1 98.9
4.9 4.5/3 0.0/6

93.6 93.6 98.9
5.3 5.3/3 0.0/8

93.6
5.3

92.1
6.8

92.34
6.55

92.94
5.95

93.01
5.88
M.H. cover

89.09
3.80
INVert

T.P. 13.19 ⟨119.78⟩ 0.37 ⟨106.59⟩

3+10

3+02 9' Lt. = P. pole # P.O. 20790

+76

2+40

T.B. 8.26 ⟨106.96⟩ 0.19 98.70

2+25

w = bottom of wash

2+10

1+95 = Cross row of trees, average trunk diam = 5"

+92 { 10' Lt. = intake 24" N.+S. culvert
3' Lt. = wly. end rock wall for culvert

+90 7' Rt. = 6" diam eucalyptus

1+87.56 Δ 50° 19' Rt.

⟨98.89⟩

107.0 102.2 102.2 102.2 104.2 109.0

0.0 / 12 | 4.8 / 11 w | 4.8 / 6 w | 2.8 | +2.0 / 7

99.4 104.2 108.7

7.6 / 11 w | 2.8 | +1.7 / 6

97.0 98.0 102.6 107.0

10.0 / 20 w | 9.0 / 13 | 4.4 | 0.0 / 6

⟨106.96⟩

98.9 104.9

0.0 | +8.0 / 10

94.9 91.4 94.9 96.3 98.9

4.0 / 18 | 7.5 / 15 w | 4.0 / 13 | 2.6 | 0.0 / 15

93.7

5.7

90.5 93.8 93.9

8.4 / 10 invert | 5.1 | 5.0 / 10

93.5 93.8 93.9

5.4 / 10 | 5.1 | 5.0 / 10

⟨98.89⟩

4'Rt. 4+99
Set B.M.
Nail pole "BC 2070

9.98 ⟨141.81⟩ 0.28 ⟨131.83⟩ BM #3

5+08 25 Δ 15°-22' Lt. Lee 2016 30

4+99 4'Rt. = B.C. 2070

4+85

4+54

4+42

T.P. 12.85 ⟨132.11⟩ 0.52 ⟨119.26⟩

4+14 cross wash

4+09± 12 Lt. = 4×4 post.

4+00

+80 cross wash

3+59 67 Δ 3°-46' Rt.

⟨119.78⟩

E W

132.1 126.1 129.1 131.0 137.1
0.0/18 6.0/9 3.0/5 1.1 +5.0/10

130.1 123.0 126.4 131.1
2.0/15 9.1/5 W 5.7 1.0/10

126.1 121.1 124.2 128.1
6.0/15 11.0/5 W 7.9 4.0/12

125.7 120.5 116.1 122.5 126.7
6.1/14 11.6/4 16.0 W 9.6/8 5.4/18

⟨132.11⟩

123.0 115.8 112.6 116.8 118.3
+4.0/10 4.0/2 7.2 W 3.0/2 1.5/10

120.8 117.5 110.8 115.3 118.3
+1.0/8 2.3 9.0/5 W 4.5/8 1.5/15

118.8 114.3 119.8
1.0/10 9.5 W 0.0/10

109.7 115.05 119.7
10.1/9 W 4.73 Hub 0.1/7

⟨119.78⟩

6+09 6' Lt.: end of defined wash

6+08

6+04 Cross wash

6+00

T.P. 9.66 (148.39) 3.08 (138.73)

5+85

5+70

5+50

5+42

5+35

(141.81)

142.2 / 6.2 / 6 W — end of W

142.3 / 6.1

138.5 / 9.9 / 6 W

141.5 / 6.9

138.2 / 10.2 / W

140.8 / 7.6

138.0 / 10.1 / 6 W

(148.39)

142.8 / +1.0 / 10

138.7 / 3.1

138.0 / 3.8 / 3

135.3 / 6.5 / 5 W

136.1 / 3.7 / 7

138.8 / 3.0 / 15

145.4 / +3.6 / 10

138.4 / 3.4

135.0 / 6.8 / 11 W

136.8 / 5.0 / 15

137.4 / 4.4 / 20

138.8 / 3.0 / 10

133.6 / 8.2

130.3 / 11.5 / 5 W

133.6 / 8.2 / 10

133.6 / 8.2 / 5

128.9 / 12.9 / W

133.1 / 8.7 / 5

136.8 / 5.0 / 20

132 / 9.8 / 12

127.4 / 14.4 / 6 W

132.0 / 9.8

136.6 / 5.2 / 10

(141.81)

T.P. on Hub
P.O.T. 7+85.70 12.93 (170.53) 0.71 (157.60)

7+70 { 5' Lt. = start plank retaining wall
{ 18 Lt. = Pole # P.C. 2040

7+65

7+35

7+23 1' Lt. = 8" tree

7+15 7' Rt. = 10" tree

6+86.58 Δ 12°-03' Rt.

T.P. 10.05 (158.31) 0.13 (148.26)

6+58 1' Rt. = 4x4 post (wood bridge)

6+54

6+51 0.8 Lt. = 4x4 post - (wood bridge

6+25

(148.39)

157.2 ? 145.6 13.3/15 162.3 +4.0/25 154.9 3.4/20 152.3 6.0/15 153.1 5.2/15

157.5 145.9 13.0/5 154.4 1.9/15 154.5 3.8/15 151.7 6.6/5 149.9 8.4/6

156.6 146.4 13.9 (170.53) 154.6 1.7/4 153.4 4.9/12 151.7 6.6 149.2 9.1

(158.31)

156.6 158.3 154.6 0.0/10 156.5 159.1 +0.8/10 154.0 4.3 151.7 154.8 157.3 3.5/7 1.0/15 149.7 152.8 8.6/11 5.5/20

148.4 0.0/10 145.7 2.7/4 145.9 2.5 147.4 1.0/10

143.8 4.6/10 143.4 5.0 145.1 3.3/10

(148.39)

+24 - 11' Lt. = 12" diam. plum tree
for elder tree at 9+30 - 3' Rt.

7+23 - 4' Lt. = start 10" diam tree row.

8+95 4' Lt. = Pole P.C. 2034

T.P. 12.20 ⟨180.43⟩ 2.30 ⟨168.23⟩

+83 3' Rt. = 18" Eucalyptus

+73 3' Rt. = 16" Eucalyptus

8+65

+64 3' Rt. 12" diam. elder

+58 5' Lt. = 4" diam tree

+35

+33 { 5' Lt. = end wood retaining wall
3' Rt. = 4" diam. fruit tree

8+30

8+29 9' Lt. = end row (6 trees) Eucalyptus

8+07 2' Lt. = 2" diam eucalyptus

7+88 { 4' Lt. = 4" diam. Acacia
8' Lt. = start row Eucalyptus. 12" to 30" diam.

7+71

⟨170.53⟩

172.0 170.3 171.3 173.9

8.4/20 10.1/10 9.1 6.5/10

⟨180.43⟩

167.5 167.0 167.5 170.5

3.0/10 3.5/5 3.0 0.0/10

166.13 165.7 166.4 165.7 169.3

4.4/10 4.8/5 5.1 4.8/12 1.2/20

167.5 165.8 164.5 164.7 165.0

3.0/15 4.7/6 6.0/5 5.8 5.5/15

160.5 160.4 157.5 156.6 156.8 161.6

10./15 10.1/6 13.0/5 13.7 13.7/5 8.9/10

⟨170.53⟩

T.P. 12.29 ⟨205.01⟩ 0.03 ⟨192.72⟩

10+30

10+19 — 3 3/5 Lt. = End lath fence + start board fence
2 5/5 Lt. = deadman
4' Lt. = End conc. wall (8" wide E & W. wall)

9+91 3' Lt. = pole # P.C. 2030

+86 05 4 4/5 Lt. = Pipe + disk #

+74 60 4.8 Lt. = disk in pipe (Disk # 2317)

+74 15 4 4/5 Lt. = iron pin

+66 11' Lt. = 10" diam. plum tree

+56 11' Lt. = 4" diam fig tree

+55

T.P. 12.49 ⟨192.75⟩ 0.17 ⟨180.26⟩

+46 4 5/5 Rt. = 10" Acacia

+43 12' Lt. = 14" plum tree

+38 4 5/5 Lt. = start lath fence

9+30 — 3' Rt. = 12" diam elder

9+25

⟨180.43⟩

190.2 190.0 189.5 189.9

2.6/10 2.8/5 3.3 2.9/10

184.8 184.3 184.6

8.0/10 8.5 8.2/10

180.8 179.8 180.4 181.8 182.3

12.0/30 13.0/20 12.4/10 11.0 10.5/10

⟨192.75⟩

175.4 176.4 178.0

4.9/10 7.0 2.4/10

⟨180.43⟩

Lots 1-12 La Jolla Hills

38

0.84 ⟨215.67⟩ 215.61 2028 37

11+42.5 ℄ = End exist. ch. + ch. inlet

11+25.5 ℄ = ℄ Soledad Rd. (Conc. pave)

also = end ch. inlet.

