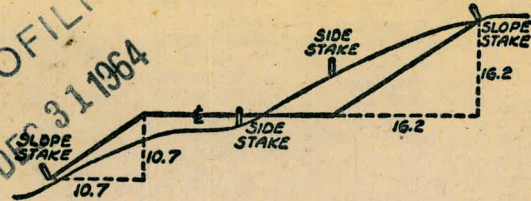


2054

TRAVEL BOOK

MICROFILMED
DEC 31 1964



4744

INDEXED

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Alvarado Sewer
Line Change of 463

For final line see F.B. 2040

also

F.B. 1629

✓ 1631

✓ 1703

✓ 1873

✓ 2003

✓ 2040

College outfall

66 to 78

W.O. 20129 Alvarado Sewer
Line Change from
463+80.86 (See 1873
28)

10-11-49 Clear Nat'l
McCoy
Moore
Herrcomb

465+20 87+30.63

131.2 ✓
11.5

+50 86+80.63

129.1 ✓
13.6

+10 86+40.63

~~10.1~~

~~16.3~~

126.4 ✓
16.3

464+00 86+30.63

124.7 ✓
18.0

463+80.86 = 86+11.49
@ 35° 10' RT.

123.2 ✓
19.5

468+67.23 - 3.09
2003
63.

142.71 ✓

139.61 ✓

142.71 ✓

T.P. 12.43 $\langle 166.79 \rangle$ 0.40 $\langle 154.36 \rangle$

+50 90+80.63

149.5 ✓
5.3

468 90+80.63

143.8 ✓
11.0

+50 89+80.63

142.9 ✓
11.9

T.P. 12.42 $\langle 154.76 \rangle$ 0.37 $\langle 142.34 \rangle$

467+00 - in old Road.
89+80.63

~~road~~

$\langle 154.76 \rangle$
141.4 ✓
1.3

+50 88+80.63

138.9 ✓
3.8

466+00 88+80.63

137.3 ✓
5.4

465+50 89+80.63

135.1 ✓
7.6

$\langle 142.71 \rangle$

$\langle 142.71 \rangle$ ✓

T.P. 13.28 <204.13> 0.80 <190.85>

+50

471

T.P. ^(near start +40) 12.69 <191.65> 0.35 <178.96>

+40

470

+78

T.P. 12.93 <179.31> 0.41 <166.38>

+50

469

<166.79>

<204.13>

187.6
4.0

184.2
7.4

<191.65>

178.5
0.80

170.7
8.6

166.8
12.5

<179.31>

163.2
3.6

155.4
11.4

<166.79>

+12

+09

Top. Loose Rock

A73

+93

+85

T.P.

12.16

$\langle 216.17 \rangle$

0.12

$\langle 204.01 \rangle$

+70

+57

+40

+1A

A72

$\langle 204.13 \rangle$

214.3 ✓

1.9

215.5 ✓

.7

209.2 ✓

7.0

206.6 ✓

9.6

205.1 ✓

11.1

$\langle 216.17 \rangle$

203.6 ✓

0.5

200.3 ✓

3.8

198.6 ✓

5.5

193.6 ✓

10.5

189.0 ✓

15.1

10.4 ✓

192.2 ✓

11.9

194.9 ✓

9.2

10 Rt ✓

$\langle 204.13 \rangle$

473 + 97

473 + 96.⁶⁶

T.P. Sub-473 + 96.⁶⁶

+90

+70

+60

+50

+39

+34

+30

T.P.

6.54

222.68

0.03

216.14

216.17

2 Levels

New line and Levels from here see Pg 11 for Sketch

1.72 220.42

218.70

Boulder 5' Rt

Top. loose Boulder

217.0

3.4

220.42

218.70

3.98

218.6

4.1

219.4

3.3

218.7

4.0

216.4

6.3

216.4

6.3

218.7

4.0

216.6

6.1

222.68

218.5

1.9

7.2

5

218.56

2003.

63 + 68

+31 Bottom Wash

+28 Bottom Wash

+26 edge Solid Rock

+21.55 Δ in ϕ flat Rock 8x8

\leftarrow (A changed to 474+22.35
see sketch pg 11 left)

+16.7

+16.5

+10.5

+10 edge Solid

+08 "

47A

on loose rock

202.4 \checkmark
18.01 97.8 \checkmark
22.6207.5 \checkmark
12.9207.4 \checkmark
13.0207.6 \checkmark
12.8205.4 \checkmark
15.0206.4 \checkmark
14.0210.3 \checkmark
10.1210.4 \checkmark
10.0215.2 \checkmark
5.2 \langle 220.42 \rangle

+63 Solid Rock

+62 Solid Rock

+61

+60.5

+59

+56

Rock 5 R + 3 L.

+50

figure

+48.5

edge Rock.

+48

1.7 R
edge Rock

+38.5

9x6. Red R edge 1. R.

+38

A7A + 36

$\frac{132}{4.04}$

207.8 ✓
12.6

212.9
 $\frac{7.5}{5R}$

211.2 ✓
9.2

7

209.6 ✓
10.8

209.2 ✓
11.2

210.7
9.5

211.1 ✓
9.3

207.8 ✓
12.6

207.5 ✓
12.9

210.7 ✓
9.7

210.9 ✓
9.5

205.9 ✓
14.5

202.3 ✓
18.1

<220.42>

Continued Page 13

0+08 Bridge survey #1.

474 + 95.5 = 0+05.30W
#1 Bridge survey Levels 1873 F.B.

+86

+79

+77.

+77 face big rock on Rd

+73

<220.4>

205.4	214.4
<u>15.0</u>	<u>6.0</u>
116	96

205.0
<u>15.4</u>
5.6

205.0
<u>15.4</u>
5.6

203.8	207.3
<u>16.6</u>	<u>13.1</u>
6.4	5.6
Rock L.	

215.22 ✓
5.20 3' below J.G. Pipe.214.75 ✓
5.65214.7 ✓
5.7213.4 ✓
7.0205.1 ✓
15.5208.5 ✓
11.9

<220.42>

213.2 ✓
7.2
10R

212.8	214.6
<u>7.6</u>	<u>5.8</u>
10R	13.

205.3	212.7	214.5
<u>15.1</u>	<u>7.7</u>	<u>5.9</u>
3.5R	4'R	9R

209.5 ✓
10.9
5R + R.R.

Newcomb
McCoy
W. Moore

10-12-49

Recheck of Levels
on line from 468+67.49
to 472+60 (Orig. Levels $\frac{2003}{63}$)

Step level
shown photo

+87
+50

T.P. Rock 12.10 <176.83> 0.19 <164.73>

+50

+10

470

+85

T.P. (Rock) 12.46 <164.92> 0.20 <152.46>

+50

+30

+10

469

468+67.49 13.04 <152.66> <139.62> Page 1
+
2003
63

161.2 ✓
 $\frac{15.6}{10}$

167.0 ✓
9.8

1655 ✓
 $\frac{11.3}{10}$

9

<176.83>

163.2 ✓
1.7

160.3 ✓
4.6

158.6 ✓
6.3

155.6 ✓
9.3

<164.92>

152.0 ✓
0.7

149.0 ✓
3.7

145.6 ✓
7.1

140.0 ✓
 $\frac{12.7}{20}$

143.4 ✓
9.3

147.8 ✓
4.9
20

138.3 ✓
 $\frac{14.4}{20}$

141.1 ✓ 145.1 ✓
 $\frac{11.6}{15}$ $\frac{7.6}{30}$

<152.66>

B.M. Top 6 Round Boulder 3 out of ground
52'R 472+25 $1.40 \langle 200.04 \rangle$

T.P. (rock) $12.48 \langle 201.44 \rangle$ $0.58 \langle 188.96 \rangle$

+60

+35

472.

T.P. (rock)

$13.16 \langle 189.54 \rangle$ $0.45 \langle 176.38 \rangle$

+65

+50

+10

A71

$\langle 176.83 \rangle$

$\frac{185.5 \checkmark}{10}$

$\frac{181.3 \checkmark}{8.2}$
 $\frac{10}{10}$

$\frac{176.1 \checkmark}{13.4}$
 $\frac{10}{10}$

$\frac{189.0 \checkmark}{0.5}$

$\frac{184.3 \checkmark}{5.2}$

$\frac{178.5 \checkmark}{11.0}$

$\frac{193.5 \checkmark}{10}$

$\frac{188.0 \checkmark}{1.5}$
 $\frac{10}{10}$

$\frac{181.2 \checkmark}{8.3}$
 $\frac{10}{10}$

$\langle 189.54 \rangle \checkmark$

$\frac{171.6 \checkmark}{5.2}$
 $\frac{10}{10}$

$\frac{173.9 \checkmark}{2.9}$

$\frac{175.6 \checkmark}{1.2}$
 $\frac{5}{5}$

$\frac{173.1 \checkmark}{3.7}$

$\frac{171.2 \checkmark}{5.6}$

$\frac{169.8 \checkmark}{1.0}$

$\langle 176.83 \rangle \checkmark$

10-13-49
H.C. Coy
Morr
Herrcomb.

Levels from
here. Pg. 13

207. on Rock
478+97.89

493.10' Rt.
475+54.22



0+08 #1 Bridge Survey
FB 1873

= 474+95.77 Ah.
474+96.30
Δ 29° 30' Lt.

Δ 47° 28' Lt.
474+95.77 × 0.0530
Bridge Survey

0+00
#1 Bridge Survey
1873

Voided See 2003
69-58

(Voided)
474+21.55
79.6

37° 13' Lt.
474+30.20 Back = 474+22.25 Ah.

Stub
473+96.66
(FB-2003)
63-68

473+61.52 Δ 19° 10' Rt. (11/30/49)

on Loose Rock
on Loose Rock
on Loose Rock

(Levels Pg. 13)

11

478+92.88 Δ 13° 06' Rt.
478+73
478+43.

478+16.01 = 478+16.68 old line
Δ 22° 57' Lt.

~~477+60.95 Ah.~~
477+60.95 Ah. ←
Δ 13° 29' Lt.
477+60.44 Back =
(11/30/49)

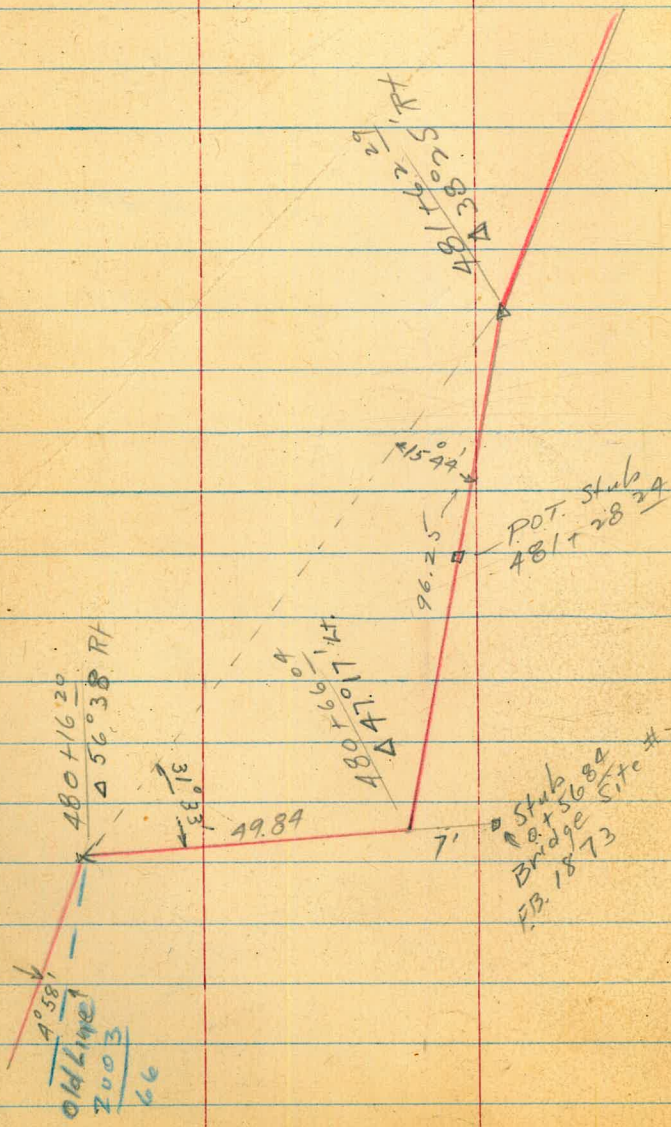
477+00.71 11/30/49
= Δ 44° 42' Lt.
out
477+07.88
429' 29' Lt.

