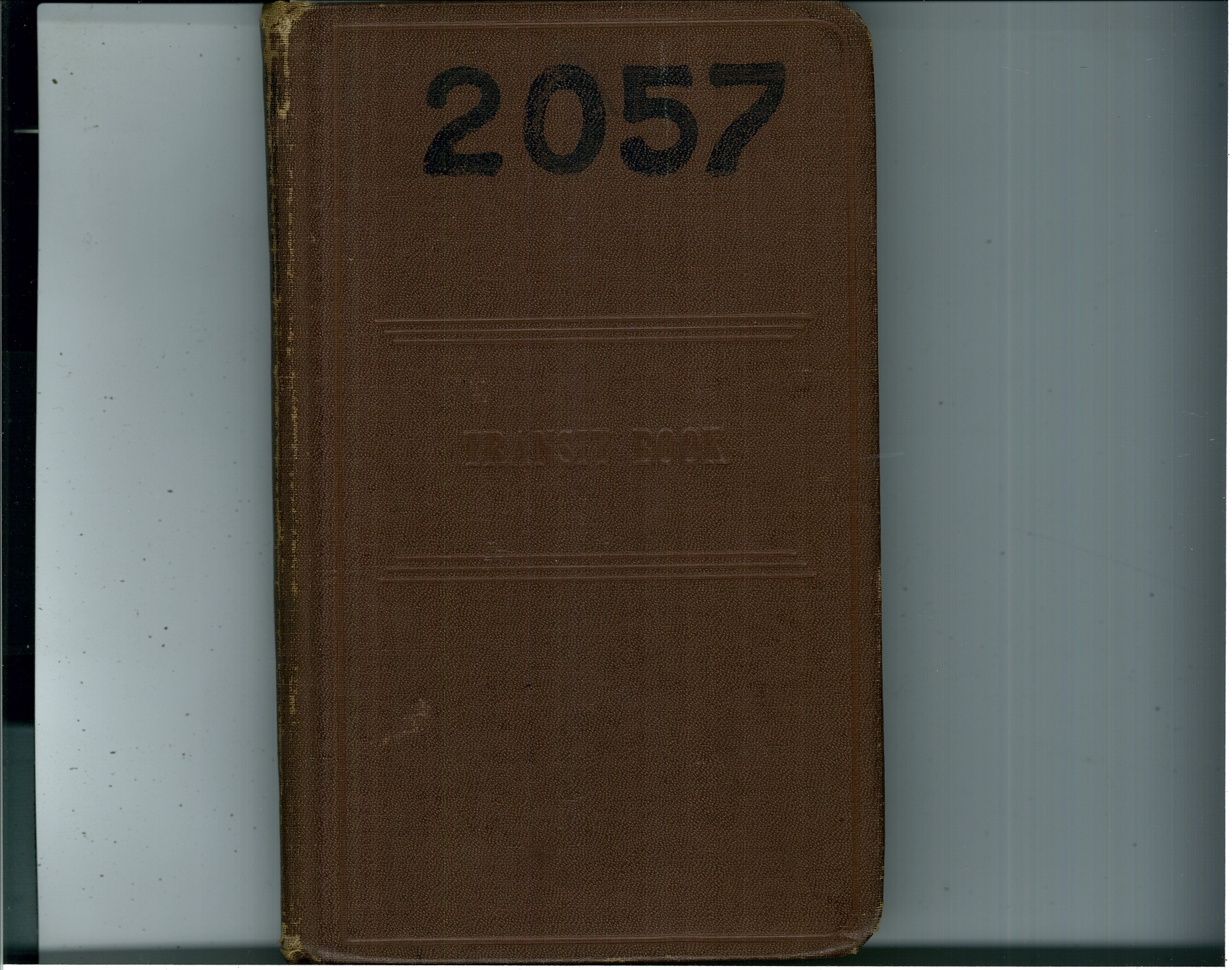
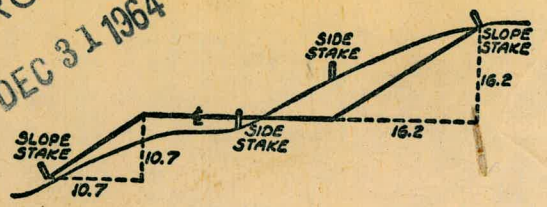

2057



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4 10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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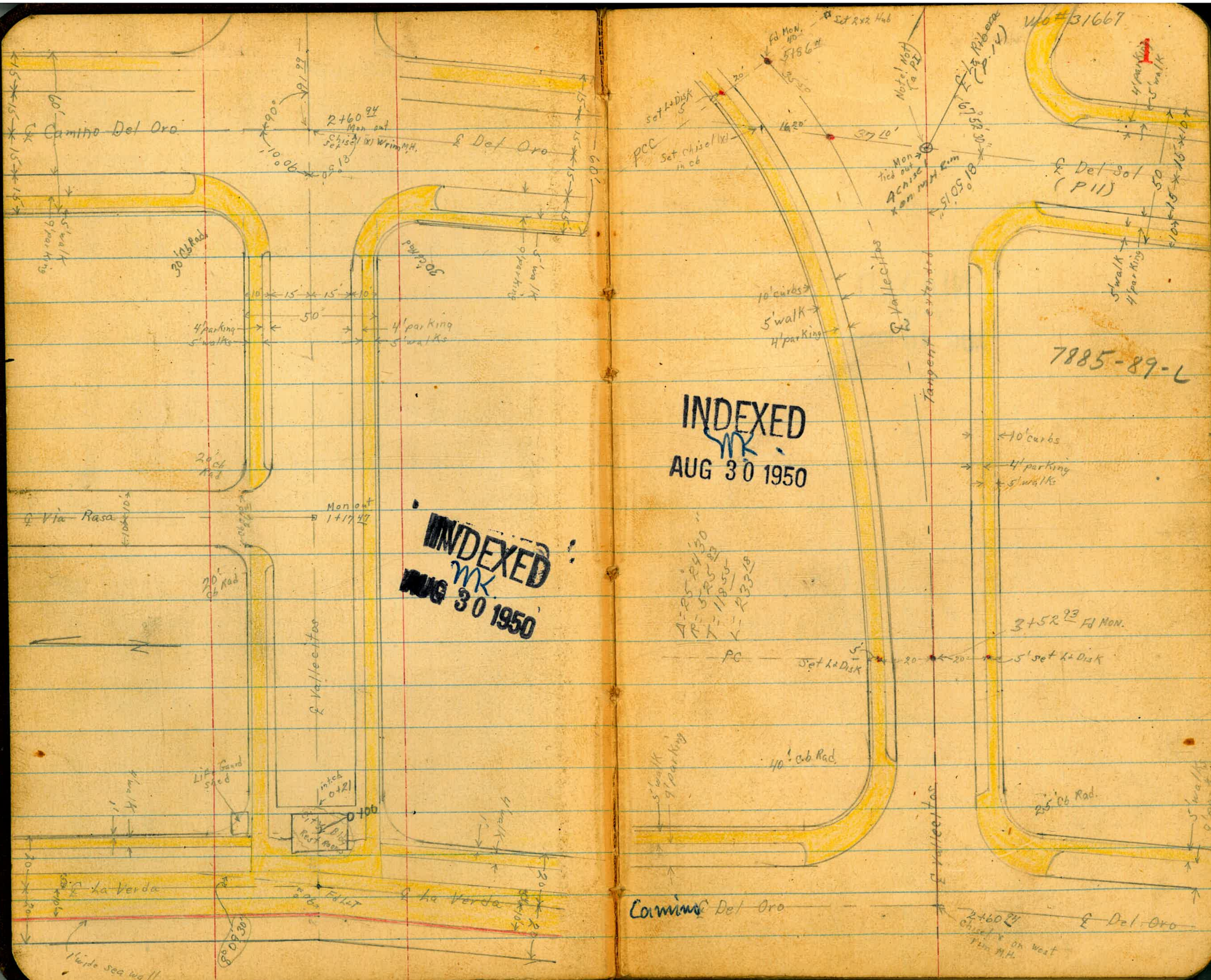


7885-89-L

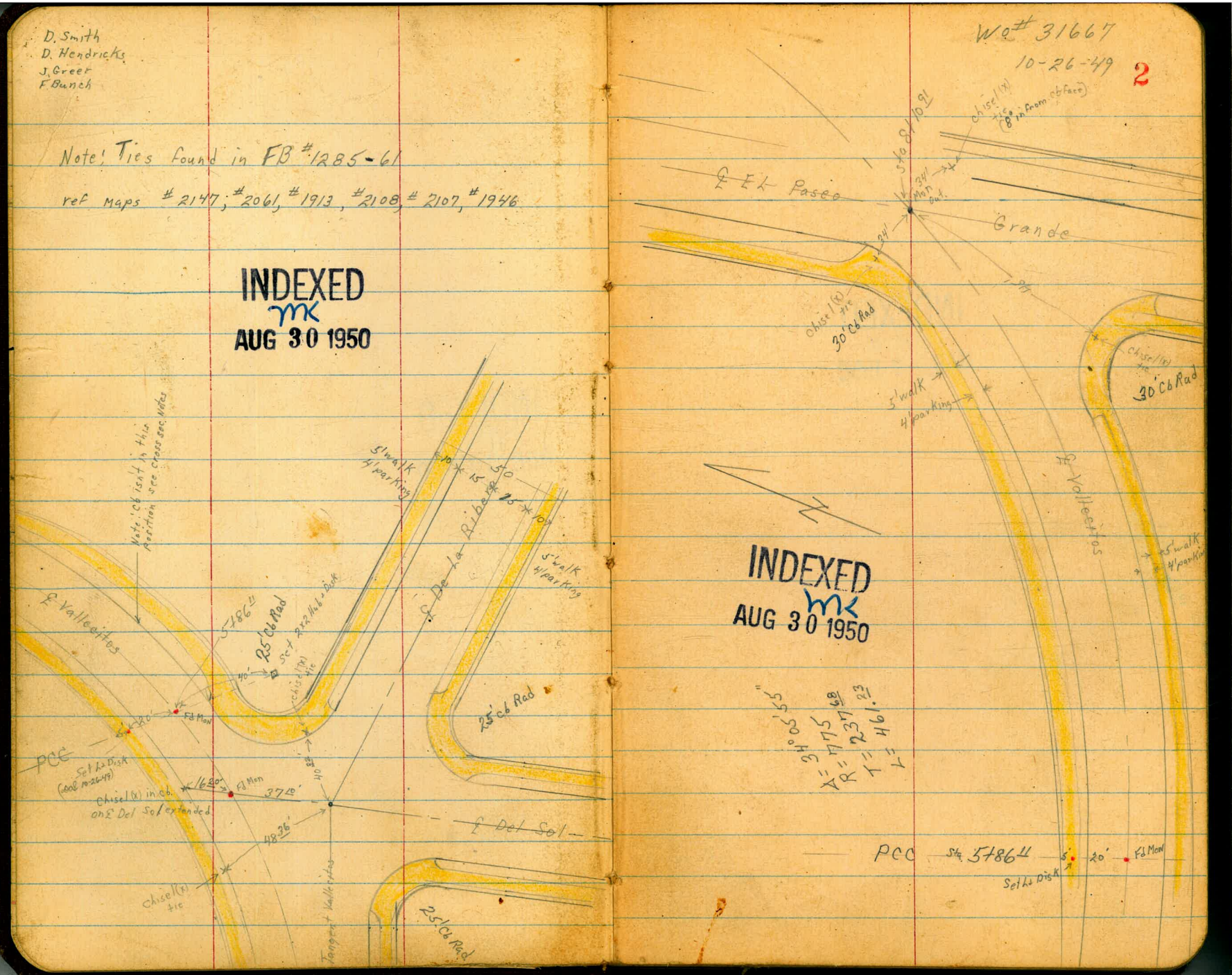
D. Smith
D. Hendricks
J. Greer
F Bunch

W.O. # 31667
10-26-49
2

Note! Ties found in FB #1285-61

ref Maps #2147; #2061, #1913, #2108, #2107, #1946

INDEXED
MK
AUG 30 1950



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AUG 30 1950

Wo # 31667
10-27-49

3

Cross Section Vallecitos

La Vereda to El Paseo Gramde

Lt = North ℄ Rt = South

0+00 East prop. Line La Vereda (at 90°)
Int. of prop. lines + ℄

0-01 Easterly edge 4' con walk parallel to La Vereda

0-5.7 Westerly of Rest Rooms Bldg con floor

0-14.6 Easterly of walk on edge

0-20 ℄ La Vereda taken along ℄

0-30 Easterly of sea wall taken along line of wall

BM 3 33 6 84 3 51 (3 ℄ also)

BP End Sea Wall La Playa + La Vereda

	2.0	2.0	2.1		2.1	2.0	2.0
	4 8	4 8	4 7	14 bldg	4 7	4 8	4 8
	50	25	13		13	25	50
	1.99	2.03			1.94	2.03	
	4 85	4 81		14 bldg	4 80	4 81	
	50	25			25	50	
			2.20				
			4 64				
			floor				
	1.89		1.90		1.86		
	4 95		4 94		4 98		
	25				25		
	1.74		1.79		1.78		
	5 10		5 05		5 06		
	25				25		
3.63	1.57		1.67		1.70	3.67	
3 21	5 27		5 17		5 14	3 17	
25 top wall	25 walk		walk		25 walk	25 top wall	

6 84

Cont.

1+05 Knk cb Return

Middle existing return

0+87.47 15° Lt cb PC

0+50

0+21 where cb crosses st.

0+11 Easterly Rest Rooms Bldg

TP 5.05 7.36 4.53 2.31

Elev. of Grate at End of Vallecitos (sta. 0+21)

	Rod	El.
FL.	- 7.11.	0+41
Grate -	- 6.22	1.30
Cb -	- 5.37	2.15

BM +4.01 7.52 3.51

Seawall La Playa

2' opening

2' x 2' grate

7.36

Cont.

1+05 Knb cb Return

Middle existing return

0+87 47 15' Lt cb PC.

0+50

0+21 where cb crosses st.

0+11 Easterly Rest Rooms Bldg

TP 5.05 7.36 4.53 2.31

2.4 2.51 2.2 2.3 2.0 2.3 2.51 2.5
4.9 4.85 5.2 5.1 5.4 4.99 4.85 4.9
25 23.2 Knb cb 15 15 15 94t 19 walk 25
4.87 22.49

2.7 2.53 2.43 2.0 2.3 1.8 2.30 2.41 2.3
4.7 4.73 4.63 5.4 5.1 5.6 5.06 4.95 5.1
25 19 walk 15 cb 15 94t 15 94t 15 cb 19 walk 25

2.4 2.43 2.33 1.9 2.2 2.3 2.18 2.33 2.4
5.0 4.93 5.03 5.5 5.2 5.1 5.18 5.03 5.0
25 19 walk 15 cb 15 94t 15 94t 15 cb 19 walk 25

3.5 2.18 2.3 2.20 2.16 2.16 2.3 2.26 2.5
4.9 5.18 5.1 5.16 5.20 5.30 5.1 5.10 4.9
25 19 walk 15 94t 15 cb Top cb 15 cb 15 94t 19 walk 25

2.5
4.9
Ground

7.36

Vallecitos
Cont

	Lt			℄	Rt	
2+15 94 15' Lt PC cb return	3.2 / 42 / 25	2.93 / 443 / 19 walk	2.87 / 449 / 15 cb	2.2 / 52 / 15 gut	2.3 / 51 /	1.7 / 556 / 15 gut	2.79 / 457 / 15 cb
2+08 92 15' Rt PC cb return	3.2 / 42 / 25	2.87 / 449 / 19 walk	2.83 / 453 / 15 cb	2.1 / 53 / 15 gut	2.2 / 52 /	1.9 / 55 / 15 gut	2.69 / 467 / 15 cb
2+00	3.2 / 42 / 25	2.82 / 454 / 19 walk	2.81 / 455 / 15 cb	2.1 / 53 / 15 gut	2.3 / 51 /	1.9 / 55 / 15 gut	2.64 / 472 / 15 cb
1+47 47 15' Lt cb pcc	2.9 / 45 / 25	2.71 / 465 / 19 walk	2.65 / 471 / 15 cb	2.1 / 53 / 15 gut	2.3 / 51 /	2.0 / 54 / 15 gut	2.01 / 489 / 15 cb
1+30 24° Lt end cb return as exists	2.8 / 46 / 25	2.77 / 459 / 24 cb ext	2.8 / 446 / 24 gut	2.2 / 52 / 15	2.4 / 50 /	2.0 / 54 / 15 gut	2.38 / 498 / 15 cb
1+17 47 ℄ Via Rosa			2.6 / 48 / 25	2.3 / 51 / 15	2.3 / 51 /	2.0 / 54 / 15 gut	2.39 / 497 / 15 cb

2.87 / 449 / 19 walk	2.83 / 453 / 15 cb	2.1 / 53 / 15 gut	2.2 / 52 /	1.9 / 55 / 15 gut	2.69 / 467 / 15 cb	2.87 / 449 / 19 walk
2.82 / 454 / 19 walk	2.81 / 455 / 15 cb	2.1 / 53 / 15 gut	2.3 / 51 /	1.9 / 55 / 15 gut	2.64 / 472 / 15 cb	2.87 / 449 / 19 walk
2.71 / 465 / 19 walk	2.65 / 471 / 15 cb	2.1 / 53 / 15 gut	2.3 / 51 /	2.0 / 54 / 15 gut	2.01 / 489 / 15 cb	1.85 / 471 / 19 walk
2.77 / 459 / 24 cb ext	2.8 / 446 / 24 gut	2.2 / 52 / 15	2.4 / 50 /	2.0 / 54 / 15 gut	2.38 / 498 / 15 cb	2.60 / 476 / 15 walk
2.6 / 48 / 25	2.3 / 51 / 15	2.3 / 51 /	2.0 / 54 / 15 gut	2.39 / 497 / 15 cb	2.54 / 482 / 19 walk	2.5 / 49 / 25

7 36

Cont

3+52 93 B.C. Lt From here all sections taken radially

3+15 94 15' Lt PC cb return

3+01 5 15' Rt PC, cb return

2+75

2+60 94 Int ℄ Del Oro and ℄ Vallecitos

2+42

	Lt			℄		Rt			
	3.36	3.28	2.5	2.8	3.0	2.9	2.5	3.06	3.19	3.4
	4⁰⁰	4⁰⁸	4⁹	4⁶	4⁴	4⁵	4²	4³⁰	4¹²	4⁰
	19 w&k	15 cb	15 Sat	8		8	15 Sat	15 cb	19 w&k	25
	3.2	3.13	2.99	2.5	2.7	2.8	2.6	2.3	2.90	3.00	3.3
	4²	4²³	4³⁷	4²	4⁷	4⁵	4⁸	5¹	4⁴⁶	4³⁶	4¹
	25	19 w&k	15 cb	15 Sat	8		8	15 Sat	15	19 w&k	25
	2.87	2.5	2.5	2.7	2.8	2.4	2.2	2.82	3.02	3.1
	4⁴⁹	4⁷	4⁹	4⁷	4⁶	4⁹	5²	4⁵⁹	4³⁴	4³
	17 cb	17 Sat	15	8		8	15 Sat	15 cb	19 w&k	25
	2.6	2.9	2.9	2.5	2.2					
	4⁸	4⁵	4⁵	4²	5²					
	25	15		15	25					
	2.7	2.8	2.83	2.7	2.6					
	4⁷	4⁶	4⁵³	4⁷	4⁸					
	25	15	1 m MH.	15	25					
	2.4	2.7	2.5	2.6	2.5					
	4⁹	4⁷	4⁹	4⁸	4⁷					
	25	15		15	25					

7 36

Vallecitos
cont.