11+12 7.8' Rt. = Ely end exist ch.

11+06.6 3' Lt. = 18" Pole P.C. 2020 Δ 6°00 Lt

T.P. 11.70 ⟨216.51⟩ 0.20 ⟨204.81⟩

11+00 13' Rt. = outlet 36" conc. drain

10+96.33 = 4' Lt at 90° = pipe + disk # 2236

+89

+87 - 12.5' Lt. = S.W. cor. frame garage.

10+75 - 6' Lt. = N.W. cor. frame garage.

10+55 - 4.7' Lt. = end board fence

⟨205.01⟩

205.87 10.64 top ch.

N 05.12 11.39 ℄ on ℄ produced.

204.95 11.5 c

204.4 12.1

205.24 11.27 78 top ch

204.41 12.10 ℄ 78

⟨216.51⟩

196.1 8.9 13 invert

197.1 7.9 10

197.3 7.72 Hub.

196.4 8.6 10

195.8 9.2

193.01 17.00 15

192.5 12.5 4

192.0 12.1

193.3 11.7 15

⟨205.01⟩

LOWRY TERRACE.

Pasco Dorado to Roseland Dr.

6-14-49
W.O. 31720

Sommermeyer
McCoy
Allen
Bunch

INDEXED
MK
JUN 19 1950

2+30.34
Δ 22°-45' Rt.

Δ 22°-45'
℄ Rad. 200
T 40.24

6-15-49
See 2019
3

97°.02'

A.82

0+00

Pasco Dorado

4+04

See 2019
3

Note
Data from
Assessors Maps
#33A sheet 1
#33A " 2
+ Tentative map
folder #23092

105

104

103

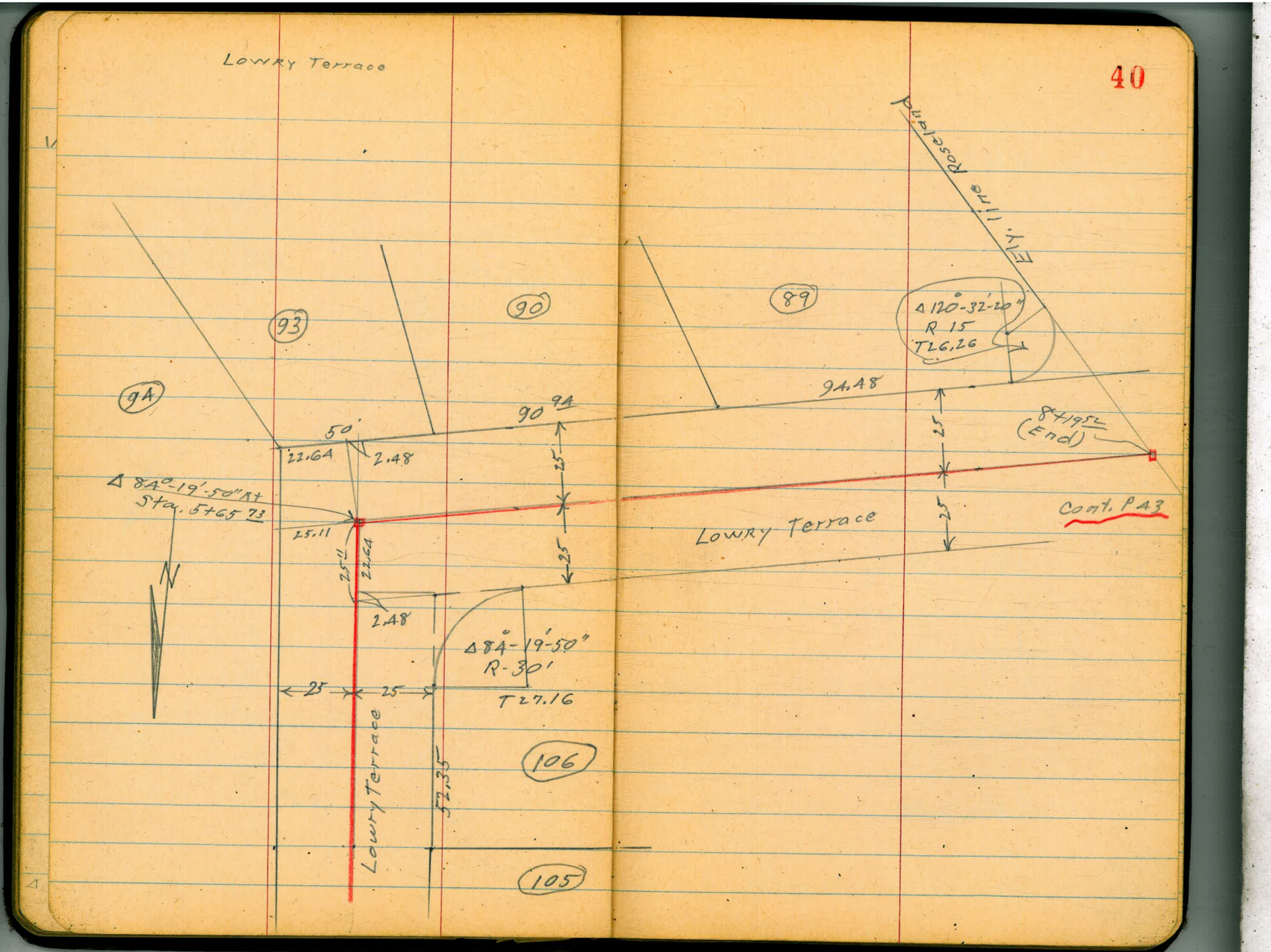
8½'

29'

curve E.C.

Δ 22°.45
℄ R=200.
T.=40.24

2+30.34
Δ 22°-45' Rt


Lowry Terrace
Roseland Ave.
93
90
89
94A
Δ 84°-19'-50" At Sta. 5+65.73
Δ 120°-32'-20"
R 15
T 26.26
91.48
90.94
50'
22.64
2.48
25
8+19.52
(End)
Cont. P 43
Lowry Terrace
25.11
22.64
Δ 84°-19'-50"
R-30'
T 27.16
25
25
Lowry Terrace
52.35
106
105

Lowry Terrace

2+30 31 = Δ 22°-45'- RT = stub				10.68
2+00				11.1
+50				11.5
1+00				12.3
+50				12.8
0+13	Top - back of roll curb.			12.28
0+12	Gutter			12.58
0+00				12.34
T.P.	12.36	16.98	6.13	4.62	16.98
N.E.S.P. Paseo Dorado Calle de la Plata.	3.08	10.75	—	7.67	

