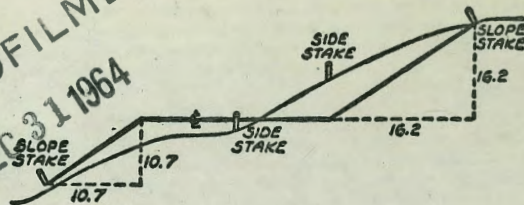


2048

DATE 1942

MICROFILMED  
DEC 31 1964



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if out, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

INDEXED

through page 62

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

See Page 1

Waverly St.

27

Electric Ave

45

INDEX

1

<u>Page</u>	<u>Description</u>
2-9	Proposed storm drain in Buena Vista Tract
10	X-sec Alley 234 P. 13,
17	Const. 42" Storm Drain Archer & La Jolla Mesa Dr.
27	X-sec. Waverly St. - Calmar to Midway
45	X-sec. Electric - Gravilla to Bon Air
52	
56	X-sec. Hilltop from 47 <sup>th</sup> East to gulley
60	Drainage survey, Lot 9, BIK. D. StarKeys Prospect Park
64	Levels curbs E. side 55 <sup>th</sup> from Monteguma Rd. to N. L. of Sub.
67	Alley BIK. F. University Heights - X-sec. for paving

9-6-49  
 Hendricks  
 Roberts  
 Greer  
 Bunch  
 W/O# 20565

Proposed Storm Drain  
 Buena Vista Dwg. 7744-L

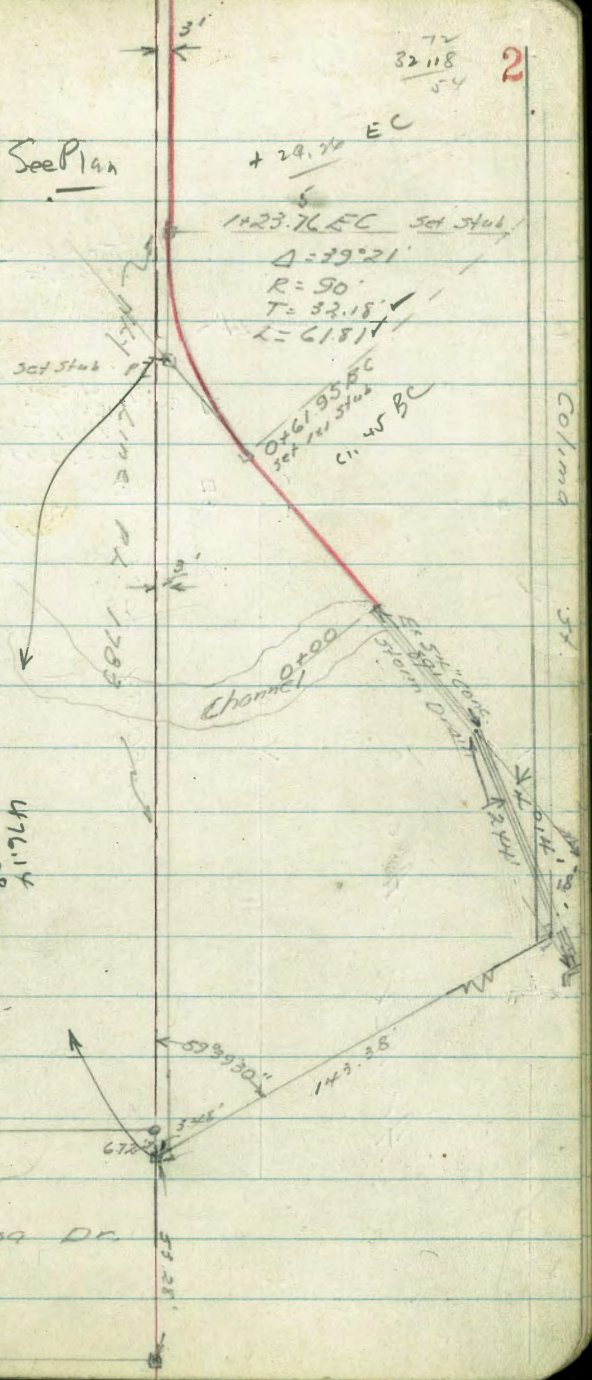
INDEXED  
 Y.K.  
 SEP 16 1949

41.86  
 204.83  
 32.18  
 278.87

ER = 91.7  
 T = 32.68  
 L = 62.08  
 BC = 0461.95  
 62.18  
 1724.28 = EC

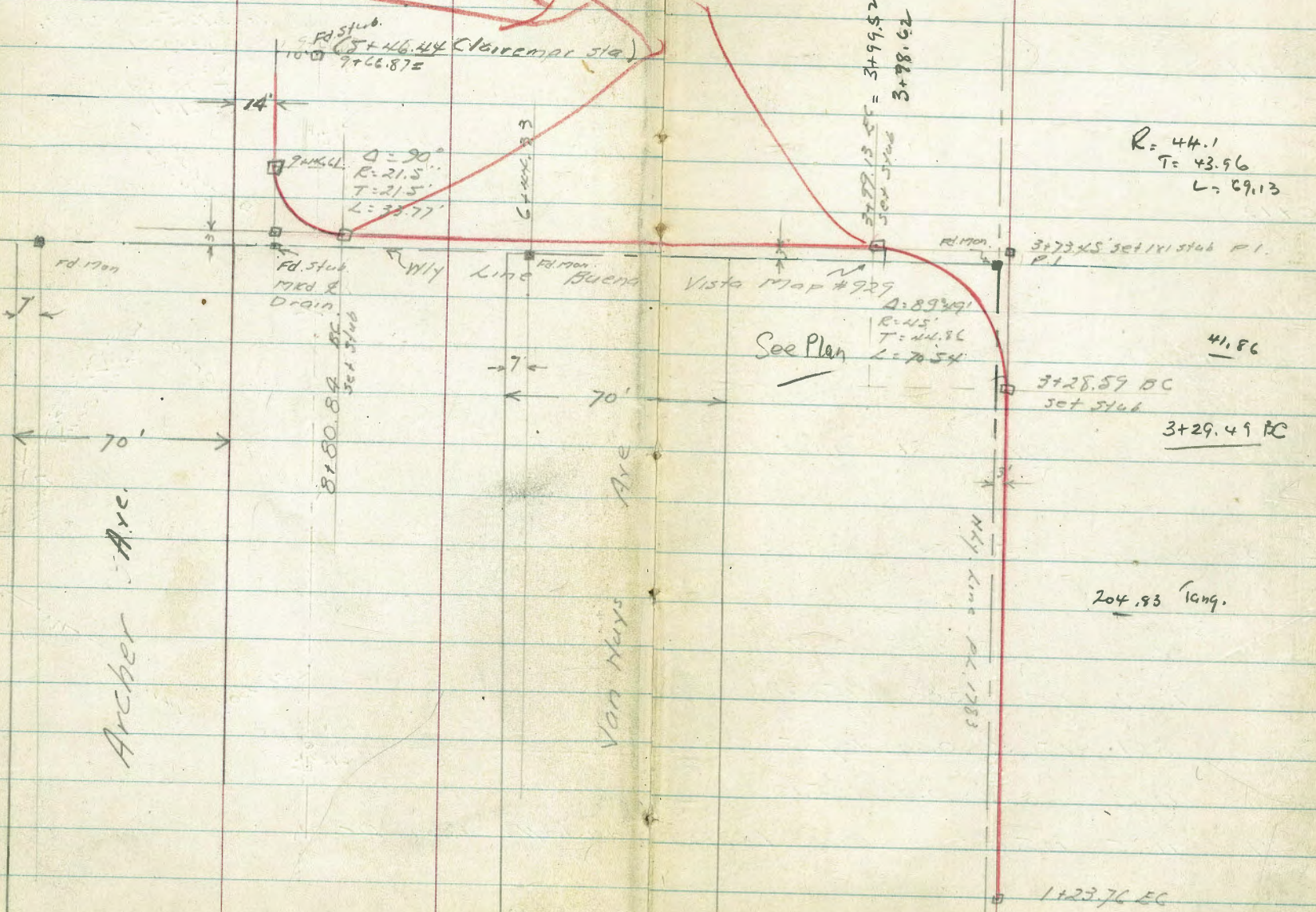
476.14  
 10.28  
 486.42  
 278.87  
 207.55  
 613.4  
 200.11

See Plan



La Jolla Mesa Dr.

Moved 2' w/ly



Fd. Stud. 10' 5+46.44 (Claremont Sta.) 7+66.87E

2 W.K.L. D=90' R=21.5' T=21.5' L=33.77'

3+79.13 EC = 5+99.52 Turn - 3+78.62 EC Turn.

R=44.1  
T=43.96  
L=69.13

See Plan

A=89.49'  
R=45'  
T=44.86  
L=70.54

41.86

3+29.49 EC

204.93 Tang.

1+23.76 EC

Archer Ave.

Von Nixs Ave

Vista Map #929

WVY Line

Fd. Stud. MKD & Drain

Set 1st Stud P.I.

3+28.59 DC Set Stud

3+73.45 Set 1st Stud P.I.

7'

70'

14'

6' max. 3'

8+80.82 DC Set Stud

rd. 1700

rd. 1700

Levels Proposed Storm Drain  
Buena Vista

0+17

145.5 146.6 148.4 146.7 149.9 149.9 152.0  
17<sup>3</sup> 16<sup>3</sup> 14<sup>5</sup> 14<sup>3</sup> 13<sup>0</sup> 13<sup>0</sup> 10<sup>9</sup>  
37 28 8 3 7 13

0+13

143.4 148.5 149.4 148.6 148.7 150.0 150.5 152.5  
9<sup>5</sup> 14<sup>4</sup> 13<sup>5</sup> 14<sup>3</sup> 14<sup>3</sup> 12<sup>9</sup> 12<sup>6</sup> 10<sup>5</sup>  
42 18 9 6 3 8 13

0+00 Outlet Ex 54" Conc. Pipe

153.5 150.1 150.0 149.1 158.9 147.4 150.6 152.4  
9<sup>5</sup> 12<sup>8</sup> 12<sup>9</sup> 13<sup>5</sup> 15 20 12<sup>3</sup> 9<sup>7</sup>  
29 14 5 3 FL 8 16

T.P. 1.55 162.91 12.59 161.26

162.91 ✓

+ 333' Inlet of Ex 54" Conc. Pipe

12.58 161.41

T.P. 9.25 173.95 0.45 164.70

173.95 ✓

T.P. 12.77 165.15 3.88 152.38

Top Ex 54" Conc. Pipe

T.P. 8.61 156.26 0.68 147.65

T.P. 13.23 148.33 0.03 135.10

B.M. 11.85 135.13 123.28

Cont. from E. Line Mission Blvd. to 7' Line Archer  
(FB 1715 P. 62)

Levels Storm Drain  
cont'd

1123.76 B.C.

141.9 142.0 142.2 142.3 142.4  
85 84 82 71 73  
10 5 7 15

0+61.95 B.C.

146.4 146.2 147.1 147.1 147.4  
20 22 34 33 22  
30 16 9 17

0+47

146.6 147.9 147.9 148.7  
38 25 25 17  
22 7 18

TP. 0.16 150.41 1266 150.25

150.41 ✓

0+41

146.7 150.1 150.4 150.6 149.4  
16 12 12 12 13  
22 6 8 17

0+30

148.8 149.5 151.1 150.9  
14 13 11 12  
20 6 15

0+25

148.3 148.1 149.1 149.4 151.4  
14 13 13 13 11  
21 11 6 10

162.91  
✓

162.91 ✓  
✓



Levels Storm Drain Cont'd

3+99.13 E.C.

1285.5  
5.9  
10

1288  
8.5  
10

1288.4  
9.0  
10

3+28.59 B.C.

130.4  
7.0  
10

130.0  
7.4  
8

130.1  
7.3  
8

3+00

132.1  
5.2  
10

131.5  
5.2  
9

131.8  
5.5  
9

2+50

2.8  
134.6

T.P. - 0.18 137.42 12.81 137.60

(Hail in fence R1 2+15) 137.42 ↓

2+00

137.5  
12.9  
10

137.2  
13.1  
10

137.2  
13.2  
10

150.41  
↑

150.41  
↑

Levels Storm Drain Cont'd.

7+00

6+50

TP 1.69 126.08 13.03 124.39

6+00

5+50

5+00

4+50

137.42  
↑

120.1  
60  
10  
119.9  
60  
10  
119.1  
70  
10

7

122.1  
120

126.08  
↑

124.8  
125  
10  
124.2  
13  
10  
123.4  
14  
10

120.5  
119

121.3  
10  
10  
121.0  
10  
10  
120.9  
11  
10

128.3  
9

137.42  
↑

Levels Storm Drain  
Cont'd.

9+14.61 EC.

110.2 111.1 111.6  
15.4 15.0 14.5  
10 12

8+80.84 BC.

114.5 113.0 112.1 111.5  
11.6 13.1 14.0 14.6  
10 5 10

8+50

113.1  
13.0

8+00

115.6 115.3 114.9  
10.5 10.8 11.2  
10 10

7+85 Sewer M.H. 4' H.

110.19 116.21  
15.87 9.87  
4 4  
F.L. Rim

7+50

85 117.5

126.08  
✓

126.08  
✓

Levels Storm Drain  
Cont'd.