57' in loose rock
476+59.21
262' 57' Lt.
Δ = 22° 30' 11/30/49

on Rock
475+97.89

Top small loose rock
475+62.22

475+54.22
0+6375
Δ 43° 10' Lt.



1' N of Approx Brd
of 21" Y.C. Beamed
Pipe Under Freeway.

erished Pt. on Rock

(Levels P917
To 2, 1)

485+19.75
40
485+59.75
1+80.
487+39.75
8+24 38
82.63

485+19.75

488+95 P.O.T.

482+68.75 Δ 21° 51' RT

481+62.29 Δ 38° 25' RT

481+28.24 POT (Stub)

480+16.20
49.84
480+66.04
24
480+90.04

Bonhard Granite Hedge
Near Bridge Site No II

Pt on Large Loose Rock

486+66.04 Δ 47° 17' LT

Bridge Site No II

480+16.20 Δ 56° 38' RT

4° 58' Old Line
See 2003
66

479+41.00

10-14-49
 Mc Coy
 Moore
 Newcomb

L.R. = boose Rock
 S.W. Solid Ledge

13

235.2 233.9 233.9 ✓
 $\frac{4.1}{10.0}$ $\frac{5.9}{6.0}$ $\frac{5.4}{1.0 \text{ w.R.}}$ 229.5 228.1
 9.8 11.2
 10.

+50.0

231.4 ✓
 $\frac{7.9}{10.0}$ 228.4 ✓
 10.9 11.6 227.7 225.9
 5.0 13.4
 10.0

+25

231.2 ✓
 $\frac{8.1}{10.0}$ 228.5 ✓
 10.8 227.7 ✓
 11.6
 7.0

+10

231.2 ✓
 $\frac{8.1}{10.0}$ 228.2 ✓
 11.1 226.4 ✓
 12.9
 8.0

476 + 00

⟨239.28⟩ ✓

T.P. top Rock 187

13.18 ⟨239.28⟩ ✓ 0.67 ⟨226.10⟩ ✓

226.0 ✓
 $\frac{0.8}{5.0}$ 224.3 ✓
 2.5 222.9 ✓
 3.9
 8

+80

225.1 ✓
 $\frac{1.7}{5.0}$ 224.1 ✓
 2.7 223.8 ✓ 221.9 ✓ 215.4 ✓
 3.0 4.9 11.4
 1. 1.5 10

+73 top Solid rock

221.1 ✓
 $\frac{5.7}{3.0}$ 220.7 ✓
 3. 216.6 ✓ 215.3 ✓
 10.2 11.5
 4 10.

+68.5

226.8 ✓ 225.2 ✓ 220.5 ✓
 $\frac{0.6}{7.0}$ $\frac{1.6}{4.0}$ $\frac{6.3}{3.0}$ 218.7 ✓
 8.1 216.4 ✓ 215.3 ✓
 10.4 11.5
 5.0 10.0

+67.5

224.8 ✓ 219.6 ✓
 $\frac{2.0}{3.0}$ $\frac{7.2}{2.0}$ 216.3 ✓
 10.5 215.0 ✓
 11.8
 7.0

+62

475 + 54.22 = 1063.75 Bridge Site 1 FB 1873

214.47 ✓
 12.30

Sub 473 + 96.66

8.01 ⟨226.77⟩ ✓
 ⟨218.70⟩ 995

⟨226.77⟩ ✓

+27

478 + 16.01 Δ

478

+83

477 + 60.95

+33

+22

477 + 07.58

1.P. 477 + 07.58 ~~1.1~~

f75

476 + 59.21

12.57 < 251.57 >

0.28

239.00

254.3
+ 2.7
7

253.9
+ 2.3
10.0

253.6
+ 2.0
10

251.3
0.3
10.0

248.7
2.9
10.0

244.8
6.8
10.0

243.3
8.3
10

10.7
10.0

239.6
+ 3
10.0

239.9
4.4
10

250.5
1.1

249.29
2.28

249.4
2.2

246.1
5.5

245.6
6.0

243.4
8.2

240.7
10.9

< 251.57 >
239.0
0.28

236.1
2.9

232.34
6.89

< 239.28 >

249.0 247.0
2.6 4.6
6 11

246.1
5.5
10.0

241.9
9.7
10.

242.4
9.2
10.0

250.6
11.0
10.0

242.7 240.8
8.9 10.8
5.0 10

238.8
12.8
10

237.0
14.6
10.0

235.1
4.2
10

230.4
8.9
10

14

+ 30

$$\begin{array}{r} 259.0 \\ 0.0 \\ \hline 7.0 \end{array}$$

$$\begin{array}{r} 252.9 \\ 6.1 \\ 4.0 \\ \hline \text{ledge} \end{array}$$

$$\begin{array}{r} \checkmark \\ 257.6 \\ 7.4 \end{array}$$

$$\begin{array}{r} 248.3 \\ 10.7 \\ \hline 5.0 \end{array}$$

+ 10.

$$\begin{array}{r} 259.0 \\ 0.0 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} 253.8 \\ 5.2 \\ 4.0 \end{array}$$

$$\begin{array}{r} \checkmark \\ 257.5 \\ 7.5 \end{array}$$

$$\begin{array}{r} 249.8 \\ 14.2 \\ \hline 10 \end{array}$$

479.

on Hedge Loose Rock

$$\begin{array}{r} 258.0 \\ 1.0 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} \checkmark \\ 254.3 \\ 4.7 \text{ L.R.} \end{array}$$

$$\begin{array}{r} 253.7 \\ 5.3 \\ 12.8 \\ \hline 4.0 \text{ L.R.} \end{array}$$

$$\begin{array}{r} 246.2 \\ 8.0 \text{ Below} \\ \hline \text{L.R.} \end{array}$$

478 + 92.88 sub.

$$\begin{array}{r} 259.5 \\ 0.5 \\ \hline 10 \end{array}$$

$$\begin{array}{r} \checkmark \\ 253.42 \\ 5.62 \end{array}$$

$$\begin{array}{r} 250.0 \\ 9.0 \\ \hline 7.0 \text{ ledge break} \end{array}$$

limit ht.

$$\begin{array}{r} \text{L.R. } 258.7 \\ 254.6 \\ - .8 \\ \hline 7.0 \end{array}$$

$$\begin{array}{r} \checkmark \\ 252.7 \\ 6.3 \end{array}$$

$$\begin{array}{r} 249.4 \\ 9.6 \\ \hline 5.0 \text{ limit Right} \end{array}$$

+ 83

+ 73

on Lg Rock Loose.

$$\begin{array}{r} \checkmark \\ 255.3 \\ 3.7 \end{array}$$

+ 72

$$\begin{array}{r} 256.0 \\ 3.0 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 252.4 \\ 6.6 \\ 2.0 \end{array}$$

$$\begin{array}{r} \checkmark \\ 257.5 \\ 7.5 \end{array}$$

$$\begin{array}{r} 248.1 \\ 10.9 \\ 6.0 \end{array}$$

$$\begin{array}{r} 247.0 \\ 12.0 \\ \hline 10.0 \end{array}$$

+ 57

$$\begin{array}{r} 258.4 \\ 0.6 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} \checkmark \\ 254.1 \\ 4.9 \end{array}$$

$$\begin{array}{r} 252.0 \\ 7.0 \\ 3.0 \end{array}$$

$$\begin{array}{r} 249.8 \\ 9.2 \\ \hline 11.0 \end{array}$$

+ 43

$$\begin{array}{r} 257.5 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} \checkmark \\ 254.6 \\ 4.4 \end{array}$$

$$\begin{array}{r} \checkmark \\ 253.1 \\ 5.9 \\ 3.0 \end{array}$$

$$\begin{array}{r} 250.6 \\ 8.4 \\ \hline 15 \end{array}$$

Ledge

I.P. L.R.

$$1.86 \langle 259.0A \rangle$$

$$0.39 \langle 251.15 \rangle$$

$$\langle 259.04 \rangle$$

480+78.05 Δ all Station

480+16.20 Δ = 0+00 of Bridge Site No. II.

480+05

+96

+92

+85

+78

+70

+55

+44

479 + 40 on big loose Rock.

257
1.3
458.3

4.5
2.4
2.1

1873
60

4.1
1.3
2.8

4.1
2.4
1.7

257.0
1.3
258.3
4.1
254.2

2.0

254.6 I.G.
3

257.6 fall sand
1.5 I.G.

259.1 I.G.
2003
66
256.8

16

251.02
2.02
254.63
4.41

258.1 255.1 253.7 253.5 251.0 249.7
0.9 3.9 5.3 5.5 8.0 9.3
10. 1.5 1.0 5.0 5.0 10.0
Wedge S.L.

258.3 256.8 253.9 253.2 250.6 249.1
0.7 2.2 5.1 5.7 8.4 8.9
7.5 2.0 5 5.0 7.0 10
S.L.

258.3 255.8 254.7 257.3 253.3 249.5
0.7 3.2 4.3 4.7 5.7 8.5
7.0 3.5 7.0 S.L. 10.0 12

259.0 254.6 257.2 253.5 253.6 251.1
0.0 4.4 4.8 5.5 5.4 7.9
4.0 Wedge 2.0 4.0 6.0
S.L.

257.0 252.8 252.5 248.1
2.0 6.2 6.5 10.9
5.0 5.2 2.0 4.0 8.0
Wedge Wedge

257.2 253.9 250.9 250.7 249.6
1.8 5.1 8.1 8.3 14.4
5.0 4.0 6.0 10

255.9 252.9 249.1
on ledge on ledge 252.2 9.9
3.1 6.1 6.8 6.0
5.0 2.0

255.0 249.1 247.8
4.0 252.4 9.9 11.2
5.0 6.6 3.0 6.0

256.0
3.0

259.04

10-17-49 Rain
McCoy
Moore
Hewcomb.

3.4

481 + 62.29

267.2
12.3
10.

268.97 ✓
10.2
10.55
269.3
10.2
272.0
7.5
8.5
10.
271.0
17

+50

263.6
15.9
10.

267.2 ✓
12.3

271.1
8.4
10.

+38

263.5
16.0
10.

267.9 ✓
11.6

271.2
8.3
10

T.P. Δ 481 + 28.24 11.51 (279.52) ✓
481 + 25 + 4.7 to R = 481 + 23.24 old line

0.57 (267.95) ✓

264.0
15.5
10.

263.6
15.9
4.0

267.2
12.3
2.0

270.2
9.3
10

(279.52) ✓

+16

258.7
9.8
11.

263.5
5.0
2.

266.1 ✓
2.4
S.R.

268.5
0.0
10.

+11

255.8
12.7
15.0

261.3
7.2
5.0

263.5 ✓
6.0

264.2
4.3
7.0

266.3
2.2
12.

481

252.5
16.0
14.

254.5
14.0
9.

260.9 ✓
7.6

265.9
2.6
10

+90

255.0
13.5
11.

256.1
12.4
3.

258.4 ✓
10.1

262.5 ✓
6.0
5.