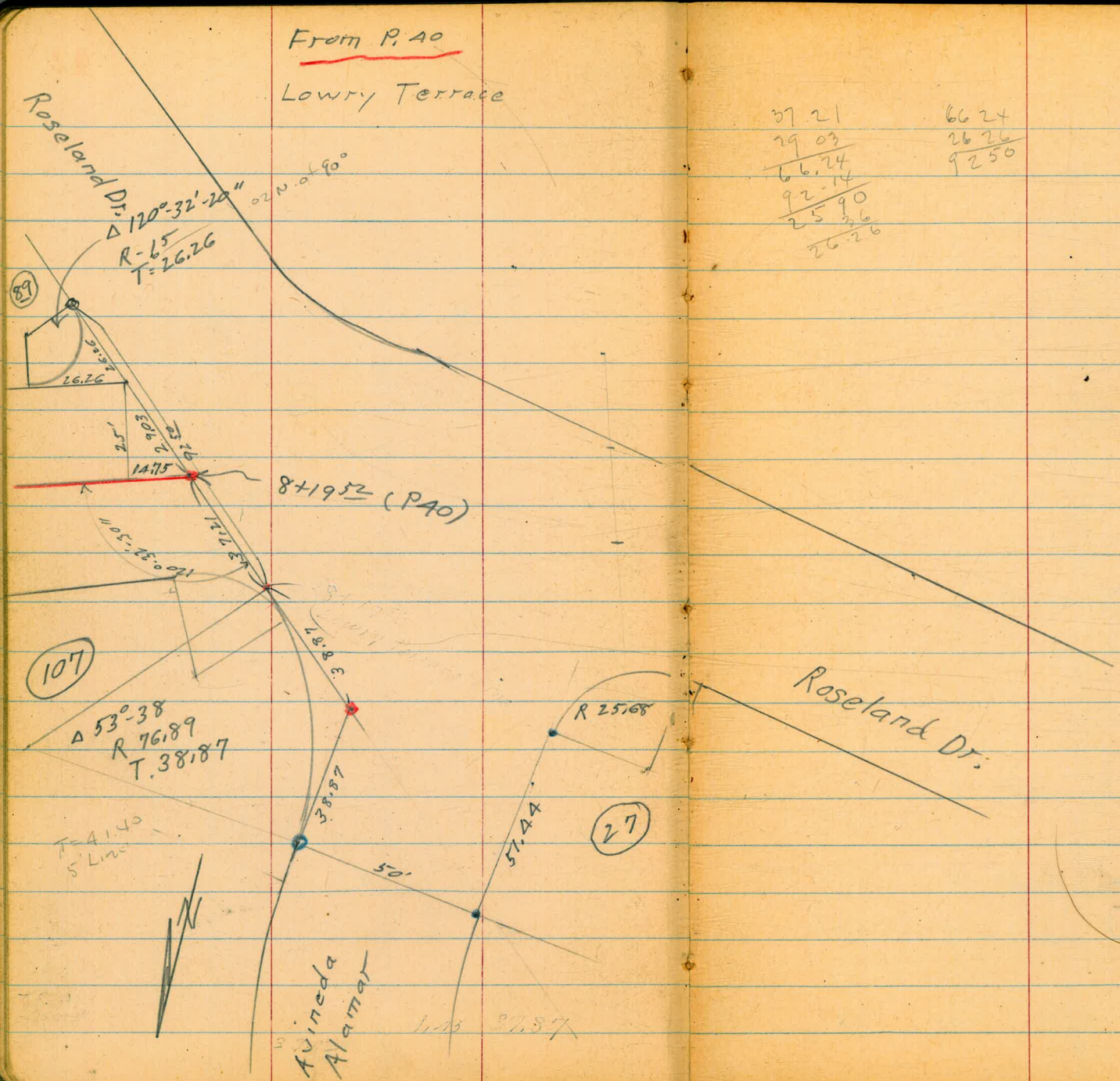
Lowry Terrace

5+50				
+40				
5+00				
T.P.	12.03	39.32	1.60	27.29
4+50				
T.P.	12.73	28.89	0.82	16.16
4+00				
+50				
3+00				
2+70				
		16.98		

4.2/50	2.2	1.8/40
5.3/50	7.7	7.0/50
7.8/50	11.1	14.7/50
	39.32	
5.9/50	7.1	8.6/50
	28.89	
	1.3	
	5.8	
	9.1	
	10.1	
	16.98	

From P. 40

Lowry Terrace



37.21
29.03
66.24

66.24
26.26
92.50

92.90
25.90
26.26

Lowry Terrace

B.M. #4 2019/43		3.67	44.71 (44.75)				
				4.12 stub			
8+00				3.3			
+50				3.1	3.0/25	5.1/50	6.2/75
7+00				7.00			
+75				9.5	10.5/34	16.9/46	19.9/75
+50				9.9			
6+00				10.5	10.8/21	16.7/31	16.9/50
5+65 73	Δ 84°-19'-30" Rt			10.65			
set B.M. on Δ / stub		10.65	37.73	48.38			
T.P. Stub.		10.51	48.38 / 39.32 From P42	1.45	37.87		

6/15/49

AVENIDA ALAMAR

Roseland to Paseo Dorado

Line Change

see Sketch FB. 2019 P. 40-41 + 42

T.P. 0.41 (33.13) 12.69 (32.72)

1+37 end of crossing Wash

1+32 Bottom of Wash

1+25 start of crossing of Wash

1+00

0+40

0+25 edge oil pvt

0+00 ± 1079.48 (2019 / 42) ON oil pvt

BM #4
2019
43 + 0.66 (48.41) — (44.75) (2019 / 43)

℄

3 N. 8 ✓ 12.6

N 8.8 ✓ 16.6 / 4 Bottom Wash

3 N. 8 ✓ 12.6 / 10 edge Wash

N 9.3 ✓ 16.1 Bottom Wash

3 0.8 ✓ 14.6 / 5 Bottom Wash

3 4.3 ✓ 11.1 / 1 edge Wash

3 4.3 ✓ 11.1

3 4.5 ✓ 10.9 / 15

3 3.1 ✓ 12.3 / 30

3 N. 8 ✓ 12.6 / 12 Bottom Wash

3 6.2 ✓ 9.2 / 9 edge wash

3 6.1 ✓ 8.7

3 6.1 ✓ 8.7 / 8 edge wash

AN. N ✓ 3.2

AN. 65 ✓ 2.76 edge oil pvt

43.45 ✓ 1.96

(45.41) ✓

Avinida Alamar
Line change 6-15-49

Levels Contd 2019/46

= 2+91.54
3+03.60 = Δ

2+80

2+42

2+34

2+25

1+85

1+75

33.13

0.83
12.30
3+46.

42.
10.9
8
End wash

27.
10.9

25.1
8.0
7

24.3
8.8
5
wash

25
7.9
2

25.1
7.9

23.6
8.5

26.0
7.1
10

26.3
6.8

23.9
9.2
3
wash

26.4
6.7
6

28.7
4.4
10

29.
3.9

26.4
6.7
1

26.4
6.7
5
wash

29.3
3.8
6

29.9
3.2

33.13

Additional Levels
Paseo Dorado + Spindrift Dr.

Sketch 2019/4

6-15-49

Original notes in F.B. 2019/4

INDEXED
M.C.
JUN 19 1950

= 15+37.00
15+36.78 = Roseland Drive line intersection

15+00

14+80± (See Sketch locating Seawall of Tennis Club 2019. Back Flyleaf)

+50

14+00

T.P. 11.30 ⟨17.47⟩ 1.13 ⟨6.17⟩

13+45.61 = Δ 9° Rt. on split of Δ = ob.
75°-01' Lt

13+00 3° Lt. = ob.

=10+69.00 cc 5.76 ⟨7.30⟩ — ⟨15.4⟩
0+00 2@28/40

47

See page 49
for change 6/17/49

15.13
2.34

11.68
5.29

9.05
8.42

6.55
10.92
⟨17.47⟩

4.35
2.95

2.64
4.66

⟨7.30⟩

Additional notes

Villa tract. La Jolla Park.

Original notes (2019 57-65)

Stationing from original notes

5+80

4+18 Cont.

4+18

3+30 Cont.

3+30

2+51

Elevations shown.

104.0 / 60 — 91.0 / 39 — 84.6 / 29 — 83.0

124.5 / 60 — 119.5 / 50

111.4 / 38 — 102.3 / 24 — 94.4

134.0 / 65 — 129.7 / 55

124.7 / 45 — 112.5 / 25 — 103.6 / 10 — 103.7

119.6 / 20 — 111.7 / 13 — 118.1

Levels on Spindrift Change

Sec 2019 / 4

6-27-49

Sommermeyer
McCoy
Bunch

13+79.$\frac{68}{}$ = Δ 50°-12' Lt.

+35 2' Lt. : face ch.

13+00 9898

12+80.$\frac{70}{}$ Δ 33°-50' Lt.

+50

12+00

+50

11+00

10+69.$\frac{66}{}$ Δ 4°37' Rt (2019 / 4) 6/27/49

7.58 ⟨9.12⟩ — 1.54 10+67.66' P.47

5.84 ✓
3.28

3.67 ✓
5.45

2.62 ✓
6.50

2.38 ✓
6.74

2.16 ✓
6.96

1.90 ✓
7.22

1.74 ✓
7.38

1.56 ✓
7.56

1.54 ✓
7.58

⟨9.12 ✓⟩

Spindrift.