5+50

5+00

4+73 29± Rt End driveway

4+50

4+19 19± Rt Begin driveway

TP 6.08 9.35 4.09 3.27

4+00

7

Lt Rt

4.4	4.11	4.03	3.6	3.7	3.9	4.2	4.1
5.0	5.24	5.32	5.2	5.7	5.5	5.2	5.3
25	18± walk	14± cb	14± 9+t	7		12	25

4.0	4.01	3.90	3.3	3.5	3.8	3.9	3.8
5.4	5.34	5.45	6.1	5.9	5.6	5.6	5.6
25	18± walk	19± cb	14± 9+t	7		15	25

						2.97	3.54
						6.38	5.81
						29± Lip Drive	33± walk

4.0	3.96	3.92	3.0	3.5	3.6	3.7	2.85	3.54
5.4	5.39	5.43	6.1	5.9	5.8	5.7	6.50	5.81
25	19± walk	15± cb	15± 9+t	8		10	24± Lip drive	28± walk

							2.75	3.45
							6.60	5.90
							19± Lip Drive	23± walk

9.35

3.9	3.75	3.67	2.8	3.1	3.4	3.4	2.6	2.25
3.5	3.61	3.69	4.6	4.3	4.0	4.0	4.8	4.11
25	19± walk	15± cb	18± 9+t	8		6	17 9+t	17 cb

7.36

Vallecitos
cont.

8

	Lt					℄			Rt		
7+50	6.1	6.14	6.11	5.1	5.3	5.7	5.5	5.4	6.33	6.47	6.81
	3 3 25	3 21 19 walk	3 24 15 c6	4 3 15 94t	4 1 8	3 7	3 2 8	4 0 14 94t	3 02 14 c6	2 88 18 walk	2 84 23 walk
7+00	5.6	5.53	5.46	4.6	4.8	5.2	5.1	4.7	5.49	5.56	5.60
	3 8 25	3 82 19 walk	3 89 15 c6	4 8 15 94t	4 6 9	4 2	4 3 9	4 6 16 94t	3 56 16 c6	3 29 20 walk	3 25 25 walk
6+50	4.9	4.80	4.77	3.8	4.3	4.8	4.5	4.0	4.47	4.72	4.90
	4 5 25	4 55 19 walk	4 58 15 c6	5 6 15 94t	5 1 9	4 6	4 9 12	5 4 18 94t	4 58 18 c6	4 63 22 walk	4 45 27 walk
6+00	4.7	4.44	4.36	3.6	4.0	4.4	4.3	3.5	4.16	4.26	4.33
	4 7 25	4 91 18 walk	4 99 14 c6	5 8 14 94t	5 4 8	5 0	5 1 12	5 2 22 94t	5 12 22 c6	5 09 26 walk	5 02 31 walk
	4.5	4.25	4.21	3.6	3.8	4.3	4.3	3.6	3.95		4.21
	4 9 25	5 10 18 walk	5 14 14 c6	5 8 14 94t	5 6 8	5 1	5 1 12	5 8 24 94t	5 40 24 c6		5 14 33 back crest walk

5+86 PCC Lt also PC & tr return 24 Rt

9.35

Vallecitos
Cont.

Lt. & Rt

			BP La Playa ✓ End Sea Wall	
BM starting		3^{42}	3^{52}	3^{51}
	on N 9' line La Playa			
TP	& Del Sol	4^{59}	6^{94}	7^{00} 2^{35}
			8' in from Ck on chisel (X) tie SE cor Paseo Grande Vallecitos	
TP to BM		1^{90}	7^{45}	

8+10 ^{91} Int & El Paseo Grande and & Vallecitos
Sec. taken radially

		6.2	6.3	6.4	6.4	6.4
		3^{2}	3^{1}	3^{0}	3^{0}	3^{0}
		25	15		15	25

		6.45	5.5	5.7	6.0	5.9	5.8
7+80		2^{90}	3^{9}	3^{7}	3^{4}	3^{5}	3^{4}
		15	15	8		11	25
		04	94				

9^{35}

55' Long 5 parts 11' eq.
30' Rad
SW Return El Paseo Grande & Vallecitos

		Top curb	gutter
PRC Vallecitos		3.00	4.0
		6.53	5.4
1		2.82	4.0
		6.58	5.6
2		2.77	3.8
		6.79	5.9
3		2.66	3.5
		6.50	5.8
4		2.85	3.6
		6.55	5.7
PC Grande		2.80	3.7
		6.35	5.6
PC + 25' South on Grande		3.00	3.8

HI 9.35

50' long 5 parts 10' eq.
30' Rad. NW Return Grande & Vallecitos

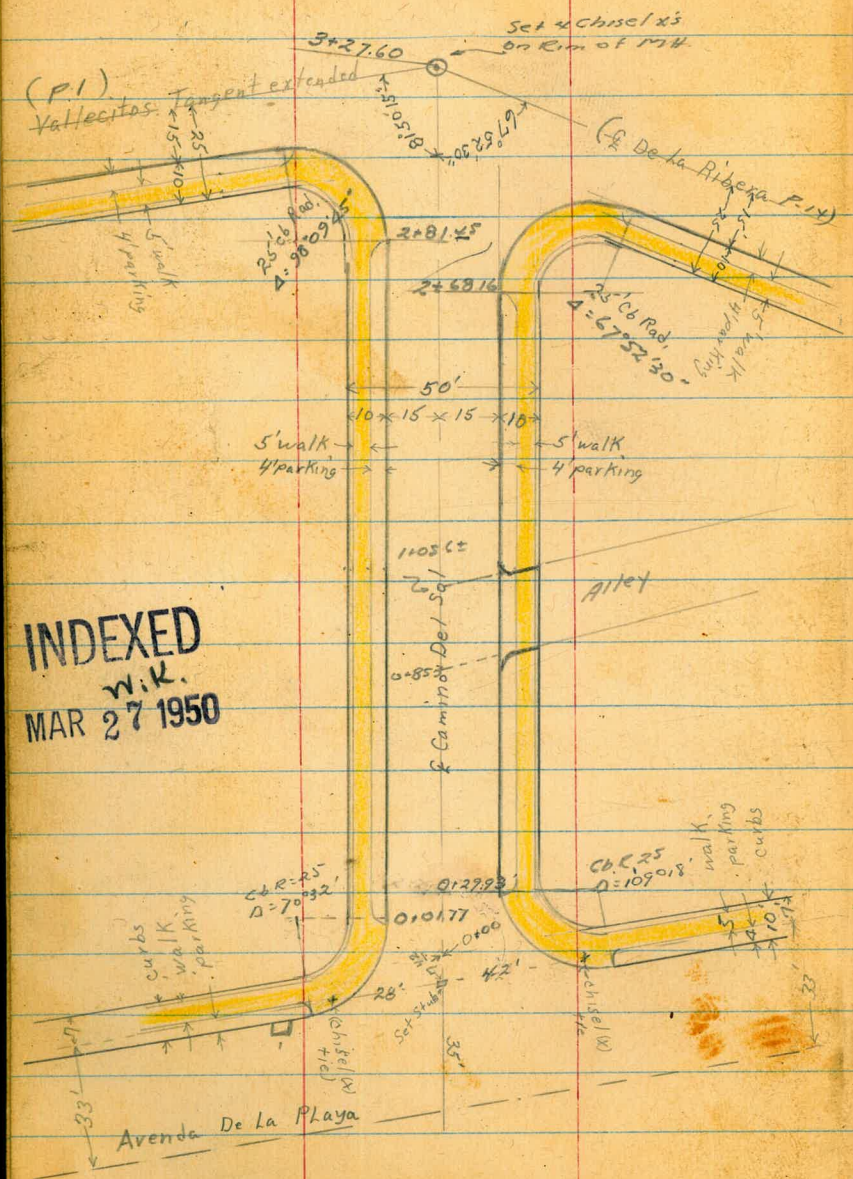
		Top curb	d. 29	gutter
PCC. Vallecitos		3.06		4.1
			6.41	5.53
1		3.24		3.9
			6.52	5.7
2		2.83		3.8
			6.56	5.7
3		2.79		3.7
			6.70	6.2
4		2.63		3.2
			6.81	6.2
PC Grande		2.54		3.2
			6.88	6.1
PC + 25' North Grande		2.47		3.3

HI 9.35

W.O. # 31667
10-28-49

11

X Sec Camino Del Sol
La Playa to Vallecitos



Levels Del Sol

0+99 2.5 x 2.5' Gas & Elec MH 7.9 Lt

0+85.3± Inter. of Production of Alley Cb on Dieg

0+50

0+00 Lt. Ls to Del Sol

NE Cb Ret La Playa & Del Sol 5 parts BC on La Playa (L=47.4)

NW Cb. Ret La Playa & Del Sol (4 parts BC on La Playa L=31.3

0-10.60 No. Cb. Line La Playa. Sec. Parallel to La Playa.

BM 6.64 8.99 235

6" 2.88
7.9
Q MH

3.31 3.53
5-68 5-46
17.9 26.7
EC
Cb 86 Cb 8 G

3.02 2.5- 2.9 3.0 3.30
5-97 6-5- 6.1 6.0 5-69
15 15 15 15
Cb G G Cb

2.7 2.9
6-3 6-3 6.1 6.0
15 14 40

3.0 3.51 3.0 3.54 3.0 3.56 2.7 3.48 2.6 3.40 2.8 3.34
6.0 5-48 6.0 5-45 6.0 5-43 6.2 5-51 6.4 5-59 6.2 5-45
G Cb G Cb G Cb G Cb G Cb. G Cb
BC ① ② ③ ④ EC

2.5 3.02 2.6 3.06 2.5 3.04 2.6 3.11 2.4 3.05
6.0 5-97 6.4 5-83 6.4 5-93 6.4 5-88 6.4 5-94
G Cb G Cb G Cb G Cb G Cb.
(BC) ① ② ③ EC

2.88 2.6 0.34 2.47 3.02 2.5- 2.5-
6" 6.4 8.5 6.5.2 5-97 6.5 6.5 6 2.8 6.2 2.8 6.0 3.51 5-48 3.2 5.8 3.74 5-25
53 53 38.2 38.2 33.59 33.59 15 22 51.15 51.15 100 100
Cb 6 FL Grate Cb G 8.99 G Cb. G Cb

On Stub & Del Sol N.T. Line La Playa (P.T.)

B.M. (Levels Del Sol) cont'd 1.61 7.46 7+45 (P9 this Bk)

SW1 Cb Ret Del Sol & Vallecitos BC on Del Sol
(L= 40' 2 parts)

3+00

2+81.45 BC Cb Ret Lt

2+68.16 BC Cb Ret on Rt

T.P. 5.05 9.07 4.97 4.02

2+50

2+00

1+50

1+05.6 ± Int of Production of Alley Cb at ℄ Del Sol

1+00

8.99

Chisel X on SE Vallecitos & Pascos Grande

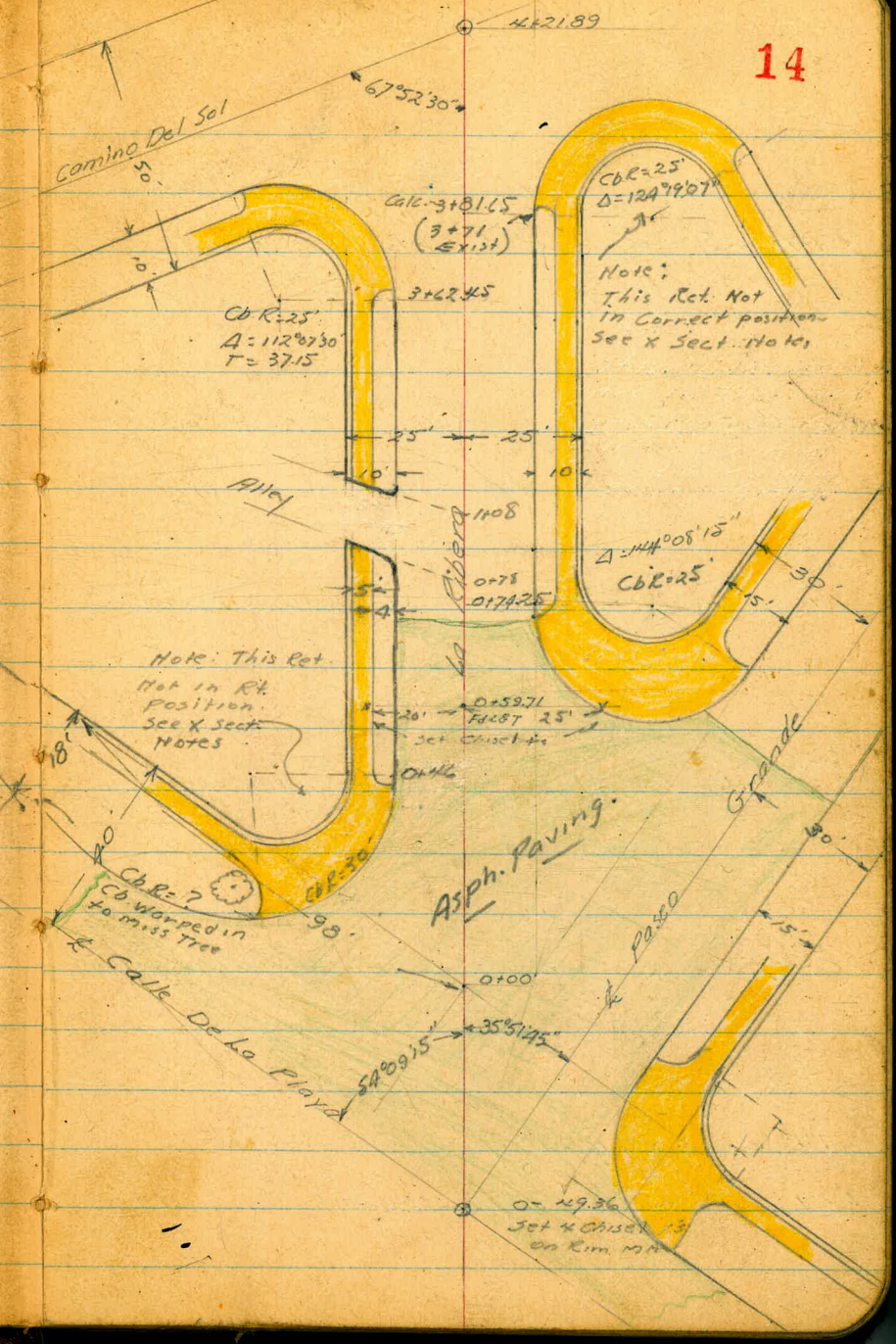
BC. ① ② ③ E.C.

9.07

8.99

11-49
Hendricks
Johnson
Greer
Cota
WO# 31667

X Section De La Ribera
Calle De La Playa to Del Sol



Levels De La Ribera

EC Cb Ret on Rt
0+74.25 End Asp. Pav.

0+46 EC Cb. Ret. on Lt.

0+00 No Line La Playa (Rt. Ls to Ribera)

0-24.68 No Cb Line La Playa on Rt (Sec. Parallel to La Playa)

0-49.36 ℄ La Playa section Parallel to La Playa

TP	4.21	10.39	5.75	6.18	
BM	4.48	11.93		7.45	Chisel X SE Cor Paseo Grande & Valleciitos (P.g this BK)

10.39

4.98 4.40 4.85 4.37 5.10
5.41 5.99 5.54 6.09 5.39
15 15 15 15
Cb G G Cb

5.17 4.63 5.10 4.99 4.76
5.22 5.76 5.29 5.40 5.63
15 15 15 30
Cb G

4.49 5.37 5.57 5.64 5.37
5.40 5.02 4.92 4.75 5.02
30 15 15 50

5.07 4.46 4.8 5.2 5.4 5.4 5.8 6.01 6.42 6.77 7.39
5.32 5.87 5.6 5.2 5.0 5.0 4.6 4.38 3.77 3.62 3.00
74 74 50 30 20 50 66 66 100 100
Cb G G Cb G

5.75 6.04 6.32 6.50 6.98
4.67 4.35 4.07 3.89 3.41
50 25 Rim HH. 26 50

De La Ribera Contd

1+50

1+08 ℄ Inter of Prod. Alley Cb on Lt.