B.M.		3.30	127.29 (123.28)
T.P.	7.22	126.59	6.71 119.37

Cont. Mon. E line Mission Blvd. 50.7' line Nether

(5 + 46.44 = Clarence sta.)  
9 + 66.87 =

126.08  
X

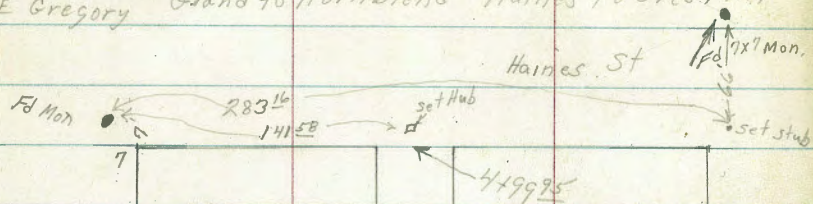
Notes Reduced. 9-12-09

108.19  
17.30  
10  
(on stub  
Mkt C 8.19)  
126.08  
X

D. Smith  
W Moore  
J Clark  
E Gregory

X Sec. Alley BIK 234 Pacific Beach  
Grand to Hornblend Haines to Gresham

W<sup>o</sup># 25020  
9-30-49 10



INDEXED

W. K.  
OCT 3 1949

notes Reduced &  
Plotted Profile 4045  
McClaren 10/1/49

Hornblend.

X  
BIK 234

Grand Ave



40

X Sec Alley BIK 234

Pacific Beach

10' Lt SW cor double garage con floor apron  
0726 11' RT NW cor 3 car garage con floor apron

NE

0700 11' RT NW cor 3 car garage con floor apron

0700 10' Lt SW cor Double garage con floor apron

0700 East Prop Gresham

0-07 10' Lt 2' cor walk end 3' rail fence

0-125 10' Lt Begin 3' rail fence

0-15

0-23

0-40 2 Gresham

TP 41<sup>6</sup> 50<sup>44</sup> 753 46<sup>28</sup>

BM 139 53<sup>81</sup>

52<sup>48</sup> SW 9' Lot  
Barnet  
Gresham

WA 25000

Lt = North

RT = South

11

46.79	46.43	46.2	45.9	45.9	46.00	46.22
365	401	42	45	45	444	422
12	10	10	10	10	11	13
Floor	Apron				Apron	Floor
46.80	46.39	46.0	45.6	45.4	45.83	46.11
354	405	44	48	50	451	433
12	10	10	10	10	11	13
Floor	Apron				Apron	Floor

76.39  
405  
102  
walk

46.4	45.6	45.1	45.0	44.6
40	48	53	54	58
50	10	10	10	50
45.51	44.9	44.8	44.6	43.9
49	55	55	50	65
50	10	10	10	50

45.6	45.1	45.14	44.8	44.2
45	53	530	56	62
50	10	10	10	50
		11/11		
		11/11		

50<sup>44</sup>

cont.

1+26 9° Lt SE cor garage

1+21 4 1/2 Lt E con apron to garage

1+08 9° Lt SW cor single garage

1+04 9° Lt E 2' con walk

1+00 9° Lt End Board fence Begin stucco fence

0+76 8 1/2 Lt begin comb fence + bldg

0+73 5 9° Lt E tel pole # 464034 H

0+67 5 8° Lt E single garage con floor + apron

0+50 9° Rt E Power pole # 1410

0+48 5 11° Rt E 3' con walk

0+42 11° Rt E laundry room con floor

12

LT	RT
48.67	47.96
177	248
92	46
Floor	Apron

47.68				
276				
92				
walk				
47.6	47.5	46.9	46.9	47.0
28	29	35	35	35
20	10	10	10	20

47.74	47.07		
220	337		
127	82		
Floor	Apron		
46.7	46.7	46.4	46.3
33	32	40	41
20	10	10	10

46.56
358
115
walk
46.51
392
115
Floor

5044

cont

2147 Lt SF cor double garage con floor + apron

2127 Lt SW cor double garage con floor + apron

2100

TP 12<sup>98</sup> 62<sup>49</sup> 087 49<sup>57</sup>

1+75 10<sup>2</sup> Lt End 6' Board Fence

1+627<sup>2</sup> Rt E power pole JPA # 1430

1+50

1+33<sup>5</sup> 10<sup>3</sup> Rt E 1/2' com walk

1+26 10<sup>4</sup> Lt Begin 6' Board Fence

Lt

E

Rt

53.21	53.17					
928	932					
13 <sup>0</sup>	10 <sup>2</sup>					
Floor	Apron					
53.19	52.47					
930	10 <sup>02</sup>					
13	10 <sup>2</sup>					
Floor	Apron					
	50.5	50.4	50.3	50.2	50.2	
	12 <sup>0</sup>	12 <sup>L</sup>	12 <sup>3</sup>	12 <sup>2</sup>	12 <sup>3</sup>	
	20	10	10	10	20	

62 49

49.0	48.9	48.3	48.2	48.1	
14	15	21	22	23	
10	10	10	10	20	
					48.02
					242
					103
					walk

50 44



cont

4700 9<sup>30</sup>LT Begin 5' Rail Fence  
4700 9<sup>20</sup>LT End Fence 5' Board  
47

3750

3734 9<sup>40</sup>RT & 3' cen walk  
3734 9<sup>20</sup>LT Begin 5' Board Fence

3717 7<sup>30</sup>RT & power pole JPA #1456

3700 10<sup>20</sup>RT Begin 5' Board Fence

2775 8<sup>50</sup>LT & tel pole #464037H

2775 9<sup>00</sup>RT End 4' huth fence

2755 9<sup>40</sup>RT Begin 4' huth fence

2750

14

LT

E

RT

59.1 58.8 58.3 57.5 57.7  
34 32 42 50 52  
20 10 10 20

57.9 57.5 57.0 57.0 57.2  
46 50 55 55 53  
20 10 10 20

56.51

598

94

walk

55.5 55.2 54.8 54.9 55.1  
70 73 72 76 75  
20 10 10 20

53.4 53.3 52.88 52.7 53.0  
91 92 96 98 95  
20 10 10 20

6249

cont

ht

15

5122

61.1	60.0	59.5	60.1	59.0
62	72	72	72	82
50	10	10	10	50

4199<sup>25</sup> west Prop Haines

61.4	60.7	60.4	59.6	59.6	58.7
58	65	68	76	76	85
50	14	10	10	10	50

TP 769 67 <sup>19</sup> 299 59<sup>50</sup>

6719

4190 7° RT & anchor line r

4175<sup>85</sup> H & tel pole # 464038H

60.4	60.3	59.7	59.5	59.1
24	28	28	29	34
14	10	10	10	20

4169<sup>65</sup> RT & power pole # JPA 1486

60.34	60.01
25	24
14	10
Floor	apron
60.34	59.99
25	25
14	10
Floor	apron

4167 10° Lt SE cor double garage con floor 2 apron

59.4	59.1	58.7
31	34	38
10	10	20

4150 10° Lt SW cor double garage con floor 2 apron

4150 10° RT End 5' Board fence

4150 2° Lt End 5' Rail fence

6249

cont

LT

Σ

LT

16

BM starting page 16 17<sup>25</sup> 52<sup>43</sup> 50<sup>42</sup>

TP 2<sup>83</sup> 69<sup>67</sup> 0<sup>35</sup> 66<sup>84</sup>

5439<sup>85</sup> E. Haines

5431

60.5	59.6	59.4	59.1	57.8
62	76	78	81	94
50	10	10	10	50

60.0	59.2	59.0	58.8	57.3
73	80	83	84	99
50	10	10	10	50

67<sup>19</sup>

CONST. 42" Storm Drain  
 W. end Archer St. N Ly  
 and Ely to La Jolla Mesa Dr.  
 Acct. 2 - S.M. Holes, Moved Line  
 2' W Ly, Archer to St. Bird Rock Add.

0 + 33.77 F.C.

INDEXED

W.K.  
 NOV 21 1949

0 + 16.88 E curve

0 + 15.17 Ctr Spec. C.B.

0 + 00 B.C. Lt. Reversed Sta.  
 9 + 12.01

TP	6.37	<u>118.74</u>	1200	112.42
BM.	114	124.42		123.28
PER PLAN				

NOTE: 7' Mon. at S. side  
 Archer St Ref. ELY  
 25' = 2 x 2 Hub, check  
 SET CUTS 7' FT.

MOORE  
 SHERRILLAN VVO. 20565  
 Crawford 7758 L  
 11-9-49

17

Record sheet  
 on tie sheet  
 ALSO P. 19 & 25

INV.  
 103.95  
 14.79  
 5.77  
 C 9.02

NOT SET

TOP GRATE  
 15' off/set

110.70	103.39 = PLAN
8.04	15.35
5.98	5.98
C 2.06	C 9.37

15.67  
103.07 → INV. 0 + 00  
 15 x 42" Pipe

118.74  
 H.I.

1750

$$\begin{array}{r} 107.24 \\ 11.30 \\ 1.75 \\ \hline C 9.55 \end{array}$$

1725

Near S.M.H.

$$\begin{array}{r} 106.69 \\ 12.05 \\ 2.65 \\ \hline C 9.40 \end{array}$$

1700

$$\begin{array}{r} 105.74 \\ 12.80 \\ 3.90 \\ \hline C 8.90 \end{array}$$

0775

$$\begin{array}{r} 105.19 \\ 13.55 \\ 5.04 \\ \hline C 8.51 \end{array}$$

0750

118.74

$$\begin{array}{r} 104.44 \\ 14.30 \\ 5.56 \\ \hline C 8.74 \end{array}$$
118.74

2 + 75

2 + 70.5 = 5' W of 7' Mon. H. R. P. <sup>2x2</sup> 25' Ely of  
at S. side of Van Nuxs <sup>CON. MON</sup>

+ 50

+ 25

2 + 0.0

T.P.

5706 175

1253

130.52

0.75

117.99

1 + 75

118.74

11119

19.33

7.78

C 11155

11044

20.08

873

C 11135

10969

20.83

9.92

C 10991

10894

21.58

11.38

C 1020

130.52           = H.I.

10819

10.55

0.75

C 9.80

118.74

2 4 100

$$\begin{array}{r} 114.94 \\ 15.58 \\ 3.68 \\ \hline C 11.90 \end{array}$$

175

$$\begin{array}{r} 114.19 \\ 16.33 \\ 4.48 \\ \hline C 11.85 \end{array}$$

150

$$\begin{array}{r} 113.44 \\ 17.08 \\ 4.87 \\ \hline C 12.21 \end{array}$$

2 125

$$\begin{array}{r} 112.69 \\ 17.83 \\ 5.24 \\ \hline C 12.59 \end{array}$$

3 100

$$\begin{array}{r} 111.94 \\ 18.58 \\ 6.55 \\ \hline C 12.03 \end{array}$$
130.52130.52

5+15.8~ BC RT

4750  
T.P. 5' RT 11.54 140.11 195 128.57  
Wedge MH Riv

5+20 11-9-49 end staking

475

450 CUT on S.M.H. Top  
5' RT West Riv

4725

130.52

118.48  
21.63  
11.35  
C 10.28

140.11  
W

117.94  
12.58  
2.01  
C 10.57

117.19  
13.33  
2.06  
C 11.27

116.44  
14.08  
1.95  
C 12.13

115.69  
14.83  
2.82  
C 12.07

130.52  
2  
H.I.



C + 00

$$\begin{array}{r}
 121.46 \\
 18.65 \\
 9.42 \\
 \hline
 C 9.73
 \end{array}$$

S + 84.95 E C

$$\begin{array}{r}
 120.56 \\
 19.58 \\
 9.98 \\
 \hline
 C 9.57
 \end{array}$$

S + 67.66

$$\begin{array}{r}
 120.04 \\
 20.07 \\
 10.58 \\
 \hline
 C 9.79
 \end{array}$$

S + 50.38

$$\begin{array}{r}
 119.52 \\
 20.59 \\
 11.26 \\
 \hline
 C 9.77
 \end{array}$$

S + 33.10

$$\begin{array}{r}
 119.00 \\
 21.11 \\
 11.68 \\
 \hline
 C 9.43
 \end{array}$$

$$\begin{array}{r}
 120.11 \\
 \hline
 \end{array}$$

7+00

$$\begin{array}{r}
 127.43 \\
 12.68 \\
 \underline{.384} \\
 C887
 \end{array}$$

6+9145 Bink

$$\begin{array}{r}
 126.83 \\
 13.88 \\
 \underline{4.42} \\
 C886
 \end{array}$$

775

$$\begin{array}{r}
 125.96 \\
 14.15 \\
 \underline{5.34} \\
 C887
 \end{array}$$

750

$$\begin{array}{r}
 124.46 \\
 15.65 \\
 \underline{6.55} \\
 C910
 \end{array}$$

6+25

$$\begin{array}{r}
 122.96 \\
 17.15 \\
 \underline{8.32} \\
 C883
 \end{array}$$

7+7.5

11.84 151.20 075 139.36

7+50

90/0

7+41.45 BRK.

90/0

7+25 BRK.

80/0

7+10.45 BRK.

