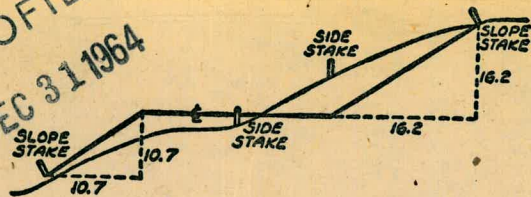


2033

WASH BUCK

MICROFILMED
DEC 31 1964



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

INDEXED

to page #60

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.887	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

P

Edwards St Tennis Court 1-5
 Gibbs Airport-Road 6-16
 Gibbs " Sewer Ditch 20-24
 Upsher St 16-19
 X-Sec. Jewell - Fortuna to Pac. B. Dr. 43-49

D. Smith
 W. Moore
 J. Clark
 F. Acuna

Profile levels for tennis court

BK 20 Draper + Kline St.

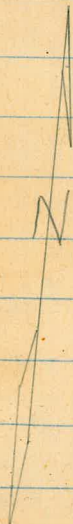
LA JOLLA PARK

20466-71-11
 W0# 60367
 5-26-49
 1

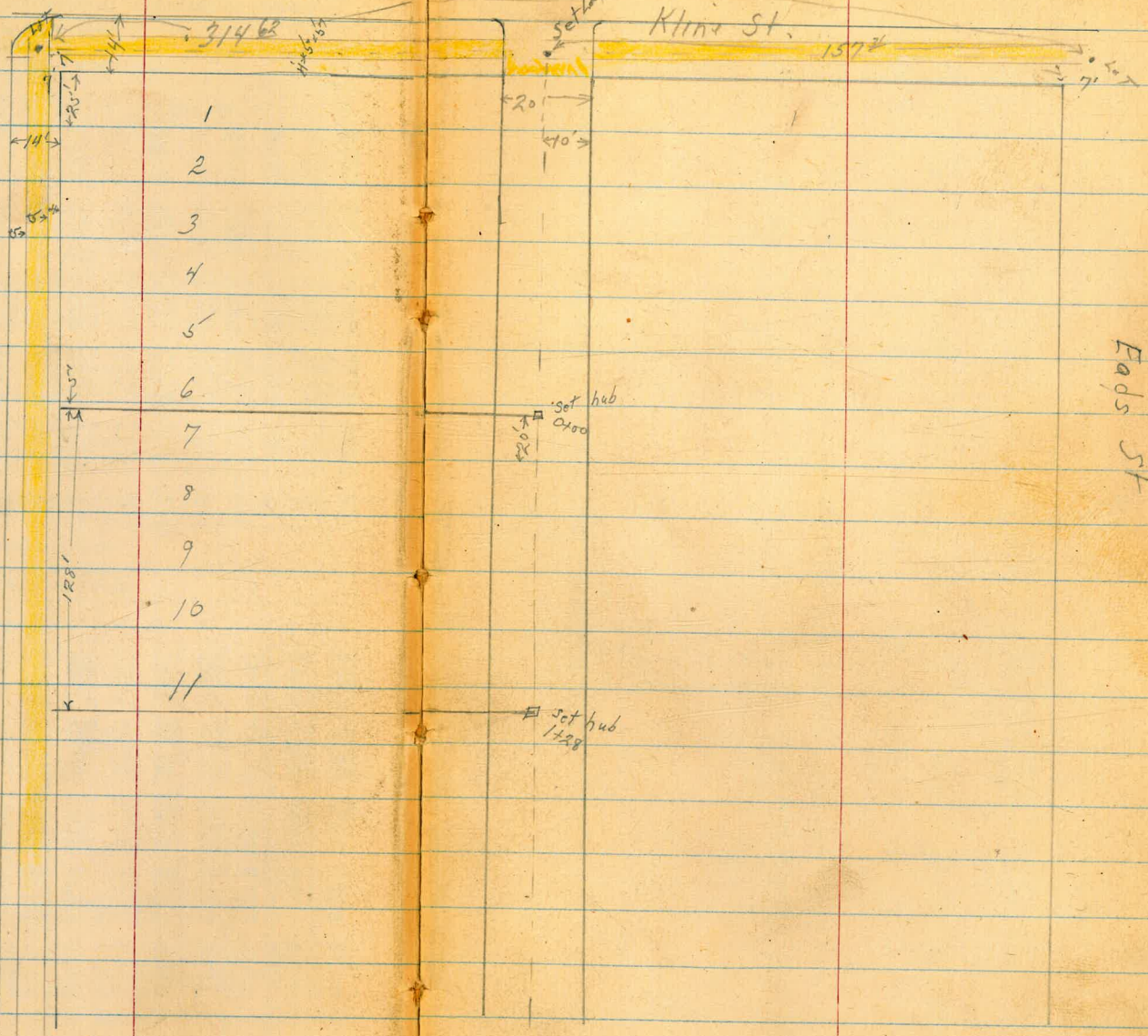
INDEXED

WK

MAY 31 1949



(See Field Book G 206 - 53 levels 2/10-44)



concrete

Profile Levels of Tennis court

Area BK 20, Kline + Draper St.
LA JOLLA PARK

	Alley 5'	10' AT	25' AT West	50' AT	75' AT	100' AT	125' AT	Prop Draper 150' AT	164' AT Draper Top curb	164' AT Draper Gutter		
1428 South end courts	72.6 112	72.6 112	71.9 71	71.3 72	71.5 72	71.3 72	71.0 80	71.7 82	71.5 112 153	71.92 12 OF	71.38 12 62	2
1400	72.3 112	73.0 104	71.1 62	71.6 74	71.8 75	71.1 72	71.0 80	71.6 84	73.2 108 153	73.03 10 97	72.35 11 65	
1475	71.8 92	71.6 88	71.2 68	71.8 72	71.5 75	71.2 78	71.9 81	71.8 82	71.4 98 153	71.23 9 77	73.54 10 46	
1450	71.0 60	71.3 62	71.1 62	71.9 71	71.6 74	71.4 70	71.2 78	71.2 78	71.4 86 153	71.38 8 62	71.77 9 23	
1425	71.1 52	71.4 58	71.3 62	71.9 71	71.7 73	71.6 74	71.5 75	71.6 74	71.6 74	71.63 7 37	71.12 7 88	
1408	71.0 50		71.6 64	71.3 62	71.2 68	71.7 73	71.0 70	71.4 68	71.7 623	71.77 6 23	71.12 6 88	
North prop 1410 of courts	71.5 45		80.5 35	80.4 36	80.3 32	79.9 41	79.5 45	78.7 53	78.20 5 80	77.56 6 44		
TP	456	82.99 ✓	1301 on hub 2' ally	79 43 ✓								
BM	640	92.44 ✓		86.04 ✓	SEBP Kline + Draper							

Coburn 5-31-49

Note. See G-206/53

Additional Notes & Levels
 Lt = East & Alley

June 3 1949

3

Rt = West

0478 9° Lt & Tel Pole # 897744

72.9 13.0
 11.2 10.2 ✓
 20 10

0475

71.9 16.0
 6.2 5.9
 20 10

0450

0446 9° Lt End 4' Picket Fence

71.9 16.2
 6.0 5.3
 15 10

0425

72.6 19.2
 5.3 4.2
 20 10

0400

0-5 10° Lt Begin 4' Picket Fence

0-07 8° Lt & Tel Pole # 4140764

79.9 80.2 80.6 80.9 81.1
 4.2 3.2 3.3 3.0 2.8
 10 10 25 50

81.0

2.3
 7.5

80.9

3.0
 10.0

80.3

3.5
 12.5

79.7

4.2
 15.0

78.78

5.4
 16.4
 carb

78.16

5.93
 9.77

0-12

TP

446

8389

7943 ✓

Hub & Alley + North
 Prop line Lots

East Lt \oplus

1760 H. on line End temporary shed

Lt. on Line Begin temporary shed,

1753 3rd Lt end wing of House

1745	77.4	77.4	77.3	76.7	76.4
	65	65	66	73	75
	3		10	25	50

RT = West

76.3	76.3	76.0	75.7	72.1	71.63	71.04
76	76	72	82	11E	1226	1285
75	100	125	150	153	164	164
					carb	94th

1745 3rd Lt Begin closet wing of Calif House

1728	72.1
	118
	7

1720 7th Lt to base structure of House
2nd Lt. begin overhang porch

1707 10th Lt & Power Pole # A7605

1700	72.1
	118
	7

0796 7th Lt to base structure
5th Lt NW cor overhang of Calif House

83 89 ✓

Lt = East

E

Rt = West

1785

15.8	13.5	12.3	11.8	11.0	16.5	15.5	15.5	15.5	71.3
8L	104	116	12L	122	74	84	84	84	125
10		10	23	50	65	100	125	140	150

1770

16.8	16.6	15.9	15.8	16.0	16.1	15.9	15.9	14.4	71.7
7L	73	82	81	72	78	82	82	95	125
10		10	25	50	75	100	125	140	150

83 89 ✓

Walker
Boggs
Shawmon
Richard
8-30-49

Gibbs Airport

Location - Proposed Road

6+16.97 = E.C.

INDEXED

W.K.
DEC 22 1949

$\Delta = 35^{\circ}21'$
 $L = 616.97$
 $R = 1000'$
 $T = 318.66$

State
3M 398.62
4A

0+00 = BC Proposed Road

P.O.T. 6+43.59

6+16.97

E.C. R.P. #100

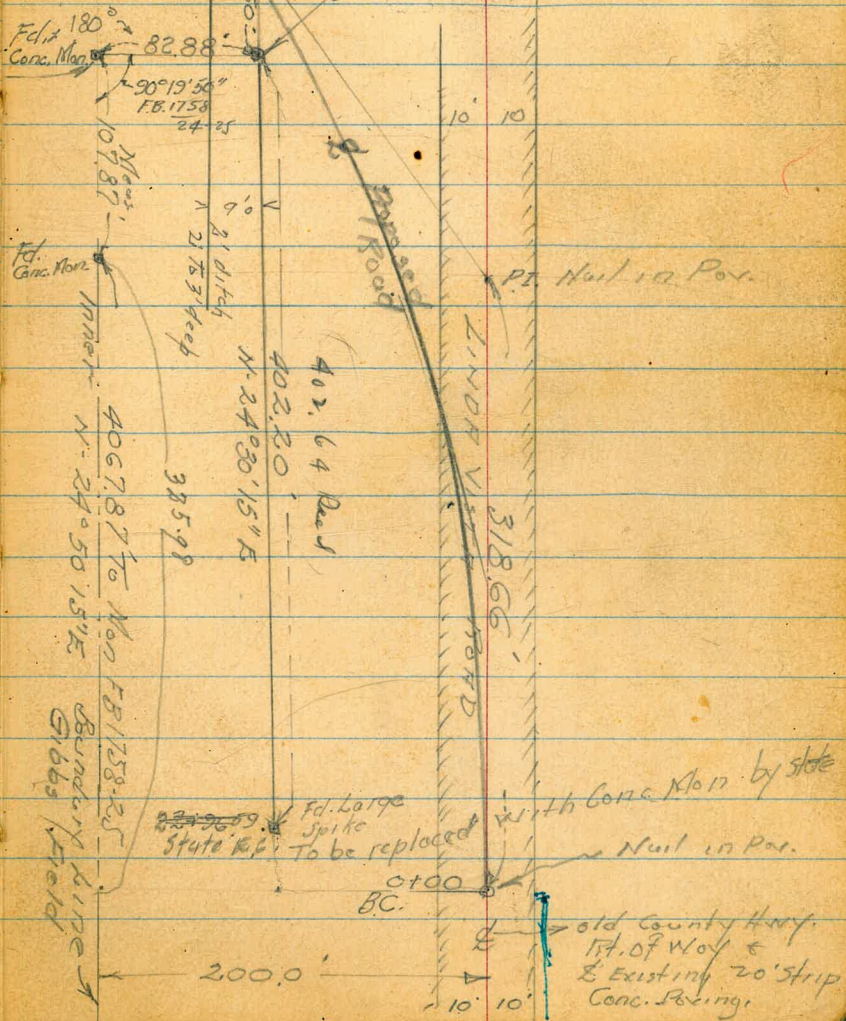
Set 2 "x 2"

Fd. 180° Conc. Mon. 82.88'

Fd. Conc. Mon.

Inner - N. 24° 50' 15" E

Boundary Line of Gibbs Field



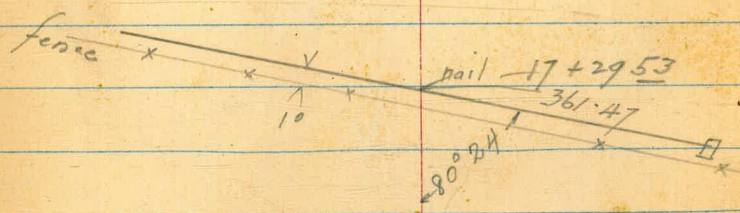
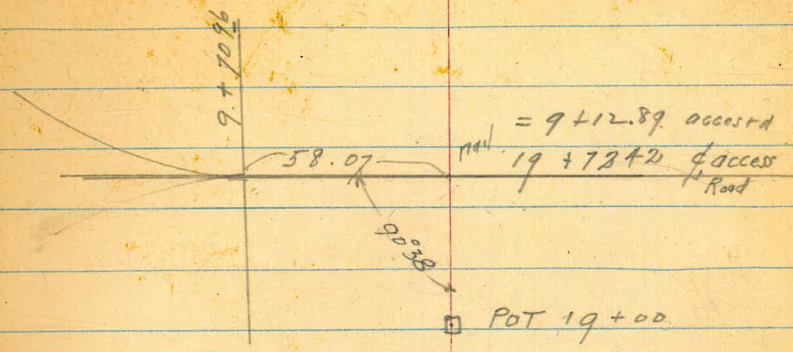
22+96.59 = state station
Fid. State Mon.

10' 10' strip

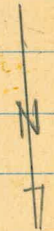
old County Hwy.
1st. of Way &
Existing 20' strip
Conc. Paving.