265.7
2.8
10

+73

Corner edge 251.7
16.8
7

253.8 ✓
14.7

258.0
10.5
10

(Sketch Pg 12)

480 + 66.04 (ent top large loose rock)

Sketch
P. 12

480 + 78.05 18. 11.50 (268.52) ✓

(257.02) P. 16

253.6 ✓
14.9
(268.52) ✓

482 + 89

+ 81

+ 75

Δ 482 + 68.75

+ 62

+ 48

+ 15

482

+ 85

281 + 70

 $\langle 279.52 \rangle$ 266.6
Creek

267.6	271.0	271.3	274.7	276.0
$\frac{12.9}{10}$	$\frac{11.9}{8.0}$	$\frac{8.5}{6.0}$	$\frac{4.8}{3.}$	$\frac{3.5}{10}$

267.1	268.5	271.0	273.0	273.8	276.1
$\frac{12.4}{10}$	$\frac{11.0}{8}$	$\frac{8.5}{5.}$	$\frac{6.5}{5.0}$	$\frac{5.7}{L.R.}$	$\frac{3.4}{10}$

268.6	268.8	270.4	270.7	274.7	275.9
$\frac{10.9}{L.R.}$	$\frac{10.7}{5}$	$\frac{9.1}{L.R.}$	$\frac{8.8}{1.0}$	$\frac{4.8}{6.}$	$\frac{3.6}{10}$

266.9	273.9	274.2	271.5	271.8	275.3
$\frac{12.6}{8}$ L.R.	$\frac{5.6}{6.0}$ Rock	$\frac{5.3}{4.}$ Rock	$\frac{8.0}{1.0}$	$\frac{7.7}{2}$	$\frac{4.2}{10}$

267.9	272.9	272.2	272.3	274.9
$\frac{12.1}{10.}$	$\frac{6.6}{5.0}$ Rock	$\frac{7.3}{2}$ Creek	$\frac{7.2}{L.R.}$	$\frac{4.6}{10}$

269.9	270.7	271.6	275.2
$\frac{9.6}{10}$	$\frac{8.8}{3.}$	$\frac{7.9}{L.R.}$	$\frac{4.3}{10}$

265.5	269.2	271.5	273.2
$\frac{14.0}{16.}$	$\frac{10.3}{10.}$	$\frac{8.0}{L.R.}$	$\frac{6.3}{10.}$

267.8	271.8	272.5	274.5
$\frac{11.7}{20}$	$\frac{7.7}{10.}$	$\frac{7.0}{L.R.}$	$\frac{5.0}{10.}$

269.2	271.2	271.8	273.4
$\frac{10.3}{20}$	$\frac{8.3}{10}$	$\frac{7.7}{L.R.}$	$\frac{6.1}{10}$

269.4	270.9	272.1
$\frac{10.1}{10}$	$\frac{8.6}{L.R.}$	$\frac{7.4}{10}$

 $\langle 279.52 \rangle$

+31

271.6
12.2

+41

275.8	274.0	273.8	273.5	275.5
8.0	9.8	10.0	10.3	8.2
B.R.	7.0	5R	5	10
	270.5	272.0	272.2	274.6
	13.3	11.8	11.6	9.2
	1.0		5	6
				8.0

+33

271.0
12.8

+29

267.7	269.5	274.0	273.9	275.9
14.1	14.3	9.8	9.9	7.9
10	1.0		5	10
B.R.	B.R.			
268.4	270.8	273.1	274.3	276.3
15.4	13.0	10.7	9.5	7.5
8	3	2	5	10
B.R.			S.R.	

+27

+20

TR old subs. 483+39.91 not on line 792 (283 .84) 3.60 (275.92)

(283.84)

+12

275.1
44 top Rock horse

+06

268.0	270.6	270.2	274.9
11.5	8.9	9.3	4.6
B.R.	6.0	2	

+03

267.8	269.6	271.1	272.4	275.3	275.8
B.R.	11.7	9.9	7.1	9.2	3.7
	7	5	4	5	10

483+0A

(279.54)

(279.52)

+75

+50

+25

ABA

483 + 95.00

+85

+75

+71

+61

+55

⟨283.84⟩

275.6

$$\begin{array}{r} 8.2 \\ 10 \end{array}$$

$$\begin{array}{r} 275.7 \\ 8.1 \end{array}$$

276.4 278.2

$$\begin{array}{r} 7.4 \\ 15 \end{array} \quad \begin{array}{r} 5.6 \\ 25 \end{array}$$

275.4 274.2 274.6

$$\begin{array}{r} 8.4 \\ 10 \end{array} \quad \begin{array}{r} 9.6 \\ 6 \end{array} \quad \begin{array}{r} 9.2 \\ 2 \end{array}$$

LR LR

$$\begin{array}{r} 275.3 \\ 8.5 \end{array}$$

$$\begin{array}{r} 274.8 \\ 9.0 \\ 5 \end{array}$$

$$\begin{array}{r} 274.6 \\ 9.2 \\ 11 \end{array}$$

$$\begin{array}{r} 275.7 \\ 8.1 \\ 15 \end{array}$$

274.2

$$\begin{array}{r} 9.6 \\ 10 \end{array}$$

$$\begin{array}{r} 274.4 \\ 9.4 \end{array}$$

$$\begin{array}{r} 274.8 \\ 9.0 \\ 10 \end{array}$$

$$\begin{array}{r} 277.7 \\ 6.1 \\ 20 \end{array}$$

273.2

$$\begin{array}{r} 10.6 \\ 10 \end{array}$$

LR

$$\begin{array}{r} 274.3 \\ 9.5 \end{array}$$

LR

$$\begin{array}{r} 274.2 \\ 9.6 \\ 6 \end{array}$$

$$\begin{array}{r} 275.7 \\ 8.1 \\ 10 \end{array}$$

LR

274.32

$$\begin{array}{r} 9.52 \end{array}$$

273.4

$$\begin{array}{r} 10.4 \\ 10 \end{array}$$

LR

$$\begin{array}{r} 273.5 \\ 10.3 \end{array}$$

LR

273.4

$$\begin{array}{r} 10.4 \\ 6 \end{array}$$

275.6

$$\begin{array}{r} 8.2 \\ 10 \end{array}$$

273.0

LR

273.6 273.8 272.9

$$\begin{array}{r} 10.4 \\ 10 \end{array}$$

LR

$$\begin{array}{r} 10.5 \\ 5 \end{array}$$

LR

$$\begin{array}{r} 10.9 \\ 4 \end{array}$$

LR

$$\begin{array}{r} 273.2 \\ 10.6 \end{array}$$

LR

273.2

$$\begin{array}{r} 10.6 \\ 2 \end{array}$$

LR

275.5

$$\begin{array}{r} 8.3 \\ 10 \end{array}$$

272.5

$$\begin{array}{r} 11.3 \\ 10 \end{array}$$

LR

$$\begin{array}{r} 273.6 \\ 10.4 \end{array}$$

LR

274.0

$$\begin{array}{r} 9.8 \\ 6 \end{array}$$

LR

276.1

$$\begin{array}{r} 7.7 \\ 10 \end{array}$$

271.6

$$\begin{array}{r} 12.2 \\ 10 \end{array}$$

$$\begin{array}{r} 272.1 \\ 11.7 \end{array}$$

$$\begin{array}{r} 273.1 \\ 10.7 \end{array}$$

LR

$$\begin{array}{r} 273.0 \\ 10.8 \\ 5 \end{array}$$

$$\begin{array}{r} 274.8 \\ 9.0 \\ 7 \end{array}$$

$$\begin{array}{r} 275.4 \\ 8.4 \\ 10 \end{array}$$

⟨283.84⟩

292.31
286.16
6.15

485+19.75
5.27
487+9.20

19-18-49 clear cut

21

+50

281.5
8.8

BM. → 4.17 <290.33> <286.16>
BM. → RR Spike in 24" Sycamore Tree. 1.62 <286.16>

+38.50 and Concrete
487+38.25 upstream end Concrete Enc.

282.51
5.27

279.8 I.G

upstream end of 15" Multi Plate

T.P. Corrected. 10.03 <287.78> <277.75>

281.1
6.7
<287.78>

(Sketch From Here Pg 25)

T.P. 62 N end Culvert 15" Multi Plate

<277.89>
5.95

21" Y.C.
Top Concrete Encasement

278.3
5.5

15"
Flow Line Multi Plate Culvert

276.7
7.1

485+19.75 Approx end Pipe

279.4
4.4

+14

276.4
7.4
10
277.3
6.5
280.9
2.9
10

485

276.8
7.0
10
277.6
6.2
277.9
5.9
10

<283.8A>

<283.8A>

491

+57.12 A

490

+75

+40

+23 Tree 5'R. 18" Sycamore

489

+50

488

487 + 89.88 A

(59° W)

+65

290.33

1018-49
McCoy
Moore
Newcomb

Clear Co.

 $\begin{array}{r} 283.4 \\ 6.9 \\ \hline 10 \end{array}$ $\begin{array}{r} 283.9 \\ 6.4 \\ \hline 15 \end{array}$ $\begin{array}{r} 282.9 \\ 7.4 \\ \hline 11 \end{array}$ $\begin{array}{r} 282.3 \\ 8.0 \\ \hline 11 \end{array}$ $\begin{array}{r} 281.6 \\ 8.7 \\ \hline 13 \end{array}$ $\begin{array}{r} 281.8 \\ 8.5 \\ \hline 10 \end{array}$ $\begin{array}{r} 281.7 \\ 8.6 \\ \hline 15 \end{array}$ $\begin{array}{r} 281.7 \\ 8.6 \\ \hline 25 \end{array}$ $\begin{array}{r} 281.9 \\ 8.4 \\ \hline 10 \end{array}$ $\begin{array}{r} 284.6 \\ 5.7 \end{array}$ $\begin{array}{r} 284.35 \\ 5.98 \end{array}$ $\begin{array}{r} 283.8 \\ 6.5 \end{array}$ $\begin{array}{r} 283.4 \\ 6.9 \end{array}$ $\begin{array}{r} 282.4 \\ 7.9 \end{array}$ $\begin{array}{r} 282.9 \\ 7.4 \end{array}$ $\begin{array}{r} 282.0 \\ 8.3 \end{array}$ $\begin{array}{r} 282.8 \\ 7.5 \end{array}$ $\begin{array}{r} 283.25 \\ 7.08 \text{ sub} \end{array}$ $\begin{array}{r} 282.9 \\ 7.4 \end{array}$

290.33

 $\begin{array}{r} 285.6 \\ 4.7 \\ \hline 10 \end{array}$ $\begin{array}{r} 284.9 \\ 5.4 \\ \hline 10 \end{array}$ $\begin{array}{r} 284.2 \\ 6.1 \\ \hline 10 \end{array}$ $\begin{array}{r} 284.7 \\ 5.6 \\ \hline 13 \end{array}$ $\begin{array}{r} 284.0 \\ 6.3 \\ \hline 5 \end{array}$ $\begin{array}{r} 283.9 \\ 6.4 \\ \hline 10 \end{array}$ $\begin{array}{r} 282.6 \\ 7.7 \\ \hline 10 \end{array}$ $\begin{array}{r} 284.4 \\ 5.9 \\ \hline 20 \end{array}$ $\begin{array}{r} 285.0 \\ 5.3 \\ \hline 15 \end{array}$ $\begin{array}{r} 283.3 \\ 7.0 \\ \hline 10 \end{array}$

22

+62

+50

495

+50

494

+50

+31

12" Sycamore 7.5 Lt

+27

Creek West Small

493 + 01.41 T.P. 8.74 <294.86> A.21 <286.12>

+50

492

491 + 50

<290.33>

291.1 ✓
3.8
10

289.8 ✓
5.1
4

289.6 ✓
5.3
washed

290.1 ✓
4.8
10
washed

289.8 ✓
5.1
washed

289.1 ✓
5.8
10

289.1 ✓
5.8

288.6 ✓
6.3
10

289.1 ✓
5.8

287.1 ✓
7.2
9
Break to Creek N

288.7 ✓
6.2

286.3 ✓
8.1
6
P.R.

285 ✓
9.7

285.4 ✓
4.9
10

<294.86> ✓
286.1 ✓
4.21

287.8 ✓
2.5
10

283.9 ✓
6.4
10

285.6 ✓
4.7

287.7 ✓
2.6
10

283. ✓
7.1
10

284.6 ✓
5.7

286.6 ✓
3.7
10

282.9 ✓
7.4
15

284.5 ✓
5.8

286.5 ✓
3.8
10

<290.33> ✓

291.0 ✓ 294. ✓
3.9 9 send big rock
8 8

291.3 ✓ 291.8 ✓
3.6 3.1 Head Rock
5 13

23

289.1 ✓ 291.1 ✓
5.8 3.7
9 20
washed

290.1 ✓
4.8

289.2 ✓
5.5
10

286.5 ✓
8.4
10 creek

287.3 ✓
7.6
10

10-19-49
 McCoy
 Moore
 Newcomb

+50

498

+50

497

496+48.72

496+48.72 T.P. Δ

+22

+10

496

+95

+75

8.16

$\langle 300.26 \rangle$

2.76 $\langle 292.10 \rangle$

$$\begin{array}{r} 294.5\checkmark \\ \underline{5.8} \\ 10 \\ \text{Creek Bed.} \end{array}$$

$$\begin{array}{r} 293.7\checkmark \\ \underline{6.6} \\ 10 \end{array}$$

$$\begin{array}{r} 292.6\checkmark \\ \underline{7.7} \\ 12 \end{array}$$

$$\begin{array}{r} 292.6\checkmark \\ \underline{7.7} \\ 10 \end{array}$$

$$\begin{array}{r} 292.1\checkmark \\ \underline{8.2} \\ 10 \end{array}$$

$$\begin{array}{r} 292.7\checkmark \\ \underline{2.2} \\ 15 \end{array}$$

$$\begin{array}{r} 292.0\checkmark \\ \underline{2.9} \\ 15 \end{array}$$

$$\begin{array}{r} 290.8\checkmark \\ \underline{4.1} \\ 7 \\ \text{B.R.} \end{array}$$

$$\begin{array}{r} 290.1\checkmark \\ \underline{4.8} \\ 10 \\ \text{Rock} \\ \text{Buck.} \end{array}$$

$$\begin{array}{r} 290.5\checkmark \\ \underline{A.A} \\ 12. \\ \text{Brew.} \end{array}$$