134.10

133.60

17.60

10.00

C 7.60

151.20

131.35

8.76

0.75

C 8.01

77

130.58

9.53

1.23

C 8.30

129.26

110.85

2.32

C 8.53

128.58

11.53

2.91

C 8.62

140.11

8 + 39.45

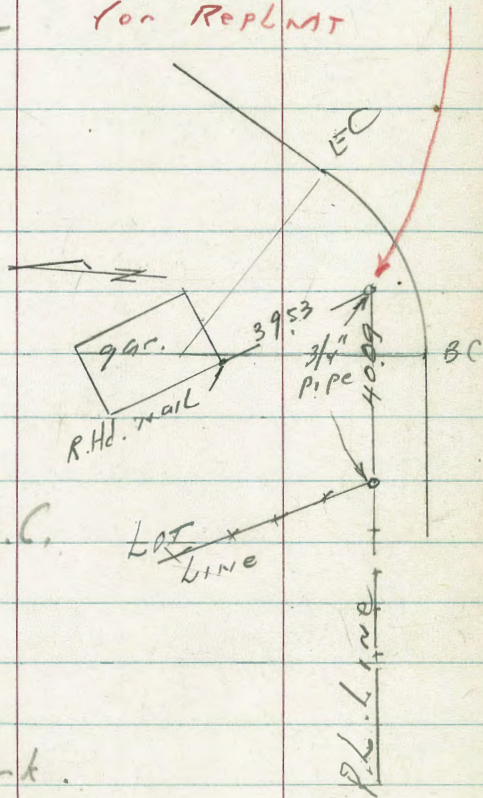
139.94  
 11.26  
 4.95  
 C 6.31

8 + 23.75

Record Pipe Log  
 for REPLMT

138.35  
 12.85  
 6.31  
 C 6.54

8 + 08.05



136.76  
 14.44  
 7.51  
 C 6.93

7 + 92.35 B.C.

LOS  
 LINE

135.17  
 16.03  
 8.88  
 C 7.15

7 + 91.45 Brk.

P.L. Line

135.08  
 16.12  
 9.00  
 C 7.12

151.20

Rod to top inside pipe

151.20	#1
40.66	
151.86	
151.91	
<u>        </u>	
.05	

Existing flow line  
9 + 16.5

inside Diam 147.41 see p 4  
~~14.50~~  
 Top inside — 151.91

9

146.06  
 5.14  
 1.33  
 C 3.81

8 + 75

143.53  
 7.67  
 1.34  
 C 6.33

8 + 55.6 E C

141.53  
 9.67  
 3.98  
 C 5.69

151.20

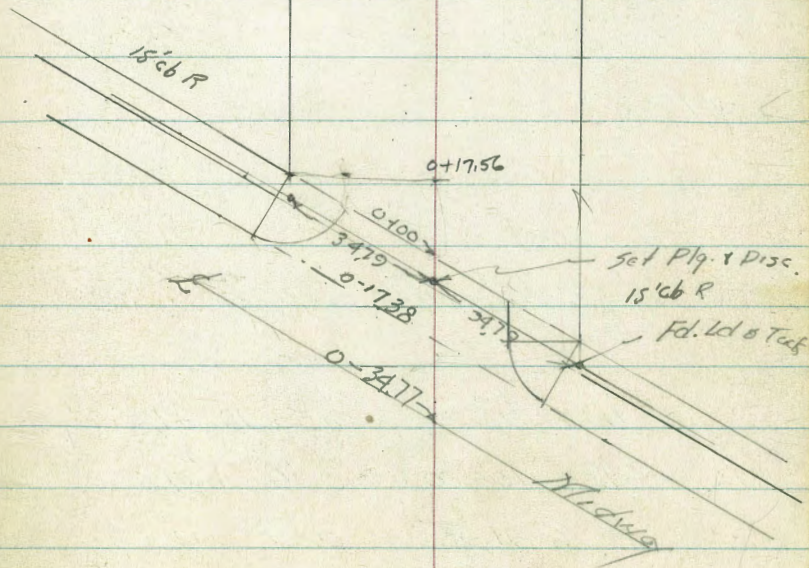
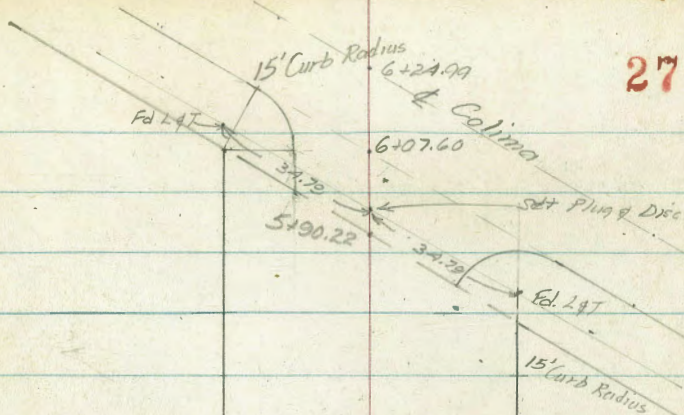
CROSS SECTION - WAVERLY AVE.  
 from Midway to Colima Sts.  
 140 31239

Walker  
 F. Gregory  
 G. Pope  
 R. Sisson  
 1-10-50

INDEXED  
 W.K.  
 JAN 12 1950

Notes Reduced by  
 Paul Tornheim  
 6/16/50

27



Waverly St. - Cross Sections

0-17.56 = Pt. to Prop. Car on Lt.

0+00 diag. Sec

0-17.38 Cont.

0-17.38

diag. Sec.

0-34.77 = Midway = diag. Sec on S. Midway

T.P. 11.32 113.79 0.53 102.47

T.P. 11.33 103.00 0.26 91.67

T.P. 12.76 94.93 0.68 79.17

8.05 79.85 71.80 B.M.

Lt. 110.86 110.0 109.3 108.7 108.2 108.7 108.5 108.4 28

2.93 3.8 4.5 5.1 5.6 5.1 5.3 5.4  
30 18 18 15 18 30 40  
on Walk on Walk on Walk on Walk

28.41 109.99 109.38 109.00 108.34 108.19 108.81 108.82

2.93 3.80 4.1 4.79 5.45 4.95 4.97  
34.76 198 198 174 174 34.76  
on Walk cb Gut. Gut. cb on Walk

59.16 107.65 6.14 5.55  
34.76 34.76  
Gut cb

110.51 109.61 109.61 109.06 108.57 108.10 107.10 105.81

32.8 392 423 475 522 563 583 523  
438 438 34.76 17.38 17.38 25.8 25.8  
cb & R. Gut Gut cb & R. return

112.07 109.55 109.11 108.81 108.30  
3.72 4.24 4.68 5.20 5.78  
34.76 17.38 Rim MH. 17.38 34.76

113.79

SEBP Midway of La Jolla Blvd.

Waverly St. - Cross sections

Lt.

Rt.

Lt.

29

1+50

108.9	108.6	107.9	107.3	106.9	106.3	105.5	105.9	105.4
2.6	2.9	3.6	4.2	4.6	5.2	5.0	5.6	6.1
40	30	18	15		14	16	30	40

1+35.5 - 30.7' Rt. 3' Conc. Walk

106.08  
105.85  
5.42  
30.7  
on Conc. Walk

1+09 - 30.6' Rt. End Conc. Curb for driveway

109.9	109.6	108.7	108.3	107.6	107.0	107.1	106.2
1.6	1.9	2.8	3.2	3.9	4.5	4.1	5.3
40	30	17	15		13	16	30

5.27  
30.6  
on Conc. Curb  
106.23  
106.10

1+00

1.6	1.9	2.8	3.2	3.9	4.5	4.1	5.3	5.5
40	30	17	15		13	16	30	40

14' gravel driveway

0+99.5 - 30.8' Rt. End Conc. Curb for driveway

5.07  
30.8  
on Conc. Curb

0+76.5 - 28.7 Lt. End 1' Wide Black Wall

0-05.0 on Cap Disc  
& Waverly  
TR

2.61 111.50 490 108.89

112.18  
111.32  
111.00

110.68 110.32 109.77 109.11 111.50

108.2  
107.5  
107.9  
107.9  
107.6

0+50 - 3' Conc. Walk on Lt.

161 247 292  
46 292 29  
Walk Walk Walk

311 347 402 4.7  
246 245 186 15  
Walk Walk on walk

113.79

113.79



Waverly Street - Cross Section

Lt.

\$

Rt.

30

2+50

107.9	107.00	106.3	105.9	105.7	105.3	105.5	104.7	104.4
4.1	4.5	5.2	5.6	5.8	6.2	6.0	6.8	7.1
40	30.0	19.0	16.0		14	16.0	30	40

2+43.4 - 28.8' Rt. End 7.5' Conc. Drive

107.72

107.33

105.10

104.75

2+35.2 - 30.0' Lt. 3' Conc. Walk

3.78	4.17
40	30.0
on Walk	on Walk

6.40	6.75
28.8	40
on Drive	on Drive

2+34.2 - 28.7' Rt. Begin 7.5' Conc. Drive

105.15	104.71
6.35	6.79
28.7	40
on Drive	on Drive

2+33 - 28.8' Rt. End 8' Conc. Drive

105.13	104.75
6.37	6.75
28.8	40
on Drive	on Drive

2+24.6 - 28.7' Rt. Begin 8' Conc. Drive

105.7	104.69
6.33	6.81
28.8	40
on Drive	on Drive

2+02.4 - 29.2' Rt. 3' Conc. Walk

108.7	107.9	106.7	106.2	105.8	105.6	105.16	104.84
2.8	3.6	4.8	5.3	5.7	5.9	6.34	6.66
40	30	16		13	20	20.2	40
						on Walk	on Walk

2+00

105.0	104.6
6.5	6.9
30	40

1+96 - 30' Lt. 3' Walk Conc

108.32	108.75
3.08	2.75
30	40
Conc. Walk	Conc. Walk

111.50

111.50

Waverly St. Cross Sections

3+60

Lt. 106.8  
4.7  
40

106.3  
5.2  
30

105.9  
5.6  
21

105.3  
6.2

3+50

104.8  
6.7

104.5  
7.1

104.7  
6.8

104.0  
7.5

103.6  
7.9

3+25 2 1/2' Conc. Walk 31.5' Lt.

107.18  
4.32  
40

106.78  
4.72  
31.5  
on walk

3+13.5 4' Conc. Walk 29.3' Rt.

104.34  
7.16  
29.3  
on walk

103.93  
7.57  
40  
on walk

3+04 Eucly. tree 20.5 Lt. ←

107.2  
4.3  
40

106.7  
4.8  
30

106.2  
5.3  
19

105.5  
6.0  
16

105.3  
6.2

3+00

104.8  
6.7  
15

105.0  
6.5  
16

104.1  
7.4  
30

103.8  
7.7  
40

2+95.4 Manhole

105.42  
6.08  
Rim  
of M.H.

2+68 28.9 Lt. 3' Conc. Walk

107.57  
4.13  
40

106.90  
4.60  
28

2+62 28.7 Rt. 3' Conc. Walk

104.55  
6.95  
28  
on walk

104.40  
7.10  
40  
on walk

72.8 11.50

Waverly St. - Cross Sections

4+50

4+37

4+24

4+18

4+03

4+00

3+98

3+85

TP

2' dia. Eucly.

2' dia. Eucly.

1 1/2' dia. Cypress

1' dia. Cypress

2 1/2' dia. Eucly. tree

2 1/2' dia. Eucly. tree

108.93  
2  
111.50  
2

21.0 Rt. -

20.5 Lt. -

20.5 Rt. -

20.5 Lt. -

20.5 Rt. -

26 Lt. -

106.18

104.2 104.0 104.2 104.1 103.7 104.2 103.2 102.6  
4.7 4.9 4.7 4.8 5.2 4.7 5.7 6.3  
40 30 15 10 12 30 40

106.4 106.0 106.3 104.5 104.3 103.9 104.5 103.5 103.1  
2.5 2.9 2.6 4.4 4.6 5.0 4.4 5.4 5.8  
40 30 27 15 11 13 30 40  
edge of road edge of road

108.93  
2

Waverly St. - Cross Sections

Lt.

£

Rt.

33

5+22 2' dia Cypress 21' Lt. -

5+18 2 1/2' dia. Euclly. 21' Rt. -

5+03 2 1/2' dia. Euclly. 21' Lt. -

5+00

108.7	108.7	108.6	109.1	108.13	103.7	104.5	104.0	104.5
4.2	4.2	4.3	4.8	4.80	5.2	4.4	4.9	4.4
40	30	18	14		16	11	30	40

4+83 2 1/2' dia. Cypress 20.5 Lt. -

4+78 2 1/2' dia. Euclly. 20.5 Rt. -

4+62 1' dia. Euclly. 20.5 Lt. -

4+60 Edge of driveway 28.6 Rt

4+52 Edge of driveway 28' Rt.

108.93  
3

108.93  
2

163.33	103.22
5.60	5.71
28.6	40
103.33	103.18
5.60	5.75
28	40

Waverly St. - Cross Sections

Lt.

¢

Rt.

34

6+24.99

¢ Colima Diag. Sec. ¢

107.64 106.90 106.35 105.89 105.27 104.68  
 2.08 2.58 3.09 3.66 4.25  
 34.8 17.4 Rlm of 17.4 34.8  
 Pave. Pave. M.H. Pave. Pave

6+07.60

Gutter Line Diag. Sec.

105.83 1.29 50 106.62 106.95 106.65 105.19 104.67 103.93 104.61  
 2.00 2.31 2.98 3.28 3.74 4.26 5.00 4.32  
 50 25.7 25.7 17.4 17.4 43.8 43.8  
 Gut Curb B.C. Gut B.C. Pave. Pave. Gut B.C. Curb

5+90.22

N. Prop. Line on Colima Diagonal Sec.

106.85 106.06 105.32 105.21 104.44 105.00 104.82  
 2.08 2.87 3.51 3.72 4.49 3.93 4.11  
 34.76 17.4 17.4 on Pave. 19.8 19.8 34.76  
 on walk Curb Gut. on Pave. Gutter curb on wall

5+83

3' Eucly. 23' Lt. -

5+72.66

Rt. ¢ to Prop. Cor. on Rt.