Sta	Def
6+16.92	17° 40' 30
6	17° 11' 30
5	14° 19' 30
4	11° 27' 30
3	8° 36' 00
2	5° 44
1	2° 52
0+00	0° 00

See p 6



Proposed Rd



Gibb Airport

X Sections

Proposed Road

8

Begg
Sherman +
Sision

41

1 + 00

0 + 50

0 + 0 BC

Redwood
9.14.49
Kenny Jr

NOTE: All
elevations are
to U.S.G.S. staff
6.12 above City datum

5.78404.40

398.62

state BM 61.

256 392.52

6.58 395.08 1.02 388.50

BM. — +8.67 389.52 380.85

16 + 18 —

state BM 386.97
6.12

~~393.28~~
~~399.40~~
5.00
15

393.63
~~399.75~~
4.65
15

393.58
~~399.70~~
4.70
15

392.95
~~400.07~~
4.33
15

394.25
~~400.37~~
4.03
13.75

394.12
~~400.54~~
3.96
15

394.11
~~400.23~~
4.17
15

394.71
~~400.83~~
3.57
15

395.11
~~401.23~~
3.17
15

394.42
~~400.54~~
3.86
15

404.40

A 26 + 35 chis sq. Head Wall opp 1 + 00 Proposed Road

398.62 state BM

~~392.52~~
6.12

BM Hd Wall

A 16 + 18

state BM on Head Wall left side Road they say
380 + 85 is now covered up

4+00

398.0 404.1	390.5 396.6	389.9 396.0	389.3 395.4	390.4 396.5	391.8 398.9
0.3	7.8	8.4	9.0	7.9	5.5
41	31		11	25	44

3+50

391.6 397.1	390.8 396.9	389.8 395.9	390.3 396.4	391.5 397.6	392.8 398.9	389.9 396.0
6.7	7.5	8.5	8.0	6.8	5.5	8.4
40	20	7		15	28	33
						9

3+00

391.5 397.6	390.3 396.4	391.8 397.9	392.9 399.0	390.4 396.5	390.93 397.05
6.8	8.0	6.5	5.4	7.9	7.35
35	23		10	15	25
					9

2+50

391.7 397.8	392.3 398.4	391.92 398.04	391.08 397.20	391.78 397.90
6.6	5.0	6.36	7.20	6.50
25	3		2	15

2+00

393.7 399.8	394.0 400.1	391.70 397.82	392.17 398.29	392.48 398.60
4.6	4.9	6.58	6.11	5.80
20	13	7		15

1+50

392.68 398.80	392.96 399.08	392.98 399.10
5.60	5.32	5.30
15		15

404.40

6 1697 EC

6 + 00

5 + 50

5 + 00

4.83 405.10

4 + 89

4 + 55

4.13 400.27

404.40

T.P.

400.0	399.5	399.0	398.6	398.2	10
5.1 50	5.6 25	6.1	6.5 25	6.9 50	
399.6	399.3	398.7	398.4	398.2	
5.3 50	5.8 25	6.4	6.7 25	6.9 50	
393.0	392.6	392.2	392.6	392.6	
399.1	398.7	398.4	398.7	398.2	
6.0 50	6.4 25	6.7	6.4 20	9.8 39	53

394.3	394.5	394.1	394.7	394.0	389.5
400.4	400.6	400.2	400.8	396.1	385.6
4.7 50	4.5 25	4.9	4.3 10	9.0 24	9.5 40

395.3	394.6	405.10	394.9	390.2	389.6	387.5
401.4	400.7	397.6	401.0	396.3	395.7	394.6
3.0 40	3.7 20	3.7	3.4 3	8.1 17	8.7 30	9.8 50
396.6	396.6	390.7	388.7			
402.7	402.7	396.8	394.8			
1.7 30	1.7 16	7.6	9.6 33			
		404.40				

9 + 00

8 + 50

8 + 00

7 + 50

7 + 00

7.21 406.26 6.05 399.05

6 + 50

405.10

399.5	399.6	399.1	398.7	397.9 11
6.8	6.7	7.2	7.6	8.4
50	25		25	50

399.0	398.8	398.6	398.2	397.6
7.3	7.5	7.7	8.1	8.7
50	25		25	50

400.9	401.1	400.9	399.9	399.2
5.4	5.2	5.4	6.4	7.1
50	25		25	50

401.5	401.9	401.7	400.8	400.1
4.8	4.4	4.6	5.5	6.2
50	25		25	50

401.7	401.4	400.8	400.0	399.5
4.6	4.9	5.5	6.3	6.8
50	25		25	50

TPonEC.

406.26

400.9	400.5	400.1	399.4	399.0
4.2	4.6	5.0	5.7	6.1
50	25		25	50

405.10

397.9	397.5	397.1	396.8	396.3
6.6	7.0	7.4	7.7	8.2
50	25		25	50

397.0	396.4	395.8	395.6	395.2
7.5	8.1	8.7	8.9	9.3
50	25		25	50

397.5	397.1	396.7	396.6	396.8
7.0	7.4	7.8	7.9	7.7
50	25		25	50

398.4	398.2	398.3	398.2	398.3
6.1	6.3	6.2	6.3	6.2
50	25		25	50

602 404.54774 398.52 TP

404.54

400.3	400.4	400.5	400.2	399.5
6.0	5.9	5.8	6.1	6.8
50	25		25	50

401.7	401.5	401.0	400.1	399.3
4.6	4.8	5.3	6.2	7.0
50	25		25	50

406.26

406.26

12

11 + 50

11

10 + 50

10

9 + 50

15 + 50

7.97 404.42 8.09 396.45 TP

15

14 + 50

14 + 00

13 + 50

13

12 + 50

404.54

406.26

50

25

25

50

397.7

397.4

398.1

397.3

397.4

13

6.7

7.0

6.3

7.1

7.0

404.42

398.0

397.2

397.9

397.3

396.4

6.5

7.3

6.6

7.2

8.1

397.0

397.1

397.3

396.6

397.2

7.5

7.4

7.2

7.9

7.3

397.8

397.1

397.1

396.5

396.2

6.7

7.4

7.4

8.0

8.3

397.9

397.9

397.5

397.0

396.8

6.6

6.6

7.0

7.5

7.7

398.5

398.0

397.7

397.1

396.9

6.0

6.5

6.8

7.4

7.6

398.5

398.1

397.6

397.0

396.3

6.0

6.4

6.9

7.5

8.2

50

25

25

50

406.26

404.54

18+50

18+00

17.50

2.14 404.90 1.66 402.76 TP

17

16+50

16

404.42

50 25

25 50 **14**

399.9 399.4 398.9 399.4 399.7
5.0 5.5 6.0 5.5 5.2

399.2 399.1 398.6 398.9 399.4
5.7 5.8 6.3 6.0 5.5

399.2 399.0 398.3 398.5 399.0
5.7 5.9 6.6 6.4 5.9

fence see map
404.90

398.4 398.3 397.6 397.3 397.3
6.0 6.1 6.8 7.1 7.1

398.6 398.3 397.2 397.9 397.2
5.8 6.1 6.2 6.5 7.2

398.3 398.4 397.7 397.7 396.9
6.1 6.0 6.7 6.7 7.5
5.0 2.5 404.42 2.5 3.0

395.36
392.36
399.15
395.9

No check
395.36 Equal El. before grading
Just happens to hit because of
6.12' diff. in S.M.'s

19 72 40 ♀ Access Road

395.9	394.2	393.5	392.9	392.2	391.1
9.0	10.7	11.4	12.0	12.7	13.8
58	25		25	50	100

19 52 40 Shoulder of Road

396.1	393.6	393.8	393.2	392.6	391.9	390.4
8.8	11.3	11.1	11.7	12.3	13.0	14.5
100	50	25		25	50	100

19 149 ♀ of Ditch

391.9
13.0

19 144

397.0	395.4	394.6	393.7	393.3	392.7	391.2
7.9	9.5	10.3	11.2	11.6	12.2	13.7
100	50	25		25	50	100

19 10 Hub

400.0	399.2	398.7	398.04	397.3	396.8	395.3
4.9	5.7	6.2	6.86	7.6	8.1	9.6
100	50	25		25	50	100

18 180 Top of cut

402.2	401.2	400.0	400.2	399.9	399.9	398.8
2.7	3.7	4.9	4.7	5.0	5.0	6.4
100	50	25		25	50	100

404.42
404.90

Hendricks
Johnson
Greer
Cota
12-9-49
W.O. #31498

X-section Upshur St.
Rosecrans to Termination

16

7333

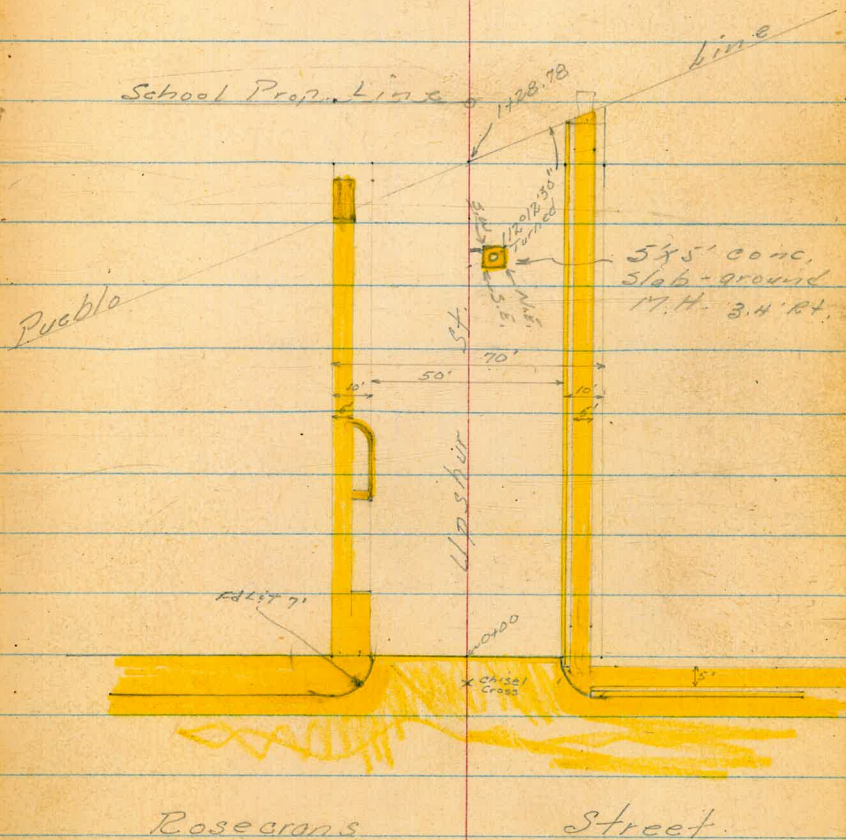
INDEXED
W.K.
DEC 22 1949

1+44.02 = Int. of Upshur & School Prop.

1+28.78 = Int. of Upshur & Pueblo Lot Line

1+01.7 = 5'x5' Conc. slab ground M.H.

0+00 = West Prop. Line Rosecrans & Upshur



Upshur Street
Cont.

Left

R

Right 17

0+00

19 40	19 41	19 49	19 51	19 50	19 51	19 54
869	908	880	871	880	904	861
25	25	125		125	25	25
cb	G			cb	G	cb

T.P. 8.01 28.29 9.01 20.28

28.29

N.W. Cb Return

19 47	19 56	19 59	19 54	19 20	19 52	19 24	19 57
10 10	9 23	10 10	9 55	10 29	9 57	10 25	9 52
G	cb	G	cb	G	cb	G	cb
BC Rosecrans		#1		#2		E.C. Upshur	

S.W. Cb Return

19 18	19 44	19 21	19 53	19 21	19 27	19 51	19 51
10 12	9 81	10 28	9 26	10 28	9 22	10 26	9 58
G	cb	G	cb	G	cb	G	cb
BC Rosecrans		#1		#2		E.C. Upshur St	

0-10 = Whately Cb Line Rosecrans

19 34	19 44	19 48	19 17	19 17	19 30	19 34	19 31	19 23	19 19	19 51	19 18	19 17
9 45	9 81	9 81	10 12	10 12	9 29	9 25	9 28	10 26	10 23	10 23	10 23	10 23
cb	G	cb	BC G	25	125		125	25	G	cb	G	cb
60		35							BC	35	45	

Check

10.83 18.46

= S.E. Cb BC. FB 2005-P 96

T.P.

7.97 29.29 3.30 21.32

29.29

T.P.

1.92 24.62 6.75 22.70

1.63 29.45 27.82

N.W. B.P. Bessemer & Rosecrans

Upshur St
Cont.

1+02 = Pole 27.2' LT #511271 H

1+01.7 = 3.4' RT to 5'x5' Conc. Slab
ground M.H.

1+00

0+70

0+56.2 = B.C. of 4" Cb

0+41 = 8' sidewalk start 9" Cb

0+16.4 = End Curb on Left

Left Right 18

23.85	23.25	23.8	23.20	23.20	23.20	23.44	23.31
420	426	425	52	51	51	485	485
35	30	25	21	12.5	12.5	25	25
Back	Edge	Edge				G	Cb
Edge	Sidewalk	Sidewalk					

22.86	22.42	22.01	22.2	22.2	22.2	22.2	22.22
542	567	63	61	61	63	64	597
35	30	25	12.5	12.5	12.5	25	25
Back	Edge	Edge				G	Cb
Edge	Sidewalk	Sidewalk					

21.8	21.2	21.2	21.2
614	607	607	607
25.3	25.3		
G	Cb		

21.42	21.22	20.2	20.2	21.2	20.2	20.2	21.2
687	697	76	70	71	75	77	712
30	25.2	25.2	12.5	12.5	25	25	25
Cb	G						Cb

20.24	19.2
80	86
25	25
CD	

28.29

Upshur St
Cont

Left Right 19

CK

983 1846 = 1846 = SE Ch BC FB 2005 P46

7+00

22	51	2	22	2	5
14	10	19	19	19	12
35	25	12.5		12.5	29

1+44.025 End Upshur St & Start
School Prop.