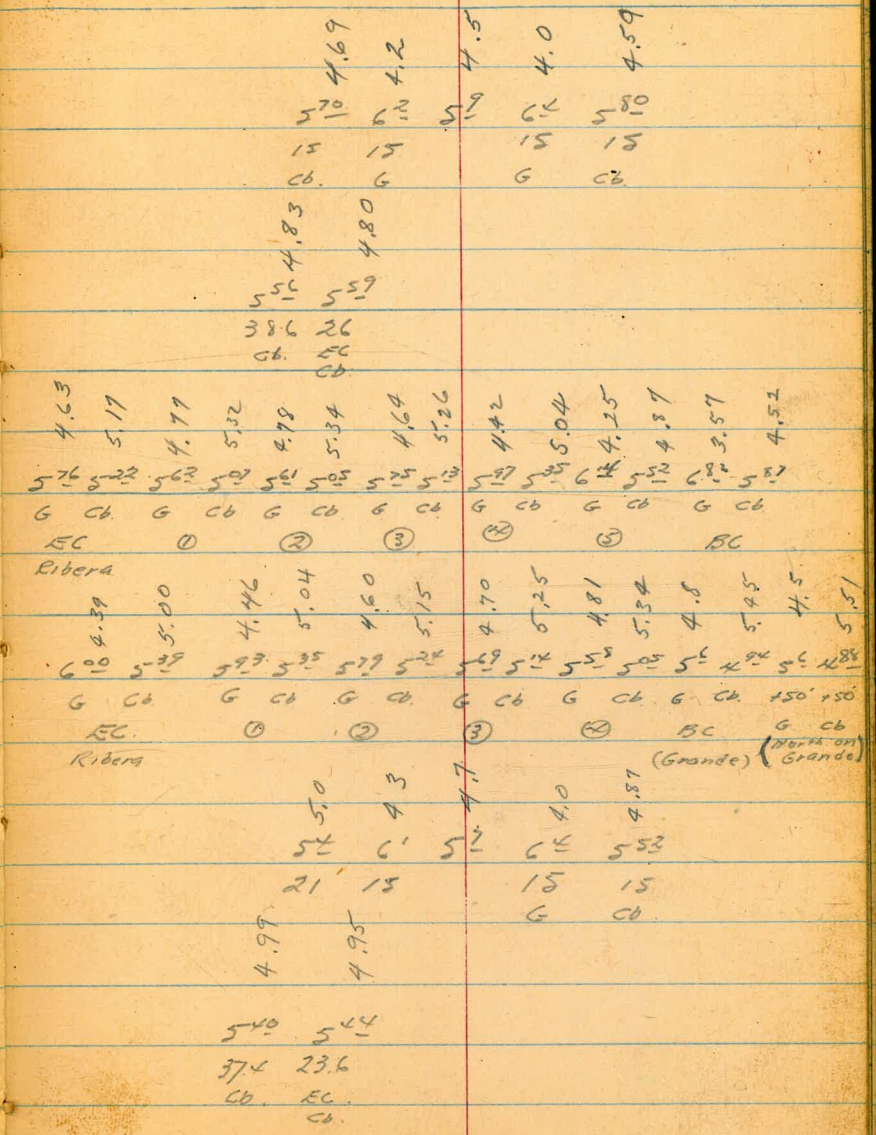
NWly Ret. La Playa & De La Ribera L=100'
(E.C. on Ribera) (6 parts)

NWly Cb Ret. Paseo Grande & De La Ribera.
L= 623 (5 pts) E.C. on Dela Ribera

1+00

0+78 ℄ Inter. of Prod. Alley Cb. on Lt.

10.39



10.39

De La Ribera Cont'd.

4+00

3+50

3+22 ℄ 21' Conc. Drive on Lt.

TP. 4.87 8.98 6.28 4.11

3+00

2+50

2+00

10.39

3.6 3.8 3.8 4.0 3.9
5.4 5.2 5.2 5.0 5.1
30 15 15 30

3.80 3.4 4.0 3.5 4.10
5.8 5.6 5.0 5.5 4.88
15 15 15 15
Cb. G. G Cb.

4.06 3.58
4.92 5.40
19 15
SW G

8.98

4.08 3.6 4.1 3.7 4.16
6.31 6.8 6.3 6.7 6.23
15 15 15 15
Cb. G. G Cb

4.27 3.6 4.2 3.3 3.95
6.12 6.8 6.2 7.1 6.44
15 15 15 15
Cb. G G Cb.

4.51 3.9 4.3 3.6 4.44
5.88 6.5 6.1 6.8 5.93
15 15 15 15
Cb. G. G Cb

10.39

De La Ribera Cont'd

BM 6.64 2.34 2.35

Stub & Del Sol N.T. Line La Playa (P.S this Bk)

3.4 3.92
5 5.06 5 3.4 5 3.05 5 3.4 5 3.93 5 3.3 5 3.90 5 3.3 4 4.01
G Cb G Cb G Cb G Cb G Cb
BC ① ② ③ EC
Ribera Del Sol

3.5 4.02 3.5 3.90 3.5 4.00 3.5 3.6 3.4 3.5 3.99 3.5 3.93
5 4.96 5 3.5 5 3.08 5 3.5 4 4.08 5 3.6 5 3.04 5 3.5 4 3.99 5 3.5 5 3.04
G Cb G Cb G Cb G Cb G Cb G Cb
BC ① ② ③ ④ EC
Ribera Vallecitos

3.8 3.9 3.85 4.1 4.2
5 3.7 5 3.1 5 3.13 4 4.9 4 4.8
30 15 Rim 15 30

JEly Ret. Ribera & Del Sol BC on Ribera.
L=48' 2 part.

NEly Ret. Ribera & Vallecitos BC on Ribera.
L=49.4 (5 parts)

4x 21.89 & Del Sol (Sewer MH)

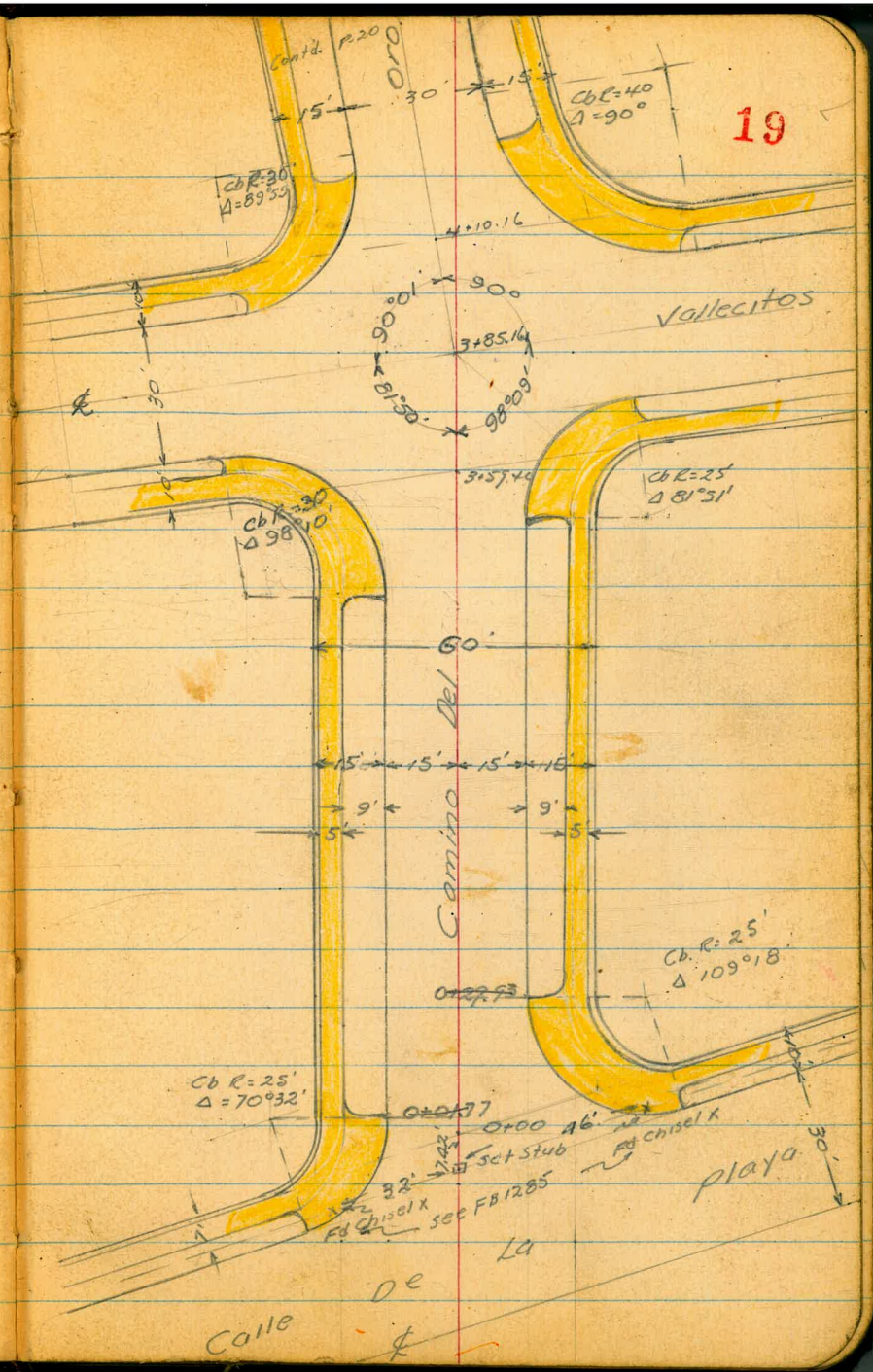
8.98

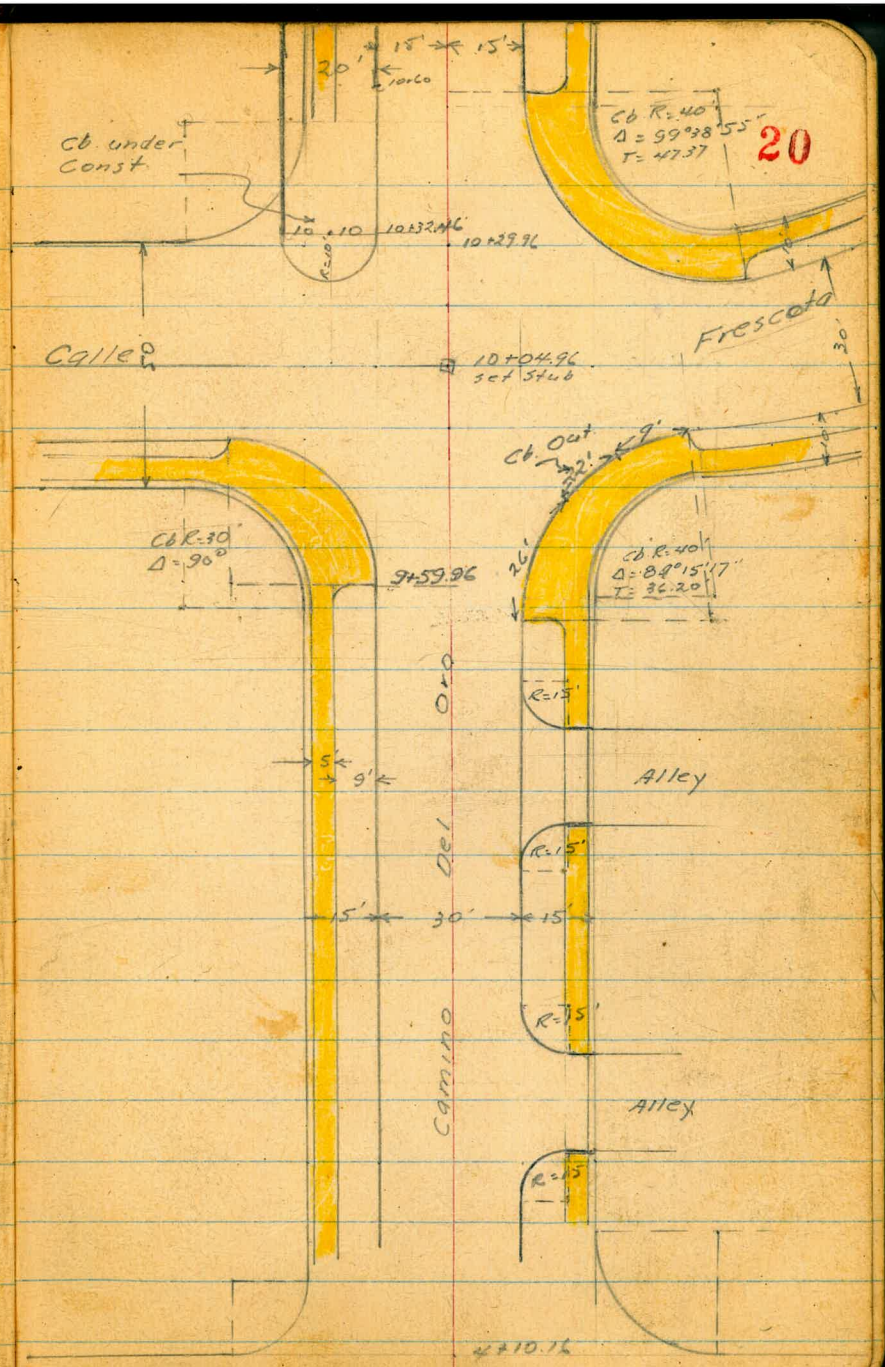
8.98

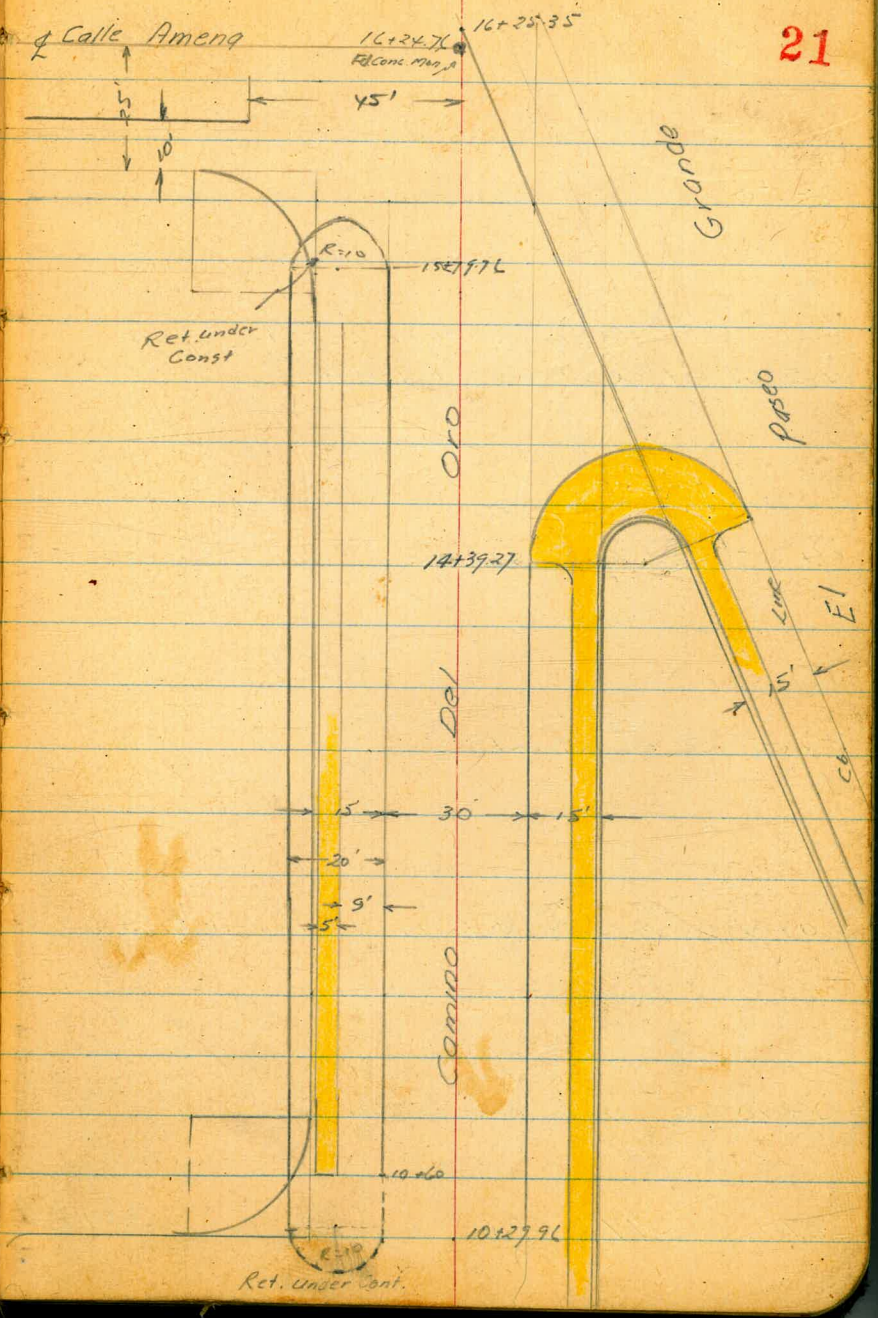
11-49
Hendricks
Johnson
Greer

RVO#31667

X Section Camino Del Oro
Calle De La Playa to
Paseo Grande




20'
15'
15'
10'c.o.
Cb under Const.
Cb R=40'
Δ=99°38'55"
T=47.37
10+10
10+32.46
10+29.96
R=10'
Frescota
30'
Calle 2
10+04.96
set stub
Cb Out
9'
32'
Cb R=30'
Δ=90°
9+59.96
26'
Cb R=40'
Δ=89°15'17"
T=36.20
0+0
R=15'
5'
9'
Alley
Del
15'
30'
15'
R=15'
Camino
R=15'
Alley
R=15'
4+10.76
Vallecitos
Cont'd from P. 19
St.



15+79.96
10+32.16
47.80

14+39.27
10+56.
383.27

Level Del Oro

0+50

BC on La Playa L=53.7 ~ 5 parts

NE Cb. Ret. La Playa & Del Oro

0+35 EC. Cb. Ret. Rt.

0+05 EC. Cb Ret. Lt.

0+00 No. Line La Playa section at Rt. Ls

section Parallel to La Playa.

0 - 10.60 N. Cb. Line La Playa.