106.4 106.2 105.5 104.9 104.8 104.3 105.3 104.8  
 25 2.7 3.4 4.0 4.1 4.6 3.6 4.1  
 40 30 18 12 15 16 30

5+63

2 1/2 Cypress 21' Lt. -

5+50

106.0 105.9 105.3 104.4 104.6 104.1 105.1 104.4 104.0  
 2A 3.0 3.6 4.5 4.3 4.8 3.8 4.5 4.9  
 46 30 16 13 13 14 30 40

5+43

2' dia. Eucly. 21' Lt. -

108.93

108.93

2

2

Waverly St. - Cross Sections

				7798 S.W.B.P.	Colima & La Jolla Blvd.
		5.04		77.98	
T.P.	4.71	23.02	9.00	78.31	
T.P.	0.36	87.31	12.48	86.95	
T.P.	10.17	99.43	9.67	99.26	
		<u>108.93</u>			

Johnson  
Greer  
Bunch  
3-29-50  
W.O. 31868

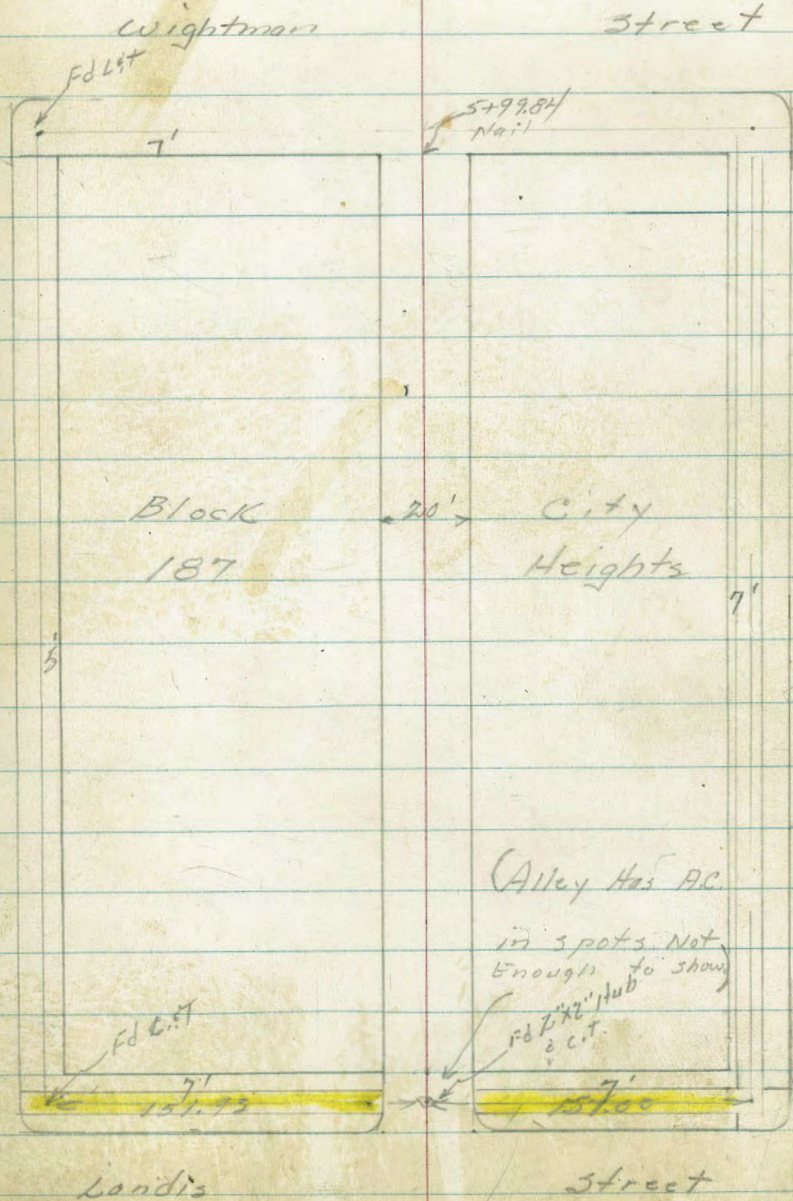
4-sect Alley Blk 187  
Landis to Wightman  
Btwn Boundary & N. 1/2  
City Heights

36

INDEXED

MAR 31 1950

Boundary Street



4 sect Alley BIK 187  
Landis to Wightman

37

Lt.

Q

Rt.

Note: All shots were taken  
with self reading Rod so  
therefore All elevations are  
true!!

North East Curb Return - 3' Radius

326.4	326.65	326.7	326.65	326.95	326.64
G	cb	G	cb	G	cb
B.C. in Alley		Center Radius		E.C. on Landis	

North West Curb Return - 3' Radius

326.4	326.99	326.48	326.98	326.5	326.99
G	cb	G	cb	G	cb
B.C. in Alley		Center Radius		E.C. on Landis	

0+05 = 4' Hedge 9.7' Rt

0+00 = North Prop. line of Landis St

327.1	327.10	326.49	326.7	326.81
G	cb	G	cb	cb
10		9.8		

0-14 = North Curb Line Landis St

326.92	327.59	326.50	326.99	326.35	326.05	326.64	325.62	326.2
G	cb	G	cb	G	G	cb	G	cb
50		13		13		46		

0-40 = E Landis St.

327.15	326.64	325.78
50		50

B.M.

2.63 331.67

329.09

N.E.B.P. Landis Boundary



4-section Alley BIK 187  
Landis to Wightman

Lt.

\$

Rt

38

1+35 = \$ of 3' square incinerator 8.4 Lt

12.4 wide conc. floor.  
1+34 = \$ Single car garage 19.4' Rt

326.08

19.4

Floor

1+24 = 4' board fence 8.5' Lt

T.P. 4.55 331.48 5.04 326.63

1+00

326.4 326.9 326.5 326.4 326.6  
30 10 10 30

12.3 wide  
0+68 = \$ single car garage 10.6' Rt

326.66

326.75

10.6

13

Ramp

Floor

18.5' wide  
0+65 = \$ double garage 10.1' Lt conc floor

327.10

10.1

0+50 = Power Pole 8.3' Lt #JPA 3705

327.0 326.9 326.8 326.6 327.0  
30 10 9 30

conc. Ramp is 15.3' wide  
0+38 = single Car Garage 11.6' Lt

327.39 327.32

13 11.6'

floor Ramp

331.67  
A

4 section Alley B/K 187

Landis to Wightman  
City Hgts

lt.

£

Rt

39

2+01 = End of 12.2' x 16.2' frame - 7.3' lt

2+00

1+8.5 = Start of 12.2' x 16.2' frame building 7.5' lt

327.2 326.4 326.4 326.6 325.5  
25 7.3 10 30

1+77 = End frame building 9.7' lt

1+75 = £ 18" oak tree 8.3' lt

start of 19' x 10' frame Building 10.3' lt

1+68 = 6" oak tree 9' lt

J

1+57 = £ single car garage 19.5' Rt

325.9

19.5  
dirt floor

1+56 = £ of 10' x 8' frame Building 9.4' lt

1+51 = End of 4' board fence 8.3' lt

1+50 = Power Pole 7.5' lt

#D.27488+

327.3 326.8 326.4 326.6 326.0  
20 10 10 20

331.48

4-sect Alley BIK 187  
 handis to Wightman

LT.      \$      RT.      40

3+02 = start of frame House 9.9' RT

3+00

2+96 = 4" tree 9.6' LT

327.0   326.7   326.1   326.0   325.3   324.6  
 25      10                      8      11      25

2+91 = 2.5 conc. walk 8.4' LT

326.80   326.61  
 10.6      8.4  
 Floor of House

2+80 = E of 24" pepper center 10' LT

2+77.5 = Power Pole 9.6' LT # D 27487T

2+61 = E single garage 25.3' RT

325.30  
 25.3  
 conc. floor

2+50 = End of double garage 9' LT to ramp

327.33   326.79   326.5   326.0   325.4  
 11      9'                      10      25  
 Floor      Ramp

2+38 = E of double garage - 19.3' RT  
 20.3' wide

325.69      326.04  
 19.3      25.5  
 Ramp      Floor

2+30 = Start of comb. apron & sidewalk 8.4' LT  
 E double garage

327.10   326.91  
 15      8.4

331.48  
 1

X-sect - Alley BIK 187  
 Sandis to Wightman

Lt.

¢

Rt.

41

4+00 = Power Pole 8.8' Lt # D37486T

324.1 323.1 322.3 321.9 321.0  
 35 10 10 25

3+88 = \$ double garage 18.2' wide  
 17.2' Rt conc floor

322.39  
 17.2  
 Floor

3+73 = End of 4' fence 10.8' Rt

3+65 = 2.5' conc walk 9.3' Lt

324.82 324.46  
 25 93

3+50

325.3 324.8 324.7 325.0 324.7 323.5  
 25 10 8 10 25

3+41 = 4' fence iron posts 9.5' Rt

T.P. 2.31 - 325.81 5.95 323.50  
 ^

3+19 = \$ of single car garage 12' wide

326.73 326.24  
 15 10.5  
 Floor Ramp

T.P. 3.99 329.45 6.02 325.46  
 ^

3+15 = End of Frame House 9.6 Rt

325.63

331.48  
 ^

Floor

4-500t - Alley BIK 187  
Londis to Wightman

Lt.

£

Rt.

42

4793 = £ 16' x 30' frame House 10.8' Lt

321.38 318.5  
10.8 10.8'  
Floor Ground

4782

320.3 319.6 319.2 319.0 316.7 316.2 317.9  
25 10 8 14 24 35

4776

320.2 319.7 319.1 318.7 317.2 315.4 316.5  
25 10 10 13 18 35

4773

320.5 319.9 319.2 318.7 318.0 318.5  
25 10 10 23 20

4768 = £ single garage - 23' rt dirt floor

318.0  
23  
Floor

4750

321.8 320.8 320.2 320.0 318.4 317.5  
30 10 10 13 25

4727

321.9 321.7 321.4 321.2 319.9 318.2  
20 10 11 13 25

4733

322.0 322.0 321.5 321.3 320.5  
20 10 10 25

£ of single garage 23' Rt facing east  
4707 = £ 8.5' x 6.5' shed 10.2' Lt

325.81  
K

322.5  
10.2  
Floor

321.2  
25  
Floor

4500ft Alley BNC 187  
Londis to Wightman

43

5760

321.2 316.5 314.6 312.0 310.8 312.6 312.6 310.4  
35 25 7 9 10 25 50

5755 - 12" water line exposed

312.98  
Elev. on  
Top of pipe

320.7 316.8 315.0 313.0 312.9 312.9 316.1  
85 25 5 10 24

dirt wall stops

5750

320.5 316.6 315.7 315.5 315.5 313.1 313.4 316.4  
85 27 10 10 17 23

3' Retaining Wall

4" wide Single Car garage  
5737 = End conc found. 9.8' RT

320.2 316.6 316.1 315.8 316.87 315.9 313.1 316.5  
35 30 10 9.8 9.8 17 24  
Conc. dirt  
Floor

4" wide Single car garage  
5725 = Start conc found. 10' RT 12' x 18'

316.87  
10

5703

319.0 317.1 312.3 317.1 317.3 315.5 317.5  
35 14 10 9 16 35

T.P.

3.24 320.47 8.58 317.23  
^

3' pepper Tree center 9' Lt  
5706 = Power Pole 7.5' Lt #D 27485+

320.3 319.2 (317.7) 317.5 317.4 315.5 318.5  
35 14 10 8 16 35

32581  
^

4-sect - Alley BIK187

0.03  
329.04

Landis & Boundary

£

RT

44

Landis to Wightman

4.07  
329.01

T.P. 332.3333.08 6.46 329.76

T.P. 10.21 336.16 1.99 325.95

T.P. 11.45 327.94 2.50 316.49

T.P. 11.80 318.99 0.22 307.19

Water Pipe at E of Wightman St Elev - 312.98 to top pipe

6+39.84 = £ Wightman St 322.9 320.8 304.1 301.7 305.38 298.6 298.0  
71 56 22 2 50 100

Ground Top Manhole

6+06.84 322.2 316.2 307.2 303.4 302.0 300.9 300.2 300.2 299.3  
71 56 35 26 10 10 10 50 100

T.P. 0.04 307.41 13.10 307.37

↑

5+99.84 = South Pl. Wightman St, 322.2 322.5 317.1 313.5 305.3 302.1 301.3 299.9 298.4  
71 40 95 27 7 10 50 100