To Page 26

$$\begin{array}{r} 295.3\checkmark \\ \underline{5.0} \\ 10 \\ \text{on Rock} \end{array}$$

$$\begin{array}{r} 294.1\checkmark \\ \underline{6.2} \\ 10 \end{array}$$

$$\begin{array}{r} 293.4\checkmark \\ \underline{6.9} \\ 10 \end{array}$$

$$\begin{array}{r} 292.6\checkmark \\ \underline{7.7} \\ 10 \end{array}$$

292.1

$\langle 300.26 \rangle$

$$\begin{array}{r} 292.7\checkmark \\ \underline{2.2} \\ 15 \end{array}$$

$$\begin{array}{r} 292.0\checkmark \\ \underline{2.9} \\ 15 \end{array}$$

$$\begin{array}{r} 292.5\checkmark \\ \underline{2.4} \\ 10 \\ \text{Sand rock} \end{array}$$

$$\begin{array}{r} 292.8\checkmark \\ \underline{2.1} \\ 15 \\ \text{B.R.} \end{array}$$

$$\begin{array}{r} 291.8\checkmark \\ \underline{3.1} \\ 5 \\ \text{B.R.} \end{array}$$

$$\begin{array}{r} 291.1\checkmark \\ \underline{3.8} \\ 10 \\ \text{Rock} \end{array}$$

$$\begin{array}{r} 290.9\checkmark \\ \underline{4.0} \\ 10 \\ \text{Rock} \end{array}$$

$$\begin{array}{r} 291.3\checkmark \\ \underline{3.6} \\ 10 \end{array}$$

$\langle 294.86 \rangle$

$$\begin{array}{r} 295.0\checkmark \\ \underline{5.3} \\ 6 \\ \text{Rock} \end{array}$$

$$\begin{array}{r} 294.0\checkmark \\ \underline{6.3} \\ 4 \end{array}$$

$$\begin{array}{r} 293.5\checkmark \\ \underline{6.8} \\ 4 \end{array}$$

$$\begin{array}{r} 293.1\checkmark \\ \underline{7.2} \\ 5 \end{array}$$

$$\begin{array}{r} 292.6\checkmark \\ \underline{7.7} \\ 5 \end{array}$$

$$\begin{array}{r} 299.7\checkmark \\ \underline{1.2} \\ 10 \end{array}$$

$$\begin{array}{r} 292.1\checkmark \\ \underline{2.8} \\ 15 \end{array}$$

$$\begin{array}{r} 291.2\checkmark \\ \underline{3.7} \\ 10 \\ \text{Rock} \end{array}$$

$$\begin{array}{r} 291.8\checkmark \\ \underline{3.1} \\ 5 \end{array}$$

$$\begin{array}{r} 291.8\checkmark \\ \underline{3.1} \\ 10 \\ \text{embedded} \\ \text{rock} \end{array}$$

246.7 **24**

$$\begin{array}{r} 246.7\checkmark \\ \underline{3.6} \\ 10 \end{array}$$

$$\begin{array}{r} 295.8\checkmark \\ \underline{4.5} \\ 10 \end{array}$$

$$\begin{array}{r} 295.2\checkmark \\ \underline{5.1} \\ 10 \end{array}$$

$$\begin{array}{r} 294.2\checkmark \\ \underline{6.1} \\ 10 \end{array}$$

$$\begin{array}{r} 293.6\checkmark \\ \underline{6.7} \\ 10 \end{array}$$

+75

+73
+729.5" R. 15" Syc.
3' Rt. 6+8" Sycamore500 + 50.68 Δ 8.26 <305.62> ✓ 2.90 <297.36> ✓
500 + 48-8" Sycamore 6' Rt

+25

500

2.5 R DbL Sycamore
40 R. to Rock

+90

+80

+60

+37

+32 14" Sycamore edelvine S. side

A99

From Pg 24

<300.26> ✓

 $\frac{8.2}{10}$ 297.9 ✓
8.1 $\frac{7.4}{14}$

Toe wedge 30' RqR

<305.62> ✓

 $\frac{3.3}{10}$ 297.36 ✓
2.90 $\frac{2.9}{2}$ $\frac{2.3}{10}$ $\frac{2.3}{15}$ 296.4
 $\frac{3.9}{10}$ 297.5 ✓
2.8296.8
 $\frac{3.5}{6}$ 298.3
 $\frac{2.0}{6}$ Toe
wedge
ledge

Rock

296.5 ✓
3.8 $\frac{4.5}{10}$ 295.9 ✓
4.4 $\frac{4.3}{4}$ $\frac{3.2}{10}$ $\frac{4.8}{10}$ 296. ✓
4.1 $\frac{2.7}{-10}$ $\frac{2.7}{6}$ $\frac{4.6}{10}$
creek. $\frac{4.2}{5.0}$ 296.9 ✓
3.4 $\frac{2.2}{5}$ $\frac{2.2}{10}$ $\frac{4.9}{10}$
creek $\frac{4.6}{4}$ 296.8 ✓
3.5 $\frac{3.0}{10}$ 295.0
 $\frac{5.3}{10}$
creek295.4 ✓
4.9296.0
 $\frac{4.3}{5}$ 296.0
 $\frac{2.3}{10}$

<300.26> ✓

502 + 65.65 11.28 <315.18> 1.72 <303.90>

+55

+50

+35

+25

502

+75

+52 18" Syc A.Lt.

+50

+25

+23-26 ~ Miller Stumps

501

<305.62>

304.0 ✓
 $\frac{1.6}{10}$
edge S.R.

303.90 ✓ 302.4 ✓
 $\frac{1.72}{10}$ $\frac{3.2}{10}$ **27**

303.1 ✓
2.5
or bank

$\frac{2.1}{10}$ $\frac{2.1}{5}$ $\frac{2.5}{4}$
S. Hook.

301.4 ✓
4.2 $\frac{7}{4.6}$ $\frac{15}{4.6}$

$\frac{4.2}{10}$ $\frac{4.9}{4.0}$ 300.7 ✓
4.9 $\frac{4.8}{3}$ $\frac{4.0}{10}$
Creek.

$\frac{4.9}{10}$ 300.9 ✓
4.7 $\frac{3.4}{10}$ $\frac{toe\ line}{20}$
Creek

$\frac{6.2}{10}$ $\frac{6.2}{7.0}$ 300.9 ✓
4.7 $\frac{4.9}{12}$
Creek Toe Hill

300.5 ✓
 $\frac{5.3}{10}$ 5.1 $\frac{4.9}{7}$
toe hill

Creek 30 $\frac{5.7}{10}$ 299.9 ✓
5.7 $\frac{5.7}{7.0}$ toe line

$\frac{8.5}{15}$ $\frac{9.0}{7}$ 299.5 ✓ 299.5
Creek $\frac{6.1}{10}$ toe line

297.3 297.9 ✓
 $\frac{8.3}{10}$ $\frac{7.7}{2}$ 298.4 ✓ 299.4 ✓ 298.7 ✓
Creek $\frac{7.2}{10}$ $\frac{6.2}{6}$ $\frac{6.9}{10}$
toe line

<305.62>

+87

$$\begin{array}{r} 308.7 \checkmark \\ 6.5 \\ \hline 5.R \end{array}$$

+75

$$\begin{array}{r} 5.8 \\ 10 \\ \hline 5.R \end{array}$$

$$\begin{array}{r} 308.9 \checkmark \\ 6.3 \\ \hline 5.R \end{array}$$

$$\begin{array}{r} 7.4 \\ 4. \\ \hline 5.R \end{array}$$

$$\begin{array}{r} 5.9 \\ 12 \\ \hline 5.R \end{array}$$

+70

$$\begin{array}{r} 306.6 \checkmark \\ 8.6 \\ \hline 5.R \end{array}$$

+62

$$\begin{array}{r} 307.4 \checkmark \\ 7.8 \\ \hline 305.8 \end{array}$$

step in rock

+61

$$\begin{array}{r} 9.4 \\ \hline 5.R \end{array}$$

+50

Begin Solid ledge.

$$\begin{array}{r} 9.5 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 305.9 \checkmark \\ 9.3 \\ \hline \end{array}$$

$$\begin{array}{r} 305.7 \\ 9.5 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 8.9 \\ 6 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ 12 \\ \hline 2 \end{array}$$

+25

$$\begin{array}{r} 306.3 \checkmark \\ 8.9 \\ \hline \end{array}$$

+20

$$\begin{array}{r} 11.8 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 11.8 \\ 6. \\ \hline \end{array}$$

$$\begin{array}{r} 307.0 \checkmark \\ 8.2 \\ \hline 5.R \end{array}$$

$$\begin{array}{r} 8.4 \\ 2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.3 \\ 8 \\ \hline \end{array}$$

$$\begin{array}{r} 11.4 \\ 13. \\ \hline \end{array}$$

+09

$$\begin{array}{r} 307.7 \checkmark \\ 7.5 \\ \hline \end{array}$$

on loose rock.

+07

$$\begin{array}{r} 303.5 \checkmark \\ 11.7 \\ \hline \end{array}$$

603.

$$\langle 215.14 \rangle \checkmark$$

$$\begin{array}{r} 10.0 \\ 25 \\ \hline \end{array}$$

the highway embankment.

$$\begin{array}{r} 11.2 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 303.6 \checkmark \\ 11.6 \\ \hline \end{array}$$

$$\begin{array}{r} 10.0 \\ 7 \\ \hline \end{array}$$

7 edge creek bank

$$\langle 315.18 \rangle \checkmark$$

+18

505

+90

+74.7²Δ

Loose
Rock
2 higher

+64

+61

T.P. on Rock

12.47

327.17

0.48

314.70

+50

+45

small

+10

50A

315.18

7.5

7
S.R.

10.5

3
S.R.

316.1

11.1
S.R.

11.6

1.5

8.6

2.0

Big W.R. **29**

316.2

11.0

5.1

316.1

11.1

5.2

9.0

10

10.9

5

11.2

3

14.1

8

14.4

13

20.

15

313.1

8.5

17
S.R.

8.1

9
S.R.

314.6

12.6

5
S.R.

13.5

5.2

14.9

11
S.R.

312.3

14.9

5.2

315.2

12.0

Top hedge

13.1

11

10.9

10
S.R.

11.1

3
S.R.

14.3

2
S.R.

15.3

8
S.R.

18.3

11
S.R.

327.17

312.0

5.2

2.3

10

2.5

4
S.R.

5.7

7
S.R.

7.0

15
Creek

311.2

4.0

2.5

10

5.2

10
S.R.

310.1

5.1

3.8

10

7.0

10 tubes

308.9

6.3

2.1

10
X.R.

7.0

5

1.3

10
Tubes

315.8

506 + 67.044

+ 35

+ 27

+ 15

506

+ 75

PT. 1.111 of Top NE end concrete

P.M. #A $\frac{1813}{10}$ El. 320.11

Bottoms of Spill on Top Dam

+ 40

+ 30

505 + 26

 $\langle 327.17 \rangle$ $\frac{6.4}{10}$

319.24 ✓

7.93

 $\frac{9.3}{20}$ $\frac{6.8}{10}$ $\frac{7.9}{5}$

318.8 ✓

8.4

 $\frac{9.3}{10}$ $\frac{5.4}{10}$ $\frac{6.3}{5.0}$

319.3 ✓

7.9

 $\frac{9.2}{10}$ $\frac{4.7}{10}$ $\frac{5.5}{4}$

321.1 ✓

5.5

 $\frac{7.4}{5}$ $\frac{9.3}{14}$
meters $\frac{4.6}{10}$

321.9 ✓

5.3

 $\frac{5.4}{3.5}$ $\frac{3.8}{9}$ $\frac{8.2}{11}$ $\frac{5.3}{10}$

320.9 ✓

6.3

320.3 ✓

 $\frac{6.85}{1.1}$ $\frac{7.7}{9}$ $\frac{9.3}{9}$
Water Level
Small Res.

7.03

 $\langle 320.14 \rangle$ ✓

7.80

319.37

 $\frac{6.2}{10}$

SR

8.3

1. SR

316.9 ✓

10.3

SR

12.3

10

SR

16.3

12

creek

7.1

10

S.R.

7.5

1. SR

S.R.

319.4 ✓

7.8

2. SR

8.5

2. SR

9.5

4 SR

12.6

5 SR

315.7 ✓

11.5

Area S.R.