BM. 2.77 6.28 3.51

B.P. Sea Wall La Playa

Del Oro Contd

3+33 BC Cb. Ref. on Lt.				
3+00				
2+50				
2+00				
1+50				
TP	5.96	7.58 ↑	4.66	1.62
1+00				
	6.28 ↑			

Q

2.85 2.1
4.73 5.5
15 15
Cb G

2.77 2.1 2.1 2.2 2.80
4.81 5.5 2.5 5.4 4.78
15 15 15 15
Cb G G Cb

2.6 1.6 1.9 2.1 2.60
5.00 6.10 5.7 5.5 4.88
15 15 15 15
Cb G G Cb

2.37 1.4 1.8 1.7 2.45
5.21 6.12 5.18 5.9 5.13
15 15 15 15
Cb G G Cb

2.14 1.2 1.5 1.4 2.20
5.44 6.4 6.1 6.12 5.38
15 15 15 15
Cb. G. G Cb.

7.58 ↑

1.92 1.0 1.4 1.3 2.10
4.24 5.3 4.9 5.0 4.18
15 15 15 15
Cb. G G Cb

6.28 ↑

Del Oro Cont'd

4+10.16 No Line Vallecitos

W. Rim Sewer M.H.

3+85.16 & Vallecitos Rt. Ls to Back Line

(inter. at Del Oro)

3+59.40 3o. Line Vallecitos Rt. Ls to Del Oro

L = 46.6 — 4 parts

5E Cb Ret. Del Oro & Vallecitos BC on Del Oro

L = 52.3' (4 parts)

3W Cb. Ret. Del Oro & Vallecitos BC on Del Oro

3+44 BC Cb Ret on Rt.

7.58

7.58

Del Oro Cont'd

5+00

4+50

L = 63.1' 4 parts

N.E. Cb. Rel. Del Oro & Vallecitos BC on Vallecitos

L = 46.4' (4 parts)

N.W. Cb. Rel Del Oro & Vallecitos BC on Vallecitos

4+40.16 E.C. Cb. Rel. on Rt.

4+30.16 E.C. Cb. Rel on Lt.

7.58

7.58

Del Oro Cont'd

T.P. 4.86 7.51 4.93 2.65

6+00

5+65 EC Alley Ret. Rt.

5+50 No Line Alley

5+40 ℄ Alley & Sewer MH.

5+30 So. Line Alley

5+15 BC Alley Ret. Rt.

7.58

3.24 2.2 2.7 2.7 3.65

4.34 5.14 4.9 4.2 3.95

15 15 15 15

C6 G G C6.

2.9 3.87

4.7 3.71

15 15

G C6.

3.25 2.7 2.8 2.7 3.5 3.54 3.8

4.33 4.9 4.8 4.9 4.1 4.04 3.8

15 15 15 30 30 50

C6 G C6.

3.26 2.7 3.17 2.9 3.1 3.4

4.32 4.9 4.41 4.7 4.14 4.12

15 15 Rim 15 30 50

C6 G

3.27 2.6 2.7 2.7 3.27 3.5

4.31 5.10 4.7 4.9 4.31 4.1

15 15 15 30 50

C6 G. G&C6

2.7 3.48

4.9 4.10

15 15

G C6.

7.58

8+50 So. Line Alley

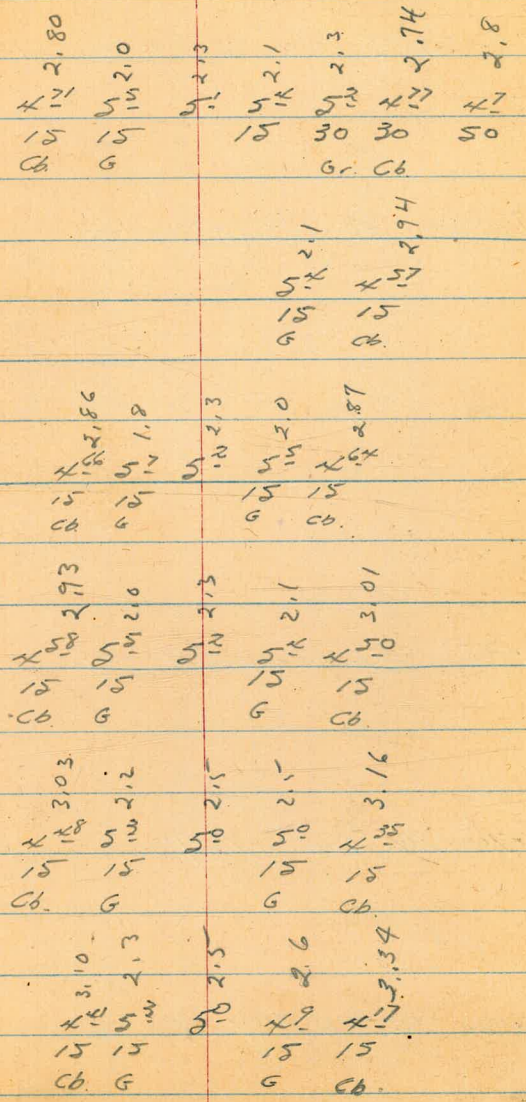
8+35 BC Alley Rel on Lt.

8+00

7+50

7+00

6+50



7.51

7.51

Del Oro Contd

9+59.96 BC Cb. Ret. on Lt.

9+55.7 BC Cb. Ret. on Rt.

9+00

8+85 EC. Alley Ret. Rt.

8+70 No. Line Alley

8+60 ℄ Alley

7.51
A

℄

2.8.3 1.9
4 6.8 5.5
15 15
Cb G

2.78 1.8 2.2 2.2 2.19
4 7.3 5.7 5 7.2 5 7.3 4 7.2
15 15 15 15
Cb G G Cb.

2.73 1.8 2.3 2.0 2.80
4 7.8 5.7 5 7.2 5 5.5 4 7.1
15 15 15 15
Cb. G G Cb.

2.1 3.87
5 1.4 4 6.4
15 15
G Cb.

2.76 1.9 2.4 2.2 2.40 2.1
4 7.2 5.6 5 7.1 5 7.3 4 7.1 4 7.4
15 15 15 30 50
Cb G G8Cb

2.86 2.0 2.4 2.3 4 7.8
4 7.5 5.4 5 7.1 5 7.2 5 7.1 4 7.1
15 15 15 30 50
Cb. G

7.51
A

Del Oro Cont'd.

10+29.96

10+04.96 ℄ Frescota

(L = 57.0 ⅄ parts)
S.E.Cb.Ret. Del Oro & Frescota B.C. on Del Oro

L = 47.0 ⅄ Parts.
S.W.Cb Ret. Del Oro & Frescota B.C. on Del Oro

9+89.86 So. Cb. Line Frescota

T.P. 5.1⅄ 7.24 5.41 210

9+79.96 So. Line Calle Frescota

7.51

℄

7.24

℄ Stub Del Oro & Frescota

7.51

Del Oro Cont'd.

11+50

11+00.

10+60 Beg Cb 15' Lt.

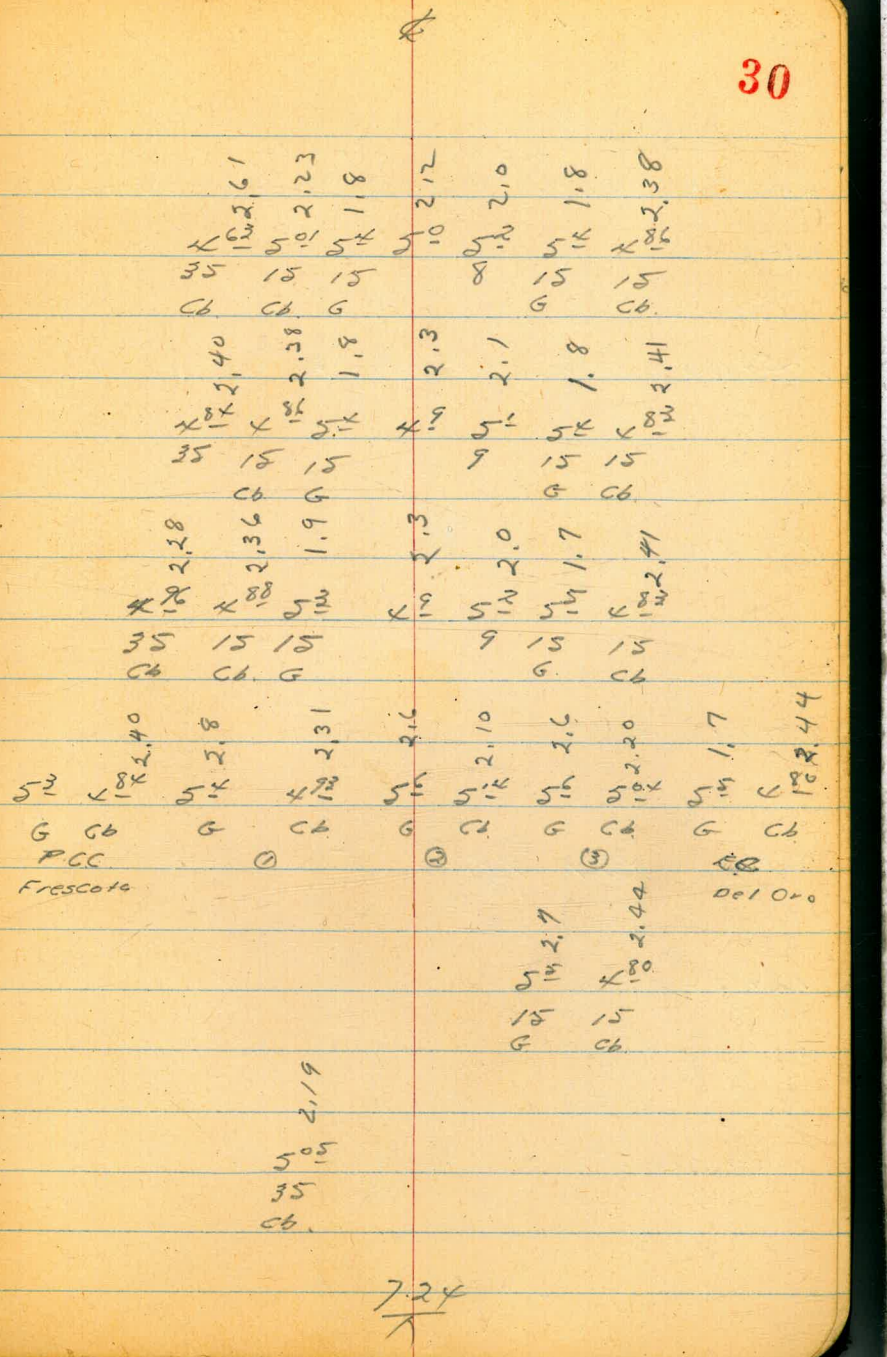
L = 60 4 parts.

NE Cb. Ret Del Oro & Frescota BC on Frescota

10+56 EC Cb. Ret. on Rt.

10+32.46 Beg New Cb. 35' Lt.

7.24



Del Oro Cont'd.

K = 1121' (Par.)

Cb. Ret. Del Oro & Paseo Grande BCon Del Oro

17+00

13+50

13+00

T.P. 4.99 7.23 5.00 2.24

12+50

12+00

7.24

BC. Del Oro = Sta 14+39.27

Grande

7.24

Del Oro Cont'd.

16+06.8(So Cb. Line Among
(as const)

15+99.76 So Line Among

15+79.76 End Present Cbs 158.35' Lt

15+50

15+00

14+50

7.23

7.23

B.M.			2.72	7.43	7.45
T.P.	7.01	10.15	4.09	3.14	

Chisel x SE Cor. Grande & Vallecitos (P.9 this BK)

16+80

2.0	2.2	2.1	2.2	2.0	2.1
5½	5°	5½	5°	5½	5½
60	30	15		15	25

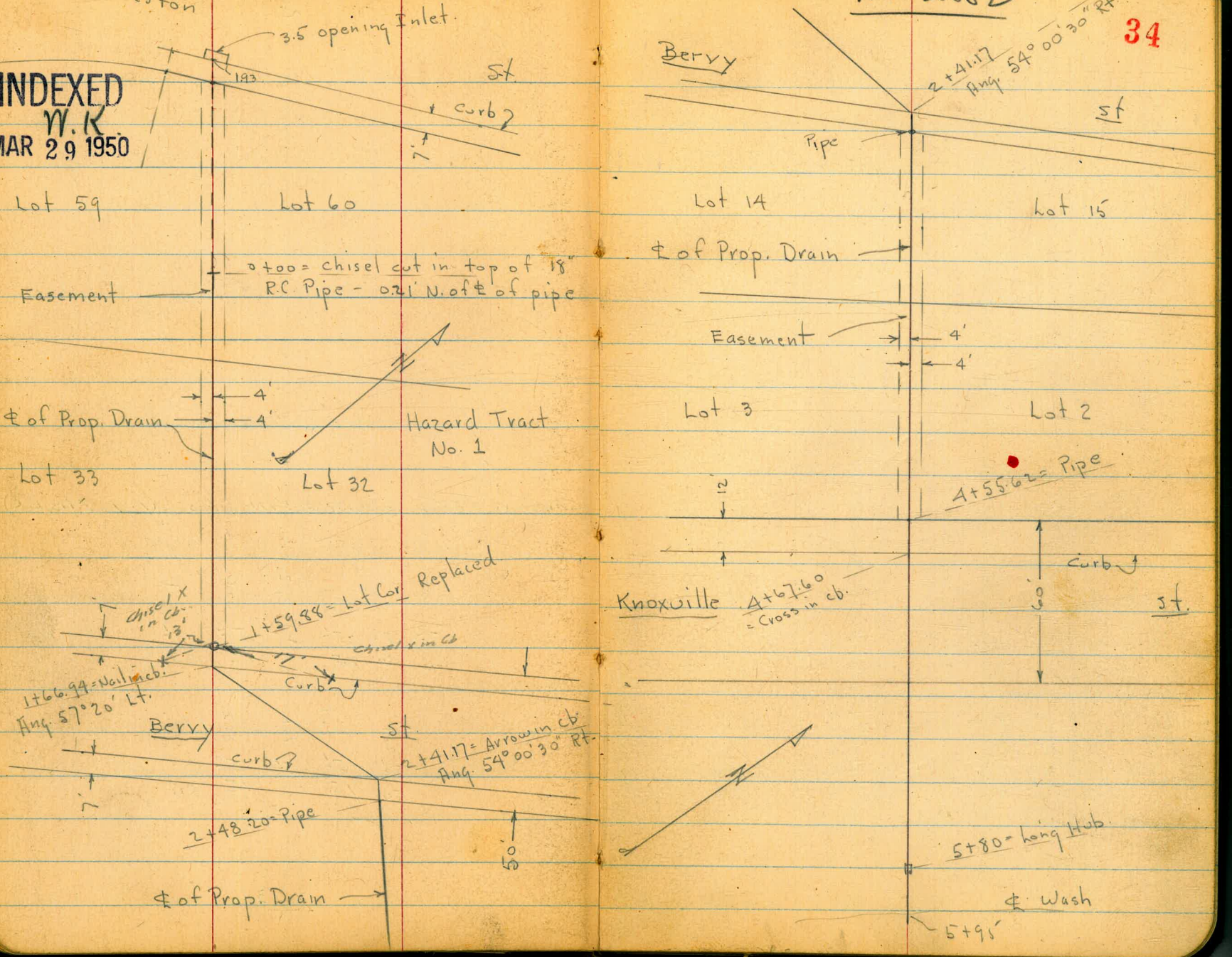
16+25. 35 Inter. W. Line Paseo Grande

2.1		2.1	2.1	2.2	1.8
5½	5½	5½		5°	5½
50	15			15	26

7.23

7.23

WO-20652



Survey for Proposed Drain - from end of Existing 18" R.C. Pipe - E. of Galveston St. Between Lots 59 + 60 - in Hazard Tract No. 1

See Sketch - P. 34.

3-29-50

Osborne
Hardin
Hatch
Shepard.

#

W.O. 20652

Beg. Levels along ℄ of Prop. Drain

				Lt.	℄	Rt.
1+05					16.45 4.69 2 edge	16.45 4.99 ℄ Drain
0+55				16.93 4.21 4 edge	16.65 4.49 2 ℄ Drain	16.9✓ 4.22 edge
0+30 = ℄ Drain						4.20 16.94
cold Lay Drain						
0+00 = outlet of 18" Pipe - Beg. 4' wide Dip Sect.						4.02 17.1✓ I.E. of Pipe + C.L.
Set B.M. - S.W. B.P.		2.30	18.84 - ✓	+ Bervy + Littlefield		
	7.62 21.14✓	3.73	13.52			21.14 ✓
	6.34 17.25✓	1.14	10.91			
B.M.	2.01 12.05✓		10.04 ✓	B.P. in Tecolote Bridge + Morena Blvd.		

3+00

T.P. 4.97 21.07 5.04 16.10

2+75 - House - both sides

2+65

2+50

2+41.17 = Hng. 54° 00' 30" Rt. = Arrow in cb. face

2+04 = ℄ st.

1+66.94 = Hng. 57° 20' Lt. = Nail in cb.

1+25 = opp. ℄ of Houses - both sides

Lt. ℄ Rt.

15.3 15.2 15.1
5.8 5.9 6.0
10 10

21.07

14.9 14.9 14.8
6.2 6.2 6.3
8.6 10.9
ground at House ground at House

6.3 14.8

4.8 16.3

16.54 16.44 16.0 16.24
4.60 4.70 5.1 4.90
12 = edge of Drive Top cb. gut. 20 Top cb.

16.1 16.1 15.8
5.0 5.0 5.3
10 10

16.44 16.28 16.18 15.7 15.74 16.15 16.00
4.70 4.86 4.96 5.4 5.40 4.99 5.14
20 5 Top cb. gut 2.5 ± Drain 4.5 edge = Top cb 20
Top cb. Top cb.

16.14 15.8
5.0 5.3
10.4 10.8 = ground at House
ground at House

21.14

5

5 + 50

5 + 16

5 + 13 = Dirt gutter

4 + 90 = ℄ Rd.

4 + 67.60 = Cross = cb. face

4 + 50

4 + 15 - Houses both sides

4 + 00

3 + 50 - 15 Lt. = ℄ P. pole # C 2480

Lt. ℄ Rt.

16.5
4.6

16.6 16.3 16.6
4.5 4.8 4.5
10 10

N.4 N.4 15.3
5.7 5.7 5.8
10 10

15.9
5.2

16.13 16.02 15.6 16.00
4.94 5.05 5.5 5.07 = Top cb.
20 Top cb. gut 4.0 edge of Dr.
Top cb.