20	24	24	24	20	25	25
24	35	36	36	32	28	25
45	25	12.5		12.5	25	43

1+39 = End Ch on Rt

1+32 = 11' drive 25' rt

24	24	24	24	24	24
41.9	41.8	20	20	20	20
35	45				

1+23.5 = End side walk on Lt.

24	24	24	24	24	24
44	43	46	46	46	46
35	30	25	12.5		

28.29

LOCATION EXISTING

SEWER DITCH

GIBBS AIRPORT

Levels - P. 21

Walker
F. Gregory
G. Pope
R. Sisson
12-21-49

INDEXED

W.K.

DEC 22 1949

7+60 = end Proposed Ditch

3+50 = Approx. end ditch

L. Hub (6+1627) P. 11 980

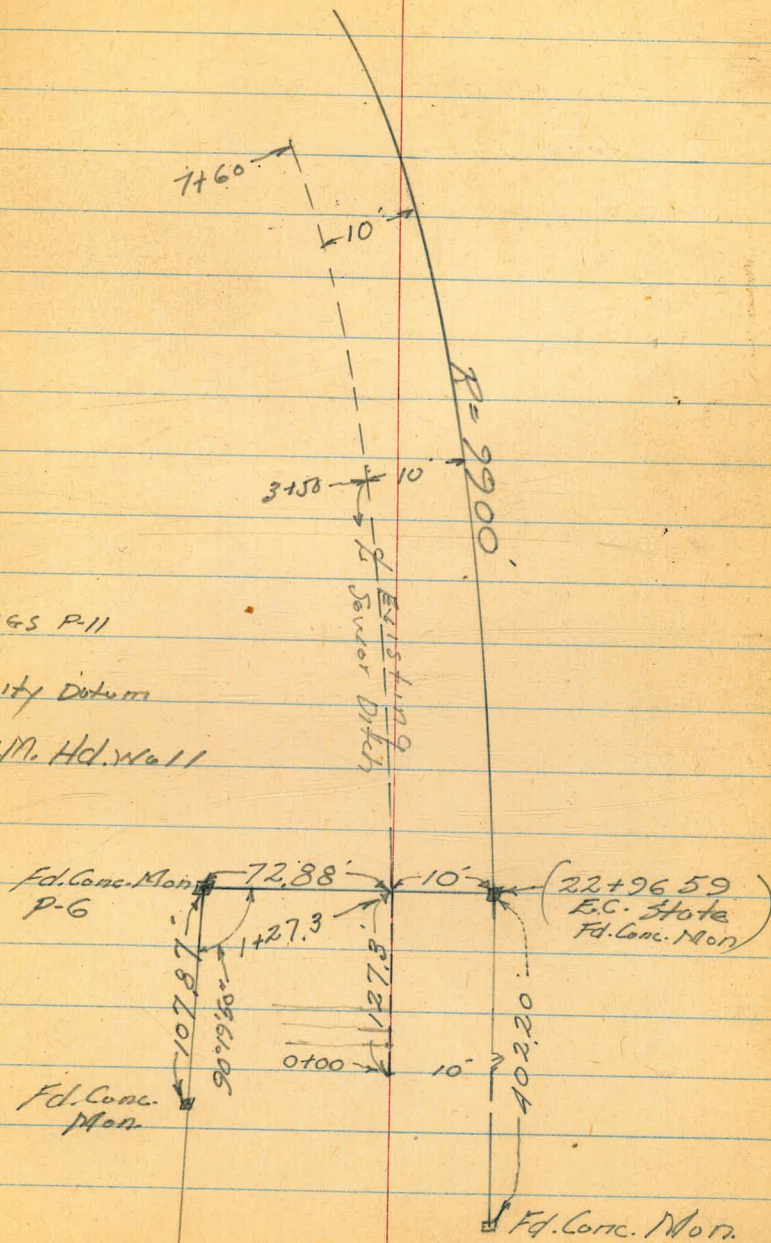
10+23 102.73

0+00 = Beg. Sewer Ditch

392.05 = USGS P. 11

392.93 = City Datum

392.50 = B.M. Hd. Wall



Gibbs Airport

Sewer Ditch Levels.

Location - P-20

Note: Ditch = 2' Wide to 2+00

2+00

Lt. 9.0

391.1
11.4

Rt. 9.5

5

5

1+50

Lt. 7.0

392.1
10.4

Rt. 7.5

5

5

1+00

Lt. 7.5
392.5
5

9.7

Rt. 5.5

5

5

0+50

Lt. 4.4

394.9
7.6

Rt. 4.4

5

5

0+00

Lt. 4.3

395.4
7.1

Rt. 4.3

5

5

402.52

~~408.64~~

402.52
9.59 ~~408.64~~

392.93
399.05

→ P-20 = city datum

B.M. on E.C. Hub (+16.97) P-11

Gibbs Airport
Levels - Sewer Ditch
Cont. from p. 21

Lt. E Ft. 22

5+00

389.6
56 57 65 62
5 2 5

4+50

300.1
54 52 60 56
5 2

4+00

390.4
47 47 57 51
2 5

3+50

390.5
45 48 56 47
5 2 5

3+00

391.0
41 41 51 47
5 3 5
396.14
~~402.26~~

T.P. 321 396.14 392.93
 ~~402.26~~ 2.59 399.05

2+50

391.1
10.0 114 10.8
5 5
402.52
~~408.64~~

7+20

10.8

386.0

101

11.6

7+11

10.3

6.7

on 2" water No. 17

7+00

9.0
5

386.1

94

97

95

1
5
on 2" water No. 17

6+50

8.0
5

386.0

81

82

6+00

7.7
5

388.1

80

79

5+50

5.6
5

5.8
2

389.3

68

65
5

396.14

~~468.26~~

lt L RT

Gibbs Airport
Sewer Ditch Levels
Cont. from P. 23

7+60

7+35

182
5

119
5

177.5
196
382.0

141
396.14
~~102.26~~

210
5

150
5

Gibbs Airport

Levels on Existing 3"
Tile Drains to Sewer Ditch.

Walker
Gregory
Pope
R. Sisson
12-28-49

25

1+27.3
P-20

Existing Sewer Ditch
P-20

6+16.97 P-20
Check L. Hub. 995

0.02
392.93
392.95

0+35 on Invert 763

394.27
394.56
394.49

0+19 " " 724

0+03 on Invert 741

1040 402.90 392.50 B.M. on Hd. Wall

3" Tile
Drain

El. 394.27

0+35

3" Tile

El. 394.66

0+19

3" Tile

El. 394.89

0+03

0+00 Beg. Sewer Ditch

X Sec for change of grade UPAS St
bet Arnold & Villa Terrace

Moore 3/16/50

W.O. 25020

Begg

Sherman

Crawford

INDEXED

W.R.

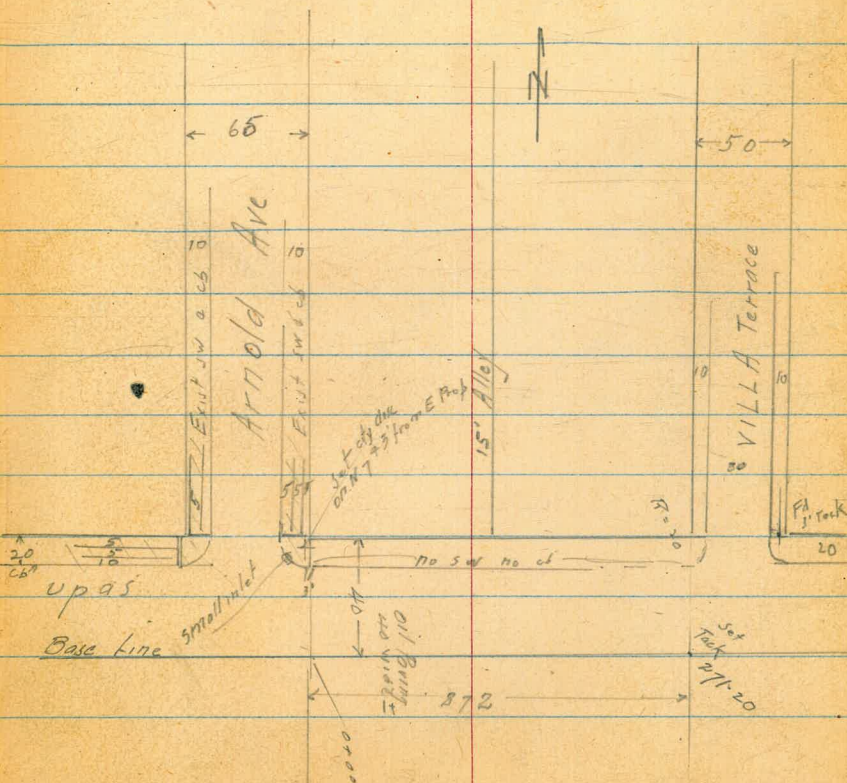
MAR 17 1950

BM 328.80 3E BP UPAS & 28th

BM BPNW 269.95 Arizona & Upas

BM BPSW 295.80 Park Blvd & Upas

Existing
sidewalk
acb



X Sec for change of grade UPAS

LT

RT

67

Base Line

0 + 40

2639	2630	26250	26244	26228	26195	26189	26229	2631
6.2	7.1	7.55	7.61	7.77	8.10	8.16	7.2	7.0
40	22	19	10		10	15	20	4
		20				20		

0 + 20

26228	26226	26205	26203	26183	26141	26110	2612	2621
7.3	7.5	8.00	8.02	8.22	8.64	8.25	8.2	8.0
40	22	19	10		10	17	19	40
		CO = end of oil				edge oil		

Reduced: March 17, 1950
John Firebaugh

0 + 00 E. Line Arnold

26210	26198	26140	26153	26147	26109	26034	25980
7.95	8.07	8.65	8.52	8.58	8.96	9.71	10.25
40	cb	20	10		10	20	33
on wk	end of	9	end of oil				Top of head Wall of outlet

0 + 0 270.05

269.95 BM

NW
UPAS & Arizona

270 05

X sec UPAS

1+40

1+20

1+00

0+80

0+60

3' wide
of gor apron

266.25
3.80
58

265.26
4.79
40

264.92
5.13
365

370.05

268.66
1.5
40

269.0
1.1
22

268.47
1.58
19
00

268.63
1.42
10

268.71
1.34
10

268.49
1.56
10

268.46
1.59
15.5

269.5
0.6
20

268.3
1.8
40

28

266.8
3.3
40

267.2
2.9
20

266.68
3.37
19
00

266.83
3.22
10

266.97
3.08
10

266.75
3.30
10

266.73
3.32
15
00

267.6
3.5
19

267.3
3.8
40

266.2
4.1
40

265.6
4.5
21

265.24
4.81
19
00

265.37
4.68
10

265.49
4.56
10

265.31
4.74
10

265.26
4.79
16
00

266.1
4.0
19

265.6
4.5
40

264.87
5.18
34
conc
drive

264.1
5.7
22

264.05
6.00
19
00

264.03
6.02
10

264.00
6.05
10

263.87
6.18
10

263.77
6.38
16
00

264.8
5.3
19

265.0
5.1
40

264.1
6.0
40

264.1
6.0
22

263.15
6.90
19
00

263.21
6.84
10

263.07
6.98
10

262.97
7.08
10

262.85
7.20
16
00

265.0
5.1
22

264.6
5.5
40

370.05

X Sec U.P.A.S

Lt

Base Line

114

29

TP 1193 294.72 0.44 282.29

2+20

	282.3	281.4	280.19	280.27	280.18	279.81	279.54	280.1	279.3	277.1
	0.4	1.3	2.54	2.46	3.55	2.92	3.19	2.6	3.4	5.0
	40	24	19.5	10		10	15	18	28	40
			20				20			

2+00

	277.2	277.2	277.18	277.05	277.01	276.70	276.35	277.2	276.2	273.5
	5.0	5.0	5.55	5.68	5.72	6.03	6.38	5.5	6.5	9.2
	40	22	19	10		10	15	19	30	40
			20				20			

1780

	274.2	274.3	273.68	273.91	273.85	273.55	273.34	274.4	273.5	271.0
	8.5	8.4	9.05	8.82	8.88	9.18	9.39	8.3	9.2	11.7
	40	22	20	10		10	15	19	31	40
			20				20			

1+60

	271.1	271.5	270.96	271.07	271.06	270.95	270.75	271.2	270.7
	11.6	11.1	11.77	11.66	11.67	11.78	11.98	11.0	12.0
	40	22	19.5	10		10	16	19	40
			20				20		

1314 292.73 0.46 269.59

270.05

283.73

X Sec UPAS

30

2 + 71 20 cont

291.89

290.63

289.40

289.58

288.94

288.64

287.99

287.47

287.22

11.7
40

287.8

287.3

284.2

2 + 71 20

2.33

3.59

4.82

4.64

5.28

5.58

6.83

6.75

7.00

6.4

7.0

9.4

40
on W/K

30
on W/K

23
9

errd/corb

10

15

17

28

36

00

282.2

2 + 60 contd

11.7

40

12.2

40

2 + 60

291.4

288.2

288.4

287.27

287.14

286.58

286.03

285.89

286.6

285.7

283.3

2.8

5.3

5.8

6.95

7.08

7.64

8.19

8.33

7.6

8.5

10.9

40

36

25

19.5

10

10

10

15

18

26

37

00

00

2 + 40

286.5

284.9

284.9

283.50

283.57

283.40

283.08

282.77

283.5

282.0

7.7

9.3

9.3

10.72

10.65

10.82

11.14

11.45

10.7

12.2

40

34.0

23

18.5

10

10

10

15

15

18

27

00

00

294.22

294.22

14.5

40

2.03 299.92
 8.11 301.95 0.38 293.84

X Sec O.P. A.S
 300.01 Myrtle & Villa Terrace NW BP
 299.92
 0.09

A+81²⁰ cont'd

2851 2866
 41 7.6
 40 36

A+81²⁰ Wcb of Villa Terrace

291.84	291.37	290.19	289.70	289.04	288.60	288.32	288.8	288.1
238 2.85	4.03	4.52	5.18	5.62	5.90	5.4	6.1	
40 40	20	10		10	15.5	18	28	
cb								