= 15+37.00 Ahead } = Δ 2°-17' Rt.
15+35.75 Back }

15+00

1A+50

T.P. 10.17 ⟨18.02⟩ 1.27 ⟨7.85⟩

1A+00

⟨9.12⟩

15.1 ✓
2.90

11.77 ✓
6.25

9.81 ✓
8.81

⟨18.02⟩ ✓

6.81 ✓
2.31

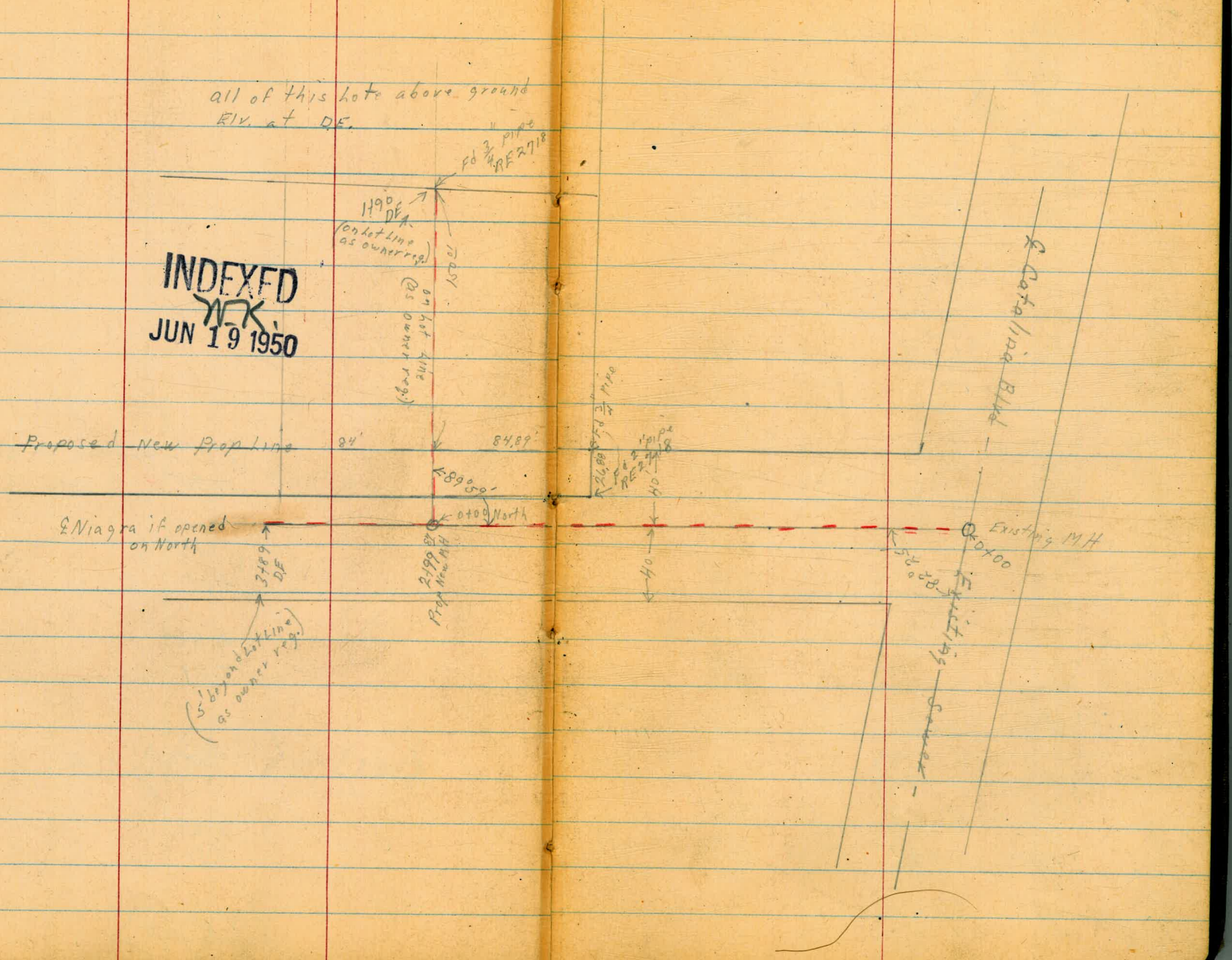
⟨9.12⟩ ✓

D. Smith
E. Sherman
G. Cota

Alignment Proposed Sewering Lot 18 South of Niagra West of Catalina

7-16-50

51



D. Smith
E. Sherman
G. Cota

W.O.# 62184

7-16-50

52

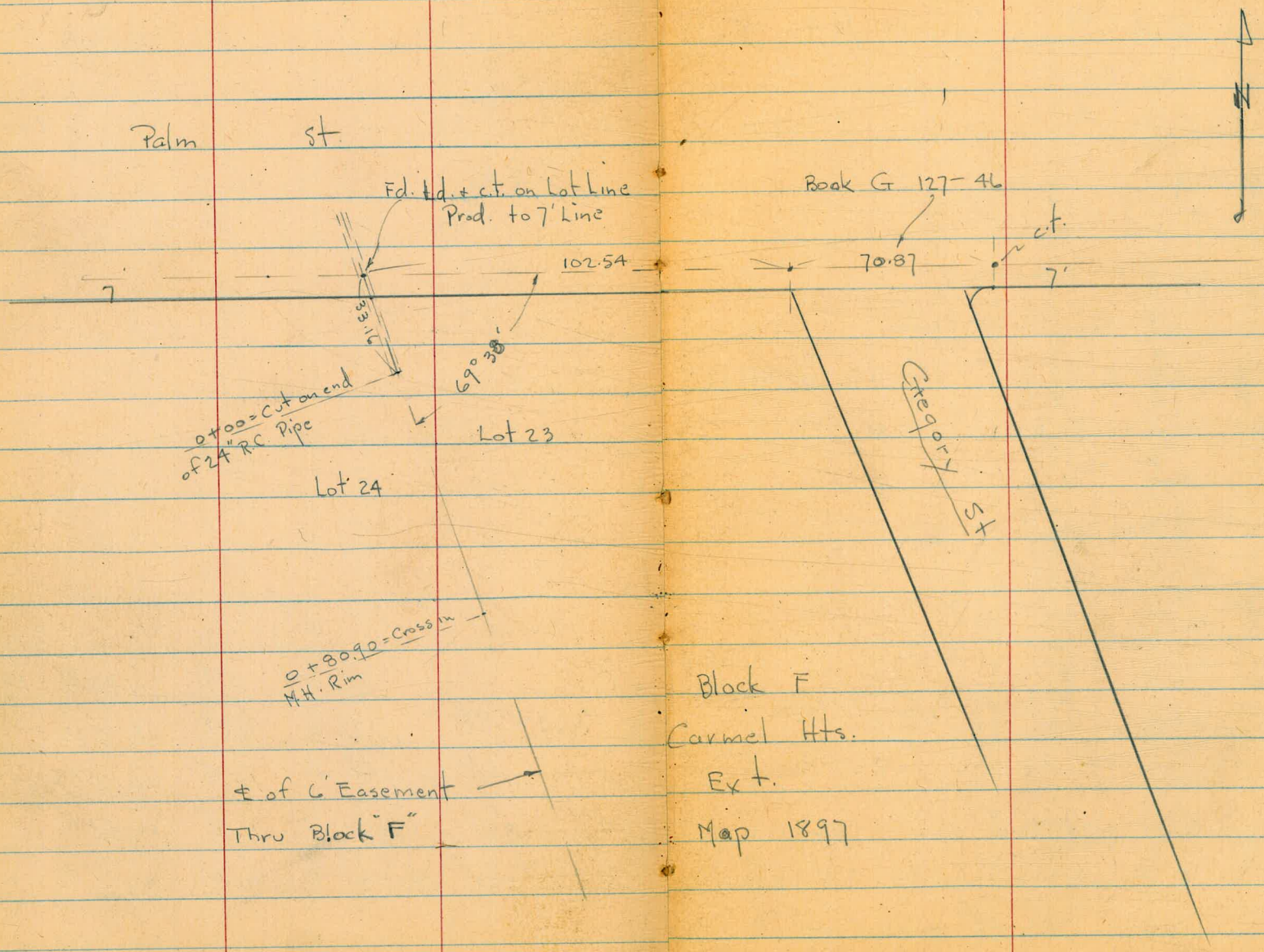
Levels Proposed Sewering of Lots 18 South side Niagra west of Catalina

			Proposed Line			
1450			1 3	162.4		
				156.1		
1400			7 6			
TP 2	11 33	163 66	0 17	152 33		
				152.1		
0470			0 4			
				146.93		
6+32.78 WP on Prop Catalina			5 52			
				145.20		
0421			7 25			
				139.00	144.40	
0400 MH on Catalina			13 45 FL		2.05 rim	
TP 4	4 14	152 45	10 88	148 31		
BM	167	159 92		157 52	NE BP Narragansett Catalina Blvd	

					189.1	190.0 197.0
3445					6 2	5 52 25 +1 40 N Prop
TP 5	11 43	195 88			0 17	184 45
						181.2
2+99.87 = 0400 to North Proposed MH.					3 4	
					176.2	177.6 181.7
2470					8 4	7 0 2 2 30 40 N Prop
TP 4	11 25	184 62			0 57	173 32
					171.6	
2435					2 3	
					168.0	
2400					5 2	
					165.2	169.4
1475					8 7	4 5 40 N Prop
TP 3	11 24	173 94			0 96	162 20