 $\langle 327.17 \rangle$ ✓

+50

511

+50

510

+50

509

+50

TP

8.85 $\langle 328.42 \rangle$ 7.60 $\langle 319.57 \rangle$

Toplock by 508

 $\langle 328.42 \rangle$

508

+50

507

 $\langle 327.17 \rangle$ 324.9 ✓
3.5 $\frac{3.9}{10}$ 324.2 ✓
4.2 $\frac{4.4}{10}$ 323.3 ✓
5.1 $\frac{5.3}{10}$ 322.7 ✓
5.7 $\frac{5.9}{10}$ 322.0 ✓
6.4 $\frac{7.5}{10}$ 320.7 ✓
7.7 $\frac{7.9}{10}$ 319.9 ✓
8.5 $\frac{7.7}{10}$ 319.6 ✓
7.6 $\frac{7.5}{10}$ $\frac{8.2}{10}$ 318.8 ✓
8.4 $\frac{8.4}{10}$ $\frac{7.8}{10}$ 318.8 ✓
8.4 $\frac{8.9}{10}$ $\langle 327.17 \rangle$

515

+50

+35

+20

514

(Sketch from Here Pg 33)

513 + 75.07-A

6.6

<331.21>

3.81

<324.61>

Top sub.

+50

513

+50

512

<328.42>

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$\frac{5.1}{10}$

325.5 ✓
5.7

$\frac{6.7}{5}$

$\frac{6.7}{10}$

32

325.7 ✓
5.5

325.5 ✓
5.7

324.4 ✓
6.8

$\frac{6.3}{10}$

324.8 ✓
6.4

$\frac{6.3}{10}$

<331.21>

$\frac{3.6}{10}$

324.6 ✓
3.8

3.8

EL 321.3

EL 321.4

321.4

220

250

70

125

180

220

250

324.7 ✓
3.7

old
creek bed

North Hill

$\frac{3.5}{10}$

324.7 ✓
3.7

$\frac{3.9}{10}$

325.0 ✓
3.4

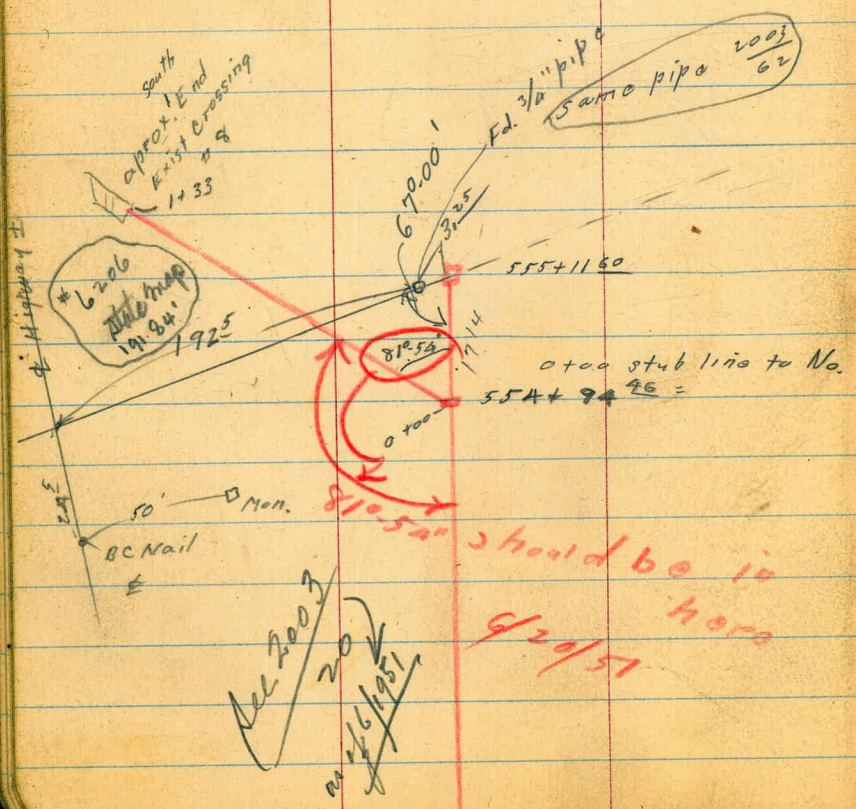
$\frac{3.1}{10}$

325.0 ✓
3.4

$\frac{3.4}{10}$

<328.42>

10-21-49 Clear-Cool
McCoy,
Moore,
Newcomb



523

+50

522

+50

+25 10' Sycamore 4.5R.

521 8.01.

+50

520 top Sta 4.9. 693 <337.66> ✓ 0.48 <330.13> ✓

+50

519

<331.21> ✓

$$\frac{4.7}{20}$$

$$\frac{5.8}{10}$$

$$\frac{333.1}{4.6}$$

$$\frac{332.4}{5.3}$$

36

333.4	332.8	337.7
$\frac{4.3}{150}$	$\frac{4.9}{250}$	$\frac{0}{300}$

329.1

329.8

$$\frac{2.8}{165}$$

80
150
Creek

6.1
140

5.7
85

7.9
70
Creek

5.6
50

5.8
15

$$\frac{332.7}{5.0}$$

$$\frac{5.1}{30}$$

$$\frac{7.7}{45}$$

$$\frac{5.6}{60}$$

$$\frac{4.8}{80}$$

$$\frac{7.5}{87}$$

$$\frac{4.3}{105}$$

3300
for Leo
25.5.

333.1

$$\frac{4.6}{25}$$

$$\frac{332.2}{5.5}$$

331.8

$$\frac{5.9}{10}$$

$$\frac{5.9}{30}$$

$$\frac{331.7}{6.0}$$

$$\frac{330.9}{6.8}$$

$$\frac{331.34}{6.3}$$

$$\frac{330.9}{6.8}$$

$$\frac{9.0}{30}$$

Creek

$$\frac{330.4}{7.3}$$

$$\frac{330.3}{7.4}$$

$$\frac{330.2}{7.5}$$

$$\frac{330.1}{7.6}$$

$$\frac{329.3}{8.4}$$

$$\frac{337.66}{330.0}$$

1.2

$$\frac{228.8}{2.4}$$

$$\frac{228.8}{2.4}$$

$$\frac{228.7}{2.5}$$

$$\frac{229.8}{1.4}$$

<331.21> ✓

528

+50

527

+83

526 + 57.80 = 527 + no. of ltr

5.62

hub.
335.41

526

+50

525 TR. Top Stake 4.90 <341.03>

153

<336.13>

+50

524

+50

<337.66>

$\frac{4.0}{25}$

$\frac{7.3}{6.}$

$\frac{333.4}{76}$ ✓
Creek

$\frac{6.8}{18}$

$\frac{3.0}{25}$

37

$\frac{3.9}{20}$

$\frac{5.6}{8}$

$\frac{332.7}{8.3}$ ✓
creek

$\frac{8.9}{10}$

$\frac{7.1}{23}$

$\frac{4.7}{30}$

$\frac{5.3}{10}$

$\frac{334.1}{6.9}$ ✓

$\frac{9.1}{9}$

$\frac{8.0}{28}$ $\frac{4.5}{40}$

$\frac{334.8}{6.2}$ ✓

$\frac{5.0}{25}$

$\frac{335.4}{5.62}$ ✓

$\frac{10.0}{20}$

$\frac{5.5}{50}$

Creek

$\frac{6.7}{30}$

$\frac{335.1}{5.3}$ ✓

$\frac{5.7}{5}$

$\frac{10.0}{35}$

$\frac{8.1}{50}$

Creek

$\frac{4.9}{10.}$

$\frac{336.2}{4.8}$ ✓

$\frac{5.5}{7}$

<341.03> ✓
Creek Bank

$\frac{2.1}{25}$

$\frac{335.4}{2.3}$ ✓

$\frac{2.5}{7}$

$\frac{3.7}{20}$

$\frac{7.6}{25}$

Creek

$\frac{334.8}{2.9}$ ✓

$\frac{3.4}{30}$

$\frac{333.7}{4.0}$ ✓

$\frac{4.5}{10}$

$\frac{3.7}{30}$

$\frac{5.9}{35}$

$\frac{7.4}{60}$

Creek

$\frac{333.2}{4.5}$ ✓

<337.66> ✓

+50

+30

531

+50

530

+50

T.P. Rock in Creek on line +25
 11.3 ~ $\langle 345.66 \rangle$

6.69 $\langle 334.3A \rangle$

529

+75

+73

8 ft to 18" Willow

+70

+51 .9.5 R. 12" Pepper tree

+50

$\langle 341.03 \rangle$

338.8 ✓

 $\frac{6.9}{\text{Creek}}$
 $\frac{4.8}{2.3}$
 $\frac{8.4}{14}$
 $\frac{340.2}{5.5}$ ✓

 $\frac{5.0}{10}$

Creek

 $\frac{6.0}{2.0}$
 $\frac{7.9}{11}$
Creek

 $\frac{338.9}{6.8}$ ✓

 $\frac{6.0}{10}$
 $\frac{6.0}{2.5}$
 $\frac{8.5}{8.5}$
Creek

 $\frac{338.6}{7.1}$ ✓

 $\frac{6.9}{10}$
 $\frac{7.9}{10}$
 $\frac{336.7}{9.0}$ ✓
Creek

 $\frac{7.4}{10}$
 $\frac{7.4}{20}$
 $\frac{9.6}{8}$
 $\frac{10.9}{3}$
 $\frac{335.3}{10.4}$ ✓
Creek

 $\frac{10.3}{3}$
 $\frac{8.8}{5}$

Creek

$\langle 345.66 \rangle$
 $\frac{334.5}{\text{Creek}}$

 $\frac{2.4}{70}$
 $\frac{5.2}{50}$
 $\frac{6.6}{20}$
 $\frac{334.7}{6.3}$ ✓

 $\frac{7.1}{9}$
 $\frac{4.2}{11}$
 $\frac{1.7}{20}$

Creek

 $\frac{333.3}{7.7}$ ✓
Creek

 $\frac{335.0}{6.0}$ ✓

 $\frac{3.3}{35}$
 $\frac{5.3}{20}$
 $\frac{7.8}{11}$
 $\frac{334.7}{6.3}$ ✓
Creek

 $\frac{5.2}{15}$
 $\frac{5.1}{25}$

$\langle 341.03 \rangle$

+15

341.9 ✓
3.8

534

 $\frac{1.6}{2.5}$ $\frac{4.3}{7}$ 342.1 ✓
3.6 $\frac{4.3}{7}$ $\frac{3.6}{2.0}$ Slope to
x-ray

+50

 $\frac{5.4}{3}$ 341.3 ✓
4.4

533

343.2 ✓

 $\frac{2.5}{30}$ 340.6 ✓
5.1342.4 ✓
 $\frac{3.3}{2.0}$ Slope to
x-ray

+80

340.6 ✓
5.1

+50

342.9 ✓

 $\frac{2.8}{2.5}$

339.7 ✓

 $\frac{6.0}{7}$ 340.5 ✓
5.2341.7 ✓
 $\frac{4.0}{2.0}$

bank

creek

532 + 89 = 492 + 89 Hills
13' R 532 + 28

5.40 (340.26)

+15

340.1 ✓

5.6

creek

+10

337.7 ✓

8.0

creek

532

342.3 ✓

 $\frac{3.4}{2.0}$

340.2 ✓

 $\frac{5.5}{8}$

337.8 ✓

 $\frac{7.9}{4}$

337.7 ✓

8.0

338.0 ✓

 $\frac{1.7}{2}$

341.3 ✓

 $\frac{4.4}{6}$

+85

339.4 ✓
6.3

(345.66) ✓

(345.66) ✓

+50

+25

536

+55

+50

+35

535

T.P. Reck +60

9.49 <351.35>

3.80 <341.86>

+50

+30

+20

<345.66>

346.4 ✓
4.9

40

344.8 ✓
6.5

5.1
20

345.4 ✓
5.9

7.1
7

7.0
30

344.2 ✓
7.1

5.9
15

6.7
3

342.8 ✓
8.5

9.9
6

9.8
20

7.4
25

crack crack

341.8 ✓
9.5

7.4
16

10.2
6
crack

341.5 ✓
9.8
crack

7.6
12

<351.35>

342.5 ✓
3.2
13

340.3 ✓
5.4
8
crack

341.4 ✓
4.3
crack

342.6 ✓
3.1
10

339.9 ✓
5.8

342.3 ✓
3.4
5

340.7 ✓
5.0
crack

341.5 ✓
4.2
10

<345.66>

T.P. Rock 7.43 <357.61> 1.17 <350.18>

+40

+20

539.