14.0
5.1

5.2 15.4 15.4
9 5.4 5.4
along House 5 - along House

15.6 15.4 15.4
5.5 5.7 5.7
10 10

15.3
5.8

21.07 ✓

check B.M.		6.39	12.02 ✓	
T.P.	3.93	18.41 ✓	6.59	14.48
		end.		

5+90 = edge of water in wash

5+80 = P.O.T.

Lt. ℄ Rt.

N.W. B.P. Knoxville - Tonapah

Notes Reduced 3-30-50

11.0
10.1 = water Level

5.9 5.89 16.0
5.2 5.18 5.1
10 on Stub. 10
21.07

37th st.

From Z st. to National Ave

Z-Sec. for grade

5/3/50

W.O.# 31636

Sommermeyer
Allen
Sherman

Tie Pt. Sheets 386 + 408

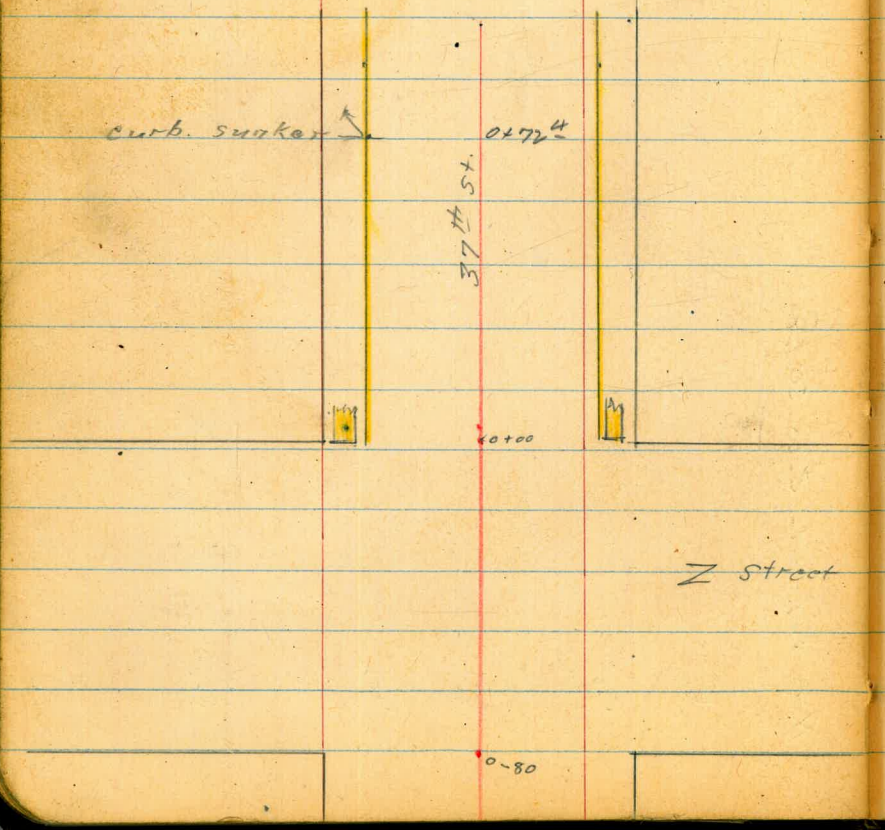
F.B. 1740/40

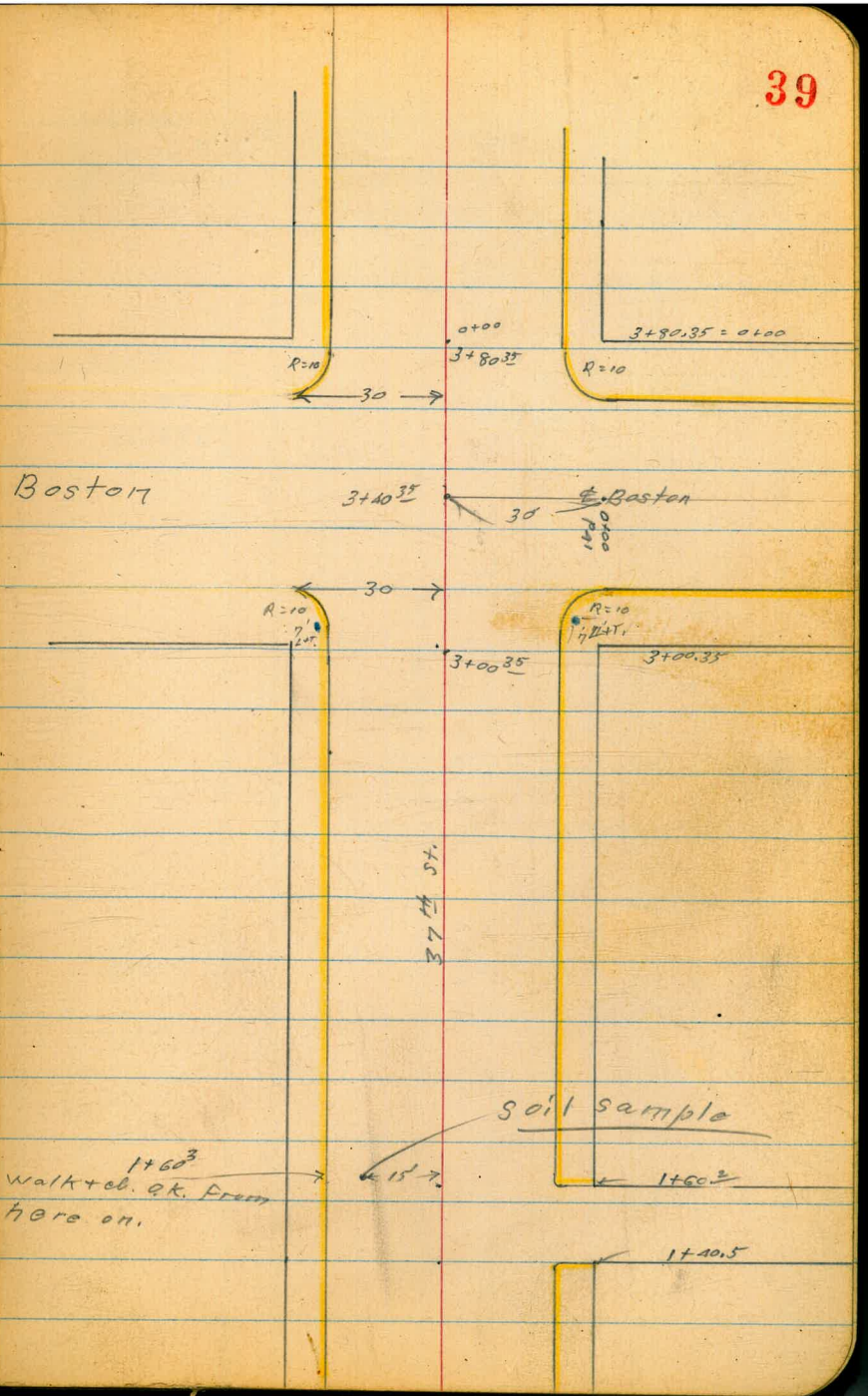
" 1763/42

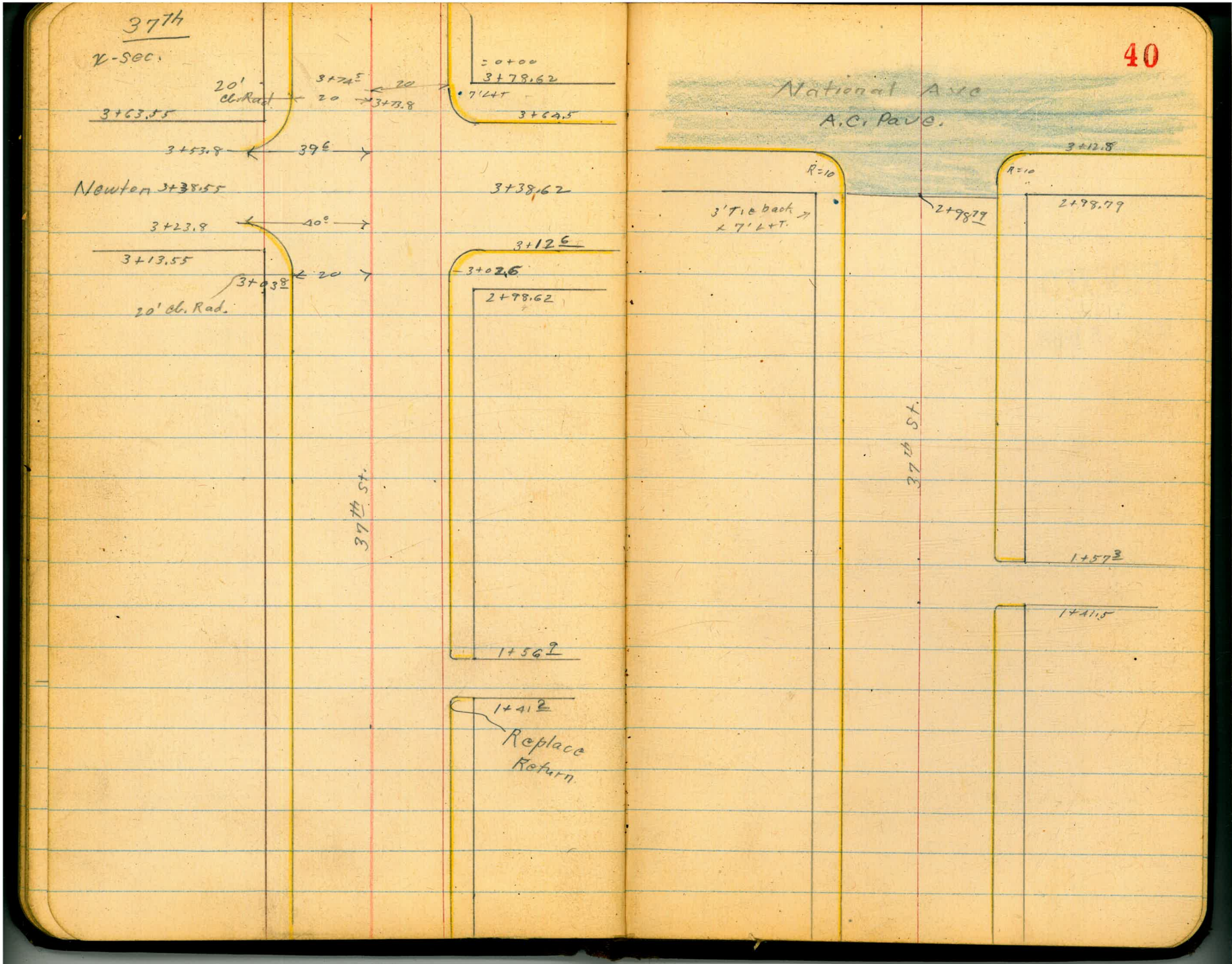
" 0-196/79

INDEXED
W. R.
MAY 5 1950

39






37th
Y-Sec.
20' Cl. Rad
3+74.5
20
20
3+73.8
3+63.55
3+53.8
39.6
Newton 3+38.55
3+23.8
40°
3+13.55
3+03.8
20
20' Cl. Rad.
37th St.
3+00
3+78.62
7' Lt
3+64.5
3+38.62
3+12.6
3+02.6
2+98.62
1+56.9
1+41.2
Replace
Return
National Ave
A.C. Pave.
R=10
3' Tie back
7' Lt.
2+98.79
37th St.
3+12.8
R=10
2+98.79
1+57.3
1+41.5

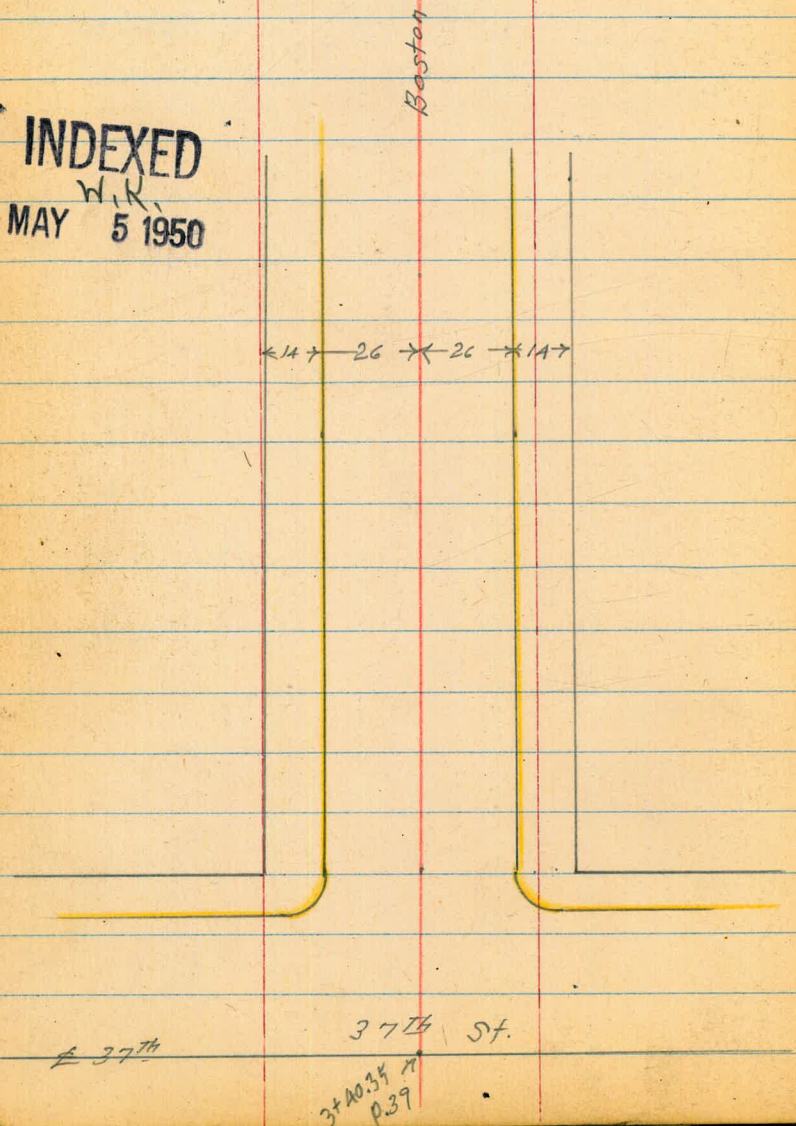
K-Sec. Boston

37th to 38th

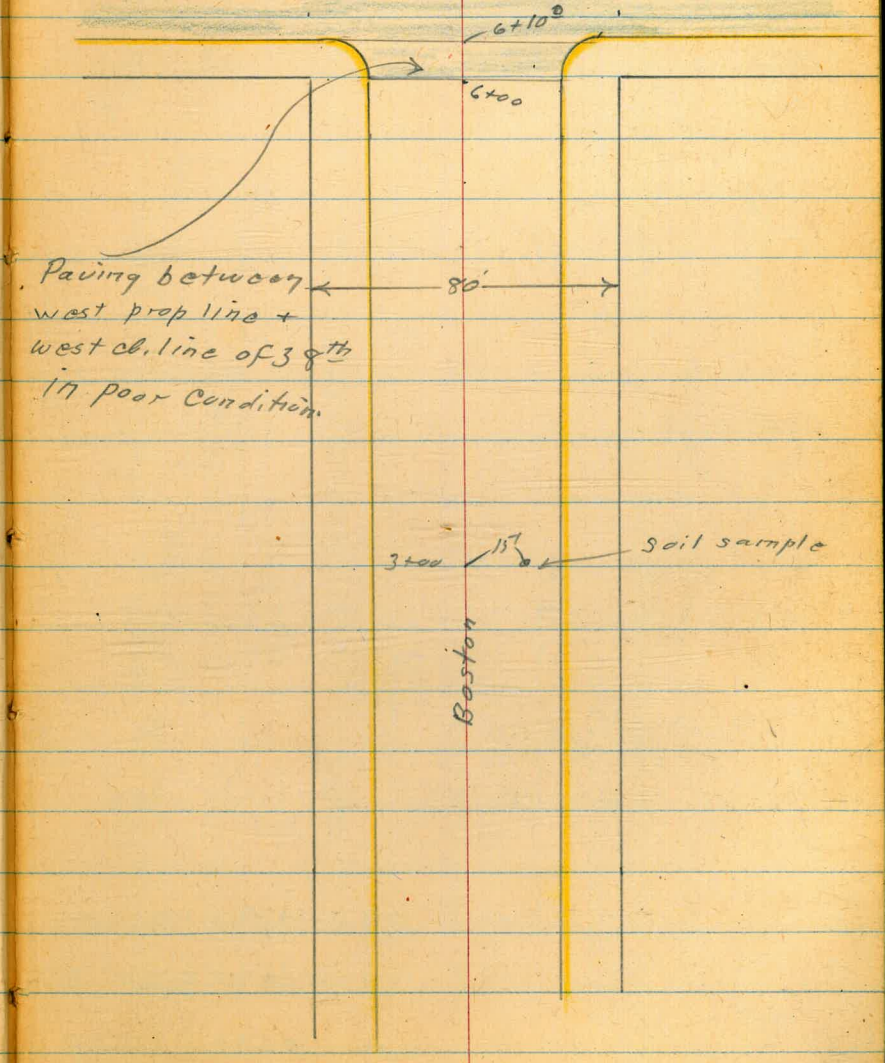
5/3/50

W.O. 31636

Levels - P. 42



38th St.



Boston

Levels 37th to 38th

	34.45	38.8	35.5	39.6	38.1	37.7	36.30
1+50	5.95 / 26 cl	6.6 / 26	5.9 / 17	5.8	6.7 / 13	7.7 / 26	7.10 / 26 cl
	36.34	38.0	38.1	38.6	37.5	36.7	37.05
1+25	7.06 / 26 cl	7.4 / 26	6.9 / 13	6.8	7.6 / 13	8.7 / 26	8.35 / 26 cl
	37.01	37.2	37.5	37.8	37.1	36.0	36.42
1+00	7.79 / 26 cl	8.2 / 26	7.6 / 13	7.6	8.3 / 13	9.4 / 26	8.98 / 26 cl
	36.72	36.1	36.3	36.2	35.9	34.8	35.45
0+50	8.68 / 25½ cl	9.3 / 25½	9.1 / 13	9.2	9.7 / 13	10.6 / 26	9.90 / 26½ cl
	35.92	36.3	36.1	34.6	34.5	33.6	34.50
0+00 = Ely line 37th	9.48 / 25½ cl	10.1 / 25½	10.3 / 13	10.6 / 45.40	10.9 / 13	11.6 / 26	10.90 / 26½ cl

(cl. = Top of curb)

25½ Lt. = cl. E.C.
26' Rt. = cl. E.C.