5+80 320.6 316.5 311.0 307.6 305.6 304.7 302.4  
32 21 12 6 10 35

5+70 321.0 316.4 309.2 307.8 307.8 308.5 308.0  
33 25 8 10 25 50

320.47

↑

X-sec. Electric Ave.  
Gravilla to Bon Air

25020  
11/28/50

45

Sommermeier  
Begg &  
Allen  
Bunch

INDEXED

DEC 4 1950

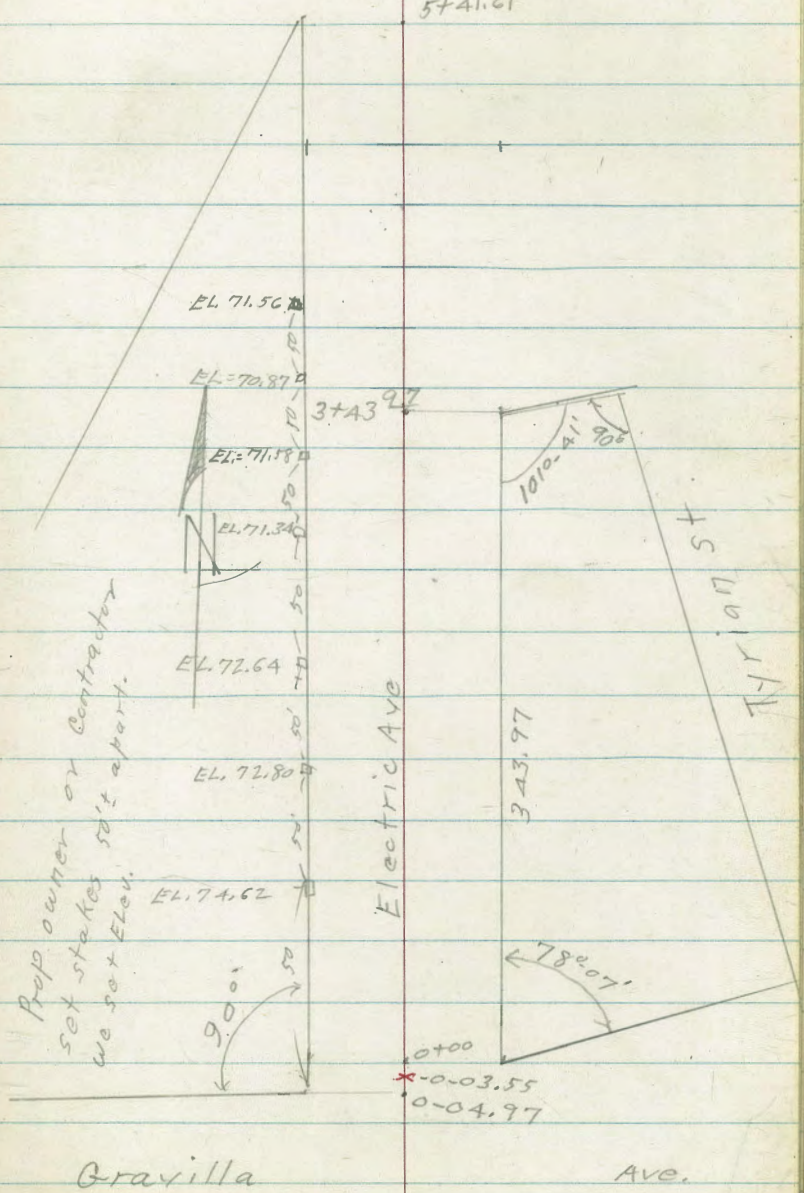
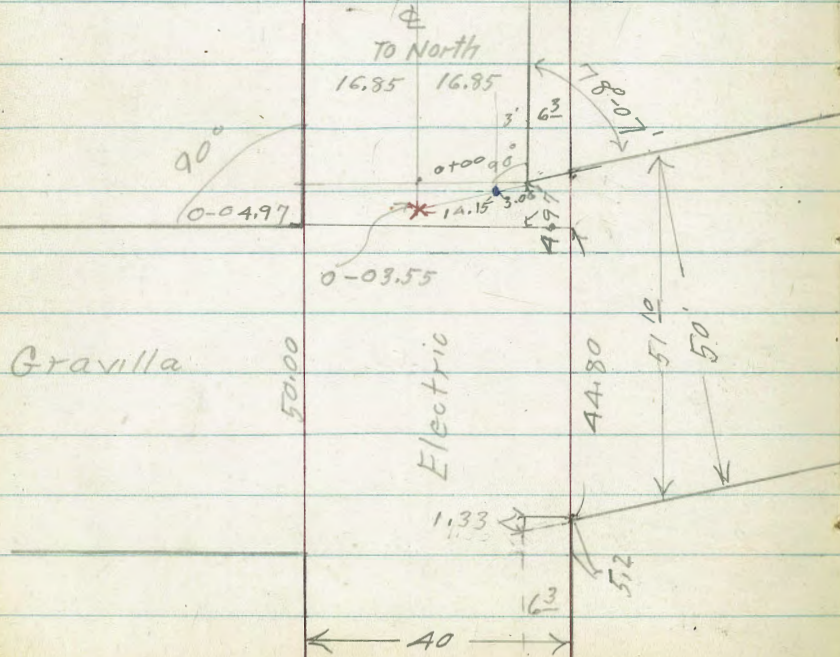
• = Fd. L+T.

X = cut cross in Pave.

TP sheet 2127  
T.P. Book #17  
Map # 1808  
" 1216  
F.B. 1279  
18

5+41.61

Intersection detail





Levels Electric Ave  
Gravilla to Bon Air. 11/29/50

46

0-04<sup>5</sup> - 11<sup>8</sup> Lt. = end curb. + Pave

15.89	15.38
<u>4.68</u>	<u>5.19</u>
11.8	11.8
top of	G

Cont.

77.11	77.66
<u>3.48</u>	<u>2.91</u>
74.4	74.4
G	cc

24<sup>4</sup> Rt. = B.C. 10' Rad cb. Rot.

0-13<sup>4</sup> cb. line Gravilla to east.

15.59	15.69	16.00	16.52
<u>4.98</u>	<u>4.88</u>	<u>4.57</u>	<u>4.05</u>
	4.8	2.49	2.44
	G	G	cc.
			B.C.

Cont.

74.74	74.17
<u>5.83</u>	<u>6.40</u>
71.8	71.8
cc	G

21.8 Lt. = B.C. 10' Rad cb. Rot.  
Δ 78°-07' 17 S.W. Quad

0+14<sup>8</sup> = curb line Gravilla to west

15.41	15.29	15.40	15.62
<u>4.76</u>	<u>5.29</u>	<u>5.17</u>	<u>4.95</u>
21.8	21.8	11.8	80.57
cb. B.C.	Q		

3.84 80.57 — 76.73

S.E. Lt. Electric + Gravilla

E = Prop. - 16.85 East

W = Prop. - 16.85 west.

— 68.86

~~N.W. P.P. Gravilla + La Jolla Blvd.~~

Electric

T.P. 4.56 77.36 7.77 72.80

1+00

0+50

0+01<sup>2</sup> Cont.

0+01<sup>3</sup> W.Rt. = end curb

See sketch for location  
0+00. 12° Rt. = Approx. E.C. Cl. Rot.

0-01<sup>8</sup> end pavement on  $\Phi$

71.5 72.7 73.5 74.9 76.6  
9.1 7.9 7.1 5.7 4.0  
50 W E W 50

74.5 75.2 75.7  
6.1 5.4 4.9  
W E

76.81 76.7  
3.76 3.9  
17 20  
Back of walk

75.89 76.41  
4.68 4.16  
12 12  
0 0

76.0 76.0 75.85 76.36  
4.6 4.6 4.72 4.21  
W G 12 12  
0 0

75.68  
4.89

80.57

2+04 17<sup>L</sup> Rt. = end Conc. wall

12.8	12.3	15.3
<u>4.6</u>	<u>5.1</u>	<u>2.1</u>
17	17 <sup>L</sup>	17 <sup>L</sup>
End	B.W	T.W

2+00

70.4	71.2	71.6	72.9	16.4
<u>7.0</u>	<u>6.2</u>	<u>5.8</u>	<u>4.5</u>	<u>1.0</u>
50	W		E	50

T.W. = top of wall.  
B.W. = base of wall or footing.

1+53 17<sup>L</sup> Rt. = start Conc. wall

13.5	12.8	15.4
<u>8.9</u>	<u>4.6</u>	<u>2.0</u>
17	17 <sup>L</sup>	17 <sup>L</sup>
End	B.W	T.W.

1+50

72.1	72.7	73.2	15.4	16.2
<u>5.3</u>	<u>4.7</u>	<u>4.2</u>	<u>2.0</u>	<u>0.8</u>
W		E	21	50

1+2A- 16<sup>L</sup> Rt. = end Conc. apron

74.10	75.20
<u>3.26</u>	<u>2.16</u>
162	223
	Gar. floor

1+03

17<sup>L</sup> Rt. = start Conc. apron  
to double Gar. Conc. floors

74.81	76.24
<u>2.55</u>	<u>2.12</u>
17	264
	Gar floor

77.36

3+00

69.8	10.2	10.7	10.8	15.8	15.8
<u>7.6</u>	<u>7.2</u>	6.7	<u>6.6</u>	<u>1.6</u>	<u>1.6</u>
50	W		E	30	40

2+83

13<sup>3</sup> Lt. = Ctr. sewer M.H.

40.9
<u>6.5</u>
13.4
Top M.H.

2+50

70.7	71.1	71.4	75.4	75.4
<u>6.7</u>	6.3	<u>6.0</u>	<u>2.0</u>	<u>2.0</u>
W		E	30	40

2+39 - 15<sup>3</sup> Rt. = end porch

71.2

6.2

15.3

End

2+24 - 17<sup>3</sup> Rt. = Joq in house  
also = start porch

73.5

3.9

17.3

End

2+12 - 20' Rt. = start house

73.1

4.3

20

End

77.36

Electric

50

T.P. 4.10 76.97 5.38 72.87

4+42 17<sup>3</sup> Lt. = end Conc. wall

72.7	71.5	72.0	72.8	73.6
5.6	6.8	6.3	5.5	4.7
17 <sup>3</sup>	17 <sup>3</sup>	17		E
T.W.	B.W.	End		

4+05 = 21<sup>5</sup> Lt. 6' wide service door to store.

41.41  
6.84  
21.5  
Floor level

4+02 17<sup>5</sup> = start conc. wall

41.7	72.6	71.3	72.3
6.6	5.7	7.0	6.0
18	17 <sup>5</sup>	17 <sup>5</sup>	17 <sup>5</sup>
conc. yard	T.W.	B.W.	End

18<sup>4</sup> Lt. = end Conc. wall.

4+96 17<sup>6</sup> Lt. = face of wall footing

70.9	72.3	73.0	73.1
7.5	6.0	5.3	5.2
17 <sup>6</sup>	W	17 <sup>6</sup>	E
B.W.	End	B.W.	

17<sup>6</sup> Lt. = Ely. face wall footing.

3+63 18<sup>1</sup> Lt. = start 6' high Conc. wall

71.3	71.7	71.0
1.0	<del>7.1</del>	6.6 7.3
19 <sup>1</sup>	<del>17<sup>1</sup></del>	18 <sup>1</sup> 17 <sup>6</sup>
T.W.	B.W.	End B.W.

T.P. 7.24 78.25 6.35 74.01

78.25

3+43.97 16.85 Rt. = Prop. Cor. Bon Air.

70.8	71.0	71.2
6.6	6.4	6.2
W		E

77.36

S.W.B.P. Ben Air + La Jolla Blvd 4.95 72.02 71.98

5+00 17<sup>1</sup> Lt. = face ~~etc~~ on Ret. <sup>Commercial gutter</sup>

71.55  
5.42  
17<sup>1</sup>  
gutter

71.57  
5.40  
W

72.71  
4.26

73.52  
3.45  
E

4+98<sup>5</sup> 16<sup>4</sup> Lt. = start com. <sup>gutter</sup> commercial

71.51  
5.10  
16<sup>4</sup>  
gutter

4+95 -20<sup>7</sup> Lt. = back edge commercial gutter

71.96  
5.01  
20<sup>7</sup>

72.50

4+92 14 cross gutter

4.47

4+86 = start Paue on t

72.68  
4.29

4+79 = start Paue. on east.

72.2  
4.8  
W

72.8  
4.2

73.14  
3.83  
E  
17 cross gutter

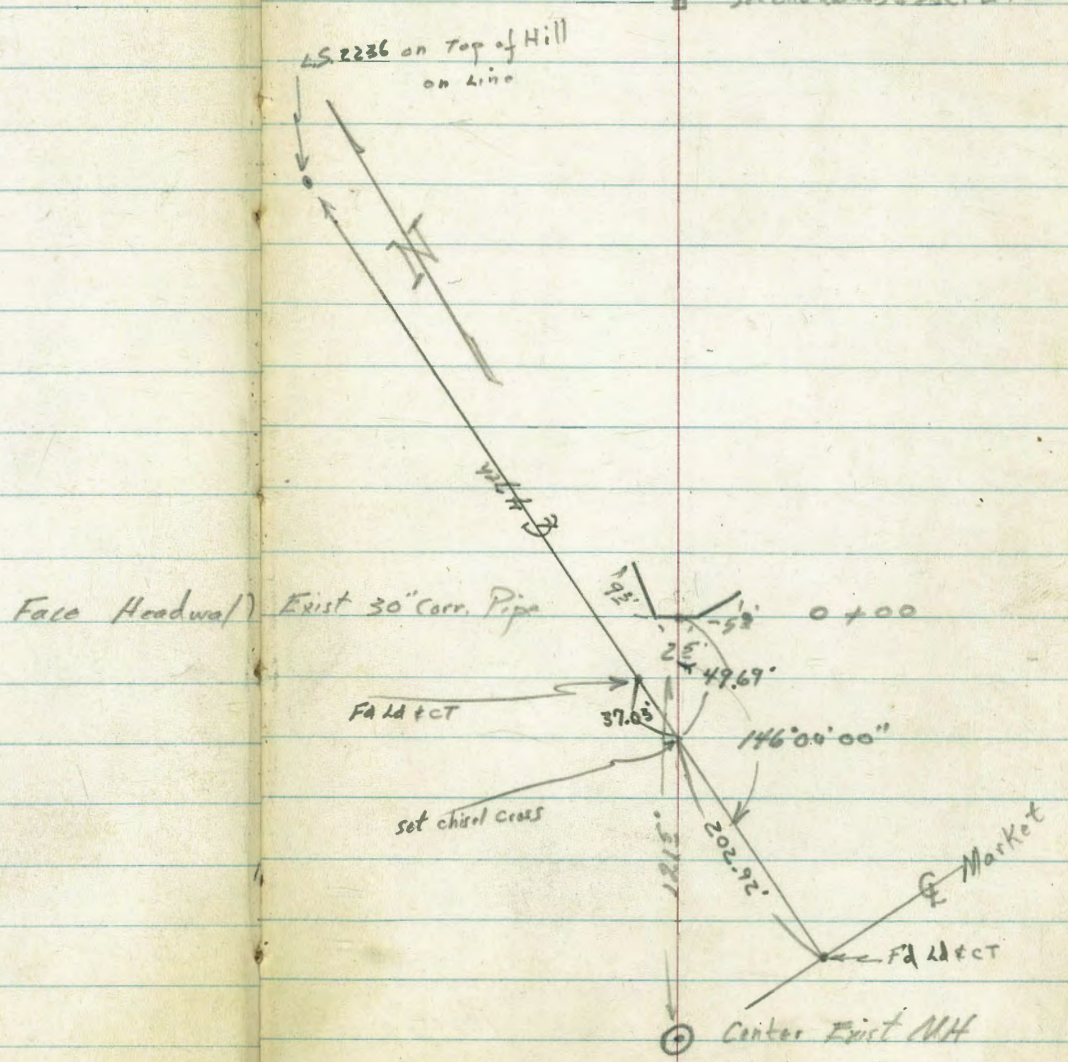
76.97

Roberts  
Cota  
Moore  
Clark  
12-27-50

Survey to Extend 30" Corr. Pipe  
Drain on East, located East Side 47th  
and North Market.