A+76²⁰ cont'd

2892
 10.0
 40

A+76²⁰

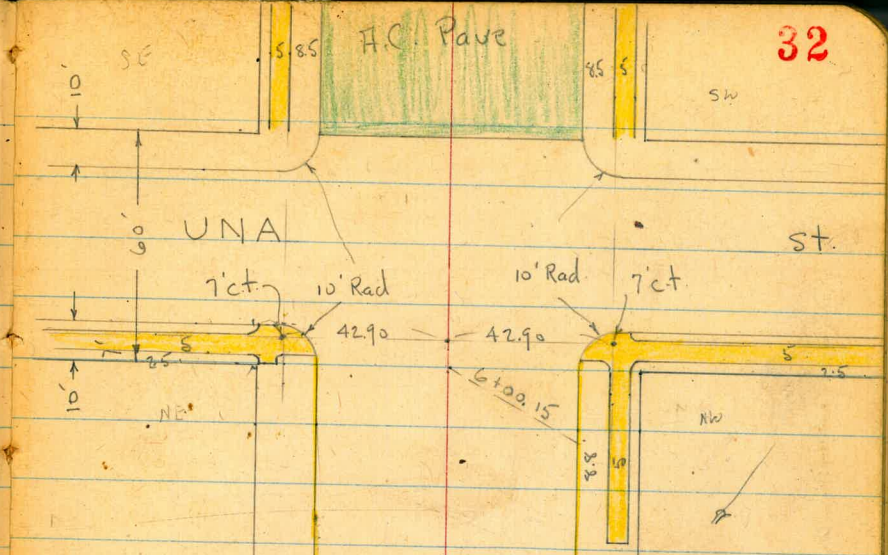
290.72	290.29	289.76	289.17	288.56	288.07	287.82	288.1	287.5	285.2
250 3.93	4.46	5.05	5.66	6.15	6.40	5.8	6.6	7.3	
cb 27.2	20	10		10	15	17	28	36	
27.2	9					20			

294.22

294.22

INDEXED
M.R.
APR 7 1950

32



Dalbergia

Dalbergia

THOR

Fd. Mon.



St.

X-Section Dalbergia St. - from
Thor to Una. - 100' St. - 16 cbs.
in sketch - P. 32

4348

W.O. 31809

4-6-50

Osborne
Hardin
Hatch
Shepard.

0+05-35.7 Rt. = E.F.H.

0+00 = E.L. Thor. - Beg. cbs.

*Reduced - April 7, 1910
B.L. Carbone*

0-10

0-30 = E Thor. - Graded - No cbs.

4.16 16.41 11.83 12.25

4.97 24.08 19.11

B.M. 19.11 N.E. 7' c.f. Una & Dalbergia St

	8.4	8.5	9.9	10.02	9.1	9.4	9.3	9.2	9.0	9.03	9.3	10.3	9.2
	8.0	7.9	6.5	6.39	7.3	7.0	7.1	7.2	7.4	7.39	7.1	6.9	7.2
	150	100	50	45	34	34	17	17	34	34	50	100	150
				Top end ch.	Top cut.				Top cut.	Top end ch.			
	6.0		7.1	8.0	8.5	8.5		8.7	8.9		9.0	9.0	
	10.4		9.3	8.4	7.9	7.6		7.7	7.5		7.4	7.4	
	150		100	50	25			25	50		100	150	
	6.2	6.5	7.9	8.4	8.7			9.1	9.3		9.1	9.0	
	10.2	9.6	8.5	8.0	7.6			7.3	7.1		7.3	7.4	
	150	100	50	25				25	50		100	150	

16.41 ✓

Dalbergia

3+50

217 Top	22.90	3.6	4.13	4.9	4.8	4.8	5.1	6.0	5.98	4.7
		48.4 along wall	Top	34.1 got.	17	17	17	33.9 got.	Top	50
		19.7	19.37	18.6	18.7	18.7	18.5	17.5	18.44	18.99
		4.4	4.70	5.5	5.4	5.4	5.6	6.5	5.63	5.4
		50	Top	34 got.	17	17	17	33.9 got.	Top	50

3+25

19.7	19.37	18.6	18.7	18.7	18.5	17.5	18.44	18.99
4.4	4.70	5.5	5.4	5.4	5.6	6.5	5.63	5.4
50	Top	34 got.	17	17	17	33.9 got.	Top	50

3+19 = ± 11' Dirt Dr. on Lt.

19.3	18.52
4.8	5.55
40	34 Dr.

3+00

19.1	18.7x	17.8	18.1	18.1	17.8	17.0	17.78	18.0
5.0	5.33	6.3	6.0	6.0	6.3	7.1	6.29	6.1
50	Top	34 got.	50	50	17	34 Top	50	50

2+94 = ± 12' Dirt Dr. on Rt.

16.98	17.7
7.09	40
34 Dr.	

2+50

17.9	17.23	16.4	16.6	16.6	16.3	15.6	16.0
6.2	6.84	7.7	7.5	7.5	7.8	8.5	7.77
50	Top	34 got.	17	17	17	34 got.	Top

2+44 = ± 12' Dirt Dr. on Rt. - 50.1 Rt. = ± 8.5 Conc. Dr.

16.7	15.63	15.50	16.0	15.47	15.39
8.57	8.1	8.57	8.1	8.60	8.70
34.1 Dr.	40	34.1 Dr.	40	50.1 Dr.	60 Dr.

2+22 = ± 10' Dirt Dr. on Lt. - W.M. = Water Meter in Dr.

24.07 ✓

Dalbergia

4+70

21.1	20.80	20.2	Lt.	20.2	20.0	19.6	19.3	19.83	36
3.0	3.27	3.9		3.9	4.1	4.5	4.8	4.24	4.4
50	Top	34		17		17	34	Top	50
		gut.					19.21	19.85	19.7

4+63 = ± 10' Dirt Dr. on Rt.

4.86
33.8
Dr.

4+30

21.7	20.80	20.1		20.1	20.0	19.7	19.1	19.82	19.9
2.8	3.27	4.0		4.0	4.1	4.4	5.0	4.25	4.2
50	Top	34		17		17	33.9	Top	50
		gut.					19.16	19.5	

4+21 = ± 10' Dirt Dr. on Rt.

4.91
33.8
Dr.

4+10 = ± 12' Dirt Dr. on Lt.

20.7
34
40

4+00

21.1	20.61	20.0		20.0	19.9	19.6	19.1	19.63	20.0
3.0	3.46	4.1		4.1	4.2	4.5	5.0	4.44	4.1
50	Top	34		17		17	34	Top	50
		gut.					gut.		

3+94 = ± 12' Dirt Dr.

20.6
35
40

3+75

20.6	20.34	19.7		19.7	19.7	19.3	18.7	19.38	19.7
3.5	3.73	4.4		4.4	4.4	4.8	5.4	4.69	4.4
48.6	Top	34		17		17	34	Top	50
along wall		gut.				16.84	19.3		

3+67 = ± 13' Dirt Dr. on Rt.

24.07

5.43
33.9
Dr.

Dalbergia

Lt.

#

Rt.

37

T.P. 4.77 23.53 5.31 18.76

23.53 ✓

5+69 = £ 10' Conc. Dr. on Rt.

5.71	5.10	5.09
33.9	42.8	47.8
Dr.	walk	

5+62.9 = Beg. walk on Rt.

5.18	5.01	4.97
34	42.8	47.8
Top	Cor.	walk

5+50

2.6	20.0	19.6	19.5	19.3	18.9	18.4	19.04	18.9
3.5	4.07	4.5	4.6	4.8	5.2	5.7	5.03	5.2
50	Top	34.1	17		7	33.9	Top	50
		gut.				gut.		

5+08 = £ 12' Conc. Dr. on Lt.

20.95	20.86	20.72	20.09
3.12	3.21	3.35	3.98
50	48	43	33.9
Dr.	£9 Dr.	£9 Dr.	

5+00

20.9	20.58	20.1	20.0	19.8	19.4	18.9	19.61	19.4
3.2	3.49	4.0	4.1	4.3	4.7	5.2	4.46	4.7
50	Top	34.1	17		17	34	Top	50
		gut.				gut.		

4+88 = £ 13' Dirt Dr. on Lt.

20.5	20.05
3.6	4.02
40	33.9
	Dr.

24.07

Dalbergia

of Returns

50' E. = E. cb.

30' E. = #

10' E. Cont.

10' E. = W. cb.

of 10' Rad. Ret.

6+00.15 = w.l. Una St.

3.7
50

#	N.E. Ret.	5.0 9.4	16.5 9.4	4.6 Top	19.07 Top	#	S.E. Ret.	5.0 9.4	17.5 Top	Rt.	18.08 5.45	38	
4.20 100 Top	4.6 100 9.4	4.4 50 Top	5.5 50 9.4	4.4 44 Top	5.0 50 9.4	5.2	6.0 34 9.4	6.2 44 9.4	5.4 44 9.4	6.4 50 9.4	5.4 50 Top	7.0 100 9.4	6.2 100 Top
		19.2 19.5	4.0 100	4.3 50	19.0 34	5.0	5.4 34	5.6 50	6.1 34	17.9 50	6.5 100		
3.18 150 Top	3.9 150 9.4	3.5 100 Top	4.1 100 9.4	3.9 50 Top	19.5 19.5		4.9 50 Top	6.7 100 9.4	5.8 100 Top	7.6 150 9.4	6.6 150 Top		
4.5 50 9.4	3.9 44 Top	4.5 44 9.4	4.6 34	4.6 7	18.9 18.9	4.9	5.3 17	5.7 34	5.7 44 9.4	4.9 44 Top	5.8 50 9.4		
		19.5 19.5	4.7 9.4	4.0 Top	19.5 19.5			5.7 9.4	17.5 17.5	5.7 9.4	4.9 Top		
3.7 50	3.8 49.5 cov. walk	3.7 44.6 Top	4.0 Top	4.6 34 9.4	4.6 17	4.9	5.2 17	5.7 34 9.4	4.9 Top	4.7 42.8 walk	4.7 47.8		
						23.53							

Lt.

#

Rt.

39

Soil Sample taken at 5+00

check B.M.

9.88

13.65

13.58 - N.W. 7' ct. Under Cottonwood.

check starting B.M.

4.43

19.10 ✓

19.11

60' E. = E.L. + edge A.C. pave.

19.00

15.46

15.56

15.46

16.07

17.45

15.09

4.53

5.07

4.97

5.07

5.46

6.05

5.44

Top

33.9

17

17

17

33.9

Top

9.4

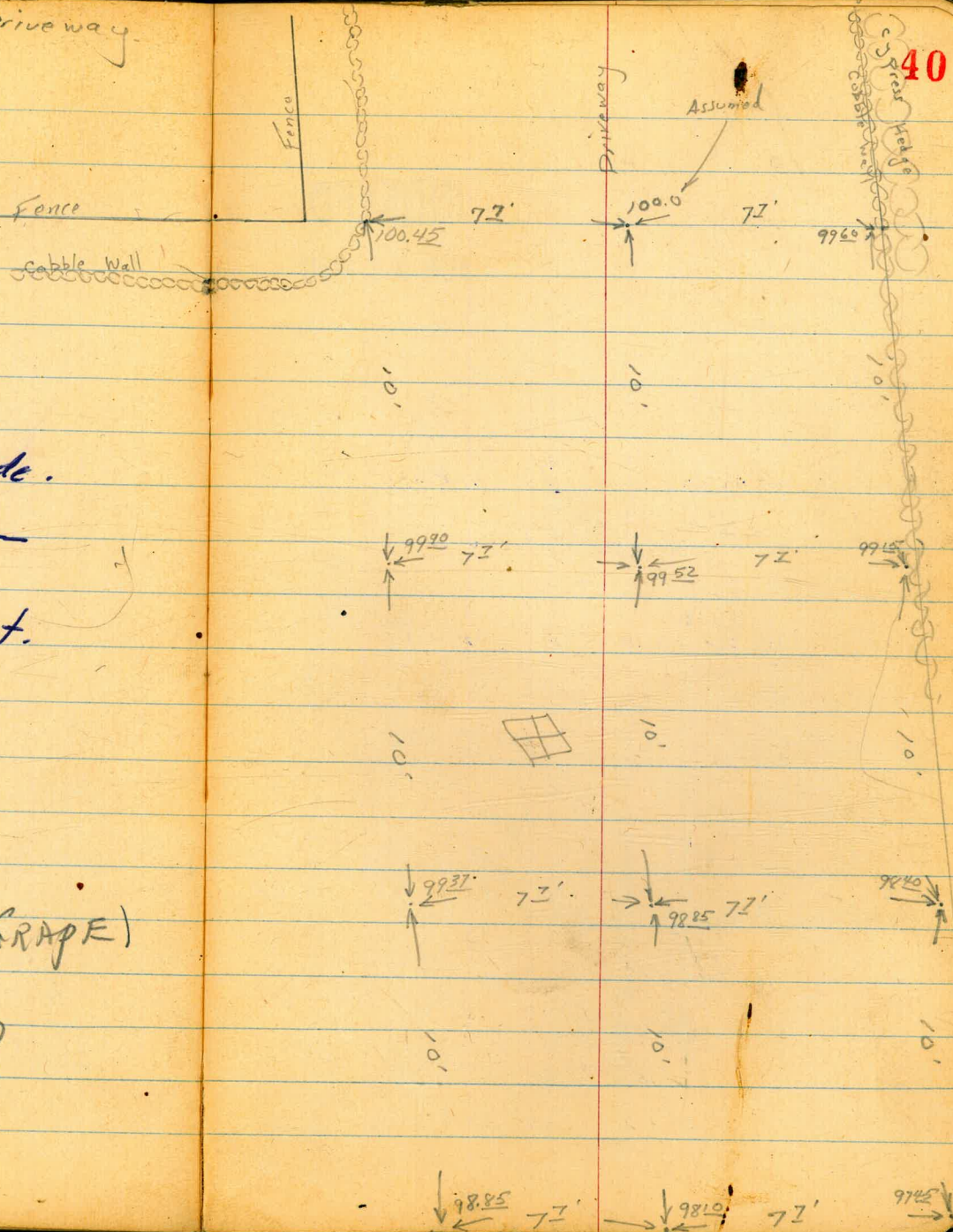
9.4

23.53

Roberts ✓
 Huber
 Moore
 Clark
 5-25-50
 W.O. 20006

Levels on Private Driveway
 West Side Sand Rock Grade
 Court Case

INDEXED
 MAY 24 1950



Approx. 5% grade.
 E. F. Gabriel
 6" in 10 feet.