1+90 Dead End		+8 3	204.4	
1+70		6	196.11	
1+40		22	193.9	
0+90		7 5	188.6	
0+40 = North Prop line		12 7	183.4	
0+30		14 5	181.6	
0+00 = Proposed MH to North		14 8	181.3	
BM = TP	11 46	196 11 ✓	184 45	
3+89 Dead End		8 7	198.2	1987 8 2 28 +27 40 N. Prop 209.6
TP	11 30	1206 88 ✓	0 30	195 58 ✓

TP			3 68	148 31 = TP1 148 31 ✓
TP	1 55	151 99 ✓	11 24	150 44 ✓
TP	0 11	161 68 ✓	12 05	161 57 ✓
TP	0 35	173 62 ✓	11 95	173 27 ✓
TP	025	185 32 ✓	11 14	184 97 ✓


Palm St
Fd. Id. + c.t. on Lot Line
Prod. to 7' Line
Book G 127-46
c.t.
102.54
70.87
7'
7
3.3'
69° 38'
0+00 = Cut on end of 24" R.C. Pipe
Lot 23
Lot 24
Gregory St
0+80.90 = Cross in M.H. Rim
Block F
Carmel Hts.
Ext.
Map 1897
℄ of 6' Easement
Thru Block "F"

INDEXED

MAR 26 1951

Drain Survey - along ℄6 Easement
Thru Block "F" - Carmel Hts. Ext.
Sketch - P. 54

5236 3-22-51 7.0.

W.O. 20809

1+00 = along wire fence

0+82 - = ℄ = Cor. Wire fence

0+84 - 2.2' Rt. = ℄ P.pole # None (To be Moved)

0+80.90 = Cross on S. Rim of Sewer M.H.

0+58 - 1.8 Rt. = Dead Man.

0+40

0+00 = outlet of 24" R.C. Pipe

	3.63	288.62✓	11.62	284.99✓
	0.10	296.61✓	9.50	296.51✓ = Nail in Pole
B.M.	0.37	306.01✓		305.64 = S.W. 7' ct. Felton + Palm.

Lt. ℄ Rt. 55

279.8	278.8	276.1	276.7	276.7	281.3
8.8	9.8	12.5	11.9	11.9	7.3
9		2	10	15	25
along Conc. wall		℄ wash			

282.9	279.08	276.8	277.9	282.7
5.7	9.54	11.8	10.7	4.9
10	on Cross	4 ℄ wash	20	30

281.3	278.3	283.4
7.3	10.3	5.2
10	℄ wash	18 - edge of fill.

280.03
8.59
I.E. Pipe

289.62✓

X-Sec. for new curbs
Newport + Abbott.

30-Mar-1951
W.O. 20608

INDEXED

Sommermeyer
Begg
Wierciszewski

▷ = set ¾ hub.

Red line = proposed curb.

Yellow line = existing curb

yellow shade = Conc.

Ⓗ = Fire Hydt.
Ⓢ = Street sign
▲ = Street light
▥ = Catch basin
} Existing

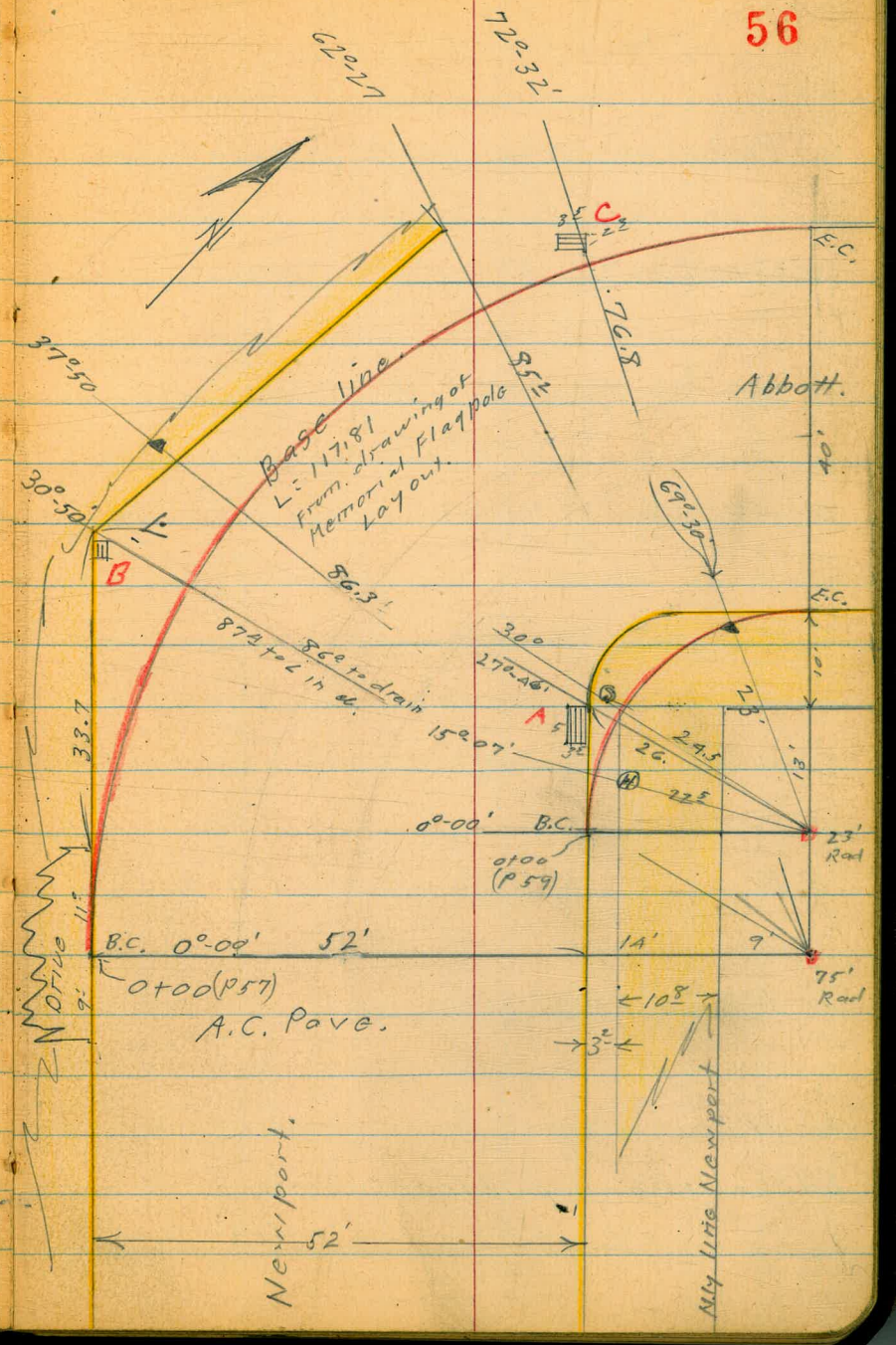
From 23' Ch. Rad.

Location of improvements on Ely. Rot.

0°-00' = parallel to Abbott
15°-07' - 22½ off Rad = ctr. of Fire Hydt.
27°-46' - 26' off Rad = Nly. Cor. 3½ x 5' grate.
30°-00' - 24½ " " = Street sign set in Conc.
69°-30' - 23' " " = Street lamp post. (Not in use)
90° ± = E.C.
Note - 30°- 23' off Rad. = intersect outside edge of Ely + wly Conc. walk.

Location of Imps on wly side off 75' Rad

0°-00' = Parallel to Abbot St.
30°-50' - 87¾ off Rad. = ∠ in curb.
86¾ off Rad. = Nly. Cor. 1½ x 1½ grate
37°-50' - 86¾ off Rad. = Ctr. Steet Lamp. in use.
62°-27' - 85½ off Rad. = End existing Ch.
72°-32' - 76⅝ = E'ly. Cor. - 2½ x 3½ grate



Abbott & Newport Elevations -

Proposed Wly curb = Base line

See sketch - P-56.

0+39.27

0+19.63 Radial (in 6 parts

0+00 = ch. B.C. 75 Rad. (Wly ch).

0-09 Start drive

0-41

0-50

0-100 in drive

0-111

Elevations by direct Fed.

6.50 ✓

6 (117.81 / 19.63

B.L.