~~1024968~~ See FB 1673 pg 47 67152  
20769

INDEXED  
M.K.  
DEC 28 1950



Cont'd From Page 52

24

R

53

0+87

	127.9	125.3	121.8	124.7	127.4
4.0		6.6	10.1	7.2	4.5
15			8	11	20

0+75

	126.5	125.5	121.5	124.2	126.6
5.4		6.4	10.4	7.6	5.8
15		5	4		15

0+60

	126.3	124.2	121.3	123.7	128.3
5.6		7.7	10.6	8.2	3.6
20		10	4		15

0+30

	124.9	123.2	119.7	122.9	126.4
7.0		8.7	12.2	9.0	5.5
15		10	5		15

0+16

	122.5	119.3	122.8
9.4		12.6	9.1
5			5

0+00 END EXIST CULVERT

118.85  
13.03  
INVERT

BM

10.92

131.88 ✓  
7

120.96 ✓

LA. C.T. & 47th & Market

131.88 ✓  
7



Cont'd From Page 53

44

Base  
Line

87

54

2+30

134.6	131.1	126.2	128.4	131.0
2.4	5.9	10.8	8.6	5.4
15		12	16	40

2+00

Hub & Disc

134.6	132.5	127.5	125.2	128.2	132.0
2.4	4.51	9.5	11.7	8.7	5.0
15	4.6	32	37	44	55

1+50

134.5	132.2	127.7	125.9	128.8	126.2	129.5
2.5	4.8	9.3	11.1	13.2	10.8	7.5
10		30	45	50	55	65

1+25

133.1	130.8	125.3	122.5	125.3	127.8
3.9	6.2	11.7	14.5	11.7	9.2
10		28	32	35	45

T.P.

777

1370.2 ✓

2.63

127.25 ✓

1370.2 ✓

4 00

128.2	126.4	125.2	122.1	125.2	127.2
3.7	5.5	6.7	9.8	6.7	4.7
10		10	14	18	25

131.88 ✓

↑

131.88 ✓

↑

Cont'd From Page 54

Lt

Base  
Line

Rt

55

Check

986

$$120.95^{\checkmark} = 120.96^{\checkmark}$$

T.P.

1.37

130.81<sup>✓</sup>

7.58

129.44<sup>✓</sup>

3+00

1.6  
40 135.4

6.8  
28 130.2

4.8  
16 122.2

1.0  
10 136.0

42.3  
15 139.3

2+60

4.4  
15 122.6

9.6  
13 127.4

4.5  
13 122.5

1.1  
38 135.9

132.02<sup>✓</sup>

↑

132.02<sup>✓</sup>

↑

X-sect Hilltop  
From 47<sup>th</sup> East to Gully

56

N.O. 26769

Lt

Rt

0-01 Telephone Pole 27<sup>th</sup> Pt # 1535598

190.3	189.3	189.28	188.4	187.5	187.1	187.1	187.8	187.1	186.8
2.5	3.5	3.48	4.4	5.3	5.7	5.7	5.0	5.7	6.0
50	30	28 # Walk	16	13		11	16	30	50

0-02 Begin 3° Wide Walk

0-06 Begin 3° steps

187.58  
51.8  
29°  
# 5 steps

INDEXED  
MK  
DEC 28 1950

0-12

186.9	186.7	184.5	186.4	186.2
5.9	6.1	6.3	6.7	6.6
50	30		30	50

0-20 Edge Paving

187.23	187.02	187.00	186.74	186.49	185.98	184.59
5.53	5.74	5.76	6.02	6.22	6.28	8.17
110	50	30		30	50	100

0-30 E 47<sup>th</sup> Ed. 114 Ct.

187.30	187.15	186.81	186.55	186.04	184.95
5.46	5.61	5.95	6.21	6.22	8.01
100	50		30	50	100

BM

5.95 192.76 ✓

186.81 ✓ A. L. & Tr. K. Hilltop to 47<sup>th</sup> See 1673 pg 18  
187.17 (?) ← From F. B. C. 1652

0+83 24' Lt & 8" Pepper

0+79 22' Rt & TP# JP 171124

0+70 24' Lt & 12" Pepper

0+57 25' Lt & 11" Wide AC Drive

0+46 27' Lt & End 3rd Walk

0+36 23' Lt & 6" Pepper Tree

0+35

0+07 23' Lt & 6" Pepper Tree

0+00 East Pl. 47th St.

Lt Rt

188.5	189.2	188.7	187.9	187.2	184.2	184.2
93	36	41	50	56	62	65
50	30	19	13		30	50

189.85	189.18	188.2	186.9	185.2
271	358	275	351	275
50	255	50	30	30
	begin Drive	End Walk		
	190.0	189.3	188.2	186.9
	28	35	46	59
	50	30		30
				50

190.2	189.4	188.4	187.8	184.4	184.2
26	34	44	50	62	65
50	30	15		30	50

187.2  
56

192.76 A ✓

X-sect. Hilltop Cont.

58

2+00

Lt.	#	Rt.
185.2	15	175.0
177.1	9.0	174.8
177.1	20	174.8
174.1	10.0	174.3
	16	
18	32	16
Top	30	30
Slope	30	50
	50	

T.P.

618 186.07A ✓

12.87 179.89 ✓

186.07A ✓

1480 23° Rt. & T.P. # D.37460T

1465

181.1	6.7	178.9
181.1	6.7	179.1
181.4	11.4	180.6
181.4	11.4	180.4
179.6	13.2	180.1
	16	182.1
187.9	13.7	
	20	
	30	
	50	

1430 30° Lt. Begin Fill, School Yard

186.4	6.4	183.1
185.1	7.7	183.0
182.8	10.0	183.8
	9.7	183.1
	9.8	183.0
	9.0	183.8
	9.2	183.6
	9.7	183.1
50	30	16
Begin Fill	30	20
School yard	10	30
	30	30

1413 23° Lt. 6" Pepper Tree

1400

187.4	5.4	185.3
187.2	5.6	186.0
187.1	5.7	185.4
185.7	7.1	185.4
	7.0	185.0
	7.5	
	6.8	
	7.2	
	7.8	
50	30	16
	18	20
	10	30
	30	30

192.76A ✓

Check B.M.  
T.P.

715 192.65 ✓ 5.84 186.81 = 186.81  
057 185.50 ✓  
X- Sect. Hilltop Cont.

59

1+00

185.6	186.6	187.1	185.1	183.9	183.4	182.9	183.4	184.2	184.2	183.4
0.5	10.5	1.0	1.0	2.2	2.7	3.2	2.7	1.7	1.7	2.7
50	40	35	30	14		70	17	35	30	50
			Top	Top						

3+50

185.7	186.1	183.8	180.4	180.2	179.2	180.6	179.8	180.7	181.4	181.5
0.4	0.0	2.3	5.7	5.9	6.9	6.1	6.3	5.4	4.7	4.6
50	37	30	22	10	9		9	20	30	50
			Top	Top						

3+21 235 Pl. & T.P.#D37461T

3+00

185.7	185.7	178.9	177.7	176.2	176.2	175.0	175.9	176.7
0.4	0.4	7.2	8.1	9.9	9.9	11.1	10.2	9.4
50	42	30	28	12		20	30	50
			Top	Top				

2+65

185.7	185.1	177.7	176.4	175.1	174.5	170.7	169.6	170.8
0.4	1.0	8.4	9.7	11.0	11.6	15.4	16.5	15.9
50	44	30	27		6	16	30	50
			Top					

2+40 Bottom Gully

186.1	186.1	174.6	174.4	174.3	169.6	167.8	166.1
0.0	0.0	9.5	11.7	11.8	16.5	12.3	20.0
75	50	30		4	13	30	58
		Top	Top				

186.07 T ✓

REDUCED 14-29-50 AEA.

Drainage Survey  
 Lot #9 BIK D. Starkoys Prospect Park  
 (N. Ely. Bonair & Draper)

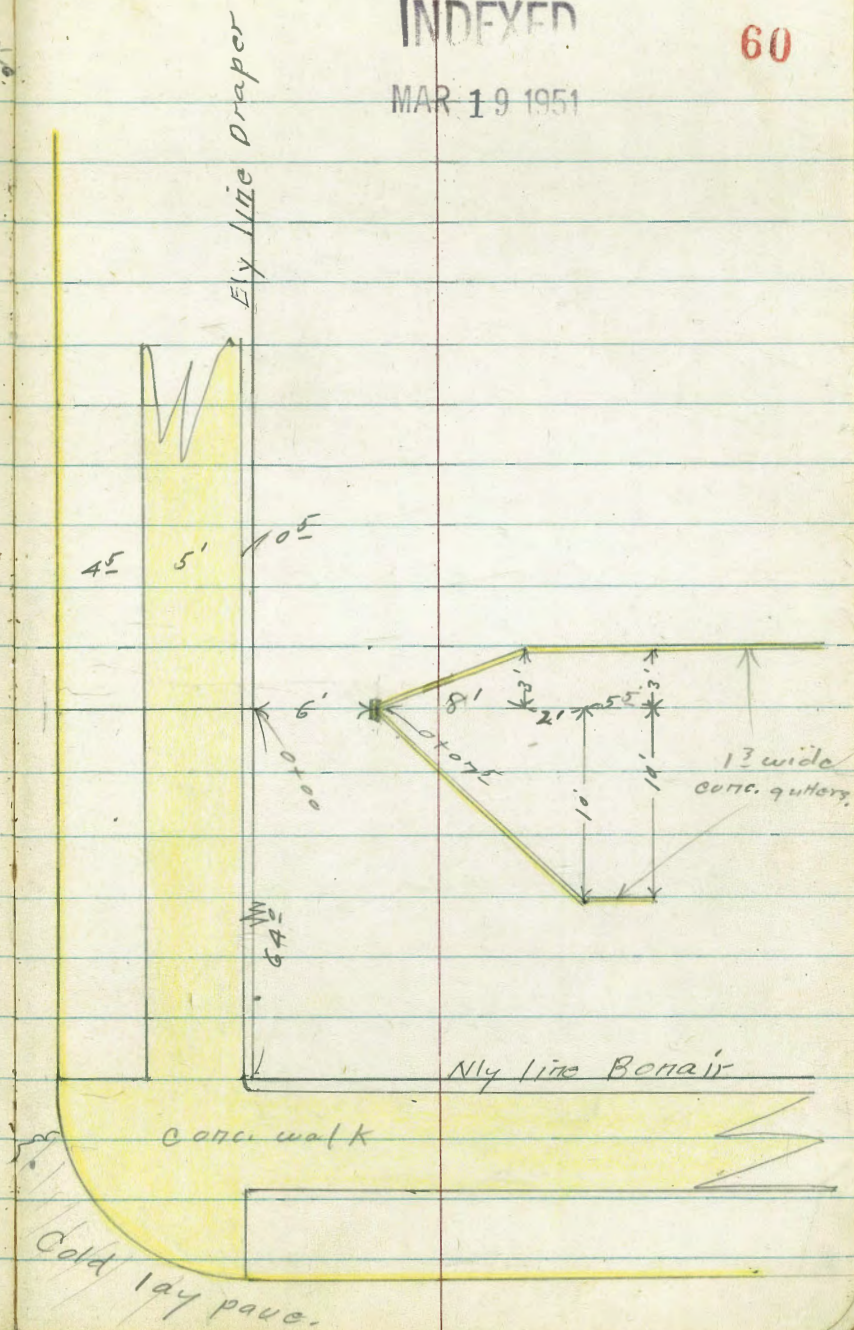
Sommermeier  
 Begg  
 Hatch  
 Wiers

Mar. 16, 1951

W.O. 20810

T.P. sheet 2124  
 Map 1729

Ely line Draper at a point 64'  
 North of Nly. line Bonair = 0+00



INDEXED

60

MAR 19 1951

Draper + Bonair

61

0+05<sup>5</sup> = Ctr. 1'x1' (inside) box inlet.  
Rock & Conc.

8.3  
5  
106.91  
8.51  
0.5  
edge box  
9.9  
Bottom  
105.2  
8.53  
0.5  
edge box  
106.57  
8.5  
5  
106.6  
8.28  
6.5  
Conc.  
walk  
2.5 wide

0+00 = Ely line Draper

8.3  
5  
106.8  
8.4  
8.4  
5

Fence + wall run N + S.