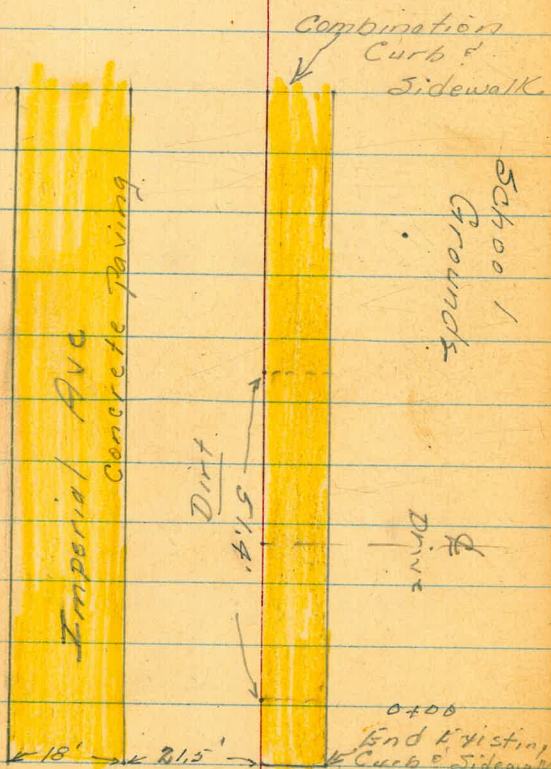
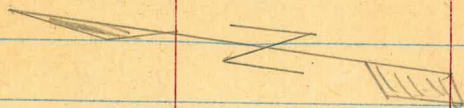
(4th BET FIRM GRADE)

9" in 50' 1 1/2% Grade.
 8' in 48' Little over 16.2%
 or 2 1/2% in 48'

Johnson
Greer
Crawford
6-9-50
W.O. 20006

Curb levels on 150'
Existing Curb
on Imperial

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JUN 13 1950



		Elev.
1750	3.07	144.42
1700	3.45	144.04
0+61.4 - End Drive	3.53	143.96
0+57.4	4.06	143.43
0+35.7 - End Drive	4.11	143.38
0+14	4.47	143.02
0+10 - Start Drive	3.96	143.53
0+00 - End Ex. Curb	4.04	143.45

147.42
T

B.M. 9.60 147.49 137.89 20' 48th & Imperial

D. Smith
G. Cota
F. Bunch

Curb levels on Imperial

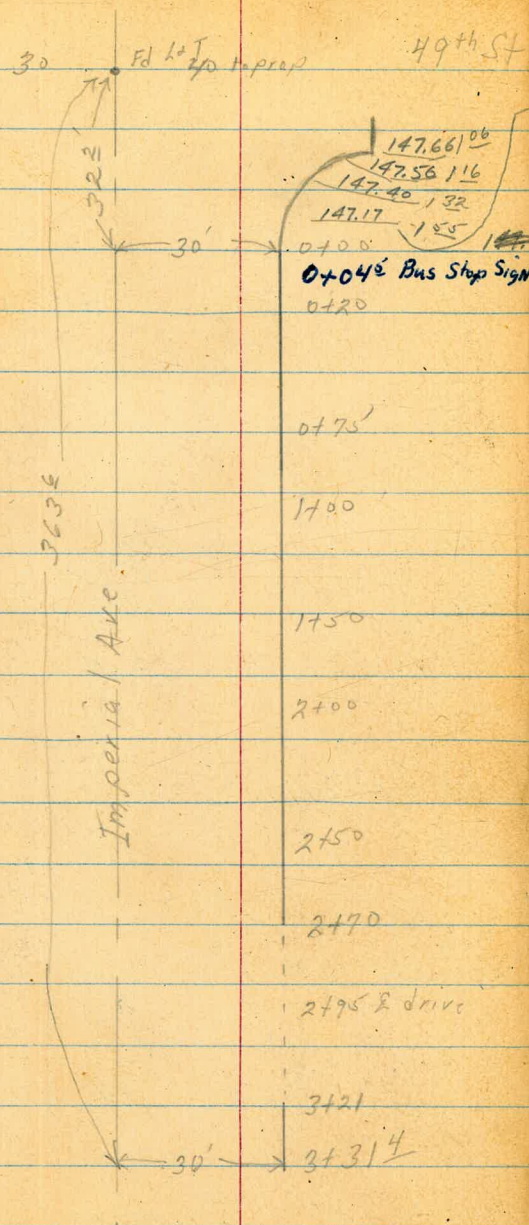
From 49th St westerly
South Side

on 6-19-50
W020006 42

all shots top of curb
or gutter in Drive



INDEXED
JUN 19 1950



rods around return

147.66100
147.56116
147.40132
147.17
155

0+00
0+04 1/2 Bus Stop Sign
0+20

0+75

1+00

1+50

2+00

2+50

2+70

2+95 1/2 drive

3+21

3+31 1/4

0+00

0+20

0+75

1+00

1+50

2+00

2+50

2+70 Fly Drive

2+95 1/2 Drive

3+21 wly Drive

3+31 1/4 End C3

169 147.03

210 146.62

310 145.62

343 145.29

408 144.64

441 144.31

420 144.02

472 143.95

535 143.37

520 143.52

529 143.43

Cont p 77

10 83

148 72

137 82

2 1+T 48 1/4 Imperial

48 1/4

2926

3147 0.74

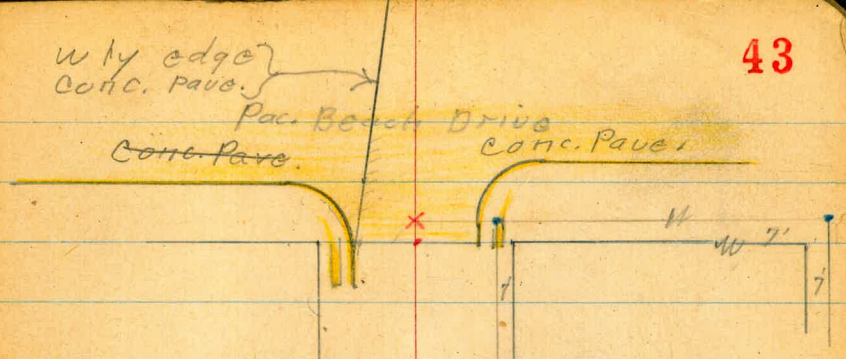
40 to prop

X-Sec. Jewell St - 75' wide
Fortuna to Pacific Beach Dr.

Sommermyer
Begg
Acuña

7-20-50
N.O. 31740

W by edge }
Conc. Pav. }
Pac. Beach Drive
Conc. Pav.



- ◻ = Fd 1/2 hub
- = Fd. L. st.
- = set nail
- ✕ = cut cross in Conc.

INDEXED
MK
JUL 24 1950

APPROX. N

← 37' ✕ 37' →

0.10 Fd LS. 2001
used as ot eo.

Fortuna ← 0-31 Street

A.C. Pav.
0-75 • 30' 50" / Fd 1/2 - S.E. 7' lines
to plant Jewell

0-31 = Nly edge A.C. Pavc.

Pi = 37[±] (or property) Lt. or Rt.

0-37[±] = ± Fortuna

0-55[±] = Sly gutter line Fortuna

0-55[±] = Sly curb line Fortuna

Set. B.M.	8.48	44.29	9.28	35.81
T.P.	3.01	45.09	6.35	42.08
T.P.	2.65	48.43	5.34	45.78
T.P.	0.57	51.12	3.33	50.55
Pavc.	8.67	53.88	—	45.21

35.44	35.30	35.49	35.73	36.31	38.83
8.85 88	8.99 P.	8.80	8.56 18	7.98 P.	5.16 88

35.46	35.33	35.41	35.53	35.81	36.37	38.91
8.93 88	8.96 P.	8.88 18	8.76	8.48 18	7.92 P.	5.38 88

35.04	34.94	35.09	35.29	35.44	35.86	38.63
9.15 88	9.35 38	9.20 18	9.00	8.85 18	8.43 38	5.66 88

35.55	35.44		36.37	39.10
8.74 88	8.85 38	44.29	7.92 38	5.19 88
OC	OC.E.C.		OC.E.C.	

Fortuna + Jewell
Set. B.M. Chisel in ch. Ctr. S.E. of Rot. B.M. #2

Set. B.M.
= S.E. 7' Lt. Jewell + Pac. B. Drive = B.M. #1

B.M. = S.W. 72 + 7. Pacific Beach Dr. & Kendall

Jewell St

1+41 36⁹ Rt. = 8' wide Conc. Dr.

43.07
43.40
45
 $\frac{1.22}{369}$ $\frac{0.89}{467}$

1+00

40.3 41.3 40.2 41.4 40.6 40.6 40.8 41.6 42.3
 $\frac{4.0}{P}$ $\frac{3.0}{18}$ $\frac{4.1}{11}$ $\frac{2.9}{5}$ $\frac{3.7}{2}$ 3.7 $\frac{3.5}{18}$ $\frac{2.7}{21}$ $\frac{2.0}{P}$

0+60

39.1 40.2 39.4 40.4 40.7 40.0 40.0 40.9 41.5
 $\frac{5.2}{P}$ $\frac{4.1}{15}$ $\frac{4.9}{12}$ $\frac{3.9}{8}$ $\frac{3.5}{2}$ 4.3 $\frac{4.3}{18}$ $\frac{3.4}{22}$ $\frac{2.8}{P}$

0+30

38.7 39.5 39.1 39.8 39.9 39.4 39.6 39.9
 $\frac{5.6}{P}$ $\frac{4.5}{15}$ $\frac{5.2}{10}$ $\frac{4.5}{6}$ 4.4 $\frac{4.9}{4}$ $\frac{4.7}{20}$ $\frac{4.4}{P}$

0+18 - 37⁶ Rt. = 3' wide Conc. walk

40.57
41.07
 $\frac{3.72}{375}$ $\frac{3.22}{475}$
017 walk

37⁶ Rt. = 3/4" pipe L.S. 2001

22² Lt. = Ely. end 8' high woven wire fence

0+00 = Nly line Fortuna

38.5 39.0 38.0 38.5 39.9
 $\frac{5.8}{P}$ 5.3 $\frac{6.3}{4}$ $\frac{5.8}{20}$ $\frac{4.4}{P}$

Reduced
7-24-50
Firebath

0-20

37.9 38.6 37.4 37.7 39.1
 $\frac{6.4}{P}$ 5.7 $\frac{6.9}{4}$ $\frac{6.6}{20}$ $\frac{5.2}{P}$

44.29

3+26 - 36' Rt. = end 3' high hedge

3+00

2+85 - 36' Rt. = start 3' high hedge

Drive level across

2+80 - 37' Rt. = 8' wide Conc. Drive

2+50

2+00

1+60 36' Rt. = 8' wide Conc. walk.

1+50

T.P. 5.63 47.40 2.52 41.77
44.27

47.40

$\begin{array}{r} \times 2.7 \\ 47 \\ \hline P \end{array}$ $\begin{array}{r} \times 3.1 \\ 413 \\ \hline 26 \end{array}$ $\begin{array}{r} \times 2.5 \\ 49 \\ \hline 20 \end{array}$ 4.1 $\begin{array}{r} \times 4.7 \\ 2.7 \\ \hline P \end{array}$

$\begin{array}{r} \times 5.04 \\ 2.36 \\ \hline 372 \end{array}$ $\begin{array}{r} \times 5.46 \\ 1.94 \\ \hline 50 \end{array}$

$\begin{array}{r} \times 2.6 \\ 4.8 \\ \hline P \end{array}$ $\begin{array}{r} \times 2.9 \\ 4.5 \\ \hline 25 \end{array}$ $\begin{array}{r} \times 2.2 \\ 5.2 \\ \hline 19 \end{array}$ 4.6 $\begin{array}{r} \times 3.2 \\ 4.2 \\ \hline 16 \end{array}$ $\begin{array}{r} \times 3.7 \\ 3.7 \\ \hline 20 \end{array}$ $\begin{array}{r} \times 4.3 \\ 3.1 \\ \hline P \end{array}$

$\begin{array}{r} \times 1.8 \\ 5.6 \\ \hline P \end{array}$ $\begin{array}{r} \times 2.5 \\ 1.9 \\ \hline 22 \end{array}$ $\begin{array}{r} \times 2.0 \\ 5.4 \\ \hline 17 \end{array}$ 5.1 $\begin{array}{r} \times 2.7 \\ 4.7 \\ \hline 17 \end{array}$ $\begin{array}{r} \times 3.2 \\ 4.2 \\ \hline 22 \end{array}$ $\begin{array}{r} \times 3.7 \\ 3.7 \\ \hline P \end{array}$

$\begin{array}{r} \times 3.22 \\ 4.18 \\ \hline 362 \text{ walk} \end{array}$ $\begin{array}{r} \times 3.42 \\ 3.28 \\ \hline 462 \end{array}$

$\begin{array}{r} \times 0.9 \\ 6.5 \\ \hline P \end{array}$ $\begin{array}{r} \times 2.0 \\ 5.4 \\ \hline 20 \end{array}$ $\begin{array}{r} \times 0.7 \\ 6.7 \\ \hline 15 \end{array}$ $\begin{array}{r} \times 1.6 \\ 5.8 \\ \hline 8 \end{array}$ 5.8 $\begin{array}{r} \times 1.6 \\ 5.8 \\ \hline 17 \end{array}$ $\begin{array}{r} \times 2.4 \\ 5.0 \\ \hline 20 \end{array}$ $\begin{array}{r} \times 3.1 \\ 4.3 \\ \hline P \end{array}$

(Drive level across)
 4+32 - 37⁵ Rt. = \pm 8' wide Conc. Drive

46.10
 $\frac{4.42}{375}$ $\frac{3.78}{475}$

Drive level across
 4+14 - 37³ Rt. = \pm 8' wide Conc. Drive

45.79
 $\frac{47.3}{377}$ $\frac{46.79}{477}$

T.P. 6.88 50.52 3.26 44.14

50.52

4+00

43.6	44.0	43.3	44.1	44.3	44.6	46.0
$\frac{3.8}{P}$	$\frac{3.4}{26}$	$\frac{4.1}{20}$	3.3	$\frac{3.1}{16}$	$\frac{2.8}{18}$	$\frac{1.4}{P}$

3+60 - 39³ Rt. = \pm 2⁵ wide Conc. walk

45.73
 $\frac{1.67}{394}$ $\frac{1.87}{494}$

3+50

43.2	43.7	42.9	43.7	43.9	44.6	45.3
$\frac{4.2}{P}$	$\frac{3.7}{26}$	$\frac{4.5}{21}$	3.7	$\frac{3.5}{17}$	$\frac{2.8}{25}$	$\frac{2.1}{P}$

3+44 - 39¹ Rt. = \pm 2⁵ wide Conc. walk

45.39
 $\frac{2.01}{392}$ $\frac{1.43}{47}$

47.40

5+34³ - 19⁸ Rt. = B.C. Cb. Ret. (22' Cb. Rad)

5+31⁷ { 4 Sly. 7' line Pac. Beach Dr.
Cut cross in Pave. = Jewell

5+24³ Cont.