+65

+30

538

+66

52.55 + 5x55 11-17-49 AM. water line 54" concrete pipe

537

next edge

(537 + 65.30 old Sta)

3.00 <348.31> 348.20

536 + 90.06 Sta

<351.35>

5.00 346.35 2002 TV

350.3 ✓
1.1

347.8 ✓
3.6

347.2 ✓
4.2
10

347.2 ✓
4.2
check

348.2 ✓
3.2
10

3.9
10

346.0 ✓
5.3
check

4.1
10

345.9 ✓
5.5
check

4.2
20

346.5 ✓
4.8

6.2 4.8
15 25

345.7 ✓
5.6

4.0
20

346.6 ✓
4.7

6.0 5.8
15 30

Reg. A.A. above top pipe

342.2 Top pipe 11-17-49 AM.

346.3 ✓
5.0

4.4
20

346.3 ✓
5.0

6.7 5.8
15 30

<351.35>

+50

+35

+20

543

+50

542

+50

541

+50

540

+50

<357.61>✓

$$\frac{6.2}{24} \quad \frac{2.5}{18}$$

$$\frac{355.1 \checkmark}{2.5 \text{ Rot}} \\ \frac{354.2 \checkmark}{3.4 \text{ Rot}}$$

$$\frac{2.8}{20}$$

42

$$\frac{355.0 \checkmark}{2.6}$$

$$\frac{3.0}{20}$$

$$\frac{354.9 \checkmark}{2.7}$$

$$\frac{2.5}{20}$$

$$\frac{353.8 \checkmark}{3.8}$$

$$\frac{4.7}{55}$$

$$\frac{6.0}{30}$$

$$\frac{353.5 \checkmark}{4.1}$$

$$\frac{3.8}{20}$$

$$\frac{353.2 \checkmark}{4.4}$$

$$\frac{7.0}{60}$$

$$\frac{7.1}{35} \\ \text{Chok}$$

$$\frac{4.7}{25}$$

$$\frac{353.3 \checkmark}{4.3}$$

$$\frac{4.5}{20}$$

$$\frac{352.4 \checkmark}{5.2}$$

$$\frac{6.4}{25}$$

$$\frac{351.1 \checkmark}{6.5}$$

$$\frac{6.5}{20}$$

$$\frac{350.4 \checkmark}{7.2}$$

<357.61>✓

545 + 71.60 Δ

End of Proposed
Trunkline. 4.22

+50

545

+88

5'R - 8" Eucalypt tree

+87

+68

(old) Dub. 545 + 25.30
3.9' R. am St. 544 + 50.5
+50

6.68

$\frac{2003}{76}$ ✓
355.30

T.P. - Rock.

1.39 < 361.98 > ✓

3.02 < 354.59 > ✓

+25

+15

544

+92

thru

+80

543 + 73

< 357.61 > ✓

357.8 ✓
4.2

357.3 ✓
4.7

$\frac{5.0}{20}$

356.8 ✓
5.2

$\frac{6.4}{10}$

$\frac{5.6}{10}$

355.9 ✓
6.1

$\frac{7.8}{12}$

353.3 ✓
8.7
Creek.

$\frac{7.0}{30}$

$\frac{8.7}{11}$
Creek

354.2 ✓
7.8

$\frac{6.4}{10}$

< 361.98 > ✓
354.9 ✓
2.7

353.8 ✓
3.8

$\frac{3.0}{10}$

$\frac{4.5}{6}$

353.1 ✓
4.5

$\frac{5.3}{10}$

352.1 ✓
5.5

352.0 ✓
5.6

$\frac{6.0}{15}$

$\frac{6.0}{7}$
Creek.

355.8 ✓
1.8

$\frac{2.0}{20}$

< 357.61 > ✓

Tie to #7 Crossing Freeway

2+11.0 Send #7 Crossing Freeway
on sub.
Pipe not uncovered.

2+00

+50

1+00

0+50

545 + 71.60 = 0+00

$\langle 358.14 \rangle$ ✓
3.84

$\frac{357.3}{4.7}$ ✓

$\frac{357.2}{4.8}$ ✓

$\frac{357.0}{5.0}$ ✓

$\frac{357.4}{4.6}$ ✓

$\frac{357.8}{4.4}$ ✓

$\langle 361.98 \rangle$

11-30-49

Newcomb
Summermeier
McCoy
Rorer

Change of Line
at Lower Creek Xing
(See Revised Sketch Pg 11)

±

45

+26

Shelf in Ledge

210.4[✓]
11.4

+25

Edge Solid Ledge

215.6[✓]
6.3

+20

3' x 3' Boulder

216.1[✓]
5.7
Not w/rt
Ground.

479-

See p. 60

12/13/49

220.5[✓]
1.3

+96

220.8[✓]
1.1

+75

219.6[✓]
2.2

473+6157

New \angle Pt. (Sketch pg 11) Stub.

216.0[✓]
5.90

Stub

473+9666
FB 2003
63-68

3.15

221.85[✓]

NOV
2/3
1949
218.70

221.85[✓]

Level change

473+61.57 fo

477+60.44

£

46

474+68

210.6 ✓
11.2

+60

211.6 ✓
10.3

+53

207.4 ✓
14.4

+50

207.2 ✓
14.7

+48

202.0 ✓
18.9

+34

202.4 ✓
19.5

+83

207.9 ✓
14.0

+30

208.5 ✓
13.3

474+29 Top Large Boulder on Shelf

215.6 ✓
6.3

<221.85> ✓

<221.85> ✓

over rocks

Revised 11-30-49

473+61.57 to 477+60.74

47

T.P. 12.69 $\langle 233.89 \rangle$ 0.65 $\langle 221.20 \rangle$

(see P11)

474+95.77 Ahead

cross on rock

474+96.30 back

Δ 29°30' Lt.

$\langle 214.75 \rangle$
7.10

+87

214.5 ✓
7.3

+78 start large rock

212.9 ✓
9.0

72^E

214.0 ✓
7.8

+77^e

209.5 ✓
12.3

+71

between rocks on lower ^{rock}

209.2 ✓
12.6

+70

212.9 ✓
9.0

474+69

213.0 ✓
8.8

$\langle 221.85 \rangle$

$\langle 221.85 \rangle$

T.P. 7.54 $\langle 252.59 \rangle$ 0.07 $\langle 245.05 \rangle$
~~233.82~~

+47

245.7 \checkmark
+0.6

+45 Top of a' diam. rock

248.1 \checkmark
+3.0

+43

244.8 \checkmark
0.3

+35

243.6 \checkmark
1.5

+22

241.0 \checkmark
9.1

477100 ⁷¹ 44°-42' Lt. (P. 11)

237.92 \checkmark
7.20
5746

476+80

236.0 \checkmark
9.1

T.P. 12.68 $\langle 245.12 \rangle$ 1.45 $\langle 232.44 \rangle$
↓

$\langle 245.12 \rangle$ \checkmark

476+59 ²¹ Δ 22°-30' (P. 11)

$\langle 232.44 \rangle$ \checkmark
1.45
5746

$\langle 233.89 \rangle$ \checkmark

$\langle 233.89 \rangle$ \checkmark

48

Levels - Line change

473+61.57

To 477+60.44

E

49

477+60.95 Ahead
477+60.44 back = $\Delta 13^{\circ}-29' 4''$

477+58

$\langle 245.68 \rangle$
6.91

246.5
6.1

$\langle 252.59 \rangle$

To. Crossing # 6A
Sketch P 33

T.P.

12.20 $\langle 346.14 \rangle$ ✓

0.13 $\langle 333.94 \rangle$ ✓

3 + 00

+ 50

2 + 00

+ 50

1 + 00

+ 50

+

+ 25

0 + 06

= 0 + 00 on branch line

A 516 + 45²⁰ (P 33)

513 + 75.07

19 32 ✓

9.46 $\langle 334.07 \rangle$ ✓

324.62 ✓

9.46

±

50

333.1 ✓
1.0

330.8 ✓
3.3

329.6 ✓
4.5

328.8 ✓
5.3

328.1 ✓
6.0

328.3 ✓
5.8

327.6 ✓
6.5

329.9 ✓
10.2

325.0 ✓
8.99
stab.

$\langle 334.07 \rangle$ ✓

To Crossing # G.A.

$$\begin{array}{r} \text{30' Nly. R.P.} \\ \hline \text{FB 2003} \\ \text{18} \end{array} \begin{array}{l} \text{State 2} \\ \text{EL.} = 351.0 \\ \hline \text{6.12} \\ \text{City EL.} = 344.88 \end{array}$$

$$\begin{array}{r} \text{30' N.P.} \\ \hline \text{2003} \\ \text{18} \end{array} \begin{array}{l} \text{7.76} \langle 344.74 \rangle \\ \hline \text{2.48} \langle 343.66 \rangle \end{array} \begin{array}{l} \text{20.18} \\ \hline \text{344.88} \end{array}$$

$$\text{TIP} \quad 8.84 \langle 352.50 \rangle$$

$$\begin{array}{r} \text{2003} \\ \hline \text{18} \end{array} \begin{array}{l} \text{4 + 66}^{25} \text{ So. End Exist Crossing \# G.A.} \\ \hline \end{array}$$

$$\begin{array}{l} 343.66 \checkmark \\ 2.48 \\ \text{stub.} \end{array}$$

+50

$$\begin{array}{l} 343.8 \checkmark \\ 2.3 \end{array}$$

4+00

$$\begin{array}{l} 340.5 \checkmark \\ 5.6 \end{array}$$

3+50

$$\begin{array}{l} 336.7 \checkmark \\ 9.4 \end{array}$$

$\langle 346.1A \rangle$

$\langle 346.1A \rangle$

Line To Sewer Crossing #9.
Sta. of Highway = 1A1+00 FB2003
12-1-49 sketch-R33
2A

T.P. 13.07 $\langle 357.13 \rangle$ 0.28 $\langle 344.06 \rangle$

+86

+82

+67

+50

1+00

+50

+25

= 0+00 on stub to North.
527+91.58 R33

From R37
526+57.72 8.93 $\langle 344.34 \rangle$ $\langle 335.41 \rangle$

±

52

343.1 ✓
1.2

341.1 ✓
3.2

340.6 ✓
3.7

339.5 ✓
6.8

338.5 ✓
5.8

337.3 ✓
7.0

336.9 ✓
7.4

333.1 ✓
11.22
stub

$\langle 344.34 \rangle$

to Crossing #9

±

53

3+90.72 so. End Exist sewer crossing #9

+50

359.1 ✓
+2.0

356.6 ✓
0.5

3+00.72 Hub P.O.T.

354.90 ✓
2.83

354.3 ✓
2.8

3+00

+50

351.4 ✓
5.7

+30

349.9 ✓
7.8

2+00

344.8 ✓
12.3
357.13 ✓

523+31⁵⁰ to 527+88⁷⁰ 12/8/49

Sketch P 33

±

54

+50

526~

+50

525~

+50

524~

+50

523+31⁵⁰ Δ

B.M.
526+57⁵⁰
P. 37

5.74 [341.15]

335.41 ✓

[341.15]

335 8 ✓
5.3

334. A ✓
6.7

336. 0 ✓
5.1

335 1 ✓
5.5

33A 1 ✓
6.4

33A. 0 ✓
7.2

333. 5 ✓
7.6

332 15 ✓
8.40
5746

12/8/49

T.P. 12.72 $\langle 345.86 \rangle$ 8.01 $\langle 333.14 \rangle$

FB 1873
17

Also = 0 + 39⁸² Catactin line

527 + 88⁷⁰ = Δ 9° 58' 30" Lt on Trunk lever

+ 75

+ 45

527 ~

$\langle 341.15 \rangle$

333.14 ✓
8.01

332.8 ✓
8.3

335.9 ✓
5.8

336.4 ✓
4.9

341.15 ✓

Catoctin Canyon St 1770

Levels
Sketch P33 + $\frac{1873}{17}$

12/8/49

3 ~

+50

2 ~

+50

+100

+70

+60

= 0 + 39 $\frac{82}{17}$

527 + 88 $\frac{72}{17}$ P55

$\langle 345.86 \rangle$
P.55

±

56

341.9 ✓
4.0

340.1 ✓
5.2

338.9 ✓
7.0

337.5 ✓
8.4

338.0 ✓
7.9

338.2 ✓
7.7

334.3 ✓
11.6

333.14 ✓
12.72
stus

$\langle 345.86 \rangle$

$$5+15 \quad \frac{1873}{19}$$

$$5+00 = \Delta 15^{\circ}-18' \text{ Lt.} \quad \frac{1873}{17}$$

+50

4~

3+50

$$345.6 \checkmark$$

$$0.3$$

$$345.3 \checkmark$$

$$0.6$$

$$343.0 \checkmark$$

$$2.9$$

$$343.2 \checkmark$$

$$2.7$$

$$\langle 345.86 \rangle \checkmark$$

12/8/49

532+88⁷⁴ + 537+21⁸⁵ = 537+22⁶⁶
Back Ahead

±

58

+55

343.8 ✓
6.3

+50

342.0 ✓
8.1

535~

341.9 ✓
8.2

+50

342.1 ✓
8.0

+25

340.6 ✓
9.5

534~

342.1 ✓
8.0

+50

Sketch p. 33

341.5 ✓
8.6

533~

340.6 ✓
9.5

532+88⁷⁴ Δ 0° 56' 30" Rt. (P. 33)

340.61 ✓
9.46

536+90⁶⁶ stub
P. 41
3.72 {350.07} - {346.35}

Hub
{350.07} ✓

537+22^{SS} Ahead
 537+21^{SE} Back = Δ 12°-08' Rt.