Set B.M.	10.92	45.40	8.83	34.48	B.M. #2
Set B.M.	0.44	43.31	7.03	42.87	= B.M. #1 =
National +37	3.01	49.90	—	46.89	S.W.B.P.

S.E. 7' L+T Boston +37th

S.E. 7' L+T. Newton +37th

Boston

℄

T.P. 12,21 68.68 0.30 56.47

3+50 ~~0.30 56.47~~

3+14 3 26'Lt = start curb

This curb broken out.

3+02 26'Lt = end curb

3+00

2+50

T.P. 12.08 56.77 0.71 44.69

2+00

1+75

54.97 54.4 54.7 54.5 54.3 53.4 54.02

1.80/26 cc | 2.4/26 | 2.1/13 | 2.0 | 2.5/13 | 3.4/26 | 2.75/26 cc

52.09

4.68/26 cc

51.11

5.66/26 cc

50.95 50.2 50.7 50.8 50.2 49.2 49.74

5.82/26 cc | 6.6/26 | 6.1/13 | 6.0 | 6.6/13 | 7.6/26 | 7.03/26 cc

46.91 46.1 46.6 46.5 46.0 45.3 45.95

9.86/26 cc | 10.7/26 | 10.2/13 | 10.3 | 10.8/13 | 11.5/26 | 10.79/26 cc

56.77

42.97 42.0 42.5 42.4 41.9 41.1 42.04

2.43/26 cc | 3.4/26 | 2.9/36 | 3.0 | 3.5/13 | 4.3/26 | 3.36/26 cc

41.05 40.3 40.8 40.5 40.1 39.2 40.09

4.35/26 cc | 5.1/26 | 4.6/17 | 4.6 | 5.3/13 | 6.2/26 | 5.31/26 cc

45.40

Boston

5+75				
5+50				
5+25				
T.P.	8.58	77.14	0.12	68.56
5+00				
4+50				
4+00				

71.62 | 70.8 | 71.0 | 71.3 | 71.0 | 70.6 | 71.20

5.52 / 26 cc | 6.3 / 26 | 6.1 / 13 | 5.8 | 6.1 / 13 | 6.5 / 26 | 5.94 / 26 cc

72.50 | 69.7 | 70.0 | 70.0 | 69.7 | 69.1 | 69.73

6.64 / 26 cc | 7.4 / 26 | 7.1 / 13 | 7.1 | 7.4 / 13 | 8.0 / 26 | 7.41 / 26 cc

69.90 | 68.3 | 68.5 | 68.3 | 67.9 | 67.4 | 68.05

8.24 / 26 cc | 8.8 / 26 | 8.6 / 13 | 8.6 | 9.2 / 13 | 9.7 / 26 | 9.14 / 26 cc

77.14

66.92 | 66.4 | 66.8 | 66.9 | 67.1 | 67.1 | 67.96

1.76 / 26 cc | 2.3 / 26 | 1.9 / 13 | 1.8 | 2.6 / 13 | 3.3 / 26 | 2.72 / 26 cc

62.95 | 62.1 | 62.8 | 63.0 | 62.4 | 61.3 | 61.96

5.73 / 26 cc | 6.6 / 26 | 5.9 / 13 | 5.7 | 6.3 / 13 | 7.4 / 26 | 6.72 / 26 cc

58.59 | 58.3 | 58.7 | 58.9 | 58.4 | 57.4 | 57.95

9.79 / 26 cc | 10.4 / 26 | 10.0 / 13 | 9.7 | 10.3 / 13 | 11.3 / 26 | 10.70 / 26 cc

68.68

Boston

6+10 Cont.

72.45 — 72.13 — 71.83 — 71.54 — 70.26 — 68.93 — 65.96

4.69/140 — 5.01/90 — 5.31/40 — 5.60/40 — 6.88/77 — 8.21/100 — 11.18/138

6+10 = Wly gutter 38th — Rods on Pave

71.53 — 71.72 — 71.74 — 71.73 — 71.69 — 71.59 — 71.62

5.31/36 — 5.42/26 — 5.40/13 — 5.41 — 5.45/13 — 5.55/26 — 5.52/36

6+10 Cont.

66.76

10.38/138

Rods on curb

= start of good pave.

6+10 = Wly. cb. line 38th

36' Rt. = E.C. 10' Rad cb. Ret.

73.05 — 72.60 — 72.29 — 72.25 — 72.33 — 72.33 — 71.07 — 69.76

4.14/140 — 4.54/90 — 4.85/40 — 4.86/36 cb. E.C. — 4.81/36 cc. E.C. — 4.81/40 — 6.07/77 — 7.38/100

Poor shape

This pavement thin. 1" to 1½"

(Return is flat.)

26' Rt. / 25' Lt. = B.C. 10' Rad cb. Ret.

6+00 = start A.C. Pave = Wly. Prop. line 38th

72.25 — 71.8 — 71.7 — 71.7 — 71.6 — 71.6 — 71.7 — 72.3X

4.86/25.9 cb — 5.3/26 G — 5.4/13 — 5.4 — 5.5/13 — 5.5/24 — 5.4/26 G — 4.80/26 cc

77.14

Boston

S.W. B.P. 37th & National

Orig. B.M.			7.88	0.04 / 46.85	(46.89)
T.P.	1.37	54.73	11.55	53.36	
T.P.	0.04	64.91	12.76	64.87 ✓	
S.E.B.P. 38th & National	1.19	77.63 ✓	3.48	76.44 ✓	(76.58)
T.P.	6.28	79.92	3.50	73.64 ✓	

6+40± Cont.

6+40± = ℄ 38th

℄

69.F3

7.31 / 100

66.80

10.34 / 138

72.62

73.20	72.95	72.50	72.74		72.42	72.23	71.18
3.94 / 140	4.19 / 90	4.34 / 40	4.40 / 26	4.52	4.72 / 26	4.91 / 40	5.96 / 77

77.14

37th St.
Levels
Z to National
Sketch P. 39

0 - 40 = Z St.

0 - 80

0 - 100

0 - 150

0 - 200

Set B.M.	5.30	31.36	9.50	26.06
B.M. #2 P. 42	1.08	35.56	—	34.48

24.6 / 6.8 / 170
26.3 / 5.1 / 130
25.9 / 5.5 / 30
24.7 / 6.7 / 15
25.7 / 5.7
25.4 / 6.0 / 15
26.3 / 5.1 / 80
26.8 / 4.6 / 80
26.5 / 4.9 / 110
24.2 / 7.2 / 170

24.3
7.1

23.7
7.7

22.7
9.1

24.1
10.3
31.36

N.W. 3' +10 back on 7' line 37th & Z streets

37th

℄

0+80 7 W walk sunken from here on.

0+80 6 W walk o.k. to here.

0+72 4 this point on curb on west sunken from curb o.k. to here

0+50

B.W. = back edge of walk.
w = edge of walk nearest curb
cb. = curb top
27 6 = back of walk
22 6 = start walk
20' Lt = start curb
27 5 Rt. = back of walk
22 7 Rt. = start walk
20' Rt. = start cb.

0+00 ℄ N. & line Z St.

27.94 27.63 27.72
3.42 3.73 3.64.
27 6 22 6 20
B.W. w cb.

27.86 27.74 27.72
3.50 3.62 3.64
27 6 22 6 20
B.W. w cb

27.78 27.67 27.64
3.58 3.69 3.72
27 6 22 6 20
B.W w cb

27.16 26.95 27.2 27.7 27.57 27.26 26.85
4.20 4.9 4.2 3.7 3.8 4.1 3.28
20 20 10 12 20 20
cb cb

26.4 26.3 26.08 27.05 27.3 27.5
5.0 5.1 5.28 4.31 4.1 3.9
40 30 27 6 27 6 30 40
B.W. B.W.

26.02 25.90 25.95 26.2 26.7 26.6 26.55 26.85 26.94
5.3A 5.46 5.9 5.2 4.7 4.8 4.9 4.51 4.42
22 6 20 20 10 13 20 20 1 W
W cb cb 22 7

31.36

37 H

4

1+29 3

29.16	25.60	28.66
2.20	2.76	2.70
27 E	22 E	20
B.W.	W	CC

1+21

28.94	28.58	28.49
2.42	2.78	2.87
27 E	22 E	20
B.W.	W	CC

1+12

28.65	28.37	28.32
2.71	2.99	3.04
27 E	22 E	20
B.W	W	CC

cont.

28.7	23.6	27.2	28.47
7.7	7.8	4.2	2.89
50	40	30	27 E
			B.W.

1+00

26.22	28.10	27.6	28.4	28.9	28.8	28.7	29.22
3.14	3.26	3.8	3.0	2.5	2.6	2.7	2.08
22 E	20	20	10		13	20	20
W	CC						CC

0+88 7

26.11	27.52	27.73
3.25	3.54	3.63
27 E	22 E	20
B.W.	W	CC

31.36

37th

T.P. 7.94 38.185. 0.45 30.91

1+50 = ± ℄ Alley to east.

1+45^{5}

Cont.

1+40^{5} = Face Alley cl. to east

1+38^{5} = B.C. 2° Rad cl, Ret.

1+37

℄

2.16 / 30 — 1.96 / 276 B.W.

29.16 29.11 29.0 29.8 30.0 30.1 29.5 29.9 30.4

2.20 / 22^{5} W — 2.25 / 20 cl — 2.4 / 20 — 1.6 / 10 — 1.4 — 1.3 / 10 — 1.6 / 20 — 1.5 / 30 — 1.0 / 120

29.39 29.08 29.98

1.97 / 27^{5} B.W. — 2.28 / 22^{5} W — 2.38 / 20 cl

27.2 27.9 29.2 29.36 34.5 34.4

4.2 / 50 — 3.5 / 35 — 2.2 / 30 — 2.00 / 27^{5} B.W. — 1.5 / 30 — 0.91 / 30 End cl.

29.04 28.90 28.8 29.5 29.7 29.8 29.6 29.9 30.27

2.32 / 22^{5} W — 2.46 / 20 cl — 2.6 / 20 — 1.9 / 7 — 1.7 — 1.6 / 10 — 1.8 / 20 — 1.5 / 22 — 1.09 / 22 E.C. 2° Ret. cl.

30.20

1.16 / 20 cl

29.26 25.90 25.80

2.10 / 27^{5} B.W. — 2.46 / 22^{5} W — 2.56 / 20 cl

31.36

37th

2+50

2+00

1+62.2 | 20' Rt. = E.C. 2° Rad. Rot.

1+60.3 = Start good walk + ch. on west

Cont

1+60.2 = Face ch. Alley to east
Also = End of poor walk + ch. on west
22' Rt. = ch. B.C. 2° Rot.

4

32.1 | 31.6 | 32.3 | 32.6 | 32.6 | 32.2 | 33.17

6.70 / 20 ch. | 7.2 / 20 | 6.5 / 10 | 6.2 | 6.2 / 10 | 6.6 / 20 | 5.68 / 20 CL

30.94 | 30.1 | 31.0 | 31.3 | 31.3 | 31.0 | 31.50

7.91 / 20 ch | 8.7 / 20 | 7.8 / 10 | 7.5 | 7.5 / 10 | 7.8 / 20 | 7.05 / 20 ch

30.83

8.02 / 20 ch

29.91 | 29.75 | 29.50

8.94 / 27.6 B.W. | 9.10 / 22.6 W | 9.35 / 20 ch

29.7 | 29.8 | 29.98 | 30.3 | 30.87

9.1 / 50 | 9.0 / 30 | 8.87 / 27.6 B.W. | 8.5 / 30 | 7.98 / 30 ch. end

29.69 | 29.50 | 29.3 | 29.9 | 30.2 | 30.3 | 29.9 | 30.1 | 30.89

9.16 / 22.6 W | 9.35 / 20 ch | 9.5 / 20 | 8.9 / 10 | 8.6 | 8.5 / 10 | 8.9 / 20 | 8.7 / 22 | 7.96 / 22 CB

38.85

37th

3+76.35

3+70.35 — 20' Rt. / 20' Lt. } = E.C. 10' cl. Ret.

Returns have straight grades.

3+66.35 — 30' Rt. = cl. Ret B.C.
30' Lt. = Cl. Ret. B.C. = end existing cl.

3+40.35 = ℄ Boston (unimproved street.)

30' Rt. = cl. Ret. E.C.
30' Lt. = End cl. Ret. = end existing cl.

3+14.35 = cl. line

Straight grade on Ret.

3+04.35 — 20' Lt. / 20' Rt. } = B.C. 10' Rad. cl. Ret.

3+00.35 = Sly. Boston

℄

35.04

3.81 / 20 E.C.

35.91

2.94 / 20 E.C.

34.89	34.1	34.1	34.4	35.0	35.2	35.1	35.2	35.94
3.96 / 30 cl.	4.7 / 30	4.7 / 20	4.0 / 10	3.8	3.6 / 10	3.7 / 20	3.6 / 30	2.91 / 30 cl.
29.6	30.7	32.7	33.4	34.2	34.6	34.7	34.7	34.8
9.2 / 150	8.1 / 90	5.1 / 30	4.9 / 20	4.6 / 10	4.2	4.1 / 10	4.1 / 20	4.0 / 30
33.53	33.3	33.2	33.7	34.0	34.1	33.7	33.6	34.53
5.32 / 30 cl.	5.5 / 30	5.6 / 20	5.1 / 10	4.8	4.7 / 10	5.1 / 20	5.0 / 30	4.32 / 30 cl. E.C.

33.55

5.30 / 20 cl.

34.36

4.49 / 20 cl.

33.57	32.7	33.4	33.7	33.7	33.3		34.30
5.28 / 20 cl.	6.1 / 20	5.4 / 10	5.1	5.1 / 10	5.5 / 20		4.55 / 20 cl.

38.85

37th

Alley cl. o.k.
Cont. good curb starts 22' Rt.

1+41 2 = Face curb - alley to east

Rebuild return.
1+39 20' Rt. = B.C. 2' Rad. alley Rot.

Curb broken here.
1+38 3 20' Rt. = End good curb.

T.P.	5.14	43.53	8.23	38.39
1+00				
T.P.	9.42	46.62	1.65	37.20
0+50				

start oil skim coat. N.G. do not consider

= 0+00
3+80 35 = Nly. line Boston

4

34.18 4.35 / 22 cl. o.k.
39.5 4.0 / 30
39.34 4.19 / 30 cl.

35.02 5.51 / 20 cl.
37.3 6.2 / 20
37.5 5.7 / 10
38.4 5.1
38.2 5.3 / 10
38.4 5.1 / 20
38.5 5.0 / 22
39.15 4.35 / 22 cl. E.C.

39.24 4.29 / 20 cl. No good

39.07 4.46 / 20 cl.

43.53

36.94 9.68 / 20 cl.
36.4 10.2 / 20
36.8 9.8 / 10
37.1 9.5
37.2 9.4 / 10
37.3 9.3 / 20
38.22 8.40 / 20 cl.

46.62

36.09 2.76 / 20 cl.
35.5 3.3 / 20
35.7 3.1 / 10
36.0 2.8
36.1 2.7 / 10
36.2 2.6 / 20
37.01 1.80 / 20 cl.

35.07 3.78 / 20 cl.
34.3 4.5 / 20
35.0 3.8 / 10
35.2 3.6
35.4 3.4 / 10
35.3 3.5 / 20
35.87 2.98 / 20 cl.

38.85

37th

2+50

2+00

1758' 20' Rt. = E.C. 2' alley return

Cont

1756' : Face alley ch. alley to east

1+49 = ℄ Alley to east ±

℄

40.46 — 3.07 / 20 ch.

39.7 — 3.8 / 20

40.1 — 3.4 / 10

40.5 — 3.0

40.7 — 2.8 / 10

40.5 — 2.7 / 20

41.72 — 1.81 / 20 cc

39.34 — 4.19 / 20 cc

38.6 — 4.9 / 20

39.0 — 4.5 / 10

39.2 — 4.3

39.5 — 4.0 / 10

39.6 — 3.9 / 20

40.54 — 2.99 / 20 cc

39.57 — 3.96 / 20 cc

39.62 — 3.91 / 22 cc B.C.

39.5 — 4.0 / 30

39.73 — 3.80 / 30 cc

38.40 — 5.13 / 20 cc

37.5 — 6.0 / 20

37.9 — 5.6 / 10

36.6 — 4.9

36.5 — 5.0 / 10

36.7 — 4.8 / 20

35.9 — 4.6 / 22

38.22 — 5.31 / 20 ch.

37.5 — 6.0 / 20

37.9 — 5.6 / 10

35.73 — 4.80 Rim M.H.

35.4 — 5.1 / 10

38.6 — 4.9 / 20

39.4 — 4.1 / 30

42.0 — 1.5 / 80

43.53

37th

22.3 Lt. = Face curb.
3+13.55 = S. line Newton to west

Cont.

21.9 Lt. = face of curb.
3+12 ℄ Sly. Cb line Newton to east

3+03.8 20' Lt. = B.C. 20' Rad. cb. Rot.

(Straight grade on Rot.)
3+02.6 20' Rt. = B.C. 10' Rad. cb. Rot.

T.P. BM #1. P.A2	4.43	47.31	0.65	42.88	(42.87)

2+98.62 = Sly line Newton to east.

℄

41.53
5.78
22.3
cb.

42.93
4.38
30
cb.
E.C.

46.72
1.11
80
gutter.

46.81
0.50
80
cb.

41.54
5.77
21.9
cb.

40.8
6.5
20

41.1
6.2
10

41.7
5.6

42.1
5.2
10

42.5
4.8
20

42.8
4.5
30

47.49
5.82
20
cb. B.C.