6.00 / 112 G — 5.36 / G — 6.02 — 6.50 / 17 — 5.99 / G — 6.56 / 48 ch

6.25 / 2.8 ch — 5.90 / G — 5.94 — 6.61 / 20 — 6.07 / G — 6.60 / 50.8 ch

6.07 / drive — 5.95 / G — 6.80 / 26 — 6.11 / 52 G — 6.64 / 52 ch

6.56 / ch — 6.02 / G

6.91 / ch — 6.31 / G — 7.16 / 26 — 6.41 / 52 G — 7.05 / 52 ch

6.48 / Drive — 6.37 / G

6.91 / Drive — 6.80 / G — 7.57 / 26 — 6.77 / 52 G — 7.37 / 52 ch

7.54 / ch — 6.87 / G

= Base El. = N.E.B.P. Abbott & Newport.

Catch basin C P-56

Catch basin B P-56

Catch basin A P-56

4 in curb. (P-56) @ 30°-50' from 75' Rad.

1+17.81 E.C. 75' Rad ℄ Also 40' Rt = E.C. 23' Rad ℄

0+98.17

0+83.8± = end of wly. curb.

0+78.54

0+58.90

BL

5.02 Grate 2.92 I.E.

5.41 Grate 3.70 I.E.

5.74 Grate 5.10 I.E. east end 4.04 I.E. west end 6.50 Grate

C.11 12" ℄ ℄ BL. 5.34 12" G ℄ BL.

5.00 G 6.05 20 5.82 G 6.40 40 ℄

No ℄ 5.104 3 G 5.23 6.08 20 6.05 G 6.44 ℄

5.73 10± ℄ 5.30 G

5.79 9± ℄ 5.35 G 5.72 6.11 17 6.126 G 6.55 37± ℄

5.94 8± ℄ 5.55 G 5.85 6.39 17 6.25 on grate 6.50 41± ℄

Levels along proposed ℄ curb line.
Ely. Rot. - Abbott & Newport.

0+00 = B.C. 23' Rad curb. (P-56)

1+36.13 (100' Nly. proposed ℄ E.C. on Abbott)

0+86.13 (50' Nly. prop. ℄ E.C. on Abbott)

0+36.13 E.C. 23' ℄ Rad

Δ 30°-00' = Intersect S.wly. walk edge

0°-00' proposed. (P-56)
0+00 = B.C. 23' ℄ Rad (Ely ℄ Rot)

Radial ∠ from 23' Rad.
0°-00' = parallel to Abbott St

B.L.

5.75 / 20 — 5.43 / G — 6.05 / ℄

5.90 / 20 — 5.60 / G — 6.24 / ℄

5.82 / G — 6.39 / ℄

6.60

6.02 / G — 6.57 / ℄ B.C.

Curb + Gutter levels

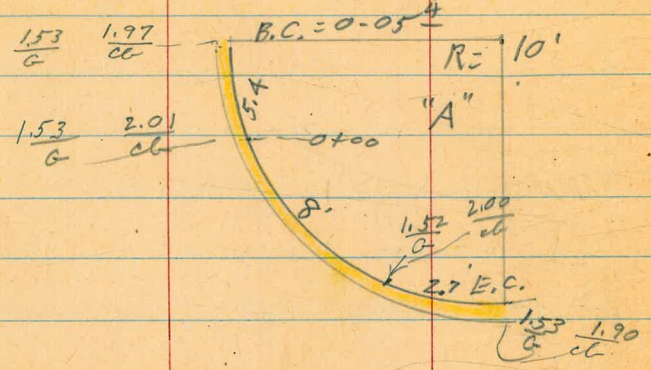
Kurtz + Riley

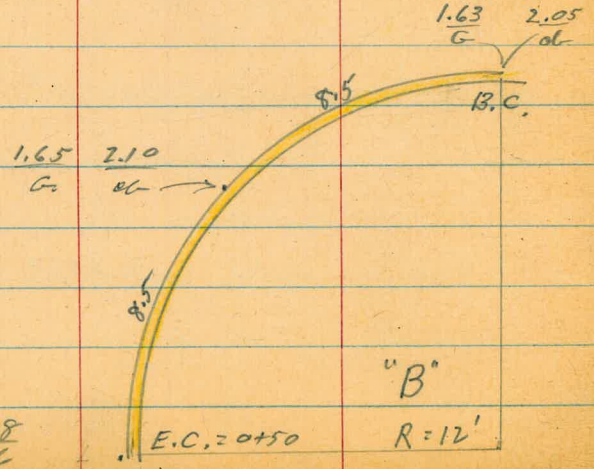
30-Apr. '51.

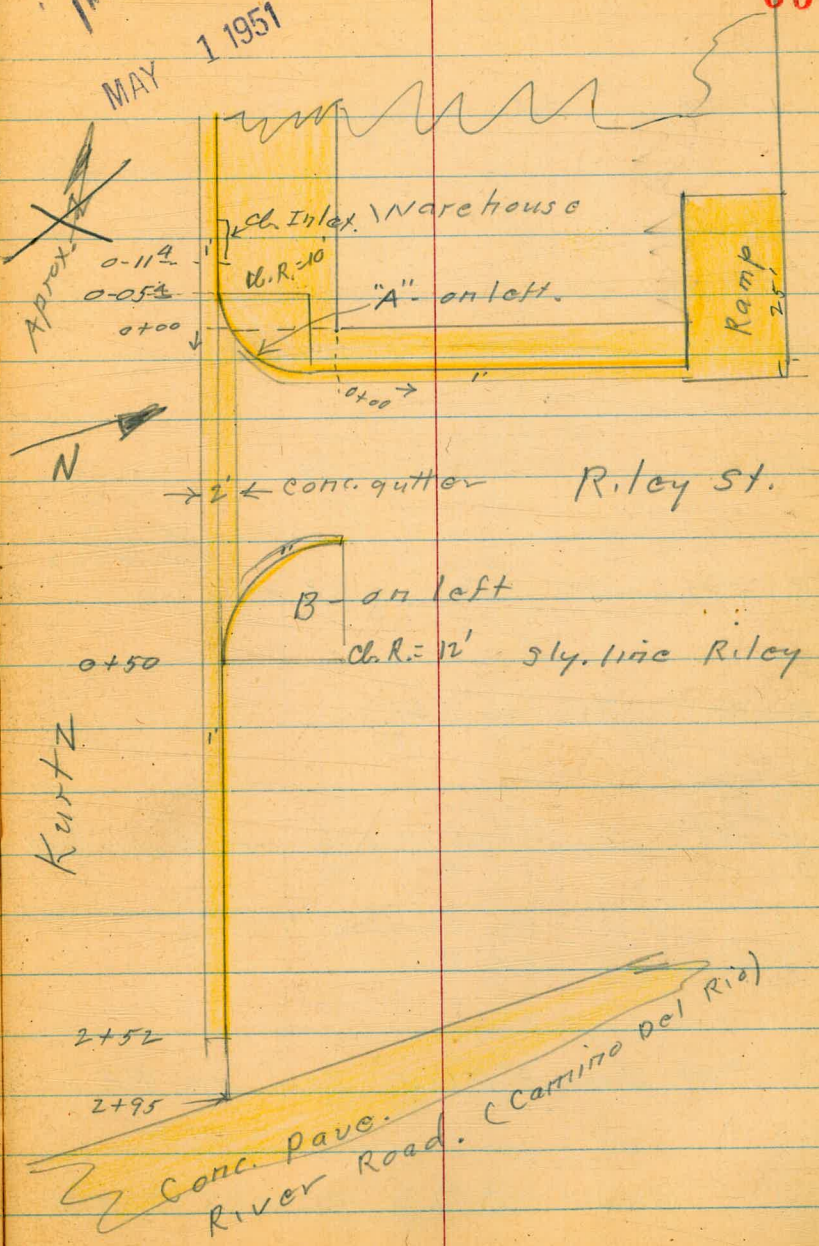
Sommermeyer
Begg.

SURVEYED
MAY 1 1951

60







Kurtz
N.Ely. ch. + gutter

1+50

1+00

0+50 = E.C. 12' Rad ch. Rot.

℄ Riley
0+25 1% Conc. gutter

0+00 1% Conc. gutter

0-05.4 = B.C. ch. Rot.

0-11.4 = Sly end curb inlet throat

B.L. = Ely ch. line Kurtz
0+00 = Nly line Riley

Set direct Elev. rod on T.P.