537 ~

+50

536

346.17 ✓
 3.90

346.0 ✓
 4.1

346.2 ✓
 3.9

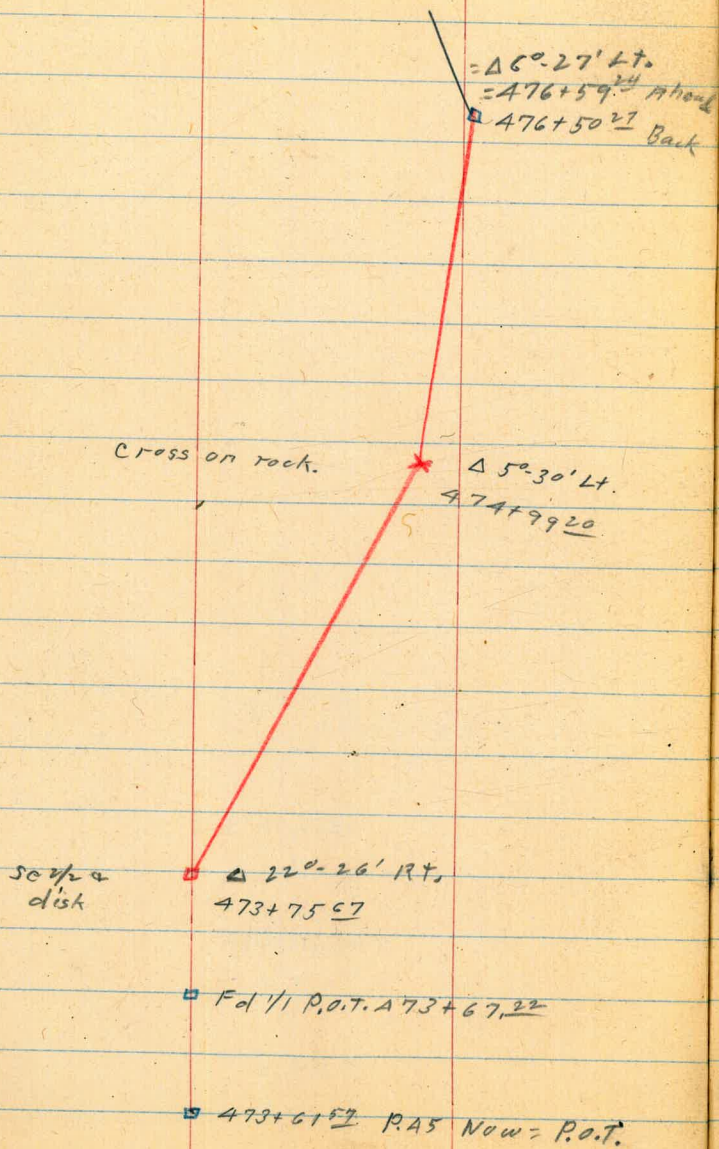
344.5 ✓
 5.6

350.07 ✓

Change 12/13/49

473+61⁵⁷ to

60



473+75⁶⁷ to 476+50⁶⁷
Sketch - P 60

±

61

+54	on rock	208.01 12.6
+53	base of boulder of rock	204.51 16.0
+48	on rock	202.31 18.2
+35	in side wash	202.01 18.5
+33	on ledge	208.01 12.5
+25	top of another boulder Face base of boulder on	209.81 10.7
474+24	Top boulder	215.21 5.3
+97		219.81 0.7
473+75 ⁶⁷ Δ		218.71 1.8

st46 473+ 9666

FB2003

63-64

EL = 218.70

1.85 <220.55> - <218.70> $\frac{2051}{5}$

<220.55>

+02
 475 +01 = end top big boulder
 47A+99²⁰ Δ 5° 30' Lt. (X on rock)

+90

top of rock
 +79 start big boulder

+77

+69

+68

47A+60 top of boulder

220.55 ✓

211.1 ✓
 7.4

214.4 ✓
 6.1

214.69 ✓
 5.86

214.4 ✓
 6.1

212.8 ✓
 7.7

214.4 ✓
 6.1

213.0 ✓
 7.5

210.4 ✓
 10.1

211.3 ✓
 9.2

220.55 ✓

+38		215.7 ^v	4.8
+37 ^L top of boulder		214.2 ^v	6.3
+37 = Face top of under cut ^{boulder} rock		208.2 ^v	12.3
+25 on loose boulder	207.1	208.6 ^v	11.7
	13.4		
	on rock		
+21 bottom of wash		205.3 ^v	15.2
+13 bottom main wash		205.0 ^v	15.6
+12		207.4 ^v	13.1
+08		207.4 ^v	13.1
475+07		210.0 ^v	10.5

220.55^v

220.55^v

+92

221.8[✓]
10.1

+87

223.0[✓]
8.9

+80

219.3[✓]
12.6

+71

221.3[✓] 218.3[✓]
10.6 13.6
2

T.P.

12.28

 $\langle 231.86 \rangle$ 0.97 $\langle 219.58 \rangle$ $\langle 231.86 \rangle$ [✓]

+64

219.3[✓]
1.2

+59

217.0[✓]
3.5

+47

base of boulder

210.4[✓]
10.1

+46

on boulder

216.8[✓]
3.7

475+41 = base of under cut boulder

208.4[✓]
12.3 $\langle 220.55 \rangle$ $\langle 220.55 \rangle$ [✓]

to 476+50²⁷

±

65

= 476+59²⁸ Ahead
476+50²⁷ Back Δ 6°-27' 4"

+42

+30

476~

232.5 ✓
+0.6

229.5 ✓
2.4

228.4 ✓
3.5

224.1 ✓
7.8

⟨ 231.85 ⟩ ✓

State College Outfall.

3/20/50

Sommermeyer
McCoy
Allen

66

Cont. P. 69 and P. 75

T.P. 8.08 $\langle 215.68 \rangle$ 2.08 $\langle 207.60 \rangle = 1/1"$

10.66 $\langle 209.68 \rangle$ — $\langle 199.02 \rangle$

Set. B.M. state data \checkmark vs 65 9.12 $\langle 199.02 \rangle$ chis off \square

201.48 City data.

(Crossing end sealed up.)
Crossing #5
stub. approx 12 above in vert. south end

West end South Head wall, state culvert
(startoo state) = Below state sewage plant

= 192.90 City data

T.P. 6.67 $\langle 208.1A \rangle$ 11.95 $\langle 201.47 \rangle$

0+00 = S.S. 6.15 207.27 = EL.

See end top of casement Crossing #5

T.P. 0.39 $\langle 213.42 \rangle$ 11.96 $\langle 213.03 \rangle$

T.P. 1.59 $\langle 224.99 \rangle$ 11.83 $\langle 223.40 \rangle$

State B.M. #10 =
1/2" Iron pin 1.88 $\langle 235.23 \rangle$ — $\langle 233.85 \rangle$ $\frac{2003}{16}$

60' Lt state sta. 83+50
= 150' Ely. of outlet to state culvert.

(See FB. 2003
16

A. line

P.O.T.

2+65.68

Levels - P 69

Office Extension

19° 20'

20'

0+00 Δ 19° 20' Lt.

Existing Sewer

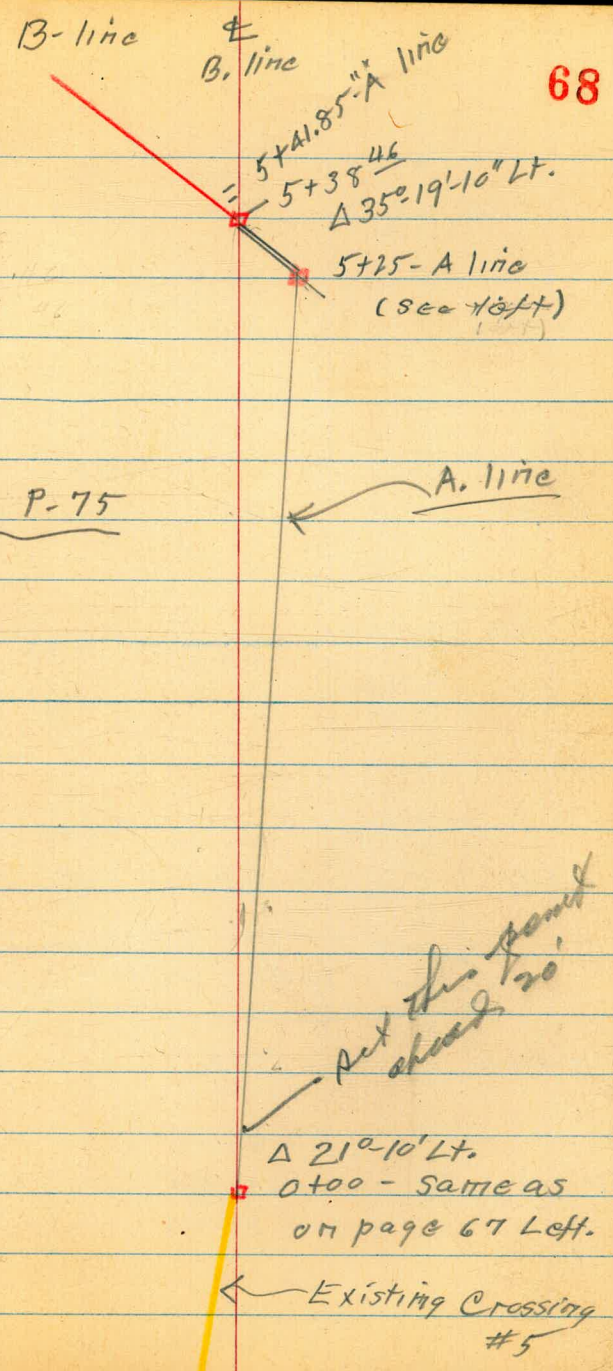
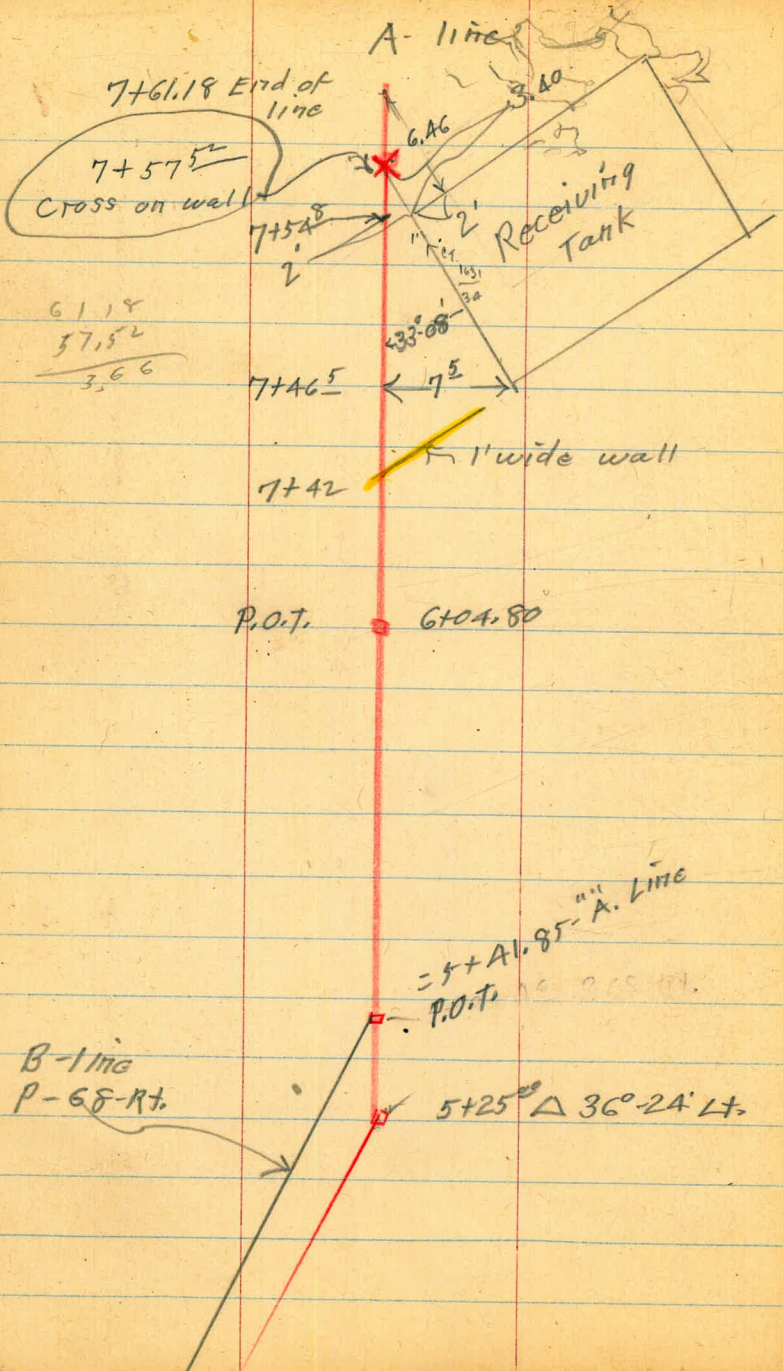
= Crossing #5

A. line

67

5+25⁰⁰

Δ 36° 24' Lt.