42.72
4.59
20
cb. B.C.

47.31

41.42
2.11
20
cb.

40.5
3.0
20

40.9
2.6
10

41.4
2.1

41.7
1.8
10

42.0
1.5
20

42.78
0.75
20
cb.

43.53

37 Th

22[6] Lt. = face curb (on Ref.)

3+63[55] N. Prop. line Newton to west

Cont.

3+53[8] - 39[6] Lt. = B.C. 20' Rad. Ch. Ret.

3+38[6] 3+38.62 = ℄ Newton to east.
3+38.55 = ℄ Newton to west

Cont

also - end existing ch.

3+23[8] 40' Lt. = end ch. Return

41.72

5.59
22[5]
ch

38.91 41.57

8.4 / 70

5.76
39[5]
ch

40.6	41.3	41.1	41.7	42.3	42.7	43.2	43.6
6.7 / 39[6]	6.0 / 30	6.12 / 20	5.16 / 10	5.0	4.6 / 10	4.1 / 20	3.7 / 30

37.2	41.0	41.0	41.5	42.1	42.6	43.1	43.7	44.7
11.1 / 130	6.3 / 30	6.3 / 20	5.18 / 10	5.2	4.7 / 10	4.12 / 20	3.9 / 30	0.6 / 100

38.9 41.44

8.4 / 70

5.87
40
ch

40.3	41.0	40.9	41.3	41.9	42.5	42.8	43.1
7.0 / 40	6.3 / 30	6.4 / 20	6.0 / 10	5.1	4.8 / 10	4.5 / 20	4.2 / 30

47.31

37th

4

1+00

0+50

= 0+00
3+78.62 } = N'ly. line Newton to East.

3+74.5 20' Rt. = E.C. 10' Rad. cl. Rot.

3+73.8 20' Lt. = E.C. 20' Rad. cl. Rot.

Cont.

3+64.5 30' Rt. = B.C. 10' Rad. Rot.
= Face N'ly. cl. Newton to east
22' Lt. = Face cl. on Rd.

43.21 | 43.1 | 43.5 | 43.8 | 43.9 | 44.2 | 44.84
4.10/20 in drive | 4.12/20 | 3.8/10 | 3.5 | 3.4/10 | 3.1/20 | 2.47/20 cc

42.68 | 42.4 | 42.6 | 43.0 | 43.1 | 43.2 | 44.03
4.63/20 cc | 4.9/20 | 4.5/10 | 4.3 | 4.2/10 | 4.1/20 | 3.28/20 cc

41.79 | 41.5 | 42.0 | 42.4 | 42.6 | 42.8 | 43.37
5.52/20 cc | 5.18/20 | 5.3/10 | 4.9 | 4.7/10 | 4.5/20 | 3.94/20 cc

43.43
3.88/20 cc. E.C.

41.76
5.55/20 cc E.C.

46.5 | 47.12
0.8/100 | 0.19/100 cc.

41.72 | 41.4 | 41.3 | 41.7 | 42.2 | 42.6 | 43.0 | 43.0 | 43.35
5.59/22.1 cc | 5.9/22.1 | 6.0/20 | 5.6/10 | 5.1 | 4.7/10 | 4.3/10 | 4.3/30 | 3.76/30 cc

47.31

37th

T.P.	5.95	52.30	0.96	46.35

1+59.3 20' Rt = E.C. 2' Rad. ob. Ret.

1+57.3 = Face N14 ob. Alley to east

1+49.4 = ℄ Alley to East ±

1+41.5 Face Sly ob. Alley to east

Rebuild return

1+39.5 20' Rt = B.C. 2' Rad. ob. ret. to alley

1+39.49 = end good curb
20' Rt = Break in ob.

℄

45.82
1.49
20
ob, E.C.

49.41	43.7	44.2	44.7	45.0	45.2	45.4	45.86	45.9	46.02
2.90/20 ob	3.6/20	3.1/10	2.6	2.3/10	2.1/20	1.9/22	1.45/22 ob bc	1.4/30	1.29/30 cc

44.29	43.6	44.1	44.6	44.9	45.2	45.5	47.9
3.02/20 ob	3.7/20	3.2/10	2.7	2.4/10	2.1/20	1.8/30	+0.6/100

44.21	43.6	44.0	44.5	44.8	45.0	45.1	45.57	45.5	45.71
3.10/20 ob	3.7/20	3.3/10	2.8	2.5/10	2.3/20	2.2/22	1.79/22 ob	1.8/30	1.60/30 cc

45.69
1.62
20
ob

45.51
1.80
20
ob

4331

37th

S.W.B.R. National + 37th
= Orig. B.M. - P - 42 5.40 46.90 (46.89)

3+12.8 = Sly curb line National

3+02.8 20' Lt. 20' Rt. } = B.C. 10' Rad. ch. Ret. (Returns on straight grade.)

2+98.79 start A.C. pave. = Sly line National

2+50

2+00

Notes Reduced - 5-6-50 - B.L.C.

45.16 44.42 46.94 46.12 46.46 46.76 47.20 47.46 48.04 49.15 49.62

7.14/80 cl. 7.88/80 G 5.36/30 cl. 6.18/30 G 6.04/20 5.54 5.10/20 4.84/30 G 4.26/30 cl. 3.15/80 G 2.68/80 cl.

44.96 5.32/20 cl. 46.24 6.06/20 G 47.20 5.10/20 G 47.94 4.36/20 cl.

46.89 5.41/20 cl. 46.30 6.00/20 G 46.53 5.47/10 47.16 5.14 47.28 5.02/10 47.24 5.06/20 G 47.97 4.33/20 cl.

45.97 6.33/20 cl. 45.30 7.0/20 45.6 6.7/10 45.9 6.4 46.0 6.3/10 46.4 5.9/20 47.14 5.16/20 cl.

45.09 2.21/20 cl. 44.3 8.0/20 44.9 7.4/10 45.2 7.1 45.3 7.0/10 45.6 6.7/20 46.36 5.94/20 cl.

52.30

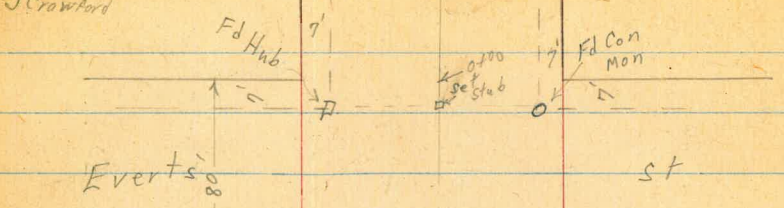
D. Smith
Wm. Fay
J. Crowford

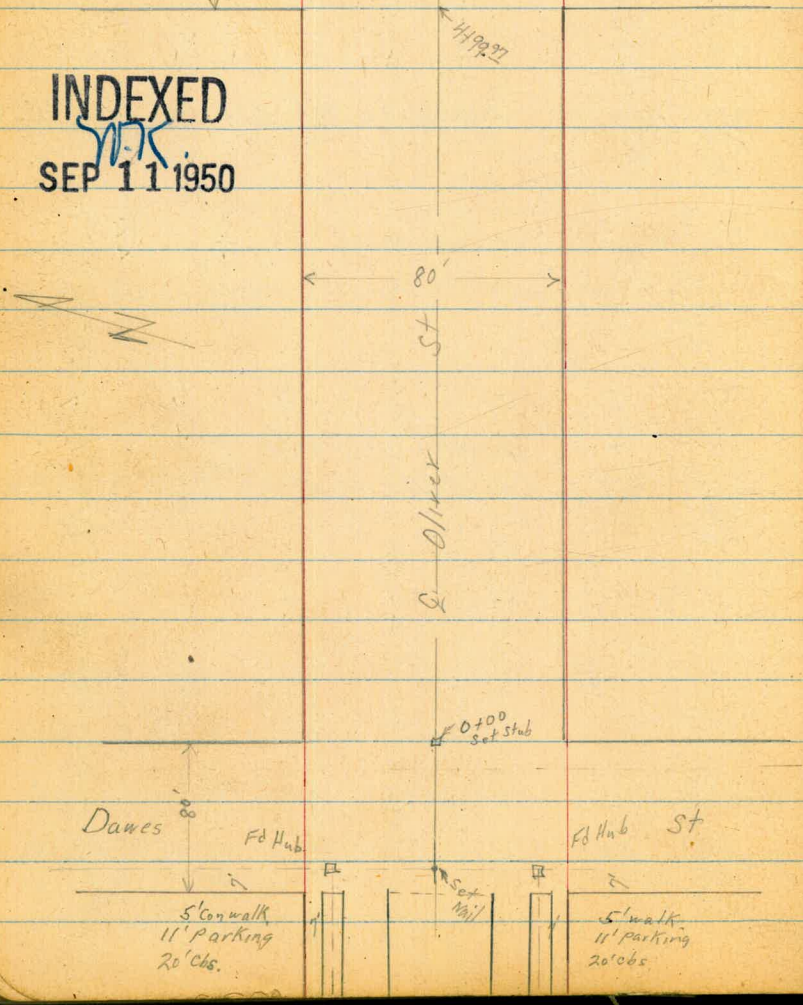
Cross Section Oliver St
Dawes to Fanuel

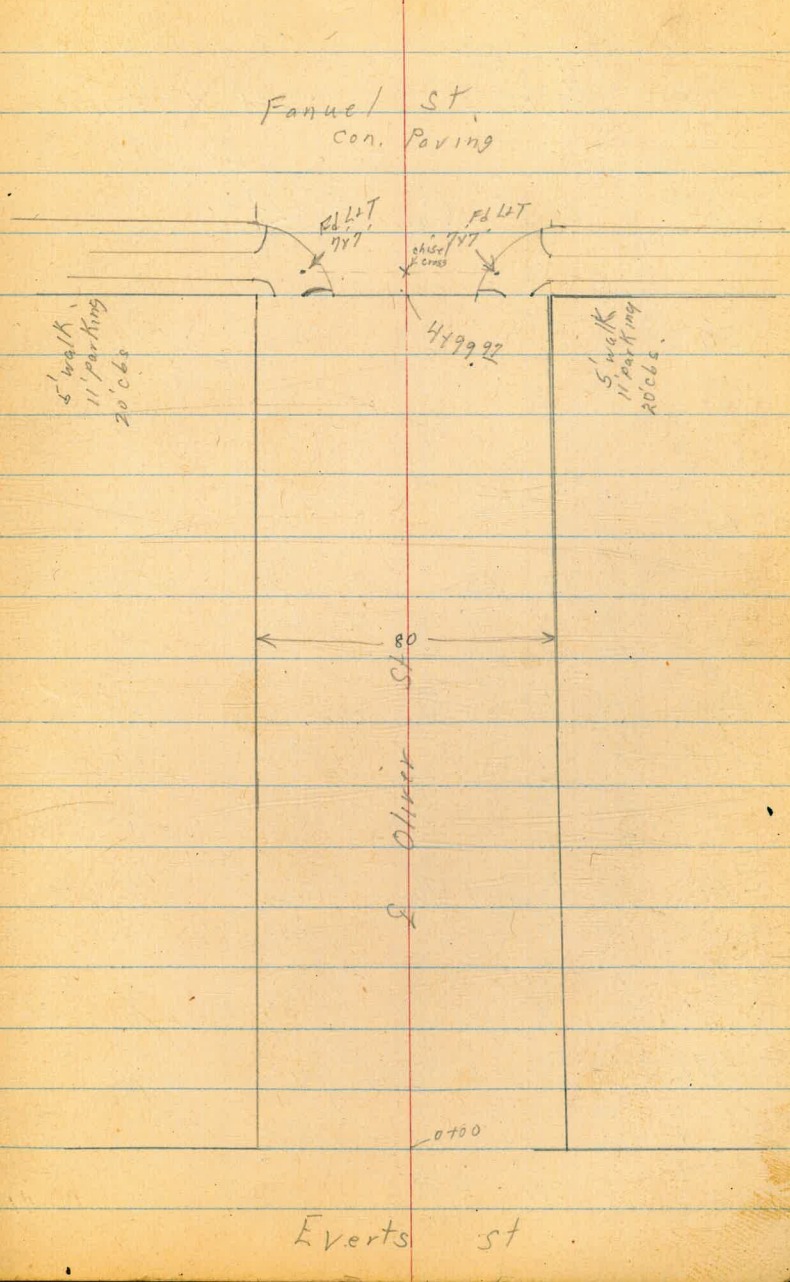
7-8-50

w.o. # 31847

60







D. Smith
Wm Fay
J. Crawford

X Section Oliver · Dawes to Fanuel

W.O.# 31847

N = Lt. ℄ S = Rt. 9-8-50

61

37° Rt.

0+00 Began 3' conc. walk ‖ to line

0-15 ℄ 6" Palm 28' Lt. ✓

0-20

0-25

0-40

0-60 W. curb line Dawes

0-79.3 End of exist. pave +Obs.

BM 5.99 8.97 2.98

NW 1' Hub Dawes & Oliver FB# 1871-47 Dayt

Walk T.C. end. Gut.

Gut. T.C. end Walk

8.97

Lt. = N. ℄ Rt. = S

0+80 40° Rt. ℄ 2½' Conc. Walk

0+74 23⁸ Lt. End of 2' Wire fence

0+59 20² Rt. ℄ 7' Conc. Drive

24⁵ Lt.
0+50 End of Pickett fence - Begin wire fence
39° Lt. ℄ 12" Pepper tree ✓

0+41 20³ Rt. ℄ 10' Conc. Drive

0+25 24⁵ Lt. Begin 3' Pickett fence

0+20 40° Rt. ℄ 2½' Conc. walk

0+06 21¹ Rt. ℄ fire hydrant

8 97/2

5.2 4.4 4.2 4.0 4.0 4.1 3.33 3.32
3⁸ 4⁶ 4⁸ 5° 5° 4⁹ 5⁶⁴ 5⁶⁵
40 20 10 14 16 37 40
walk walk

3.75 3.23
5²² 5⁶⁴
20³ 40°

3.73 3.28
5²⁴ 5⁶⁹
20² 40°

3.50 3.48
5⁴⁷ 5⁴⁹
40° 50

3.42 3.40
5⁵⁵ 5⁵⁷
40 50
walk walk

8 97

Lt. = N ℄ Rt. = S

1+96 39.9 Rt. ℄ 7' Conc. Drive

1+91 25.5 Lt. ℄ 30" Pine tree ✓

1+71 35.4 Lt. ℄ 3' Conc. walk

1+67 40.0 Rt. ℄ 3' Conc. walk

1+60 25.4 Lt. ℄ 2" Pine tree ✓

1+50 22.6 Lt. End of NS. Fence

1+12 26.4 Lt. ℄ 2" Eugenia tree ✓

1+07 37.0 Lt. ℄ 3' Conc. walk

1+00 37.0 Rt. End of 3' Conc. walk
11 to line

8 9.7 / 2

							4.91	4.80
							4.06	4.17
							39.9	50.0
		6.47	4.29					
		2.50	2.68					
		40.0	35.4					
							4.54	4.51
							48.3	44.6
							40.0	50.0
5.8	5.1	4.9	4.8	4.7	4.7	4.1		
32.0	39.0	41.0	42.0	43.0	46.0	49.0		
40	20	10		10	20	40		
3.84	3.32							
40.0 Conc.	37.0	4.7	4.4	4.3	4.1	3.9	3.61	3.67
35.5	43.3	46.0	47.0	49.0	51.0	536.0	535.0	
40	20	10		10	20	37.0	40.0	

8 9.7

Lt. = N. ℄ Rt. = S

TP 9 35 16 54 17 8 7 19

2+68 39 8 Rt. ℄ 3' Conc. walk
27 3 Lt. ℄ 18" Pine tree

2+57 28 6 Rt. ℄ 4" Palm

2+56 27 2 Lt. ℄ 3" Flaming Eucalyptus tree

2+50

2+47 36 3 Lt. ℄ 4" Conc. 2½' walk

2+21 40 1 Rt. ℄ 3' conc. walk

2+04 36 2 Lt. ℄ 3' Conc. Walk

2+00

8 97

6.95 6.87
2 02 2 10
39 8 50 0

7.57 6.9 6.4 6.4 6.4 6.5 6.4
1 5 2 1 2 4 2 6 2 5 2 5 2 6
40 20 10 10 20 40

7.67 7.60
1 30 1 37
40 0 36 3

3 63 3 68
40 1 50

6.47 6.40
2 50 2 57
40 0 36 2

6.4 5.7 5.6 5.6 5.5 5.4 5.1
2 6 3 3 3 4 3 4 3 5 3 6 3 9
40 20 10 10 20 40

8 97

Lt. = N. ℄ Rt. = S 65

3+43	24 Lt. ℄ 18" Pine tree ✓								
3+40	39° Rt. ℄ 8' conc. drive								
3+21	45° Rt. ℄ 3½' Conc. Walk								
3+18	36° Lt. ℄ 3' Conc. walk								
3+13	25' Lt. ℄ 30" Pine tree ✓								
3+00		9.0	8.5	7.7	7.5	7.4	7.5	7.6	7.5
		7.5	8.0	8.8	9.0	9.1	9.0	8.9	9.0
		40	22	20	10		10	20	40
2+99	26° Lt. ℄ 18" Pine tree ✓								
2+93	39 Rt. ℄ 6" wide 2' Ribbon Drive	9.04	8.84					7.19	7.04
2+81	35 Lt. ℄ 3' Conc. walk	7.5	7.20					9.35	9.50
		50°	35					39	30°
	16 54								16 54

8.52 8.58
8.02 7.96
39° 50°
7.94 8.02
8.60 8.52
45° 50°

9.54 9.48
7.00 7.06
40° 36°

Lt. = N ℄ Rt. = S

4 + 31 $25^{3}_{=}$ Lt. ℄ 12" Palm ✓

4 + 12 $35^{5}_{=}$ Rt. ℄ $6\frac{1}{2}$' Ribbon drive

4 + 09 $34^{5}_{=}$ Lt. ℄ 15" Palm ✓

4 + 00

3 + 89 $24^{5}_{=}$ Lt. ℄ 30" Pine tree ✓

3 + 84 $34^{8}_{=}$ Rt. ℄ $2\frac{1}{2}$' conc. walk

3 + 83 $35^{4}_{=}$ Lt. ℄ 3' Conc. walk

3 + 63 $24^{5}_{=}$ Lt. ℄ 2' Pine tree ✓

3 + 50 $35^{7}_{=}$ Rt. N.S. Lath fence

$16\frac{54}{3}$

10.39 10.37
$6^{15}_{=}$ $6^{17}_{=}$
$35^{5}_{=}$ $40^{0}_{=}$

10.9 10.5 10.3 10.2 10.2 10.5 10.0
$5^{6}_{=}$ $6^{0}_{=}$ $6^{2}_{=}$ $6^{3}_{=}$ $6^{3}_{=}$ $6^{0}_{=}$ $6^{5}_{=}$
40 20 10 10 20 40