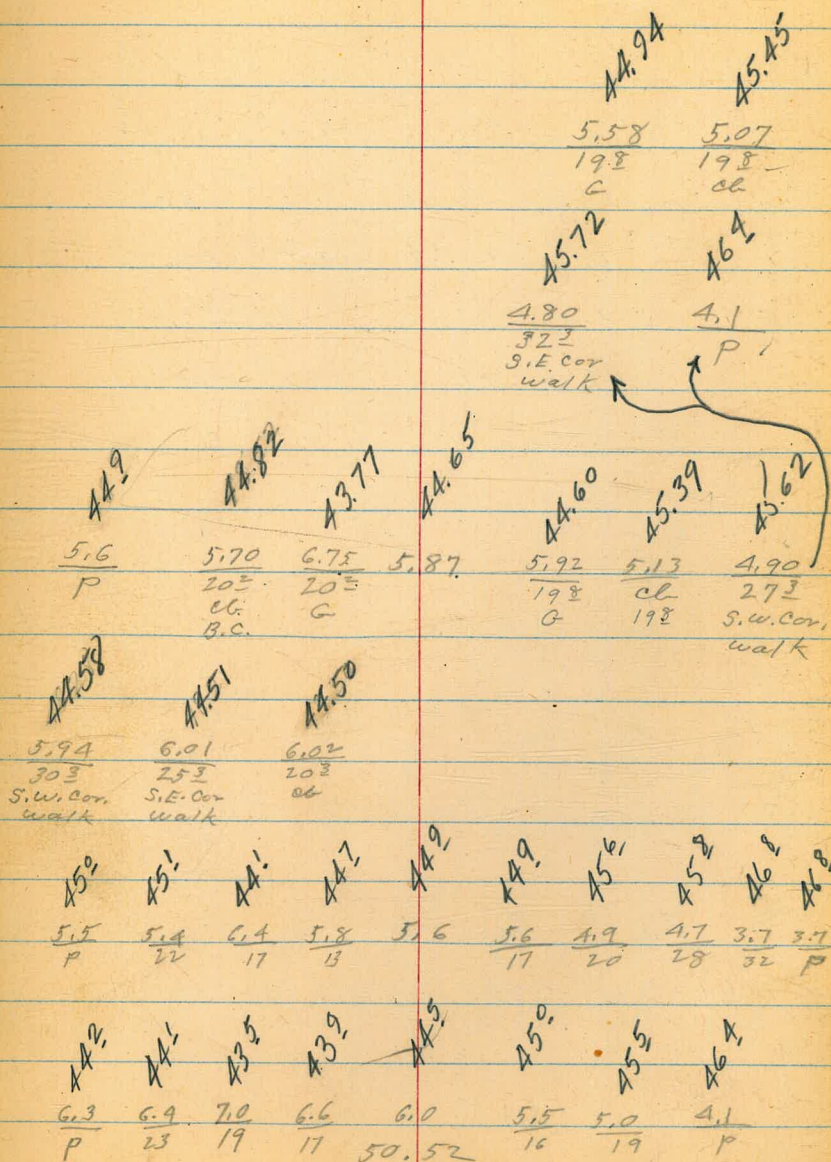
(straight grade on Returns)

5+24³ { 19⁸ Rt. = start curb + walk
20³ Lt. = B.C. Curb Ret. (20' Cb. Rad)
= start conc. pave.

5+04 - 20³ Lt. = start curb

5+00

4+50



10.80 $\frac{0.03}{45.18}$

orig. B.M. = 45.21

T.P.	9.73	55.98	9.37	46.25
T.P.	2.07	55.62	8.73	53.55
T.P. + (check to B.M.)	4.06	62.28	4.06	58.22 (0.21)
T.P.	5.40	62.28	0.16	56.88
T.P.	9.73	57.04	3.21	47.31
Check B.M.#1 - PAA		4.75	45.77	(45.78)

Shown in bench book as 58.43

Cont.

5+53³ = Sly. Cl. P.B. Dr. to East

	46.02	46.94	47.54
	4.50	3.58	2.98
	40	90	90
	Cl. E.C.	G	Cl.
44.5	44.20	44.00	44.58
6.0	6.32	6.52	5.94
40	172	129	74
Ord.	Edge	pave	
45.17	44.92	44.05	43.91
5.35	5.60	6.47	6.61
70	40	186	74
	Cl.	Edge	
	E.C.	pave	
44.63	44.84	45.02	45.10
5.89	5.68	5.50	5.42
	5.00	222	228
		G	on cl.

5+44⁵ = Sly. Cl. P.B. Dr. to West

45.17	44.92	44.05	43.91	44.63	44.84	45.02	45.10	45.54
5.35	5.60	6.47	6.61	5.89	5.68	5.50	5.42	4.98
70	40	186	74		5.00	222	228	
	Cl.	Edge				G		on cl.
	E.C.	pave						

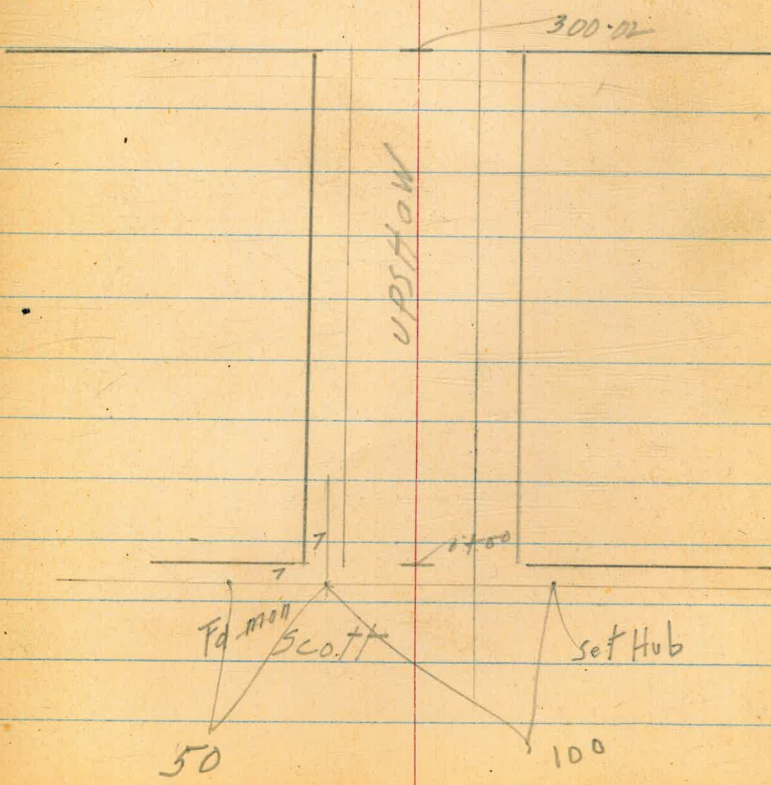
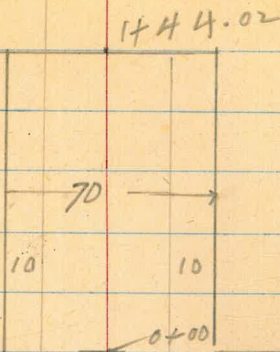
50.52

Upshaw

Grades

50

INDEXED
OCT 9 1950



1 + 20

14 29
5 5
5 1
60.4

14 80 **51**
5 00
C 4.5
0.5

0 + 00

13 77
6 0
5 3
60.7

14 27
5 5
5 4
60.1

0 + 80

13.24
6 5 6
5 6
60.9

13 75
6 05
C 5.7
C 0.35

0 + 60

12 72
7 1
5 9
60.7

13.22
6 58
5 5
C 7.1

0 + 40

12 19
7 6
6 5
C 1.1

12 70
7 1
C 6.5
C 0.6

0 + 20

11 67
8 1
6 5
C 1.6

12.17
7.63
C 6.8
C 0.8

0 + 00

Scott Street

19 80
11 15
8 6
7 5
C 1.1

19 80
11 65
8 15
C 7.0
C 1.1

19 55
3 5
19 80

SW upshar & Psecant
7 Tack

2 + 40

$$\begin{array}{r} 17.45 \\ 2.35 \\ \hline 2.0 \\ \hline C 0.3 \end{array}$$

17.52

$$\begin{array}{r} 17.93 \\ 1.9 \\ \hline 1.6 \\ \hline C 0.3 \end{array}$$

2 + 30 VC

$$\begin{array}{r} 17.19 \\ 2.6 \\ \hline 1.4 \\ \hline C 1.26 \end{array}$$

17.27

$$\begin{array}{r} 17.69 \\ 2.21 \\ \hline 2.36 \\ \hline F 0.1 \end{array}$$

2 + 20

$$\begin{array}{r} 16.93 \\ 3.1 \\ \hline 1.4 \\ \hline C 1.7 \end{array}$$

$$\begin{array}{r} 17.43 \\ 2.4 \\ \hline 2.5 \\ \hline F 0.1 \end{array}$$

2 + 00

$$\begin{array}{r} 16.39 \\ 3.41 \\ \hline 1.8 \\ \hline C 1.6 \end{array}$$

$$\begin{array}{r} 16.90 \\ 2.9 \\ \hline 3.4 \\ \hline F 0.5 \end{array}$$

1 + 80

$$\begin{array}{r} 15.86 \\ 4.0 \\ \hline 3.3 \\ \hline C 0.7 \end{array}$$

$$\begin{array}{r} 16.37 \\ 3.4 \\ \hline 3.8 \\ \hline F 0.4 \end{array}$$

1 + 60

$$\begin{array}{r} 15.34 \\ 4.26 \\ \hline 3.8 \\ \hline C 0.7 \end{array}$$

$$\begin{array}{r} 15.85 \\ 4.00 \\ \hline \text{Grade } 4.0 \end{array}$$

1 + 40

$$\begin{array}{r} 15.84 \\ 5.0 \\ \hline 4.5 \\ \hline C 0.5 \end{array}$$

$$\begin{array}{r} 15.32 \\ 4.5 \\ \hline 4.2 \\ \hline C 0.3 \end{array}$$

upshaw

53

3+00

Prosecrants

18.46

17.51

18.35

2+90

18.46
18.02
3) 46
15

18.32

17.86

2+80

upshaw

18.17

18.07

2+70

19.8
18.02
1.8
1.3
0.5

17.98

18.28

2+60

19.8
17.86
1.94
1.5
0.4

17.87

18.22

2+50

19.8
17.67
2.1
1.3
0.8

17.72

18.10
1.7

Upshaw

54

0 + 00

23 44
6 36

23 44

0 + 80

22 65

22 65

0 + 60

21 86

21 86

0 + 40

21 07

21 07

0 + 20

20 28

20 28

0 + 00

19 50

19 51

~~1 + 10~~~~2 + 20~~~~3 + 30~~

1 + 44.02

30

$$\begin{array}{r}
 30 \\
 25 \overline{) 17} \\
 \underline{48} \\
 26 \\
 \underline{22}
 \end{array}$$

$$\begin{array}{r}
 30 \\
 25 \overline{) 17} \\
 \underline{48} \\
 24 \\
 \underline{60.4}
 \end{array}$$
~~1 + 20~~

1 + 20

~~1 + 20~~

24.38

24.38

~~1 + 14.30~~~~24.00~~

$$\begin{array}{r}
 19.55 \\
 10.45 \\
 \underline{30.00}
 \end{array}$$

1-9-51
Hendricks
Shepard
Cravford
W0#125020

X Sect. Alley Block 255
Pacific Beach

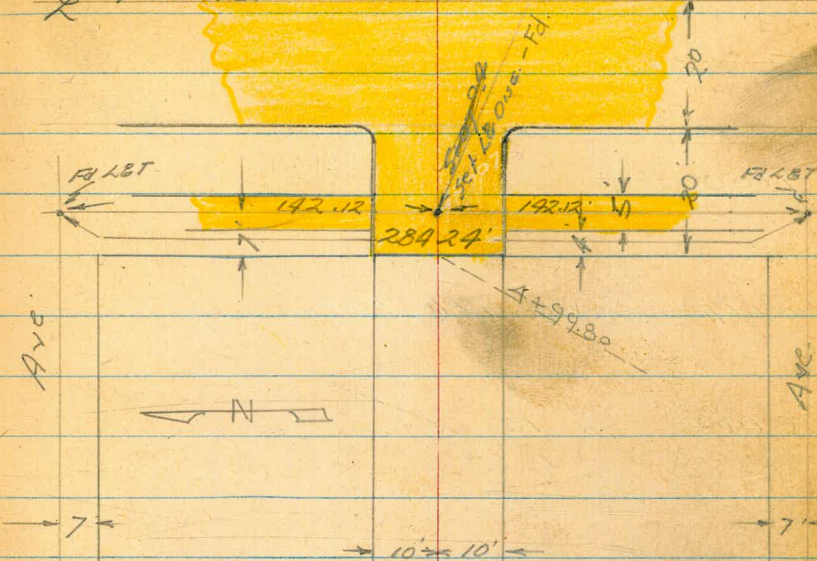
Reduced
1-11-51
P.E.R.