Levels - P-75

Put this point about 20'
 $\Delta 21^{\circ}10'$ Lt.
 0+00 - Same as on page 67 Left.
 Existing Crossing #5

A line

+35

1+18

1+00

0+9A 24" diam Cluster of sumac on line

0+80

0+15

WI = bottom of wash

0+01

0+00 = Invert So. end Crossing #5

⊕
"A" line

69

191.6 [✓]	199.7 [✓]	204.2 [✓]	209.2 [✓]
<u>18.0</u>	<u>9.9</u>	<u>5.4</u>	<u>0.4</u>
30	10		10
W			

205.3[✓]
4.3

192.0 [✓]	2013 [✓]	204.2 [✓]	209.5 [✓]
<u>17.6</u>	<u>8.3</u>	<u>5.4</u>	<u>0.1</u>
10	5		10
W			

191.6 [✓]	198.3 [✓]	205.0 [✓]	208.8 [✓]
<u>18.0</u>	<u>11.3</u>	<u>4.6</u>	<u>0.8</u>
20	10		10
W			

199.5 [✓]	202.4 [✓]	206.1 [✓]
<u>10.1</u>	<u>7.2</u>	<u>3.5</u>
10		10

202.1[✓]
7.5

199.5[✓]
10.1
Approx. invert

State Return
-11-565

209.56 City Datum
→ 215.68 From P. 66

3+90

215.6 ✓
7.3 $\left\langle \begin{array}{l} 222.92 \\ 229.04 \end{array} \right\rangle$ ✓

T.P.

7.97

 $\left\langle \begin{array}{l} 222.92 \\ 229.04 \end{array} \right\rangle$

0.56

 $\left\langle \begin{array}{l} 212.95 \\ 219.07 \end{array} \right\rangle$

3+50

208.1 ✓
 $\frac{5.4}{5}$
W211.6 ✓
1.9212.2 ✓
 $\frac{1.3}{10}$

3+10

205.5 ✓
 $\frac{8.0}{25}$
W210.4 ✓
3.1212.2 ✓
 $\frac{1.3}{10}$

2+77 = 3 strand barb wire fence.

2+65.68 = $\frac{1}{2}$ P.O.T. 5.32

+60

202.3 ✓
 $\frac{11.2}{7}$
W208.4 ✓
5.1202.0 ✓
 $\frac{11.5}{5}$
W205.5 ✓
8.0210.5 ✓
 $\frac{3.0}{4}$ 213.6 ✓
 $\frac{+0.1}{10}$

2+48

201.5 ✓
 $\frac{12.0}{7}$
W208.8 ✓
4.7213.5 ✓
 $\frac{0.0}{10}$

2+37

 $\left\langle \begin{array}{l} 213.51 \\ 219.63 \end{array} \right\rangle$ ✓

T.P.

5.04

 $\left\langle \begin{array}{l} 213.51 \\ 219.63 \end{array} \right\rangle$

1.09

 $\left\langle \begin{array}{l} 208.47 \\ 214.59 \end{array} \right\rangle$

1+95

196.6
 $\frac{13.0}{70}$
W200.6
 $\frac{9.0}{28}$ 204.6
 $\frac{5.0}{10}$ 208.2
1.4211.1
 $\frac{+1.5}{10}$

1+50

206.2
3.4209.56 City Datum
215.68 DSGS

209.56

A-line

5+25 = Δ 36° 24' Lt.

5+00

4+85 2' Rt. = 12" willow

4+79 2' Lt. = ctr. 1A" willow

T.P. 9108 $\left\{ \begin{array}{l} 231.69 \\ \hline 227.81 \end{array} \right\}$ 0.31 $\left\{ \begin{array}{l} 228.61 \\ \hline 228.79 \end{array} \right\}$

4+50

4+37

4+39

4+14

227.2 [✓]	225.74 [✓]	225.1 [✓]	225.0 [✓]
4.5	5.95	6.0	6.7
10	Hub	12	20
			W

71

224.2 [✓]	223.6 [✓]	222.0 [✓]	221.8 [✓]
7.5	8.1	9.7	9.9
10	2		2
			W

223.2 [✓]	222.5 [✓]	221.2 [✓]
8.5	9.2	10.5
15		6
		W

231.69 [✓]
<u>237.81</u>

218.9 [✓]	218.6 [✓]
4.0	4.3
	1A
	W

217.2 [✓]
5.7
W

218.2 [✓]
4.7

214.2 [✓]
8.5
15
W

216.2 [✓]
6.5

229.94 [✓]
<u>229.04</u>

T.P. 13.07 $\left\langle \begin{array}{l} \sim 80.98 \\ \underline{287.16} \end{array} \right\rangle$ 0.08 $\left\langle \begin{array}{l} \sim 67.91 \\ \underline{279.03} \end{array} \right\rangle$

6 to 4.80 = $\frac{1}{2}$ P.O.T. 2.68

5+96

T.P. 12.64 $\left\langle \begin{array}{l} \sim 67.99 \\ \underline{274.11} \end{array} \right\rangle$ 0.53 $\left\langle \begin{array}{l} \sim 55.33 \\ \underline{261.17} \end{array} \right\rangle$

5+75

T.P. 12.63 $\left\langle \begin{array}{l} \sim 55.88 \\ \underline{262.00} \end{array} \right\rangle$ 0.52 $\left\langle \begin{array}{l} \sim 43.25 \\ \underline{249.37} \end{array} \right\rangle$

5+50

T.P. 12.34 $\left\langle \begin{array}{l} \sim 43.77 \\ \underline{249.89} \end{array} \right\rangle$ 0.26 $\left\langle \begin{array}{l} \sim 31.43 \\ \underline{237.55} \end{array} \right\rangle$

5+41 $\frac{85}{2}$ = $\frac{1}{2}$ P.O.T.

1.00 $\left\langle \begin{array}{l} \sim 30.69 \\ \underline{236.81} \end{array} \right\rangle$

5+37

$\left\langle \begin{array}{l} \sim 80.98 \\ \underline{287.16} \end{array} \right\rangle$

$\frac{267.21}{5.8}$

$\left\langle \begin{array}{l} \sim 67.99 \\ \underline{274.11} \end{array} \right\rangle$

$\frac{250.4}{5.5}$

$\left\langle \begin{array}{l} \sim 55.88 \\ \underline{262.00} \end{array} \right\rangle$

$\frac{235.7}{8.1}$

$\left\langle \begin{array}{l} \sim 43.77 \\ \underline{249.89} \end{array} \right\rangle$

$\frac{230.69}{1.00}$
Hub

$\frac{227.7}{4.0}$

$\left\langle \begin{array}{l} \sim 31.69 \\ \underline{237.81} \end{array} \right\rangle$

A-line

73

7+00

293.6 ✓
11.4

T.P. 12.17 $\langle 304.99 \rangle$
311.11 0.54 $\langle 298.57 \rangle$
298.64

$\langle 304.99 \rangle$ ✓
311.11

6+70

290.0 ✓
3.1

Δ approx 10° Rt. + 170° left.
6+86 = ± 3' wide cobble drain (poor cond.)

287.3 ✓
5.8

6+80

286.5 ✓
6.6

T.P. 12.32 $\langle 293.06 \rangle$
299.18 0.24 $\langle 280.74 \rangle$
280.86

$\langle 293.06 \rangle$ ✓
299.18

6+68

279.9 ✓
1.1

6+40

274.8 ✓
6.2

6+17

269.7 ✓
11.3

$\langle 280.96 \rangle$
287.10

A-line

EL. $\langle 309.75 \rangle$
Check 470+67^{SE} $\frac{FB1631}{45}$ 5.90 $\langle 309.90 \rangle$ $\frac{309.95}{316.02} = 309.91$
1x1 City

7+61.18 = End of line

313.9 ✓
1.9

7+57.52 = Cross on wall P.O.T.

314.1 ✓
1.7

7+57 = Top. Cobble wall

311.4 ✓
4.4

7+56^E Gnd.

7+54^E 2' RT. = N.E.ly. Cor. Bldg.

306.9 ✓ 310.56 ✓
8.9 $\frac{5.24}{2}$
Floors EL.

7+46^E 7^E RT. = N.W. Cor. Bldg.

7+42 = 1' wide Conc. wall. 55° RT + 135° LT.

TOP

T.P. 11.15 $\langle 315.80 \rangle$ $\frac{321.92}{310.77}$ 0.34 $\langle 304.65 \rangle$

$\langle 315.80 \rangle$
 $\frac{321.92}{310.77}$

+29

303.3 ✓
1.7

155° RT.

7+25 = $\frac{1}{4}$ of open Cobble drain 35° Left

300.3
4.7

7+19

300.3 ✓
4.7

304.99
311.11

74

B-line
Sketch - P. 68 - right

75

1+18

204.2 ✓
5.4

1+00

202.8 ✓
6.8

+80

204.1 ✓
5.5

+15

202.4 ✓
7.2

0+01

202.1 ✓
7.5

0+00 = So. end existing Crossing #5

199.5 ✓
10.1

Aprox. invert.

~~209.56~~ ✓ City Datum
215.68 - from P. 66

B-line

2+62

2+48

2+37

T.P.

5.04

$\langle 213.51 \rangle$
219.63

1.09

$\langle 208.47 \rangle$
214.59

1+95

+50

1+35

+

76

207.0 ✓
6.5

202.0 ✓
11.5

206.7 ✓
6.8

$\langle 213.51 \rangle$
219.63

207.4 ✓
2.2

205.2 ✓
4.4

203.0 ✓
6.6

$\langle 209.56 \rangle$
215.68

B-line

±

77

4+65

218.6 ✓
4.3

4+33

216.4 ✓
6.5
W

4+15

216.1 ✓
6.8

3+90

213.7 ✓
9.2

T.P. 9.97 $\langle 222.92 \rangle$ ✓
229.04 0.56 $\langle 212.95 \rangle$ ✓
219.04

$\langle 222.92 \rangle$ ✓
229.04

3+50 @ross wash

208.1 ✓
5.4
W

3+10

208.5 ✓
5.0

$\langle 213.5 \rangle$ ✓
219.63

B-117c

4

78

= 5 + 41⁶⁸ Page 72

5 + 38 ⁴⁶ = Δ 35° - 19' - 10" Lt.

5 + 25

230.69 ✓
1.00
Hub

5 + 00 - 2' Rt. = 18" Willow

227.2 ✓
4.5

4 + 85

224.2 ✓
7.5

T.P. 9.08 $\left\langle \begin{array}{l} 231.69 \\ \hline 237.87 \end{array} \right\rangle$ 0.31 $\left\langle \begin{array}{l} 222.61 \\ \hline 228.73 \end{array} \right\rangle$

222.9 ✓
8.8

$\left\langle \begin{array}{l} 231.69 \\ \hline 237.87 \end{array} \right\rangle$

4 + 75

221.6 ✓
1.3

$\left\langle \begin{array}{l} 222.92 \\ \hline 229.04 \end{array} \right\rangle$