9.57 9.63
$6^{95}_{=}$ $6^{91}_{=}$
$34^{8}_{=}$ $40^{0}_{=}$

11.12 10.94
$5^{92}_{=}$ $5^{60}_{=}$
$50^{0}_{=}$ $35^{9}_{=}$

10.0 9.5 9.1 8.8 8.7 9.0 9.1 8.6
$6^{5}_{=}$ $7^{0}_{=}$ $7^{4}_{=}$ $7^{7}_{=}$ $7^{8}_{=}$ $7^{5}_{=}$ $7^{4}_{=}$ $7^{9}_{=}$
40 22 18 10 20 40

$16\frac{54}{}$

Lt. = N ℄ Rt. = S

4+99 25.5 Lt. ℄ 2" Palm ✓
26.0 Rt. ℄ 8" Flaming Eucly. ✓

4+84 26.0 Rt. ℄ 6" Flaming Eucly. ✓

4+78 25.8 Lt. ℄ 2" tree ✓

4+69 22.9 Rt. ℄ 3' conc. & brick walk

6.27 1947

T.B.M. SE 7' Mon. Everts & Oliver St. 3 34 13 20

4+56 26.0 Rt. ℄ 6" Acacia tree ✓

4+50 25.3 Lt. ℄ 15" Palm ✓ Lath
29.3 Rt. End of N S fence

4+34.1 34.5 Rt. ℄ 3' Conc. walk

16 54

1947

	11.1	11.6	11.3	11.4	11.5	11.2	11.7	12.4
	5.4	4.1	5.2	5.1	5.0	5.3	4.8	4.1
	40	20	10		10	20	22	40

	12.05	11.82
	7.42	7.65
	22.9	40

	10.96	10.90
	5.58	5.64
	34.1	40

16 54

0+20 25' Lt. ℄ 3" Torrey Pine ✓

0+05 21' Rt ℄ Standard fire Hyd. ✓

0+01 25' Lt. ℄ 3" Torrey Pine ✓

0+00 E Line Everts

5+60

5+40 ℄ Everts

5+20

4+99.97 W. Line Everts

1947

4. = N ℄ Rt. = 5.

15.8	15.5	15.1	14.3	14.5	14.4	14.1	14.7	14.0	13.0
3 7	4 0	4 4	5 2	5 0	5 1	5 4	4 8	5 5	6 5
90	40	25	20	10		14	20	40	90
15.5	14.7	13.9	13.9	13.9	14.1	13.7	14.0	13.7	12.9
4 0	4 8	5 6	5 6	5 6	5 4	5 8	5 5	5 9	6 6
90	40	25	20	10		14	20	40	90
14.8	14.0	13.7	13.6	13.6	13.4	12.8	13.0	12.0	
4 7	5 5	5 8	5 9	5 9	6 1	6 6	6 15	7 5	
90	40	20	10		10	20	40	90	
15.5	13.8	13.1	13.1	13.1	13.2	12.8	12.6	11.7	
4 9	5 7	6 4	6 4	6 4	6 3	6 7	6 9	7 8	
90	40	20	10		10	20	40	90	
14.5	13.2	12.8	12.5	12.5	12.6	12.5	12.6	12.6	11.5
5 0	6 3	6 7	7 0	7 0	6 9	7 0	6 9	6 9	8 0
90	40	22	20	10		10	20	40	90

1947

1+60 $39^{\frac{1}{2}}$ Lt. & 7' Conc. drive 2' Ribbons

1+50

1+19 $40^{\frac{0}{0}}$ Rt. & 3' Conc walk

1+00

0+50 $25^{\frac{6}{0}}$ Lt. & 4" Torrey Pine ✓

0+41 $40^{\frac{0}{0}}$ Lt. & 7' Conc. Drive 2' wide Ribbons

0+35 $25^{\frac{3}{0}}$ Lt. & 3" Torrey Pine ✓

0+25 $34^{\frac{6}{0}}$ Lt. & 2½' Conc. Walk

1947

Lt. = N & Rt. = S

18.39 18.29
108 118
50 $39^{\frac{2}{0}}$

18.1 17.5 17.0 17.2 17.2 17.3 17.1 16.8
14 20 25 23 22 21 29 27
40 20 16 10 10 20 40

16.25 16.18
322 329
40 50

17.2 17.1 16.3 16.5 16.5 16.5 16.1 15.7
23 24 32 29 30 30 37 36
40 20 16 10 10 20 40

16.1 16.0 15.0 15.5 15.4 15.5 15.0 15.4 15.1
34 35 45 40 39 40 45 41 44
40 24 20 10 10 20 22 40

16.92 15.89
355 358
50 40

15.97 15.94
350 353
40 346

1947

2+50				
2+45	40' Rt. ℄ 3' Conc. Walk			
2+19	39.8 Lt. ℄ 3' Conc. Walk			
2+16	43° Rt. ℄ 9' Conc. Drive			
TP	6.80	25.46	0.81	18.66
2+00				
1+99	40° Rt.	3' Conc. Walk		
1+80	38.7 Lt. ℄ 3' Conc. Walk			

19 47

Lt. ℄ Rt.

19.2 18.7 18.2 18.3 18.4 18.2 18.1 17.7

6.2 6.8 7.3 7.2 7.1 7.3 7.4 7.8

20 18 10 10 20 40

17.72 17.66

7.4 7.8.0

40' 50°

19.09 18.81

6.37 6.65

50° 39.8

17.53 16.38

7.93 8.08

43° 50°

25.46

18.8 19.1 17.6 17.8 17.9 17.8 17.4 17.4

0.7 1.4 1.9 1.7 1.6 1.7 2.1 2.1

40° 20° 16° 10° 20° 40°

18.55 17.45

1.92 2.02

40° 50°

18.96 18.65

0.51 0.82

47° 38.7

19 47

4 + 25 — 38.3 Lt. ℄ 3' Brick walk

4 + 03 — 40.3 Rt. ℄ 3' Conc. Walk

4 + 00

3 + 79 — 40.0 Lt. ℄ 3' Conc. Walk

3 + 50

3 + 19 — 40.2 Rt. ℄ 8' Conc. Drive

3 + 18 — 40.0 Lt. ℄ 2½' Conc. Walk

3 + 00

2 + 95 — 40.3 Rt. ℄ 3' Conc. Walk

Lt. ℄ Rt.

21.52 21.41 19.29 19.65 19.45

39.4 40.5 6.17 5.81 6.01
38.3 83.5 40.3 50.0

20.8 20.6 19.8 19.9 19.9 19.8 19.6 19.5

4.6 4.8 5.7 5.6 5.6 6.7 5.9 6.0
40 25 20 10 10 20 40

20.89 20.73

4.57 4.73
50.0 40.0

20.5 20.1 19.5 19.4 19.5 19.4 19.3 18.9

5.0 5.4 6.0 6.1 6.0 6.1 6.2 6.6
40 30 20 10 10 20 40.0

19.89 19.68

6.57 6.78
40.2 50.0

20.10 19.82

5.30 5.64
60.0

19.8 19.3 18.7 18.7 18.8 18.7 19.1 18.3

5.7 6.2 6.8 6.8 6.7 6.8 6.4 7.2
40 20 19 10 10 20 40

18.43 18.20

7.03 7.26
40.3 48.0

25-46

Lt. ℄ Rt.

5+20 W. Gutter Line

4+99 97 E. Line of Fence / & Edge of Conc. Pave. & Curb

4+75

4+53 40 1/2 Rt. ℄ 6' Conc. Drive 2' Ribbons

4+50

21.55 20.96 20.84 20.18 20.08 19.64 19.27 19.94 19.61 18.07 19.68

3 91 4 50 4 62 5 28 5 38 5 82 6 19 6 52 5 85 7 38 6 78

90 90 T. Curb 40 40 20 20 40 40 90 90

Curb Top Gut Gut Gut Top Curb Gut Curb

4 2 / 40

21.00 20.92 20.83 20.22 20.18 19.99 19.68 19.36 19.89 19.84 19.11

4 46 4 54 4 63 5 24 5 28 5 47 5 78 6 10 5 57 5 62 5 65

36 31 20 20 10 10 20 20 31 36

Walk Walk T. Curb Gut. Gut T. Curb Walk Walk

5 1 / 40

22.2 21.2 20.4 20.5 20.4 20.4 20.9 20.5

3 3 4 3 5 1 5 0 5 1 5 1 4 6 5 0

40 24 18 10 10 20 40

20.48 20.47

4 98 4 99

40 1 50

21.9 21.3 20.1 20.3 20.3 20.2 20.3 20.7

3 6 4 2 5 1 5 2 5 2 5 3 5 2 4 8

40 25 20 10 10 20 40

205 46

BM 4 57 20 89 NW BP Fanuel & Oliver 21 02

S.W. Return Fanuel & Oliver

5 parts 6.3 ea 31.5 Length 20' Rad.

BC. Oliver	5 57 C6	6 10 Cut
1/5	5 56	6 10
2/5	5 57	6 19
3/4	5 65	6 27
4/5	5 76	6 42
EC. Fanuel	5 85 C6	6 52 Cut
	25 46	

NW Return Fanuel & Oliver

5 parts 6.3 ea 31.5 Length 20' Rad.

	5 20.22	
4 63 20.83 C6	5 24 Cut	
4 74 20.72	5 29 20.17	
4 72 20.74	5 34 20.12	
4 66 20.80	5 33 20.13	
4 66 20.80	5 28 20.18	
4 62 20.84	5 28 20.18	
	25 46	

Cross Section Alley Block 12
La Jolla Strand.
From Palomar St to Rosemont St.

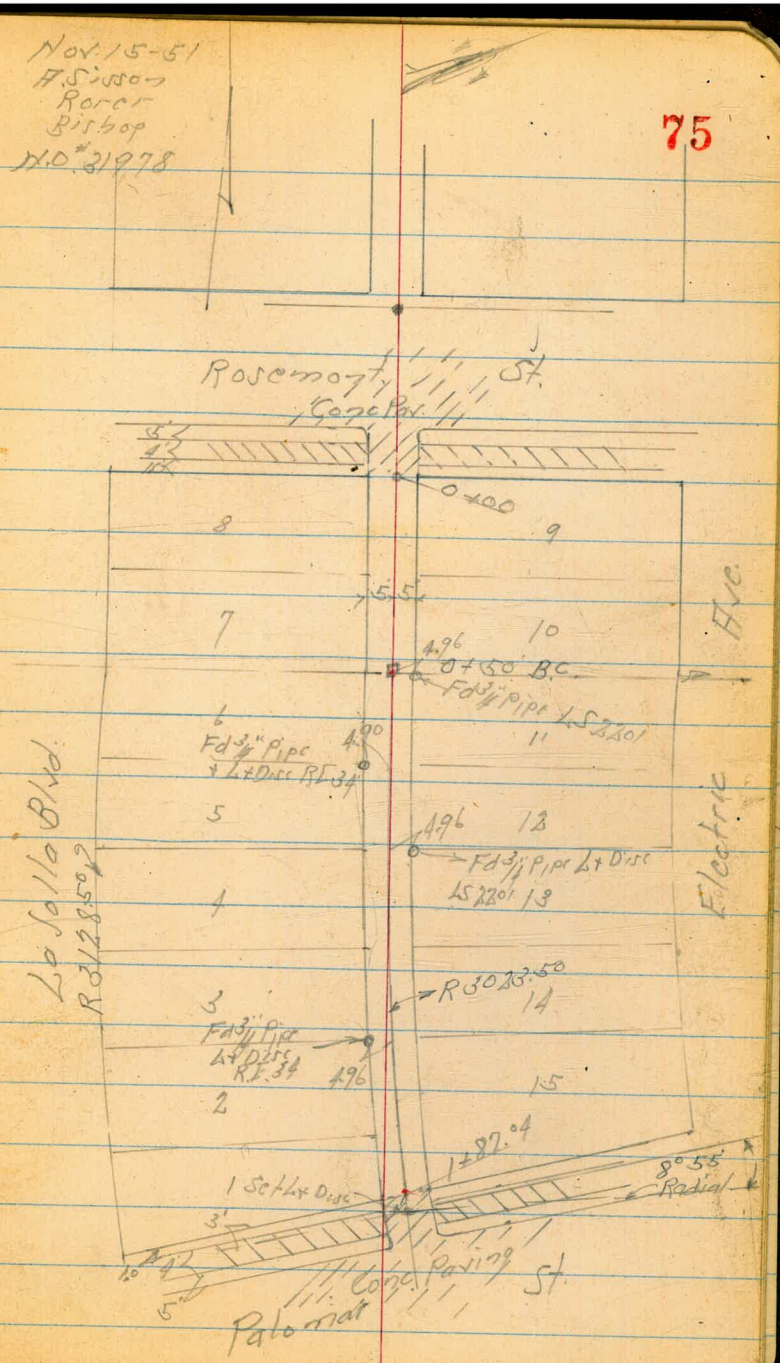
Levels next page

INDEXED
NOV 16 1951

Nov. 15-51
H. Sisson
Rodd
Bishop
No. 21978

75

Note Redrawn
Fisher
11-26-51



Alley Block 12 La Solla Strand.

Lt. ℄ ℄ Rt. W

1

TP	2.98	88.20	1.32	85.22	
+50	= B.C.Lt.	5.4 Lt. of ℄ = Sly Picket + Hly Board			Fence
+47		50' Rt. of ℄ = Hly Picket Fence			
+25					
+10					
+04		5.7' Lt. of ℄ = Hly Picket Fence			
0+0	= South Line				
0-10	= South Curb Line Rosemont				
B.M	5.74	89.54	82.80	S.E. BP Rosemont + Electric	

85.7 / 85.7 / 85.4 / 85.0

3.8 G / 2.8 / 4.1 G / 4.5 A.C.

86.1 / 85.5 / 85.5 / 85.6 / 85.6

3.4 G / 4.0 G / 4.0 / 3.9 G / 3.9 A.C.

86.3 / 85.9 / 85.1 / 85.2 / 84.9 / 84.6

3.2 A.C. / 3.6 G / 4.4 / 4.3 / 4.6 G / 4.9 A.C.

86.0 / 84.4 / 84.0 / 84.0 / 83.4

3.5 G / 5.1 G / 5.5 / 5.5 G / 6.1 A.C.

82.57 / 82.36 / 82.9 / 82.02 / 82.32 / 82.44

4.7 G: Top Curb / 7.8 G: Conc Pav. / 8.0 Dirt / 7.52 Conc Pav / 7.32 G: Conc Pav. / 7.0 G: BP

82.31 / 81.77 / 79.18 / 81.52 / 82.14

7.4 G: Top Curb / 7.7 G: Gut. / 7.8 Conc Pavings / 8.03 G: Gutter / 7.4 G: Top Curb

89.54

Lt. ℄ Rt.

+43 = ℄ 8' A.C. Drive on Rt.

+25

1+02

+90 = ℄ 8' Conc. Drive on Lt.

+85.5 55' Rt of ℄ - 5' Ly Board Fence

+75

+74.5 5' Rt of ℄ - 5' Ly Picket Fence

0+74

88.20

84.4 / 84.2 / 83.7 / 83.73 / 83.62 / 83.18

3.8 / 4.0 / 4.5 / 4.47 / 4.58 / 5.02

7.3 - Fly Garage / 6.2 - Fly 8" Conc. Drive / 5.0 - Fly 8" Conc.

79.8 / 84.1 / 84.3 / 83.4

3.6 / 3.8 / 3.9 / 4.8

103.5 Fly Bldg.

85.2 / 84.7 / 84.3 / 84.4 / 83.25 / 83.20

3.0 / 3.5 / 3.7 / 3.8 / 4.95 / 5.09

10.4 - Fly Bldg. / 5.5 - Fly Wall Conc.

84.0 / 85.1

2.16 / 3.03

19.8 - Fly Conc. Floor / 4.7 - Fly 8" Conc. Drive

85.2 / 84.9 / 83.53 / 83.50

3.0 / 3.1 / 3.3 / 4.67 / 4.70

6.1 - Fly Concrete / 4.9 - Conc. Wall

85.2 / 85.1 / 85.0 / 85.3

3.0 / 3.1 / 3.2 / 2.9

88.20 ✓

BM 478 78.47 ✓ REBP Palomar La Jolla Blvd 78.48

+97.2 = North Curb Line Palomar

+87.04 = North Line of Paving

+85

TP 400 85.25 6.95 81.25

+65

1+50

88.20

80.90 80.29 80.09 79.96 80.56

4.85 4.96 5.16 5.99 4.69

9.4-CL 9.2-Gut 10.2-Gut 10.6-CL

81.10 80.85 80.69 80.84 80.88

4.45 4.10 4.56 4.41 4.37

5.1-CL 5.1-Gut 5.1-Gut 5.1-CL

81.2 81.1 81.51 82.9

4.1 4.2 3.8 2.4

5 5 5 5

85.25

84.1 83.3 83.1 83.4 83.3 83.1

4.1 4.7 5.1 4.8 4.7 5.1

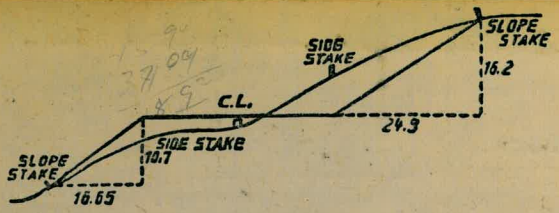
5 5 5 5 5 13.3: Fly Shimla House

45.03

3.17

74: S.W. Cor. Garage Concrete Floor South Entrance

88.20



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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