INDEXED
M.K.
JAN 10 1951

Green Profile
773A

Fanuel

56



Grand Ave.

Block

255

Ave.

Conc. Mon.
Fd Hub
& Tank

141.99

0100

Set Hub & Disc
Reset

Set 18. Disc

284.05'

283.98'

Everts

St.

Note: Set 18 Disc
from 30' cb Radius
Hub 3 ft.

135
40
85

Levels Alley Block 255
Pacific Beach

1+49- 9.7 Rt. = end fence

1+12- 99' Rt. = Beg. Picket fence

1+00

- 9.9' Rt. = end fence

0+99 = Power Pole #PA 1222 B.M. = 9.4 32.55
90' Rt. = \pm ✓

0+85- 99' Rt. = end fence

(can be broken out)

0+80 & 10' Conc. slab on Lt.

- 9.8' Rt. = fence

0+50- 10' Lt. = Beg. Picket fence ✓

- 10.1 Rt. = Beg. Picket fence

0+00 East Line Events

T.P. 31.12

T.P. 31.35

B.M. 39.53

Check Sections and add. Notes - 5-27-54 - F.O.
W.O. 32072

Lt.

Rt.

Rt.

57

32' ✓ 31.8 ✓ 31.9 ✓
25 10 32.0 31.4 31.4
25 10 10 25

31.94 ✓ 31.92 ✓
13.5 9.3
along house

31.5 ✓ 31.4 ✓ 31.3 ✓ 31.1 ✓
25 10 31.7 30.9 30.7
25 10 10 30

30.6 ✓ 30.7 ✓ 30.7 ✓ 30.9 ✓
50 28 10 31.2 30.4
50 28 10 10 50

on hub & Alley Block 255 & East Line Events

NWBP Garnet & Everts

check on Elev. Means Now O.K.

Alley Block 255
Cont'd

2+50 Beg Conc Apron on Lt. - 10.1

32³ 32⁰⁰ 31⁷² 30⁹ 30⁷ 30³
 20 149 104¹⁰ 10 25
 Gr. floor Apron

2+49 Power Pole #A1252 91 Rt

2+00 - 10' Lt. = end Conc walk

32⁶³ 32⁶⁸ 32⁶ 31⁵ 31⁵ 30⁹
 10 = Cor. walk on Conc 15 10 10 25

1+94.75 & 3.5 Conc Walk 10.0 Lt

32⁸⁵ 32⁶⁹
 15 10
 Walk

1193 End Conc Apron 10' Lt
 + Beg. Conc. walk

33⁴ 32⁷²
 154 10
 floor Apron + walk

1+59 Beg Conc Apron & Gar. on Lt

33¹⁸ 32⁶⁹
 15.4 10
 floor Apron

1+50

32⁷ 32⁶ 31⁹ 31⁵ 31²
 25 10 10 25

4+99.80
~~5+00~~ West Line Farnel
 Beg. Conc Paving & Cbs.

4+90
 4+79 - 10.5' Lt. = end fence ✓

4+50
 4+31 - 10.2' Lt. = Beg. Picket fence ✓
 4+26 - 9.4' Rt. = ± P. pole # P.A. 1282 ✓
 + 15.2' Rt. = end Row of Gar.

4+24 - 10.7' Rt. = Nly of 8" Conc wall to Gar. ✓

4+10.5' Double Garage, conc. fl., on Lt.

10.9' Lt. = end wall

4+00 - ~~Corner Lot # A1282~~ 7.4' Rt. = no ed.

+ 15' Rt. = Beg. Row of Gar. - Conc. floor

3+56 - 10.2' Lt. = Nly of 8" Conc wall

3+50 - 10.8' Lt. = Beg. 8" Conc. Block wall - 6' High

T.P. 31.11

3+00 End Conc Apron on Lt. - 10.4'

2+78 = Brk. in Conc. apron ✓

2+73 = Brk. in Conc. apron

31.75 31.36 30.90 31.06 31.26
 10 10 10.1 10.1
 Cb. C Cb
 $\frac{31.2}{10}$ 31.0 $\frac{30.9}{10}$

30.4 30.3 30.0 30.0 30.5
 25 10 10 25

30.25
 11.2 floor
 30.0 30.83 30.89
 10.7 10.7 15.2 = floor
 gr. Top wall

30.5 30.0 29.9 30.6 29.5 29.8 30.89
 25 10.9 10 10 8.6 15.1 = gar floor
 wall

30.3 29.9 29.9 30.2 30.75 30.80
 25 10.8 10 10.2 10.2 15 = floor gar
 29.2 29.2 29.2
 10 2.5
 about Bottom of footing

31.35 31.01 30.30 29.9 29.5
 14.9 10.4 10 25
 floor Apron
 31.09
 10.3 edge Conc.

31.43
 10.2 = edge Conc.

2

BM. 4564 (4560) 2.11.7' L&T Garnet & Fanuel
 TP 38.76
 T.P. - Used for BM. 30.85 2 L&Disc 5107.04

5140.04 2 Fanuel

32⁷⁶ 31⁸³ 31⁶⁶ 31⁴⁷ 30⁷¹
 50 10 10 70

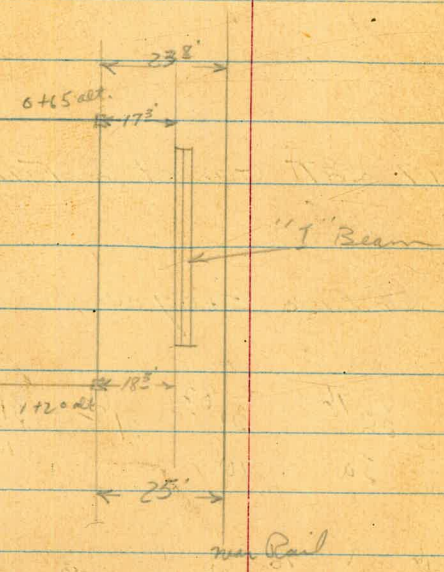
5120.04 West Ch line Fanuel

32⁷⁶ 31⁸³ 31⁶⁶ 30⁹⁰ 30⁷³ 30⁵⁴ 30⁵⁰ 31⁴⁷ 29⁹⁶ 30⁶⁰
 50 50 12 12 10 10 12 12 50 50
 Ch G G G 10 G G G G G G

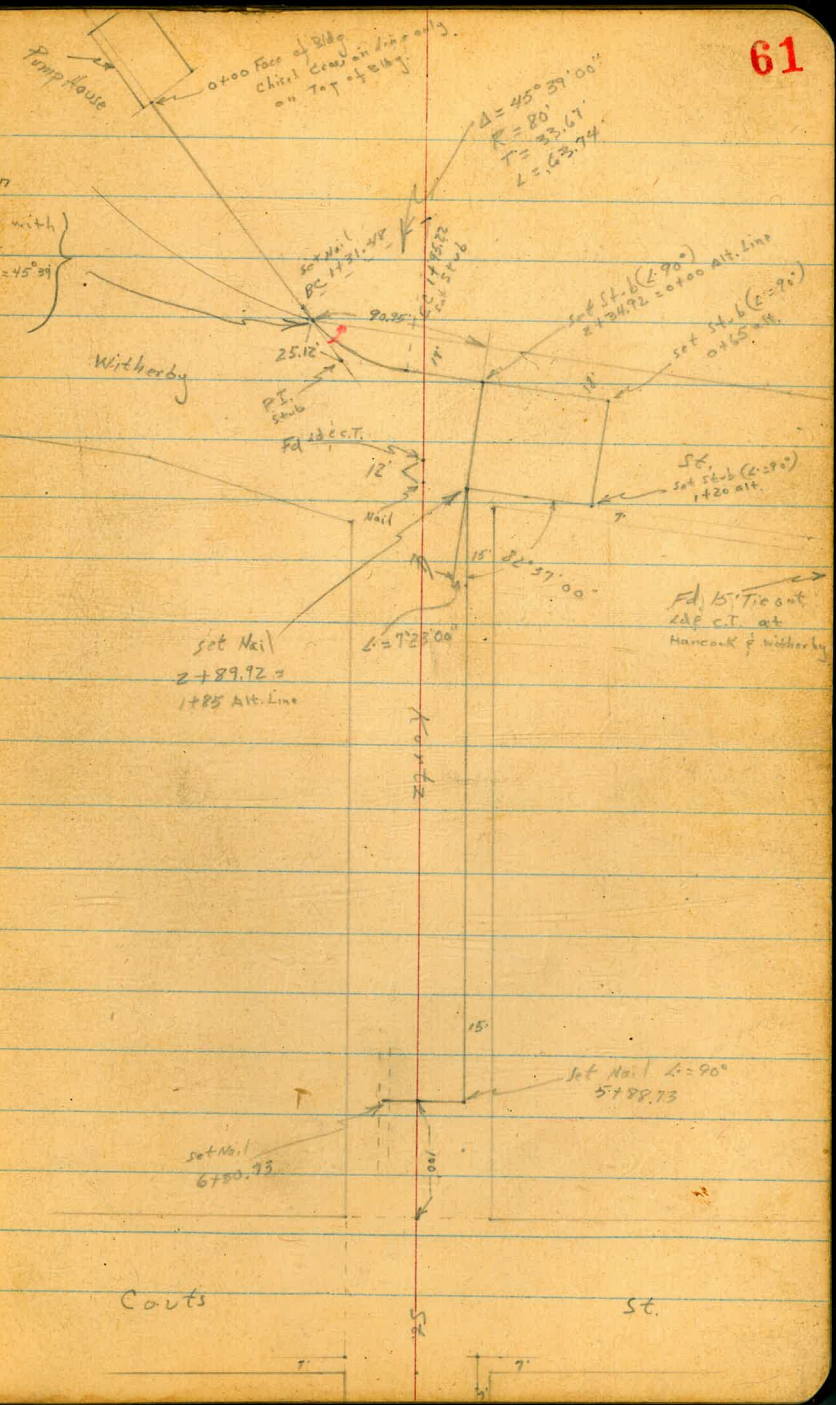
Roberts
Cota
Moore
Fisher
July 30, 1951
W.D. 20786

Survey For Replacement of Pressure Line
From Witherby St. Sewer Pump Station
to Kirtz Street

INDEXED
AUG 2 1951



Prolongation
Property line with
semi Tangent
to curve at
set stub
 $\theta = 45^\circ 39'$



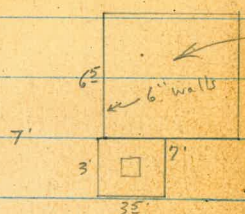
0+48^c

65

4

5.7
5.3
1.1
7.3
10.6
Top of Tank

0+42^l 7' Rt to Pit

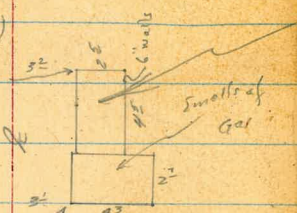


Top of Another Tank

0+33

18' 24" Egin Cradle (No tank)

3' Rt to Corner pit



More pits in this Area

5.3
7.8
4.3
Top of Tank

0+26.6

3' Rt to Corner Pit 0.4' Walls 4' x 2'

0+07^E

21' 90'

8' Chain Link & 3 barbed Fence & conduits hung on Fence

0+00

Face of Bldg

5.2
1.32
AC

5.5

0.90

-14.33

Top of Outlet Pipe inside Pump house

10.09 Floor

25.32
Top of outlet pipe where it enters side of Bldg.

T.P. 5.28 10.99 2.87 5.71 2 1/2" x 12" Tr. out of 7' 5' 10.99

BM 6.11 8.58 2.47 LA & DIS TANK Cmts & S.L. Kurtz

1738 E Hits Fence & Leaves AC. Pav.

1731.48 BC

6.0
5.0

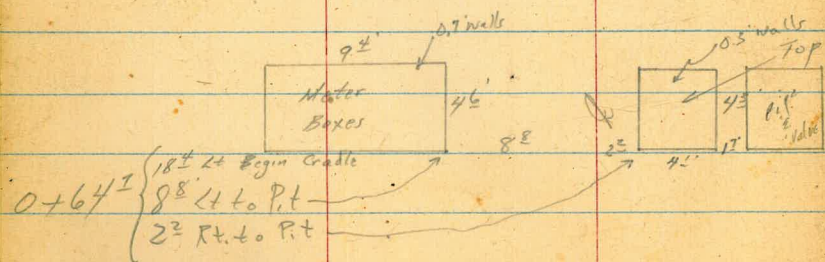
17253 7th R to Fence
2nd R to Center Pole (Not Used)

1700

5.8 5.8 5.9
5.2 5.2 5.1
1.0 1.0

0+95 16th R to Fire Hydrant

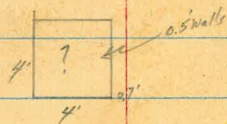
0+85 18th Lt END CRADLE



5.7 3
5.3 7.7
4.3
Top of Tank

0+53 18th Lt END CRADLE

0+57 0.7 Lt to Pit



10.99π

10.99π

1+77 5¹ Rt to Center Guy Pole

1+73^E 4¹ Lt to Deadman

1+72 10³ Lt to Deadman

1+70 15¹ Lt to Fence

1+64 10¹ Rt (Approx.) to Angle pt. in Gas Lines

18¹ Rt Back Edge Cot. Wall 15' thick

1+60 11² Lt to Fence

1+50 7¹ Lt to Fence

1+40 11¹ Lt to Fence

T.P. 482 10.53 π 5.28 5.71

10.99 π

5.5

5.0

5.9

5.6

5.7

2.09

4.6

4.9

5.2

2.44

11.2

3

10.7

TOP

Wall

5.7

5.6

5.5

4.8

4.9

5.0

7.1

Edge

Back

5.7

5.6

4.8

4.9

10

Edge

Back

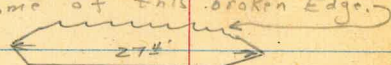
10.53 π

(Alt.) 53 RT to Back Edge Rot. Wall (15' thick at top)
 0+26 47 RT to Point of Abutment

Lt	2	Rt
K.9	6.2	K.6
4.6	4.3	5.9
183	6	8.02
Fence		5.3

0+13 (Alternate Line)

E hits some of this broken Edge.



b.6
4.9

183 Lt to Fence (25 RT to Abutment)
 2+34.92 $\angle 90^\circ$ RT = 0+00 Alternate } Back Edge is badly broken.

5.1	K.6
4.8	5.9
183	

2+32.6 27 RT to Center T. Pole #458006

1+95.22 EC 183 Lt to Fence

5.1	5.9	7.13
4.8	5.1	8.40
183	Edge Bank	5.6
		Back Edge Wall

1+92 7.4 Lt to Center Tele. M.H. Line Lick

1+90

b.5
5.0
Edge Bank

1+80 17.4 Lt to Fence

5.1	5.2	7.12
4.8	5.3	8.41
172	Edge Bank	7.0
		Back Edge Wall

10.53 RT

10.53 RT

Cont'd From Page 66

Lt

E

Rt

67

(212)
1741

3.5 7.0

(214)
1734

8.5
2.0

(214)
1720 L. Rt 90°

8.6
1.9

(214)
17131 Leaves Conc. Abutment

9.2 9.44
1.3 1.09
Grp Top
Abut.