11' Lt = Cor. fence

9' Rt. = end fence + start 6' high rock wall

0-00<sup>3</sup> = cross 6' high board fence

107.2  
7.98  
30  
106.89  
8.21  
10  
106.79  
8.31  
8.36  
10  
106.60  
8.50  
30

0-00<sup>5</sup> = Ely edge walk

107.00  
8.10  
30  
106.72  
8.38  
10  
106.64  
8.46  
106.58  
8.54  
10  
106.45  
8.65  
30

0-05<sup>5</sup> = wly edge walk

146.95  
8.15  
3.5  
0.6  
106.55  
8.55  
0.6  
106.30  
8.80  
30  
0.6  
106.03  
9.07  
6.4  
0.6  
105.53  
9.57  
70  
pave  
8.8

70' Rt. = start 1 1/2" thick plant mix  
0-10 = Ely cl. line Draper

115.10 ✓

9.51 115.10 ✓

105.59 ✓

S.W.B.P. Bonair + Draper



INDEXED

MAR 19 1951

62

also = wly. face 4' high N. & S.  
 0+54<sup>E</sup> 3' Lt. =  $\frac{1}{2}$  end of conc. trough.

108.16  
 6.94  
 3  
 I.E.T.

0+21<sup>E</sup> 10' Rt. = end trough on south

106.67  
 8.43  
 10  
 I.E.T.

0+16 10' Rt. =  $\Delta$  in 12' wide conc. trough.

106.73  
 8.37  
 9.4  
 E

106.52  
 8.58  
 10  
 I.E.T.

106.80  
 8.30  
 10.1  
 E

8' Lt. =  $\frac{1}{2}$  3' conc. walk to Gar.  
 0+14 - 3' Lt. =  $\Delta$  in trough

106.83  
 8.27  
 8  
 E

106.68  
 8.12  
 4  
 E

106.45  
 8.65  
 3  
 I.E.T.

106.61  
 8.44  
 2.5  
 E

106.7  
 8.4  
 5  
 E

E = edge of trough

I.E.T. = invert of trough (12' wide - Conc.)

0+07<sup>E</sup> "V" in trough (see sketch)

106.31  
 8.79  
 1  
 I.E.T.

106.54  
 8.56  
 106.51  
 8.13

106.57  
 8.73  
 1  
 I.E.T.

0+06 = spillway lip

Lindo Paseo

17'

42' cb. Rad.

12'

Prop. Line

st.

Curve Line is Base Line

6' cb. Rad.

5+5

12'

Pipes  
37' cb. Rad.

0+00

cb. line  
90° from Prop  
Cor.

12'

Montezuma

Rd.

8+20.20  
Fd. pipe  
12'

C.N.L. Sub.  
Marcellena Tract 63

Sec 7320-L

6+70.8

st.

Hardy st.

5+5

5+50.7 = Beg. cb.

4+55.3 = end cb.

12'

42' cb. Rad.

Lindo Paseo

INDEXED

MAY 7 1951

457.21

64

Levels + Location of Exist. curbs  
+ Returns - on E. side of 55th  
from Montezuma Rd. To N.L. of Sub.  
# 5245

W.O. 25020 4-2-51 - 7.0

B.M. = S.E. Top Hyd. College Way = Montezuma  
+ 0.65 453.16 3.33 449.83 = N.E. B.P.  
452.51  
10.48 457.08 - 6.56 446.60  
6.59 460.66 3.01 454.07  
0.62 457.21 4.07 456.59  
55th + Montezuma  
Set B.M. - N.E. B.P. 3.45 453.76

457.21

Req. Rods around N.E. Return - 37' Rad.  
58.9' around - 10' sections -  
PC - East end. Top cb.  
+ 10' 3.45 453.76  
+ 20' 3.81 453.40  
30 4.18 453.03  
40 4.44 452.73  
4.80 452.41

50 .15 Lt  
58.9 = E.C. = 0 + 20.4  
0 + 100 = opp. Prop. P.I.  
offsets from baseline to cb. face  
0 + 50 = .15 Lt.  
1 + 100 = .02 Lt  
.03 Lt.  
1 + 33.9 = P.C. 6' Rad. To Alley  
E.C. = 6' Rt  
12' Rt. = end cb. at E.L.  
12' Rt. = end at E.L. - N.L. Alley  
6' Rt. = P.C. 6' Rad.  
53' Lt.  
1 + 66.1 = E.C.  
2 + 100 = .04 Lt.  
2 + 30 = .04' Lt. = Brk.  
42' Rad Ret.  
2 + 60.5 = 0.5' Lt. = P.C.  
T.P. 1.57 452.74  
10' SE. Return  
Top  
A.C. pave gut  
20' - Top  
gut  
30' Top  
gut.

5.02 152.19  
5.13 152.08  
4.84 152.37  
4.43 152.78  
4.14 153.07  
3.96 153.25  
3.73 153.48  
3.86 153.35  
4.08 153.75  
4.35 152.86  
5.00 152.21  
5.77 151.44  
6.63 150.58  
6.04 451.17  
2.50 - 150.24  
2.86 449.88  
2.79 449.95  
3.17 449.57  
3.01 - 449.73  
3.46 - 449.28

452.74

452.74

40' Top 3.18 - 449.56

60

in Drive  
Top

5.80 - 446.94

65

gut 3.46 - 449.08

50' Top 3.30 - 449.44

66.1 = E.C. = 3 + 80.5 = Line

6.00 - 446.74

gut 3.69 - 449.05

3 + 86.5 = end Drive

5.42 - 447.12

60 Top 3.39 - 449.35

4 + 00 = 0.1 Rt.  
= end of cb.

5.97 - 446.97

gut 3.73 - 449.01

4 + 55.3 = 0.1 Rt.

7.60 - 445.74

66.5 = E.C. Top 3.43 - 449.31

gut 3.74 - 449.00

T.P. 3.61 445.53

10.82 441.92

Req. N.E. Return - 66.1' around - 10' Parts

43.4 Rad. Return

PC = E. end. Top 4.04 - 448.68

5 + 50.7 = Req. cb = PC.

3.17 - 442.36

gut 4.55 - 448.19

10

Top

3.39 - 442.14

10' Top 4.22 - 448.52

gut

3.95 - 441.58

gut 4.80 - 447.94

20

T

3.52 - 442.01

20 Top 4.38 - 448.36

9

4.12 - 441.41

gut 4.99 - 447.75

30

T

3.71 - 441.32

30 Top 4.56 - 448.18

9

4.26 - 441.27

gut 5.19 - 447.55

40

T

3.84 - 441.65

40 Top 4.78 - 447.96

9

4.40 - 441.13

gut 5.41 - 447.33

50

T

4.05 - 441.48

50 Top 5.03 - 447.71

9

4.46 - 441.07

gut 5.66 - 447.08

445.53

60

T 4.23 - 441.30

g 4.53 - 441.00

68.2 = E.C.

T 4.34 - 441.19

g 4.59 - 440.94

Beq. N.E. Ret. - 64.14 around - 10 Parts.

P.C. = E. end

T 4.82 - 440.71

g 5.22 - 440.31

10

T 4.86 - 440.67

g 5.37 - 440.16

20

T 5.02 - 440.51

g 5.56 - 439.97

30

T 5.13 - 440.40

g 5.72 - 439.31

40

T 5.22 - 440.31

g 5.91 - 439.62

Inlet.  
45.8 = end of opening

T 5.36 - 440.17

g 6.21 - 439.32

53.3 = Inlet

Top 5.46 - 440.07

gut. = grate

6.32 - 439.21

445.53

66

61.2 = end opening

T 5.52 - 440.01

g 6.35 - 439.18

64.1 = E.C.

5.57 - 439.96

= 6 + 70.8 - on line  
= end of cb.

See 7320 - L  
N.E. Cor. 55<sup>th</sup> + Hardy.  
Set B.M. - D in cb. & Inlet

5.46 440.07

60

68.2 = E.C.

Beq. N.E. Rot. - 64

P.C. = E. end

10

20

30

40

Inlet.  
45.8 = end of opening

53.3 =  $\neq$  Inlet.

gut. = gra

Copy of  
Field Notes

Alley between Lots  
(1-27) incl Collwood Gardens

E of 55<sup>th</sup>

N of Montezuma

INDEXED  
Sundries  
AUG 21 1952

A.W. DANIELS  
(L.S. 2201)

2375 SANDIEGO A  
S.D. Cal

TEL J-2657

Bench Mark (Top of F.H. S.E. Cor of College  
 Ave. & Montezuma Road. El 452.51  
 10'L      R      10'R

STATION	10'L	R	10'R
+69.25		453.32 5.90 Gutter	453.47 5.90 Top of Curb
+79.25	452.92 453.32	6.70 5.90 Top of Curb	453.07 6.15 Top of Curb
10+00	454.2 5.0	453.3 5.9	453.2 6.0
+50	454.3 4.9	453.4 5.8	453.2 6.0
9+00	454.4 4.6	453.6 5.6	453.5 5.7
+50	454.6 4.6	453.8 5.4	453.6 5.6
8+00	454.4 4.8	453.7 5.2	453.8 5.4
+50	453.8 5.4	453.7 5.5	453.8 5.4
7+00	453.9 5.3	453.8 5.4	453.6 5.6
+50	454.4 4.8	454.3 4.9	454.2 5.0
6+00	455.0 4.2	454.9 4.9	454.6 4.6
+50	455.1 3.8	454.9 4.8	455.2 4.0
5+00	455.8 3.4	454.8 4.4	455.2 4.0
+50	456.2 2.5	455.4 3.8	456.1 3.1
4+00	455.9 3.3	455.4 3.8	455.9 3.3
+50	-	455.5 3.7	455.5 3.7
3+00	-	-	-
+50	455.6 3.1	HI 459.22 3.5 = 455.2	-
2+00	455.7 3.0	455.0 3.7	456.8 1.9
+50	455.4 3.3	454.5 4.2	456.4 2.3
1+00	454.6 4.1	454.2 4.5	455.1 3.6
+50	454.3 4.4	453.8 4.9	454.5 4.2
0+00	453.1 5.6	453.0 5.7	453.3 5.4

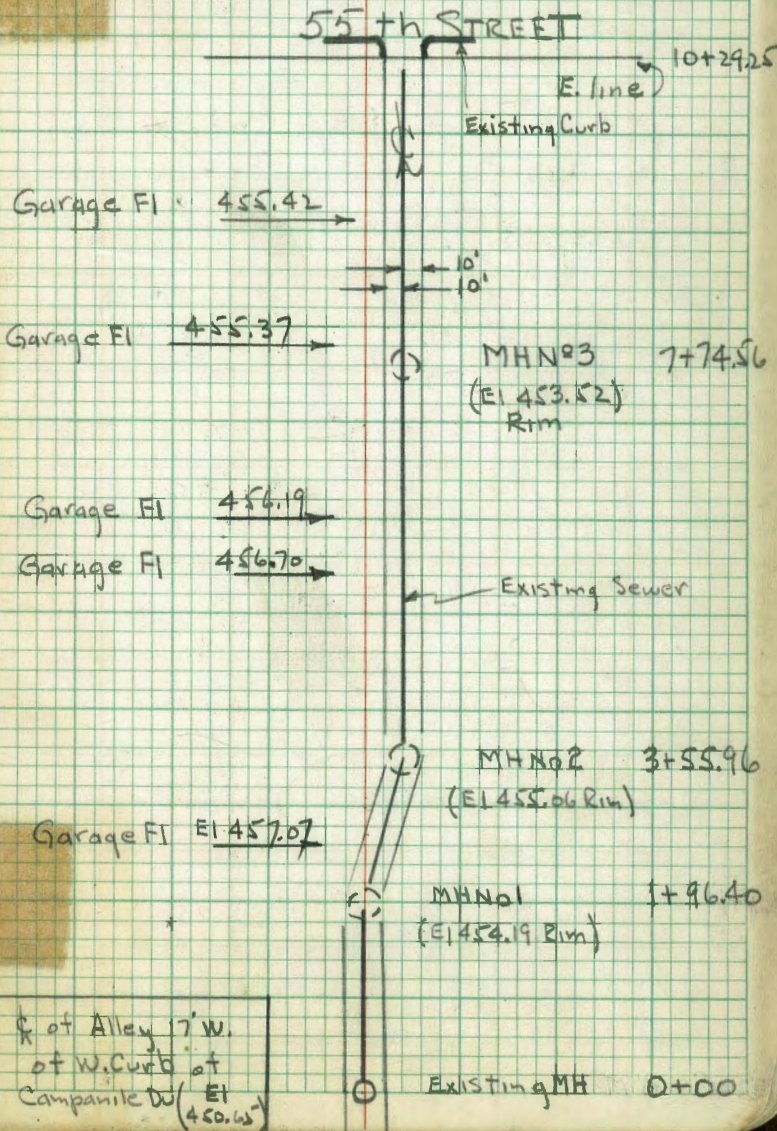
HI 458.66

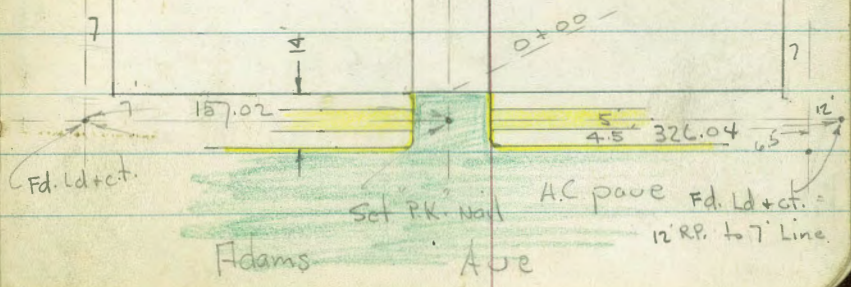
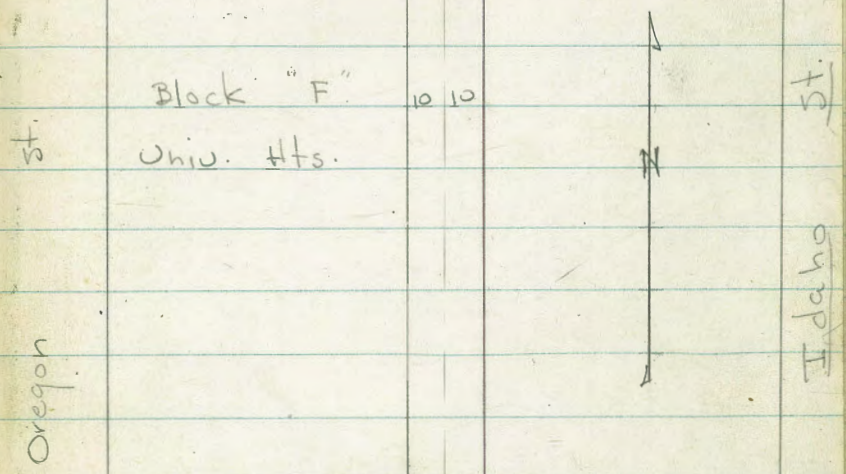
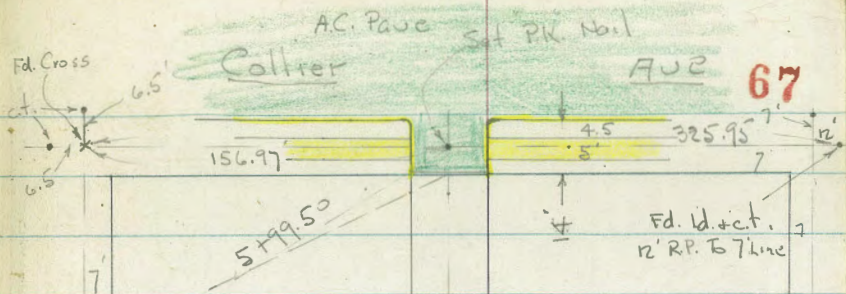
INDEXED