T.P.		4.74	2.37
4.14	7.11	—	2.97

2.18 ch. 1.75 G

2.13 ch. 1.71 G

2.08 ch. 1.66 G

1.77 ch. 1.55

12' Lt. ch. = edge Pave.
= ℄ Riley
+ N.Ely. Kurtz

1.52 G

1.97 ch. 1.53 G

1.95 ch. 1.43 G

Wly B.P. Kurtz + Rosecrans

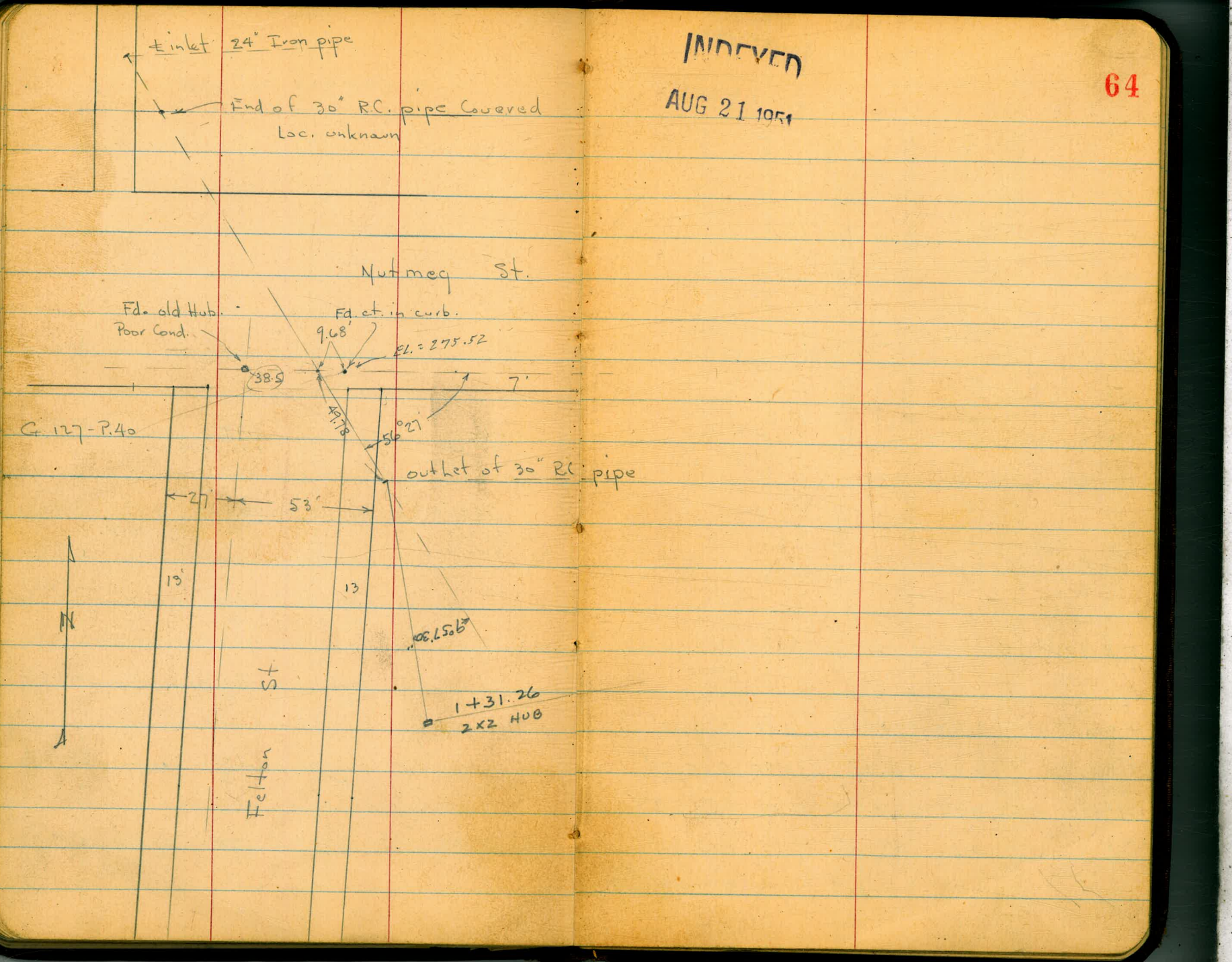
Kurtz

Camino Del Rio

2+95	ot S. wly edge Conc. Pave.	4.10	
2+80	On A.C. Pave	3.96	
2+60	on A.C. Pave	3.34	
2+52 = end conc. ch		2.97 ch.	2.90 G
2+47		3.28 ch	2.87 G
2+00		2.51 Ch	2.07 G

Riley St.
s.wly. cb. + gutter

1+50	3.12 25' Lt on ramp	2.49 End of ramp.
1+20.5 End of curb - start ramp	3.08 25' Lt on Ramp	2.22 G - start ramp.
1+15.5	2.69 cb	2.20 G
1+00	2.62 cb	2.11 G
0+50	2.34 cb	1.87 G
0+00 = NEly line Kurtz (See sketch)	1.75 cb	1.56 G.



1+00

0+80

4° Lt. = Ctr. 10" Diam Willow
0+77 2° Lt. = Ctr. 15" Diam Willow

0+75 +r

~~0+75~~

0+50.

0+49 78 = end existing 30" Conc. pipe

T.P. top of Pipe.	1.98	256.31 ✓	12.63	254.33 ✓	
T.P.	0.74	266.96 ✓	12.76	266.22 ✓	
Set B.M. #1	3.46	278.98 ✓	11.63	275.52 ✓	S.E. 7'x13' Lt. Nutmeg + Felton (SEE P.64)
T.P.	0.21	287.15 ✓	13.23	286.94 ✓	
	6.09	300.17 ✓	-	294.08 N.E. B.P.	Nutmeg + Bancroft.

250.8
5.5
10

248.3
8.0
5

246.6
9.7
4

249.0
9.3

249.7
6.6
1

253.3
3.0
6

253.0
3.3
10

250.0
6.3
6

249.5
6.8

250.7
5.6
2

253.1
3.2
7

256.1
1.2
14

251.8
4.5
9

251.0
5.3

251.3
5.0
2

253.8
2.5
10

256.3
0.0
10

253.2
3.1
4

252.8
3.5

253.6
2.7
5

256.3
0.0
10

251.37
4.94
I.E

256.31 ✓

Orig. B.M.		A.A3	294.10 ✓	294.08	
T.P.	12.42	298.53 ✓	1.15	286.11 ✓	
T.P.	11.75	287.26 ✓	3.33	275.51 ✓	275.52
T.P.	12.20	278.84 ✓	0.95	266.64 ✓	
T.P.	11.52	267.59 ✓	0.24	256.07 ✓	

B.M. #1 - P. 65

Reduced by CRL 9-14-51

1+45

1+37

1+31 26 2/2 hub. in ctr. of wash

1+26

1+21

1+03

297.6 — 8.7 — 246.7 (9.6, 5) — 244.5 (11.8, 8) ± wash

295.3 — 11.0

299.8 — 7.9, 9 — 246.8 (9.5, 4) — 245.6 (10.7, 15)

299.8 — 11.13 — 245.1 (11.2, 12) — 246.5 (9.8, 3) — 248.7 (7.6, 8)

299.1 — 7.2, 11 — 246.8 (9.5, 6) — 245.4 (10.9, 4)

245.9 — 10.4 — 247.8 (8.5, 3) — 249.3 (7.0, 8)

299.1 — 7.2, 13 — 297.1 (9.2, 8) — 245.7 (10.6, 6) — 245.9 (10.4, 2)

298.3 — 8.0

299.0 — 7.3

251.1 — 5.2, 15 — 298.3 (8.0, 8) — 246.5 (9.8, 6) — 246.5 (9.8, 3) — 252.1 (4.2, 5)

256.31 ↓

Continued from P. 33
sketch - Page 30

12+00

211.65
2.60

11+50

207.19
7.06

T.P. 8.74 (214.25) 2.62 (205.51)
of pipe
Δ 77°-50' to left. = line

(214.25)

11+31 $\frac{83}{}$ = cross 36" culvert

199.97 | 206.08 | 205.18 | 205.51 | 204.49 | 205.43 | 196.18
8.16 | 2.05 | 2.95 | 2.62 | 3.64 | 2.70 | 11.95
24 | 16 | 16 | | 14 | 14 | 27
I.E. intake | ob | grate | | Grate | ob | I.E. outlet

11+24 $\frac{63}{}$ (page 30)

204.96
3.17

3.18 (208.13) — (204.95)

11+25 $\frac{52}{}$ Page 38

(208.13)

T.P. 5.76 ⟨219.22⟩ 9.26 ⟨204.46⟩

12+00 8' Lt. = start post & wire fence.

11+93

11+89 12 = cross curb

11+89+ = gutter also end of pave.