(214)
17122

9.33 9.44
2.20 1.09
Step Top abut.

(214)
17102

8.33 5.29
2.20 5.29
Step Step

(214)
17072

2.15 5.24
12.68 5.29
Walk Step in abut.

10.537

10.537

Contd From Page 67

2+70³

2+42 E Leaves Top Abutment

2+39 I 2' Pt to Point

2+37⁵ G Hit Abutment (Broken Back Edge)

(A14)
1+85 END Alternate Line = 2+89.92

(A14)
1+78 Edge A.C. Pav.

(A14)
1+70

(A14)
1+63

10.53A

Lt

14.89
15.42 Road
14.57 Curb
-4.04

68

1.2
3.3 Top
15.56 Road
2.52
8.01
Top of
Ret. Wall

4.3
6.2 GED
1.2
3.3 Top
abut

3.28
7.05

3.5
7.0

4.1
6.4

4.3
3.2

10.53A

Cont'd From Page 68

3+50

3+05

3+00

2+89.72 L. Lt 7°23'

2+79.2 29° RT END RET. WALL

2+78

2+72

10.53 A

Lt.

E

Rt

69

7.0
3.5

7.1
3.4

3.8 3.7 3.0

6.7 6.8 7.5
6
Approx
Edge A.C.
10

7.05
3.48

5.68 2.8
4.85 7.7
TOP Ret. wall GRD

11.60 4.85
walk TOP Ret. wall
1.07 5.68

14.57 11.59
Curb walk
1.04 1.06

10.53 A

5+00

4+89[±] 15' Lt Begin Bldg.

4+68 4.7' Lt to Center T. Pole # 458005H.

4+50

4+00

3+93

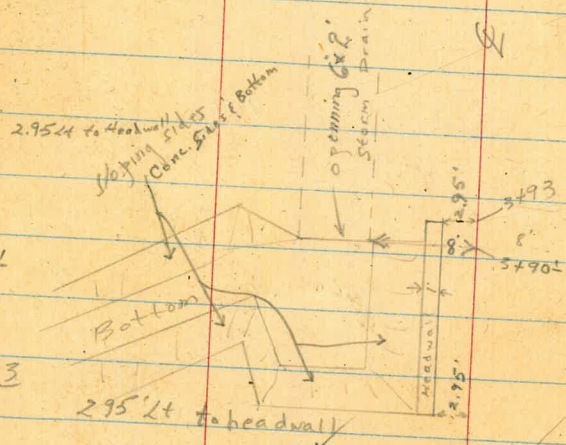
3+90[±]

3+75[±]

T.P.

3+50[±] 35' Lt to Center T. Pole # 450619H

10.53x



Lt

Rt

Rt

70

4.0 3.0 3.3
4.4 5.4 5.1
10 10

3.0
5.3

3.1
5.0

1.26 1.31 4.0 3.8 3.6 3.6
7.06 7.72 4.41 4.6 4.8 4.8
8 8 2.75 2.95
Top Invert Top GRD
Drain Storm Wall
Drain

8.41x

Cont'd from Page 70

check 5.15 2.46 = 2.47

6+30.73 END Over Existing Pressure Line (no hope)

6+11.33 Sewer line Crossing

5+88.73 L. Rt 90°

5+84.2 42' Lt to Center T. Pole # 45800 4H

5+65 15' Lt End Bldg.

5+50

5+41.8 95' Lt to Edge MH of Storm Drain
25' x 25' inside 0.5' walls

8.41 X

Lt

Rt

Rt

71

2.2
62

1.41
7.00
59
INVERT
MH
(Not used)

2.9
55

0.65
7.76
140
INVERT
MH
(Active)

1
2
57

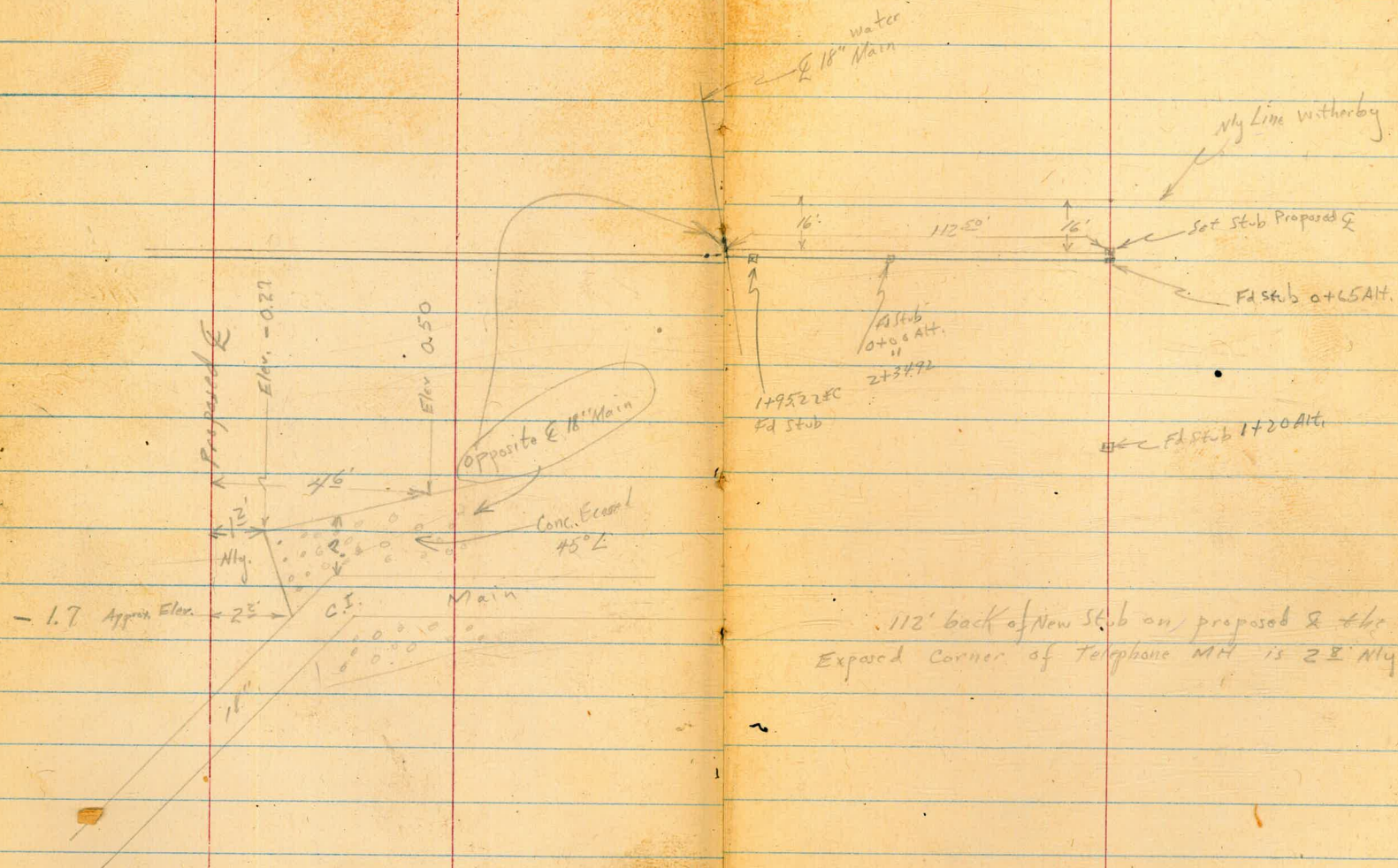
5.5
49

8.41 X

Roberts
Cota
Moore
Bullen
Oct 4, 1951
no. 20766

Location of Existing 18" water
Main for Proposed Withersby St.
Pressure Sewer.
See Page 61 This F.B.

72



Roberts Levels of Ground for Location of
Oct 4, 1951 Proposed 8" VC Vent From Junction Box.

Nly. Edge 15' Conc. Retain. Wall used
as Q for levels.

Q RT 73

0+66.3 Top about 7.3

0+43 0.5' Rt to Deadman

0+40.5 Top about 7.4

0+37.1 H.t. about 2.5 6.3
12

0+14.6 Leaves About 2.5 5.2 5.2 8.5 7.1
0.75 0.75 12
GRD

0+00 Where Alternate Line Crosses
Nly. Edge 15' Conc. Ret. Wall 5.2 5.2 8.4 8.4 7.7
0.75 0.75 2.75 2.75
GRD

BM Dired Elev. Rod used 5.71 12' Tie out of T. line witherby & Q Karte See pg 62

2+03 9^s Rt center P. Pole # 31472+00^E 3^s Rt center T. Pole # 460898H

2+00

2.1 5.3 5.8
6 11^s
Fence1+99^E 1^s Rt to Deadman

1+50

2.1 5.6
7

1+24 2' Rt center Guy Pole

1+16² BC of Wall Going around curve on
25' chords2.1 5.2
61+0⁰2.1 2.9 5.7
3 70+87⁴ Step in wall

2.5 2.1

0+67^E 3' Rt center T. Pole # 458006H

0+66.9 Leaves Abut.

2.5 5.2
8

3+09^E 4⁸' Rt \angle Fence

2+99 3³' Rt center P. Pole # 4104

2+85^E 4⁸' Rt \angle in Fence

2+75^E \angle in Ret Wall

2.1 5.9 5.9
7 7
Fence

2+74 1²' Rt to Deadman

2+67 1⁴' Rt center T. Pole = 460899H

2+50

2.1 5.8 5.8
7 8
Fence

2+39 2³' Rt to Deadman

2+28 EC of Ret Wall

2.1

Cont'd. From Page 75

F R

76

3+15² Edge Ret. Wall 7th to Bldg.

2.1 -1.6
top on
wall walk

3+14³ L in Ret Wall

2.1

	Levels 10' cbs 25 parking	Southerly 5' walk	Imperial	St Cb Line cont from p 42	
740			141 ¹²	780	136 ⁴⁰
720			141 ⁵⁰	760	137 ¹⁸
5700			141 ⁹³	740	138 ⁰⁰
780			142 ¹²	720	138 ⁶⁸
760			142 ⁴¹	6706 & Fire plug	
740			142 ⁵⁸	6700	139 ⁴⁴ cb
720			142 ⁷²	5794 & Bus stop sign	
7400			142 ⁸⁹	780	140 ¹⁰
3750			143 ²⁵	5777 1' cb Broken box drain ditch	140 ³⁰ cb
3731 ⁴ end old cbs begin new			143 ⁴³		139 ⁶⁶ 75 12 14' cbs end AC ditch
			cb elev.	5760	140 ⁶² cb elev.

Same BM as on p 42

INDEXED
Lee
JUN 18 1952

+40	125 ⁵²
+20	126 ⁴⁷
9+00	127 ³⁷
+80	128 ²²
+60	129 ⁰⁴
+40	129 ⁵²
+20	130 ⁶¹
8+00	131 ⁴⁵
+50	133 ⁵⁰
7+00	135 ⁶² cbclv

11+19 ²	117 ⁵⁸ 3' EC Ret	117 ⁶⁶ 10' cnd c6 alley
11+16 ² BC 3'c6 Red Ret.	117 ⁶⁶ BC 3' Red	
11+00	118 ²¹	
+80	118 ⁹⁵	
+60	119 ⁷⁶	
+40	120 ⁶³	
+20	121 ⁵¹	
10+00	122 ⁵²	
+80	123 ⁵²	
9+60	124 ⁵¹ cbclv	

EL 5± B.C. to P.H.

EL 2.5 B.C. to Abs⁺

use AIT line not ~~away~~

29.29
10.83
18.46

1315
65
1250

511
246
265

0.43
359
910
812

10.34
630
16.64

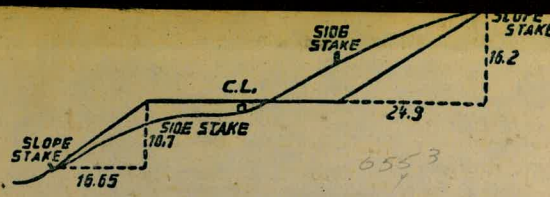
10.77
10.09
20.86

16.64
10.09
26.73

16.77
909
25.86

2532

+ 0.43
- 10.77
+ 13.59
- 9.89
+ 4.10
- 2.69



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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