Survey  
 AUG 21 1952

8-23-51  
 DANIELS  
 HALL

Alley between Lots 1-29  
 (Collwood Gardens)







Lt

Rt 68

INDEVEN

AUG 17 1951

X-Sept. 20 Alley in Block "F" - Univ. Hts.  
for Paving.

# 5703

8-15-51

W.O. 21909

7.0

0+65- 10.1' Lt. = end walk

86.88

10.1  
walk  
cor.

0+55

86.99

86.7

87.1

86.7

87.72

10

10

10

10

edge  
walk

Top wall

0+42- 10.1' pt. = Beg. Brick wall

86.45

87.63

87.14

10.1

10.1

11.8 = wh.

2' Conc. walk = 12.2' Lt. = Cor. Grav. - Conc. floor - opens South

Bottom

Top

walk

wall

wall

0+35- 9.5' Lt. = Beg. picket fence at Ely. of

86.97

86.86

12.2

9.8 = Cor.

floor.

walk

Grav.

0+25

86.79

86.2

86.5

86.1

86.65

10

10

10

11.7 = wly of

10' Lt. Beg. 4" Conc. Block Border for Hedge - Top cb.

Top Conc.  
Block

2' Conc. walk

0+00 = N.L. Adams - end of A.C. pave &amp; curbs.

85.76

85.67

85.36

85.63

85.76

Top

10

10

Top

gut.

gut.

0-14 = Uicb. Line of Adams.

85.34

84.80

85.41

84.89

84.93

85.03

85.64

85.22

85.76

Top

50

Top

10

10

Top

50

Top

gut.

2' Rad.

gut.

2' Rad.

gut.

Top

Note: used elev. Rod. - actual Elev. shown

B.M. = S.E. B.P. - Adams + Idaho 384.91

300' Elev. Not  
Noted.

Lt.      #      Rt.      **69**

1+98- 11.4' Lt. = end Conc. apron  
to Doub. Gar.

87.60      87.53  
13.2      11.4 = apron  
floor.  
gar.

1+90.5- 11' Rt. = end Conc. slope + Beg. Conc. apron

87.53  
11 = Conc. + apron

1+75- 10.9' Rt. = Beg. Conc. slope to Rock cactus  
garden.

87.95  
10.9 = edge  
Conc

1+70- 11.5 = apron on Lt.

87.60  
11.5 = apron

1+50

87.30      87.3      87.4      87.4      87.4  
11.3      10      10      15  
apron

1+47.5- 10' Rt. = end Conc. apron

87.31      87.65  
10      14.9  
apron      floor

1+46- 11.4' Lt. = Beg. Conc. apron to 5 car Gar.

87.31      87.26  
13.1      11.4 = apron  
floor  
gar.

1+26 = Middle of Gar.

87.26  
10 =  
apron

1+07- 14.9' Lt. = ± Sing Gar Conc. apron

87.45      87.38  
16.5      14.9 = apron

1+03- 9.8' Rt. = Beg. Conc. apron to 4 car Gar.

87.22      87.63  
9.8      14.9 = floor  
apron      gar.

1+00

87.2      87.4      87.1      87.3  
10      10      15

0+97- 10.4' Lt. = end fence

0+89- 10' Rt. = end wall

87.0      86.79      87.72  
10      10      10  
ground      Bottom      Top  
                 wall

0+69- 8.5' Lt. = ± P. pole # P.A. 4711

Sing. Gar. - Conc. floor  
3+60 - 9.8' Lt. =  $\pm$  11.5' Broken up Conc. Dr. to

3+50

3+27 - 8.7' Lt. =  $\pm$  P. pole # Spike in Pole = B.M.  
P.A. 4751

3+00 - 9.7' Lt. = end fence

2+94 - 13' Rt. =  $\pm$  Sing. Gar. - Conc. floor

2+65 - 11.9' Rt. =  $\pm$  frame House - Conc. found.

2+62 - 10' Lt. = end lath + beg. wire fence

2+52 - 12.2' Rt. =  $\pm$  3.5' Conc. walk

2+50

2+25 - 9.7' Lt. = Beg. lath fence

2+24 - 9.2' Lt. =  $\pm$  P. pole # P.A. 4731

2+19 - 11.7' Lt. = end conc. apron

2+12 - 10.7' Rt. = end apron

2+05 - 11.6' Lt. = Beg. Conc. apron to doub. Gar.

2+00

Lt.  $\pm$  Rt. 71

89.53  
1.8 = walk

89.48 89.59  
.11.9 16.6  
apron floor

90.1 90.3 89.7 89.6 89.6  
15 10 10 15

89.5 89.3 89.6 89.3  
10 10 15

89.5 89.5 88.8 88.8 88.8  
20 10 10 20

89.61  
16.2 = floor

89.1 88.9 88.7 88.7 88.9  
20 10 10 15

Lt

±

Rt

check B.M. - N.W. Utah + Collier 391.50

391.55 = Book

add outs showing flat gutter to E.

88.58 88.61  
75 100  
gut gut

6 + 13.50 = S. cb. line

88.58 88.72 88.98 88.45 88.38 88.49 89.00 88.50 89.04  
Top 50 Top 10 10 Top 50 Top  
gut. 2' Rad. gut. gut. 2' Rad. gut. Top

6 + 04.5 = 7.9' Rt. = end wly. of Hedge

S.L. - Pav. edge is 0.4' N. - Rods on edge of  
5 + 99.50 = S.L. Collier Ave. - curbs end on

89.01 89.81 89.63 8.50 88.96 89.26  
Top 99 8.4 10 10 11.9  
cb. gut. edge of. gut. Top cb. - end.  
ent Hedge edge walk

5 + 95.5 - 9.4' Lt. = Tel pole # D-38994 - T = 390.62

5 + 91 - 10.4' Lt. = end fence

5 + 84 - 8.8' Rt. = wly of 3.5' High Cypress Hedge

5 + 75

89.9 89.4 89.7 89.86  
10 10 11.9  
wly walk

Levels Alley East of 55th St.  
Between Lindo Pasco & Montezuma

H=5

May 8-52  
R.F.N. F.S. No. 73  
Garber Fritz

+240

457.20  
57.1 53.5 56.4 56.4  
1.10 1.8 3.8 1.9 1.9  
15.3 10 10 35  
15:30 - 11:00 am  
Cant. Floor

+50

57.2 51.5 54.0 56.5 56.3  
1.10 1.8 4.3 1.8 2.0  
15:30 - 11:00 am  
Cant. Floor

+33 = Fly Garage on H.

57.5 53.7 56.3 56.3  
1.89 1.8 4.6 2.0 2.0  
15:30 - 11:00 am  
Fly Garage on 1st Floor

+10

55.9 53.4 56.0 56.1  
2.4 4.9 2.3 2.8  
12 10 35

+50

53.9  
4.4

0+0

53.10  
5.1

B.M.

454

458.00

453.76

Spk Pole  
Rtop.  
1+54  
on Prob. 6

458.30

♂

♀

+71 = Fly Garage on Lt

70.25  
 1.71  
 1.84 = Fly Garage  
 Calc. Floor

56.5	54.5	56.2
20	40	2.3
10		10

+150

56.6	54.5	56.4	56.0
19	40	2.1	2.5
10		10	35

4+0

56.5	54.6	56.4	56.4
20	39	2.1	2.1
10		10	35

TP 3.84

458.54 3.10

455.20

458.54

+5596

0.79  
 3.48 = Fly Garage  
 Calc. Floor

57.81	56.8	55.1	56.1	55.8
15	32	2.2	2.5	2.5
10		10	35	

3+0

0.77  
 2.78 = Fly Garage  
 Calc. Floor

56.5	54.7	56.3	56.2
18	3.6	2.0	2.1
10		10	35

2+60

0.78  
 2.25 = Fly Garage  
 Calc. Floor

57.52 - 56.6	54.5	56.2	56.3
17	3.8	2.1	2.0
10		10	35

458.30

458.30

Lt.

Lt.

Rt.

75

+50

54.5  
4.0  
10

53.1  
5.4

53.3  
5.2  
10

53.0  
5.6  
35

+70

54.8  
3.7  
16

53.3  
5.2

53.7  
4.8  
10

53.5  
5.0  
18 = Cross  
Fence

+50

18.29  
22.5  
18.5 = NY Garage

55.5  
3.0  
10

53.4  
5.1

54.3  
4.2  
10

54.2  
4.2  
35

+60

56.31  
22.3  
18.5 = NY Garage

55.7  
2.8  
10

53.7  
4.8

54.7  
3.8  
10

54.9  
3.6  
35

+77

= Fly Garage on Lt.

18.29  
22.3  
18.5 = NY Garage

55.8  
2.7  
16

53.8  
4.7

55.0  
2.5  
10

55.2  
2.2  
35

+50

18.29  
1.73  
1.86 = NY Garage

56.4  
2.1  
10

53.9  
4.6

55.2  
3.3  
10

55.1  
3.1  
35

+50

56.82  
1.72  
1.86 = NY Garage

54.3  
2.2  
10

54.3  
4.2

55.4  
3.1  
10

56.0  
2.5  
35

45854

45854

Lt.

2

Pt

76

450

55.55	54.5	52.5	53.2	52.6
2.11	3.2	4.2	4.5	5.1
18.5	10		10	35

FLY GARAGE  
Cont. Floor

940

55.55	55.1	52.8	52.9	52.9
2.11	2.6	4.9	4.8	4.8
18.5	10		10	35

FLY GARAGE  
Cont. Floor

783

55.2	53.1	53.2	52.9
2.11	2.5	4.6	4.5
18.5	10		10

FLY GARAGE  
Cont. Floor

750

55.83	55.0	53.1	52.9	52.9
1.82	2.7	4.6	4.8	4.8
18.5	10		10	35

FLY GARAGE  
Cont. Floor

840

54.6	53.2	53.0	52.9
1.85	3.1	4.5	4.7
18.5	10		10

FLY GARAGE  
Cont. Floor

7477

FLY GARAGE Cont. Floor

55.9	55.0	53.7	53.2	52.9
1.83	2.7	4.0	4.4	4.8
18.5	10		10	35

FLY GARAGE  
Cont. Floor

TP

459

457.66 5.47

452.07

458.54

457.66



Lt. South

L

PTEN 77

B.M.

3.07 453.89

HERP  
Montezuma  
453.91  
Page 14

TP 2.50 456.96 420 453.46

+42 = East Curb Line 55<sup>th</sup> St.

+30 = FL 55<sup>th</sup>

10x0

9+68 = N<sup>W</sup> Entrance of Garage on Lt.

457.66

4.45  
16: Curb  
Top

48

4.67  
16: Curb  
TOP

0.00  
30  
106  
10: Top  
End

5.1

4.21  
10: Top  
End

54.6

52.6

53.3

52.8

3.2  
10

5.1

4.4  
10

4.9  
35

457.53

54.7

52.5

53.1

52.6

21  
18 = N<sup>W</sup> Entrance of Garage on  
Conc. Floors

3.0  
10

5.2

4.6  
10

5.1  
35

457.66

78



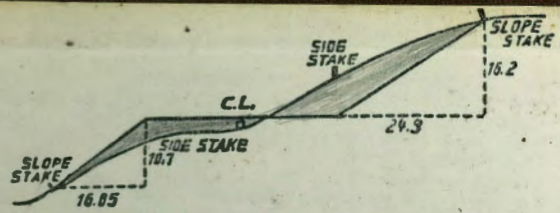
441.01  
 56 Lt. \$ 11.00  
 1.55  
 1550

7736  
 472  
 7264

12 73  
 430  
 173

80.57  
 5195  
 74.62

3604 Pershing - Penick



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY  
 HOLYOKE MASSACHUSETTS  
 NEW YORK CHICAGO BOSTON SAN FRANCISCO