11+73 12 from page 30

8.77 ⟨213.72⟩ — ⟨204.95⟩

206.1 206.3 206.2
7.3 7.4 7.5
5 5

209.0 209.3 209.6
4.7 4.4 4.1
5 5

208.77 209.31 209.81
4.95 4.41 3.85
5 5

208.55 209.05 209.59
5.17 4.67 4.13
5 5

208.78 209.28 209.78
4.94 4.44 4.94
5 5

⟨213.72⟩

11+25 52 page 38 = 13.72

13+44 66 { = cross line lot #
= ½ + Disk P.O.T.
11' Lt. = Δ Lt. in fence.

13+33 06 ½ P.O.T. 3.64

13+33 - 41' Lt. = 30" Eucalyptus. Near side of

13+10 24' Lt. = S.wly. Cor. house

T.P. 8.25 ⟨216.45⟩ 2.02 ⟨208.20⟩

12+65 57' Lt. = N.wly. Cor. house

12+50.

12+05

℄

213.6 213.39 214.2
2.8 3.06 2.12
5 5

211. 210.8 210.3 210.2 209.5
5.12 5.16 6.1 6.12 6.9
24 5 5 35

⟨216.45⟩

207.4 206.5
2.8 3.7
5 7

205.7 205.8 206.0
4.5 4.4 4.2
5 5

202.8 204.3 204.9 204.9 208.
7.4 5.9 5.3 5.3 2.0
30 5 5 15

⟨210.22⟩

T.P. 6.04 (225.50) 3.20 (219.46)
1A+50

1A+33 97 = Cross line Lot # 60.
on ℄ 3.05 (219.61)
20' Lt. = line of fence.
1A+28 96 = Δ 18°-04' Lt. = ℄ + dist

1A+26 - 7' Lt. = Eucalyptus.
Near Side 20"
1A+11 5 7' Lt. = Near Side of 30" Eucalyptus

1A+00 15 5' Lt. = line of fence.

T.B.M. #1
13+59 66 8.74 (213.92)

13+45

T.P. 9.27 (222.66) 3.06 (213.39)

℄

218.1 218.7 219.5
4.6 4.0 3.2
5 5

219.1 219.61 219.8
3.6 3.05 2.9
5 ℄ 5

211.7 215.1 216.7 216.9 217.4
11.0 7.6 6.0 5.8 5.3
35 15 5 5

213.8 213.9 214.3
8.9 8.74 8.4
5 5

213.9 213.6 213.5 212.3 214.6
8.8 9.1 9.2 10.4 8.1
5 5 25 50

(222.66)

Sta. 15+33.17 ±
Mon. - 4.33 Lt. of 15+33.17 = ½" dish P.O.T. 4.57 (220.93)

15+22

15+00

14+91 6' Lt. = end fence.

14+80

14+63 14' Lt. = 36" Eucalyptus
Near side

14+51 11.5 Rt. = 36" Eucalyptus.

(225.50)

218.3
7.2
15

221.10
3.80

222.6
2.9
5

214.5
11.0
15

217.0
8.5
3

218.7
6.8
2

219.2
6.3

220.5
5.0
5

210.3
15.2
50

215.4
10.1
5

216.2
9.3

217.4
8.1
5

216.3
9.2
6

216.4
9.1

216.5
9.0
5

216.7
8.8

217.3
8.2
5

(225.50)

+	HI	-	Elev.
8.26	207.81	291	204.91
3.17	209.09	954	199.55
1.22	214.79	8.87	205.92
	XXXX	11.93	213.57

15+50 end of line

15+34 = Cross rail force

{225.50}

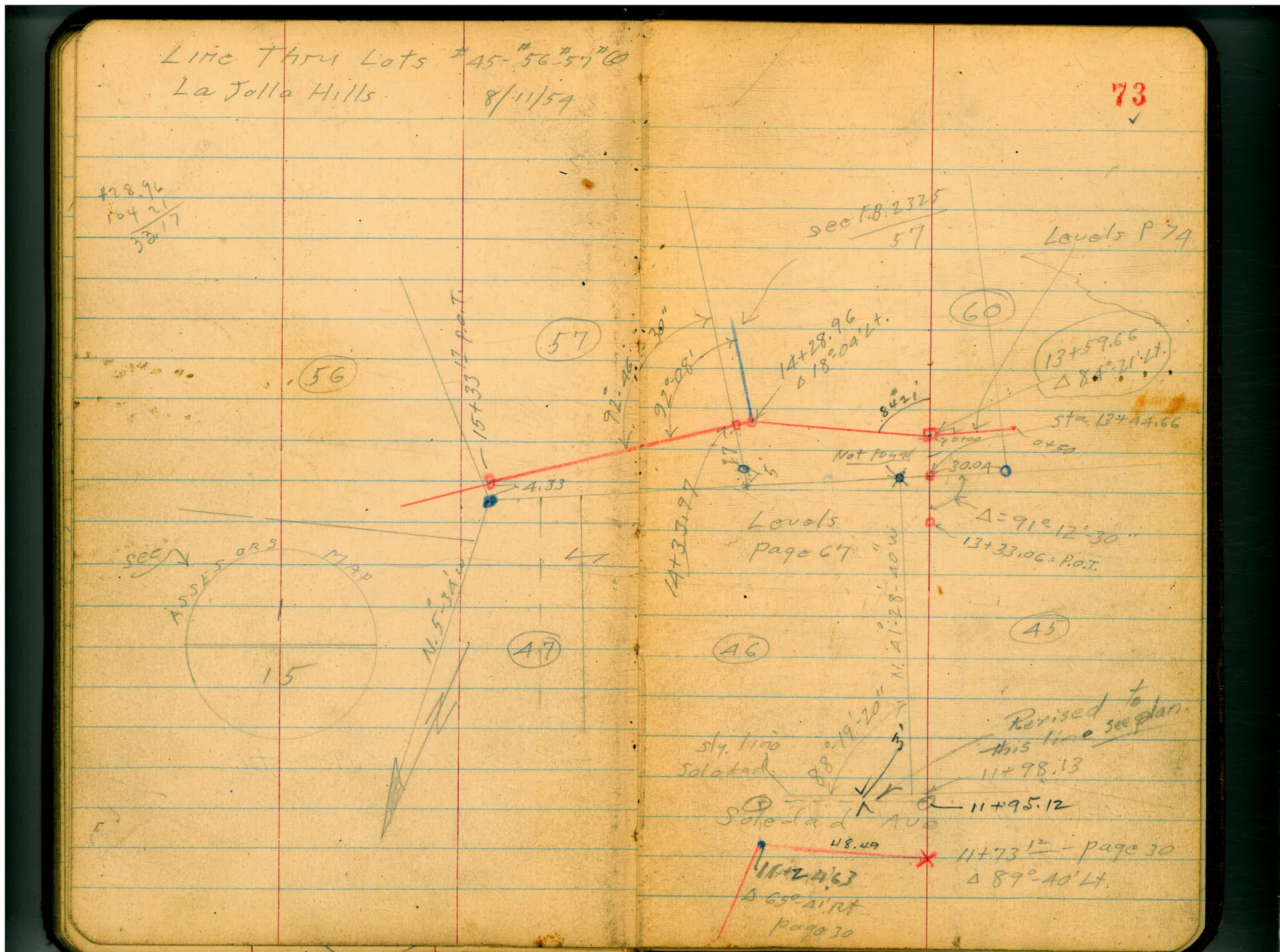
224.2 ✓ 225.4 ✓ 226.8 ✓

1.3 0.1 +1.3

5 5

{225.50}

Line Thru Lots #45-#56-#57 #60
La Jolla Hills 8/11/54



Thru. Por. of Lot #60

#1 - Elev

0 +50

216.6
5.7
5

215.5
6.8

214.5
7.8

0 +20

214.3
8.0
5

213.4
8.9

212.6
9.7
5

213.9
8.4

0+00 = (13+59.66 page 73)
8.40 (222.32)

(222.32)

– 213.92

T.B.M. #1 - P-70 (℄ 13+59.66)

Additional Elevations
for line on Page 30.38
9-23-54

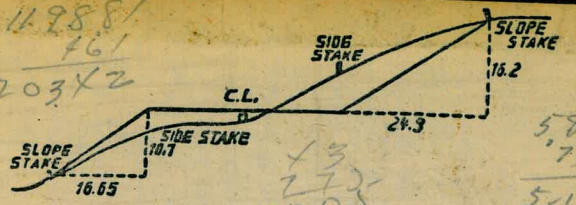
11+50.12 Page 30 Plan

202.7
4.5

11+42

204.9
2.3
(207.16)

2.21 (207.16) (204.95) 11+25.52 Page 36



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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